



# CAS Advanced Accelerator Physics

## Collective effects

### Part 3: Transverse wake fields – impact on machine elements and beam dynamics

Kevin Li and Giovanni Rumolo

We have **discussed longitudinal wake fields** and impedances and their impact on both the machine as well as the beam.

We have learned about **beam induced heating** and how it is related to the beam power spectrum and the machine impedance.

We have discussed the effects of **potential well distortion** (stable phase and synchrotron tune shifts, bunch lengthening and shortening).

We have seen one example of **longitudinal instabilities** (Microwave).

## Part 3: Multiparticle dynamics with wake fields – their different types and impact on transverse beam dynamics

- Transverse wake function and impedance
- Effect on a bunch and transverse „potential well distortion“
- Some examples of beam instabilities

We will move to the description and the impact of **transverse wake fields**.

We will discuss the **different types** of transverse wake fields, outline how they can be implemented numerically and then investigate **their impact on beam dynamics**.

We will see some **examples of transverse instabilities** such as the transverse mode coupling instability (TMCI) or headtail instabilities.

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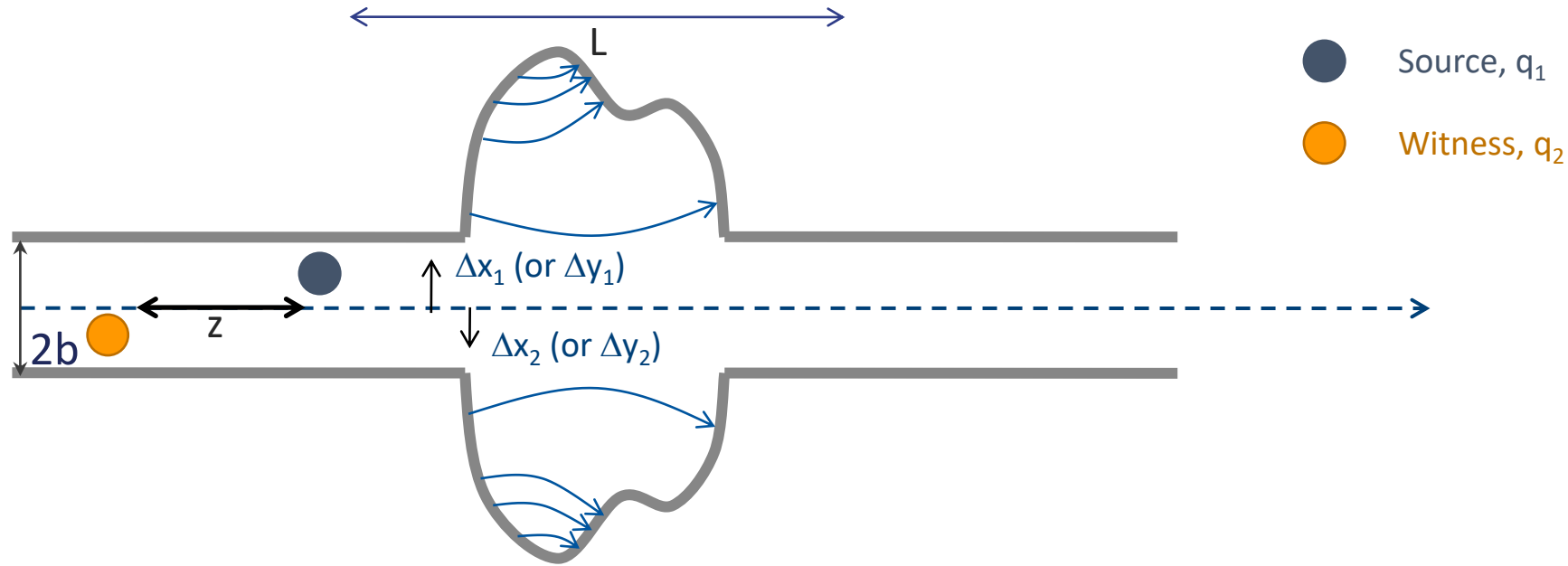
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## Part 3: Multiparticle dynamics with wake fields – their different types and impact on transverse beam dynamics

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# Recap: wake functions in general



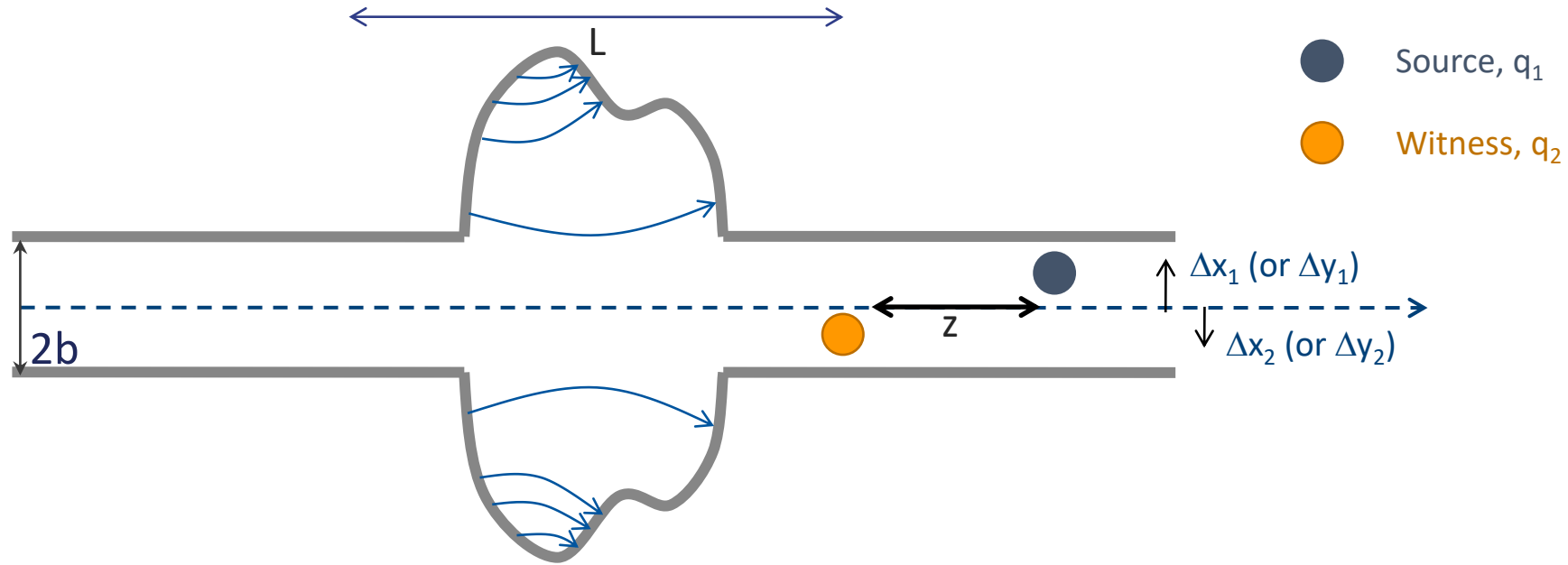
Definition as the **integrated force** felt by a witness charge following a source charge ('energy kick'):

- In general, for two point-like particles, we have

$$\Delta E_2 = \int F(x_1, x_2, z, s) ds = -q_1 q_2 w(x_1, x_2, z)$$

$w$  is typically expanded in the transverse offsets of source and witness particles. This yields the different types of wake fields (dipole, quadrupole, coupling wakes)

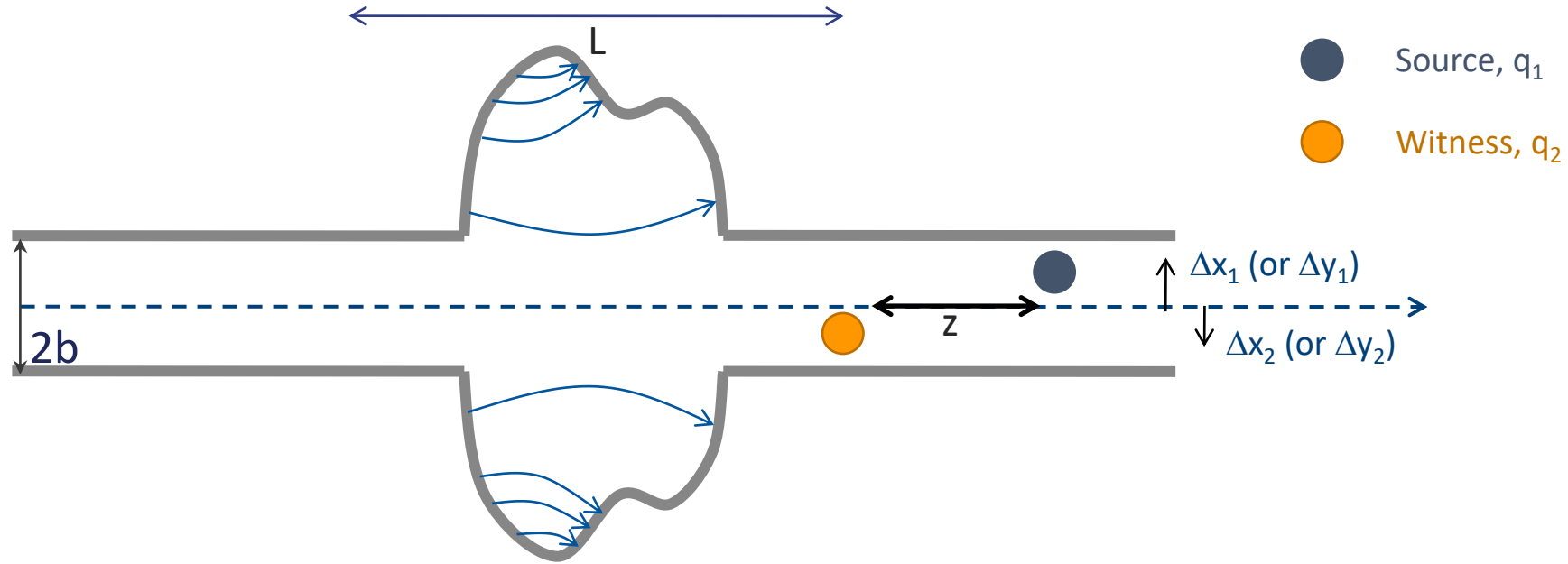
# Transverse wake functions



- Transverse wake fields

$$\beta c \Delta p_{x2} = \int F_x(x_1, x_2, z, s) ds$$

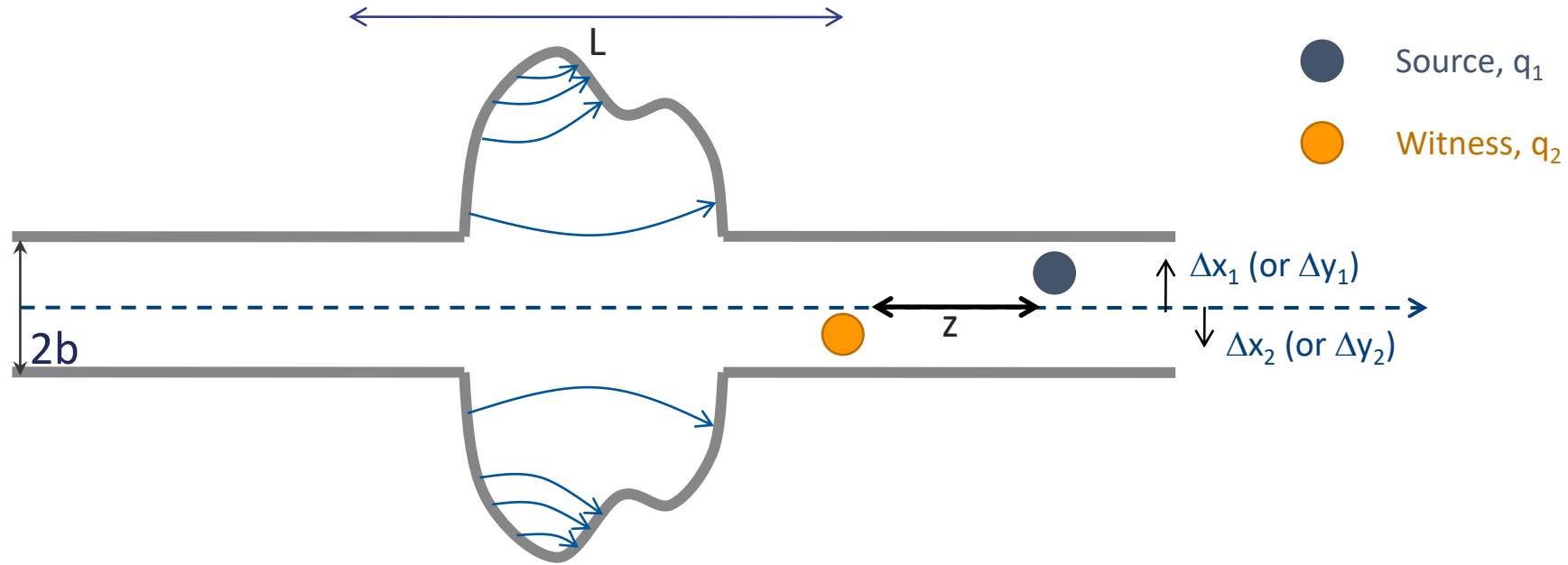
# Transverse wake functions



- Transverse wake fields

$$\beta c \Delta p_{x2} = \int F_x(x_1, x_2, z, s) ds = -q_1 q_2 (W_{C_x}(z) + W_{Dx}(z) \Delta x_1 + W_{Q_x}(z) \Delta x_2)$$

# Transverse wake functions



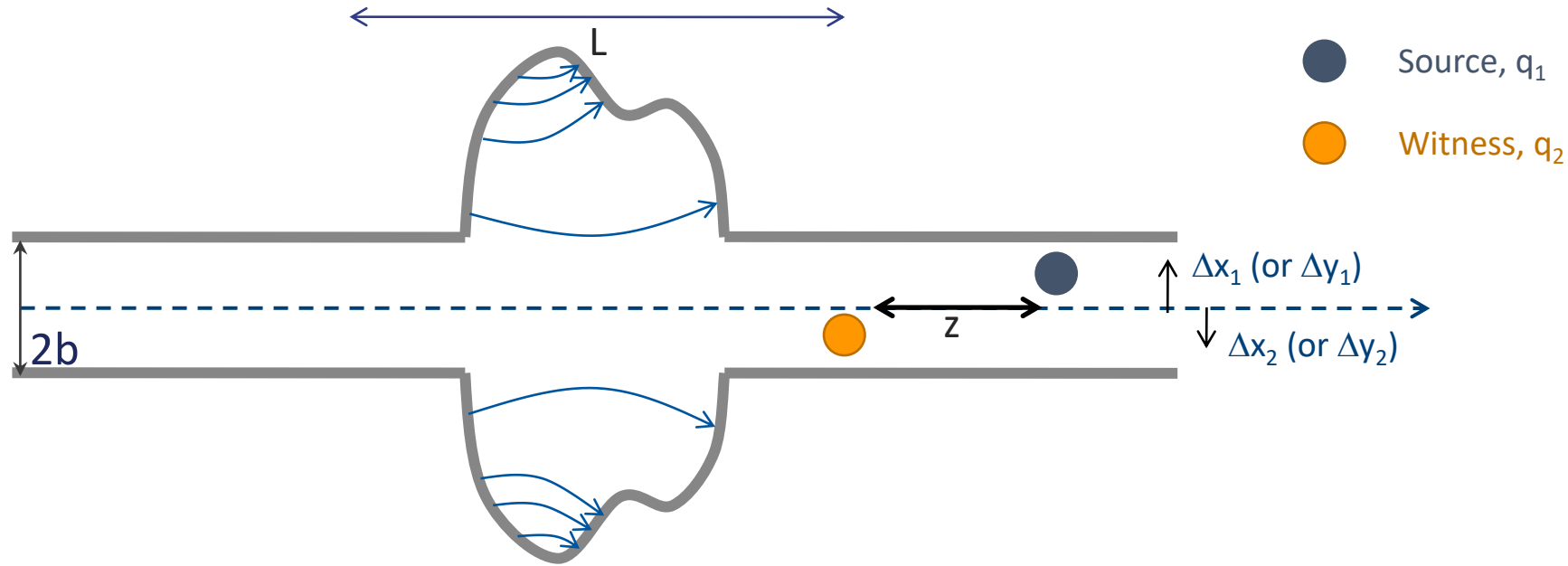
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$$\longrightarrow \frac{\Delta p_{x2}}{p_0} = \Delta x'_2$$

**Transverse deflecting kick of the witness particle from transverse wakes**

# Transverse wake functions



- Transverse wake fields

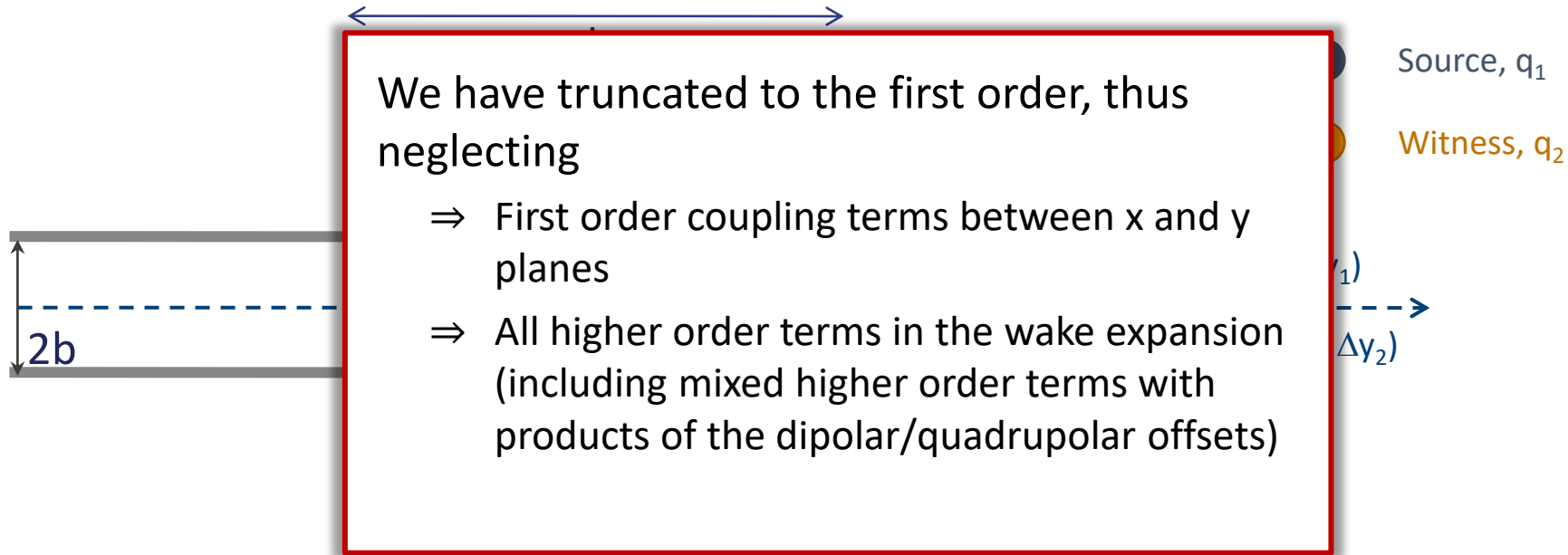
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Zeroth order for  
 asymmetric structures  
 → Orbit offset

Dipole wakes –  
 depends on **source particle**

Quadrupole wakes –  
 depends on **witness particle**

# Transverse wake functions



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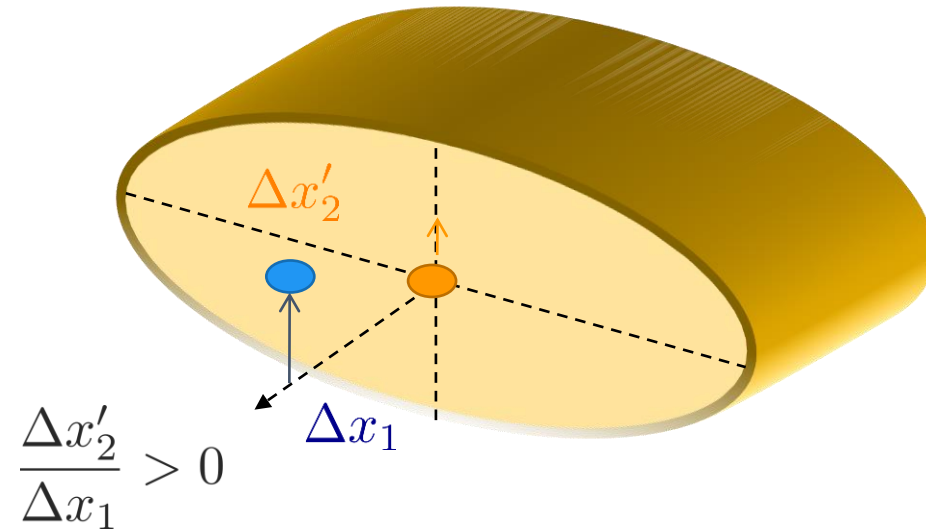
Dipole wakes – depends on **source particle**

Quadrupole wakes – depends on **witness particle**

# Transverse dipolar wake function (driving)

$$W_{D_x}(z) = -\frac{\beta^2 E_0}{q_1 q_2} \frac{\Delta x'_2}{\Delta x_1} \xrightarrow{z \rightarrow 0} W_{D_x=0}(0) = 0$$

- The value of the transverse dipolar wake function **in  $z=0$  vanishes** because source and witness particles are traveling parallel and they can only – mutually – interact through space charge, which is not included in this framework
- $W_{D_x}(0^-) < 0$  since trailing particles are **deflected toward the source particle** ( $\Delta x_1$  and  $\Delta x'_2$  have the same sign)

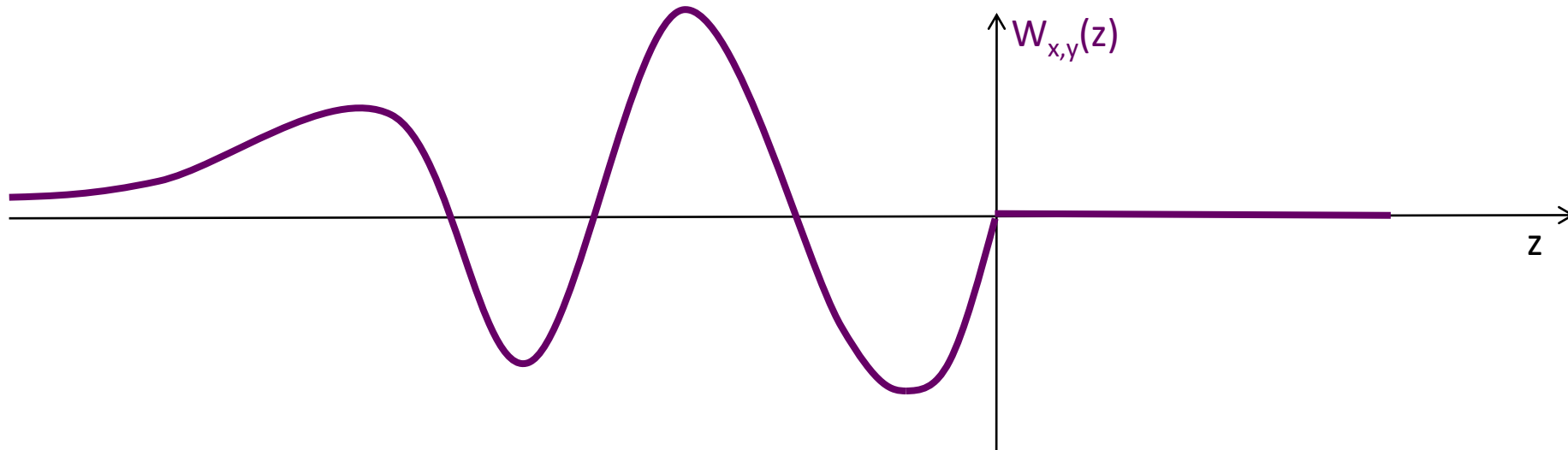




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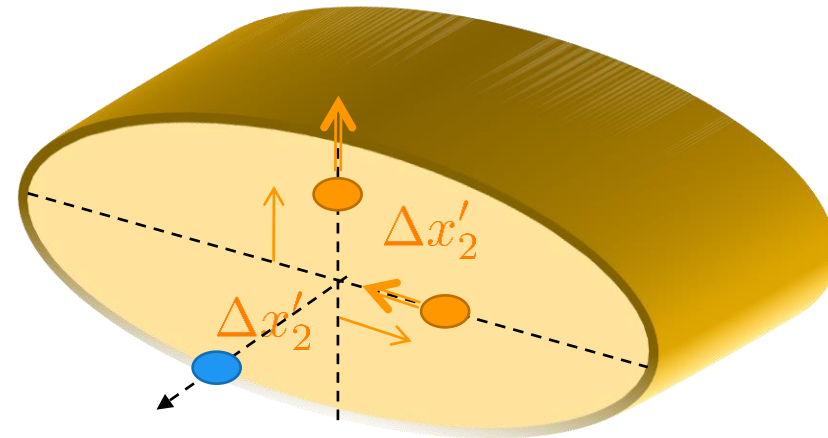
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- $W_{D_x}(z)$  has a discontinuous derivative in  $z=0$  and it vanishes for all  $z > 0$  because of the ultra-relativistic approximation



# Transverse quadrupolar wake function (detuning)

$$W_{Q_x}(z) = -\frac{\beta^2 E_0}{q_1 q_2} \frac{\Delta x'_2}{\Delta x_2} \xrightarrow{z \rightarrow 0} W_{Q_x=0}(0) = 0$$

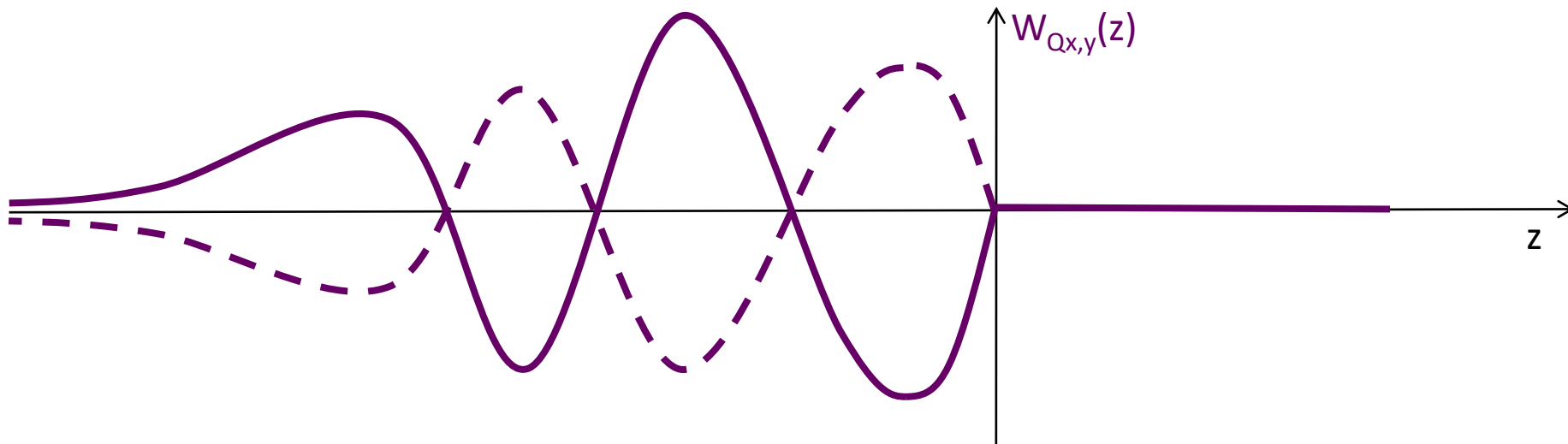
- The value of the transverse quadrupolar wake function **in  $z=0$  vanishes** because source and witness particles are traveling parallel and they can only – mutually – interact through space charge, which is not included in this framework
- $W_{Q_x}(0^-) < 0$  can be of either sign since trailing particles can be **either attracted or deflected yet further off axis** (depending on geometry and boundary conditions)



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# Transverse impedance

$$W_{D_x}(z) = -\frac{\beta^2 E_0}{q_1 q_2} \frac{\Delta x'_2}{\Delta x_1} \quad W_{Q_x}(z) = -\frac{\beta^2 E_0}{q_1 q_2} \frac{\Delta x'_2}{\Delta x_2}$$

- The **wake function** of an accelerator component is basically its **Green function in time domain** (i.e., its response to a pulse excitation)
  - Very useful for macroparticle models and simulations, because it can be used to describe the driving terms in the single particle equations of motion!
- We can also describe it as a **transfer function in frequency domain**
  - This is the definition of **transverse beam coupling impedance** of the element under study

Dipolar (or driving)

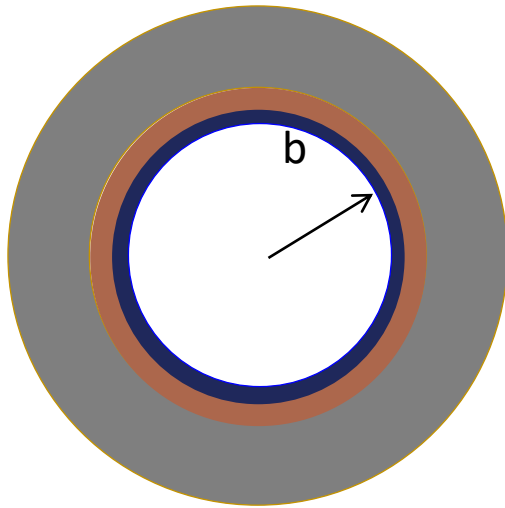
Quadrupolar (or detuning)

$$\begin{aligned} Z_{D_x}(\omega) &= i \int_{-\infty}^{\infty} W_{D_x}(z) \exp\left(-\frac{i\omega z}{c}\right) \frac{dz}{c} \\ Z_{Q_x}(\omega) &= i \int_{-\infty}^{\infty} W_{Q_x}(z) \exp\left(-\frac{i\omega z}{c}\right) \frac{dz}{c} \end{aligned}$$

[ $\Omega/m$ ]

# Examples of transverse wakes/impedances

- **Analytical or semi-analytical** approach, when geometry is simple (or simplified)
  - Same as in the longitudinal plane in terms of approach



→ An example: **axisymmetric beam chamber** with several layers with different EM properties

$$\nabla \times \vec{E} = -i\omega \vec{B} \qquad \nabla \cdot \vec{E} = \frac{\tilde{\rho}}{\epsilon_0 \epsilon_1(\omega)}$$

$$\nabla \times \vec{B} = \mu_0 \mu_1(\omega) \vec{J} + i\omega \frac{\mu_1(\omega) \epsilon_1(\omega)}{c^2} \vec{E}$$

$$\nabla \cdot \vec{B} = 0$$

+ Boundary conditions

$$\tilde{\rho}(r, \theta, s, \omega) = \frac{q_1}{r_1 v} \delta(r - r_1) \delta_P(\theta) \exp\left(-\frac{i\omega s}{v}\right)$$

