

# Layered iron-based superconductors for SRF cavities

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# Outline

- Iron-based SC and recent applications
- Iron-based SC for SRF?
- Surface resistance of Iron-based SC
- ML theory for Iron-based SC
- Remarks
- Conclusion

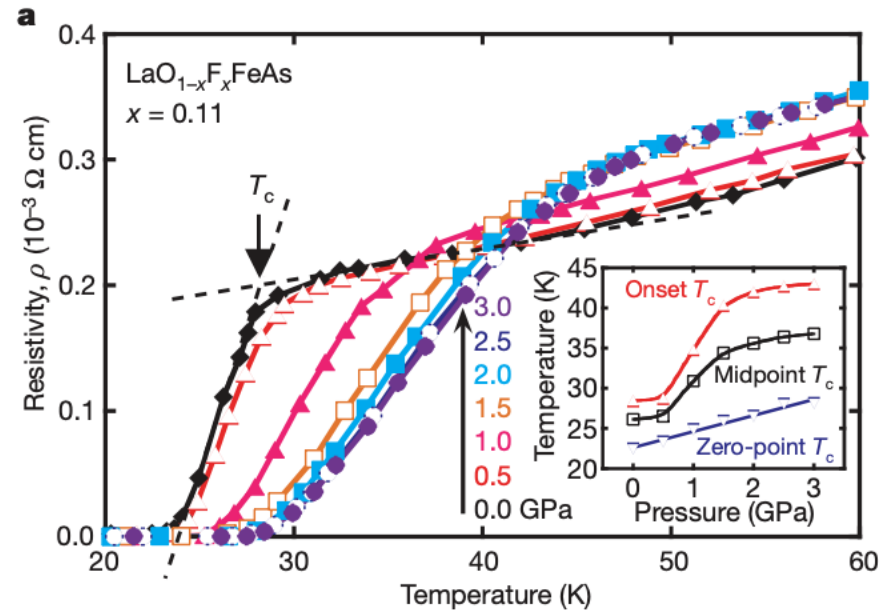
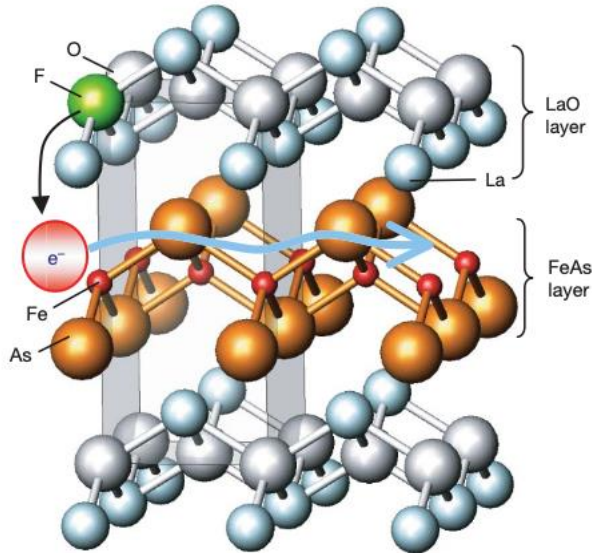
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# Iron-based superconductors

Hideo Hosono

## LaOFeAs



Y. Kamihira et al J. Am. Chem. Soc. 30, 3296-3297 (2008)

H. Takahashi et al, Nature 453, pages 376–378 (2008)



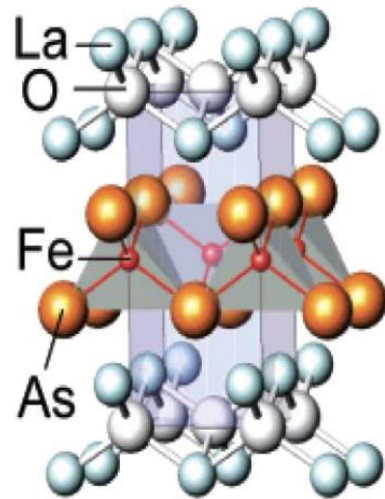
- Iron-based superconductors were discovered by the team in Tokyo Institute of Technology (currently: Institute of Science Tokyo) in 2008
- Surprising discovery: Iron is magnetic element  $\rightarrow$  usually not good for SC
- Non-BCS (i.e. phonon mediation) mechanism for SC (spin / orbit??)
- $T_c$  is higher than BCS but lower than cuprate (REBCO)

# Main known Fe-based superconductors

Among them, the three phases most relevant for wire applications are 1111, 122, and 11 types with a  $T_c$  of 55, 38 and 8 K, respectively.

X. Zhang et al "Progress in the development of high performance pnictide wires" CEC/ICMC 2017

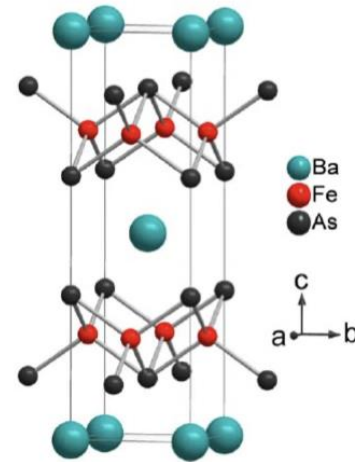
## 1111 Phase LnOFeAs



$T_c \sim 55$  K

Z. A. Ren et al., *Chin. Phys. Lett.* 25, 2215 (2008)

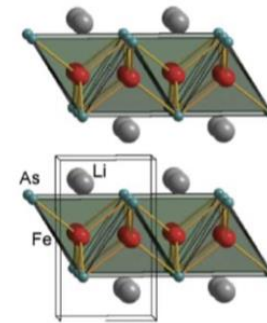
## 122 phase AFe<sub>2</sub>As<sub>2</sub> (A=Ba, Sr, Ca)



$T_c \sim 38$  K

M. Rotter, et al., *Phys. Rev. Lett.* 101, 107006 (2008)

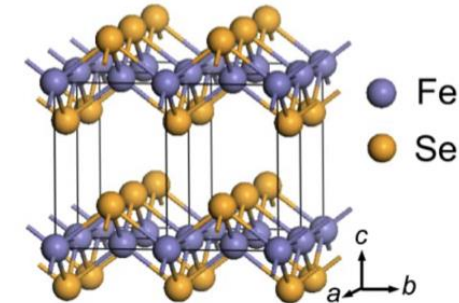
## 111 phase LiFeAs



$T_c \sim 18$  K

X. C. Wang, et al., *Solid State Commun.* 148, 538 (2008).

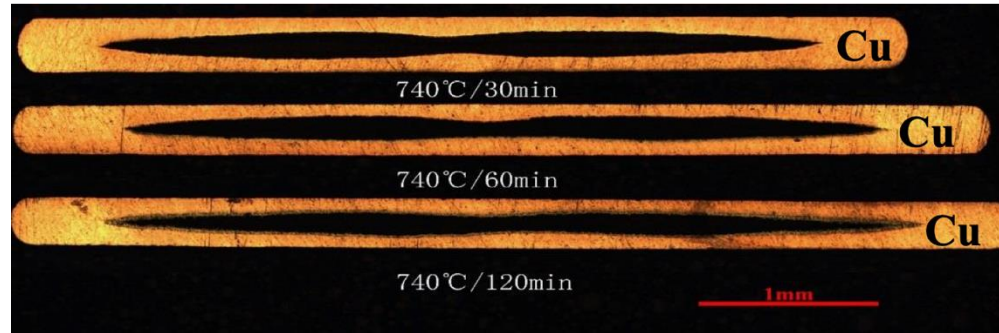
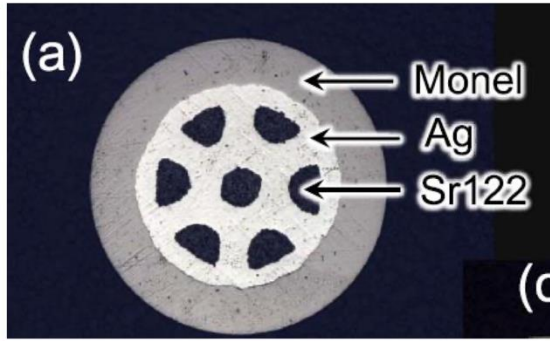
## 11 phase FeSe



$T_c \sim 8$  K

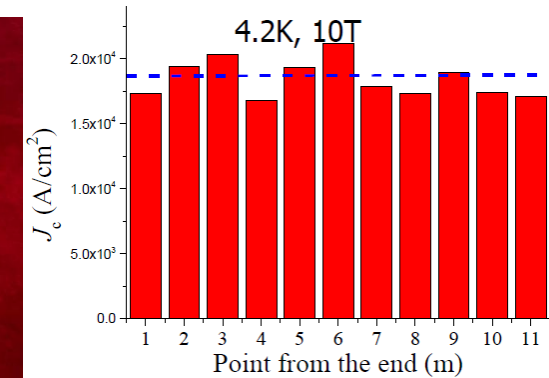
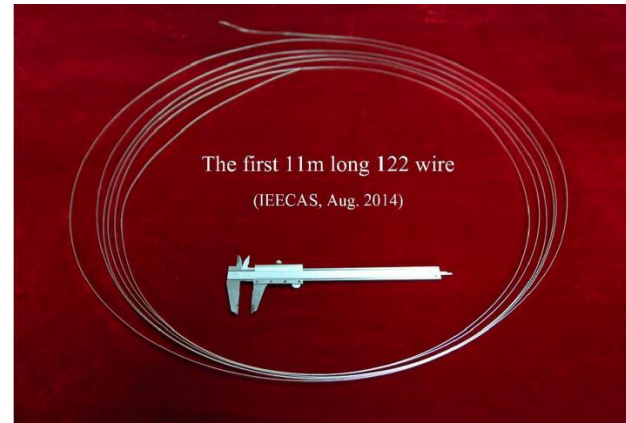
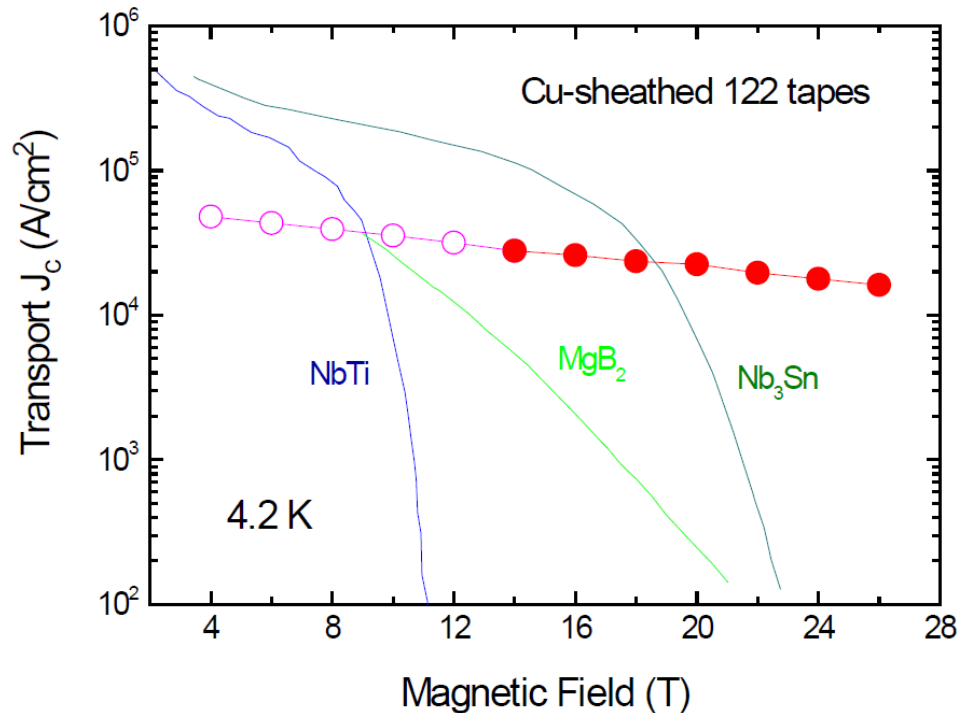
F. C. Hsu, et al., *Proc. Natl. Acad. Sci. U.S.A.* 105, 14262 (2008).

