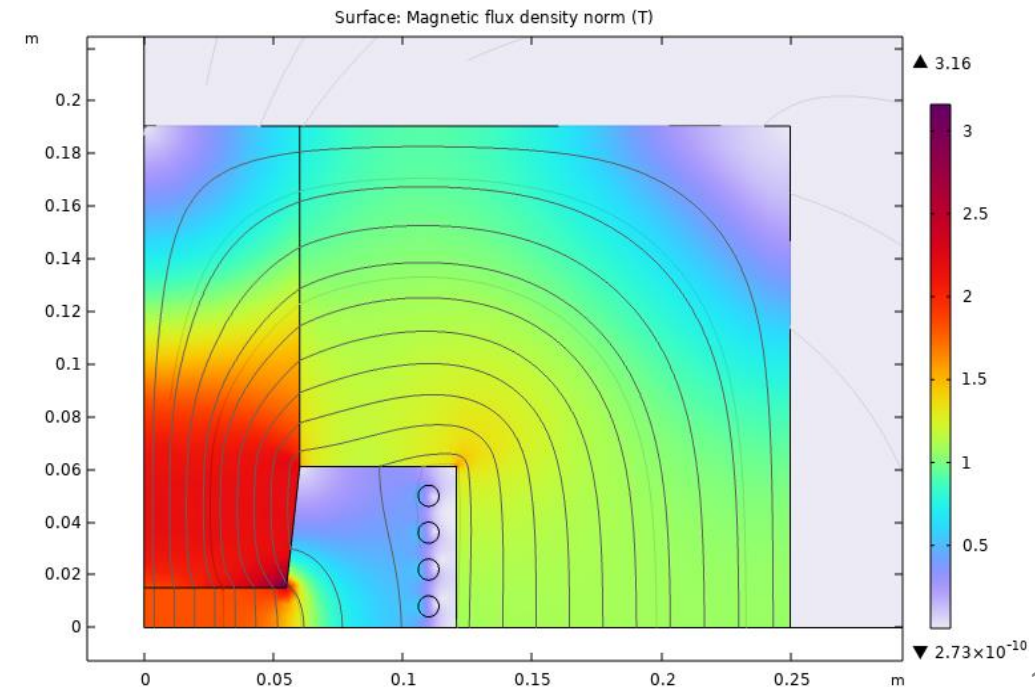


# How to reduce hysteresis loss\* in *ReBCO* based RCS super-ferric dipole magnets

\*in theory

Simon Otten, Anna Kario, Herman ten Kate

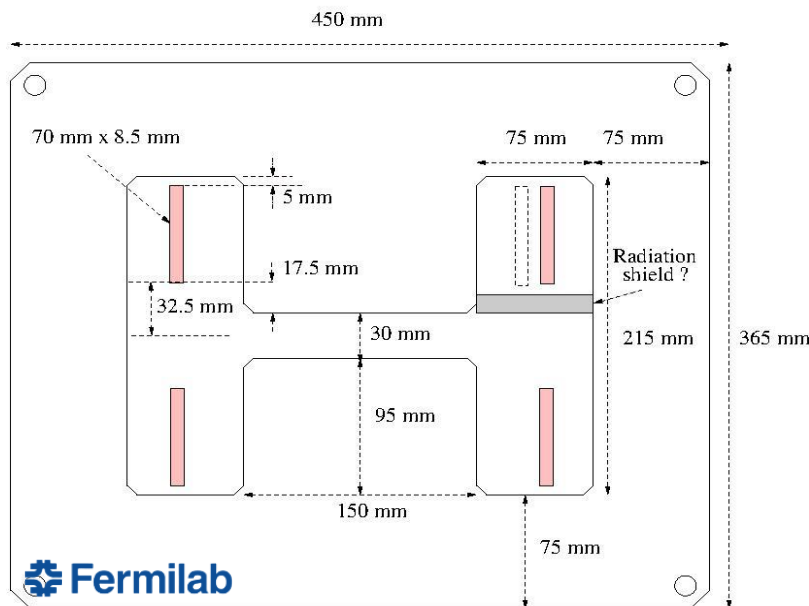
15<sup>th</sup> of May 2024



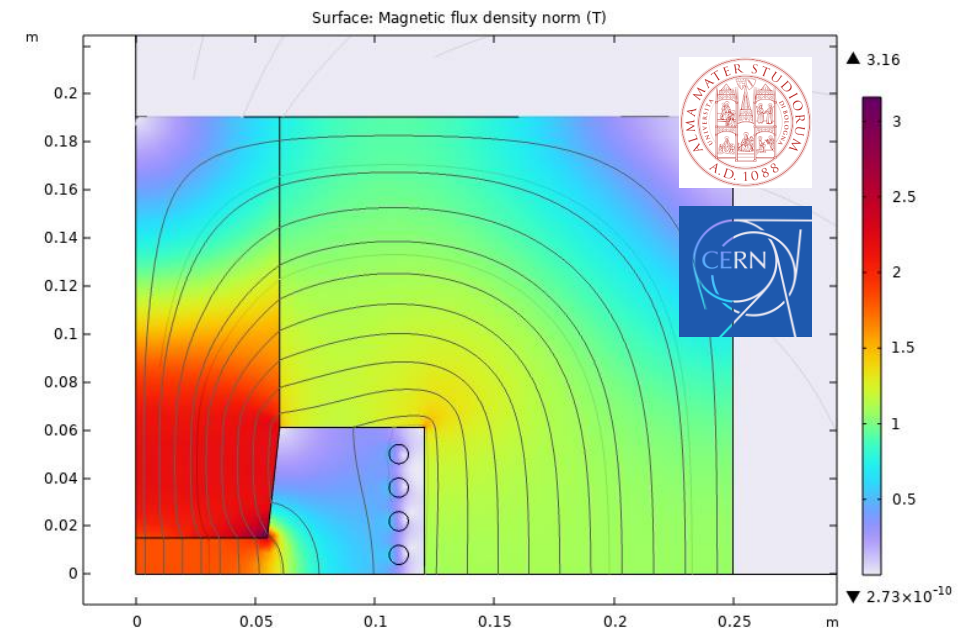
# Presented at MuCOL annual meeting

- Hysteresis loss calculations for two *ReBCO* designs for RCS fast-ramping dipoles
- Values in the range 200-500 W/m-magnet at 15-40 K found, but heat is deposited at cold!
- Is it acceptable? How to reduce it?