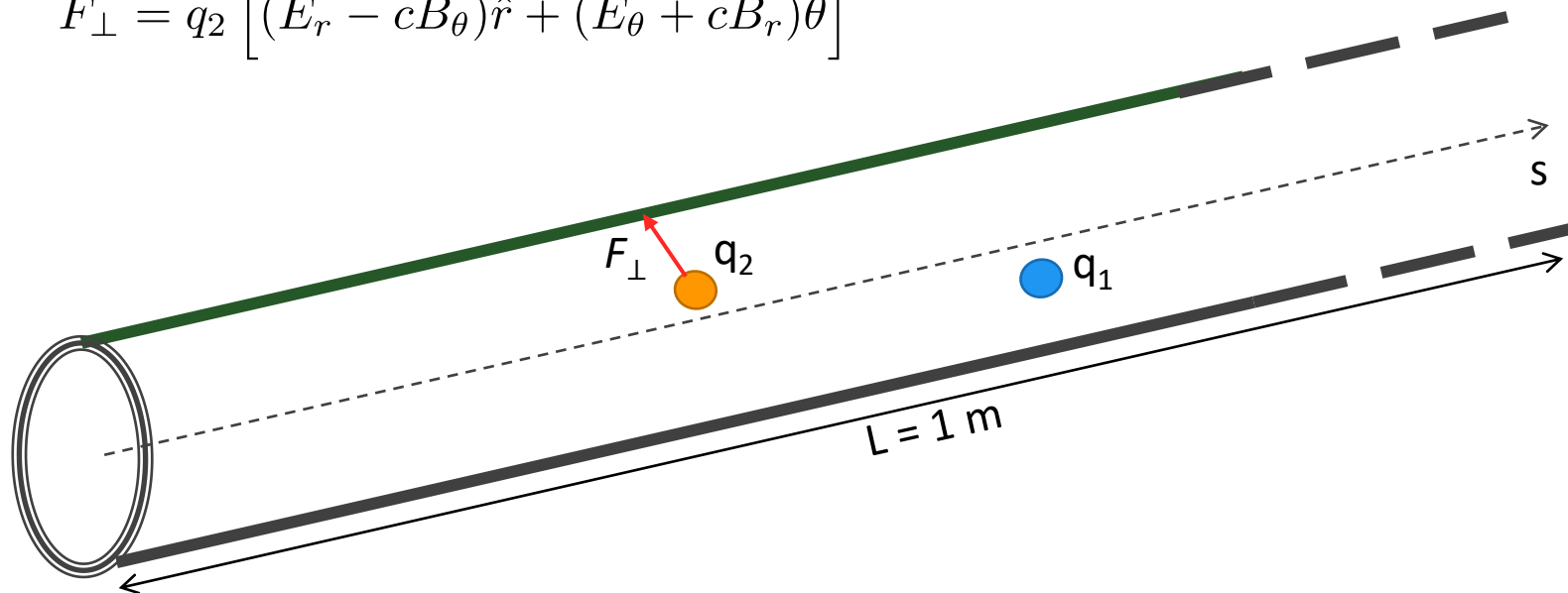
$$\vec{J}(r, \theta, s, \omega) = \tilde{\rho}(r, \theta, s, \omega) \vec{v}$$

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- **Analytical or semi-analytical** approach, when geometry is simple (or simplified)
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  - But we have to calculate the transverse force from an (offset) source to an (offset) witness

→ We are interested in the transverse force on a test charge  $q_2$  following the source  $q_1$  at a distance  $z$  (wake per unit length of chamber)

$$F_{\perp} = q_2 \left[ (E_r - cB_{\theta})\hat{r} + (E_{\theta} + cB_r)\hat{\theta} \right]$$



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$$F_r = \frac{iq_2 v}{\omega} \frac{\partial E_s}{\partial r} \quad F_{\theta} = \frac{iq_2 v}{\omega r} \frac{\partial E_s}{\partial \theta} \quad \text{Same as for the longitudinal plane}$$

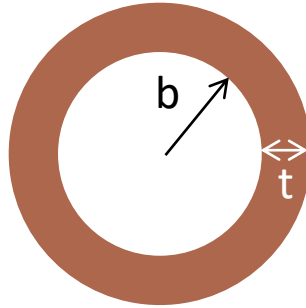
$$\left[ \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2} + \frac{\partial^2}{\partial s^2} + \frac{\omega^2}{c^2} \epsilon_1(\omega) \mu_1(\omega) \right] E_s =$$

$$= \frac{1}{\epsilon_0 \epsilon_1(\omega)} \frac{\partial \tilde{\rho}}{\partial s} + i\omega \mu_0 \mu_1(\omega) \tilde{\rho} v$$

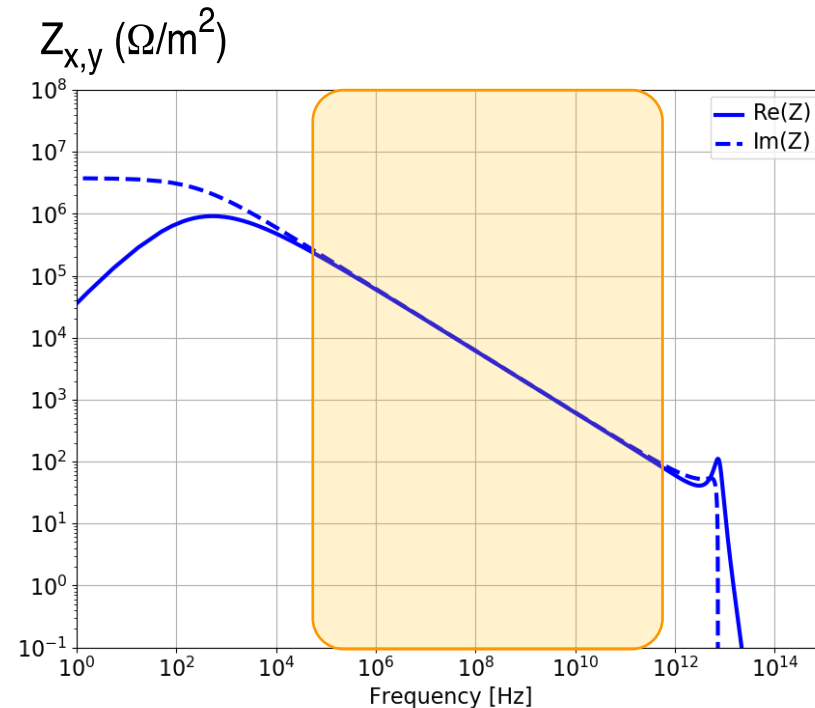
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  - We just need  $E_s$  also to characterize the transverse wake function

→ An example: a 1 m long Cu pipe with radius  $b=2$  cm and thickness  $t = 4$  mm in vacuum



- Highlighted region shows the typical  $\omega^{-1/2}$  scaling
- Scaling with respect to  $b$ :
  - Transverse impedance  $\sim b^{-3}$

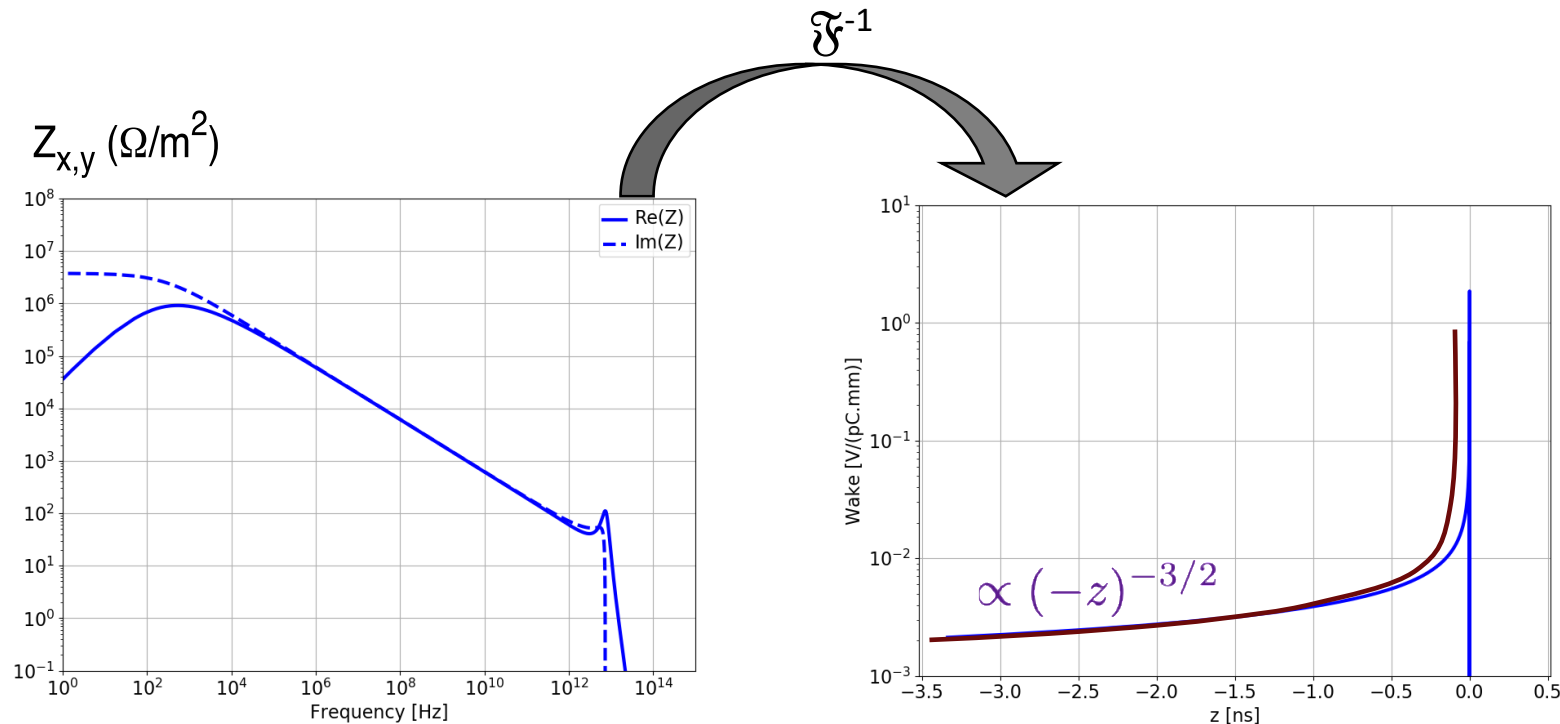




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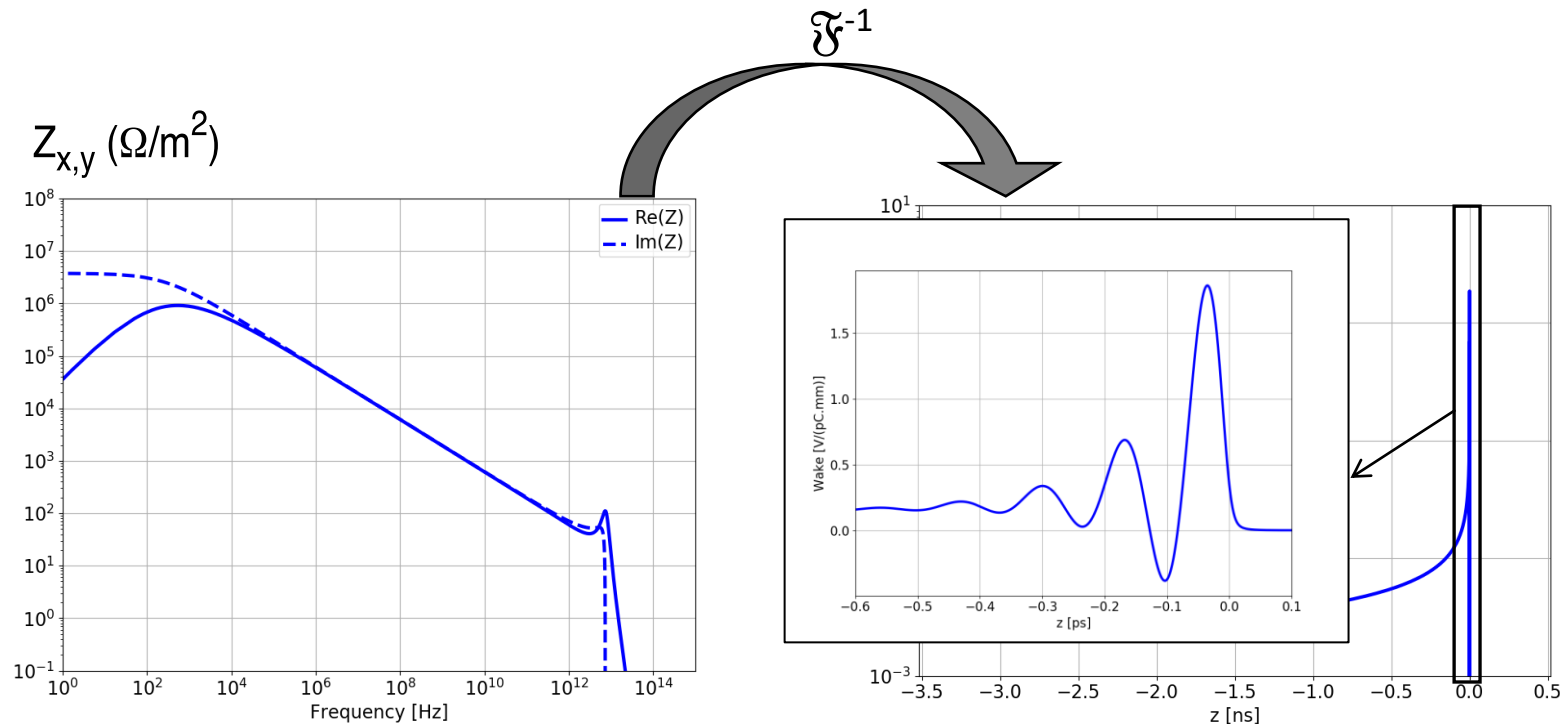
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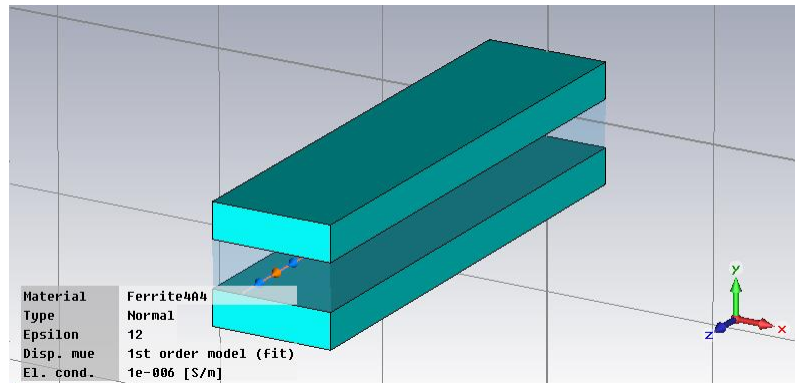


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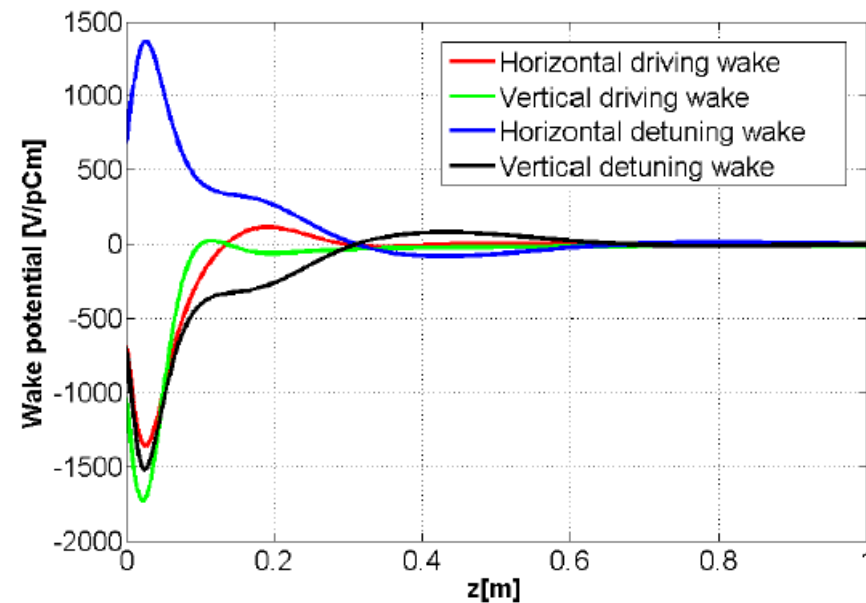
- **Numerical approach**

- Same as in the longitudinal plane
- Use numerical codes to solve Maxwell's equations numerically
- E.g. CST Particle Studio – provides driving and detuning wakes in the two planes by offsetting source and witness, respectively

→ An example: A (simplified) kicker made of two ferrite plates



- Wake is generated for a finite length excitation
- Note that  $W_{Qx}(z) = -W_{Qy}(z) \rightarrow$  general property from Maxwell's equations

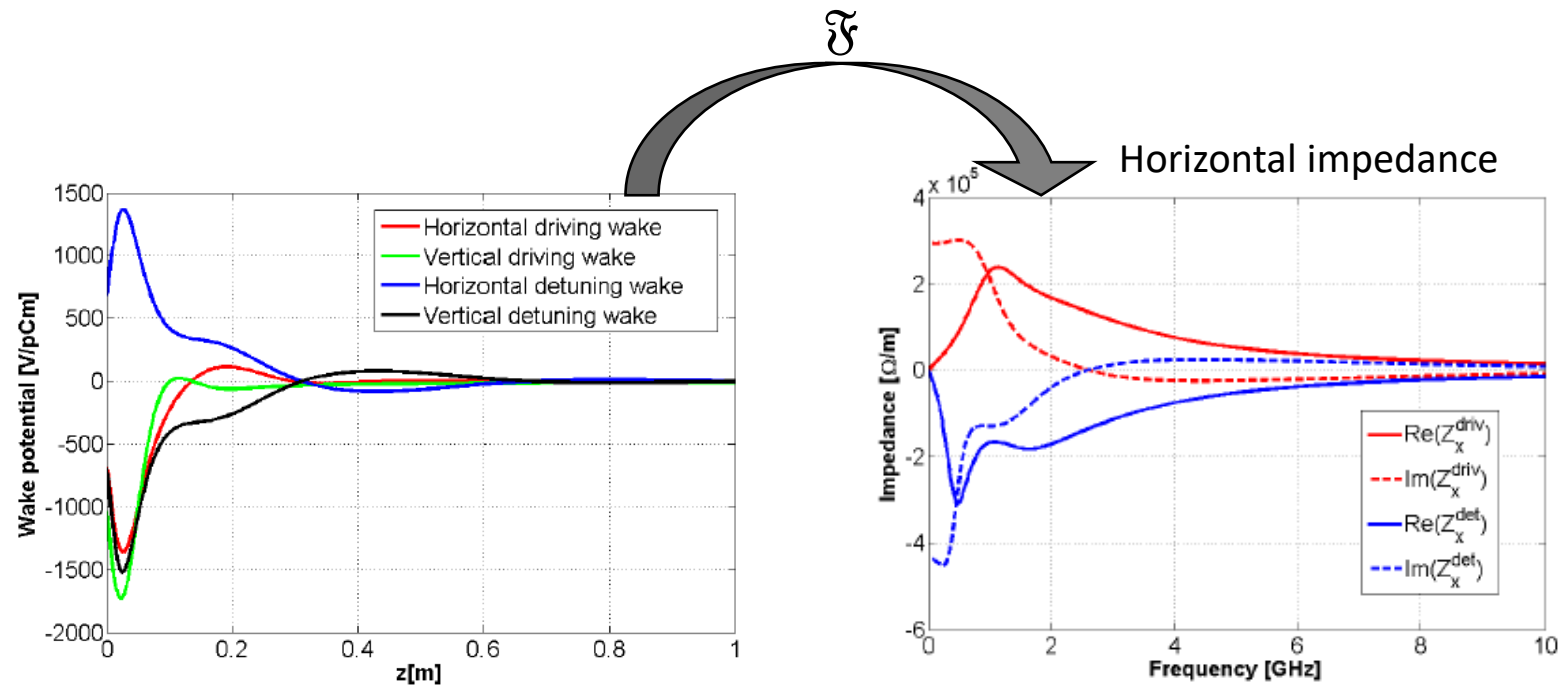


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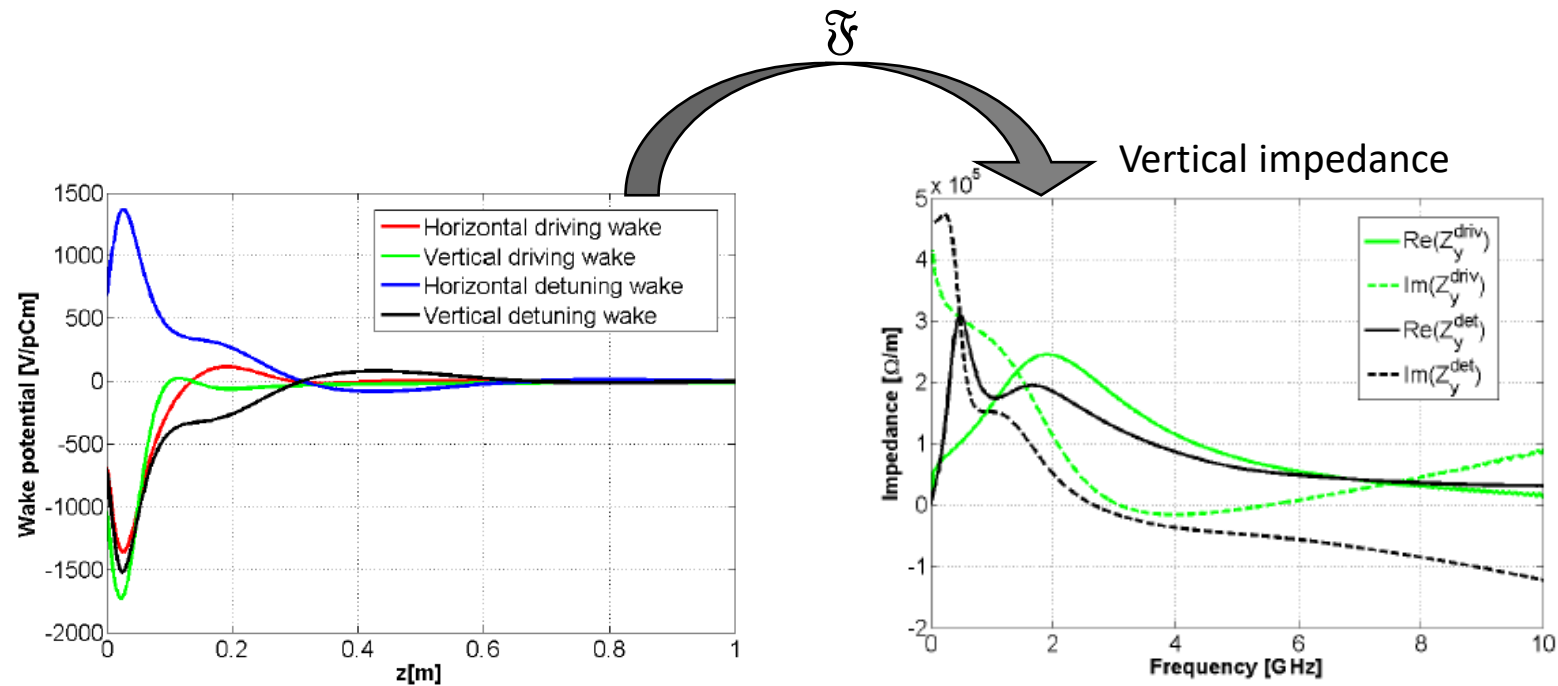


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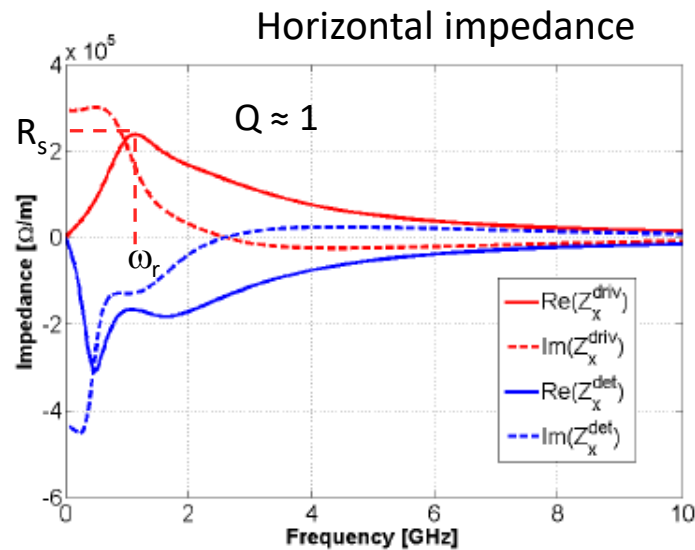


# Examples of transverse wakes/impedances

- **Numerical approach**

- Same as in the longitudinal plane
- As in the longitudinal case, sometimes it is useful to approximate the impedance with one or more resonators (e.g. one broad band resonator in the case of the kicker)

→ An example: A (simplified) kicker made of two ferrite plates



$$Z_{x,y}^{\text{Res}}(\omega) = \frac{\omega_r}{\omega} \frac{R_s(x,y)}{1 + iQ \left( \frac{\omega}{\omega_r} - \frac{\omega_r}{\omega} \right)}$$

$$W_{x,y}^{\text{Res}}(z) = \begin{cases} \frac{R_s(x,y)\omega_r^2}{Q\bar{\omega}} \exp\left(\frac{\alpha_t z}{c}\right) \sin\left(\frac{\bar{\omega} z}{c}\right) & \text{if } z < 0 \\ 0 & \text{if } z \geq 0 \end{cases}$$

$$\alpha_t = \frac{\omega_r}{2Q} \quad \bar{\omega} = \sqrt{\omega_r^2 - \alpha_t^2}$$



We have seen the **definition of transverse wake fields** and how they can be classified into constant, dipolar and quadrupolar wake fields.

We have discussed how to calculate the **transverse wakes and impedances**.

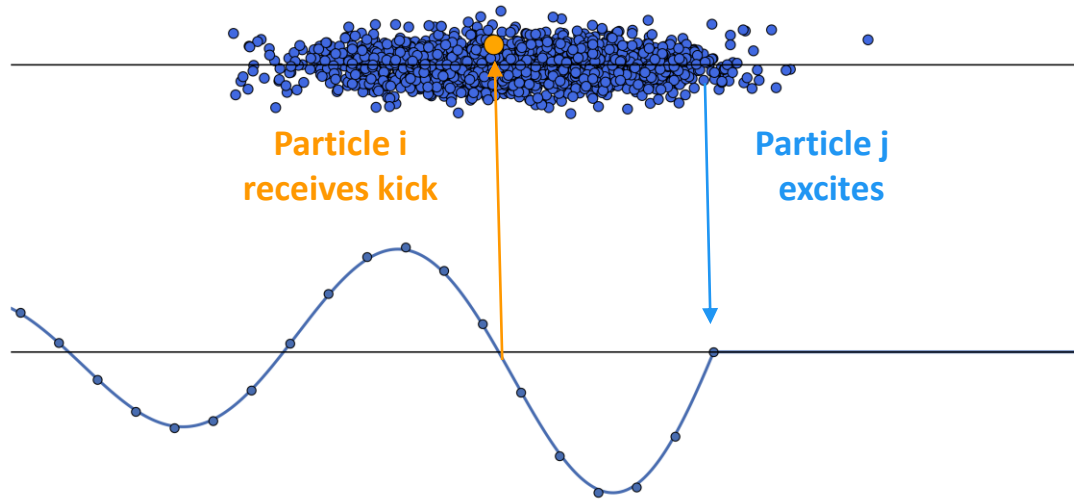
We will now look into how the impact of wake fields onto charged particle beams can be **modeled numerically** to prepare for investigating the different types of coherent instabilities further along.