# Application of Iron-based SC: Sr-122 wire



Y. Ma “Recent progress in Fe-based superconducting wires and tapes”

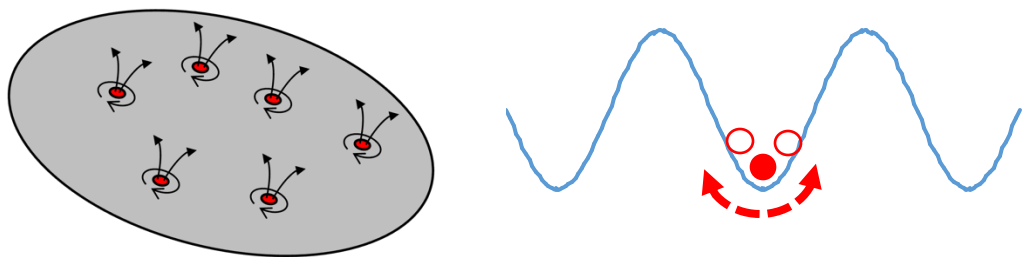
Monel/Ag, IEECAS



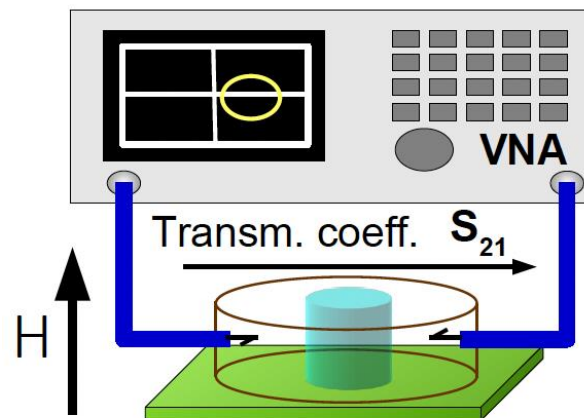
- Promising progress toward magnet applications
  - As handling in laboratory
- Market is growing → why not RF cavities as well?

# Iron-based SC and RF: DM axion

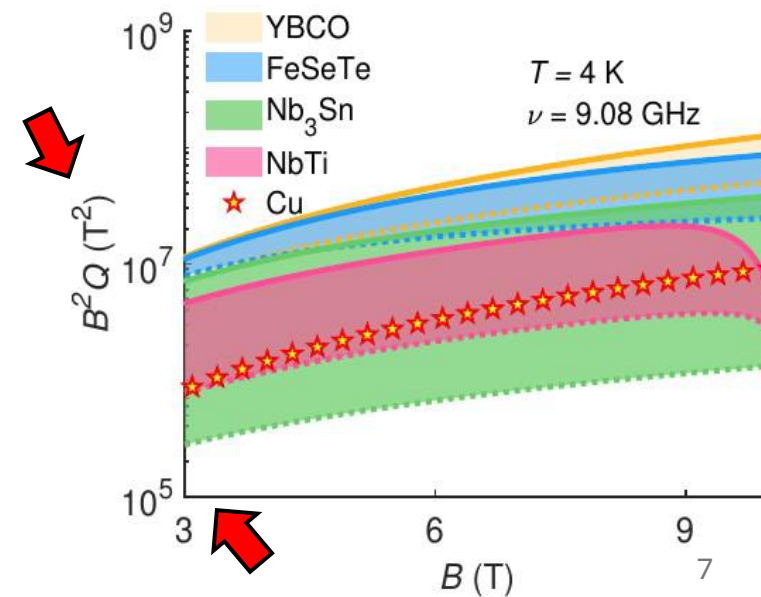
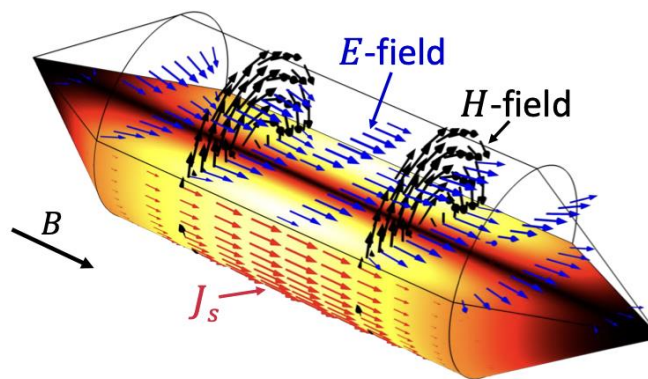
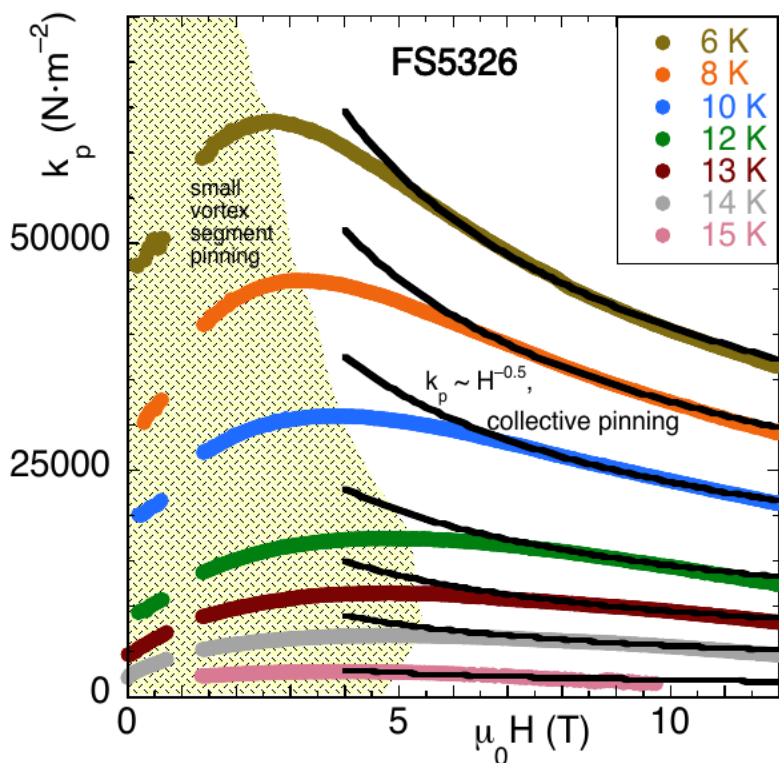
$$\eta \dot{\mathbf{x}} + k_p \mathbf{x} = \mathbf{J}_{rf} \times \Phi_0 + \mathbf{F}_{th}$$



## Dielectric cavity for sample measurement



Sample <math>\phi < 20 \text{ mm}</math>



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# Iron-based SC for SRF cavities

IOP Publishing

Supercond. Sci. Technol. 30 (2017) 034004 (25pp)

Superconductor Science and Technology

doi:10.1088/1361-6668/30/3/034004

## Theory of RF superconductivity for resonant cavities

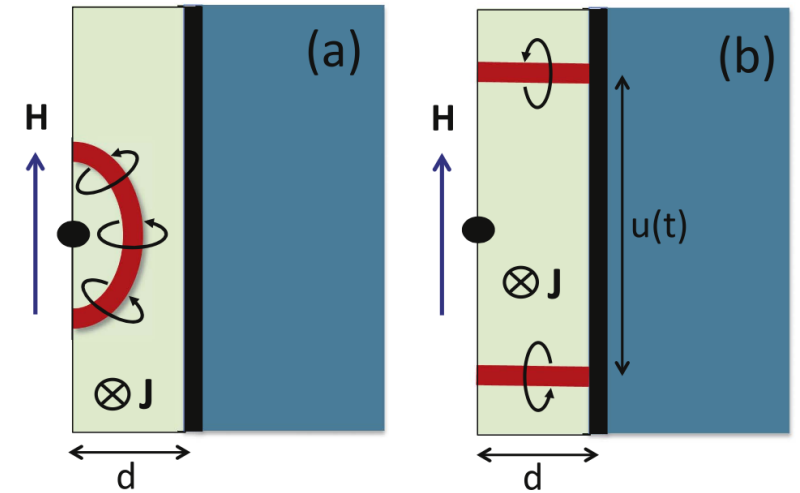
Alex Gurevich

Department of Physics and Center for Accelerator Science, Old Dominion University, 4600 Elkhorn Avenue, Norfolk, VA 23529, USA

values at low RF fields at 4.2 K. The use of multilayer coating may offer an opportunity to break the ‘Nb monopoly’ in the SRF cavities by taking advantage of many available superconductors with higher  $B_c$  and lower  $R_s$ . Technologies of *in situ* conformal coating of the inner surface of Nb cavities, particularly the atomic layer deposition [206] or hybrid physical-chemical vapor deposition [207], appear very promising

Supercond. Sci. Technol. 30 (2017) 034004

for deposition of high-quality superconducting films and multilayers of  $\text{Nb}_3\text{Sn}$  or  $\text{NbN}$  or  $\text{MgB}_2$  or superconducting pnictides [208]. Developing these and other technologies, and



layer with  $\xi \ll d_s < \lambda$ . For instance, the criterion  $J(0) < J_d/2$  assures a reasonable protection against penetration of vortices caused by low-angle grain boundaries in polycrystalline  $\text{Nb}_3\text{Sn}$  or pnictides [115], or local field enhancement at topographic defects in the Nb cavities [3]. At  $B_s \rightarrow B_s/2$  and  $B_{s0} \rightarrow 170 - 180$  mT, equations (67)–(68) give  $H_m \simeq 280$  mT at  $d_m = 0.8\lambda = 96$  nm for  $\text{Nb}_3\text{Sn}$ . If Nb can withstand the field  $B_{s0} \rightarrow 200$  mT observed on the best cavities, the maximum screening field could reach  $B_m = 295$  mT at  $d_m = 0.67\lambda = 80$  nm. Increasing  $\beta$  by the materials refinements of  $\text{Nb}_3\text{Sn}$  could push the peak fields over 300 mT. Pnictides with  $B_c \simeq 0.9$  T, such as  $\text{Ba}_{0.6}\text{K}_{0.4}\text{Fe}_2\text{As}_2$  [188, 189] could provide  $B_m = 426$  mT at  $d_m = 1.21\lambda = 242$  nm,  $\beta = 1/2$ , and  $B_{s0} \rightarrow 200$  mT.

# Significant enhancement was observed in Hc1 and Hc2

IOP Publishing

Supercond. Sci. Technol. 34 (2021) 015001 (5pp)

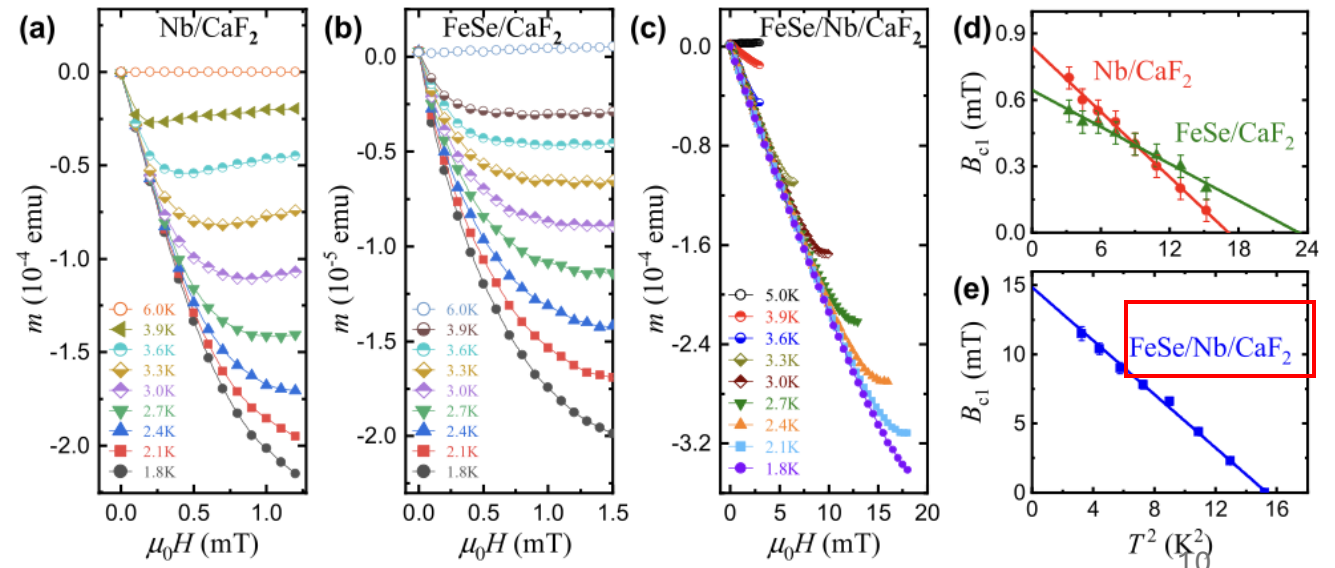
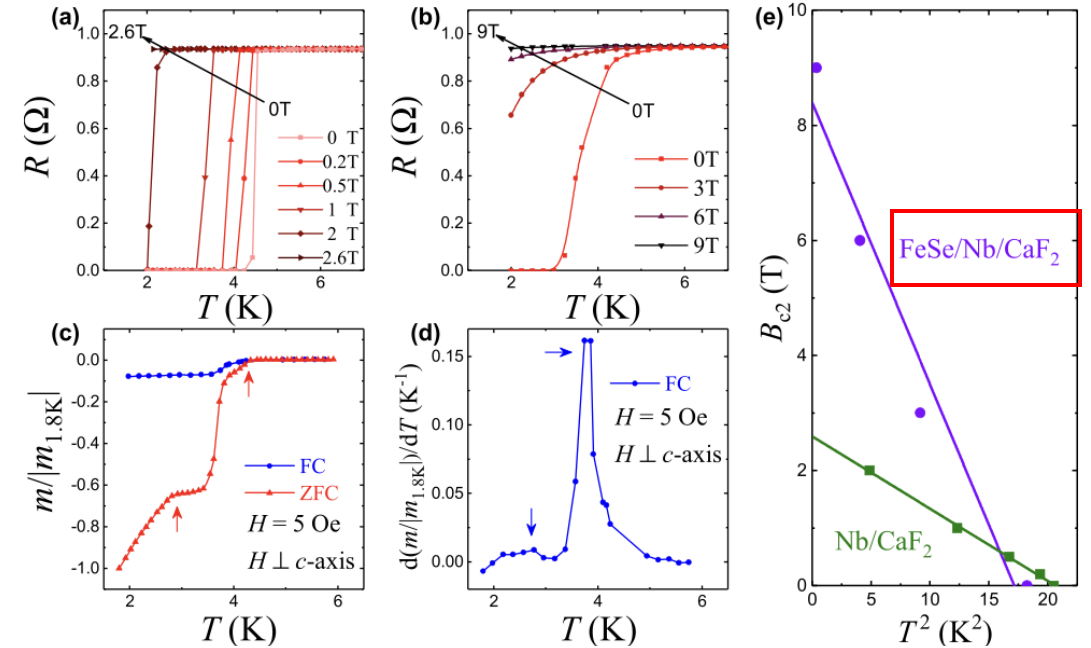
Superconductor Science and Technology

