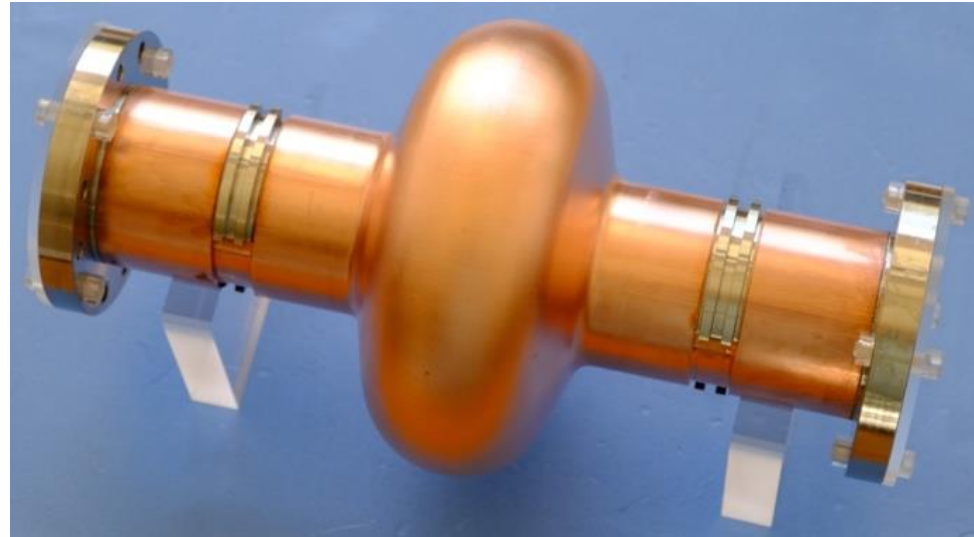


# Copper full-seamless substrate cavity manufactured by hydroforming

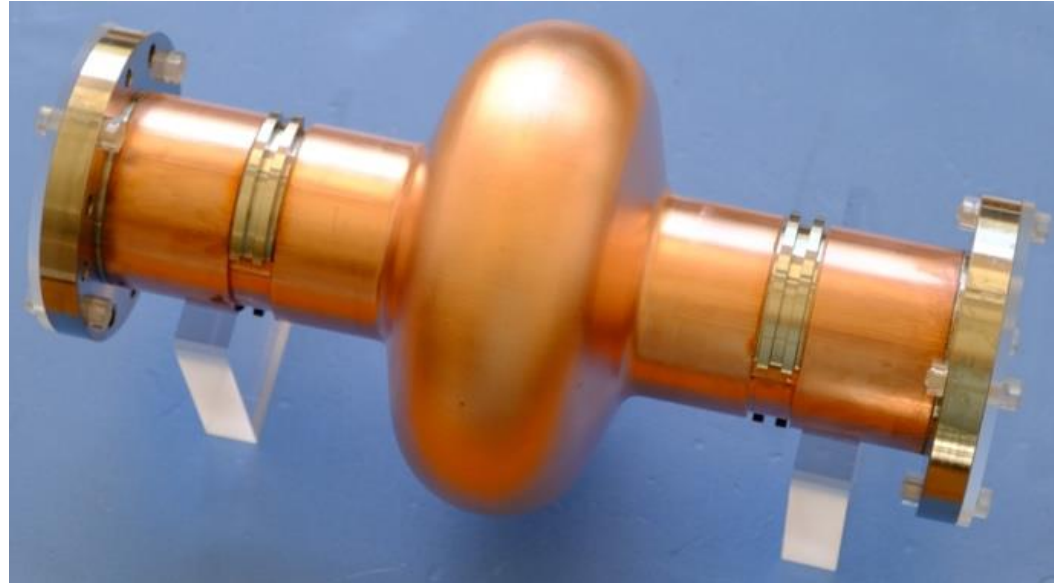


YAMANAKA Masashi, ARAKI Hayato,  
Guillaume Jonathan Rosaz,

Said Atieh, Marco Garlasche, Joanna Sylwia Swieszek

# Contents

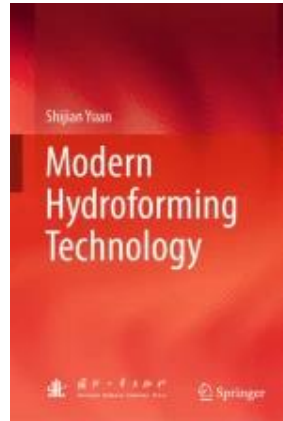
- Fabrication of full seamless cavity
- Niobium coating
- RF test



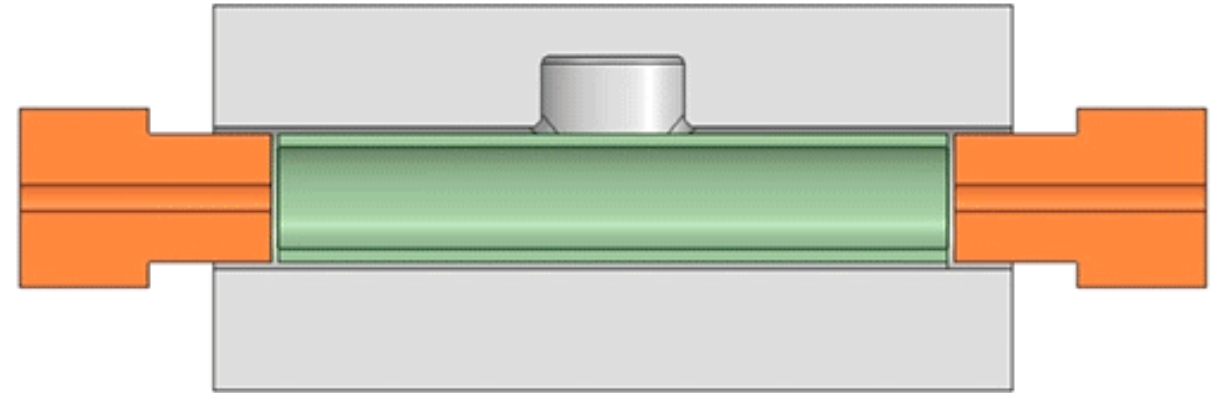
1.3 GHz one-cell full-seamless copper substrate cavity