## Part 3: Multiparticle dynamics with wake fields – their different types and impact on transverse beam dynamics

- Transverse wake function and impedance
- Effect on a bunch and transverse „potential well distortion“
- Some examples of beam instabilities

# Transverse impedance kick

- Single traversal of a bunch through an impedance source



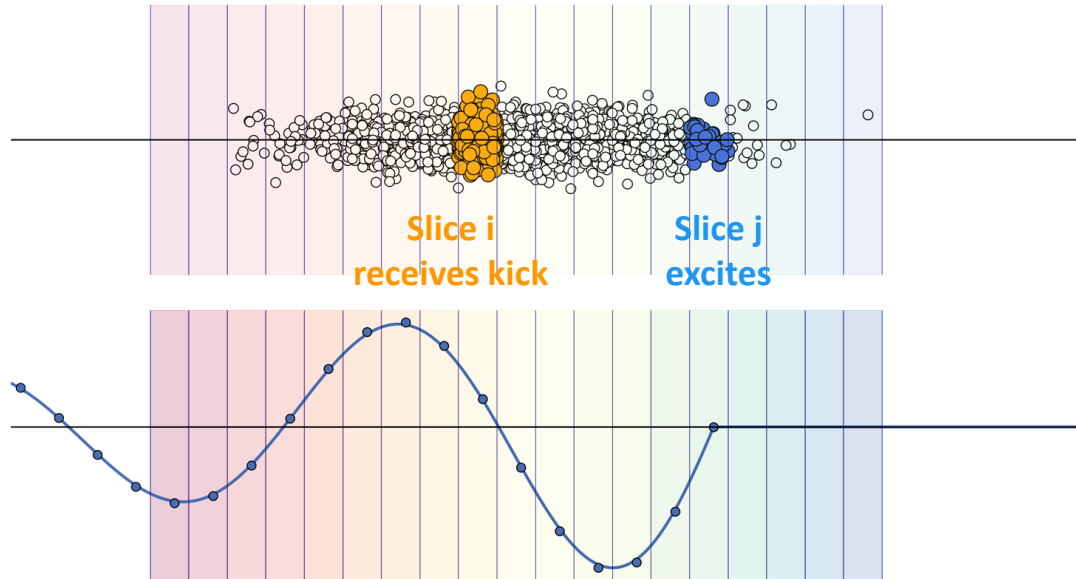
$$\Delta x'_i = -\frac{e^2}{\beta^2 E_0} \begin{cases} W_{Cx}(z_i - z_j) \\ x_j W_{Dx}(z_i - z_j) \\ x_i W_{Qx}(z_i - z_j) \end{cases}$$

$$\langle \Delta x'_{\text{bunch}} \rangle = -\frac{e^2}{N_b \beta^2 E_0} \sum_{j=1}^{N_b} \sum_{i=1}^{N_b} \begin{cases} W_{Cx}(z_i - z_j) \\ x_j W_{Dx}(z_i - z_j) \\ x_i W_{Qx}(z_i - z_j) \end{cases}$$



# Transverse impedance kick

- Single traversal of a bunch through an impedance source
  - Let's neglect the quadrupolar wake in first instance → equal kicks on particles in slice i

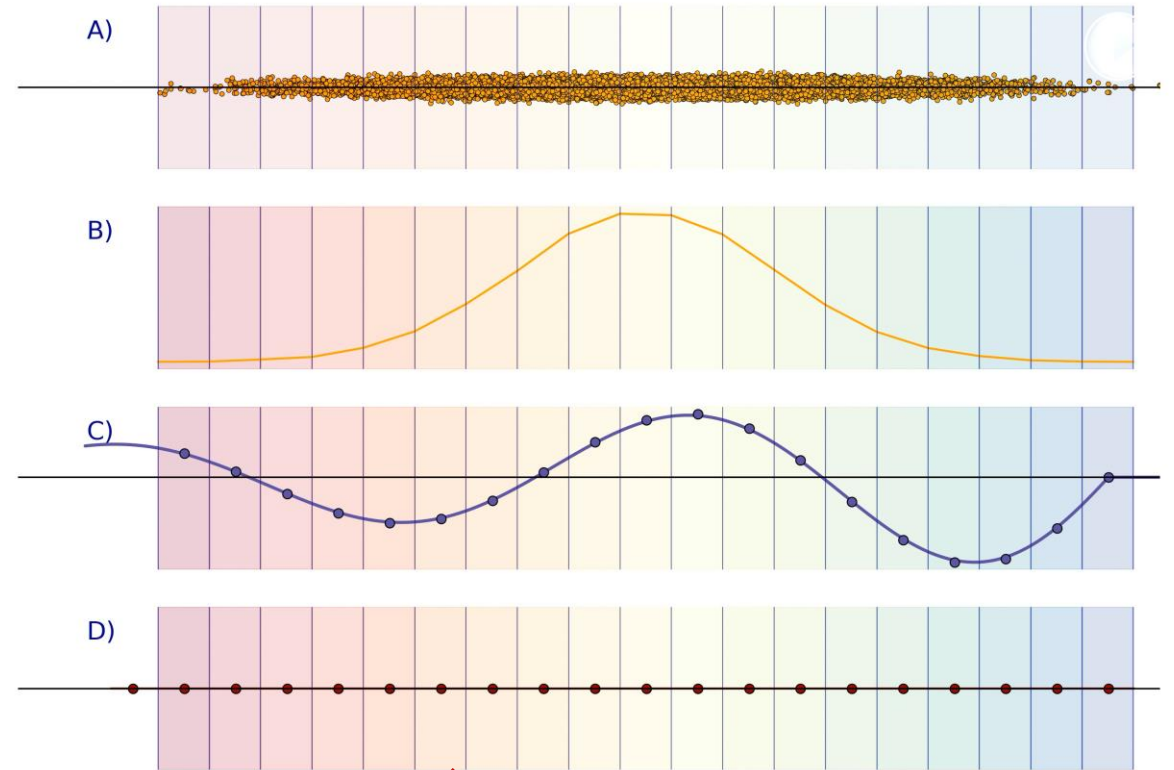


$$\Delta x'_{ij} = -\frac{e^2}{\beta^2 E_0} N[j] [W_{Cx}[(i-j)\Delta z] + \langle x \rangle[j] W_{Dx}[(i-j)\Delta z]]$$

$$\Delta x'_i = -\frac{e^2}{\beta^2 E_0} \sum_{j=0}^i N[j] [W_{Cx}[(i-j)\Delta z] + \langle x \rangle[j] W_{Dx}[(i-j)\Delta z]]$$

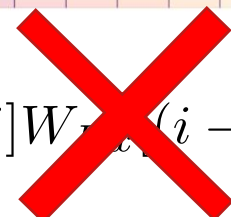
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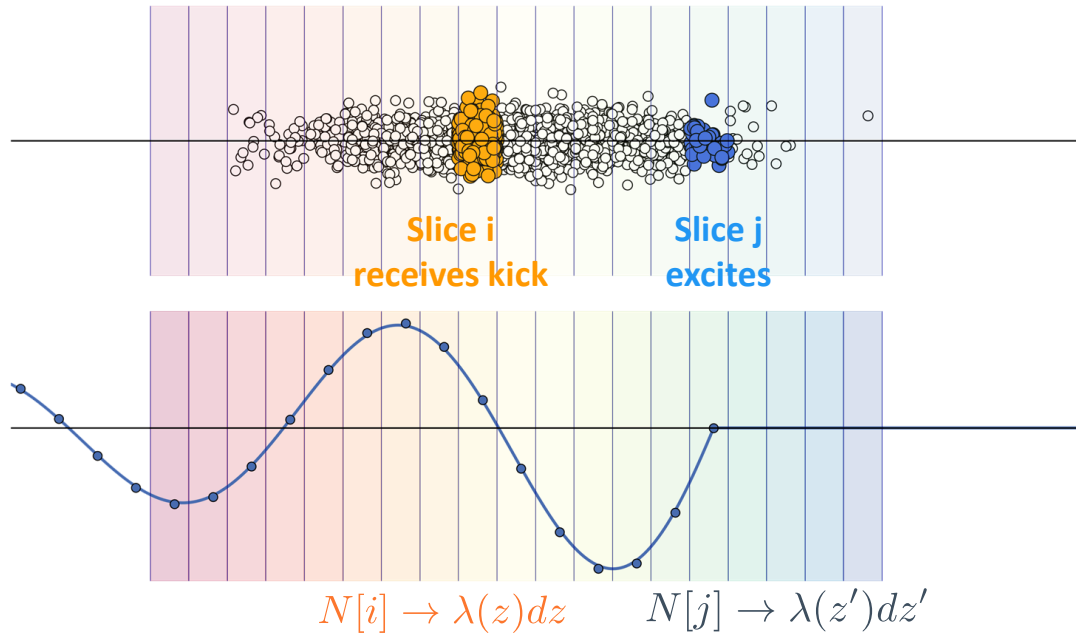
$$\Delta x'_i = -\frac{e^2}{\beta^2 E_0} \sum_{j=0}^i N[j] [W_{Cx}[(i-j)\Delta z] + \langle x \rangle[j] W_{Cx}[(i-j)\Delta z]]$$

as  $\langle x \rangle(z) = 0$



# Transverse impedance kick

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$$\langle \Delta x' \rangle_{\text{bunch}} = \frac{1}{N_b} \sum_{i=1}^{N_{\text{slices}}} N[i] \Delta x_i$$

$$\langle \Delta x' \rangle_{\text{bunch}} = -\frac{e^2}{N_b \beta^2 E_0} \int \lambda(z) dz \underbrace{\int \lambda(z') [W_{Cx}(z - z') + \langle x \rangle(z') W_{Dx}(z - z')] dz'}_{\text{Kick dependent on } \langle x \rangle, \text{ quadrupole type, associated to a detuning}}$$

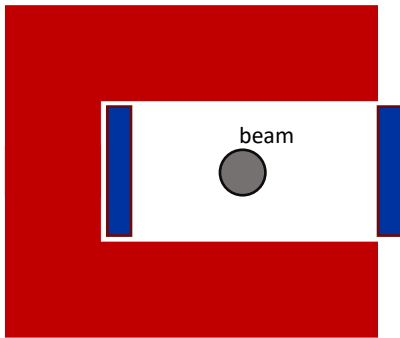
**"Constant" kick**, dipole type, associated to a closed orbit distortion

**Kick dependent on <x>**, quadrupole type, associated to a detuning

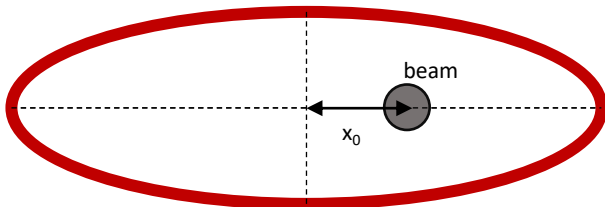
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$$\langle \Delta x' \rangle_{\text{bunch}} = -\frac{e^2 c^2}{N_b E_0} \int_{-\infty}^{\infty} |\hat{\lambda}(\omega)|^2 \text{Im} [Z_{Cx}(\omega)] d\omega$$

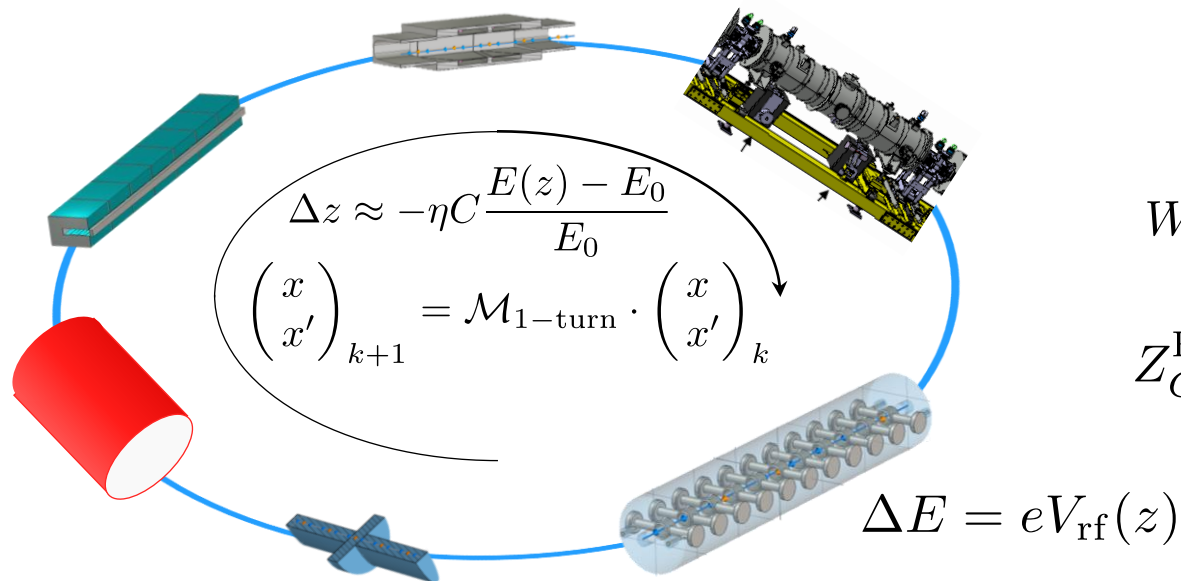


$$\langle \Delta x' \rangle_{\text{bunch}} = -\frac{e^2 c^2 x_0}{N_b E_0} \int_{-\infty}^{\infty} |\hat{\lambda}(\omega)|^2 \text{Im} [Z_{Dx}(\omega)] d\omega$$

$$\langle \Delta x' \rangle_{\text{bunch}} = -\frac{e^2 c^2 x_0}{N_b E_0} \int_{-\infty}^{\infty} |\hat{\lambda}(\omega)|^2 [\text{Im} [Z_{Dx}(\omega)] + \text{Im} [Z_{Qx}(\omega)]] d\omega$$

# Transverse wakes in beam dynamics

- Same approach as in the longitudinal plane to build the impedance model of a machine
- For simulations, the impedance is lumped in one place and kicks to beam particles are applied once per turn, with linear matrix transport between turns
  - One word of caution: The effect of the transverse impedance results in a combination of a dipole-type and quadrupole-type kick, therefore the beta functions at the real locations of the impedance source has to be taken into account when combining wakes/impedances



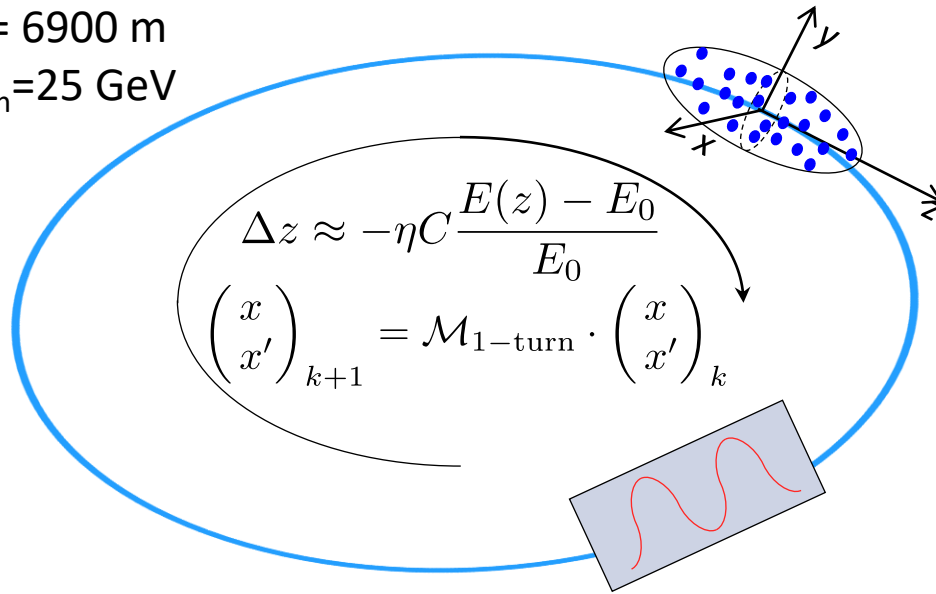
$$W_{Cx, Dx, Qx}^{\text{Ring}}(z) = \sum_i \frac{\beta_{xi}}{\langle \beta_x \rangle} W_{Cx, Dx, Qx}^i(z)$$

$$Z_{Cx, Dx, Qx}^{\text{Ring}}(\omega) = \sum_i \frac{\beta_{xi}}{\langle \beta_x \rangle} Z_{Cx, Dx, Qx}^i(\omega)$$

$$\Delta x' = -\frac{e^2}{\beta^2 E_0} \int \lambda(z') \left[ W_{Cx}^{\text{Ring}}(z - z') + \langle x \rangle(z') W_{Dx}^{\text{Ring}}(z - z') + x W_{Qx}^{\text{Ring}}(z - z') \right] dz'$$

# Effect of a transverse impedance on a bunch

SPS ring  
 $C = 6900 \text{ m}$   
 $E_{\text{kin}} = 25 \text{ GeV}$



Single Gaussian bunch

$$\sigma_z = 0.2 \text{ m (0.67 ns)}$$

Constant horizontal wake from a kicker  
 (non-axisymmetric)

Two examples:

Frozen synchrotron motion

or

Single RF system

$$\omega_{\text{rf}} = 200 \text{ MHz}$$

$$V_{\text{rf}}^{\text{max}} = 3 \text{ MV}$$

$$\Delta x' = -\frac{e^2}{\beta^2 E_0} \int \lambda(z') W_{Cx}^{\text{Kicker}}(z - z') dz'$$

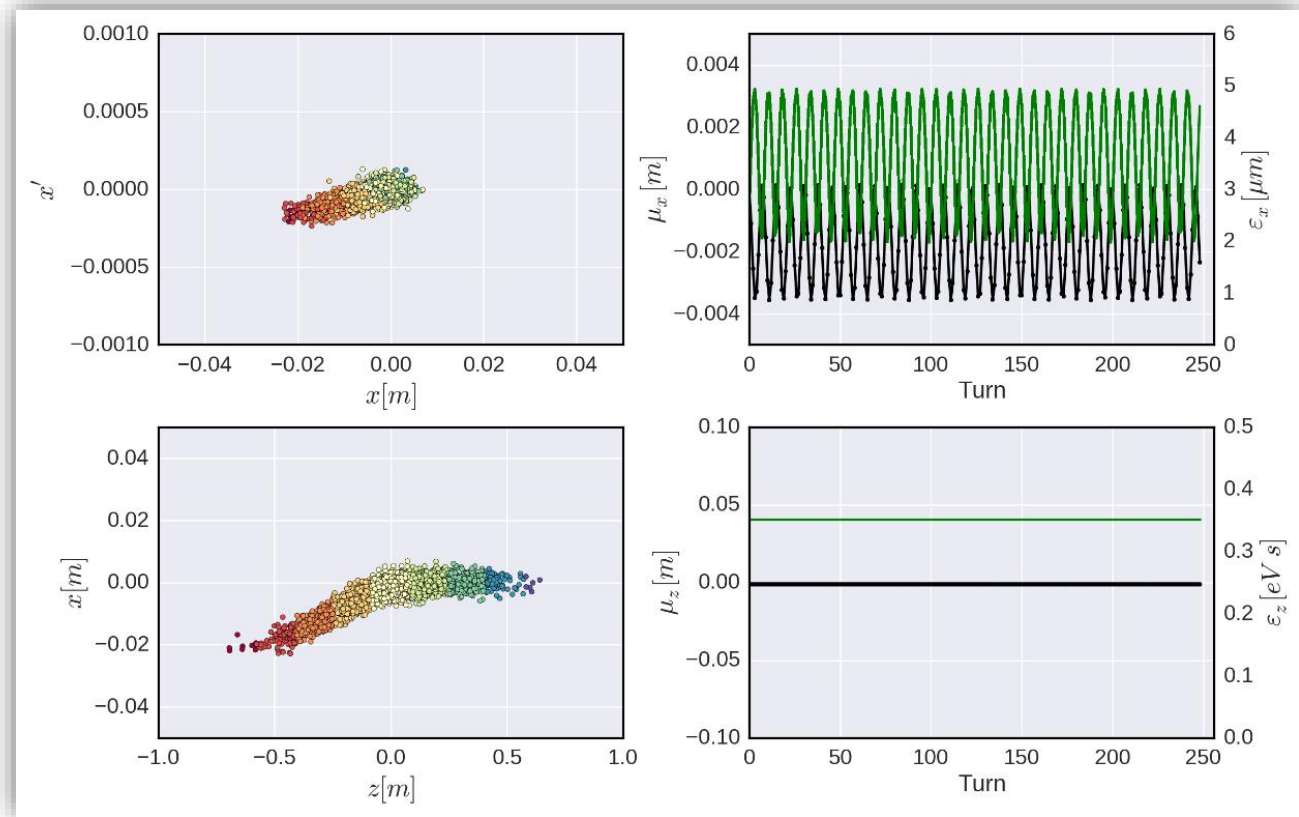
$$\Delta E = eV_{\text{rf}}(z)$$

# Examples – constant wakes

$$\Delta x'[i] = - \frac{e^2}{m\gamma\beta^2 c^2} \sum_{j=0}^i N[j] \cdot W_{Cx}[i-j]$$

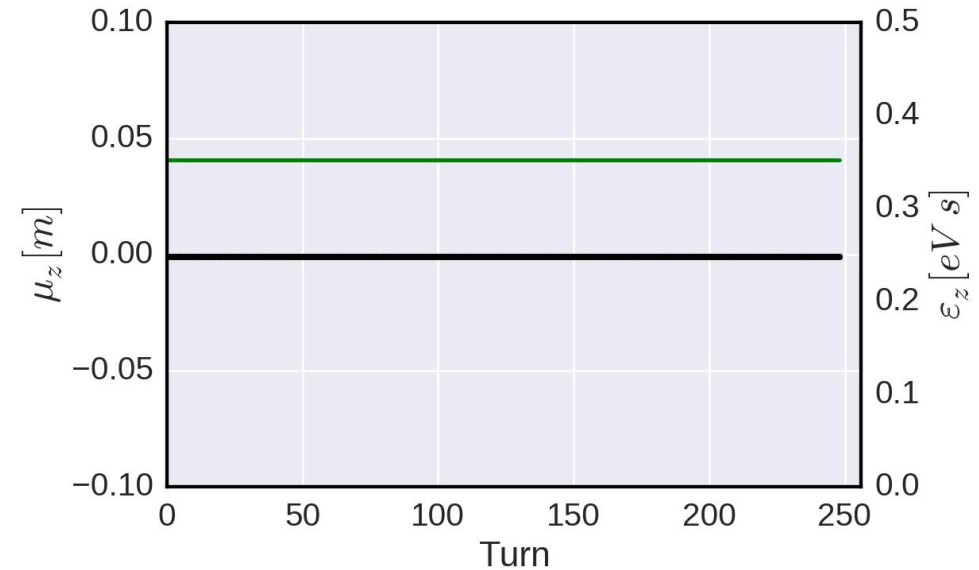
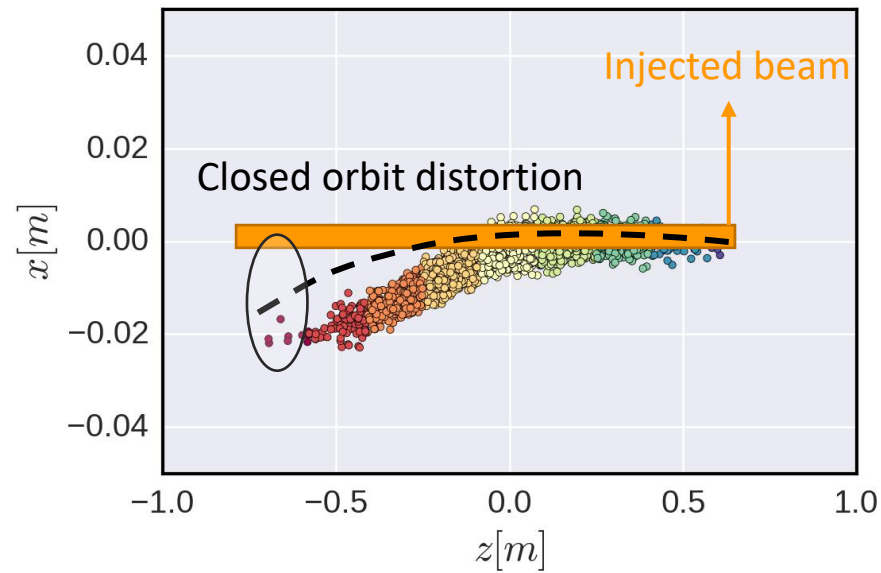
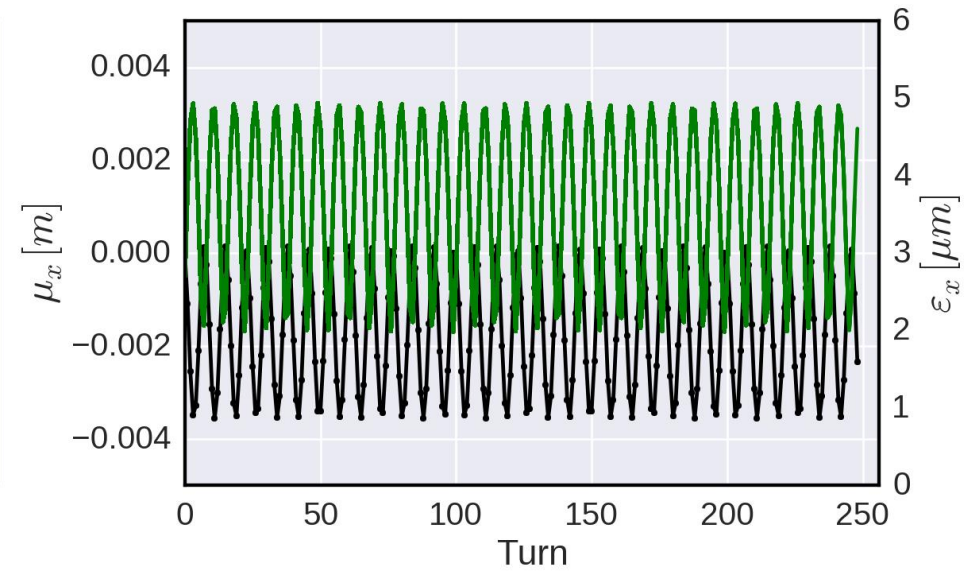
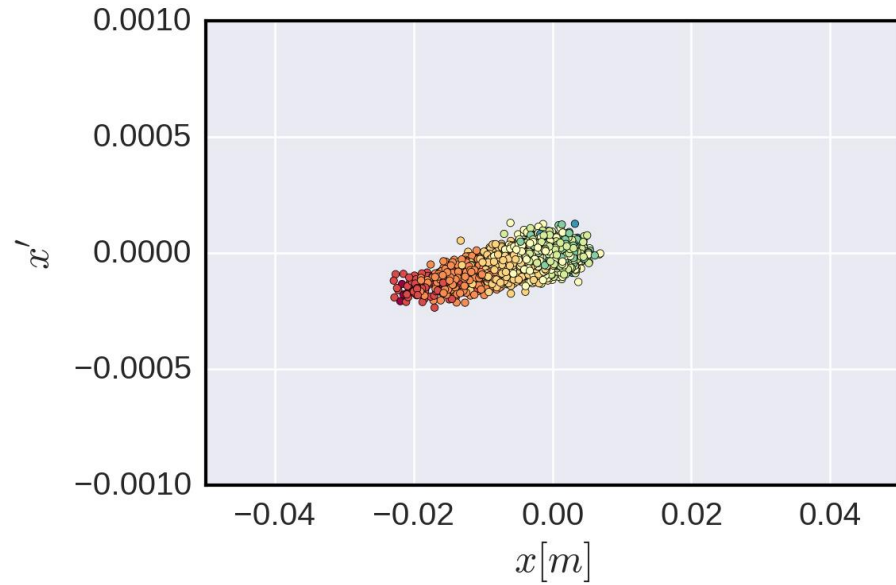
Dipolar term → orbit kick

Slice dependent change of closed orbit (if line density does not change)



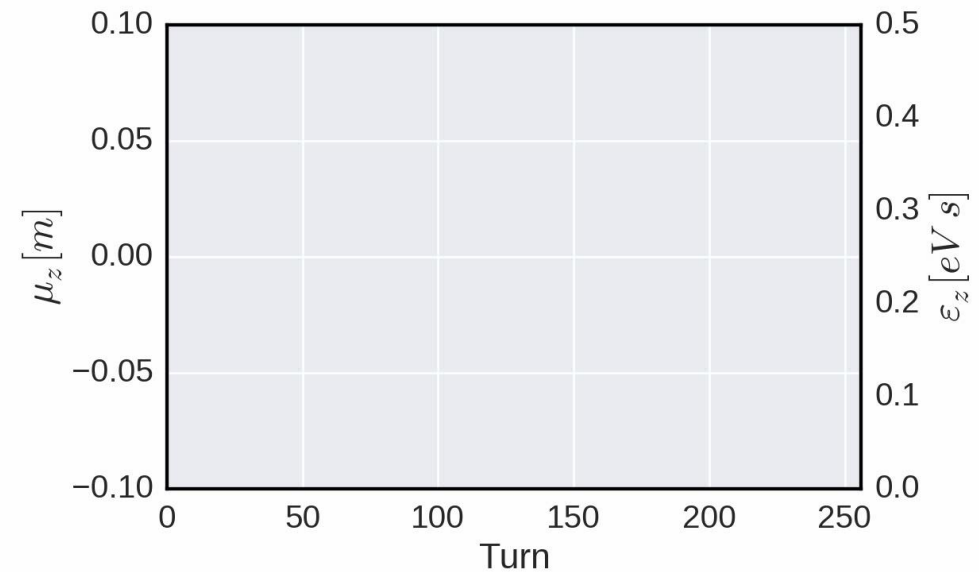
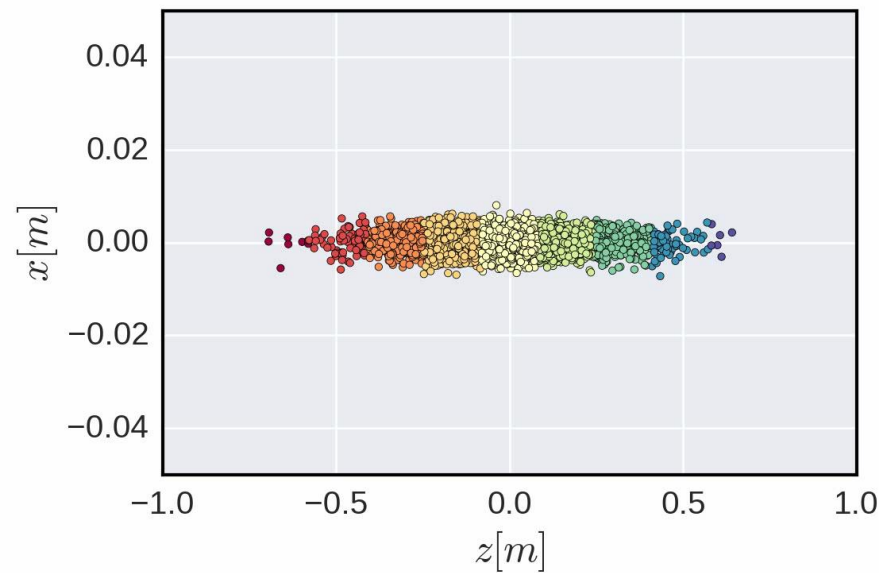
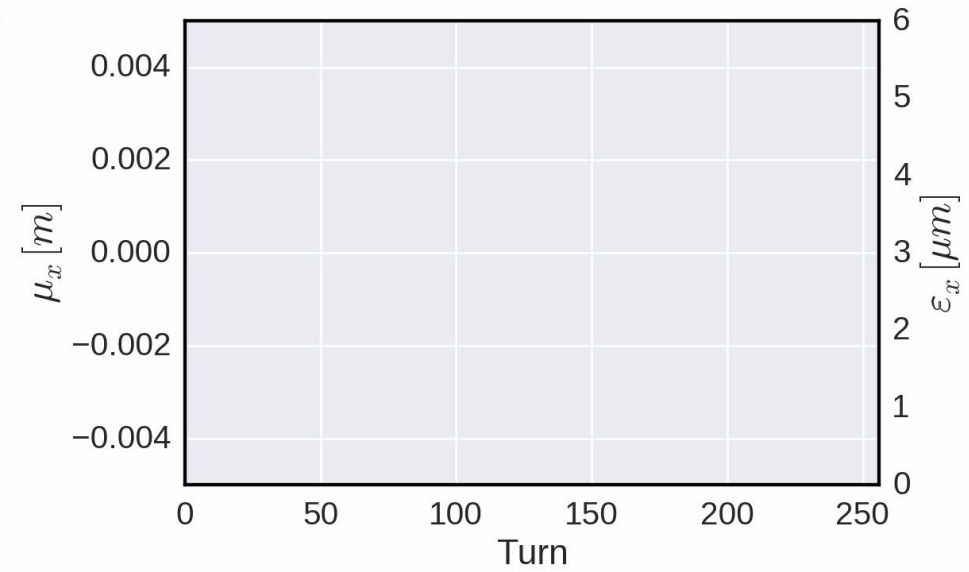
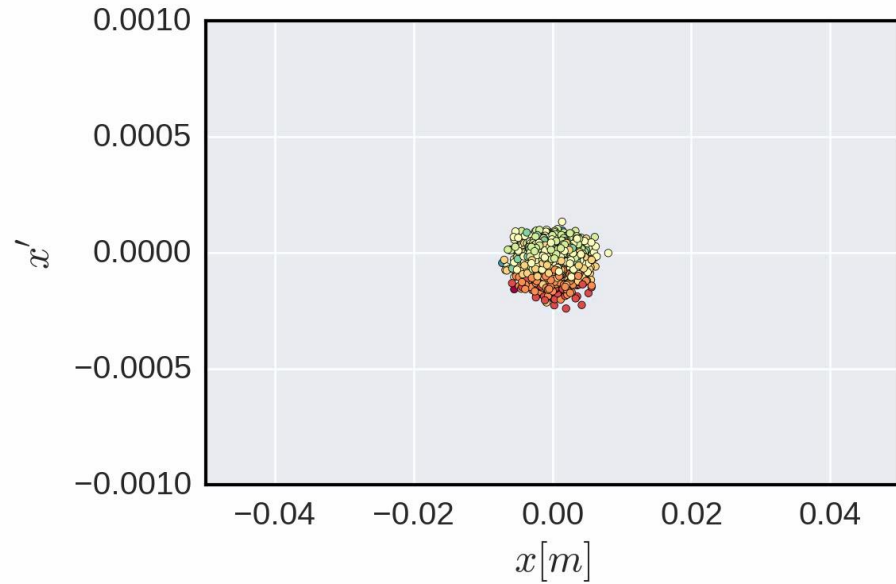