<https://doi.org/10.1088/1361-6668/abc568>

## Enhancement of the lower critical field in FeSe-coated Nb structures for superconducting radio-frequency applications

Zefeng Lin<sup>1,2</sup>, Mingyang Qin<sup>1,2</sup>, Dong Li<sup>1,2</sup>, Peipei Shen<sup>1,2</sup>, Liping Zhang<sup>3</sup>, Zhongpei Feng<sup>4</sup>, Peng Sha<sup>5</sup>, Jun Miao<sup>3</sup>, Jie Yuan<sup>1,6</sup>, Xiaoli Dong<sup>1,2,4</sup>, Chao Dong<sup>5</sup>, Qing Qin<sup>7</sup> and Kui Jin<sup>1,4,6</sup>

- Not pnictide (FeSe): Tc is as low as Nb  
→ Not for high-T SRF but high-G at 2-4 K
- Multilayer function was proven in DC
- FeSe/Nb structure showed factor 2-4 enhancement in  $H_{c2}$  and factor 16 enhancement in  $H_{c1}$  compared to Nb
- Absolute value in  $H_{c1}$  is very low

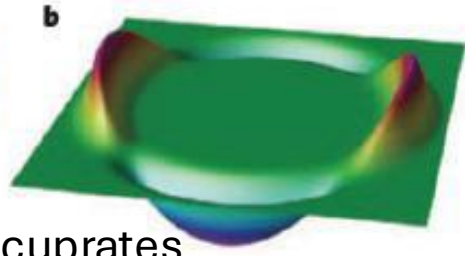


# Surface resistance: naivest possible argument

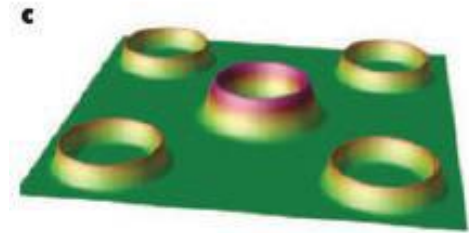
$$R_s \propto \hbar\omega(n_+ - n_-) = \hbar\omega \int_{\Delta}^{\infty} dE [f(E) - f(E + \hbar\omega)] \times N(E)N(E + \hbar\omega)$$



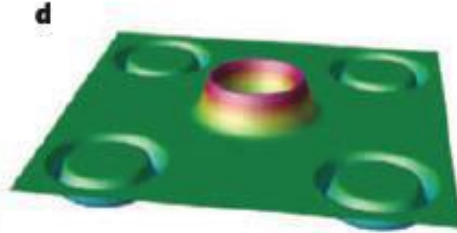
Nb, Nb<sub>3</sub>Sn, NbN



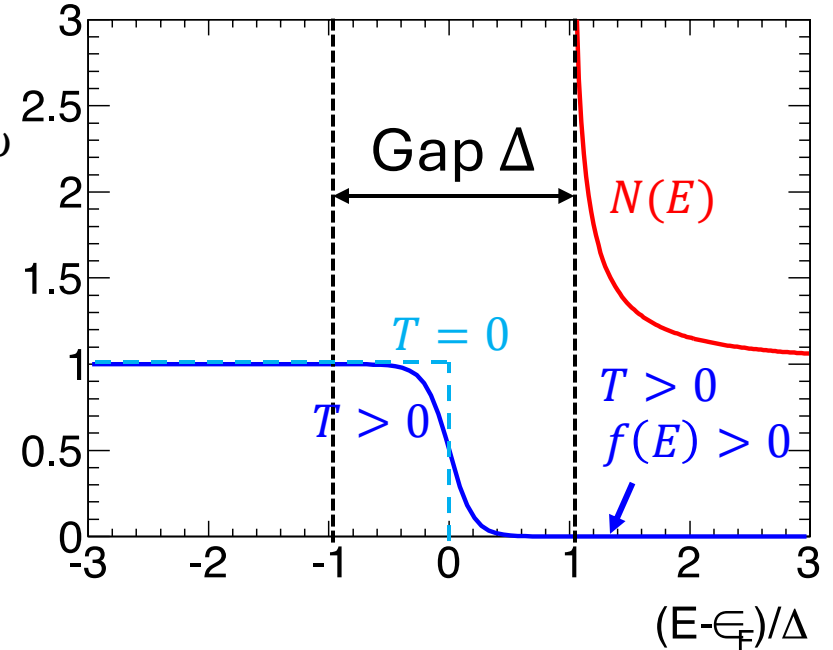
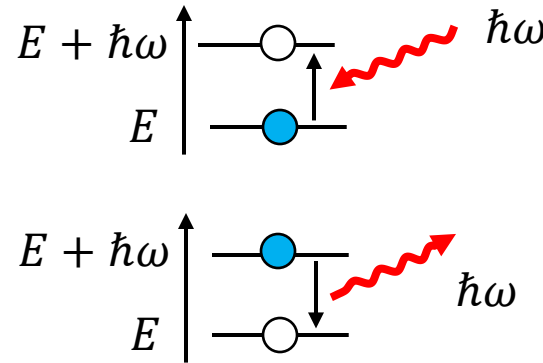
cuprates



MgB<sub>2</sub>



Iron-based



- Gapless SC may have too much thermal excitation of quasiparticles → low  $R_s$
- Gap-full is the minimum requirement
- Iron-based SC often shows two gap structure
  - If MgB<sub>2</sub> is OK, Iron-based SC would also be OK?

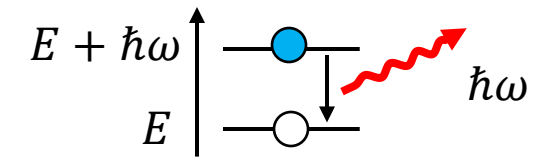
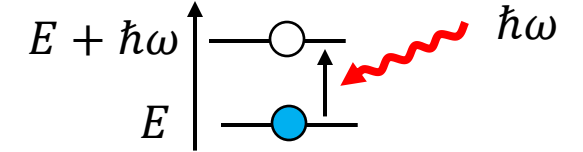
# Optical conductivity in the Meissner state

$$\sigma_1 = \frac{2\sigma_n}{\hbar\omega} \int_0^\infty [f(\epsilon) - f(\epsilon + \hbar\omega)][\text{Re}G^R(\epsilon)\text{Re}G^R(\epsilon + \omega) + \text{Re}F^R(\epsilon)\text{Re}F^R(\epsilon + \omega)]d\epsilon$$

S. N. Nam, Phys Rev 156 470 (1967)

$$\sim \frac{2\sigma_n}{\hbar\omega} (1 - e^{-\omega/T}) \int_0^\infty e^{-\epsilon/kT} N(\epsilon)N(\epsilon + \hbar\omega)d\epsilon$$

J. Halbritter Z. Physik 266 p.209 (1974)



## Quasi-classical Green functions

Conventional s-wave (Dynes)

$$\frac{N(\epsilon)}{N_0} = \text{Re} \left( \frac{\epsilon + i\delta}{\sqrt{(\epsilon + i\delta)^2 - \Delta_0^2}} \right)$$

$$\Delta_0(T) = \Delta_0 [\cos(\pi T^2 / 2T_c^2)]^{1/2}$$

Cuprate d-wave

$$\frac{N(\epsilon)}{N_0} = \text{Re} \left( \left\langle \frac{\epsilon + i\delta}{\sqrt{(\epsilon + i\delta)^2 - \Delta^2(\theta)}} \right\rangle \right)$$

$$\Delta(\theta) = \Delta_0 \cos 2\theta$$

P. Coleman "Introduction to Many-Body Physics"

Pnictide  $s_{\pm}$ -wave

$$\frac{N(\epsilon)}{N_0} = \text{Re} \left( \left\langle \frac{\epsilon + i\delta}{\sqrt{(\epsilon + i\delta)^2 - \Delta_{\alpha_{1,2},\beta_{1,2}}^2(\phi_{1,2})}} \right\rangle \right)$$

$$\Delta_{\alpha_{1,2},\beta_{1,2}}(\phi_{1,2}) = \Delta_0 \Phi_{\alpha_{1,2},\beta_{1,2}}$$