# Tube hydroforming

Well-known plastic forming technique



Shijian Yuan, Springer



Principle of hydroforming

<https://www.tube-forming.co.jp/bulge.html>



Bellows



Automobile parts  
Hydraulic joints



Flexible tubes



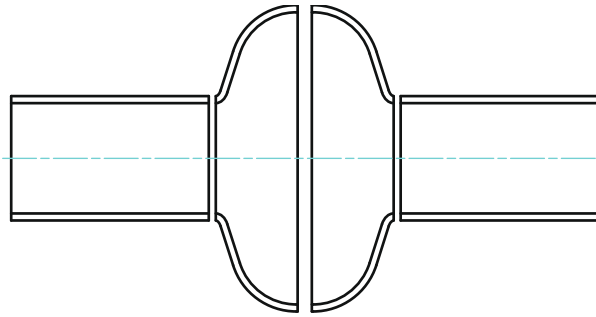
Hollow flame parts

<https://sango.jp/pipe.html>

## Industrial applications

# Full-seamless cavity concept

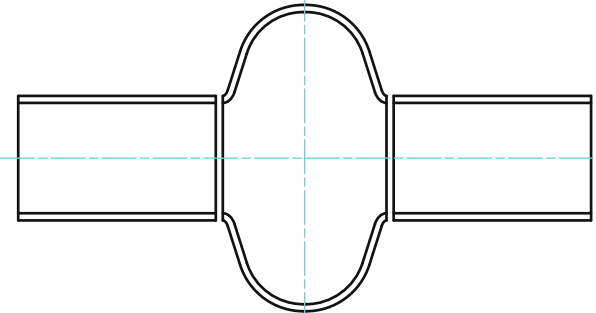
Conventional (4 pieces)



Cell part is manufactured by press-forming and EB welded with beam tubes



Seamless (3 pieces)

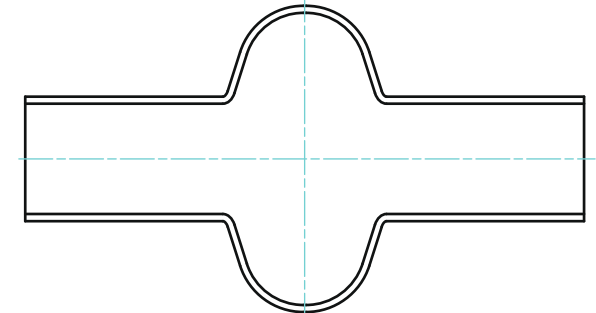


Cell part is manufactured by hydroforming from a seamless tube, then EB welded with beam tubes

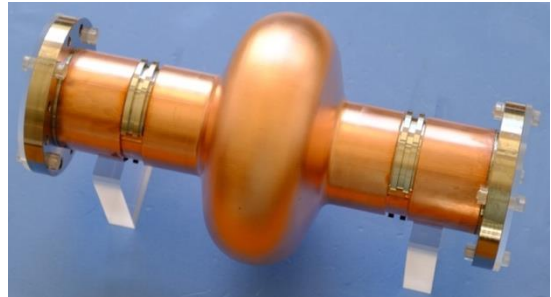
**KEK** succeeded 3-cell bulk niobium cavity in this method.



Full seamless (1 piece)