# Examples – constant wakes

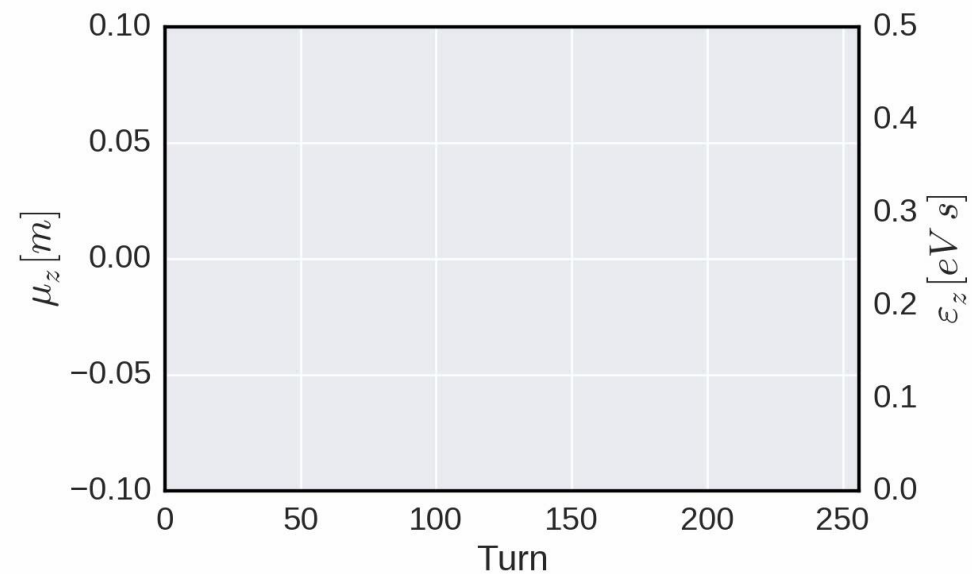
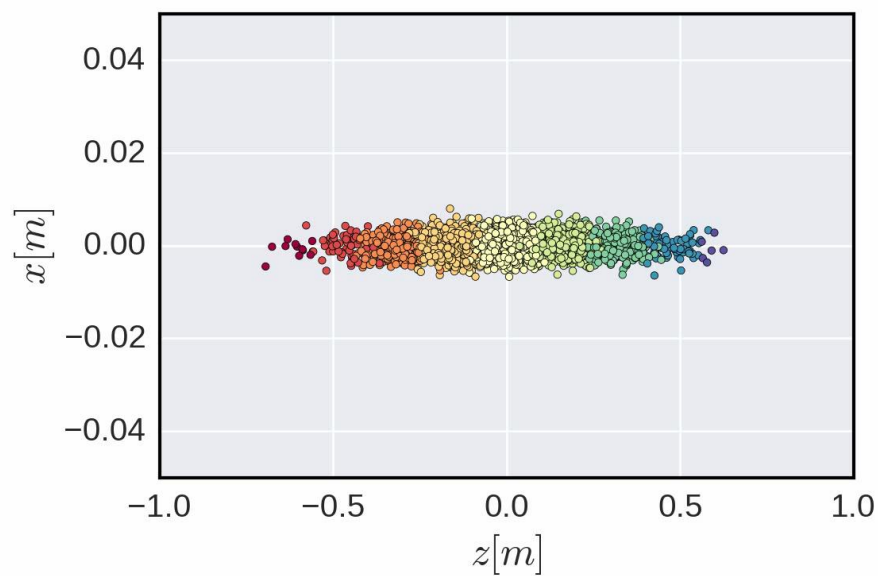
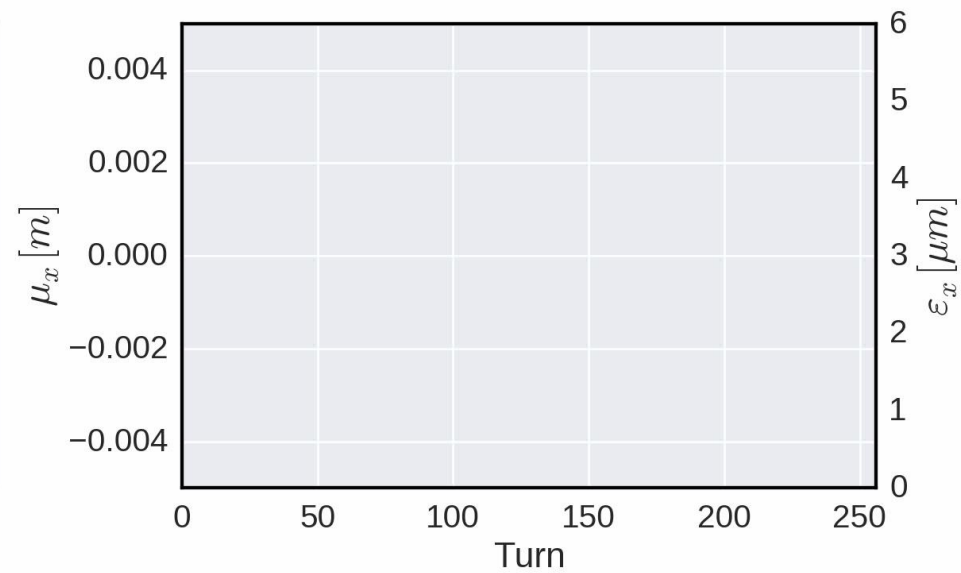
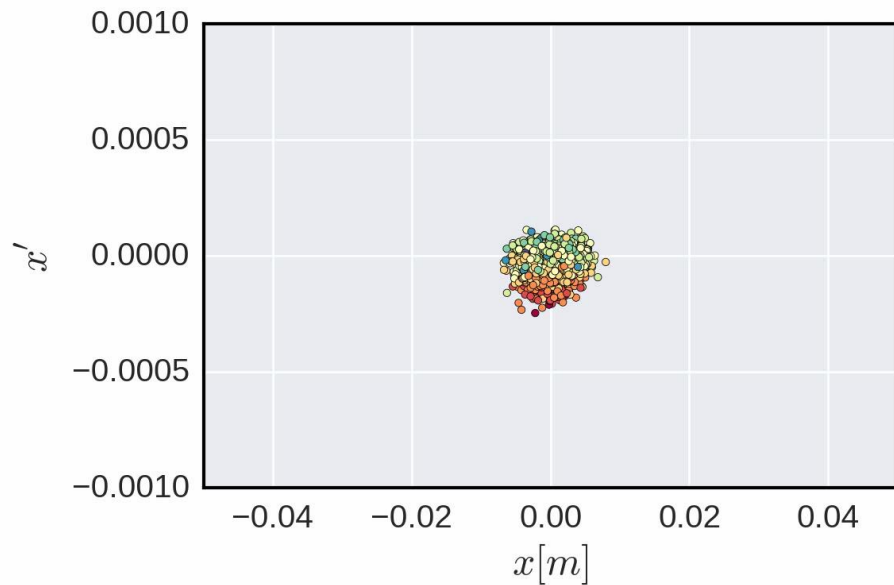




# Examples – constant wakes w/o synchrotron motion



# Examples – constant wakes with synchrotron motion





We have seen how the impact of **wake fields on charged particle beams** can be **implemented numerically** in an efficient manner via **the longitudinal discretization** of bunches.

We have used the simulation models to show **orbit effects** from transverse wake fields.

We will now look at some **transverse instabilities**.

## Part 3: Multiparticle dynamics with wake fields – their different types and impact on transverse beam dynamics

- Transverse wake function and impedance
- Effect on a bunch and transverse „potential well distortion“
- Some examples of beam instabilities

# Effect of dipole wakes on a particle bunch

$$\Delta x'[i] = -\frac{e^2}{m\gamma\beta^2 c^2 C} \sum_{j=0}^i \boxed{N[j] \langle x \rangle [j] \cdot W_{Dx}[i-j]}$$

Dipolar term  $\rightarrow$  orbit kick

Offset dependent orbit kick  
 $\rightarrow$  kicks can accumulate

- Without synchrotron motion:  
kicks accumulate turn after turn – the **beam is unstable**  $\rightarrow$  beam break-up in linacs, instabilities much faster than synchrotron motion, e.g. close to transition crossing

# Effect of dipole wakes on a particle bunch

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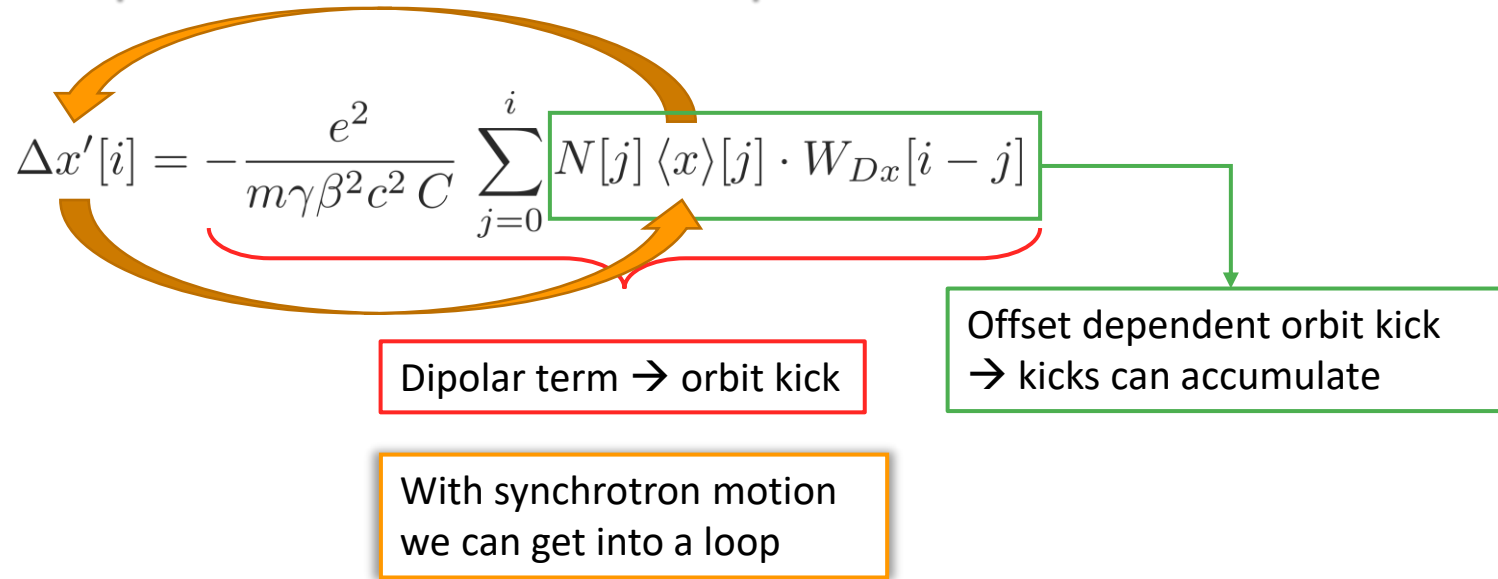
Dipolar term  $\rightarrow$  orbit kick

Offset dependent orbit kick  $\rightarrow$  kicks can accumulate

With synchrotron motion we can get into a loop

- Without synchrotron motion:  
kicks accumulate turn after turn – the **beam is unstable**  $\rightarrow$  beam break-up in linacs, instabilities much faster than synchrotron motion, e.g. close to transition crossing
- With synchrotron motion:
  - Chromaticity = 0
    - Modes related to longitudinal motion appear in transverse motion
    - Existence of an instability threshold
  - Chromaticity  $\neq 0$ 
    - **Headtail modes**  $\rightarrow$  beam is unstable (can be very weak and often damped by non-linearities)

# Effect of dipole wakes on a particle bunch

$$\Delta x'[i] = -\frac{e^2}{m\gamma\beta^2 c^2 C} \sum_{j=0}^i N[j] \langle x \rangle [j] \cdot W_{Dx}[i-j]$$


Dipolar term  $\rightarrow$  orbit kick

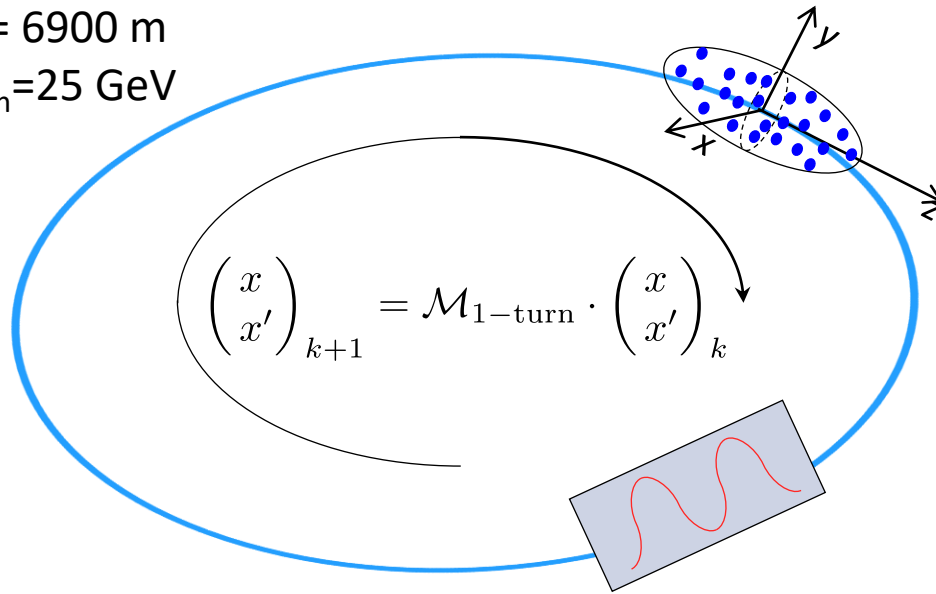
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# Effect of a transverse impedance on a bunch

SPS ring  
 $C = 6900 \text{ m}$   
 $E_{\text{kin}} = 25 \text{ GeV}$



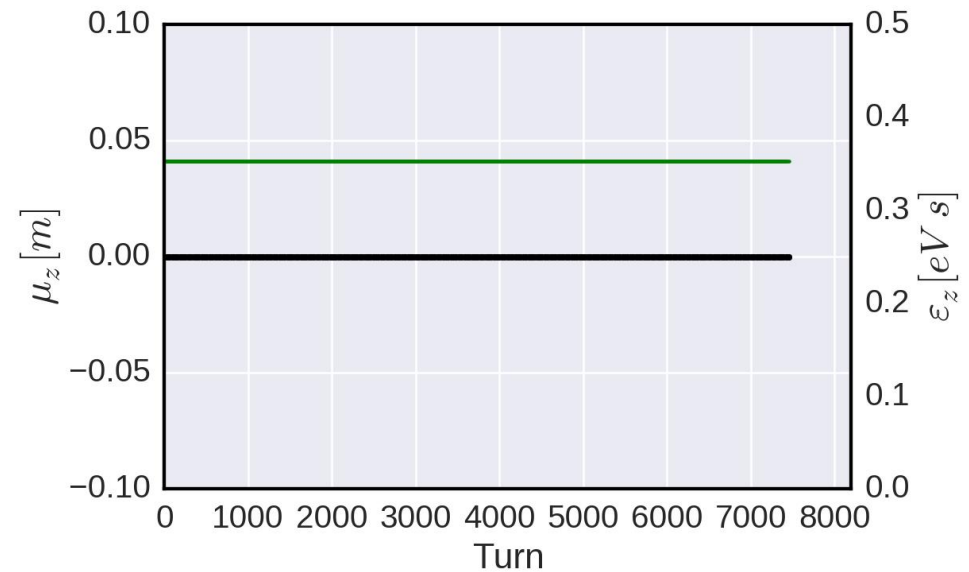
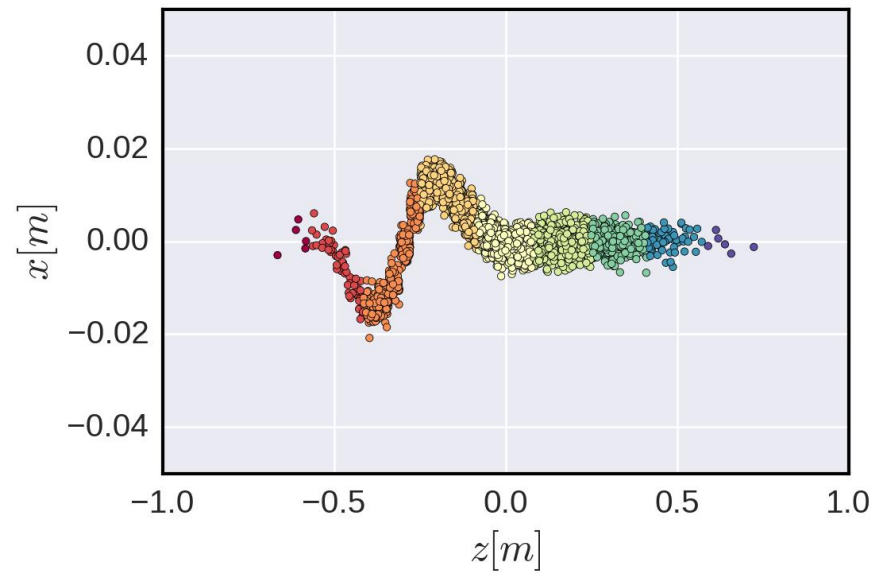
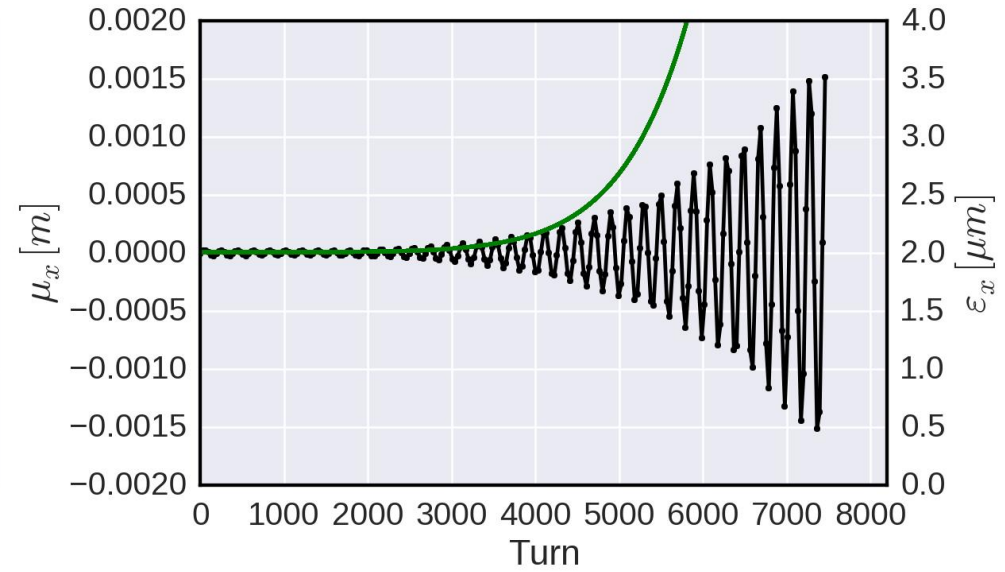
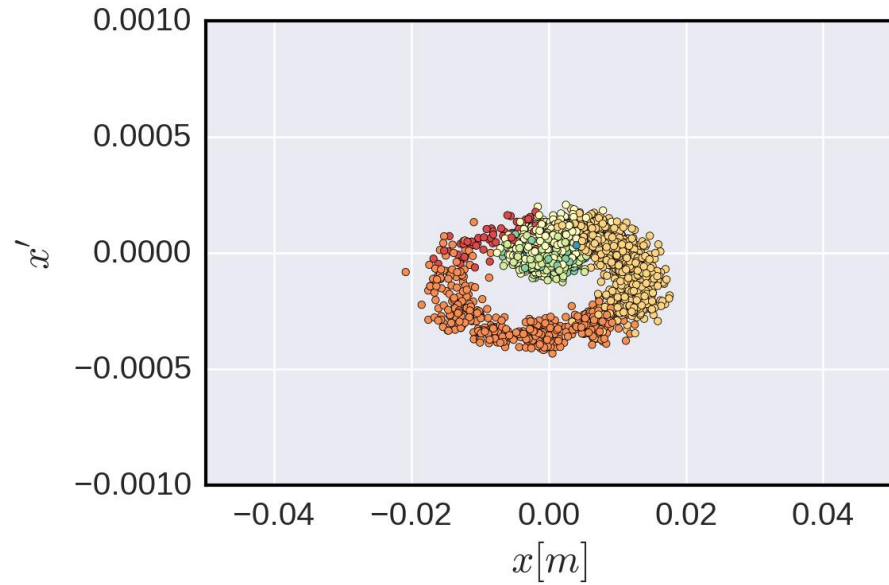
Single Gaussian bunch  
 $\sigma_z = 0.2 \text{ m (0.67 ns)}$

Dipole horizontal wake in the form of broad-band resonator

Frozen longitudinal motion or crossing transition ( $\eta \approx 0$ )

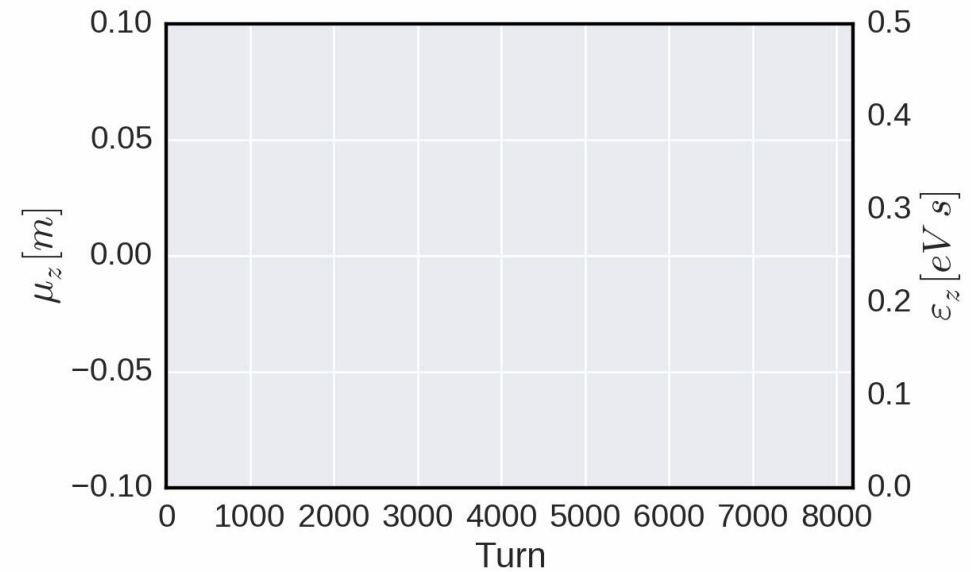
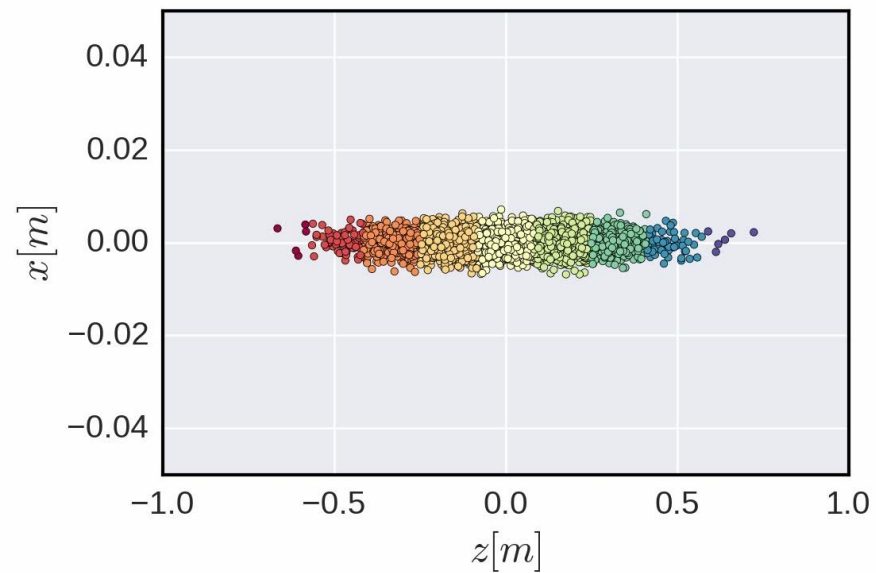
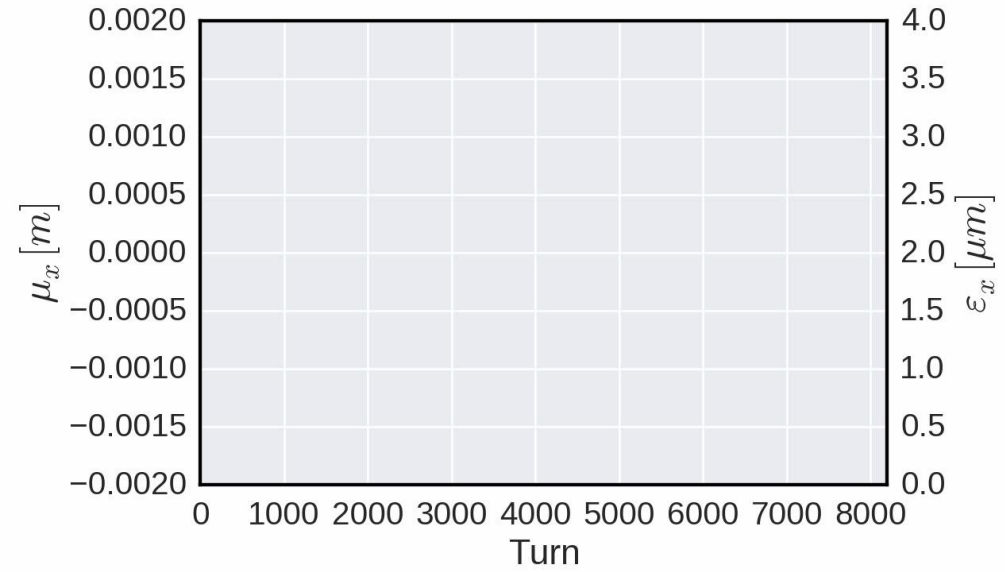
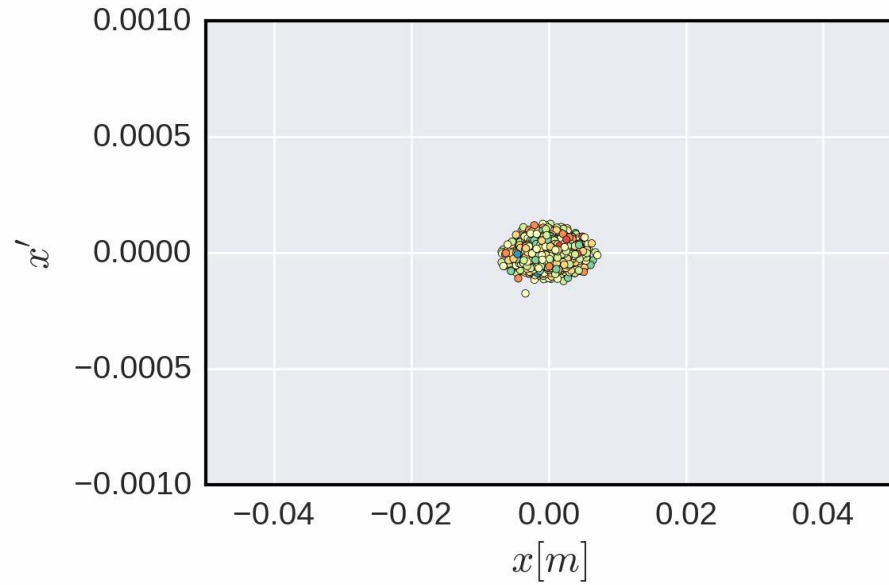
$$\Delta x' = -\frac{e^2}{\beta^2 E_0} \int \lambda(z') \langle x \rangle(z') W_{Dx}^{\text{Ring}}(z - z') dz'$$