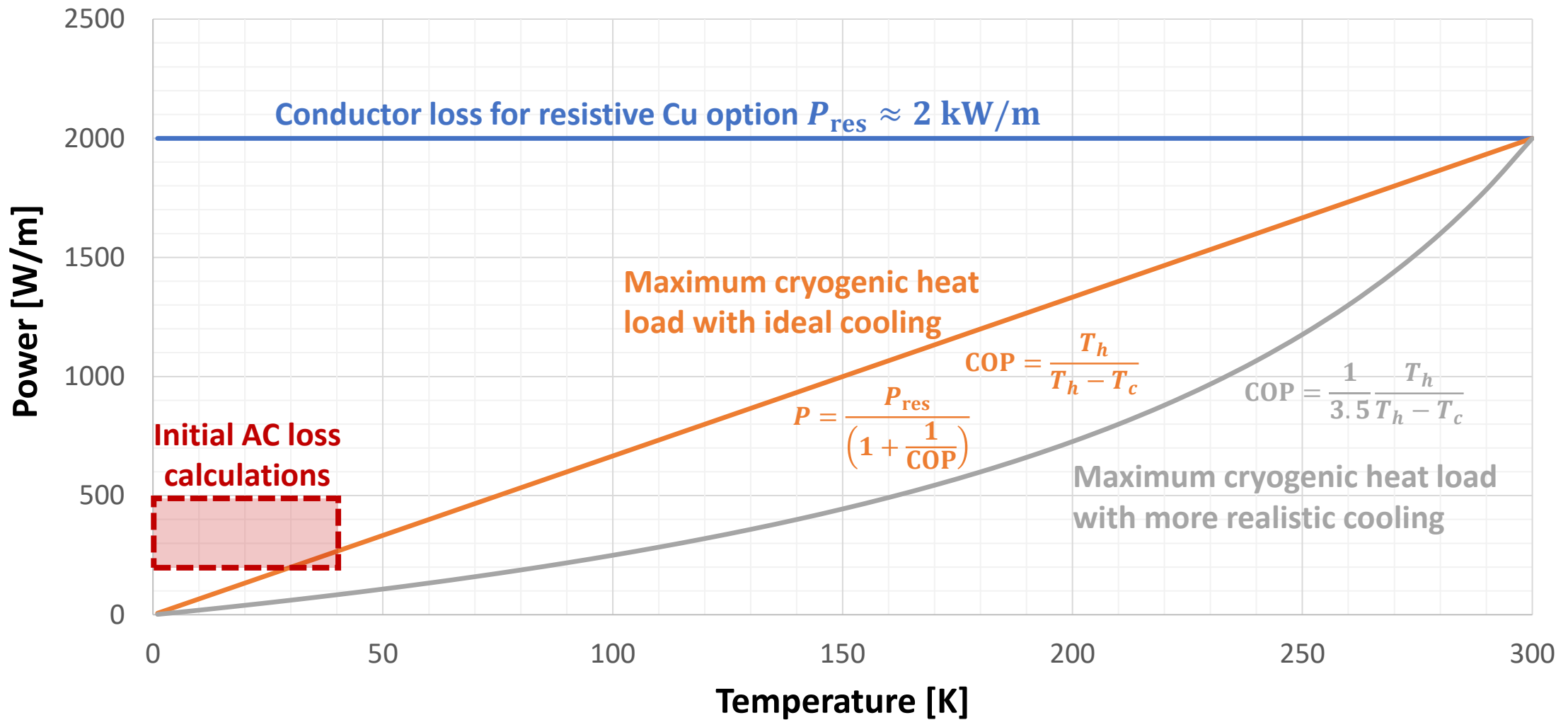
## 1. *ReBCO* magnet by FNAL (H. Piekarz et al.)



## 2. *ReBCO* magnet using Unibo/CERN yoke design (Breschi et al.)



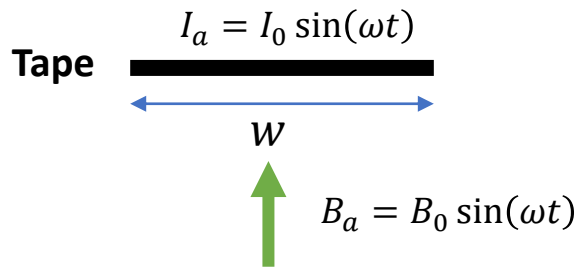
# What level of AC loss acceptable for energy saving?



- Hysteresis AC loss has to be reduced by an order of magnitude at least.