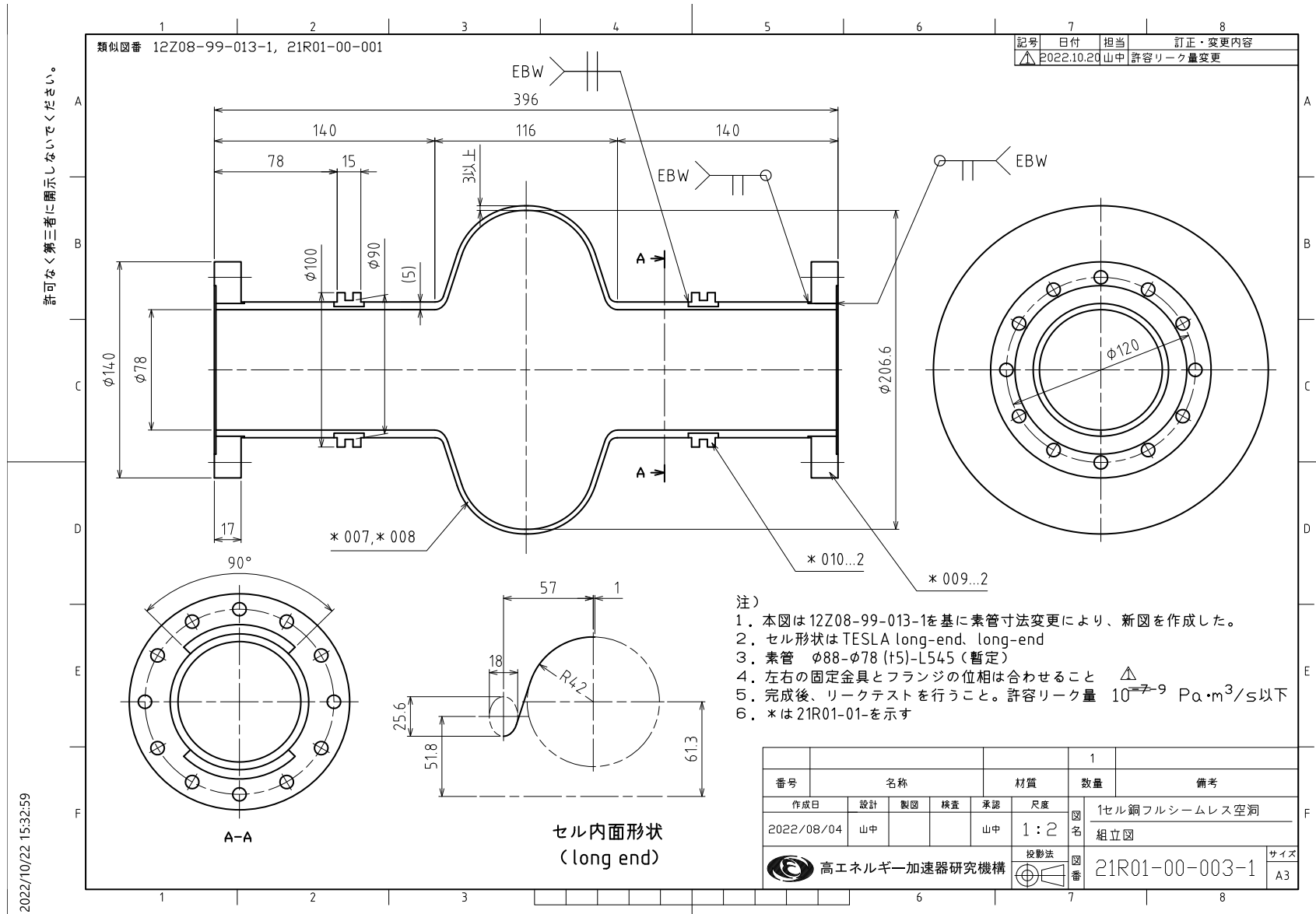


Whole cavity is manufactured by hydroforming from one seamless tube. There is no welding part (no bead).

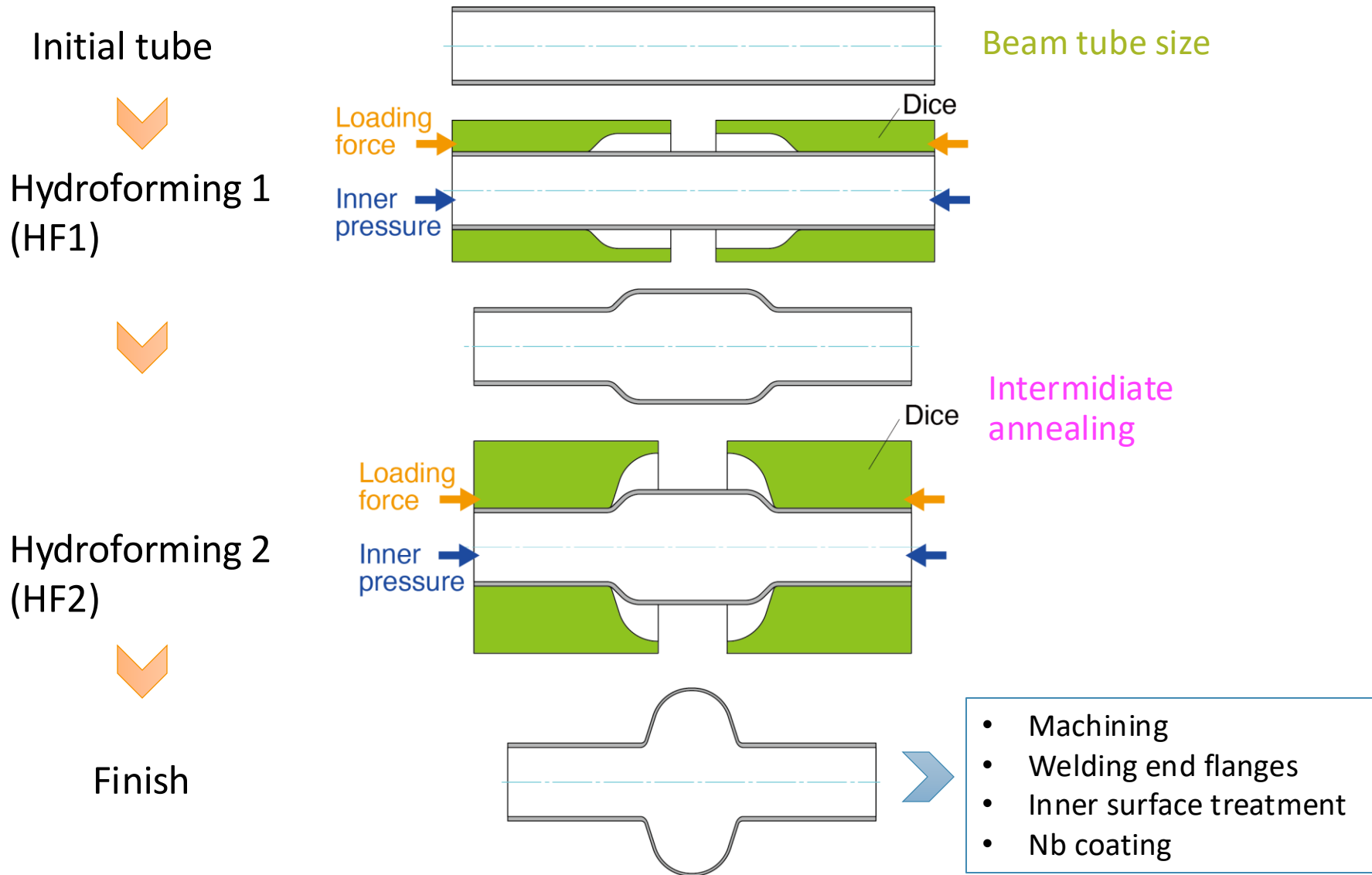


- This time, we try an **OFE copper** substrate cavity for niobium coating.
- There is no welding bead on equator and iris parts so that inner surface is so smooth. It has a big merit for niobium coating.

