Analysis of Thermal Grooving Effects on Vortex Penetration in Vapor-Diffused Nb₃Sn

Based on our recent work:

<https://arxiv.org/abs/2409.01569>

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Performance of vapor-diffused Nb3Sn grown on Nb

- 1.3/1.5 GHz single-cell cavities can attain an accelerating gradient over 20MV/m with $Q \sim 10^{10}$.
- Cavities of various frequencies (650 MHz, 952 MHz, 2.6 GHz, 3.6 GHz) coated at different facilities show comparable performance.

- 1.5 GHz five-cell and 1.3 GHz 9-cell cavities were demonstrated to reach $Q \sim 10^{10}$ at 10MV/m at 4.4K.
- Maximum gradients achieved up to \sim 20 MV/m.

G. Eremeev "Progress in Nb3Sn developments for CEBAF-style quarter cryomodule" TTC-2022,

U.Pudasaini et al. "Managing Sn-Supply to Tune Surface Characteristics of Vapor-Diffusion Coating of Nb3Sn", presented at the SRF'21, East Lansing, MI, USA, Jun.-Jul. 2021, doi:10.18429/JACoW-SRF2021-TUPTEV013.

S. Posen et al. "Advances in Nb₃Sn superconducting radiofrequency cavities towards first practical accelerator applications" Superconductor Science and Technology. 2021 Jan 11;34(2):025007.

D. Hall, "New Insights into the Limitations on the Efficiency and Achievable Gradients in Nb₃Sn SRF Cavities", PhD thesis, Cornell University (2017).

G. Jiang et al.. Understanding and optimization of the coating process of the radio-frequency Nb3Sn thin film superconducting cavities using tin vapor diffusion method. Applied Surface Science. 2024 Jan 15;643:158708.
G. F

Introduction – Topographic Defects

[1] Mullins, W.W., 1957. *Journal of Applied Physics*, *28*(3), pp.333-339. [2] Iwasaki, Tomio, et al. *JSME international journal. Ser. A, Mechanics and material engineering* 40.1 (1997): 15-22.

[4] Kubo, Takayuki, *Progress of Theoretical and Experimental Physics* 2015.6 (2015): 063G01.

Jefferson Lab

Topography Nb3Sn – Evolution with Coating Duration

Investigation

- Study samples coated from 1 to 78 hours (6 samples)
- 10x areas randomly sampled via AFM from each sample

Increased coating duration results in:

- Thickening of the coating
- Grain growth

1000

500

 $\overline{0}$

 -500

60

50

 $20\,$

 $10\,$

 $\begin{array}{c}\n 40 \\
\hline\n 30\n \end{array}\n \begin{array}{c}\n 40 \\
\hline\n 6 \text{ degrees}\n \end{array}$

- $\left[\begin{matrix} \frac{1}{2} \\ \frac{1}{2} \end{matrix}\right]$ Grooves are on the order of
- Grooves are on the order of 100 nm deep (comparable to the penetration depth)

Slope angle calculation

$$
\cos \theta = \hat{\mathbf{z}} \cdot \hat{\mathbf{n}} = \hat{\mathbf{z}} \cdot \frac{(-h_x, -h_y, 1)}{(1 + h_x^2 + h_y^2)^{\frac{1}{2}}}
$$

- Access to h_x , h_y is given by the extension of the Savitzky-Golay filter for surfaces [1]
- High slope angles exist regardless of coating duration

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Superheating Field Suppression

MFE & SFS

 (a)

Magnetic Field Enhancement Factor 900 800 700 600 $\begin{bmatrix} 500 \\ 400 \end{bmatrix} \begin{matrix} \begin{matrix} 1 \\ 8 \end{matrix} \\ \begin{matrix} \end{matrix} \end{bmatrix}$ 300 5 μ m 5 μ m

Perfect Electrical Conductor Model London Model [1] $\beta(\mathbf{r}) = |\mathbf{B}(\mathbf{r})|/B_0$ $\nabla^2\psi=0$ $\nabla \psi \cdot \hat{x} = B_0$, $\nabla \psi \cdot \hat{y} = 0$ and $\nabla \psi \cdot \hat{n} = 0$ $\psi(x, y, z_{max} = 6 \ \mu m) = -B_0 x$ **B**(**r**) = $B_0 \hat{x}$

Superheating Field Suppression Factor

1.6

 1.4

1.2

0.8

0.6

 0.4

 \circ

Results

 10^{-}

 10^{-2}

 10^{-3}

 10^{-4}

50

75

100

Relative Frequency

Results

- Bifurcation in the deviation between background plane and the topography
- This bifurcation is more clearly reflected in the SFS factor. During short annealing times
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Results

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 $\overline{\eta}$

Discussion

- Considering only the effects of superheating field suppression on the superheating field (~400 mT) peak magnetic fields of 107 -128 mT may be expected.
- Peak magnetic field enhancement values fall around ~1.7.
- There are many locations where MFE and SFS overlap. This may reduce further reduce the field of vortex penetration by $\mathrm{B}^*_{max} = \left(\frac{\eta}{\beta} \right) \mathrm{B}_{max}.$ The combined effect can reduce peak magnetic field to ~51 -77mT (12 -18MV/m in TESLA -shaped cavities).
- While this is in qualitative agreement with the field limitation in Nb₃Sn, there are many loss mechanisms which should be considered *before* topography.

Discussion – Other Performance Limiting Mechanisms

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[4] Becker, Chaoyue, et al. *Applied Physics Letters* 106.8 (2015).

Discussion – How Can The Suppression Factor Be Improved?

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[1] U. Pudasaini et al. SRF'23 (Grand Rapids, MI, USA). JACoW Publishing, Geneva, Switzerland, 2023.

[2] Rabkin, E., et al. *Journal of materials science* 41 (2006): 5151-5160.

[3] Iwasaki, Tomio, et al. *JSME international journal. Ser. A, Mechanics and material engineering* 40.1 (1997): 15-22.

Conclusions & Future Work

Conclusions

- Developed a simple model to calculate the superheating field suppression factor in the London theory.
- We have shown that superheating field suppression may be a large contributor to peak field degradation in dense, stoichiometric $Nb₃Sn$. The effect of which is compounded by local magnetic field enhancement.
- We hope that this work inspires more physically justified theories to make estimates of the geometrically suppressed superheating field in the deeper type-II limit where $Nb₃Sn$ resides.

Future work

• Compare the topography from witness samples and performance of $Nb₃Sn$ coated cavities.

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