# Hysteresis loss in a single tape

Tape with width  $w$  exposed to applied current and magnetic field

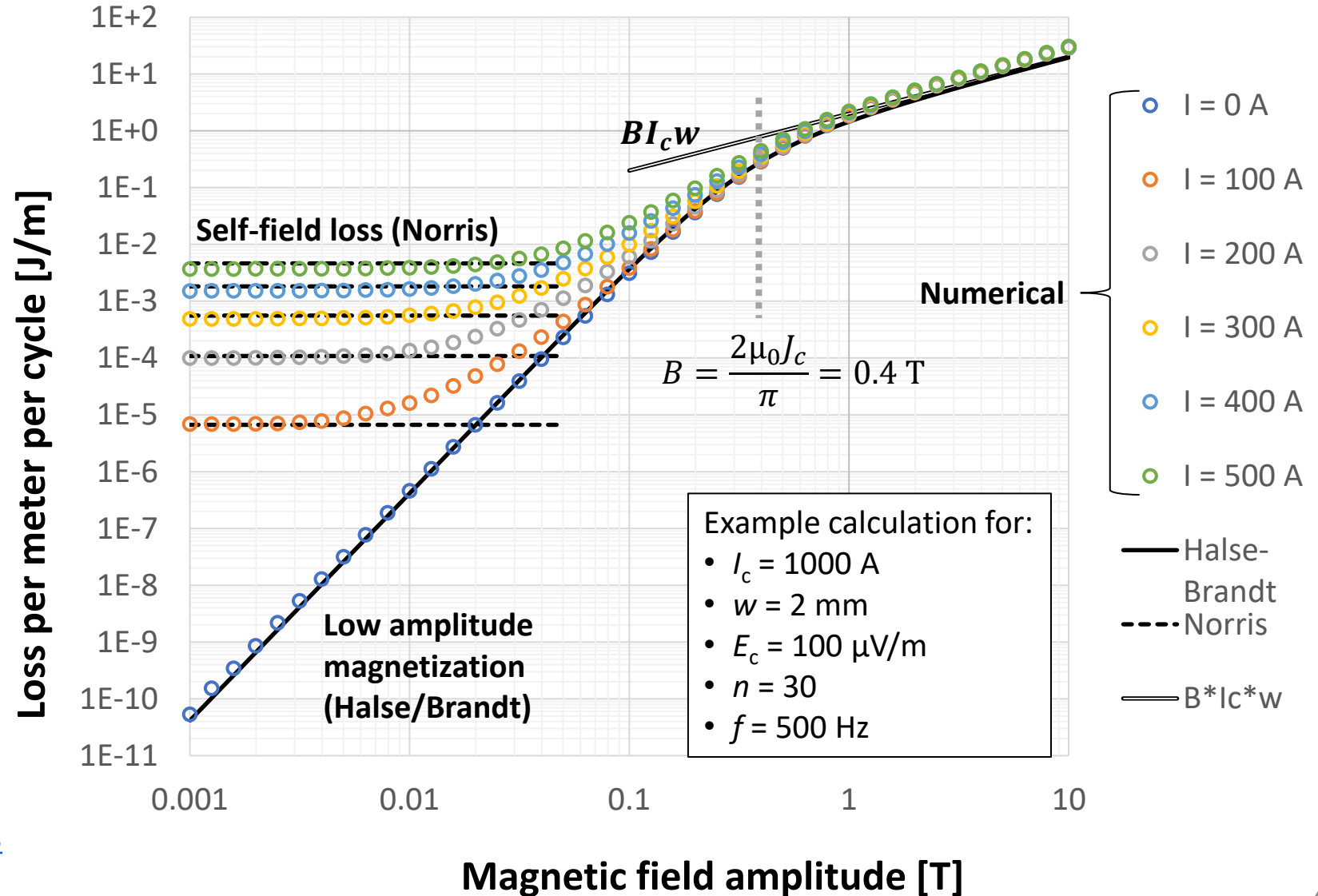


Halse-Brandt magnetization loss

$$Q = \frac{2\mu_0 J_c^2 w^2}{\pi} \left( \ln \left( \cosh \left( \frac{\pi B_0}{\mu_0 J_c} \right) \right) - \frac{\pi B_0}{2\mu_0 J_c} \tanh \left( \frac{\pi B_0}{\mu_0 J_c} \right) \right)$$

Norris self-field transport loss

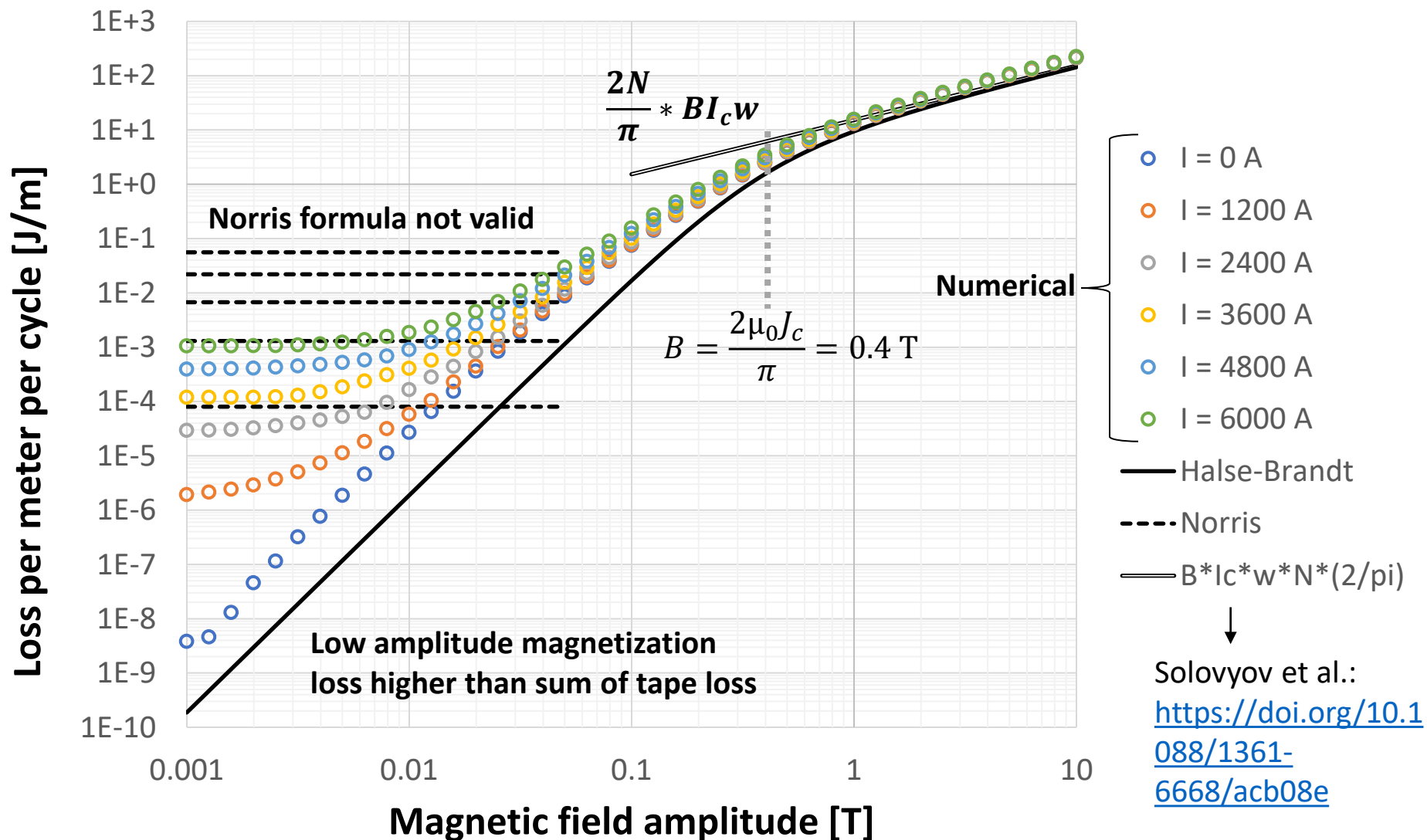
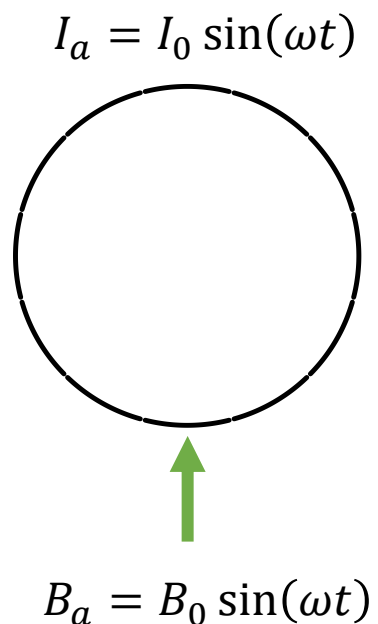
$$Q = \frac{\mu_0 I_c^2}{\pi} \left( \left( 1 - \frac{I_0}{I_c} \right) \ln \left( 1 - \frac{I_0}{I_c} \right) + \left( 1 + \frac{I_0}{I_c} \right) \ln \left( 1 + \frac{I_0}{I_c} \right) - \left( \frac{I_0}{I_c} \right)^2 \right)$$