# Dipole wakes – beam break-up



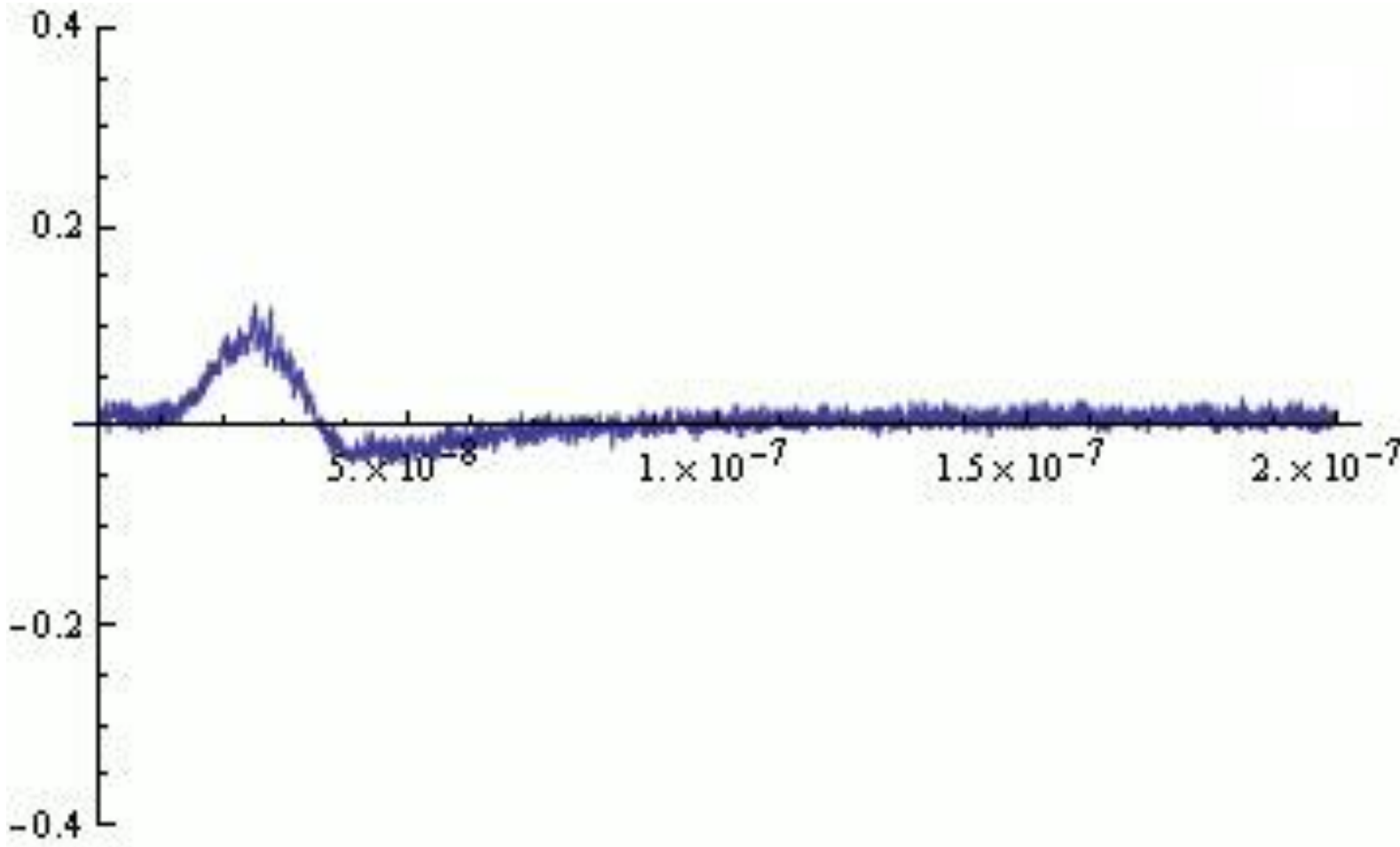


# Dipole wakes – beam break-up



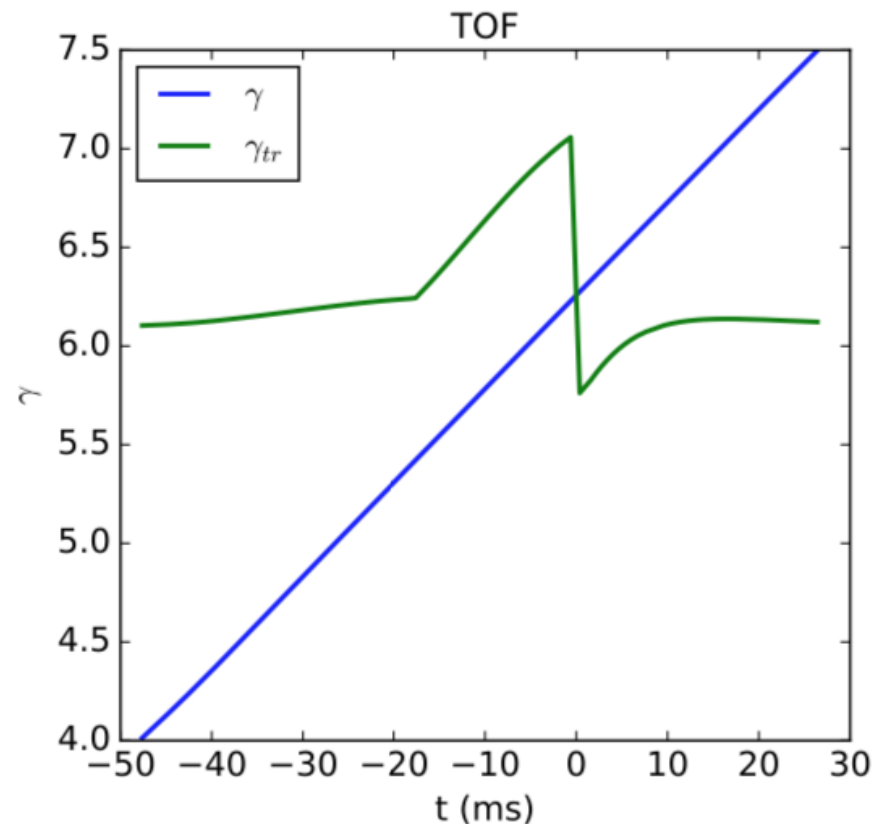
# Measurement at CERN PS

- Beam break up type instabilities have been seen in the CERN PS when crossing transition with high intensity beams



# Measurement at CERN PS

- Beam break up type instabilities have been seen in the CERN PS when crossing transition with high intensity beams
- To increase the intensity reach, it is necessary to cross transition more quickly, gamma jump scheme implemented



# Effect of dipole wakes on a particle bunch

$$\Delta x'[i] = -\frac{e^2}{m\gamma\beta^2 c^2 C} \sum_{j=0}^i N[j] \langle x \rangle [j] \cdot W_{Dx}[i-j]$$

Dipolar term  $\rightarrow$  orbit kick

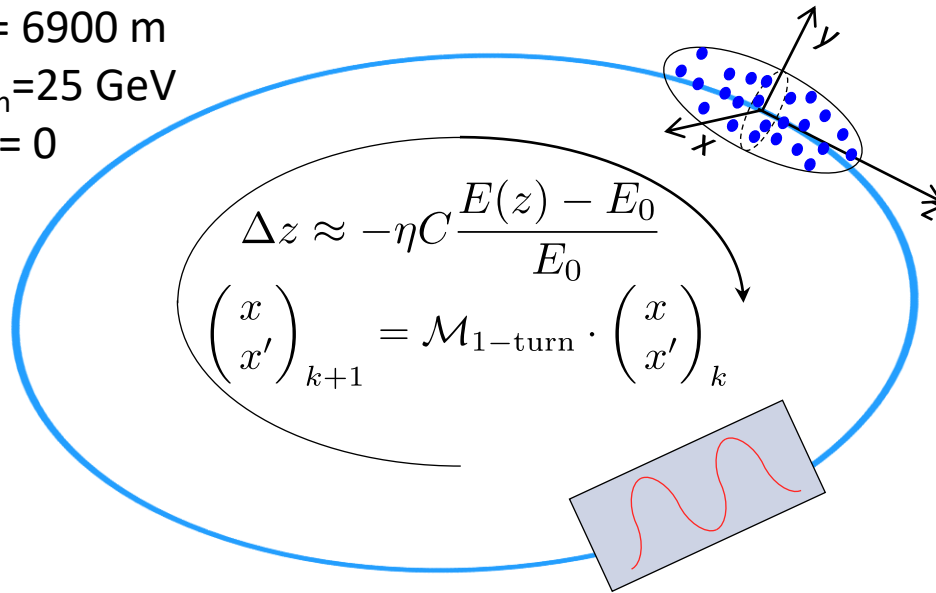
With synchrotron motion we can get into a loop

Offset dependent orbit kick  $\rightarrow$  kicks can accumulate

- Without synchrotron motion:  
kicks accumulate turn after turn – the **beam is unstable**  $\rightarrow$  beam break-up in linacs, instabilities much faster than synchrotron motion, e.g. close to transition crossing
- With synchrotron motion:
  - Chromaticity = 0
    - Modes related to longitudinal motion appear in transverse motion
    - Existence of an instability threshold
  - Chromaticity  $\neq 0$ 
    - **Headtail modes**  $\rightarrow$  beam is unstable (can be very weak and often damped by non-linearities)

# Effect of a transverse impedance on a bunch

SPS ring  
 $C = 6900 \text{ m}$   
 $E_{\text{kin}} = 25 \text{ GeV}$   
 $\xi_x = 0$



Single Gaussian bunch  
 $\sigma_z = 0.2 \text{ m (0.67 ns)}$

Dipole horizontal wake in the form of broad-band resonator

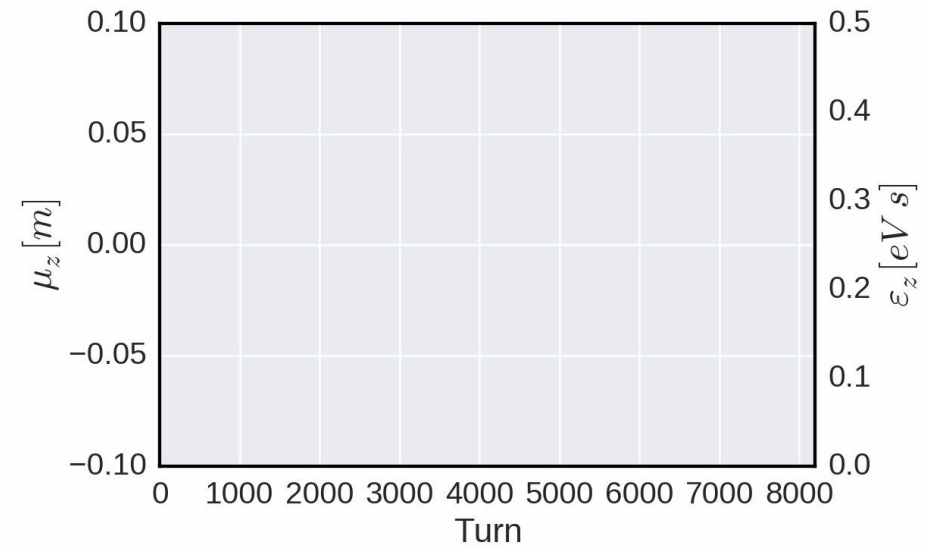
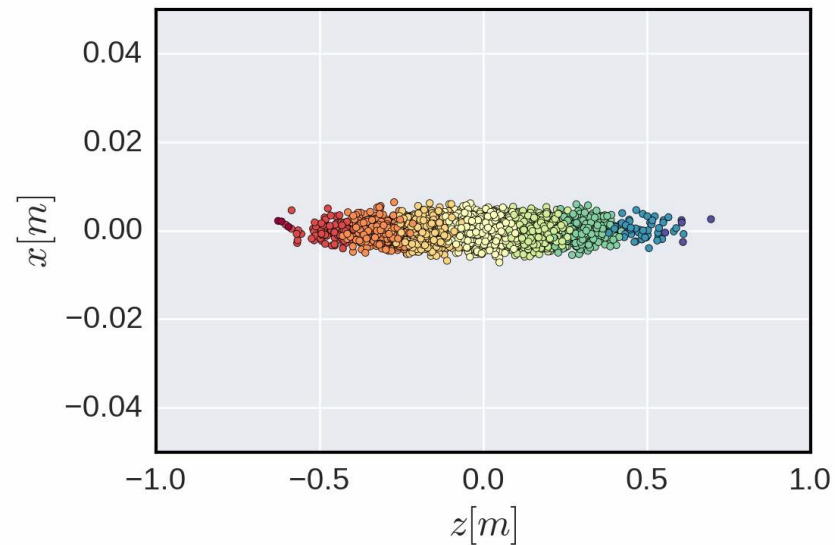
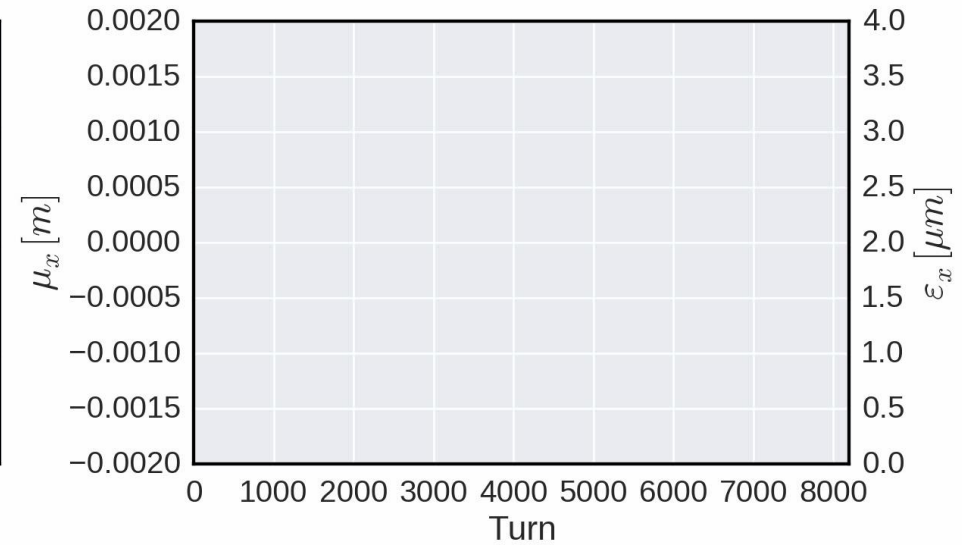
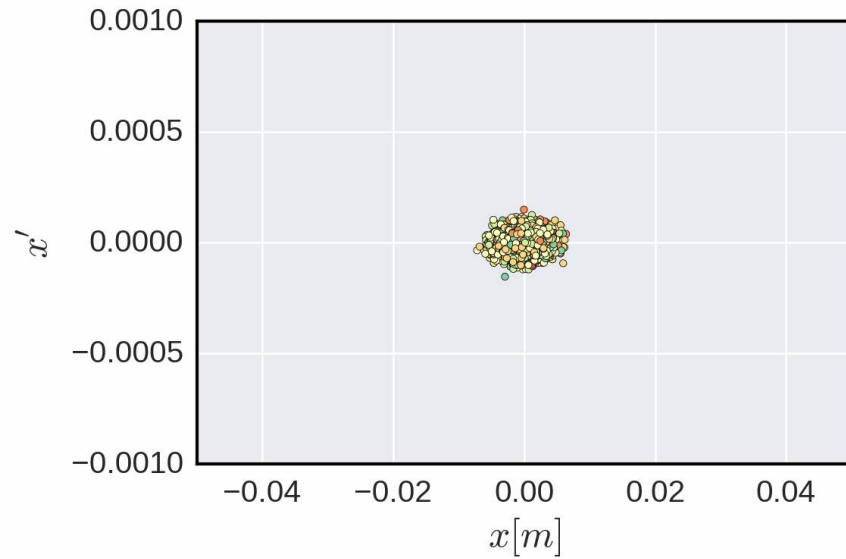
Single RF system  
 $\omega_{\text{rf}} = 200 \text{ MHz}$   
 $V_{\text{rf}}^{\text{max}} = 3 \text{ MV}$

$$\Delta x' = -\frac{e^2}{\beta^2 E_0} \int \lambda(z') \langle x \rangle(z') W_{Dx}^{\text{Ring}}(z - z') dz'$$

$$\Delta E = eV_{\text{rf}}(z)$$

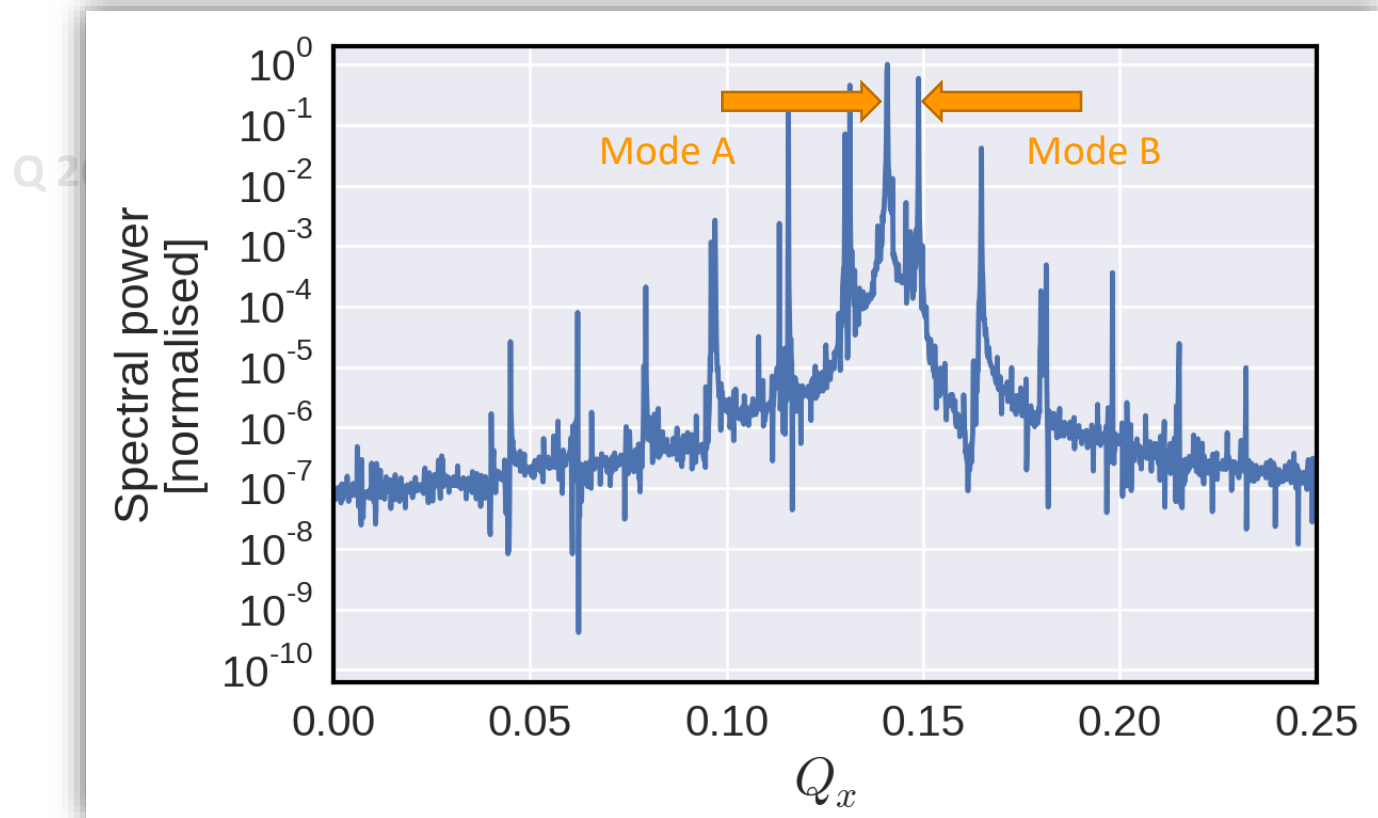
# Dipole wakes – below instability threshold

- Bunch is stable up to a certain intensity ( $N_b < N_{thr}$ )



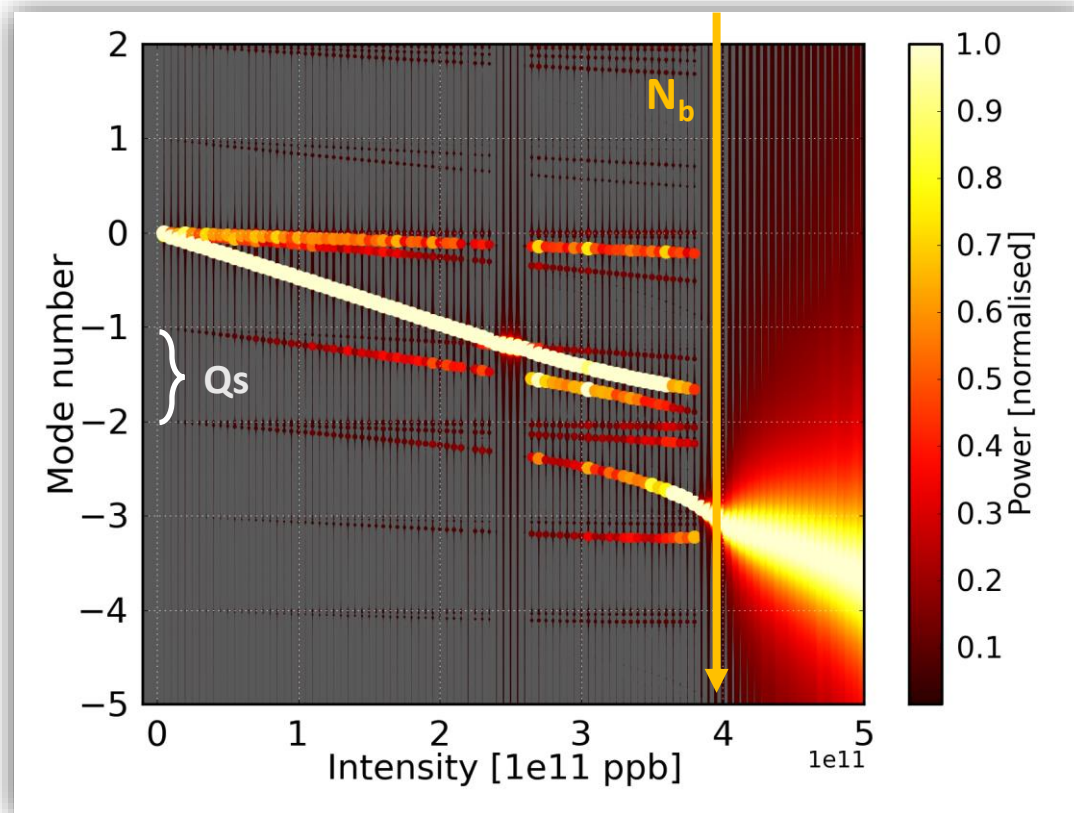
# Coherent modes of the bunch

- Bunch is stable up to a certain intensity ( $N_b < N_{thr}$ )
- Fourier analysis of bunch centroid reveals the existence of many modes



# Coherent modes of the bunch

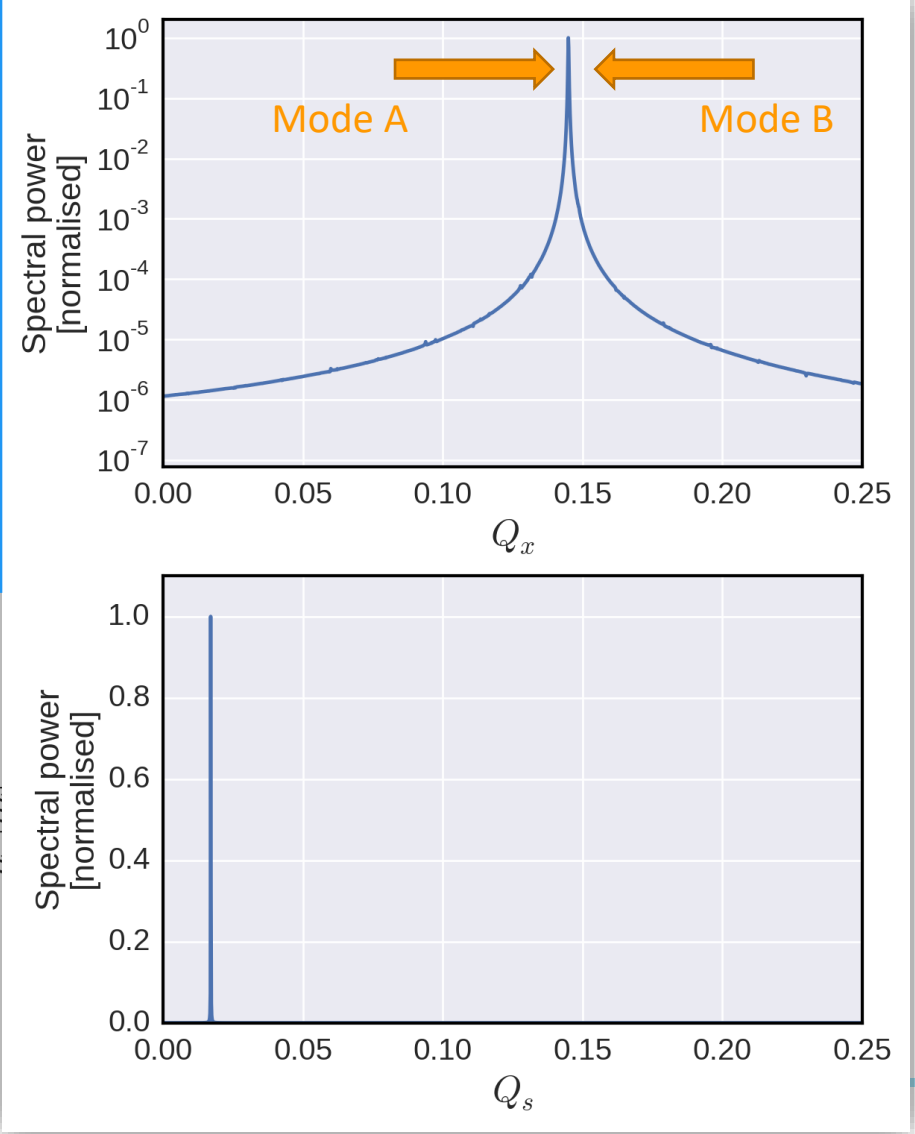
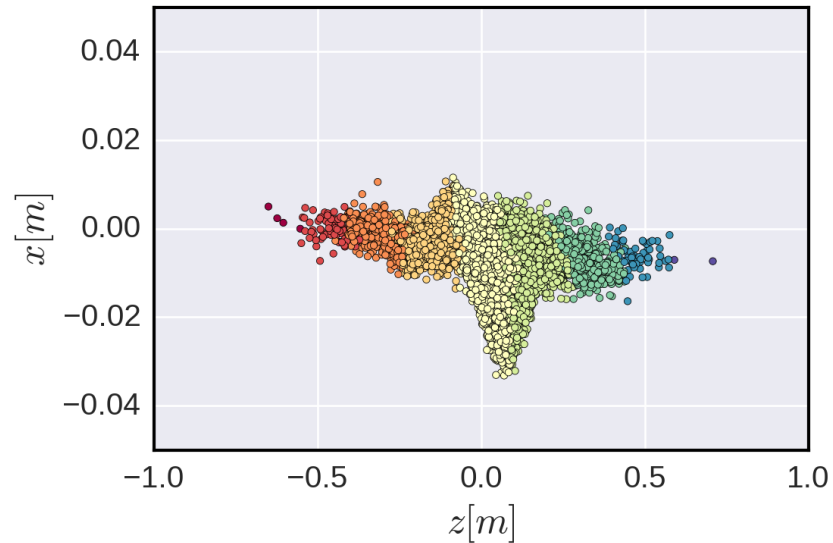
- Bunch is stable up to a certain intensity ( $N_b < N_{thr}$ )
- Fourier analysis of bunch centroid reveals the existence of many modes
  - Separated by  $\omega_s$  at very low intensity
  - Shifting closer to each other for increasing intensity and eventually merging



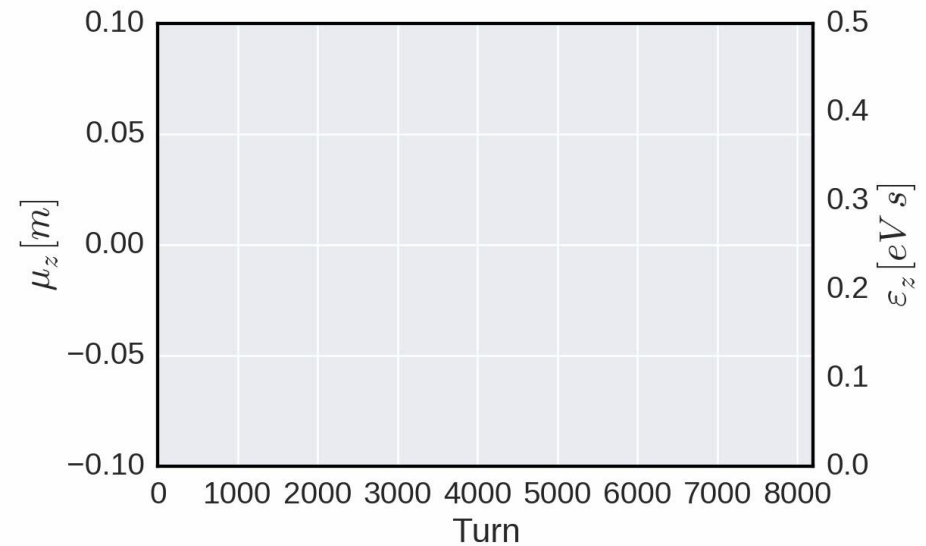
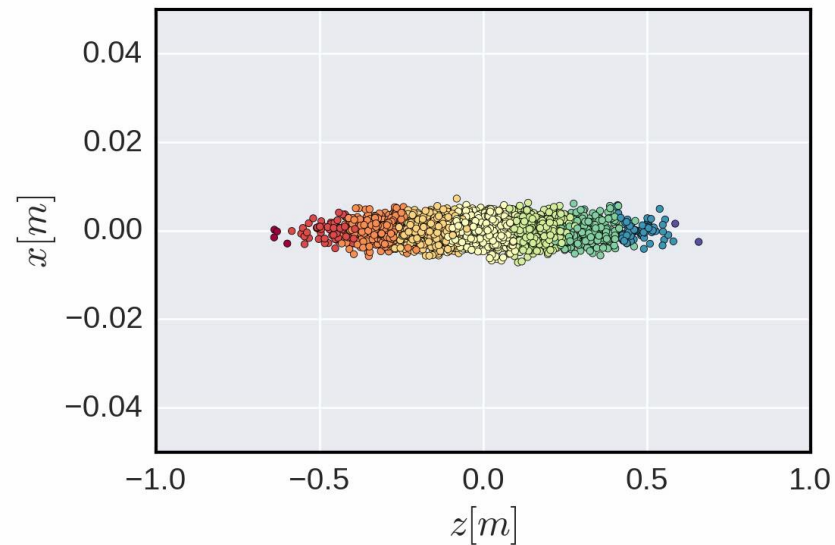
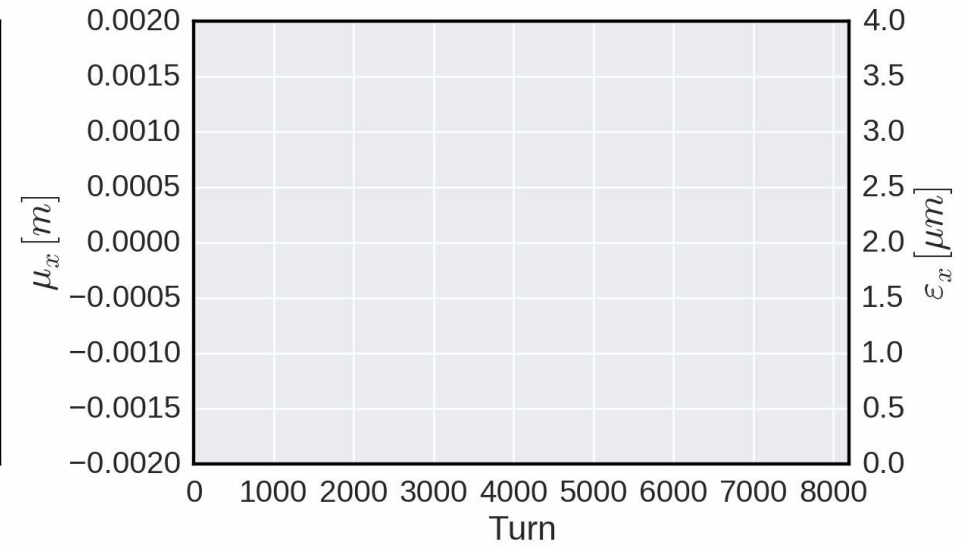
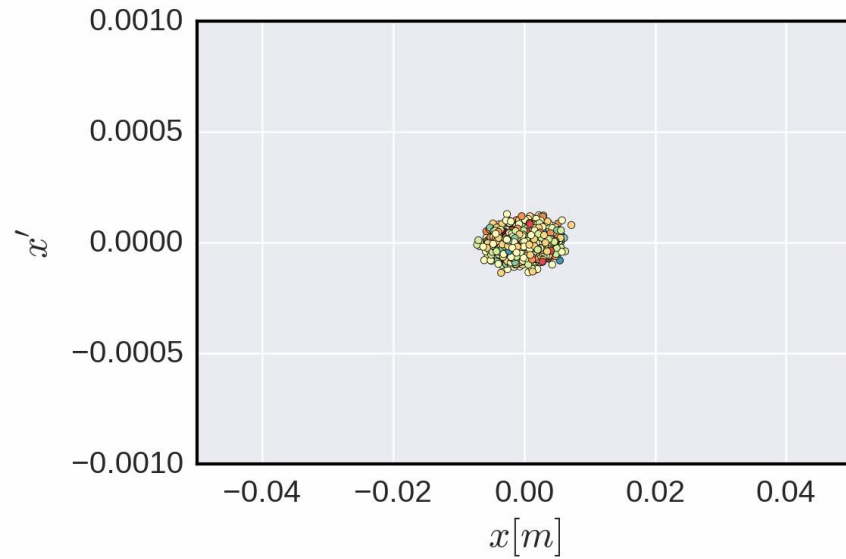