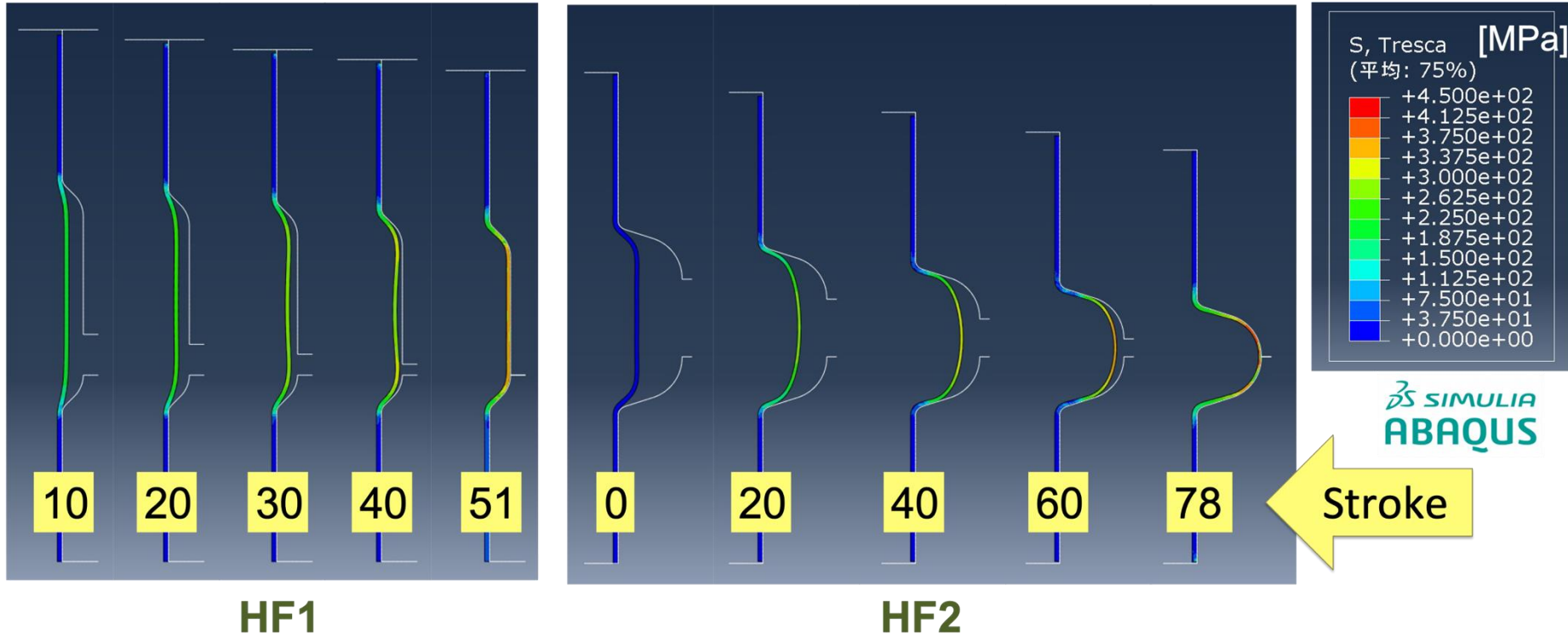
# 1.3 GHz one-cell full-seamless copper cavity



# Optimized manufacturing process

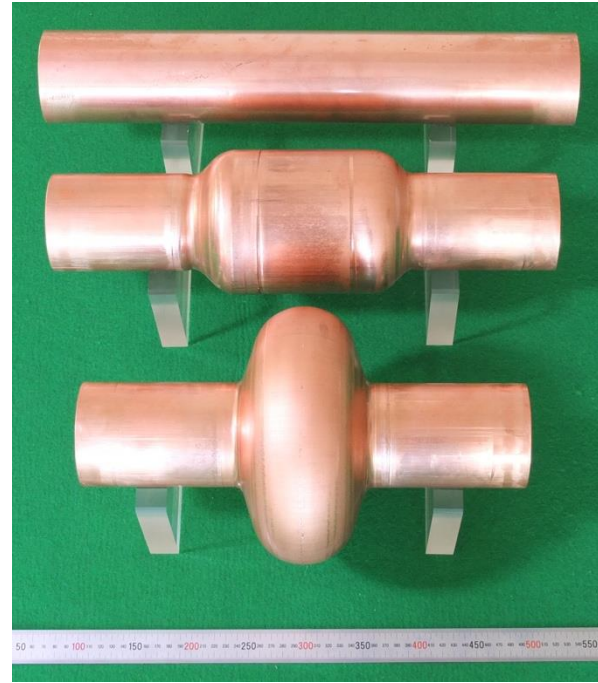
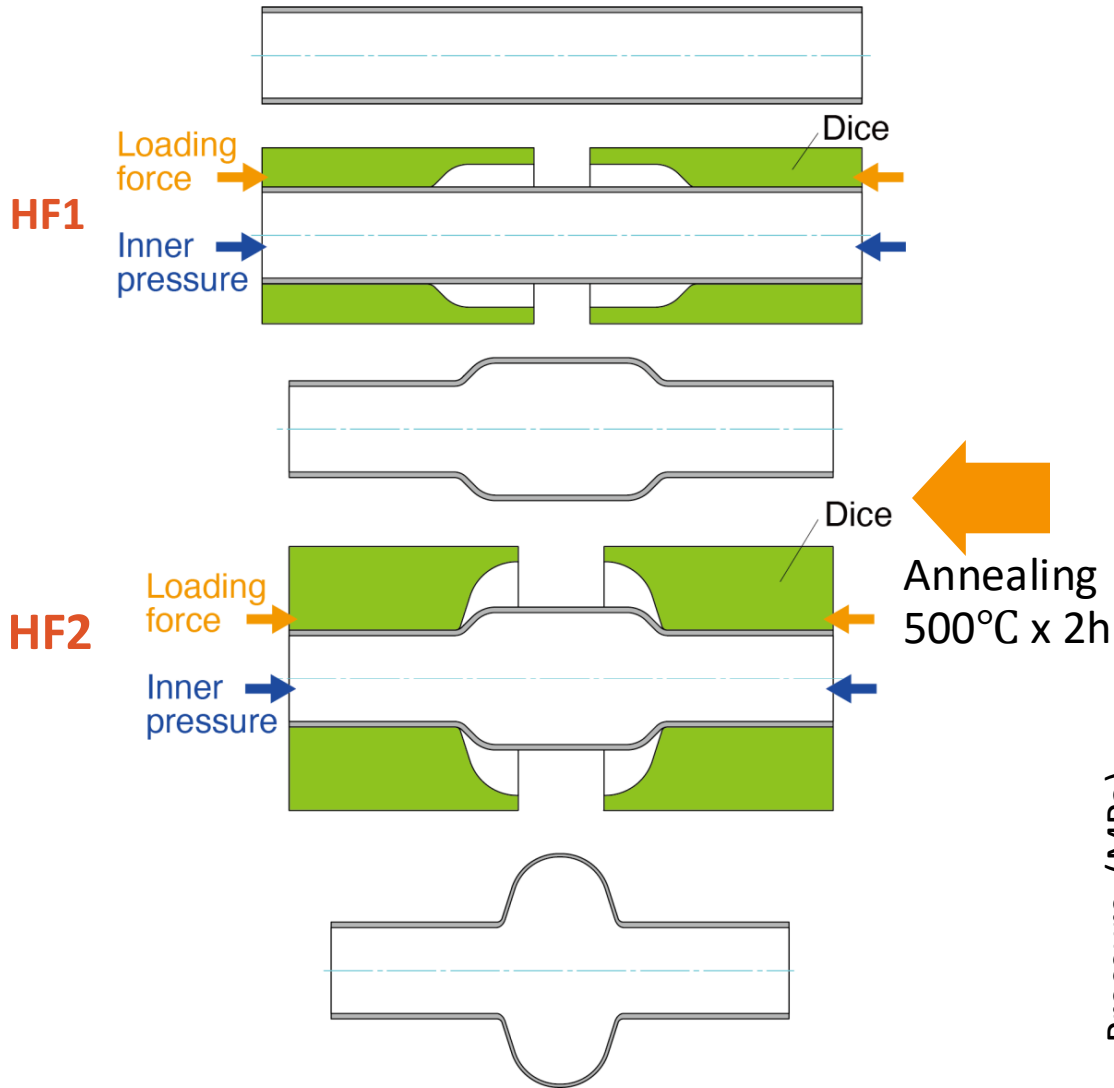