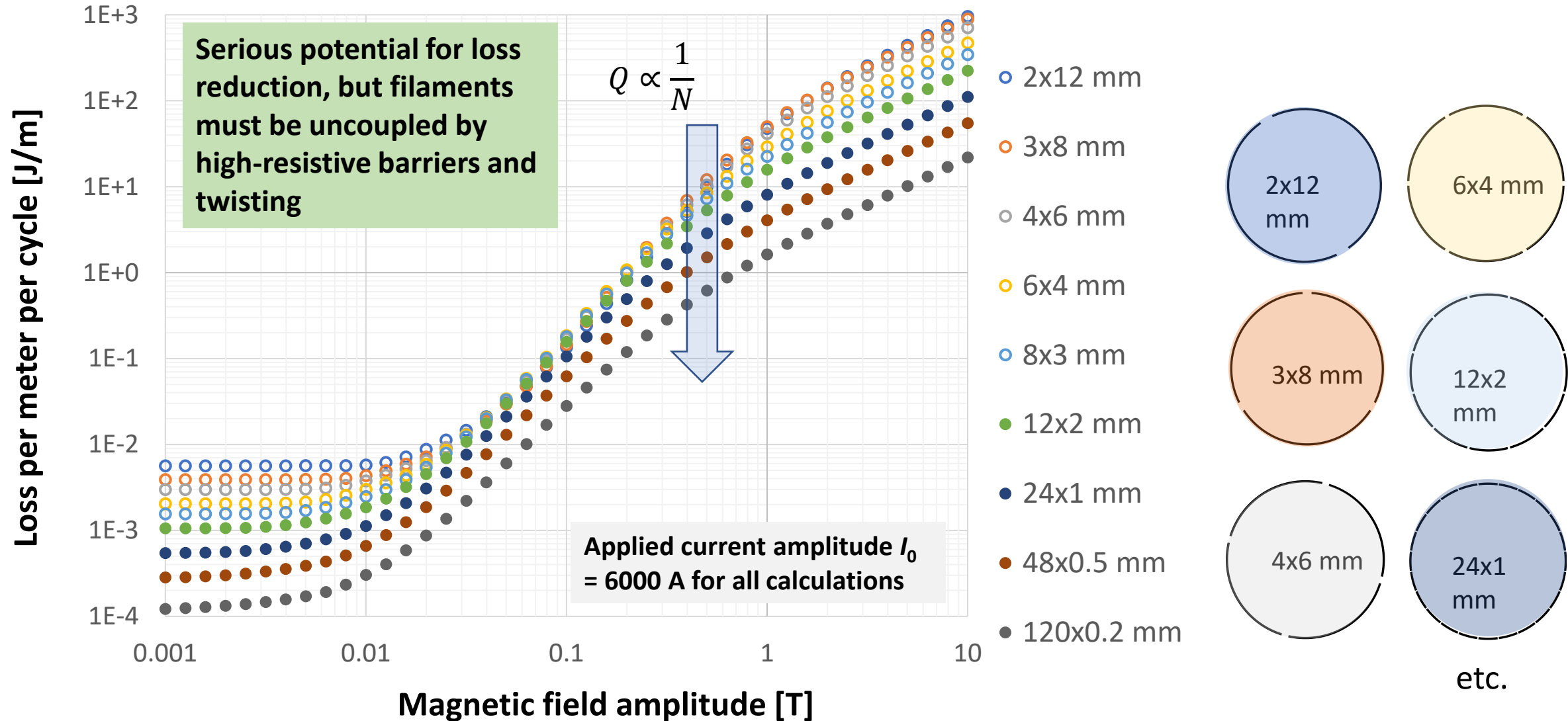
Halse: <https://doi.org/10.1088/0022-3727/3/5/310>  
 Brandt: <https://doi.org/10.1103/PhysRevB.48.12893>  
 Norris: <https://doi.org/10.1088/0022-3727/3/4/308>