$$\Phi_{\alpha_{1,2}} = -\Phi_a$$

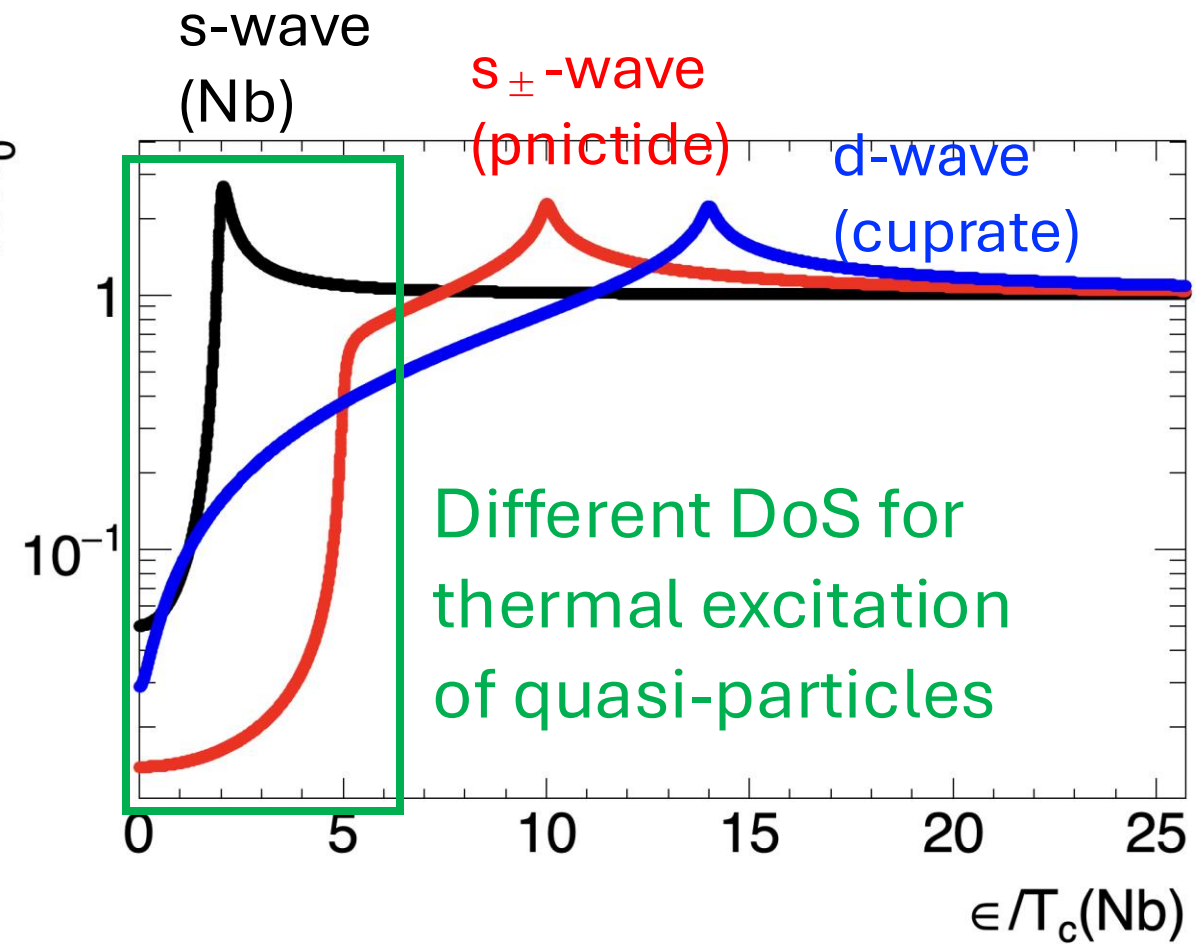
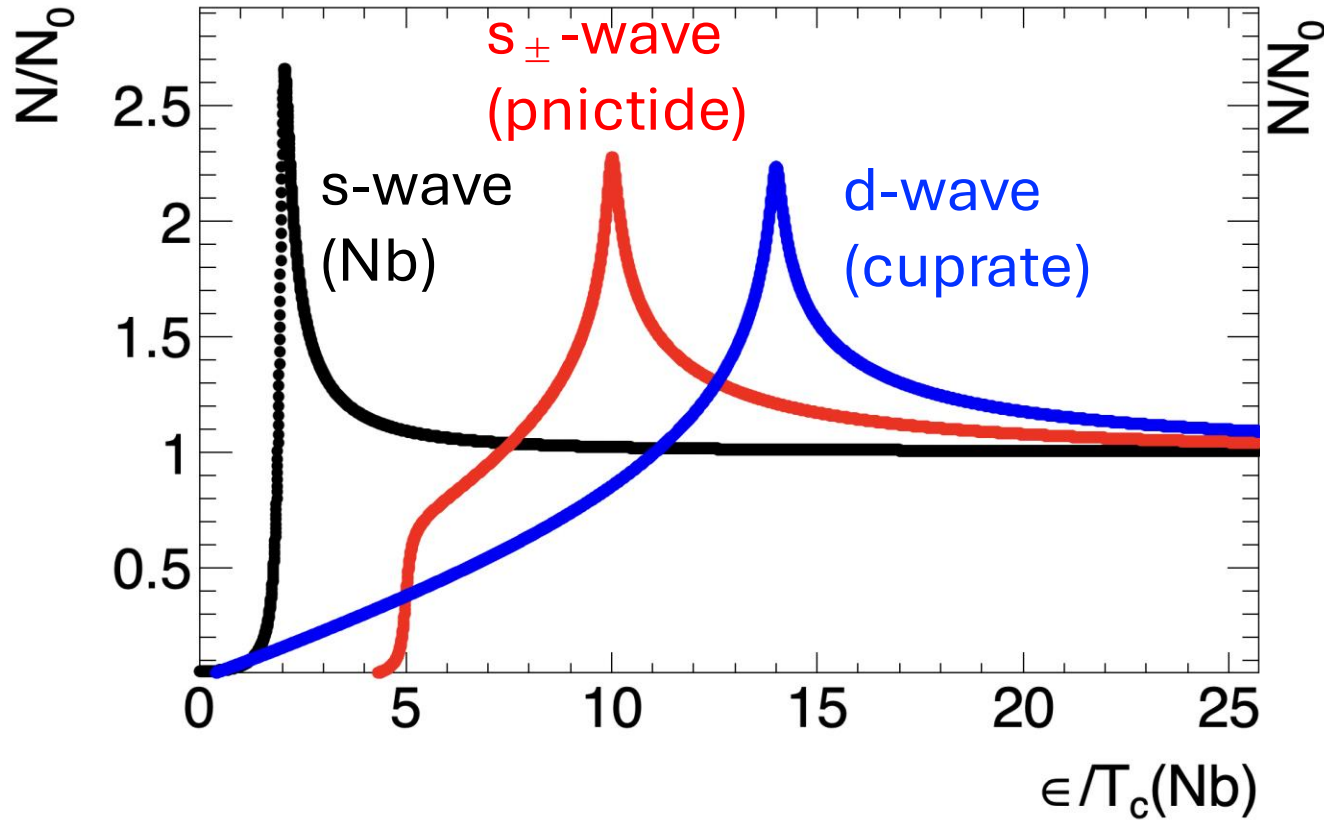
$$\Phi_{\beta_{1,2}} = \frac{1 + \Phi_{\beta_{min}}}{2} \pm \frac{(1 - \Phi_{\beta_{min}})}{2} \cos(2\phi_{1,2})$$

Y. Nagai et al New J. Phys. 10 103026 (2008)

## Assumption

- Meissner state = thermodynamical state
- Optical conductivity formulae for BCS SC may be still valid in 1<sup>st</sup> order approximation

# Density of states



The energy is normalized to  $T_c(\text{Nb}) = 9.25$  K

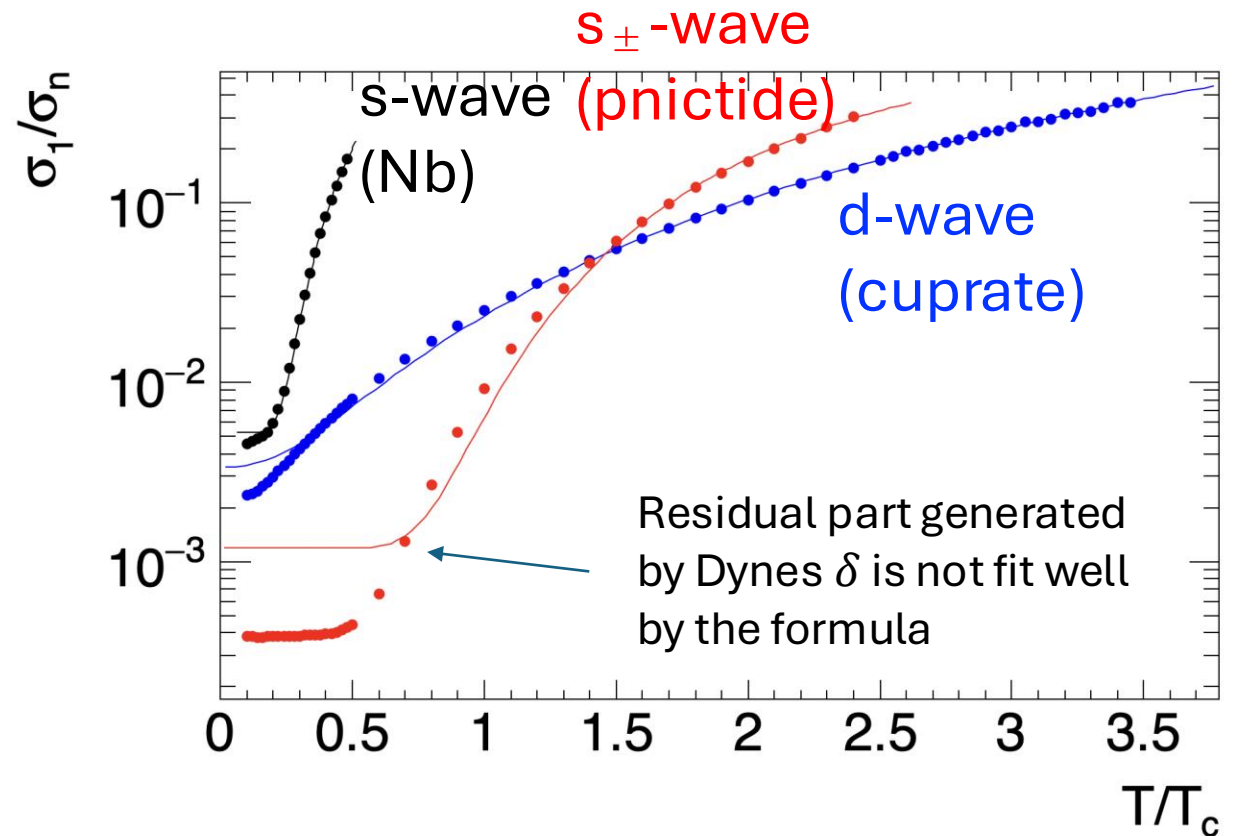
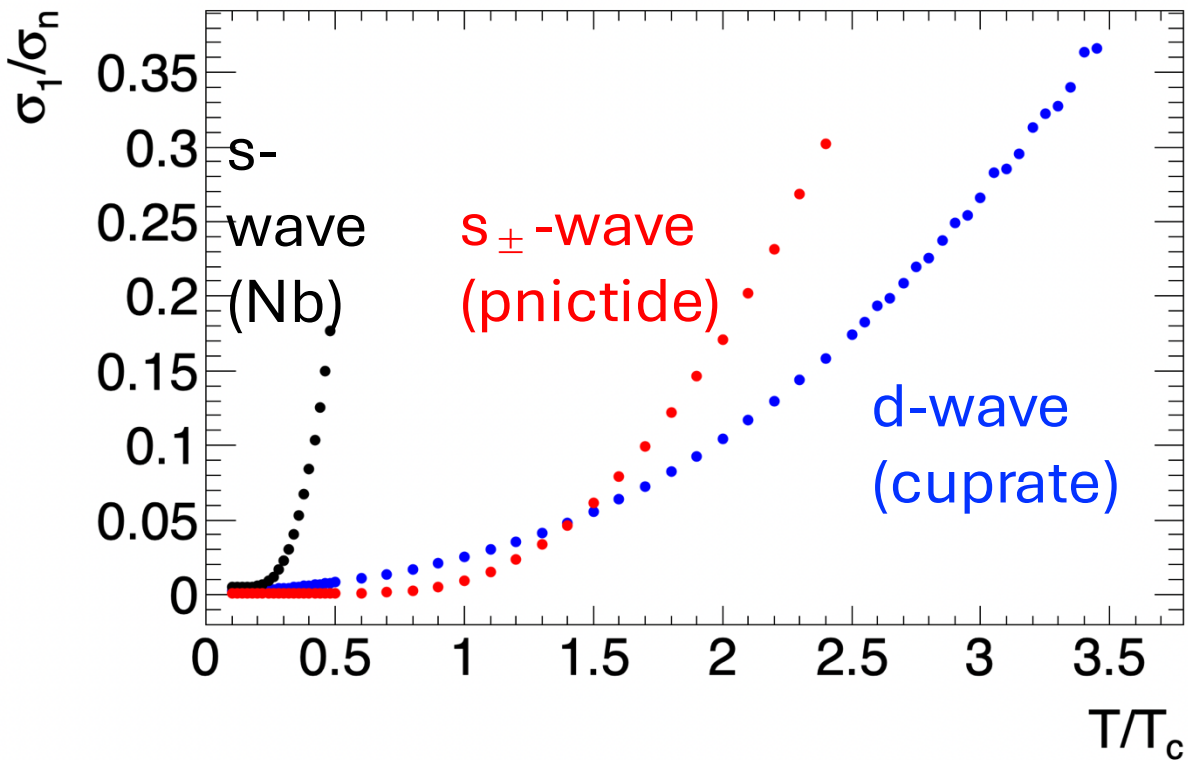
Assumed parameters:

$$\begin{aligned} T_c(\text{pnictide}) &= 5 \times T_c(\text{Nb}) \\ T_c(\text{cuprate}) &= 7 \times T_c(\text{Nb}) \\ \Delta_0 &= 2 \times T_c \end{aligned}$$

$$\begin{aligned} \Phi_a &= 1 \\ \Phi_{\beta_{min}} &= 0.5 \\ \delta &= 0.1 \end{aligned}$$

$$\frac{\sigma_1}{\sigma_n} \sim \frac{2\sigma_n}{\hbar\omega} (1 - e^{-\omega/T}) \int_0^{\infty} e^{-\epsilon/kT} N(\epsilon)N(\epsilon + \hbar\omega)d\epsilon$$

# $\sigma_1$ vs $T$ : an example ( $\omega = 0.02 \sim 600$ MHz)



## Best fitting functions

gap-full:  $\frac{\sigma_1(T)}{\sigma_n} = \frac{A}{T} \exp\left(-\frac{\Delta}{T}\right) + B$