# Simulation



**Tresca** stress distribution according to stroke  
MAX. stresses are 381.5 and 424.1 MPa at HF1 and HF2, respectively  
Hydroforming is held in vertical. Lower die is fixed, and upper die moves to the downward direction (see pic. next page).

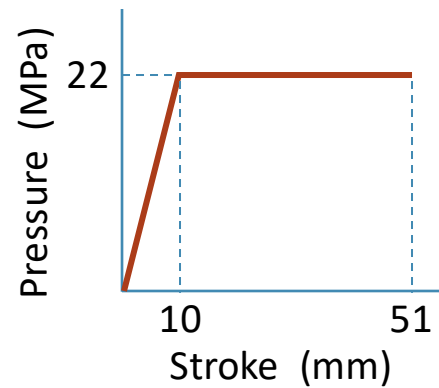
# Successful hydroforming



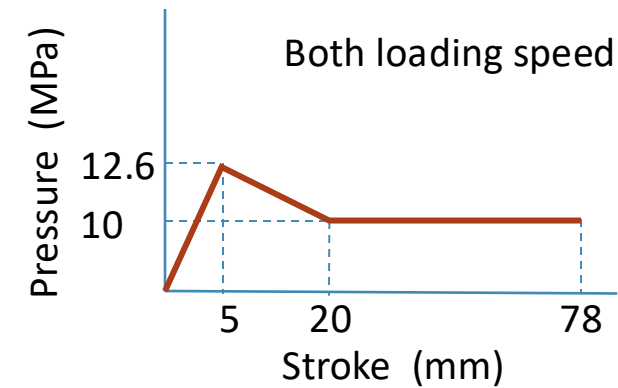
Hydroformed copper tubes



Hydroforming machine



**HF1 (1 pass)**

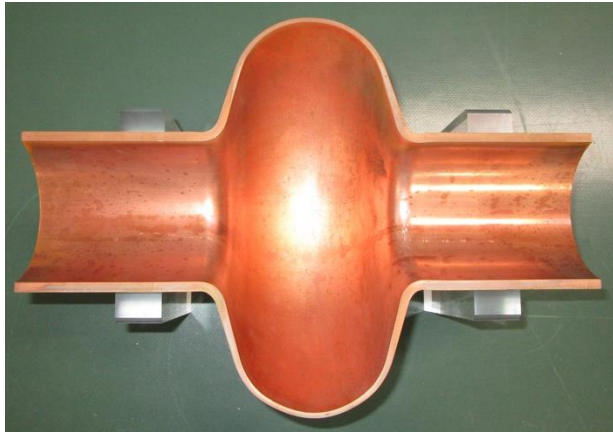


**HF2 (1 pass)**

Both loading speeds: 1 mm/s



# Measurement of roughness



Cut piece of cavity



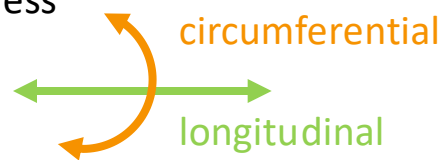
Close up at beam tube



Close up at equator



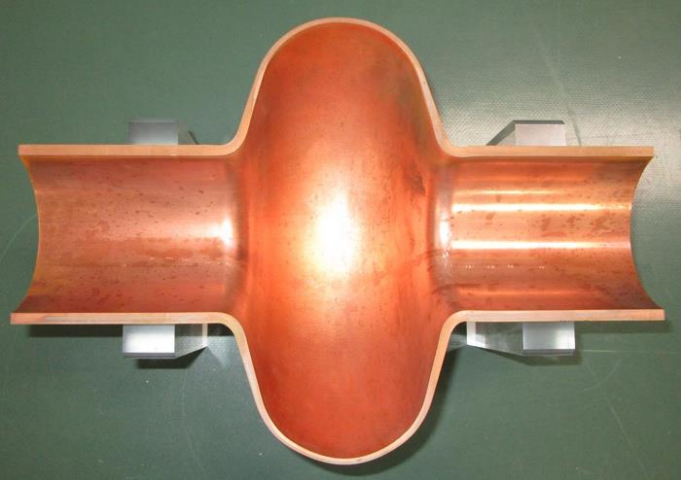
Plastic replica is used for roughness measurement