# Hysteresis loss of a single round sub-cable

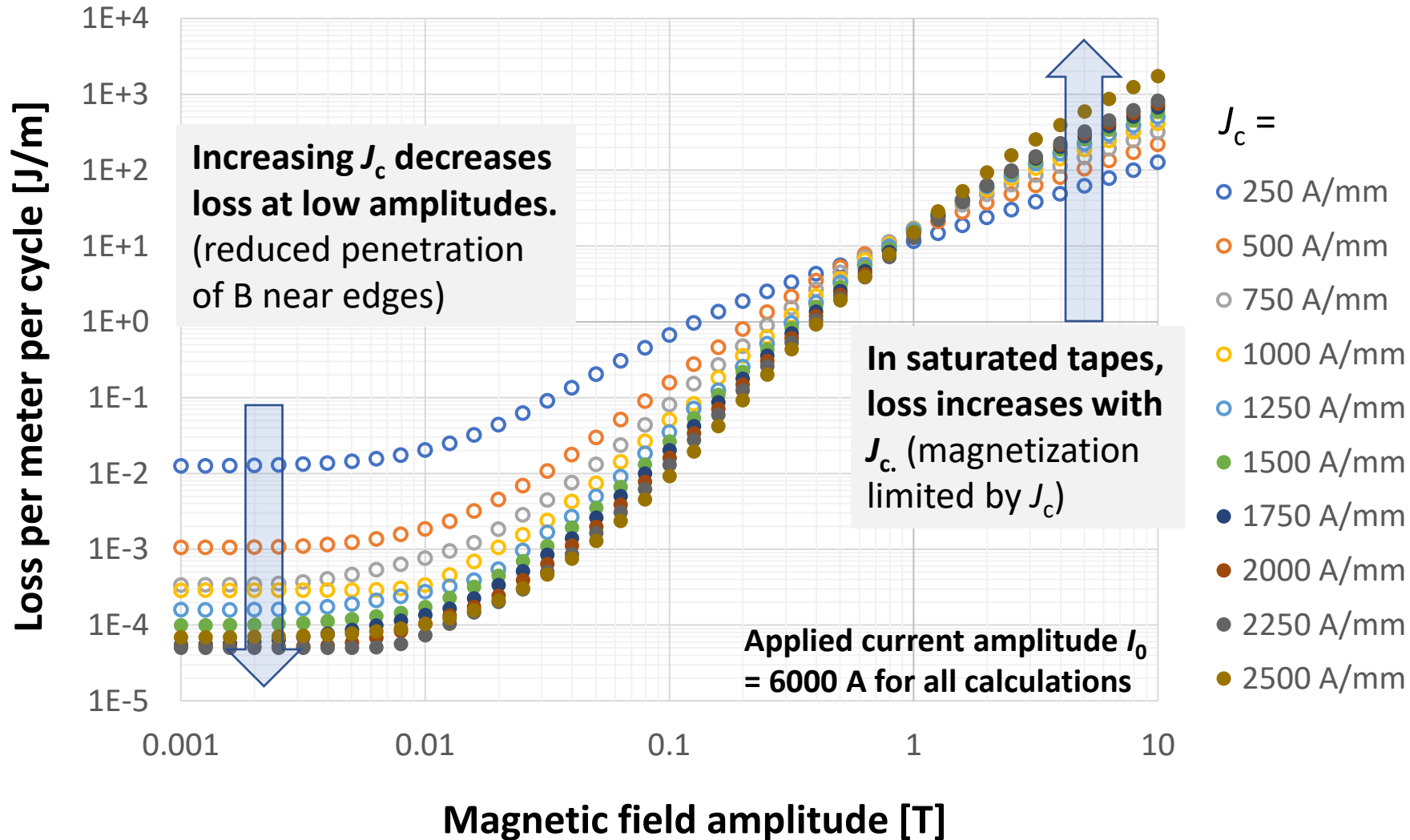
Circular cable of 12 2-mm-wide tapes on an 8 mm diameter core