# Dipole wakes – above instability threshold

When the two modes merge a fast coherent instability arises – the transverse mode coupling instability (TMCI) which often is a hard intensity limit in many machines



# Dipole wakes – above instability threshold



# Typical mode shift patterns

- Modes exhibit a complicated shift pattern depending on the bunch parameters
- The shift of the modes can be calculated via Vlasov equation, analytical expression available for low intensity

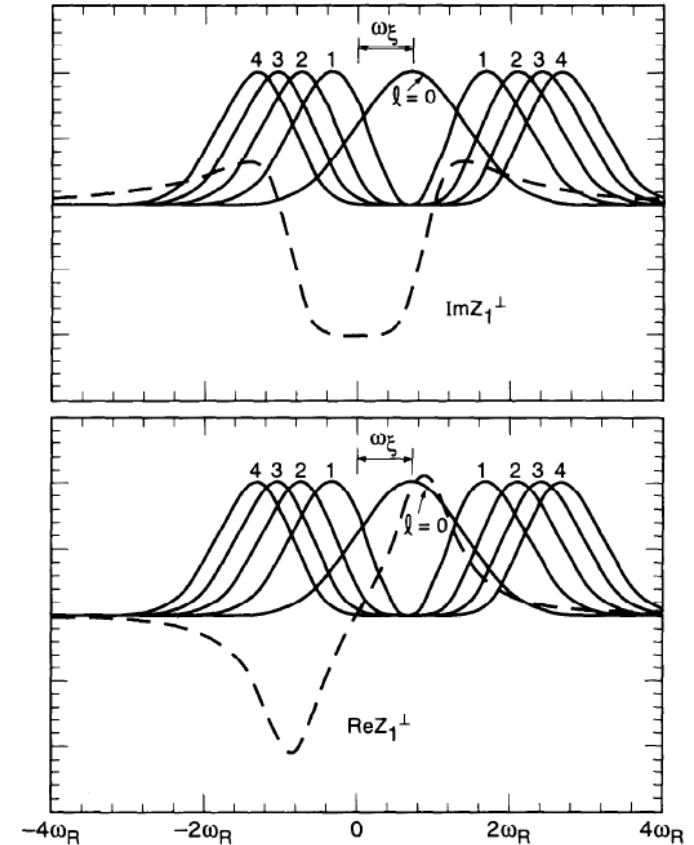
$$\Omega^{(l)} - \omega_\beta - l\omega_s \approx -\frac{i}{4\pi} \frac{\Gamma(l + \frac{1}{2})}{2^{2l} l!} \frac{Ne^2 \bar{\beta}_{x,y}}{m_0 \gamma C \sigma_z} \frac{\sum_{p=-\infty}^{\infty} Z_1^\perp(\omega') h_l(\omega' - \omega_\xi)}{\sum_{p=-\infty}^{\infty} h_l(\omega' - \omega_\xi)}$$

$$\omega' = p\omega_0 + \omega_{\beta x,y} + l\omega_s$$

$$\omega_\xi = \frac{\xi_{x,y} \omega_{\beta x,y}}{\eta}$$

$$h_l(\omega) = \frac{[J_{l+1/2}(\omega \hat{z}/c)]^2}{|\omega \hat{z}/c|} \quad \text{parabolic}$$

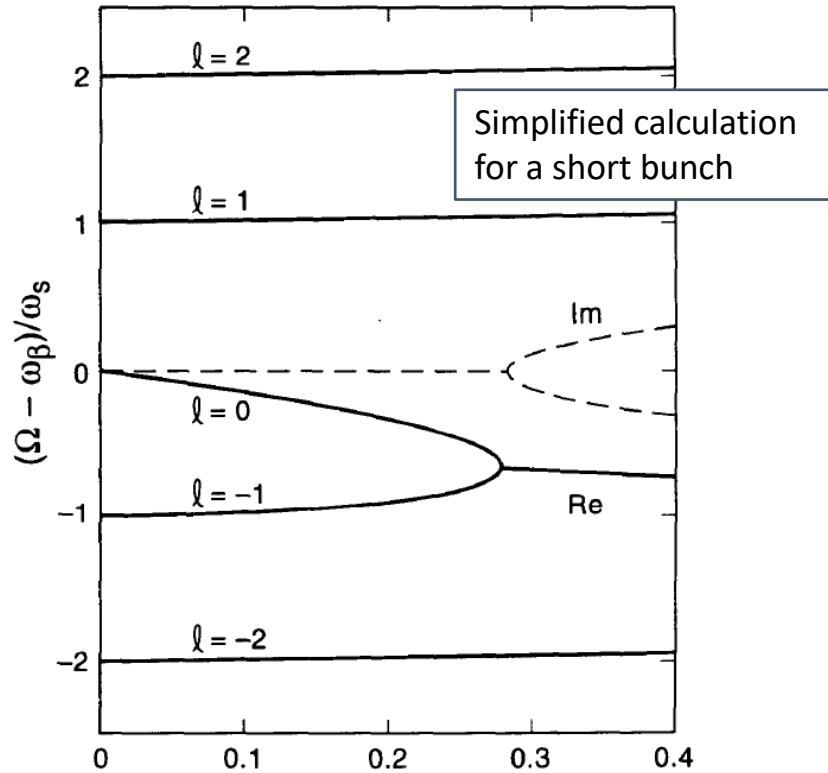
$$h_l(\omega) = \left(\frac{\omega \sigma_z}{c}\right)^{2l} \exp\left(-\frac{\omega^2 \sigma_z^2}{c^2}\right) \quad \text{Gaussian}$$



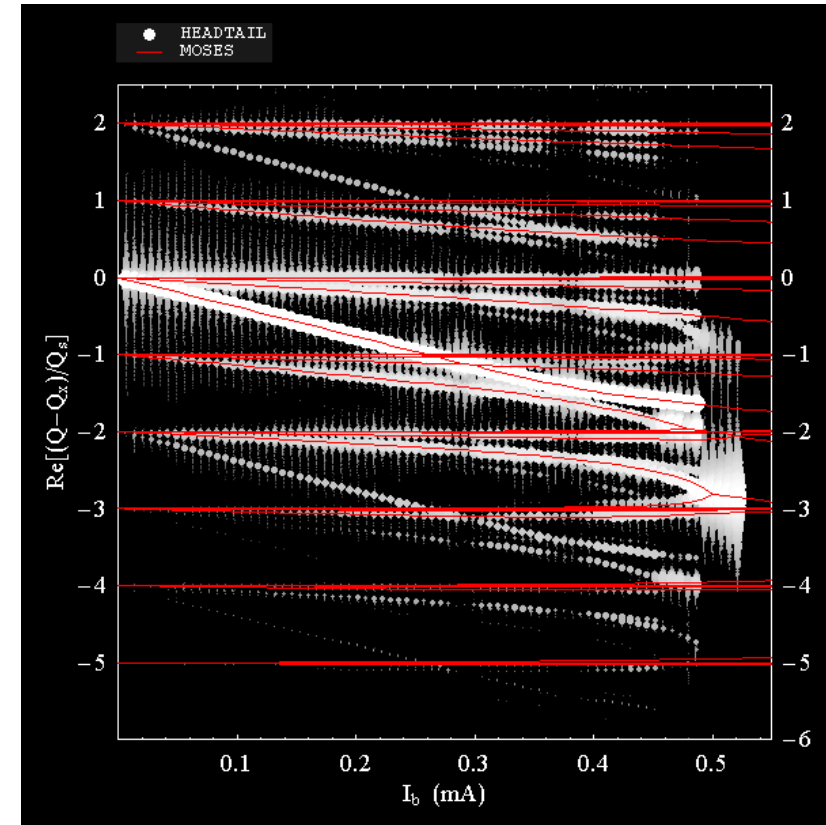
Spectra of  $h_l(\omega - \omega_\xi)$  and real + imaginary part of a broadband impedance

# Typical mode shift patterns

- Modes exhibit a complicated shift pattern depending on the bunch parameters
- The shift of the modes can be calculated via Vlasov equation



Rough criterion for instability threshold is when  $\Delta\omega_\beta|_{l=0} = \omega_s/2$



Full calculation for a long SPS bunch (red lines) + macroparticle simulation (white traces)

# Effect of dipole wakes on a particle bunch

$$\Delta x'[i] = -\frac{e^2}{m\gamma\beta^2 c^2 C} \sum_{j=0}^i N[j] \langle x \rangle [j] \cdot W_{Dx}[i-j]$$

Dipolar term  $\rightarrow$  orbit kick

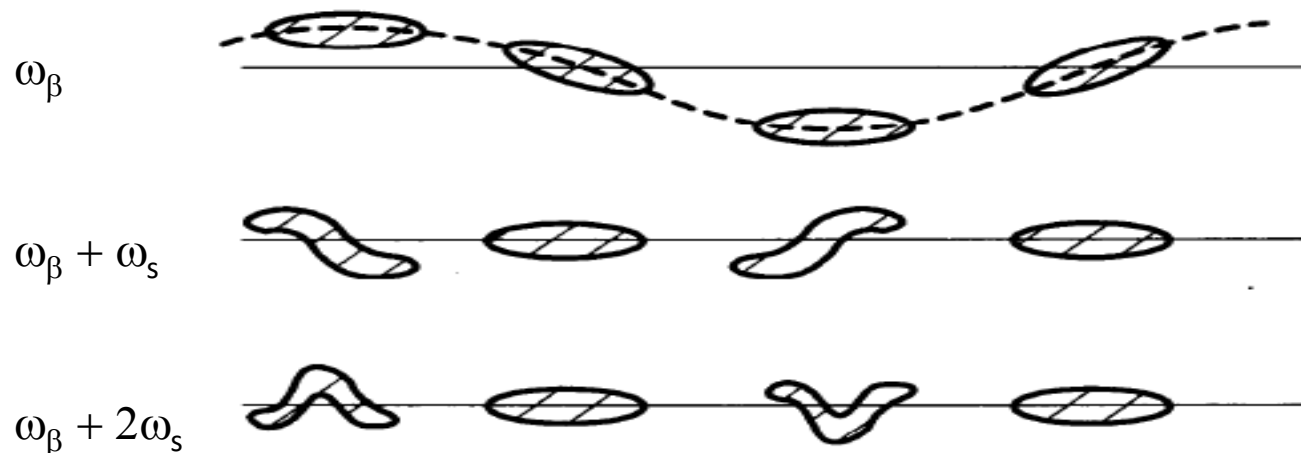
With synchrotron motion we can get into a loop

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  - Chromaticity  $\neq 0$ 
    - **Headtail modes**  $\rightarrow$  beam is unstable (can be very weak and often damped by non-linearities)

# Dipole wakes – headtail modes

- As soon as **chromaticity is non-zero**, a ‘resonant’ condition can be met as particles now can ‘synchronize’ their synchrotron amplitude dependent betatron motion with the action of the wake fields.
- **Headtail modes arise** – the order of the respective mode depends on the chromaticity together with the impedance and bunch spectrum
- Different transverse head-tail modes **correspond to different parts of the bunch** oscillating with relative phase differences, for example:
  - Mode 0 is a rigid bunch mode
  - Mode 1 has head and tail oscillating in counter-phase
  - Mode 2 has head and tail oscillating in phase and the bunch center in opposition



# Dipole wakes – headtail modes

- As soon as **chromaticity** is introduced, their synchrotron oscillations are coupled.
- **Headtail modes** are excited by the longitudinal impedance and the chromaticity.
- Different transition frequencies lead to different phase differences between the synchrotron oscillations and the dipole wakes.
  - Mode 0 is a dipole wake.
  - Mode 1 has a quadrupole wake.
  - Mode 2 has a sextupole wake.

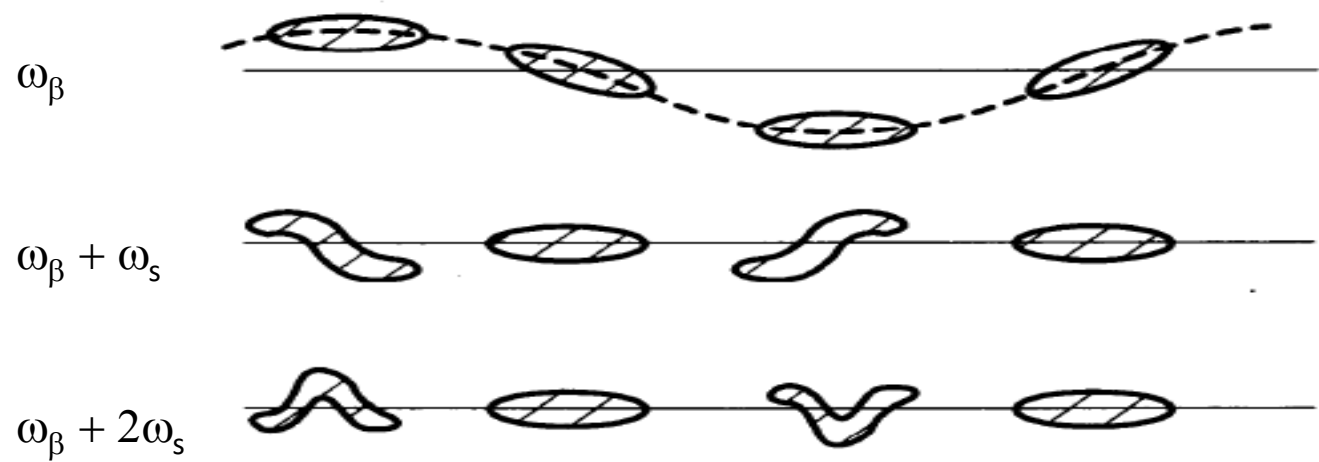
Remark:

Due to this ‘synchronicity’, **below transition** ( $\eta < 0$ ):

- Mode 0 is unstable if  $Q' > 0$ .
- Higher order modes tend to be unstable if  $Q' < 0$  (though at lower growth rates).

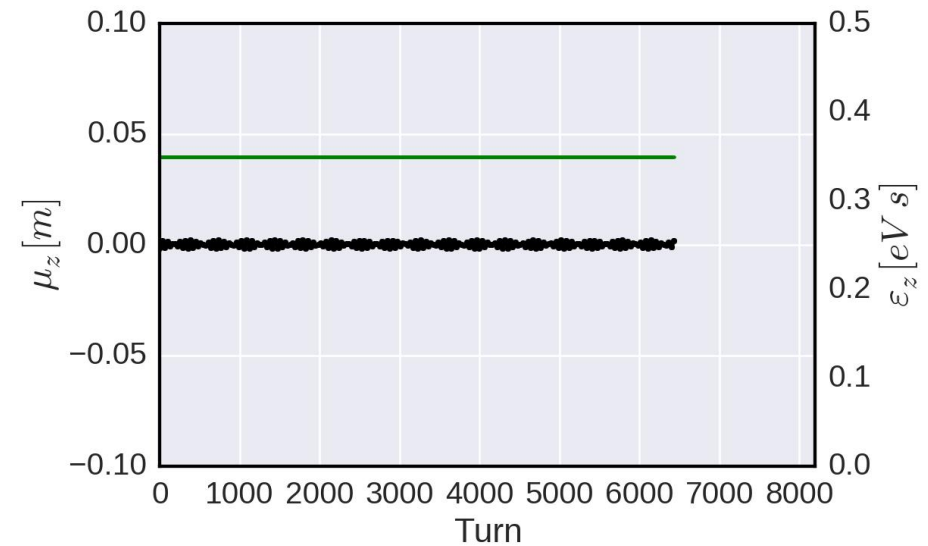
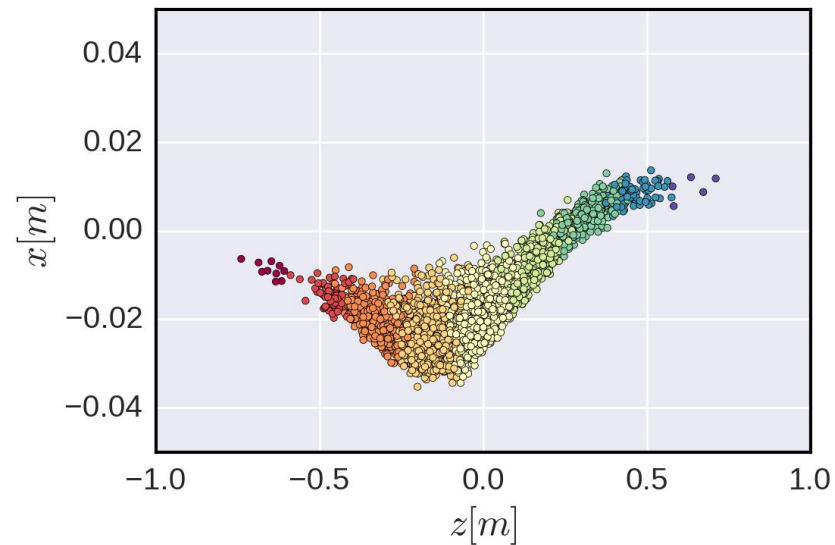
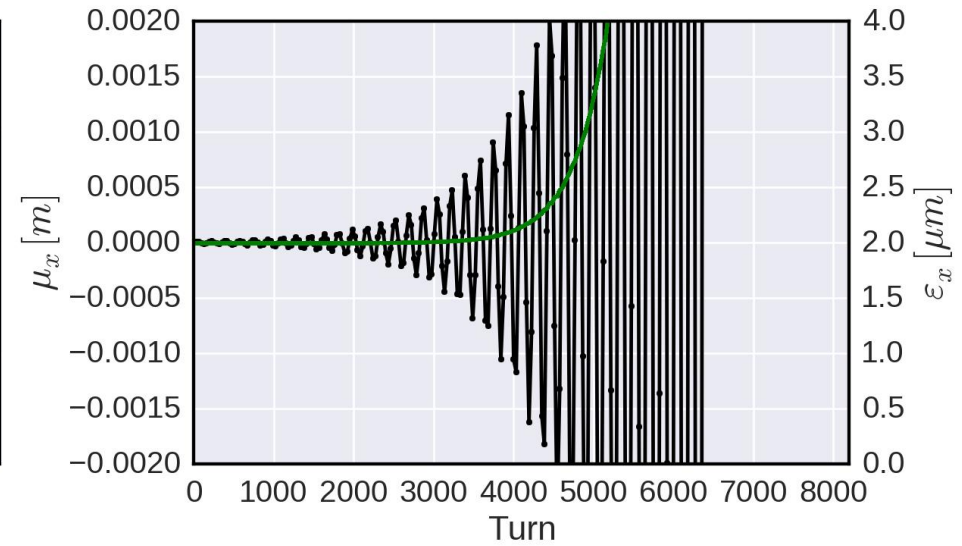
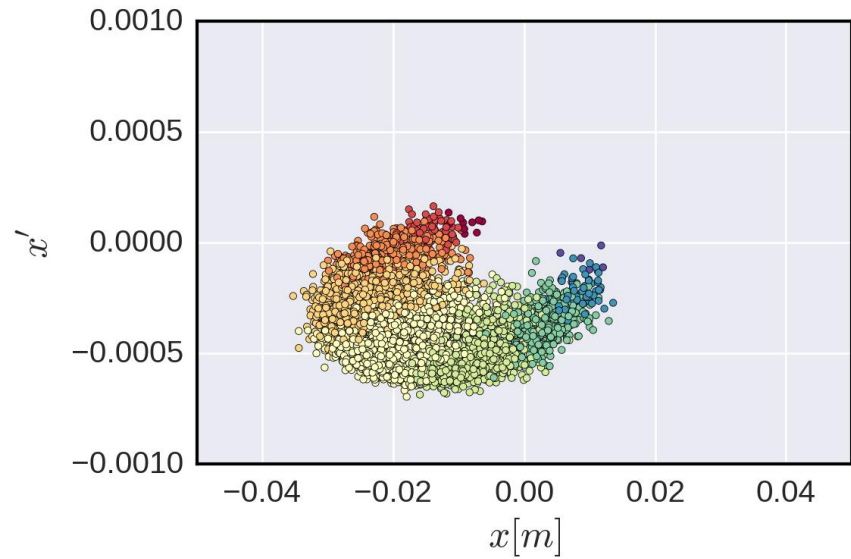
The **situation is reversed** when a machine is operated above transition.

‘synchronize’  
together with the  
synchrotron oscillations  
with relative



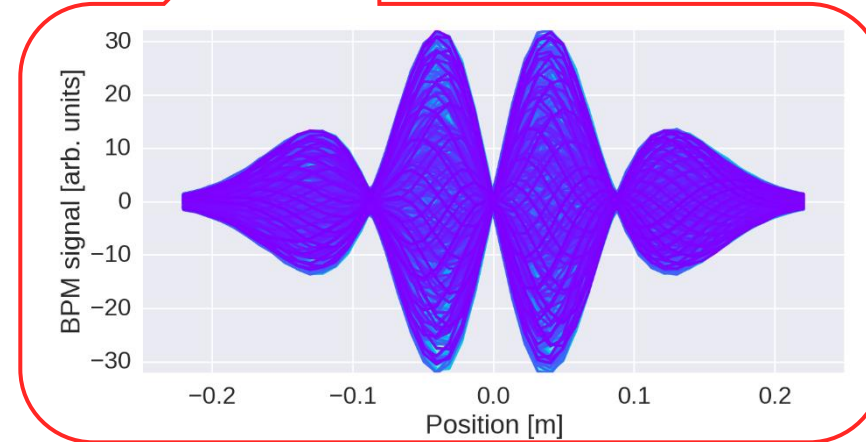
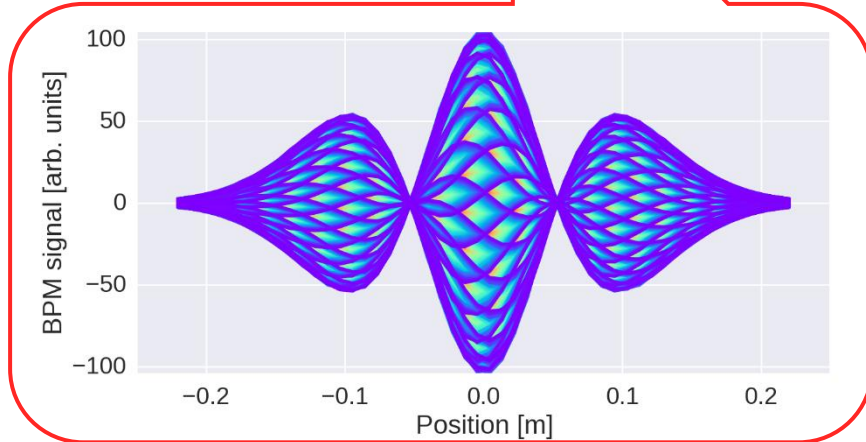
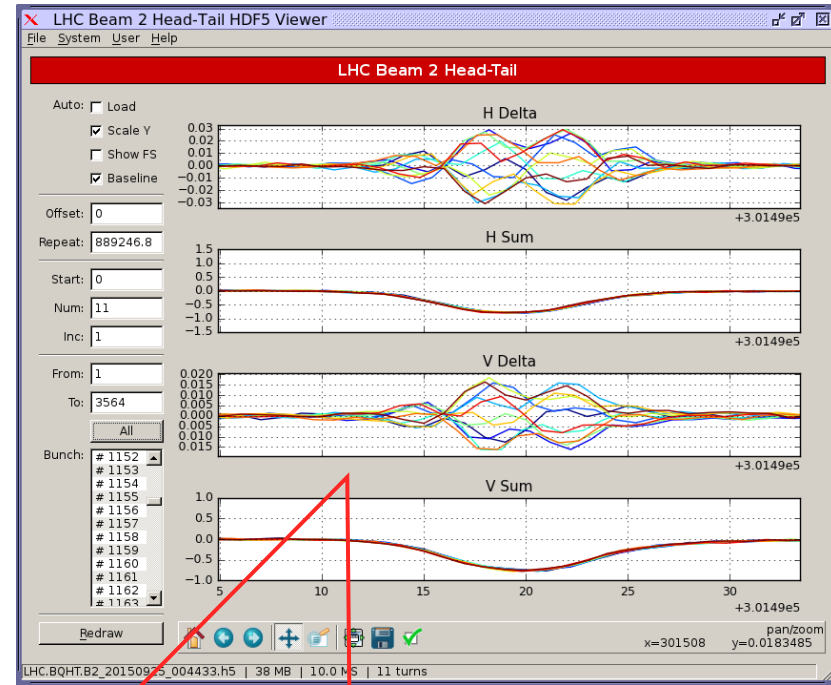
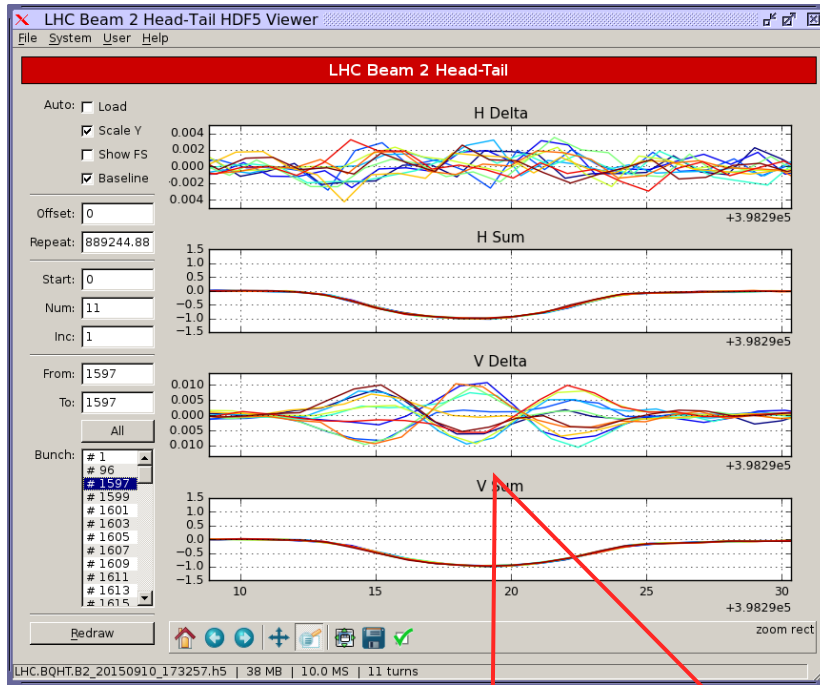


# Dipole wakes – headtail modes





# Example: Headtail modes in the LHC





We have **discussed transverse wake fields** and impedances, their classification into different types along with their impact on the beam dynamics.

We have modeled the **wake field interaction** with a charged particle beam.