Measured roughness [ $\mu\text{mRa}$ ]

Direction	Beam tube	Equator
longitudinal	1.0	2.9
circumferential	0.8	2.6

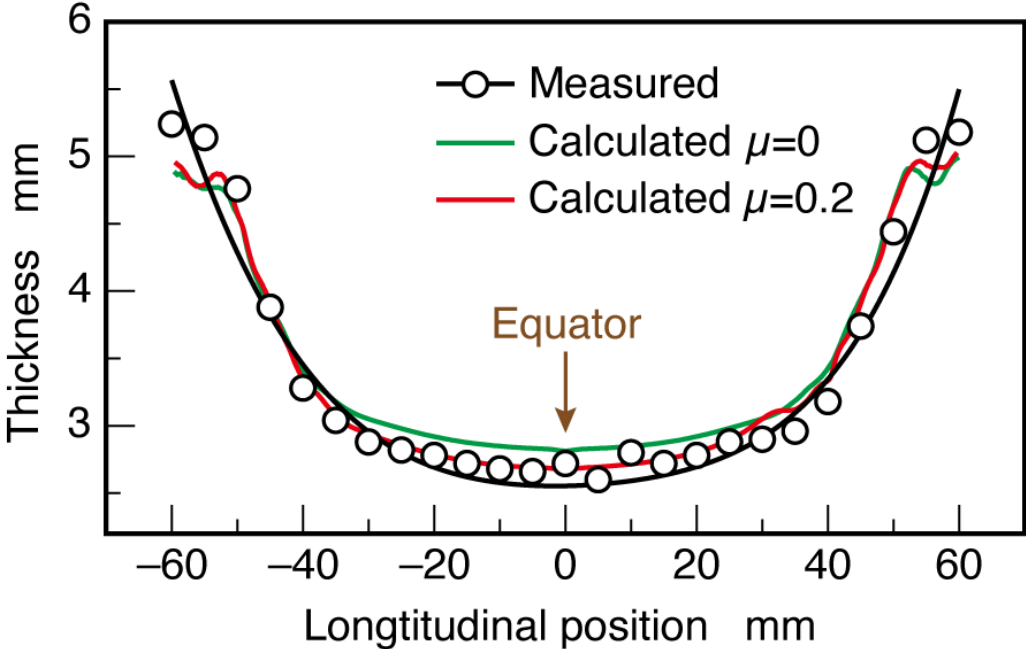
# Thickness distribution



The wall at equator becomes thick



Thickness was measured by caliper

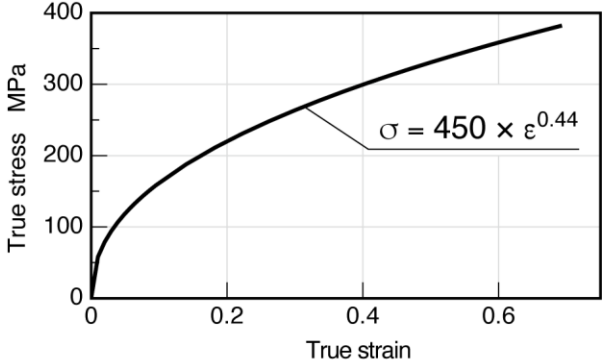


Comparison between measured and calculated thickness

In case of  $\mu=0.2$ , measured and calculated results agreed well



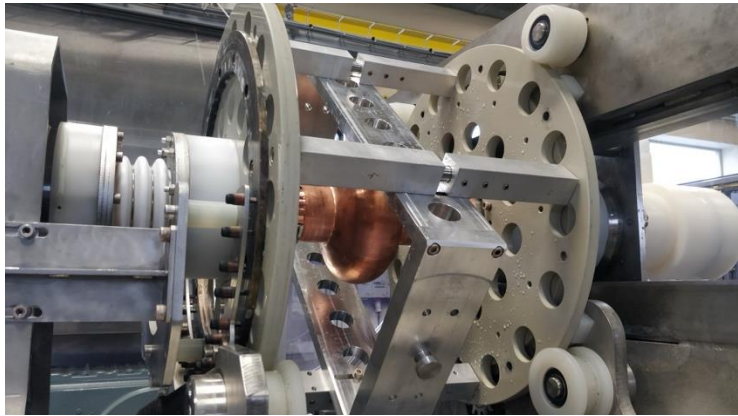
We will apply to design of dice considering thickness distribution