# Effect of tape width/filamentization

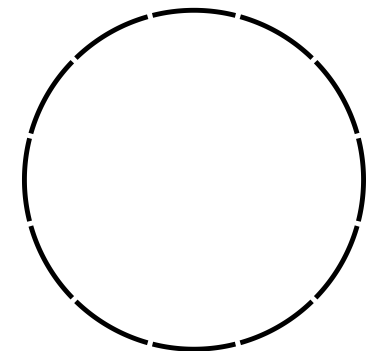


# Effect of critical current density (12x 2 mm tapes)



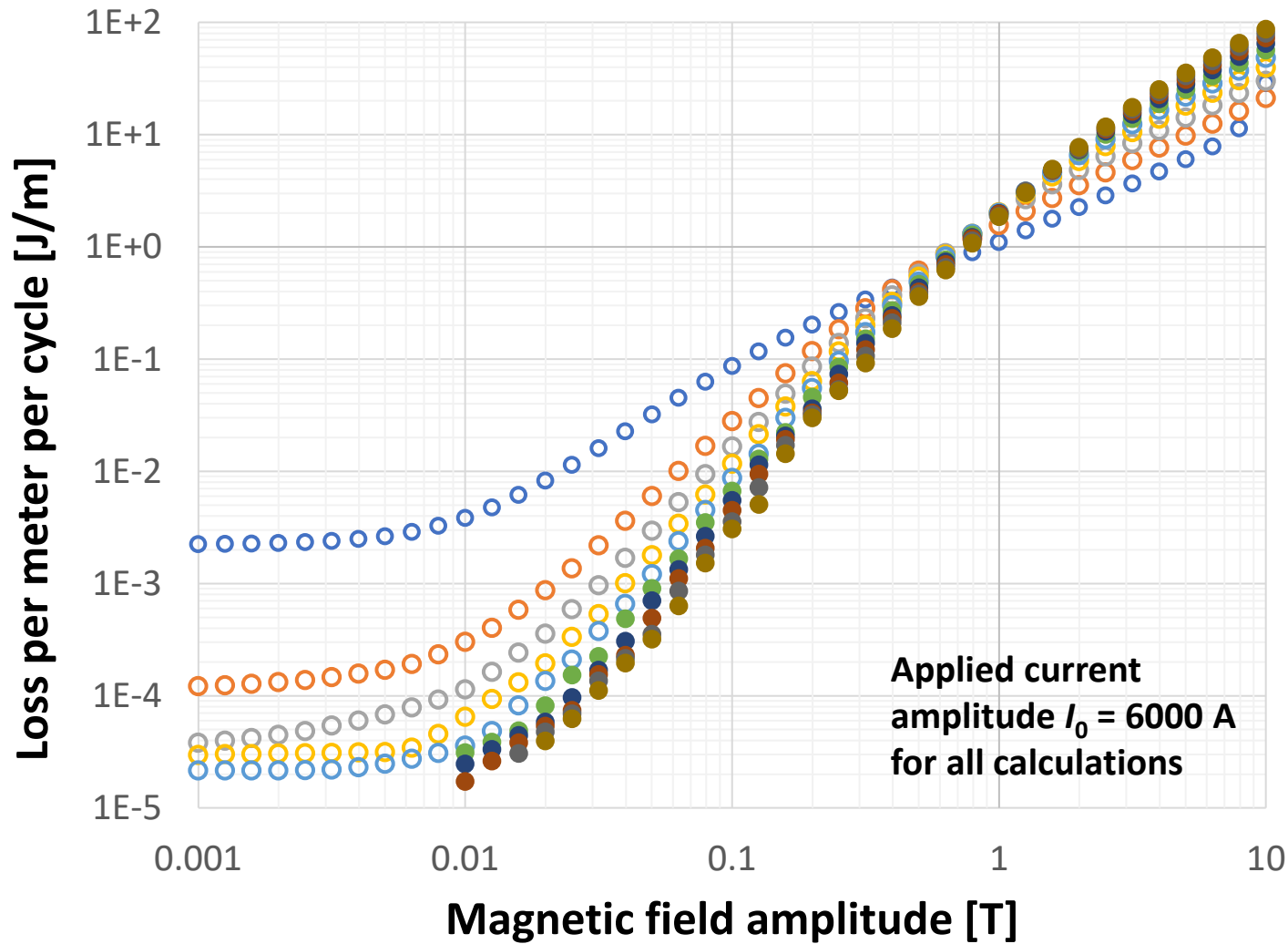
**Circular cable of 12 tapes with 2 mm width, on 8 mm diameter core**

