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# Non-Hermitian control of Hermitian waveguide arrays

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# Introduction

 Dynamical control of wave propagation in optical lattices
 execution

 of optical optical optical lattices
 execution

<u>Optical waveguides' arrays</u> beam propagates under the influence of a spatially periodic, refractive index distribution

<u>in our case</u>, wave dynamics approximated considering only amplitude/phase of each individual waveguide, simulating dynamical behavior, <u>characteristic of discrete systems</u>

### Objective

Device under investigation: array of optical waveguides with embedded, active, nonlinear elements



Analysis performed by following 3 primary steps: theoretical background of wave propagation in individual elements verification through numerical analysis in the aforementioned elements numerical analysis on the device under investigation

## **Coupled mode theory**



assumptions

$$i\frac{dA_n}{dz} + \beta A_n + \kappa (A_{n+1} + A_{n-1}) + \gamma_n |A_n|^2 A_n = 0$$

### Hermitian lattice dynamics

Linear waveguide array (γ<sub>n</sub>=0)

• plane wave:

$$E_n(z) = \varphi_n e^{ink_x D} e^{ik_z z}$$



$$k_z = \beta + 2\kappa \cos(k_x D)$$

DNLS

<u>1D waveguide array</u> <u>dispersion relation</u> . <u>phonon-like behaviour</u>



### non-Hermitian dimer dynamics

Asymmetric, nonlinear, active coupler:

$$\frac{dA_1}{dz} = i(\beta_1 + i\alpha_1)A_1 + i\gamma(|A_1|^2 + \sigma|A_2|^2)A_1 + i\kappa A_2$$
$$\frac{dA_2}{dz} = i(\beta_2 + i\alpha_2)A_2 + i\gamma(|A_2|^2 + \sigma|A_1|^2)A_2 + i\kappa A_1$$



Steady states: Nonlinear Supermodes (NS)

2 supported NS:

$$A_j = |A_j| exp(i(bz + \varphi_j))$$

with:

$$|A_1|^2 = \frac{\beta_1 \alpha (\beta - 1) + \kappa \sqrt{\alpha (\alpha - 1) \cos \varphi}}{\gamma (1 - \sigma) (\alpha - 1)}$$
$$|A_2|^2 = \frac{1}{\alpha} |A_1|^2$$

#### where:

$$b = \frac{1}{2} \left[ \beta_1(\beta + 1) + \kappa \frac{\alpha + 1}{\sqrt{\alpha}} \cos\varphi + \gamma(\sigma + 1) \frac{\alpha + 1}{\alpha} |A_1|^2 \right]$$
  

$$sin\varphi = \frac{|\alpha_1|\sqrt{\alpha}}{\kappa}$$
  

$$\alpha \equiv -\alpha_2/\alpha_1$$
  

$$\beta \equiv \beta_2/\beta_1$$

e.g.  $a_1=1$ ,  $a_2=-0.25$ ,  $\beta_1=1$ ,  $\beta_2=2$ ,  $\gamma=-1$ ,  $\sigma=0$ ,  $\kappa=0.5$ 





γ=-1, σ=0, κ<sub>d</sub>=0.5

### Model

Coupled mode equations under the assumption of nearest neigbour coupling:

 $\frac{dA_n}{dz} = i\left((\beta_n + i\alpha_n)A_n + \kappa_{n+1}A_{n+1} + \kappa_{n-1}A_{n-1} + \gamma_n A_n |A_n|^2\right)$ 

 discrete array of linear, passive waveguides (γ<sub>n</sub>=0, α<sub>n</sub>=0, without loss of generality β<sub>n</sub>=0)

- asymmetric, active dimer, with self-defocusing nonlinearity ( $\gamma_{N/2}=\gamma_{N/2+1}=-1$ )
- we investigate wave propagation by variating array's parameters,  $\alpha_1$ ,  $\alpha_2$ ,  $\beta_1$ ,  $\beta_2$ ,  $\kappa_1$ ,  $\kappa_d$
- evaluating array's properties, with the dimer acting as a scatterer, an input/output device and a detector
- scattered beam discrete gaussian with initial amplitude profile:

$$f(n, z = 0) = \frac{1}{\sigma\sqrt{2\pi}} exp\left(ik(n - n_i) - \frac{(n - n_i)^2}{2\sigma^2}\right)$$

Plane wave

**greed** approximation for a sufficiently wide gaussian beam

 $A_n = exp(ikn - i\beta z) + Rexp(-ikn - i\beta z), \ n \le 0$ 

 $A_n = Texp(ikn - i\beta z), n \ge 1$ reflection/transmission coefficients for the linear case (dimer switched off)







#### Zero reflection (geometrically dissimilar dimer (b<sub>1</sub>/b<sub>2</sub>=1)): gaussian wavepacket simulation





 $a_1 = -0.124$   $a_2 = 0.548$   $\kappa_1 = 0.300$   $\kappa_d = 0.927$  $b_1 = 0.5$   $b_2 = 1$ 

<u>Zero reflection</u> (geometrically identical waveguides (b<sub>n</sub>=0)): gaussian wavepacket simulation

#### PW calculated parameters





#### Symmetrical reflection:

#### PW calculated parameters





100

n

150 0

Ζ

 $a_1 = -0.100$   $a_2 = 3.43$   $\kappa_1 = 0.500$   $\kappa_d = 0.795$   $b_1 = 0.1$  $b_2 = 1$ 

#### **Reflection equal to transmission:**

#### PW calculated parameters



#### **Reflection equal to trransmission:**

gaussian wavepacket simulation



#### Nonlinear scattering (dimer on):

gaussian wavepacket simulation

 $a_1=1, a_2=-0.05$   $\kappa_d=0.45, \kappa_l=0.5$  $b_1=1, b_2=6$ 





 $\frac{\text{Dimer on}}{|R_L|^2 = 0.21} \\ |T_L|^2 = 0.10 \\ |R_R|^2 = 0.86 \\ |T_R|^2 = 0.12 \end{aligned}$ 

<u>Input/output device:</u>

**Isolated dimer:** 



test for different initial conditions (IC) i.e. input in loss/gain/both dimer's waveguides

taking advantage of different convergence speed to final state (NS)





But....





Treating infinities:



stabilizing through coupling with the linear lattice (κ₁≠0)

e.g.  $a_1=1$ ,  $a_2=-0.25$ ,  $b_1=1$ ,  $b_2=2$ ,  $\kappa_d=0.5$ ,  $P_0=1$ 



#### But....







KI =0.5

#### Array as a detector:

200

n

0

Ζ

#### e.g. $a_1=1$ , $a_2=-0.08$ , $b_1=1$ , $b_2=3$ , $\kappa_l=0.35$ , $\kappa_d=0.3$



200

n

0

Ζ

### Conclusions

#### In total, embedding an active, nonlinear, asymmetric dimer in a waveguide array:

- i. offers the ability to adjust asymmetric scattering of beams
- ii. offers the ability to adjust power output during dimer excitation by controlling IC, gain/loss and  $\kappa_d$
- iii. has a stabilizing effect on propagating waveforms
- iv. can be used for detection of propagating waves

Dimer controls scattering properties

Lattice modifies dimer dynamics

# The End

# Thank you for your attention!