We have seen some examples of the effects of transverse wake fields on the beam such as

**Closed orbit distortion**

Some types of **transverse beam instability**

## Tomorrow Part 4

→ Electron cloud build up and effects on beam dynamics

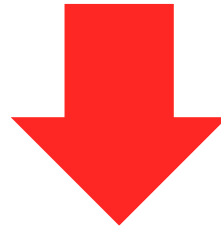
# End part 3





# The Strong Head Tail Instability

- Aka the Transverse Mode Coupling Instability:
  - To illustrate TMCI we will need to make use of **some simplifications**:
    - The bunch **is represented through two particles** carrying half the total bunch charge and placed in opposite phase in the longitudinal phase space
    - They both feel external linear focusing in all three directions (i.e. linear betatron focusing + linear synchrotron focusing).
    - Zero chromaticity ( $Q'_{x,y}=0$ )
    - Constant transverse wake left behind by the leading particle
    - Smooth approximation  $\rightarrow$  constant focusing + distributed wake



We will:

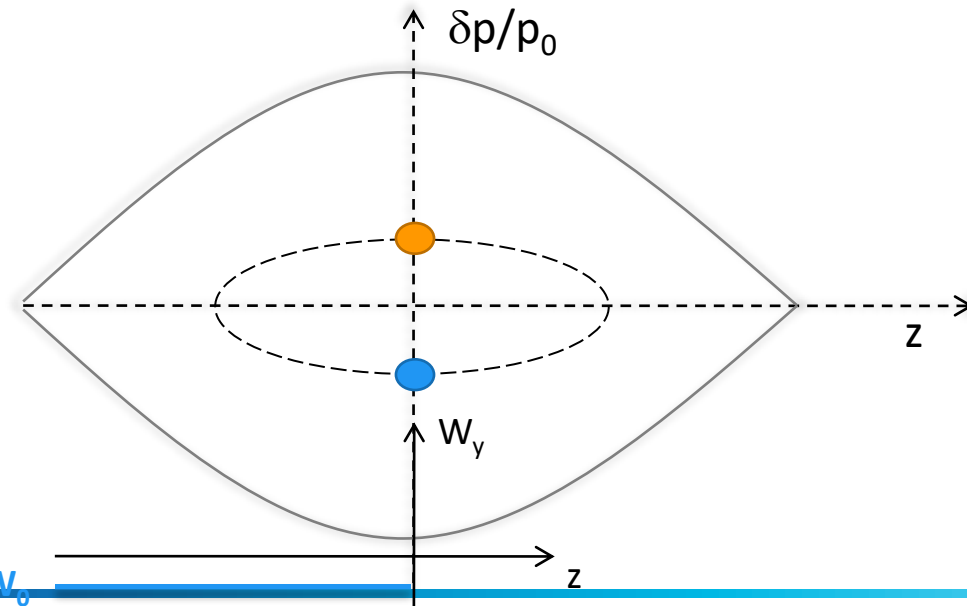
- Calculate a stability condition (threshold) for the transverse motion
- Have a look at the excited oscillation modes of the centroid

# The Strong Head Tail Instability

- During the first half of the synchrotron motion, particle 1 is leading and executes free betatron oscillations, while particle 2 is trailing and feels the defocusing wake of particle 1

$$\begin{cases} \frac{d^2 y_1}{ds^2} + \left(\frac{\omega_\beta}{c}\right)^2 y_1 = 0 \\ \frac{d^2 y_2}{ds^2} + \left(\frac{\omega_\beta}{c}\right)^2 y_2 = \left(\frac{e^2}{m_0 c^2}\right) \frac{N W_0}{2\gamma C} y_1(s) \end{cases} \quad 0 < s < \frac{\pi C}{\omega_s}$$

$T < T_s/2$



● Particle 1 (+Ne/2)

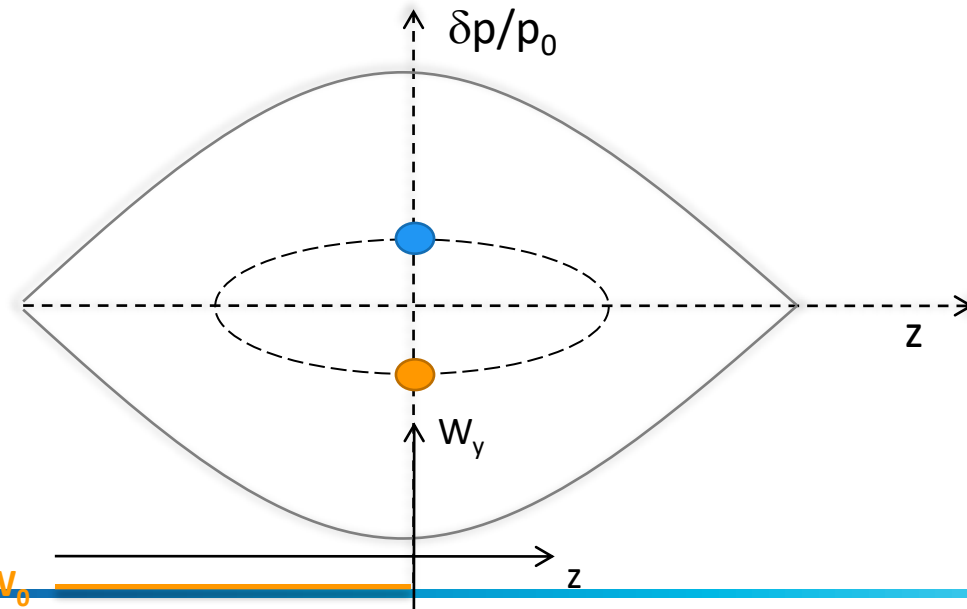
● Particle 2 (+Ne/2)

# The Strong Head Tail Instability

- During the first half of the synchrotron motion, particle 1 is leading and executes free betatron oscillations, while particle 2 is trailing and feels the defocusing wake of particle 1
- During the second half of the synchrotron period, the situation is reversed:

$$\begin{cases} \frac{d^2 y_1}{ds^2} + \left(\frac{\omega_\beta}{c}\right)^2 y_1 = \left(\frac{e^2}{m_0 c^2}\right) \frac{N W_0}{2\gamma C} y_2(s) \\ \frac{d^2 y_2}{ds^2} + \left(\frac{\omega_\beta}{c}\right)^2 y_2 = 0 \end{cases} \quad \frac{\pi C}{\omega_s} < s < \frac{2\pi C}{\omega_s}$$

$T \approx T_s/2$



● Particle 1 (+Ne/2)

● Particle 2 (+Ne/2)

# The Strong Head Tail Instability

- We solve with respect to the complex variables defined below during the first half of synchrotron period
- $y_1(s)$  is a free betatron oscillation
- $y_2(s)$  is the sum of a free betatron oscillation plus a driven oscillation with  $y_1(s)$  being its driving term

$$\tilde{y}_{1,2}(s) = y_{1,2}(s) + i \frac{c}{\omega_\beta} y'_{1,2}(s)$$

$$\tilde{y}_1(s) = \tilde{y}_1(0) \exp\left(-\frac{i\omega_\beta s}{c}\right)$$

$$\tilde{y}_2(s) = \underbrace{\tilde{y}_2(0) \exp\left(-\frac{i\omega_\beta s}{c}\right)}_{\text{Free oscillation term}}$$

$$+ \underbrace{i \frac{Ne^2 W_0}{4 m_0 \gamma c C \omega_\beta} \left( \frac{c}{\omega_\beta} \tilde{y}_1^*(0) \sin\left(\frac{\omega_\beta s}{c}\right) + \tilde{y}_1(0) s \exp\left(-\frac{i\omega_\beta s}{c}\right) \right)}_{\text{Driven oscillation term}}$$

since we consider  $s = \frac{\pi c}{\omega_s}$

- Second term in RHS equation for  $y_2(s)$  negligible if  $\omega_s \ll \omega_\beta$
- We can now transform these equations into linear mapping across half synchrotron period



# The Strong Head Tail Instability

- We can now transform these equations into **linear mapping** across half synchrotron period

$$\begin{pmatrix} \tilde{y}_1 \\ \tilde{y}_2 \end{pmatrix}_{s=\pi c/\omega_s} = \left[ \exp\left(-\frac{i\pi\omega_\beta}{\omega_s}\right) \cdot \begin{pmatrix} 1 & 0 \\ i\Upsilon & 1 \end{pmatrix} \right] \cdot \begin{pmatrix} \tilde{y}_1 \\ \tilde{y}_2 \end{pmatrix}_{s=0}, \quad \Upsilon = \frac{\pi N e^2 W_0}{4 m_0 \gamma C \omega_\beta \omega_s}$$

- In the second half of synchrotron period, **particles 1 and 2 exchange their roles** – we can therefore find the transfer matrix over the full synchrotron period for both particles. We can **analyze the eigenvalues** of the two particle system

$$\begin{aligned} \begin{pmatrix} \tilde{y}_1 \\ \tilde{y}_2 \end{pmatrix}_{s=2\pi c/\omega_s} &= \left[ \exp\left(-\frac{i2\pi\omega_\beta}{\omega_s}\right) \cdot \begin{pmatrix} 1 & i\Upsilon \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 1 & 0 \\ i\Upsilon & 1 \end{pmatrix} \right] \cdot \begin{pmatrix} \tilde{y}_1 \\ \tilde{y}_2 \end{pmatrix}_{s=0} \\ &= \left[ \exp\left(-\frac{i2\pi\omega_\beta}{\omega_s}\right) \cdot \begin{pmatrix} 1 - \Upsilon^2 & i\Upsilon \\ i\Upsilon & 1 \end{pmatrix} \right] \cdot \begin{pmatrix} \tilde{y}_1 \\ \tilde{y}_2 \end{pmatrix}_{s=0} \end{aligned}$$

# Strong Head Tail Instability – stability condition

$$\lambda_1 \cdot \lambda_2 = 1 \Rightarrow \lambda_{1,2} = \exp(\pm i\varphi)$$

$$\lambda_1 + \lambda_2 = 2 - \Upsilon^2 \Rightarrow \sin\left(\frac{\varphi}{2}\right) = \frac{\Upsilon}{2}$$

$$\Rightarrow \Upsilon = \frac{\pi N e^2 W_0}{4 m_0 \gamma C \omega_\beta \omega_s} \leq 2$$

- Since the product of the eigenvalues is 1, the only condition for stability is that they both be purely imaginary exponentials
- From the second equation for the eigenvalues, it is clear that this is true only when  $\sin(\varphi/2) < 1$
- This translates into a **stability condition** on the beam/wake parameters

# Strong Head Tail Instability – stability condition

$$N \leq N_{\text{threshold}} = \frac{8}{\pi e^2} \frac{p_0 \omega_s}{\beta_y} \left( \frac{C}{W_0} \right)$$

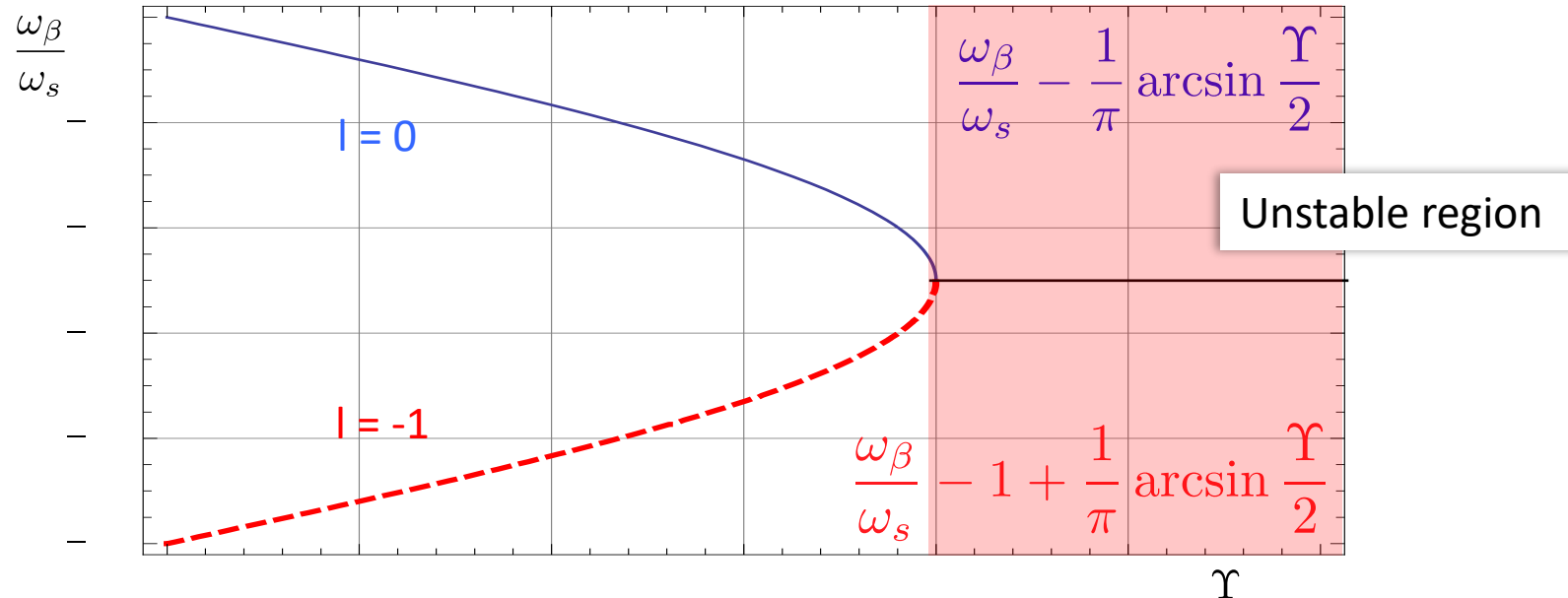
- Proportional to  $p_0 \rightarrow$  bunches with higher energy tend to be more stable
  - Proportional to  $\omega_s \rightarrow$  the quicker is the longitudinal motion within the bunch, the more stable is the bunch
  - Inversely proportional to  $\beta_y \rightarrow$  the effect of the impedance is enhanced if the kick is given at a location with large beta function
- Inversely proportional to the wake per unit length along the ring,  $W_0/C \rightarrow$  a large integrated wake (impedance) lowers the instability threshold

# Strong Head Tail Instability – mode frequencies

- The evolution of the eigenstates follows:

$$\begin{pmatrix} \tilde{V}_{+n} \\ \tilde{V}_{-n} \end{pmatrix} = \exp\left(-i\frac{2\pi\omega_\beta}{\omega_s}n\right) \cdot \begin{pmatrix} \exp\left[-2i\arcsin\left(\frac{\Upsilon}{2}\right) \cdot n\right] & 0 \\ 0 & \exp\left[2i\arcsin\left(\frac{\Upsilon}{2}\right) \cdot n\right] \end{pmatrix} \begin{pmatrix} \tilde{V}_{+0} \\ \tilde{V}_{-0} \end{pmatrix}$$

Eigenfrequencies:  $\omega_\beta + l\omega_s \pm \frac{\omega_s}{\pi} \arcsin \frac{\Upsilon}{2}$  They shift with increasing intensity

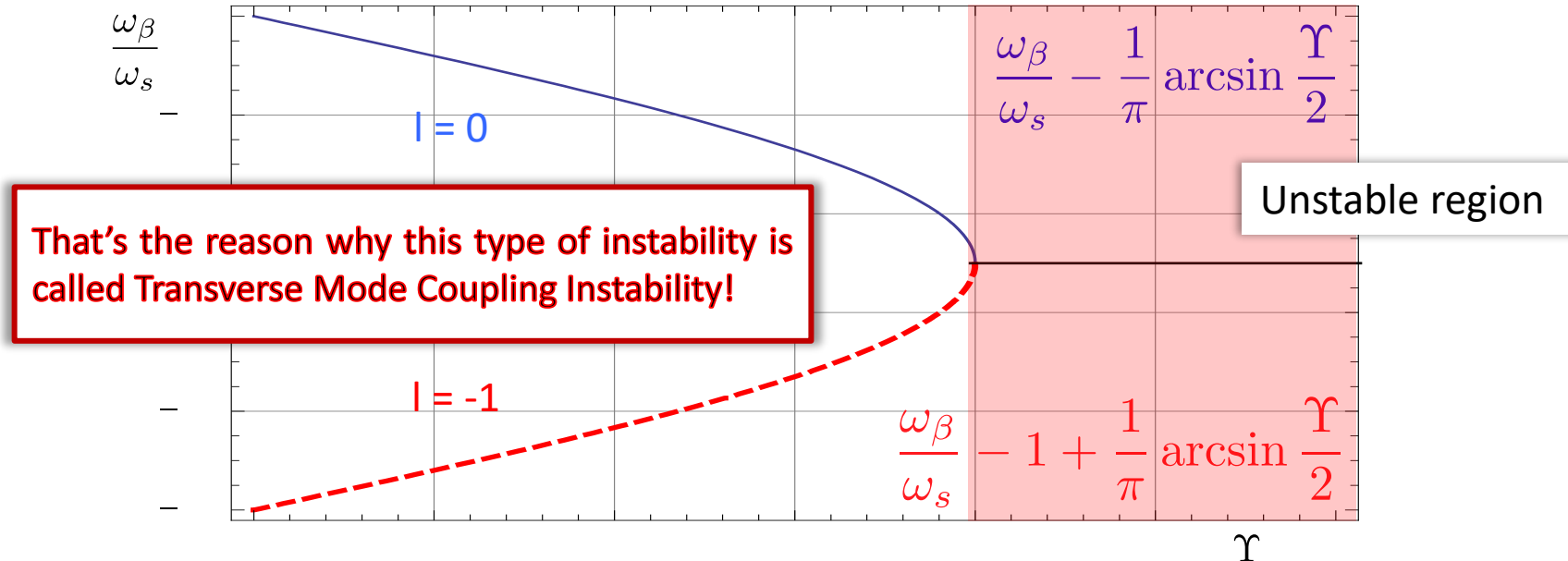


# Strong Head Tail Instability – mode frequencies

- The evolution of the eigenstates follows:

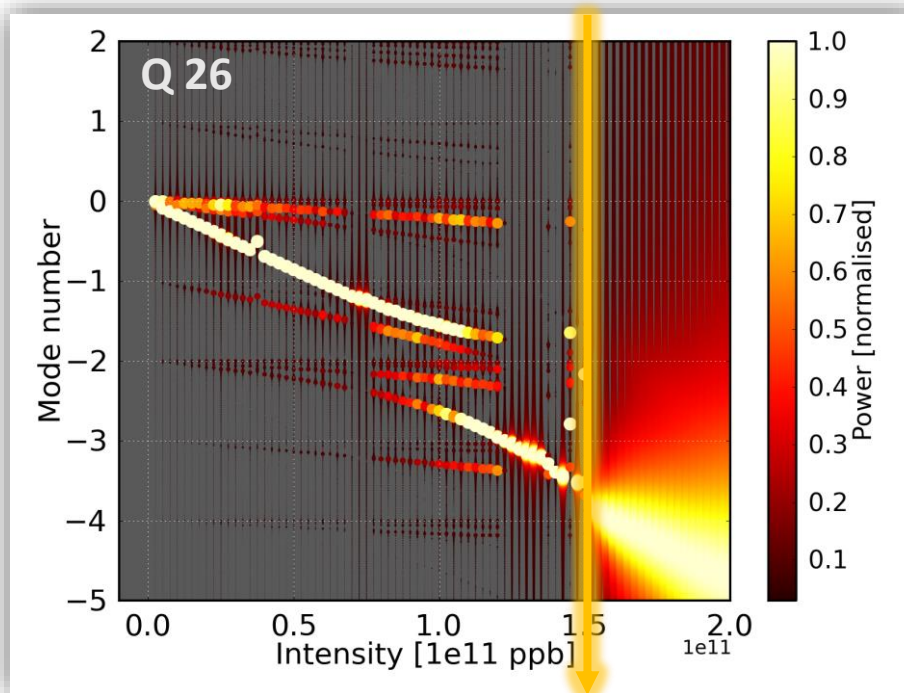
$$\begin{pmatrix} \tilde{V}_{+n} \\ \tilde{V}_{-n} \end{pmatrix} = \exp\left(-i\frac{2\pi\omega_\beta}{\omega_s}n\right) \cdot \begin{pmatrix} \exp\left[-2i\arcsin\left(\frac{\Upsilon}{2}\right) \cdot n\right] & 0 \\ 0 & \exp\left[2i\arcsin\left(\frac{\Upsilon}{2}\right) \cdot n\right] \end{pmatrix} \begin{pmatrix} \tilde{V}_{+0} \\ \tilde{V}_{-0} \end{pmatrix}$$

Eigenfrequencies:  $\omega_\beta + l\omega_s \pm \frac{\omega_s}{\pi} \arcsin \frac{\Upsilon}{2}$  They shift with increasing intensity



# Raising the TMCI threshold – SPS Q20 optics

- In **simulations** we have the possibility to perform **scans of variables**, e.g. we can run **100 simulations in parallel** changing the beam intensity
- We can then perform a **spectral analysis** of **each simulation**...
- ... and stack all obtained plot behind one another to obtain...
- ... the typical **visualization plots of TMCI**



The mode number is given as

$$m = \frac{Q_x - Q_{x0}}{Q_s}$$

The modes are separated by the synchrotron tune.

TMCI threshold

# Backup



# Wakefields – rough formalism

$$H = \frac{1}{2}p_x^2 + \frac{1}{2}K(s)x^2 + \sum_k \frac{e^2}{m\gamma\beta^2c^2C} \iiint \rho(x_s, z_s) w(x, x_s, z - z_s - kC) dx_s dz_s dx$$



# Wakefields – rough formalism

$$\begin{aligned} H &= \frac{1}{2}p_x^2 + \frac{1}{2}K(s)x^2 + \sum_k \frac{e^2}{m\gamma\beta^2c^2C} \iiint \rho(x_s, z_s) w(x, x_s, z - z_s - kC) dx_s dz_s dx \\ &= \dots + \sum_k \frac{e^2}{m\gamma\beta^2c^2C} \iiint \rho(x_s, z_s) \sum_{mn} x^n x_s^m W_{mn}(z - z_s - kC) dx_s dz_s dx \\ &= \dots + \sum_k \frac{e^2}{m\gamma\beta^2c^2C} \sum_{mn} \int x^n \int \lambda_m(z_s) W_{mn}(z - z_s - kC) dz_s dx \\ &\quad \lambda_m(z_s) = \int \rho(x_s, z_s) x_s^m dx_s \end{aligned}$$

- Expansion

# Wakefields – rough formalism

$$H = \frac{1}{2}p_x^2 + \frac{1}{2}K(s)x^2 + \sum_k \frac{e^2}{m\gamma\beta^2c^2C} \sum_{mn} \int x^n \int \lambda_m(z_s) W_{mn}(z - z_s - kC) dz_s dx$$

$$\lambda_m(z_s) = \int \rho(x_s, z_s) x_s^m dx_s$$

$$H = \frac{1}{2}p_x^2 + C + \boxed{Ax} + \boxed{\frac{1}{2}Bx^2} + \dots, \quad \text{with } \frac{dq}{ds} = \frac{\partial H(p, q)}{\partial p}, \quad \frac{dp}{ds} = -\frac{\partial H(p, q)}{\partial q}$$

Dipole term (n=1) → change of orbit

Quadrupole term (n=2) → change of tune

- Expansion – up to second order:

n	m	type
0	0, 1	
1	0	

Constant transverse wake (n=0, m=0)

Dipole transverse wake (n=0, m=1)

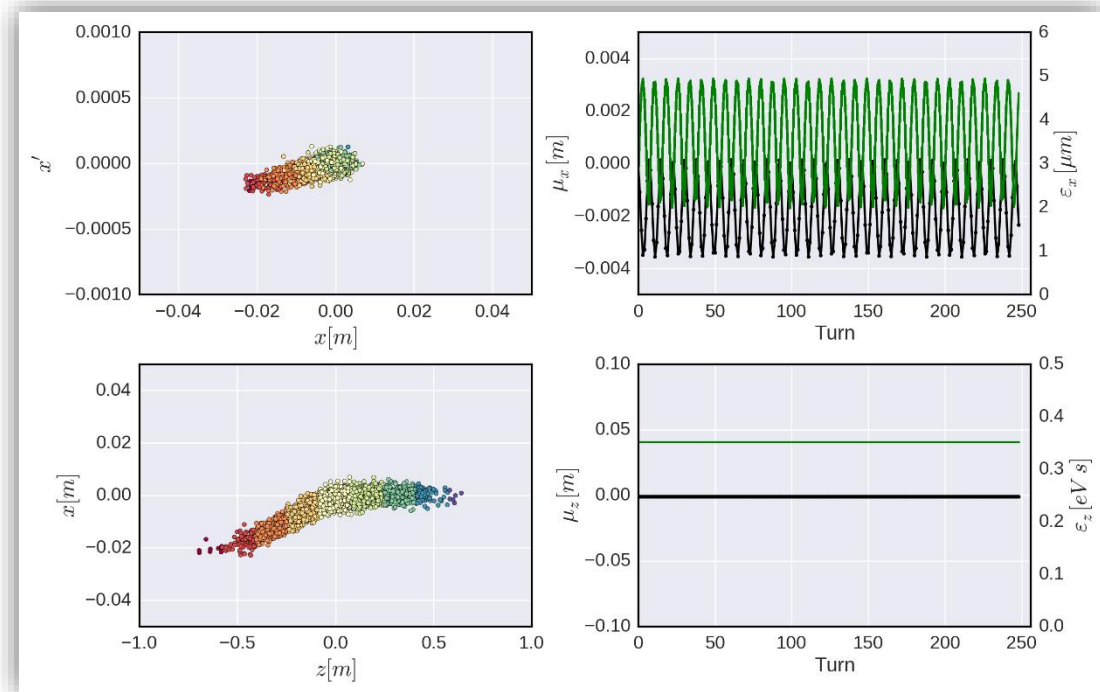
Quadrupole transverse wake (n=1, m=0)

# Examples – constant wakes

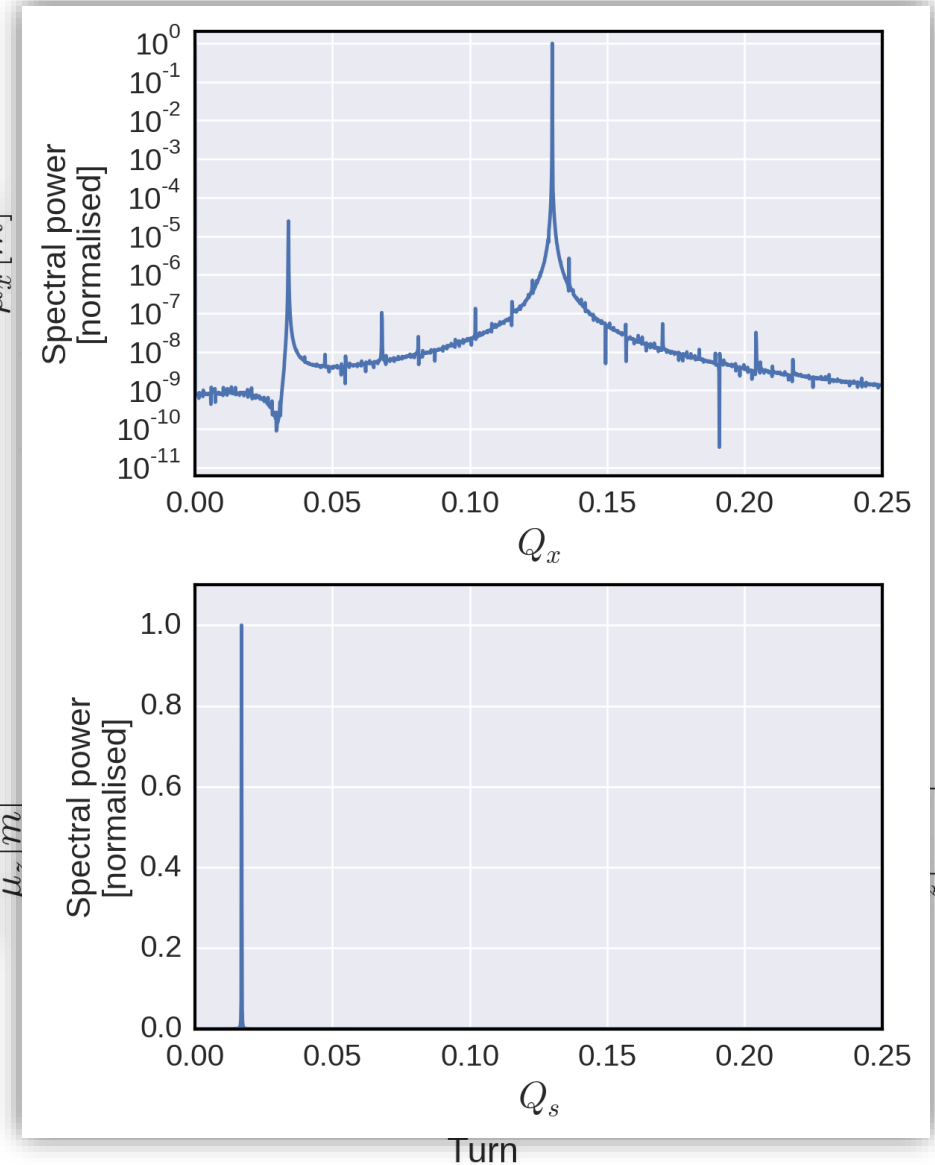
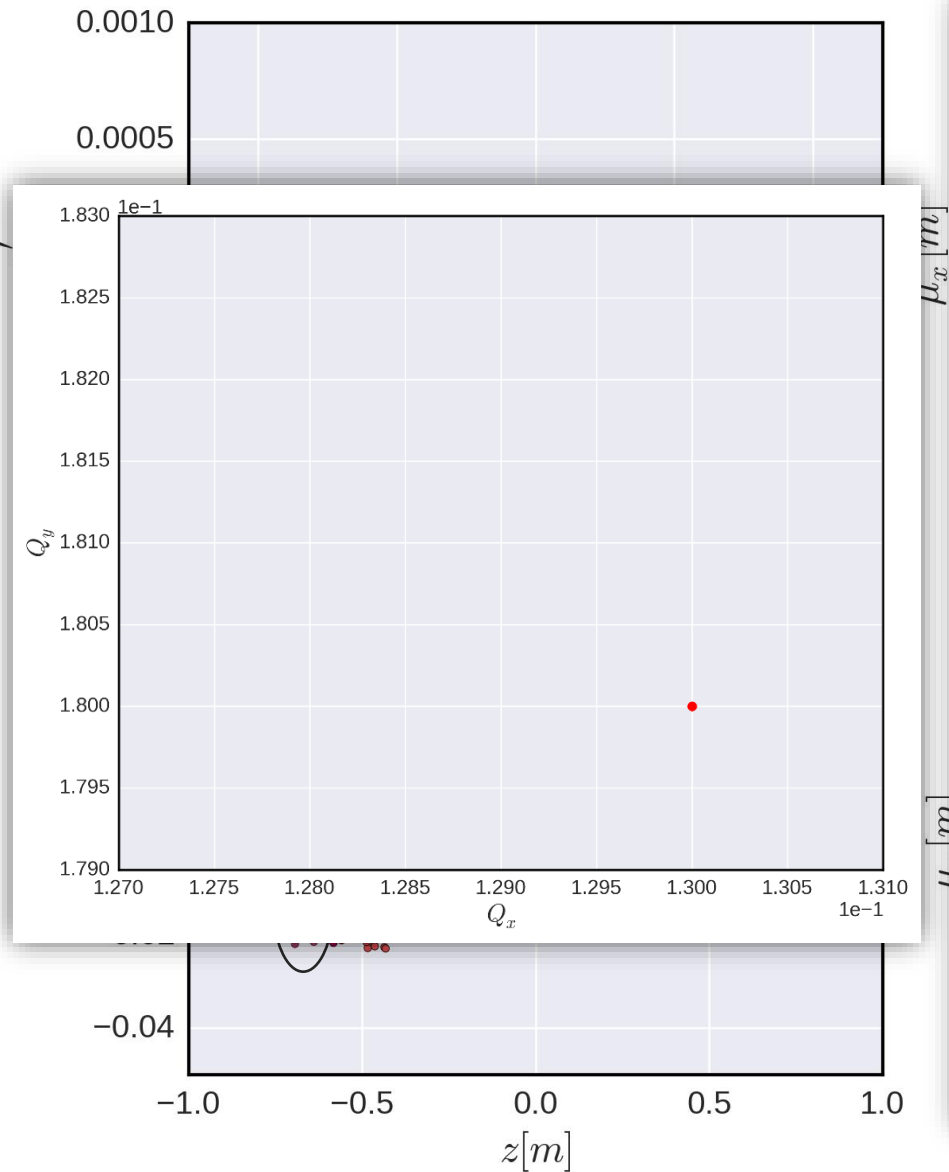
$$H = \frac{1}{2}p_x^2 + \frac{1}{2}K(s)x^2 + \frac{e^2}{m\gamma\beta^2c^2C} x \sum_{j=0}^{n\text{-slices}-1} \lambda(z_j) W_{01}(z - z_j) \Delta z_j$$

Dipolar term → orbit kick

Slice dependent change of closed orbit  
(if line density does not change)