$$I_a = I_0 \sin(\omega t)$$

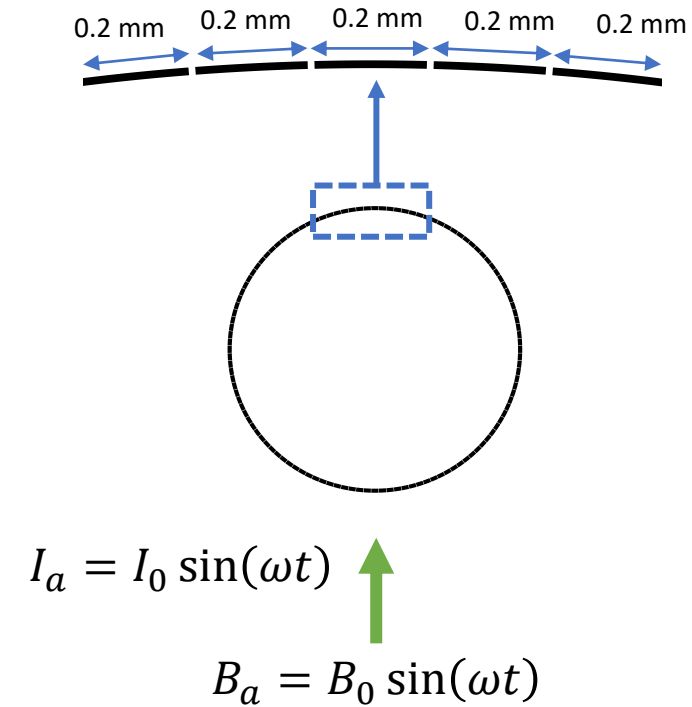


$$B_a = B_0 \sin(\omega t)$$

# Effect of critical current density (120x0.2 mm)

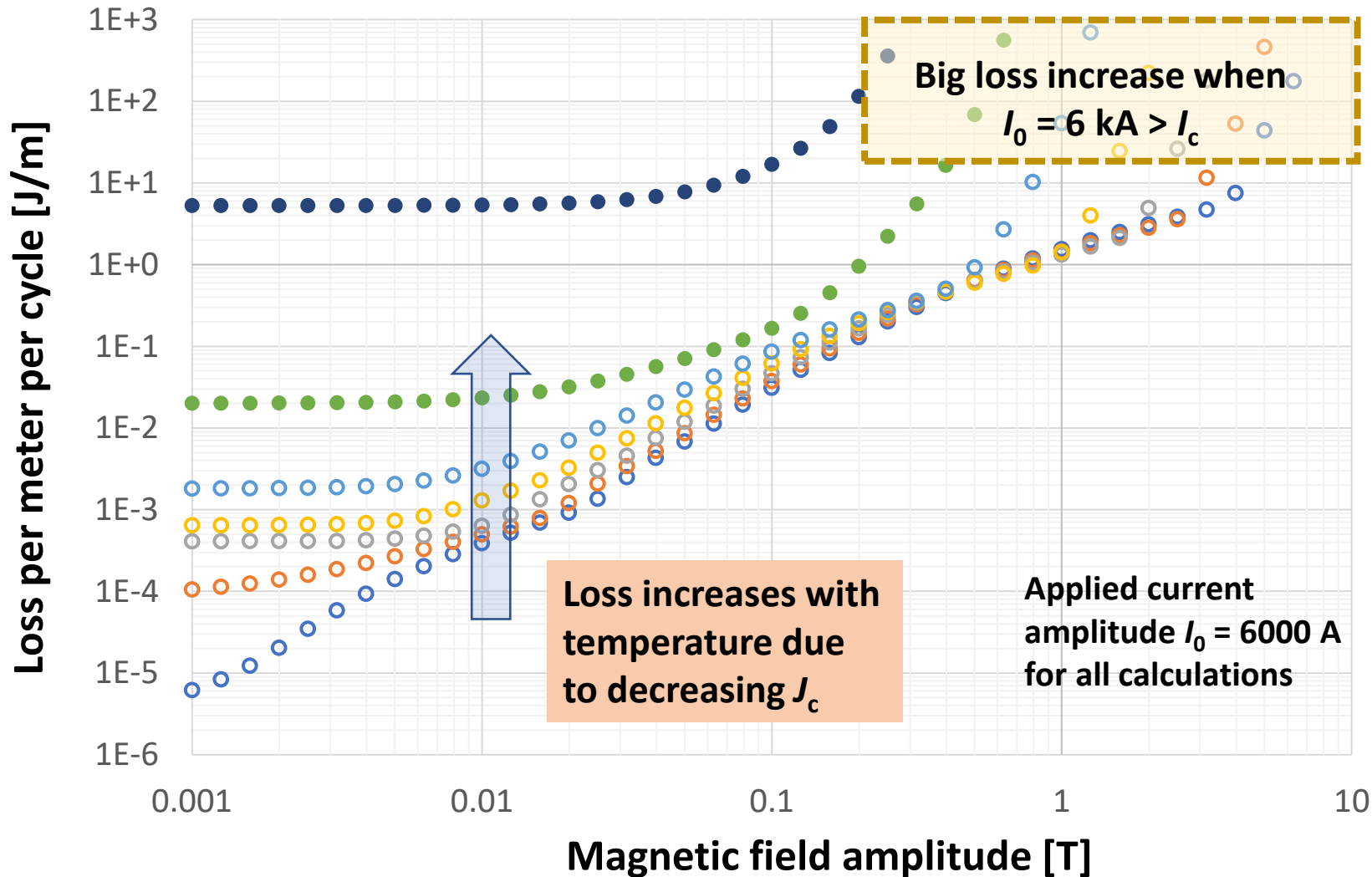


Circular cable of 120 tapes/filaments with 0.2 mm width on 8 mm diameter core





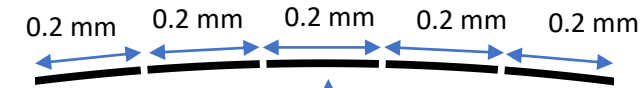
# Effect of operating temperature



Circular cable of 120 tapes/filaments with 0.2 mm width on 8 mm diameter core

$T =$

- 15 K
- 20 K
- 25 K
- 30 K
- 35 K
- 40 K
- 45 K



$$I_a = I_0 \sin(\omega t)$$

$$B_a = B_0 \sin(\omega t)$$

- Used measured  $J_c(\mathbf{B}, T)$  data for SuperPower tape from Robinson Research Institute <https://htsdb.wimbush.eu/dataset/4256624>

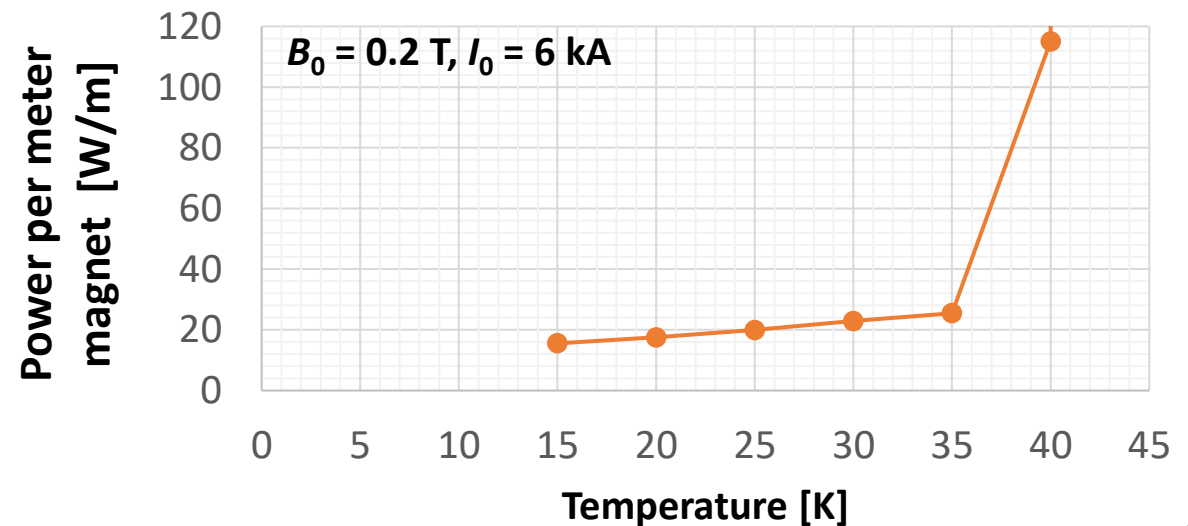
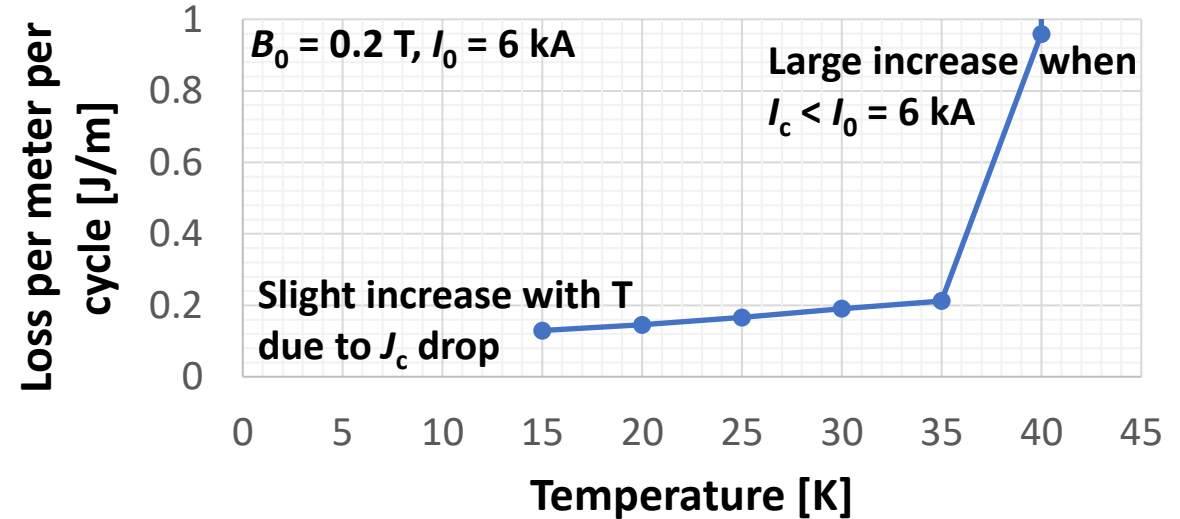
# Extrapolation to a full *ReBCO* based RCS fast-ramping dipole magnet

