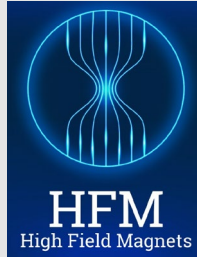


PAUL SCHERRER INSTITUT



D. Araujo, B. Auchmann, A. Brem, T. Michlmayr, C. Müller and A. Haziot :: Paul Scherrer Institute

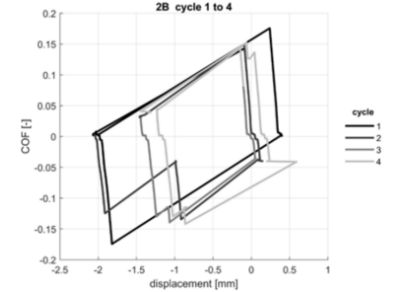
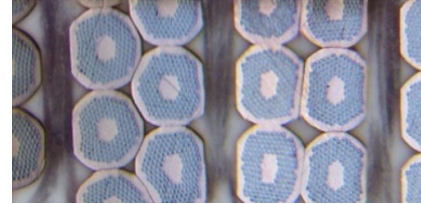
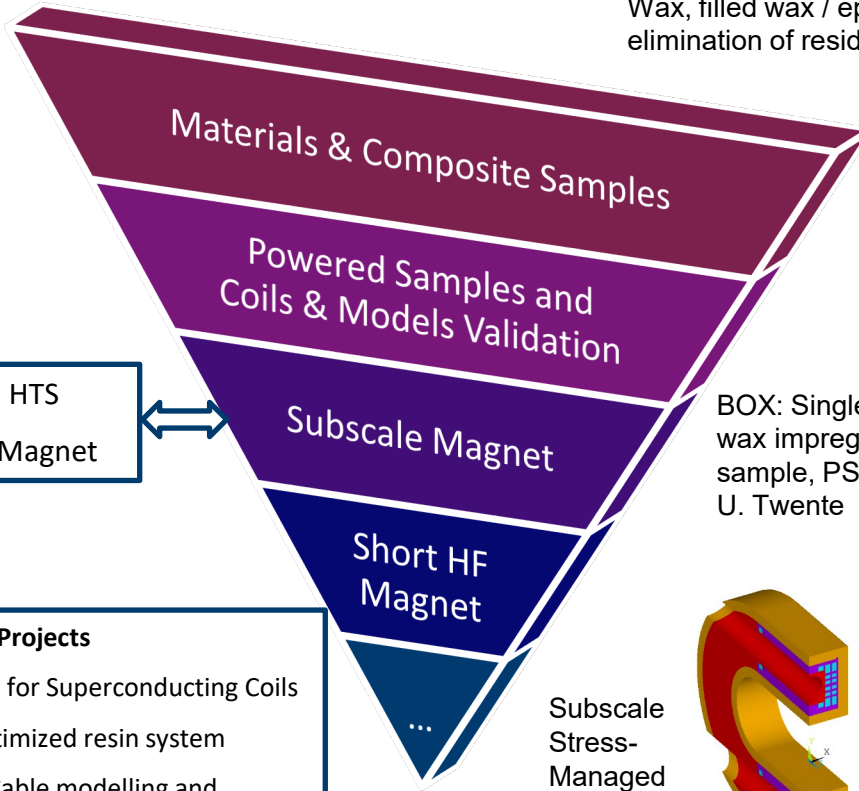
# Status of Subscale Stress-Managed Common-Coils Manufacturing and on the SMACC conceptual design

HFM Forum

Work supported by the Swiss State Secretariat for Education, Research and Innovation SERI.  
This work was performed under the auspices and with support from the Swiss Accelerator Research and Technology (CHART) program

# LTS and Hybrid LTS/HTS Roadmap

Wax, filled wax / epoxy process development, HT elimination of residues and sliding interfaces, A. Brem

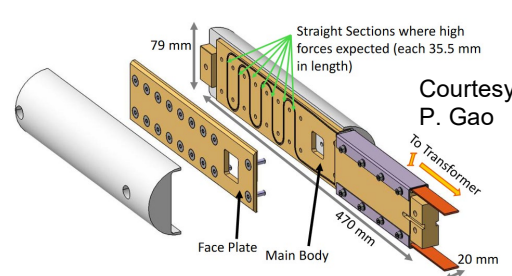


Hybrid HTS  
Subscale Magnet

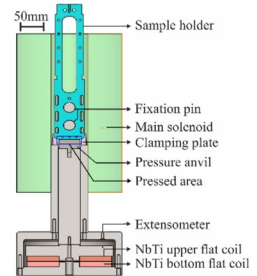


Subscale Magnet

BOX: Single-turn wax impregnated sample, PSI & U. Twente

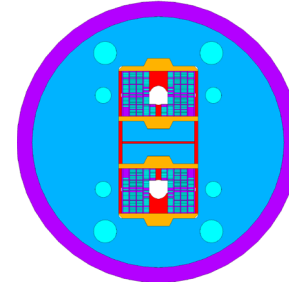
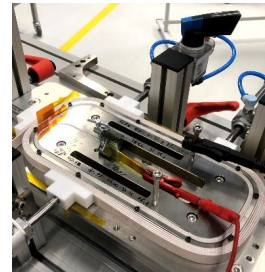
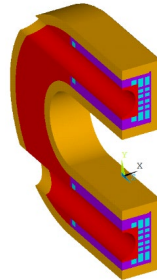