Gapless:  $\frac{\sigma_1(T)}{\sigma_n} = CT^{\alpha} + B$

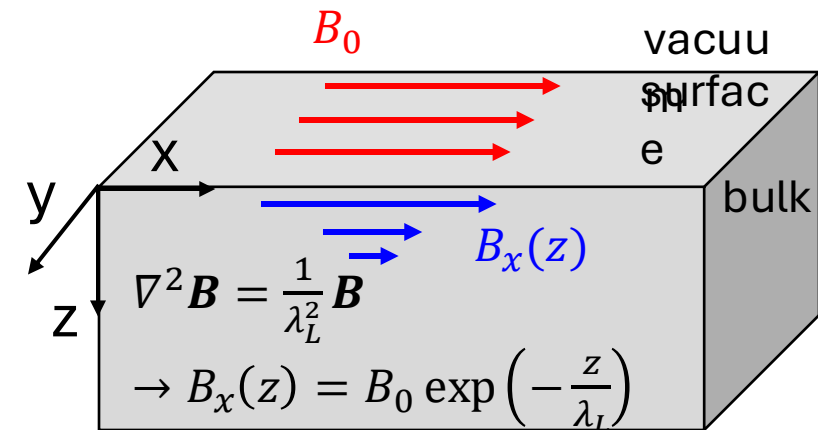
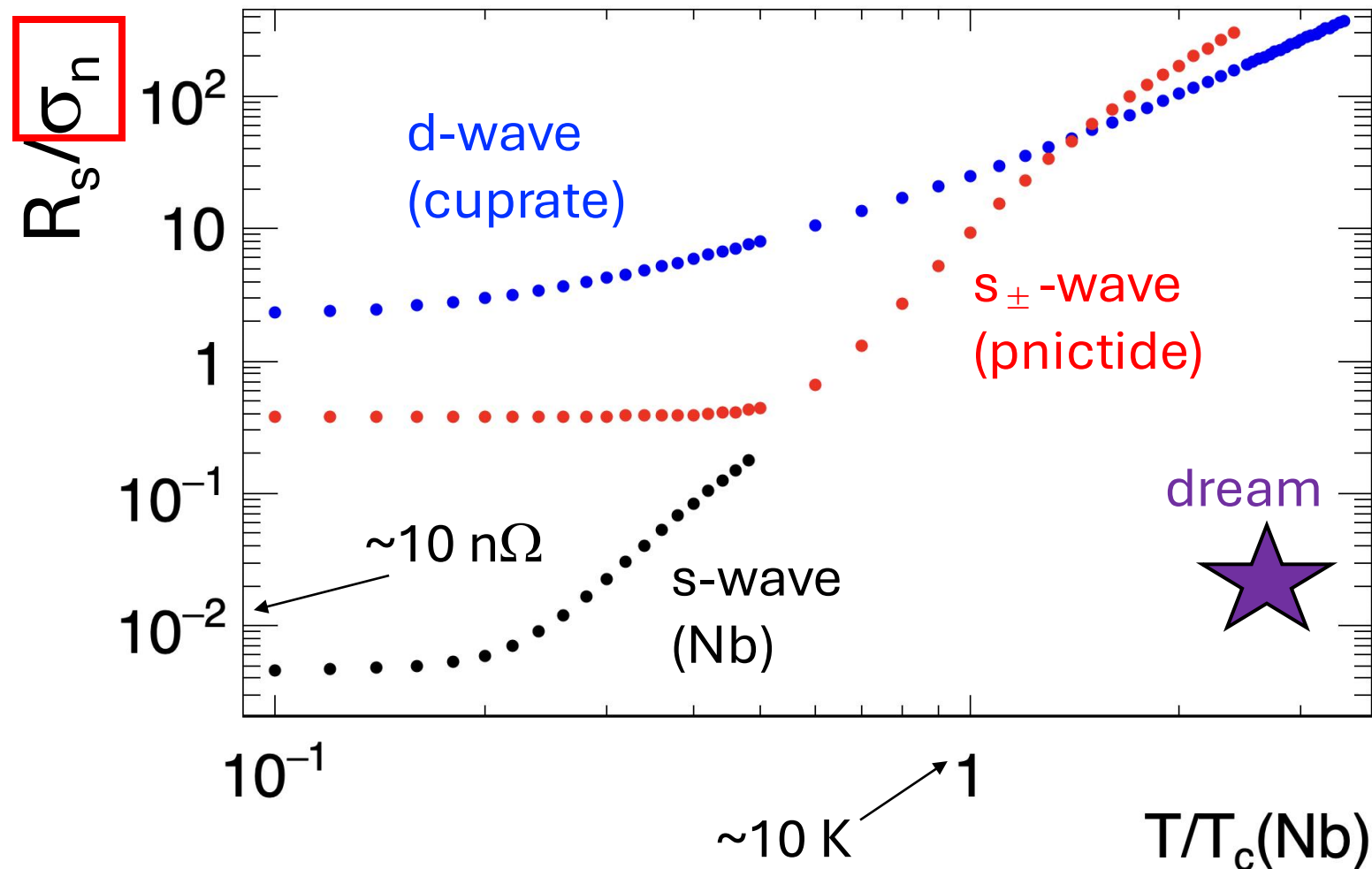
	Nb	pnictide
A	$8.67 \pm 0.23$	$23.8 \pm 0.81$
$\Delta$	$2.24 \pm 0.01$	$8.43 \pm 0.07$
B	$0.0052 \pm 0.0003$	$0.0012 \pm 0.0005$

	cuprate
C	$0.0201 \pm 0.0003$
$\alpha$	$2.341 \pm 0.015$
B	$0.0034 \pm 0.00044$

# Surface resistance

$$Z_s = \sqrt{\frac{i\omega\mu_0}{\sigma_1 - i\sigma_2}} \xrightarrow{T \ll T_c, \sigma_1 \ll \sigma_2} \sqrt{\frac{\mu_0}{\omega\sigma_2^3}} \left( \frac{1}{2}\sigma_1 + i\sigma_2 \right) \rightarrow R_s = \text{Re}(Z_s) = \frac{\mu_0\omega^2\lambda^3}{2}\sigma_1(T)$$

The penetration depth is factor 10 longer in HTS than Nb  
 → RF field looks more materials → more loss



	$\lambda_L$ [nm]
Nb	>36
pnictide	200-400
cuprate	130-170 / 500-850

→ Clearly, the chance is in multilayer  $d \lesssim \lambda$

# Lesson learned from $R_s$ calculation

- $\frac{\sigma_1(T)}{\sigma_n} = \frac{A}{T} \exp\left(-\frac{\Delta}{T}\right) + B$  may be still valid (smaller  $\Delta$  dominates) for iron-based superconductors
- REBCO could be useful in high-T pulsed operation ( $\rightarrow$  SLAC & CERN)
- Long penetration depth causes high loss
- Multilayer may be an option!
- Experimental data of  $H_{c1}$  enhancement already exists  
 $\rightarrow$  Let's apply multilayer theory for iron-based SC

A. Dhar LCWS2024

The former discussion was recently published  $\rightarrow$

## Potential of non-conventional superconductors for particle accelerator cavities

Publisher: IEEE

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Akira Miyazaki [All Authors](#)

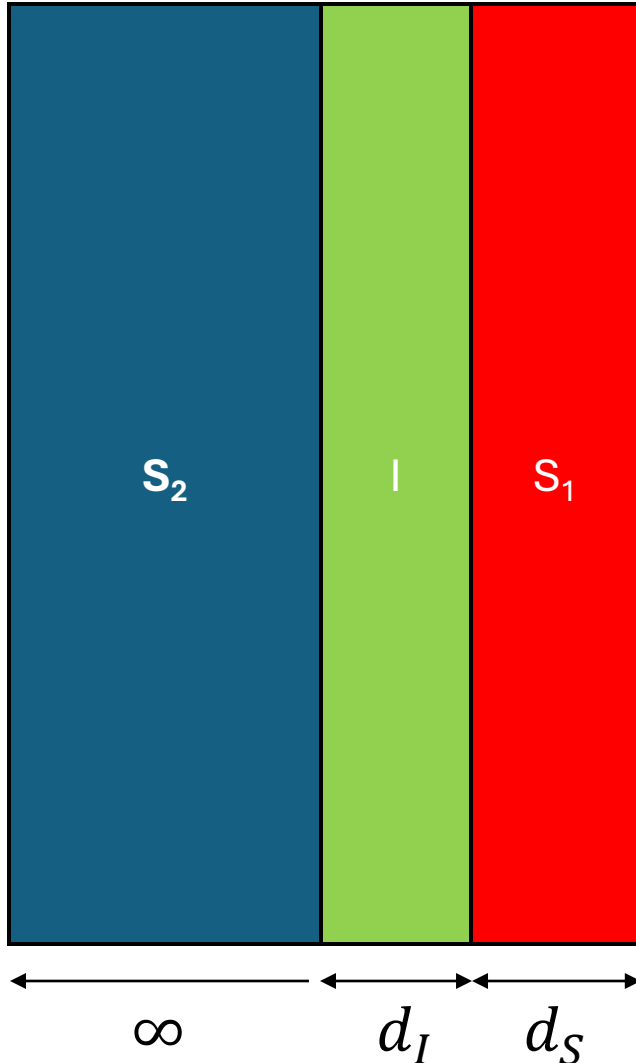


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# Multilayer theory by Kubo: London equation

T. Kubo et al arXiv:1304.6876



$$\text{If } \frac{\phi_0}{4\pi\xi_1\lambda_1} \frac{1}{\sinh\left(\frac{d_S}{\lambda_1}\right) + \left(\frac{\lambda_2}{\lambda_1} + \frac{d_I}{\lambda_1}\right) \cosh\left(\frac{d_S}{\lambda_1}\right)} < B_{sh,2}$$

$$B_v = \frac{\phi_0}{4\pi\xi_1\lambda_1} \frac{\cosh\left(\frac{d_S}{\lambda_1}\right) + \left(\frac{\lambda_2}{\lambda_1} + \frac{d_I}{\lambda_1}\right) \sinh\left(\frac{d_S}{\lambda_1}\right)}{\sinh\left(\frac{d_S}{\lambda_1}\right) + \left(\frac{\lambda_2}{\lambda_1} + \frac{d_I}{\lambda_1}\right) \cosh\left(\frac{d_S}{\lambda_1}\right)}$$

(attenuated B-field through  $S_1$  is lower than that of  $S_2$   
 $\rightarrow$  breakdown determined by  $S_1$ )

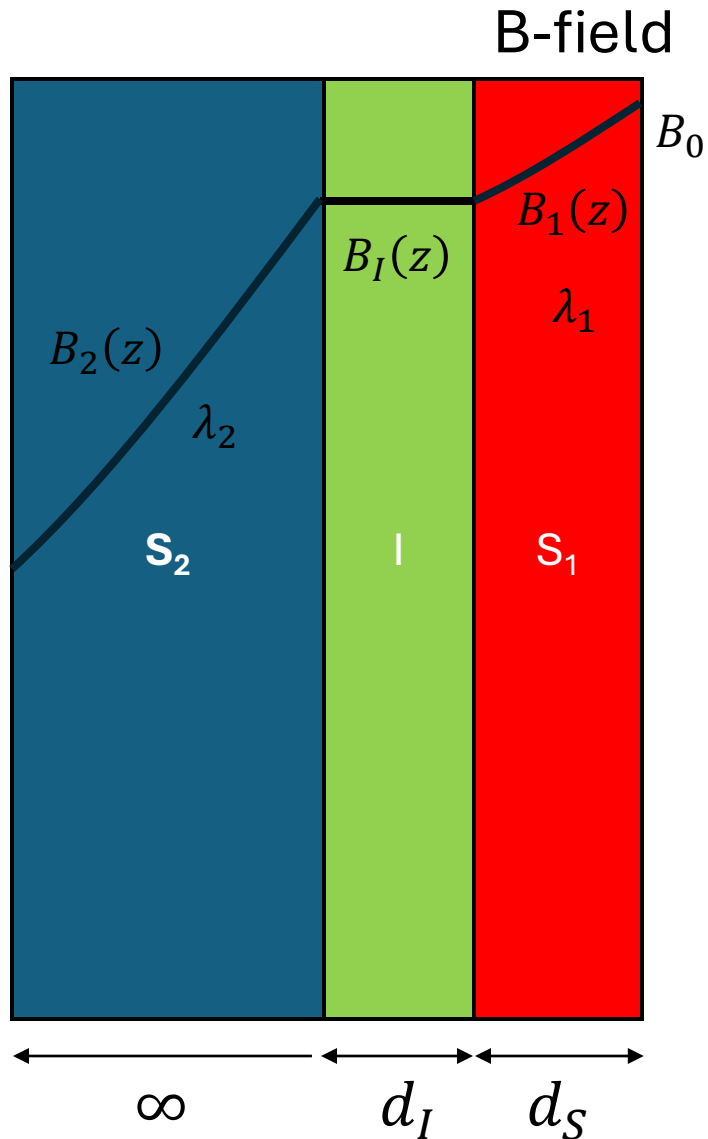
$$\text{If } \frac{\phi_0}{4\pi\xi_1\lambda_1} \frac{1}{\sinh\left(\frac{d_S}{\lambda_1}\right) + \left(\frac{\lambda_2}{\lambda_1} + \frac{d_I}{\lambda_1}\right) \cosh\left(\frac{d_S}{\lambda_1}\right)} > B_{sh,2}$$

$$B_v = \left[ \cosh\left(\frac{d_S}{\lambda_1}\right) + \left(\frac{\lambda_2}{\lambda_1} + \frac{d_I}{\lambda_1}\right) \sinh\left(\frac{d_S}{\lambda_1}\right) \right] B_{sh,2}$$

(attenuated B-field through  $S_1$  is still higher than  
that of  $S_2$   $\rightarrow$  breakdown determined by  $S_2$ )

Assumption: London equation is valid for iron-based SC (probably OK)