# Examples – constant wakes

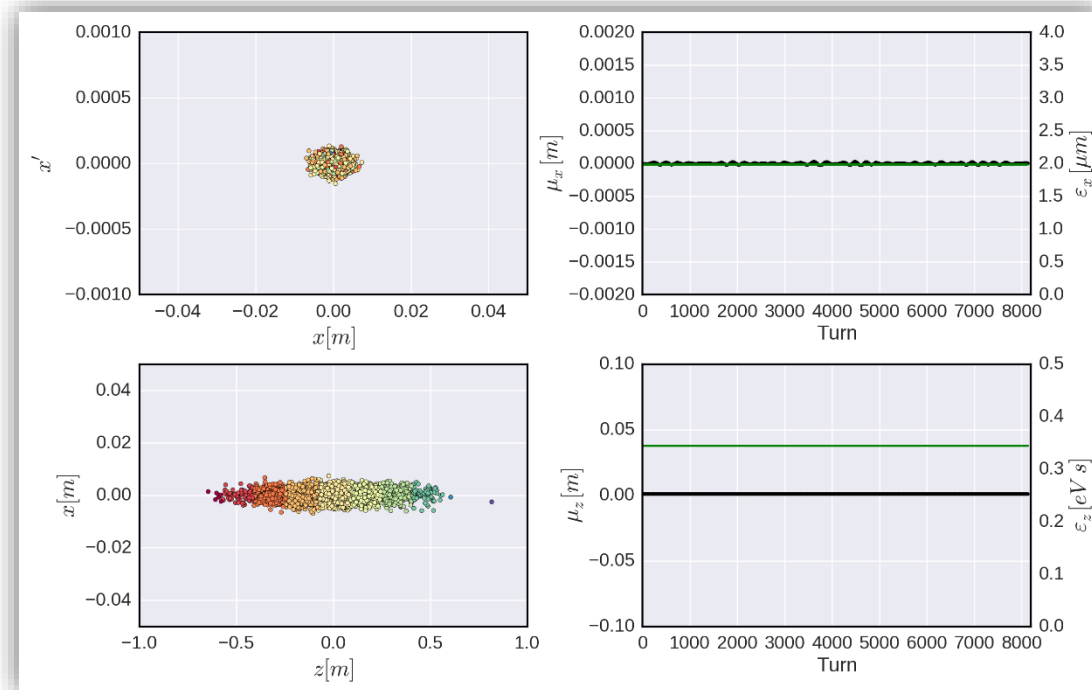


# Examples – quadrupole wakes

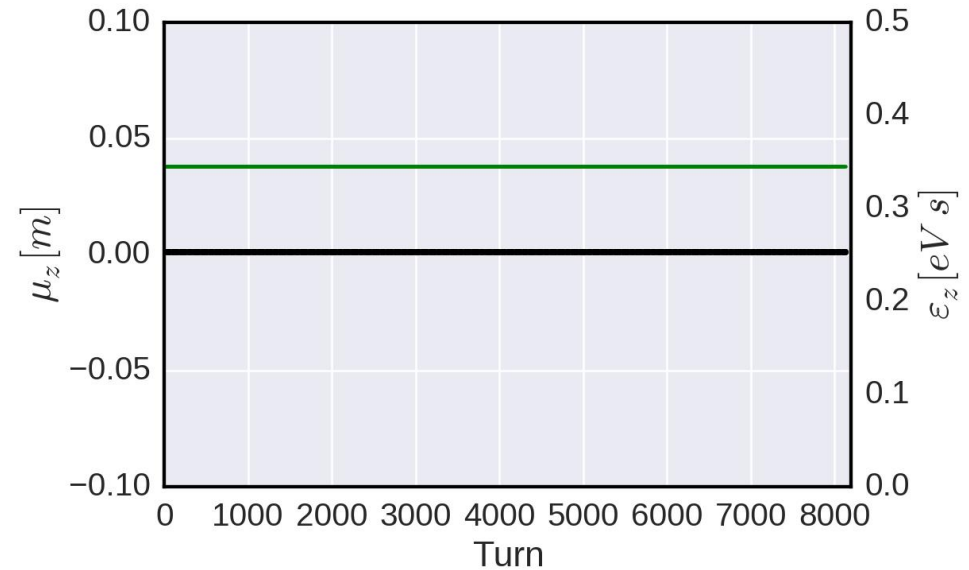
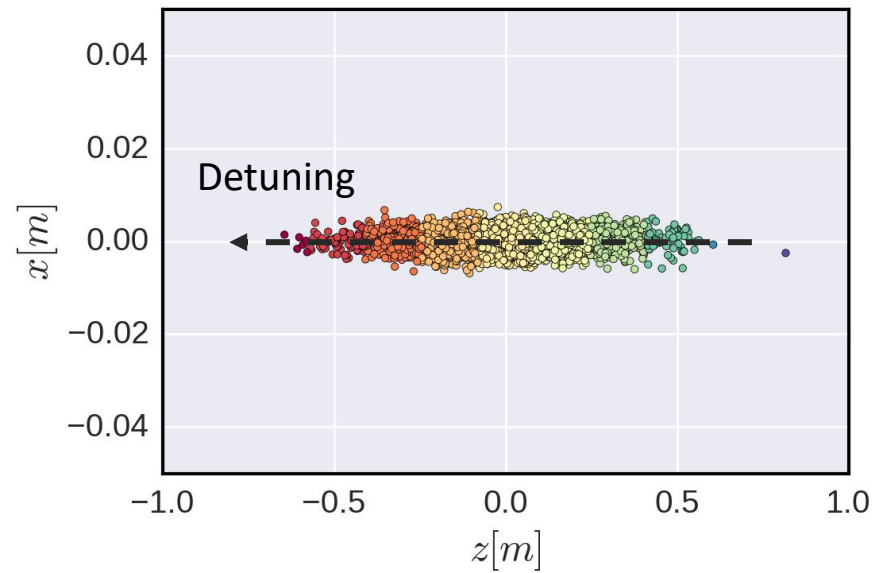
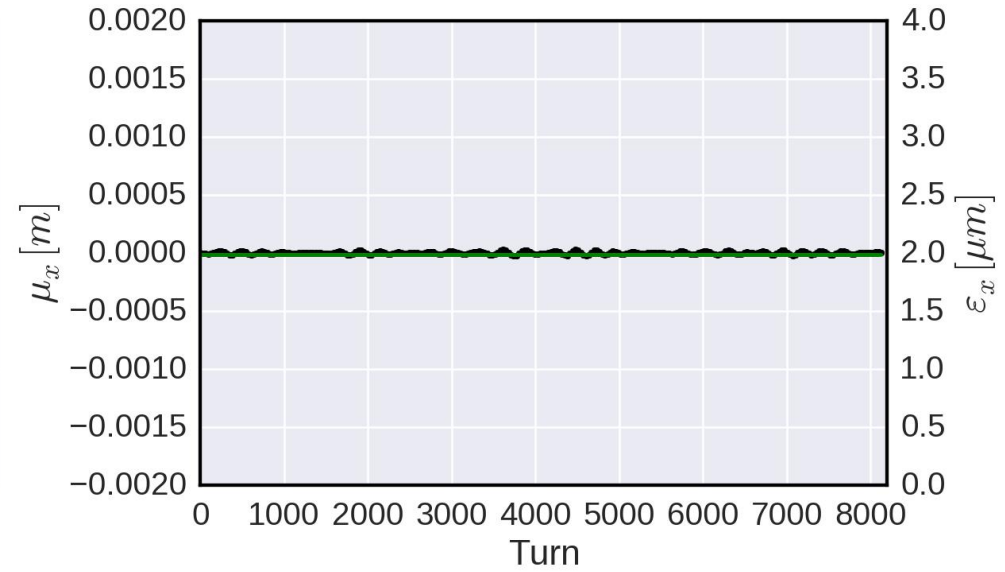
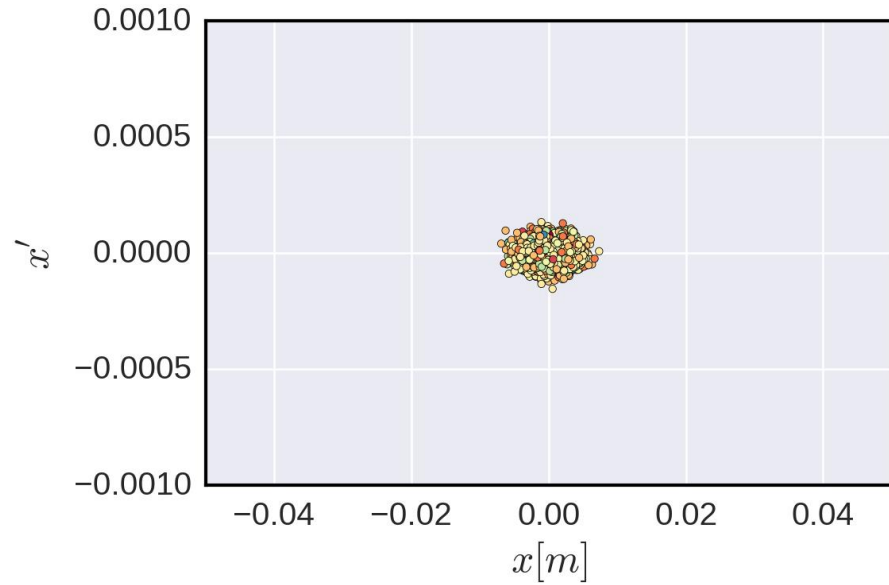
$$H = \frac{1}{2}p_x^2 + \frac{1}{2}K(s)x^2 + \frac{e^2}{m\gamma\beta^2c^2C} \boxed{x^2} \sum_{j=0}^{n\_slices-1} \boxed{\lambda(z_j) W_{02}(z - z_j) \Delta z_j}$$

Quadrupole term → tune kick

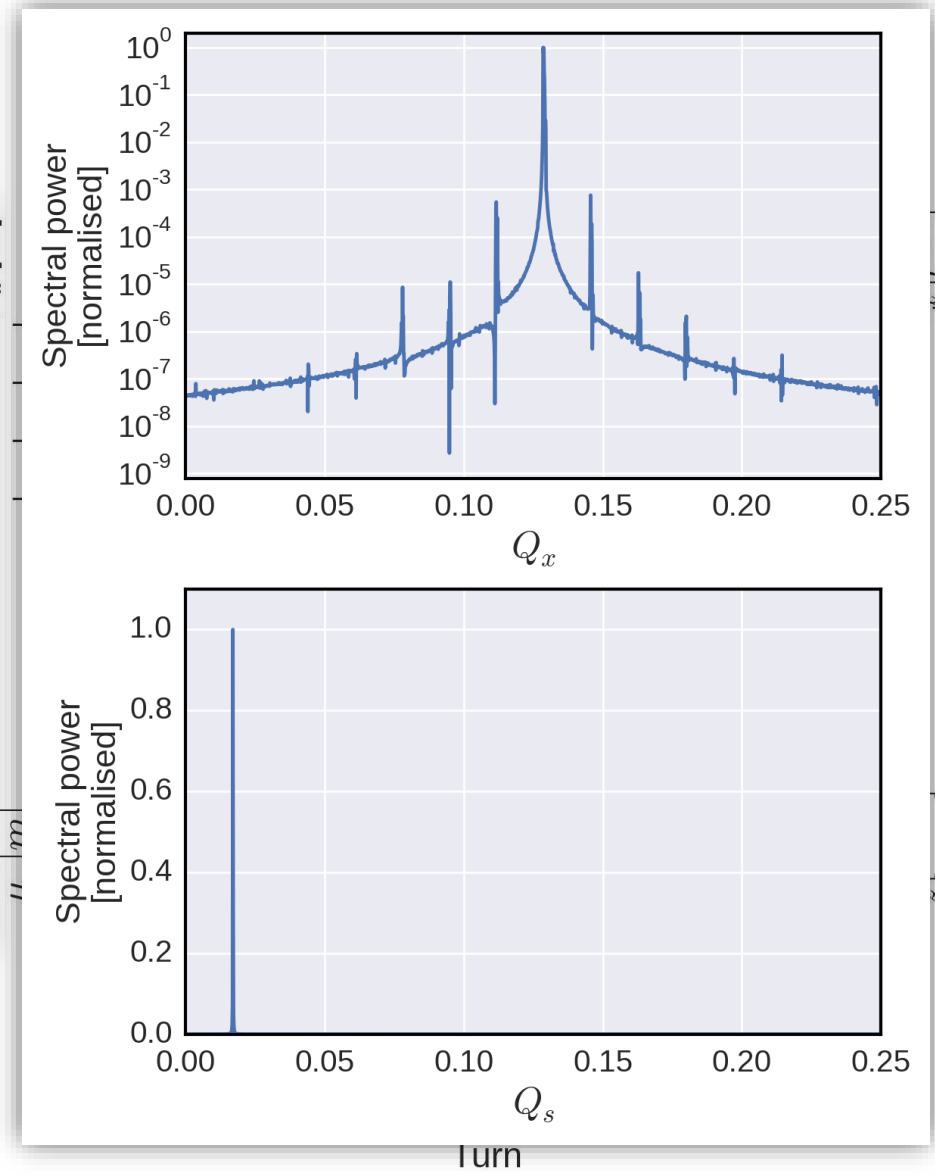
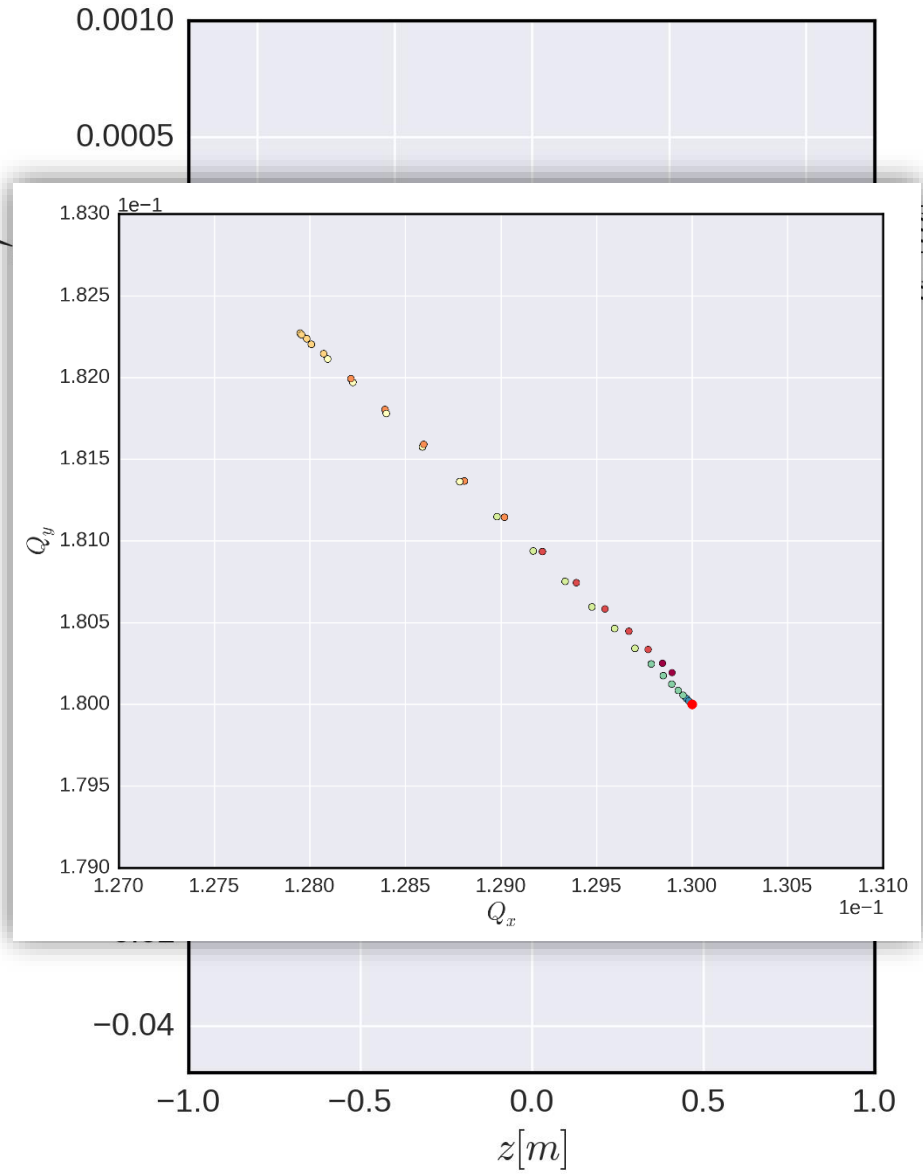
Slice dependent change of tune  
(if line density does not change)



# Examples – quadrupole wakes



# Examples – quadrupole wakes



# Examples – dipole wakes

$$H = \frac{1}{2}p_x^2 + \frac{1}{2}K(s)x^2 + \frac{e^2}{m\gamma\beta^2c^2C} x \sum_{j=0}^{n \text{ slices}-1} \lambda(z_j) \langle x \rangle_j W_{11}(z - z_j) \Delta z_j$$

Dipolar term  $\rightarrow$  orbit kick

Offset dependent orbit kick  
 $\rightarrow$  kicks can accumulate

- Without synchrotron motion:  
kicks accumulate turn after turn – the beam is unstable  $\rightarrow$  beam break-up in linacs



# Examples – dipole wakes

$$H = \frac{1}{2}p_x^2 + \frac{1}{2}K(s)x^2 + \frac{e^2}{m\gamma\beta^2c^2C} x \sum_{j=0}^{\text{slices}-1} \lambda(z_j) \langle x \rangle_j W_{11}(z - z_j) \Delta z_j$$

Dipolar term → orbit kick

With synchrotron motion we can get into a feedback loop

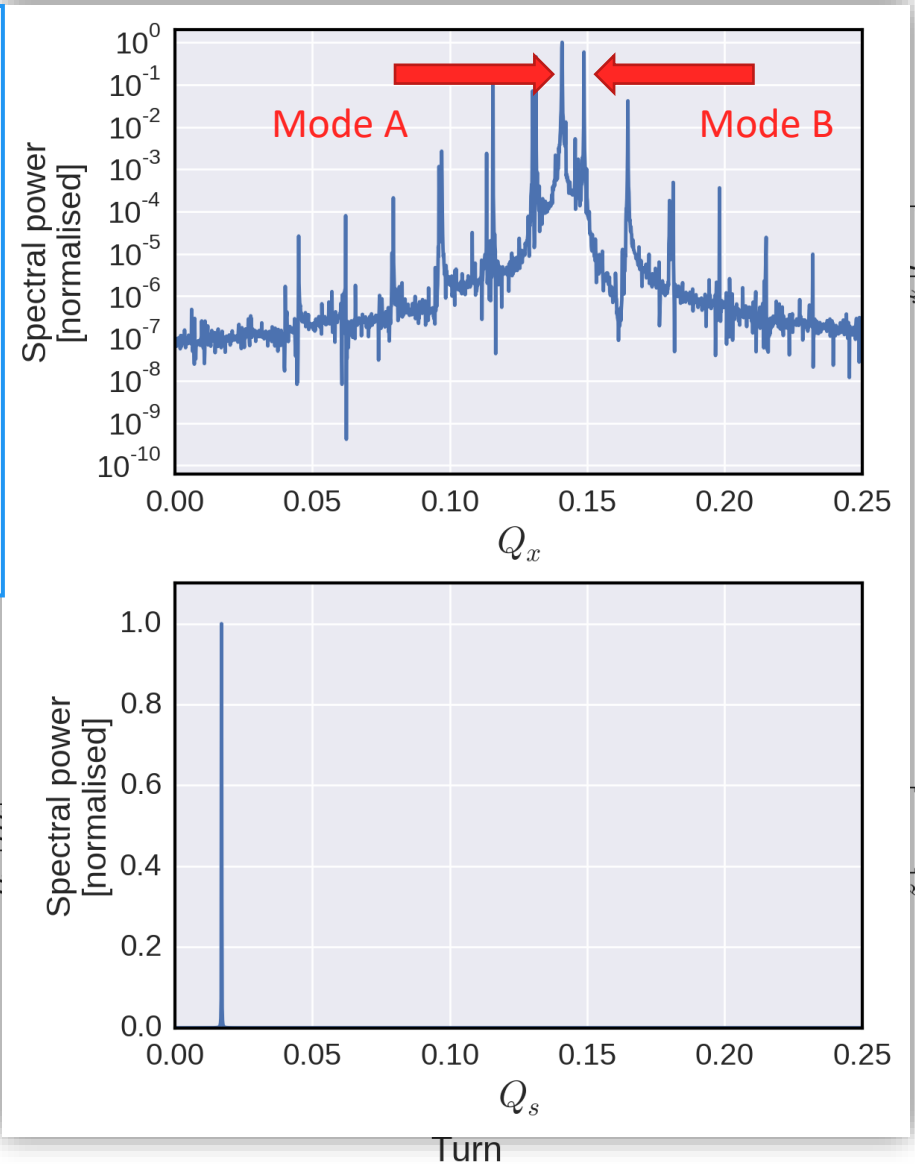
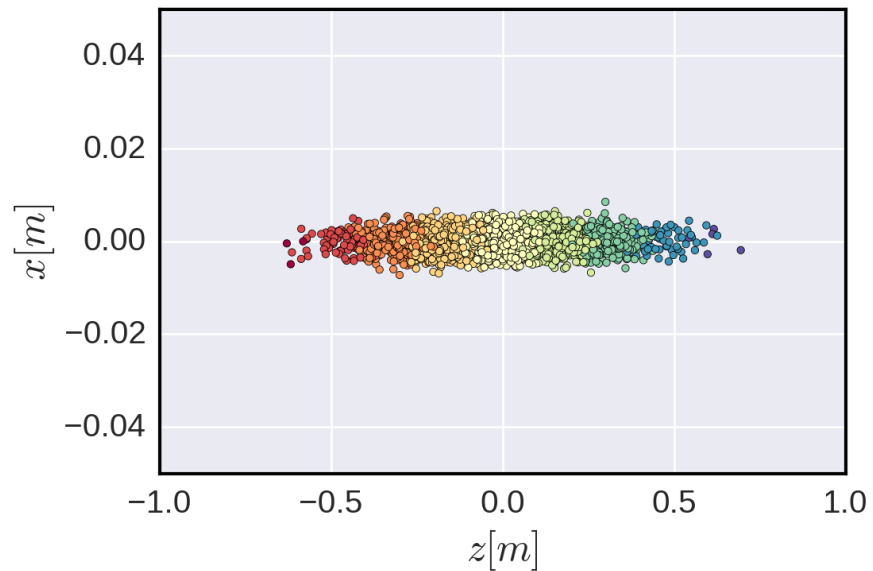
Offset dependent orbit kick → kicks can accumulate

- Without synchrotron motion:
  - kicks accumulate turn after turn – the beam is unstable → beam break-up in linacs
- With synchrotron motion:
  - Chromaticity = 0
    - Synchrotron sidebands are well separated → beam is stable
    - Synchrotron sidebands couple → (transverse) mode coupling instability
  - Chromaticity ≠ 0
    - Headtail modes → beam is unstable (can be very weak and often damped by non-linearities)

# Dipole wakes – TMCI below threshold

$x'$

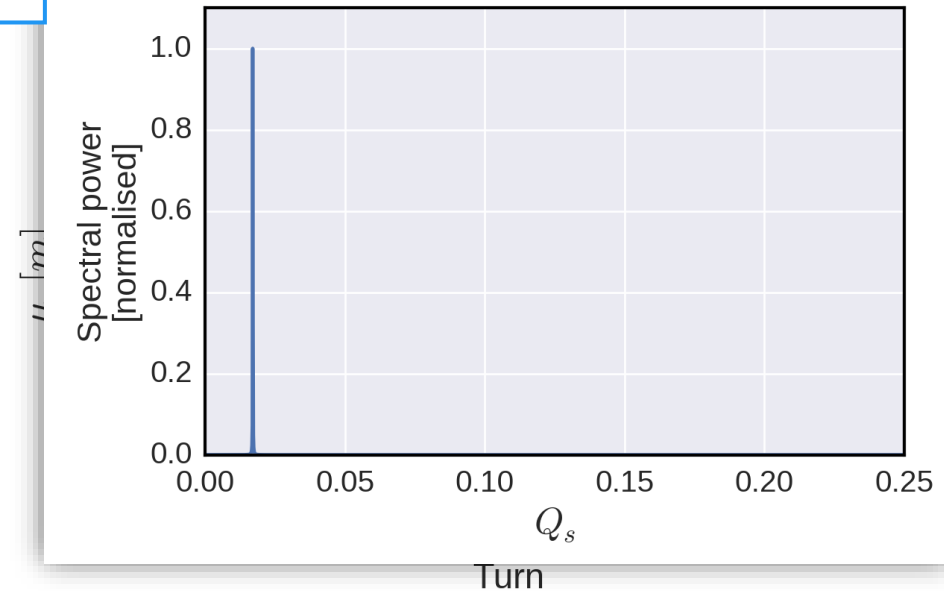
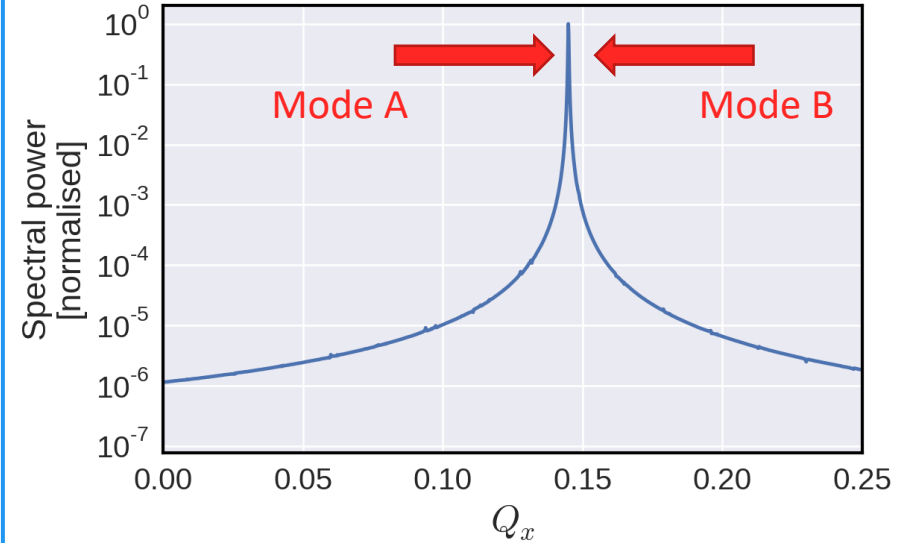
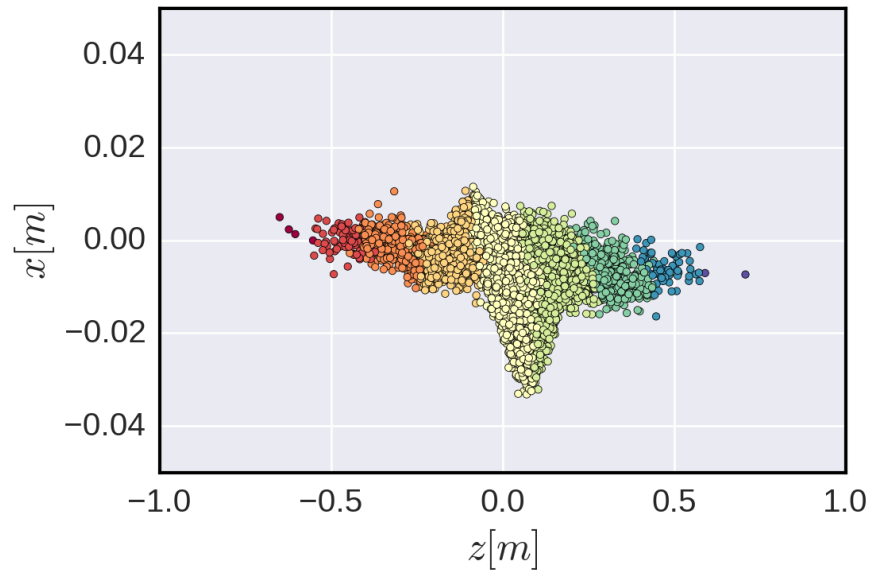
As the intensity increases the coherent modes shift – here, modes A and B are approaching each other



# Dipole wakes – TMCI above threshold

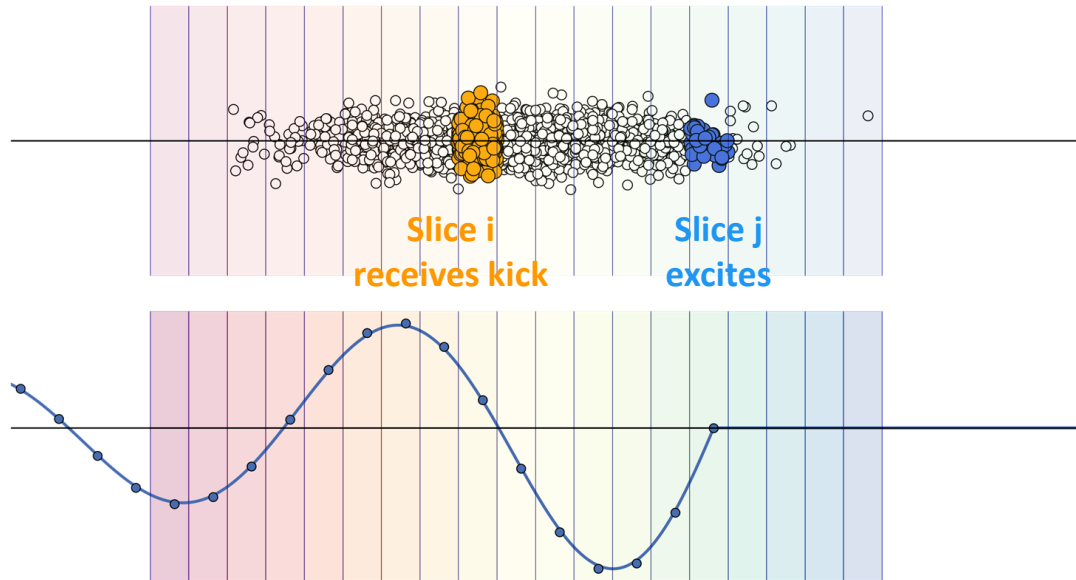
$x'$

When the two modes merge a fast coherent instability arises – the transverse mode coupling instability (TMCI) which often is a hard intensity limit in many machines



# Transverse impedance kick

- Single traversal of a bunch through an impedance source
  - Including the quadrupolar wake, kicks are different on different particles in slice i



$$\Delta x'_{ik} = -\frac{e^2}{\beta^2 E_0} \sum_{j=0}^i N[j] [W_{Cx}[(i-j)\Delta z] + \langle x \rangle[j] W_{Dx}[(i-j)\Delta z] + x_{ik} W_{Qx}[(i-j)\Delta z]]$$

With k = 1 ... # of particles in slice i

$$\Delta x' = -\frac{e^2}{\beta^2 E_0} \int \lambda(z') [W_{Cx}(z-z') + \langle x \rangle(z') W_{Dx}(z-z') + x W_{Qx}(z-z')] dz'$$