Tensile test was achieved using the specimen from actual copper tube

# Nb thin film coating

## Process flow



Cavity on the EP bench



Cavity on the HPR setup



Cavity's cell surface during cleanroom assembly



Cavity on the coating bench

# Nb thin film coating

## Process parameters

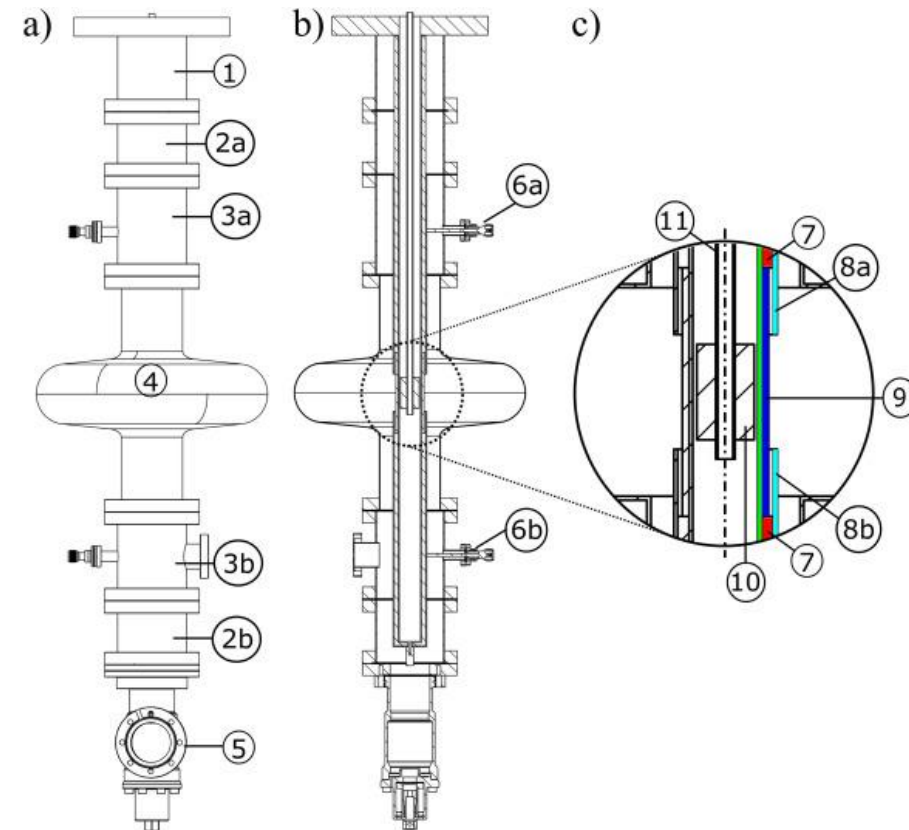
**EP:** 40 minutes, target 12  $\mu\text{m}$  removed material.

**HPR:** 100 bars, 3 hours, cavity dried under vacuum at 50°C.

**Bakeout:** 48h, 200 °C, base pressure  $\sim 2 \cdot 10^{-10}$  mbar

**Coating:** HiPIMS

- cut-offs: 350W,  $2.5 \cdot 10^{-2}$  mbar Kr, 6 positions/cut-off, 150 °C, unbiased.
- cell: 2 kW,  $2.5 \cdot 10^{-3}$  mbar Kr, 6 hours, 150 °C, -75V bias voltage
- Targeted thickness at the equator: 6  $\mu\text{m}$



Coating apparatus schematic

<https://doi.org/10.1016/j.surfcoat.2022.128306>

# RF Measurement

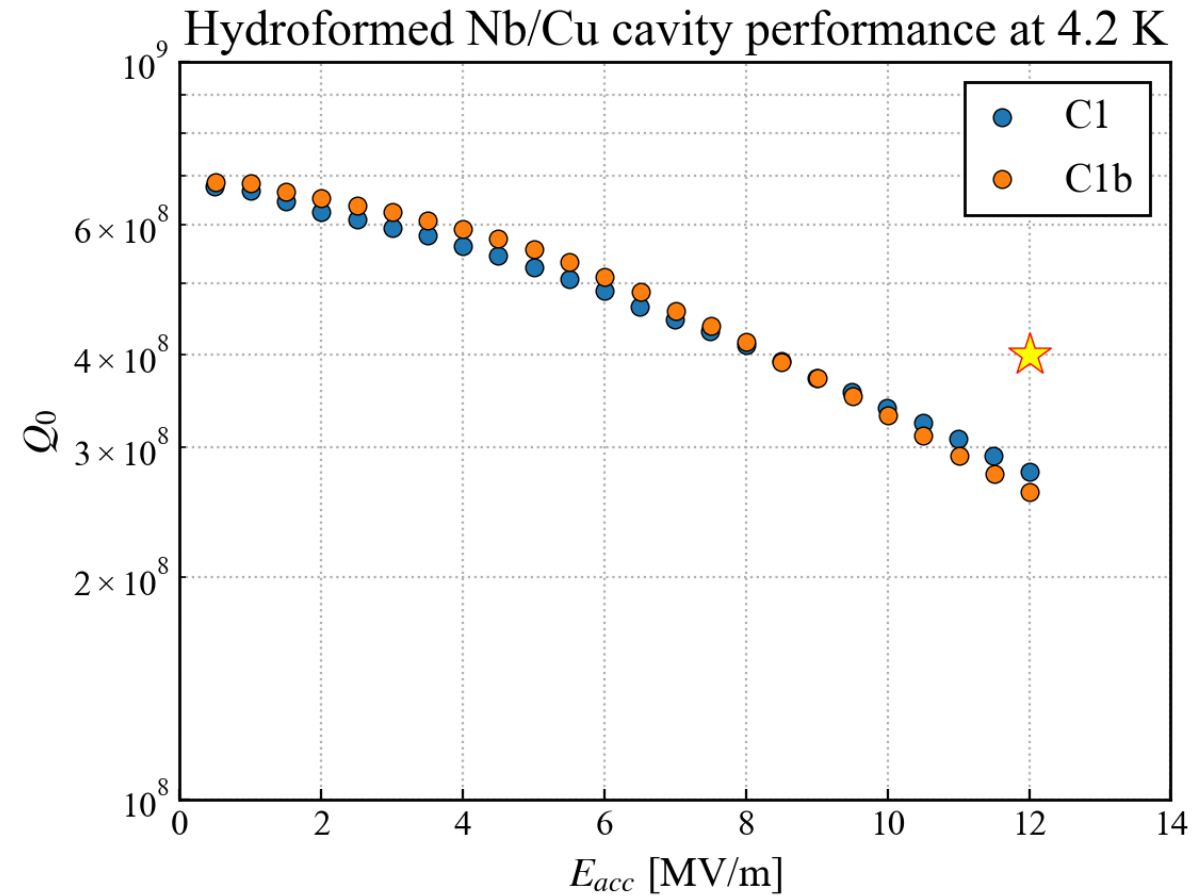
## 4.2 K Measurement

Target:  $Q > 4 \times 10^8$  at 12 MV/m

Equivalent with  $Q > 3 \times 10^9$  at 4.5 K, 400 MHz (FCC)

Result (at KEK, March 2024):