# field distribution inside a ML structure → RF loss calculation



$$B_1(z) = B_0 \frac{\cosh\left(\frac{d_s - z}{\lambda_1}\right) + \left(\frac{\lambda_2}{\lambda_1} + \frac{d_I}{\lambda_1}\right) \sinh\left(\frac{d_s - z}{\lambda_1}\right)}{\cosh\left(\frac{d_s}{\lambda_1}\right) + \left(\frac{\lambda_2}{\lambda_1} + \frac{d_I}{\lambda_1}\right) \sinh\left(\frac{d_s}{\lambda_1}\right)}$$

$$B_I(z) = B_0 \frac{1}{\cosh\left(\frac{d_s}{\lambda_1}\right) + \left(\frac{\lambda_2}{\lambda_1} + \frac{d_I}{\lambda_1}\right) \sinh\left(\frac{d_s}{\lambda_1}\right)}$$

$$B_2(z) = B_0 \frac{\exp\left(-\frac{z - d_s - d_I}{\lambda_2}\right)}{\cosh\left(\frac{d_s}{\lambda_1}\right) + \left(\frac{\lambda_2}{\lambda_1} + \frac{d_I}{\lambda_1}\right) \sinh\left(\frac{d_s}{\lambda_1}\right)}$$

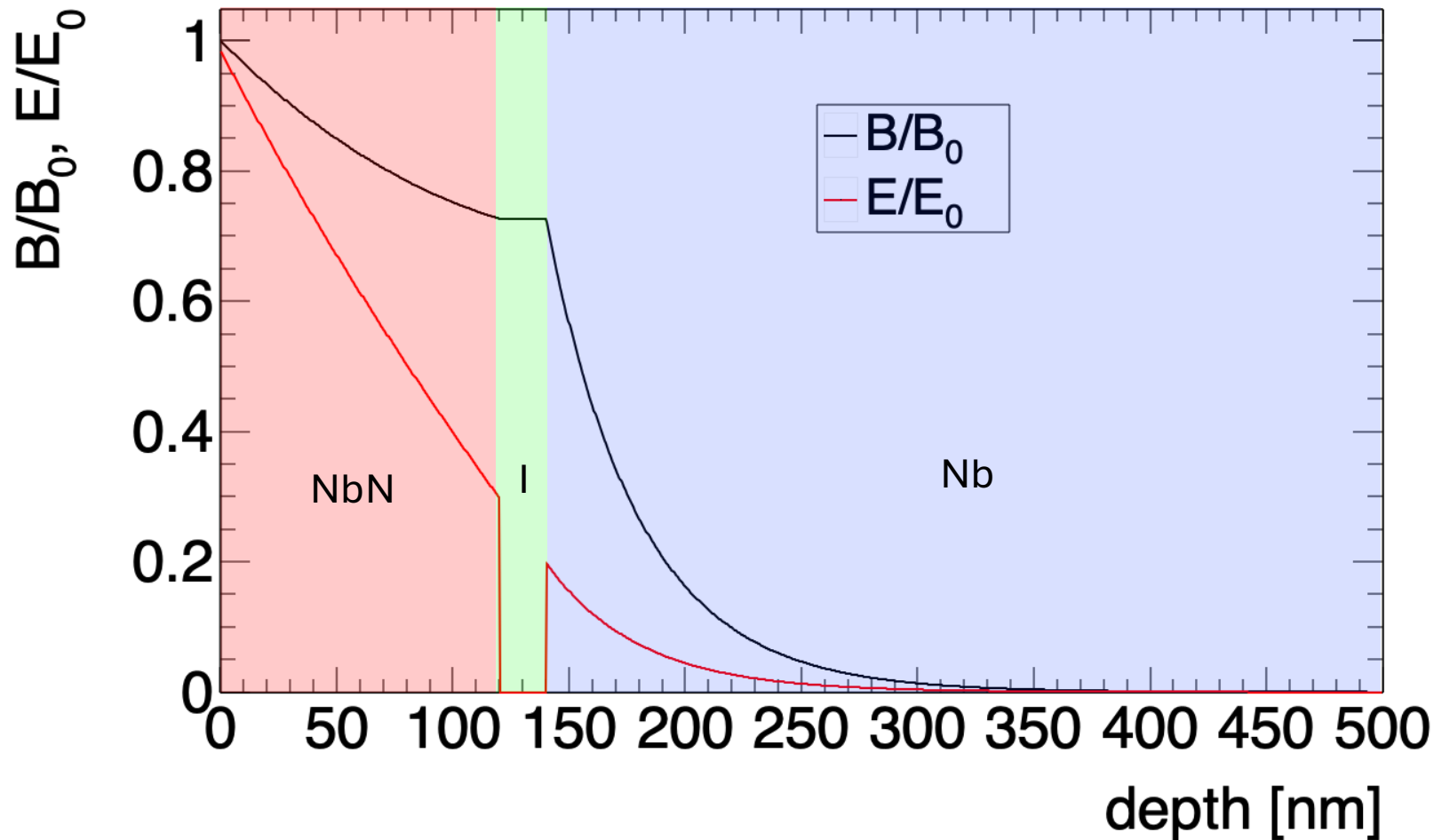
$$E_1(z) = \omega \lambda_1 B_0 \frac{\sinh\left(\frac{d_s - z}{\lambda_1}\right) + \left(\frac{\lambda_2}{\lambda_1} + \frac{d_I}{\lambda_1}\right) \cosh\left(\frac{d_s - z}{\lambda_1}\right)}{\cosh\left(\frac{d_s}{\lambda_1}\right) + \left(\frac{\lambda_2}{\lambda_1} + \frac{d_I}{\lambda_1}\right) \sinh\left(\frac{d_s}{\lambda_1}\right)}$$

$$E_I(z) = 0$$

$$E_2(z) = \omega \lambda_2 B_0 \frac{\exp\left(-\frac{z - d_s - d_I}{\lambda_2}\right)}{\cosh\left(\frac{d_s}{\lambda_1}\right) + \left(\frac{\lambda_2}{\lambda_1} + \frac{d_I}{\lambda_1}\right) \sinh\left(\frac{d_s}{\lambda_1}\right)}$$

$$E(z) = -\omega \lambda^2 \frac{dB}{dz}$$

# Field distribution → surface resistance (ex: NbN/I/Nb)



parameter	value
$\xi_{NbN}$ [nm]	5
$\lambda_{NbN}$ [nm]	200
$\lambda_{Nb}$ [nm]	40
$d_s$ [nm]	120
$d_I$ [nm]	20

Quasi-particle conductivity  
(real part of optical conductivity)

$$\sigma_{1,2} = \frac{e^2 n_N \tau}{m^*} \propto \exp\left(-\frac{\Delta_{1,2}}{k_B T}\right)$$

$$\rightarrow \sigma_{1,2} \equiv \sigma_{0,1,2} \exp\left(-\frac{\Delta_{1,2}}{k_B T}\right)$$

Surface resistance

$$\frac{1}{2} R_s H^2 = \frac{\sigma_1}{2} \int_0^{d_s} E_1^2(z) dz + q(d_I, \epsilon, \delta) + \frac{\sigma_2}{2} \int_{d_s+d_I}^{\infty} E_2^2(z) dz$$

(Dielectric loss)

# Multilayer BCS resistance

Surface resistance

$$\frac{1}{2} R_s H^2 = \frac{\sigma_1}{2} \int_0^{d_s} E_1^2(z) dz + q(d_I, \epsilon, \delta) + \frac{\sigma_2}{2} \int_{d_s+d_I}^{\infty} E_2^2(z) dz \quad \rightarrow R_s = R_{s,1} + q + R_{s,2}$$

Surface resistance

$$R_{s,1} = \mu_0^2 \omega^2 \sigma_{0,1} \exp\left(-\frac{\Delta_1}{k_B T}\right) \lambda_1^3 \frac{\left[ -2\lambda_1^2(d_I + \lambda_2) + 2d_s(d_I - \lambda_1 + \lambda_2)(d_I + \lambda_1 + \lambda_2) + 2\lambda_1^2(d_I + \lambda_2) \cosh\left(\frac{2d_s}{\lambda_1}\right) + \lambda_1(\lambda_1^2 + (d_I + \lambda_2)^2) \sinh\left(\frac{2d_s}{\lambda_1}\right) \right]}{4\lambda_1^3 \left[ \cosh\left(\frac{d_s}{\lambda_1}\right) + \left(\frac{\lambda_2}{\lambda_1} + \frac{d_I}{\lambda_1}\right) \sinh\left(\frac{d_s}{\lambda_1}\right) \right]^2}$$

Semi-infinite  
bulk surface  
resistance

$$\equiv D_1(d_s, d_I)$$

Reduction factor by the finite layer thick

$$R_{s,2} = \mu_0^2 \omega^2 \sigma_{0,2} \exp\left(-\frac{\Delta_2}{k_B T}\right) \lambda_2^3 \frac{1}{2 \left[ \cosh\left(\frac{d_s}{\lambda_1}\right) + \left(\frac{\lambda_2}{\lambda_1} + \frac{d_I}{\lambda_1}\right) \sinh\left(\frac{d_s}{\lambda_1}\right) \right]^2}$$

Semi-infinite  
bulk surface  
resistance

$$\equiv D_2(d_s, d_I)$$

Reduction factor by screening of the top layer

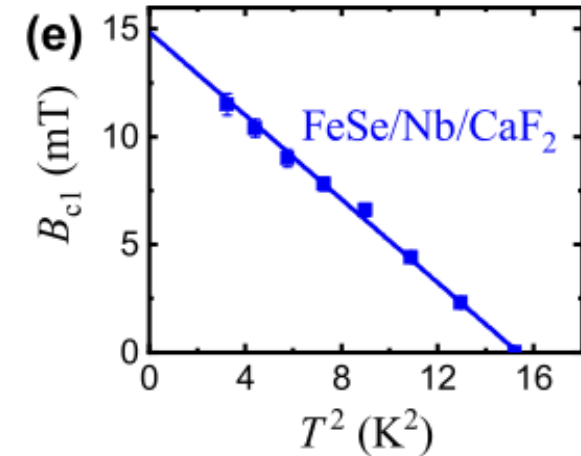
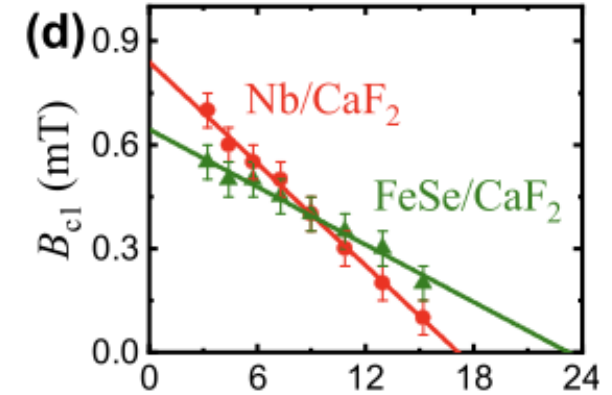
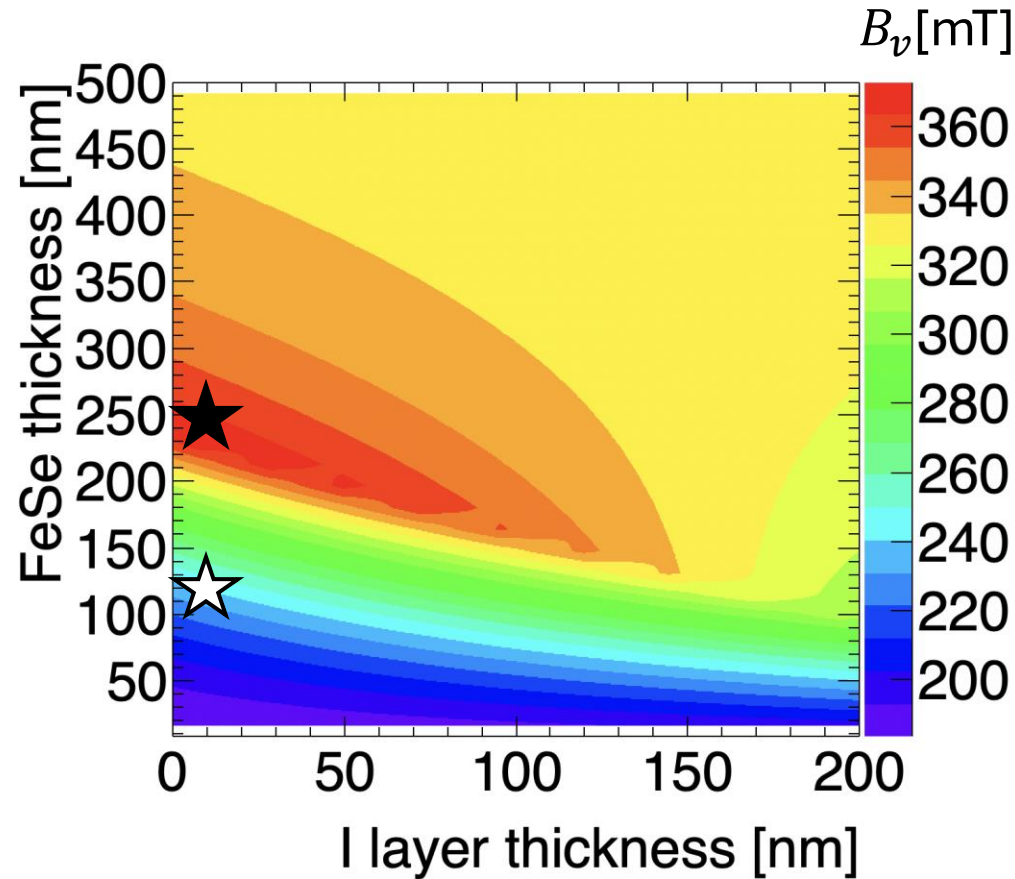
Assuming exponential formula  
validated from the former  
argument by using numerical  
integral of Green's functions