Case:

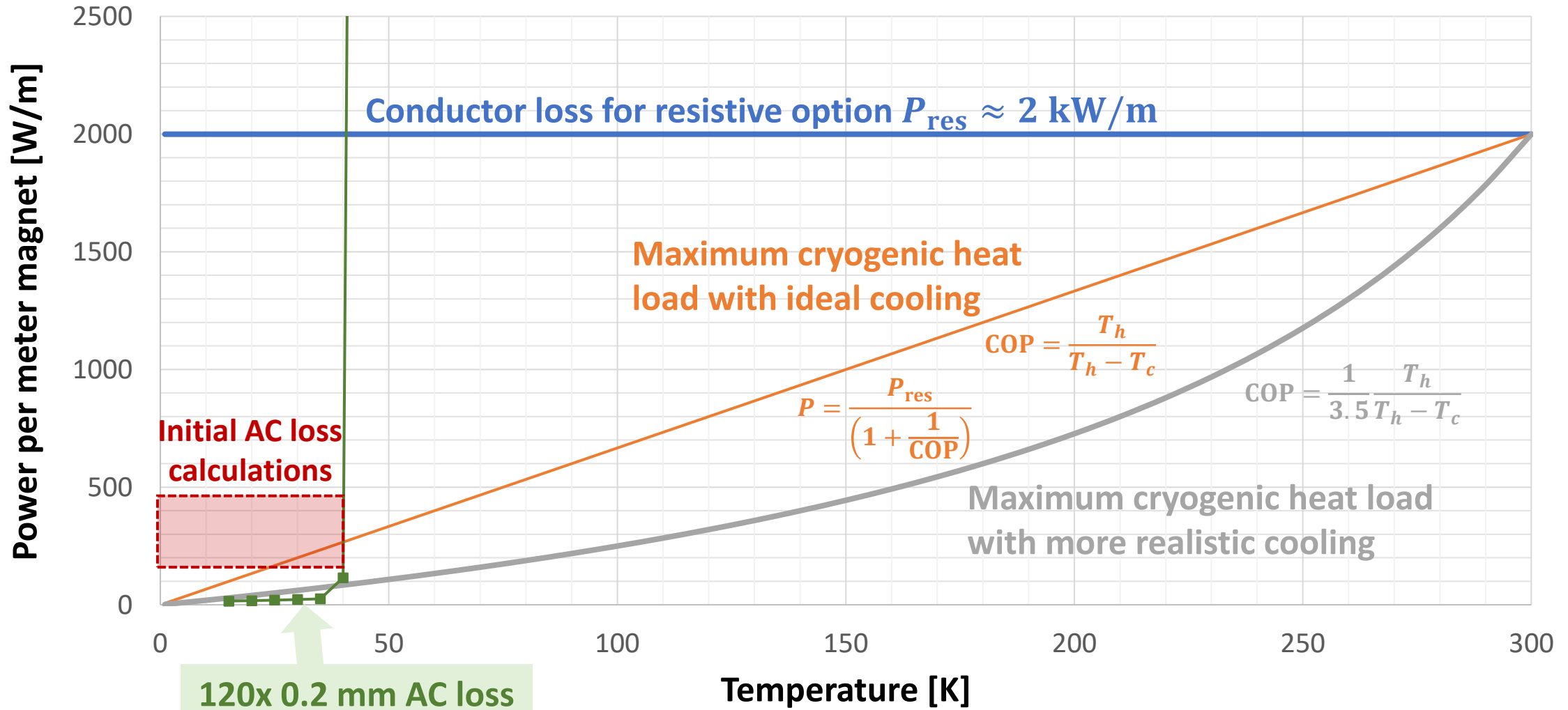
- $J_c(\mathbf{B}, T)$  of SuperPower tape (RI data)
- Layout 120 tape/filaments, 0.2 mm wide
- Applied current 6 kA, applied field 0.2 T
- Loss/cycle per sub-cable 0.1-0.2 J for  $T < 35$  K

Full magnet power:

- Multiply with number of sub-cables in the cross-section (24) and 5 Hz repetition rate
- This value is conservative as not all turns experience 0.2 T
- **Achieving 15 to 25 W in 15 to 30 K range**



# What level of AC loss acceptable for energy saving?



- 120x 0.2 mm layout yields AC loss below maximum cryogenic heat load for  $15 \text{ K} < T < 35 \text{ K}$  !

# Conclusion & outlook

- We calculated hysteresis loss by analytical and numerical methods. There will be other contributions to the cryogenic heat load: coupling loss, eddy current loss, heat leaks, etc.
- Hysteresis loss strongly increases with perpendicular field, to be minimized through optimal conductor placement and yoke design
- Further reduction by reducing tape width and/or use filamented conductors as  $Q \propto 1/N$
- Hysteresis loss *decreases* with increasing  $J_c$  for low field amplitudes and *increases* with increasing  $J_c$  for high amplitudes of magnetic field
- Case presented: round conductor with 120 filaments, 0.2 mm wide yields < 30 W hysteresis loss showing potential for saving energy compared to the resistive option