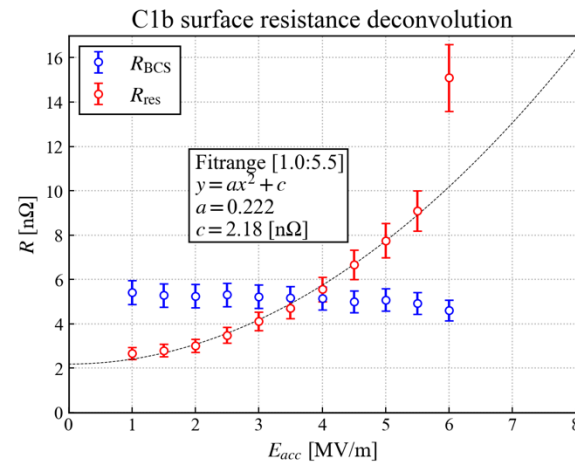
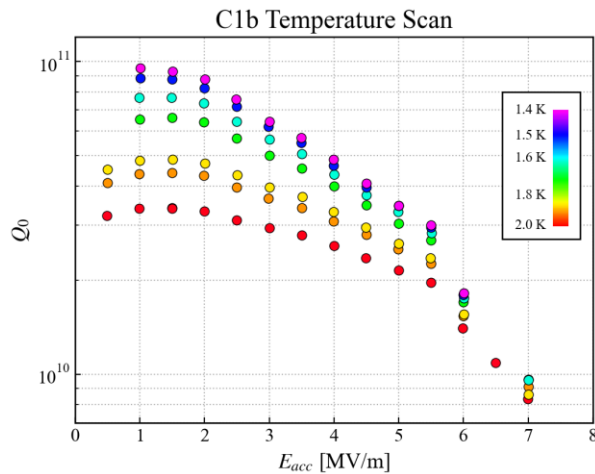
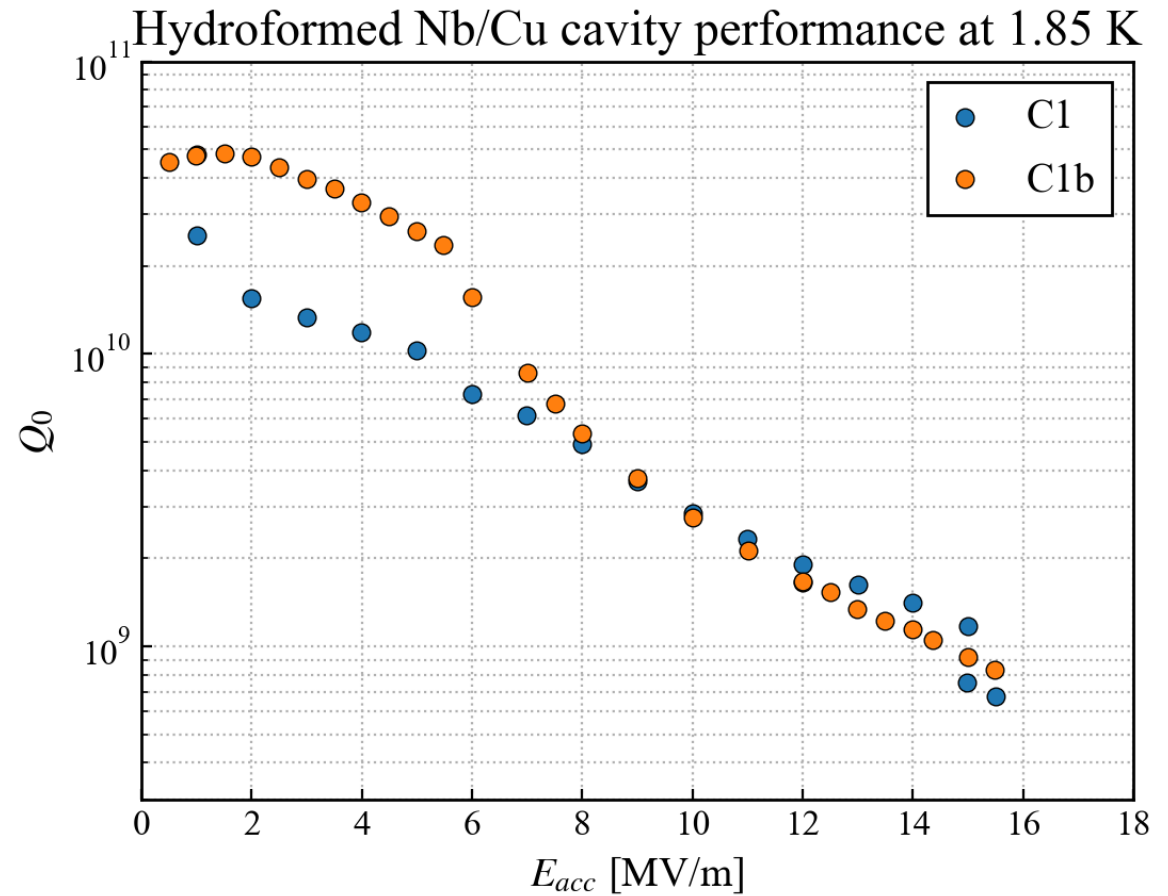
- Could not reach Q requirement
  - $2.6\text{-}2.8 \times 10^8$  at 12 MV/m
- Stopped at 12 MV/m due to power limit
- No field emission
- No quench
- Good reproducibility between the two cavities



# RF Measurement

## Below 2.0 K

- Max  $E_{acc}$ : 15.5/15.7 MV/m (C1/C1b, 1.85 K)
- Max  $Q_0$ :  $9.5 \times 10^{10}$  (C1b: 1.40 K, 1.0 MV/m)
- Quench field exceeded 12 MV/m without field emission
- High quality factor in low field
- $Q$  slope was too steep in high field
  - There is still room for improvement in surface treatment.
- Minimizing temperature gradient on  $T_c$  is essential.



# Summary

- An optimized manufacturing method has been achieved, for the cavity without seam by hydroforming
- We succeeded in manufacturing of a full seamless cavity by **hydroforming**. We thank the strong collaboration with NEURON (Japan) and CERN
- Niobium thin film was coated with HiPIMS at CERN
- RF performance was measured at KEK and confirmed to be close to FCC requirement

## Acknowledgements



EN-MME, TE-VSC, SY-RF