# Breakdown field for FeSe/(I)/N multilayer structure

parameter	value
$\xi_{FeSe}$ [nm]	2.5
$\lambda_{FeSe}$ [nm]	200
$\lambda_{Nb}$ [nm]	40
$B_{shNb}$ [mT]	180

$$\frac{280 \text{ mT}}{180 \text{ mT}} = 1.6$$

Improvement with  
FeSe thick 130 nm

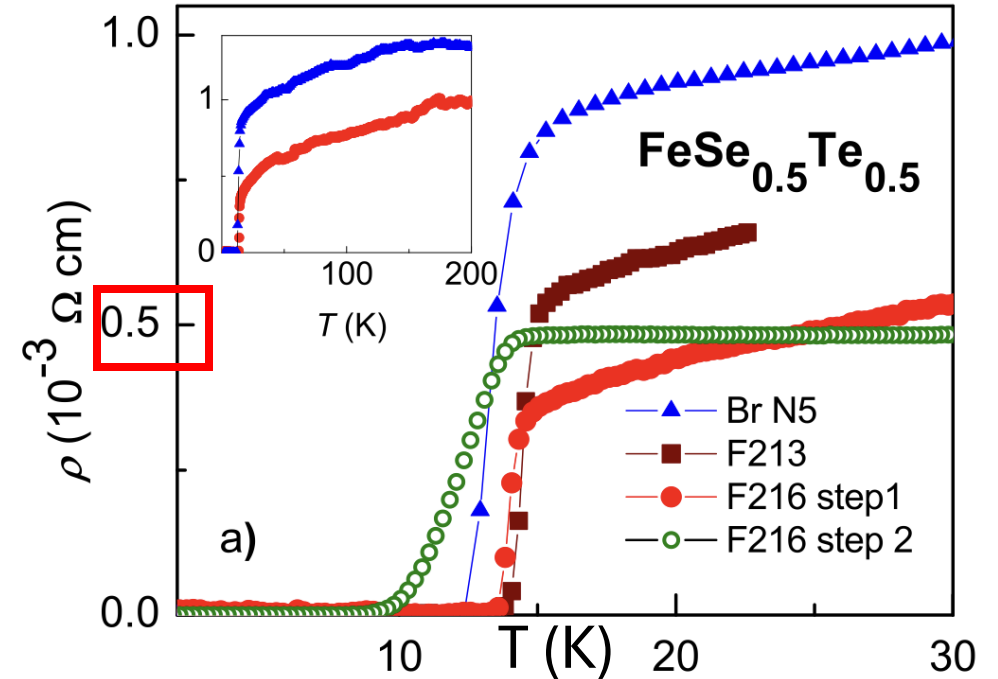


- ML enhancement of the breakdown field from 180 mT to 360 mT
  - FeSe thickness around 250 nm without insulator
- FeSe/Nb/CaF<sub>2</sub> : FeSe 130 nm thick, no insulator, Nb 115 nm thick (Z. Lin et al SUST 34 015001)

# Material parameters of FeSe

Eur. Phys. J. B 79, 289-299 (2011)

- Surface resistance of SRF cavities depend on normal conducting conductivity at cold  $R_s \propto \sigma_n$
- But it becomes superconducting in the literature ☹
- Material dependence...
- Let's simply take  $\rho = 500 \mu\Omega\text{cm}$



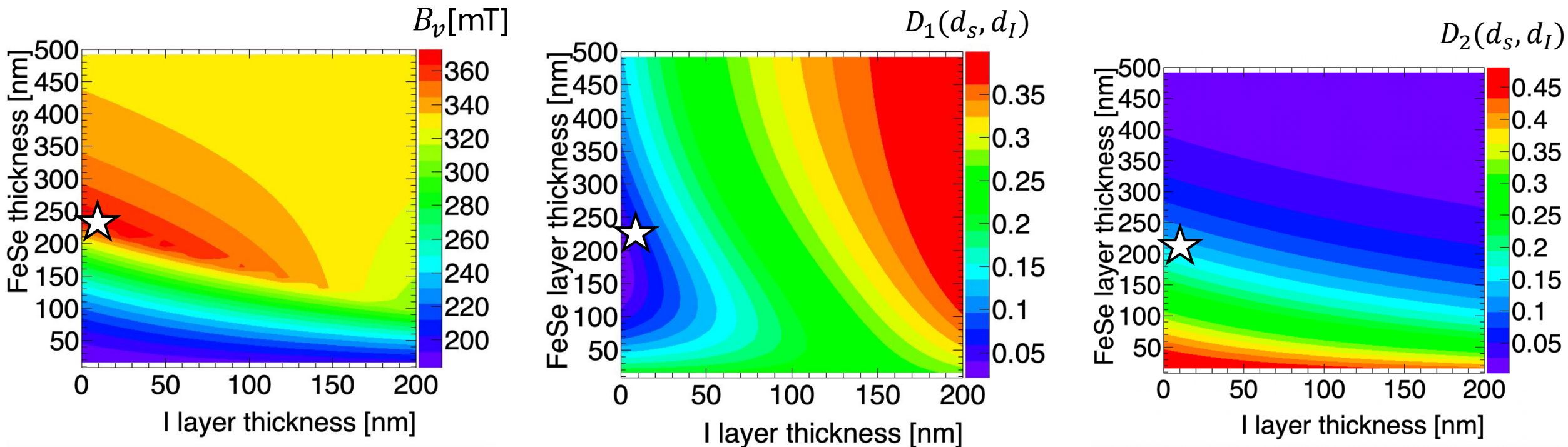
- Superconducting gap  $\Delta \sim 26 \text{ K}$
- In natural unit  

$$\Delta_{\text{FeSe}} \sim 2.2 \text{ meV} > \Delta_{\text{Nb}} = 1.5 \text{ meV}$$

TABLE III. Parameters determined from the heat capacity measurements

Sample	$\gamma_r$ (mJ/mol K <sup>2</sup> )	$\beta$ (mJ/mol K <sup>4</sup> )	$\gamma_n$ (mJ/mol K <sup>2</sup> )	$\Delta_0$ (K)	$2\Delta_0/T_c$
Br N5	5.2	0.75	24	26.6	3.94
F213	0.82	0.85	25	28.1	3.86
F216 step 1	0.96	0.94	25	25.9	3.57
F216 step 2	19.3	0.90	23	23	

# Multilayer BCS resistance for FeSe/(I)/Nb



For  $(d_I, d_s) = (0, 250 \text{ nm})$ ,  $D_1 \sim 0.1$ ,  $D_2 \sim 0.1$

$$R_S \sim R_{S,1} + R_{S,2} = \mu_0^2 \omega^2 \sigma_{0,1} \exp\left(-\frac{\Delta_1}{k_B T}\right) \lambda_1^3 D_1(d_s, d_I) + \mu_0^2 \omega^2 \sigma_{0,2} \exp\left(-\frac{\Delta_2}{k_B T}\right) \lambda_2^3 D_2(d_s, d_I)$$

$$= \mu_0^2 \omega^2 \lambda_2^3 \sigma_{0,Nb} \exp\left(-\frac{\Delta_{Nb}}{k_B T}\right) \left[ \frac{\sigma_{0,FeSe}}{\sigma_{0,Nb}} \left[ \frac{\exp(-\Delta_{FeSe}/k_B T)}{\exp(-\Delta_{Nb}/k_B T)} \right] \left( \frac{\lambda_{FeSe}}{\lambda_{Nb}} \right)^3 D_1(d_s, d_I) + D_2(d_s, d_I) \right]$$

$= R_{S,Nb}(T)$ 
 $= 0.004$ 
 $= 0.14$ 
**@4.2K**
 $= 125$ 
 $= 0.1$ 
 $= 0.1$

$$\sim 0.1 \times R_{S,Nb}(T = 4.2 \text{ K})$$

Large  $\rho_n \rightarrow$  small  $\sigma_n \rightarrow$  small  $R_S$

parameter	value
$\lambda_{FeSe}$ [nm]	200
$\lambda_{Nb}$ [nm]	40
$\Delta_{FeSe,1}$ [meV]	2.2
$\Delta_{Nb}$ [meV]	1.5
$\rho_{FeSe}$ [ $\mu\Omega\text{cm}$ ]	500
$\rho_{Nb}$ [ $\mu\Omega\text{cm}$ ]	2



# Outline

- Iron-based SC and recent applications
- Iron-based SC for SRF?
- Surface resistance of Iron-based SC
- ML theory for Iron-based SC
- **Remarks**
- Conclusion

# Residual resistance caused by weak link

PHYSICAL REVIEW B

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1 MARCH 1991

## Residual surface resistance of polycrystalline superconductors

Carmine Attanasio, Luigi Maritato, and Ruggero Vaglio  
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 (Received 2 April 1990; revised manuscript received 29 August 1990)

Journal of Superconductivity, Vol. 8, No. 6, 1995

## Nonlinear Surface Impedance of YBCO Thin Films: Measurements, Modeling, and Effects in Devices

Daniel E. Oates,<sup>1</sup> Paul P. Nguyen,<sup>2</sup> Gene Dresselhaus,<sup>3</sup> Mildred S. Dresselhaus,<sup>4</sup> Gad Koren,<sup>5</sup> and Emil Polturak<sup>5</sup>

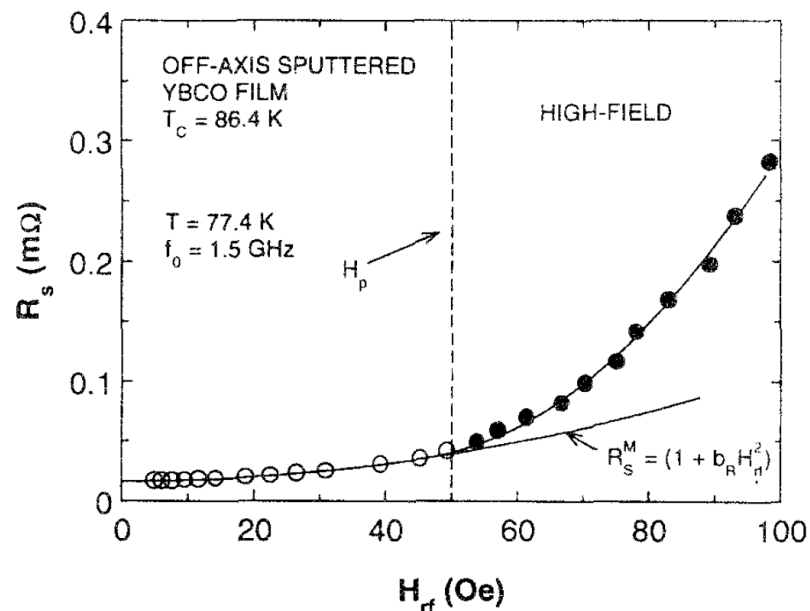
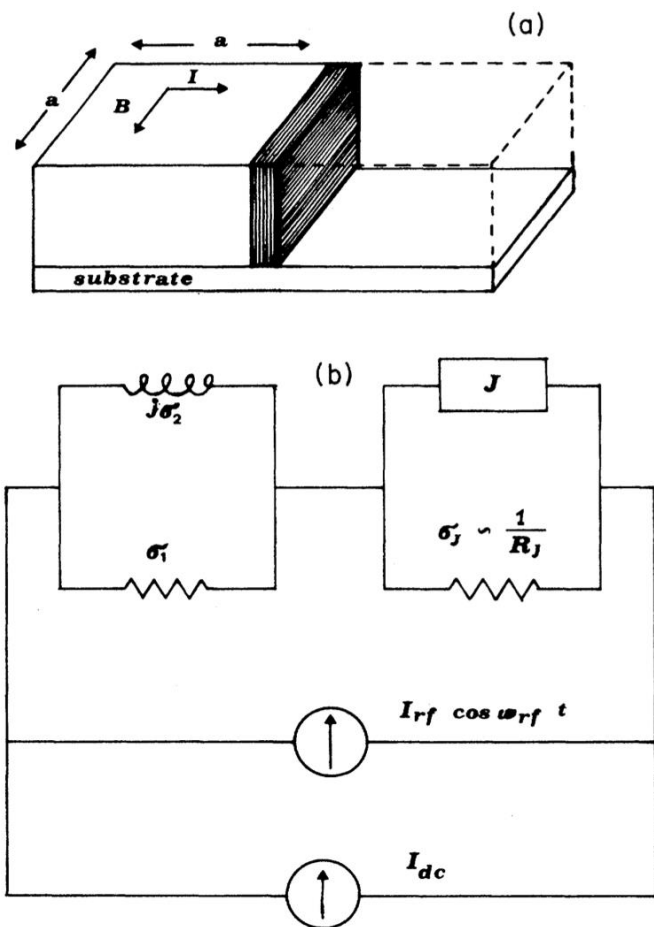


Fig. 7.  $R_S$  vs.  $H_{rf}$  showing the low- and intermediate-field region ( $\circ$ ), which is fitted by the modified coupled-grain model as shown by  $R_S^M$  and the high-field region ( $\bullet$ ), which is fitted by the combination of the coupled-grain model and the Bean model.

- It is known that YBCO showed nonlinear residual resistance (Q-slope) well explained by the weak link model
- Iron-based superconductors also show weak-link structure (from wire studies)
- This term would appear on top of quasi-particle contributions discussed so far

# Outlook: probably 30-year business

- More reliable material parameters (?)
  - Sample measurement on DC electric conductivity at cold
- Multi-layer sample
- Weak link calculation on multilayer
- Dielectric loss
- Find collaborators
  - Material science
  - Theorists
  - RF engineers



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# Conclusion

- 16 years have passed since Iron-based SC was discovered in 2008
- Application of Iron-based SC for wire / tape / magnet is a hot topic
- RF application has been limited
  - Recent proposal for axion dark matter project
- Multilayer would be the way to go
  - Enhancement of critical fields has been experimentally shown
  - Enhancement of surface barrier was re-calculated (London equation)
- Gapless nature would also be excellent for surface resistance
  - The conventional BCS-like formula may still be valid
  - Long penetration depth is problematic → layer thick thinner than  $\lambda$
- Multilayer surface resistance was estimated
  - Small normal conducting DC electric conductivity helps (if the theory is valid)
- Residual resistance from weak link must be evaluated as well
- Looking for somebody who are willing to collaborate

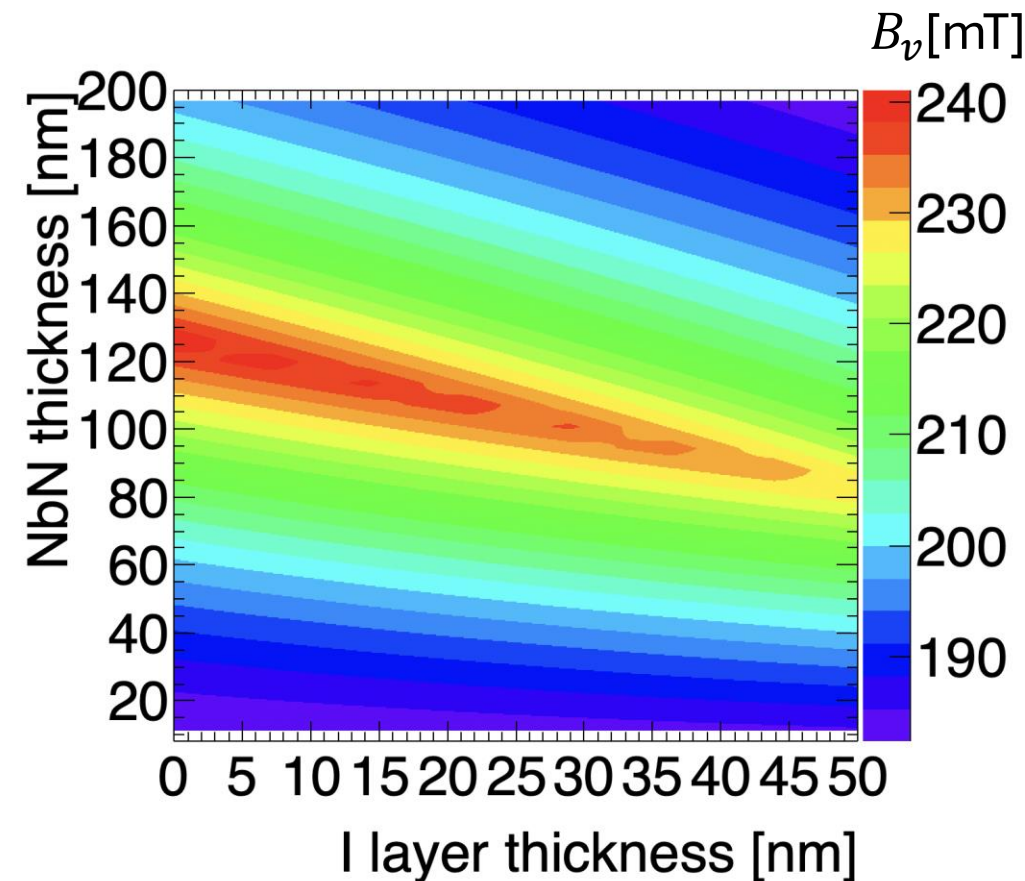
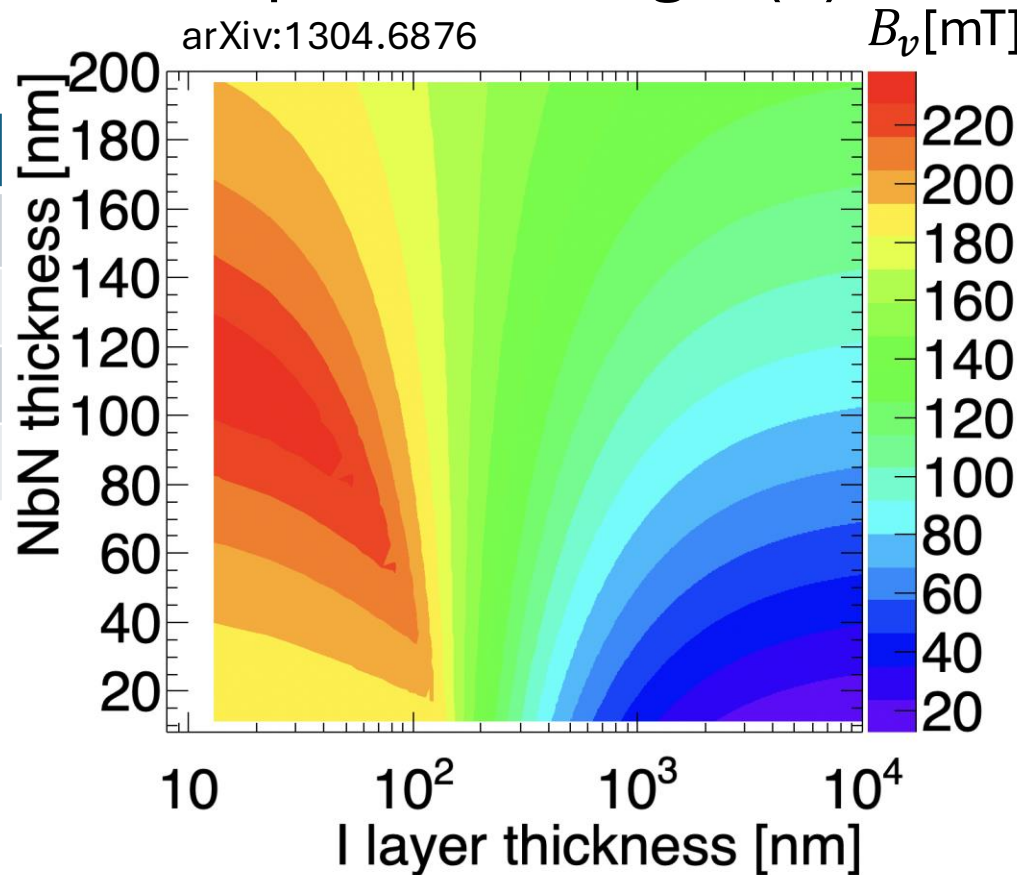
backup

# Kubo's calculation for NbN/I/N was reproduced

Reproduced Fig.3 (a)

arXiv:1304.6876

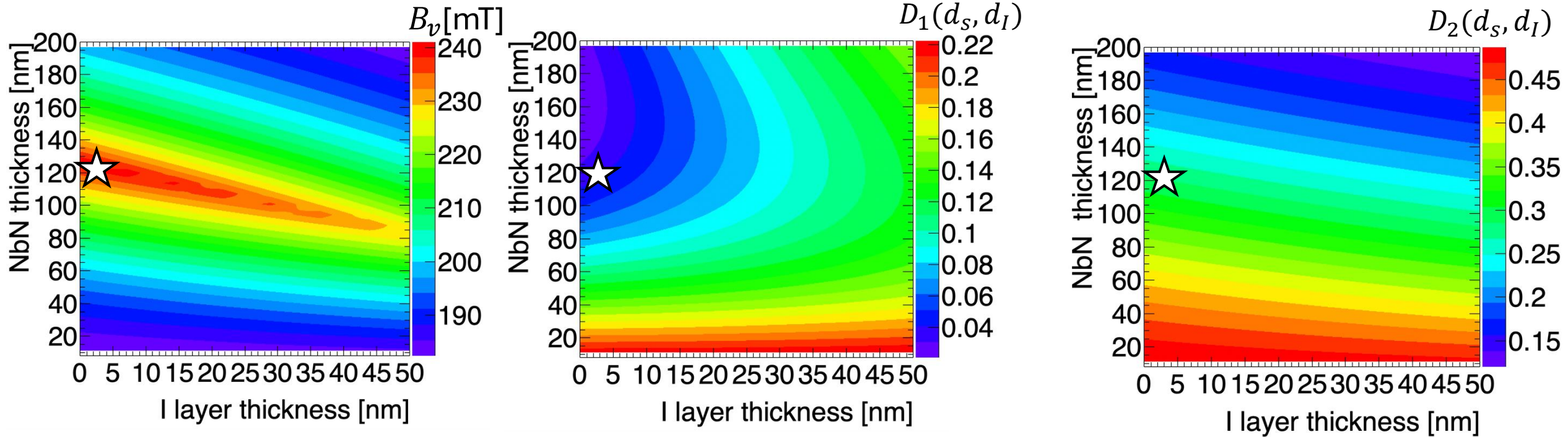
Enlarged around thinner I layer



parameter	value
$\xi_{NbN}$ [nm]	5
$\lambda_{NbN}$ [nm]	200
$\lambda_{Nb}$ [nm]	40
$B_{shNb}$ [mT]	180

ML enhancement of the breakdown field from 180 mT to 240 mT is predicted with NbN thickness around 120 nm without an insulation layer

# Multilayer BCS resistance for NbN/I/Nb



For  $(d_I, d_s) = (0, 120 \text{ nm})$ ,  $D_1 \sim 0.05$ ,  $D_2 \sim 0.3$

$$R_S \sim R_{S,1} + R_{S,2} = \mu_0^2 \omega^2 \sigma_{0,1} \exp\left(-\frac{\Delta_1}{k_B T}\right) \lambda_1^3 D_1(d_s, d_I) + \mu_0^2 \omega^2 \sigma_{0,2} \exp\left(-\frac{\Delta_2}{k_B T}\right) \lambda_2^3 D_2(d_s, d_I)$$

$$= \mu_0^2 \omega^2 \lambda_2^3 \sigma_{0,Nb} \exp\left(-\frac{\Delta_{Nb}}{k_B T}\right) \left[ \frac{\sigma_{0,NbN}}{\sigma_{0,Nb}} \left[ \frac{\exp(-\Delta_{NbN}/k_B T)}{\exp(-\Delta_{Nb}/k_B T)} \right] \left( \frac{\lambda_{NbN}}{\lambda_{Nb}} \right)^3 D_1(d_s, d_I) + D_2(d_s, d_I) \right]$$

$= 0.029 \quad = 0.048 \text{ @4.2K} \quad = 125 \quad = 0.05 \quad = 0.3$

$= 0.017 \times R_{S,Nb}(T) \Big|_{T=4.2 \text{ K}}$

**ML is promising for higher Q not only high gradient**

parameter	value
$\lambda_{NbN}$ [nm]	200
$\lambda_{Nb}$ [nm]	40
$\Delta_{NbN}$ [meV]	2.6
$\Delta_{Nb}$ [meV]	1.5
$\rho_{NbN}$ [ $\mu\Omega\text{cm}$ ]	70
$\rho_{Nb}$ [ $\mu\Omega\text{cm}$ ]	$2^{32}$