Courtesy P. Gao



- CHART Mag Projects**
- MagAM:** AM for Superconducting Coils
  - MagRes:** Optimized resin system
  - MagComp:** Cable modelling and characterization
  - MagNum:** Modelling & Optimization

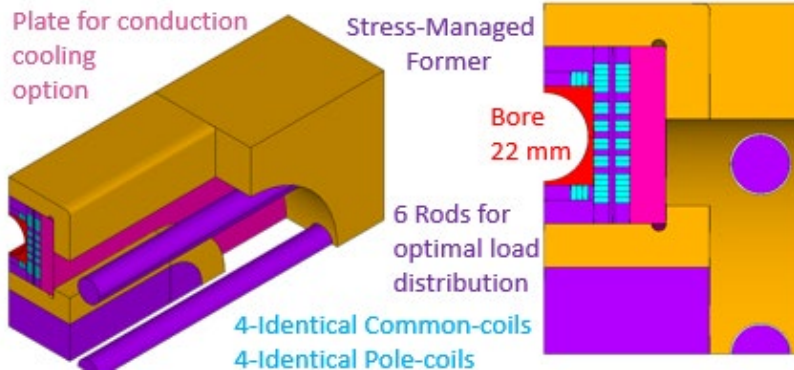
Subscale Stress-Managed Common-coils



Stress-Managed Asymmetric Common Coils

# Subscale LTS ( $\text{Nb}_3\text{Sn}$ ) Magnet

- Validating **manufacturing process** and introducing advanced concepts: **coil pre-load free**, at room temperature; stress-management structure and **splicing on the low-field region**.
- Fast turn-around platform for testing matrix systems; protection concepts and cooling options.
- Hybrid magnet with LTS ( $\text{Nb}_3\text{Sn}$ ) Common-Coils and HTS racetracks
- LTS ( $\text{Nb}_3\text{Sn}$ ) conductor manufactured by LBNL (cct subscale cable)



Magnet parameters for testing all coils or the common-coils. The coils straight section is 150 mm. The values refer to the fitted wire  $I_c$  curve at 4.2 K values.

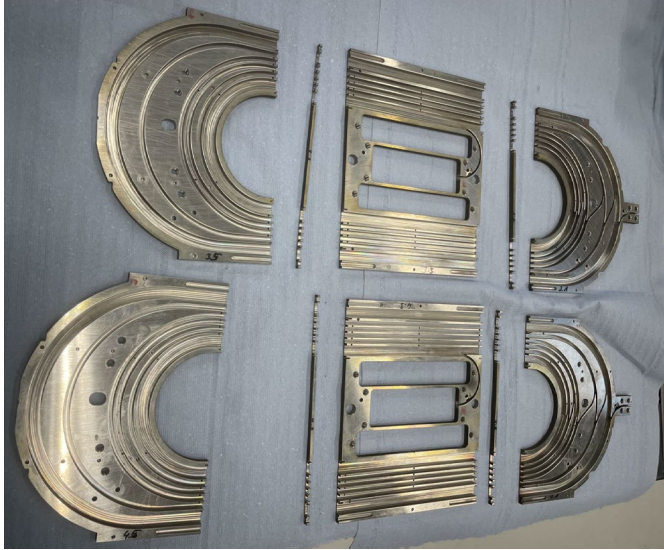
Parameter	All coils	CCs
$B_{0_{ss}}$ in T	5.15	5.1
$B_{peak_{ss}}$ in T	6.45	6.3
$I_{ss}$ in kA	8.25	9.2
$E_{mag_{ss}}$ in kJ	15.2	16.4



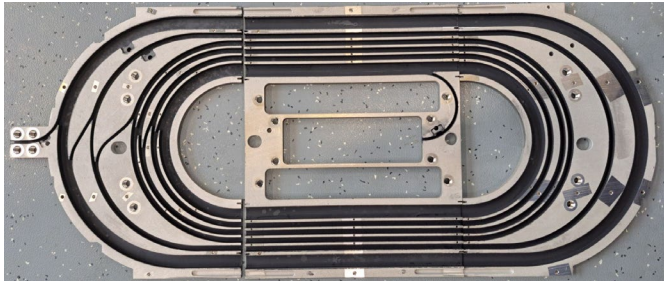
# Subscale – Former preparation



5 pieces  
former



Dip  
coating



Ceramic  
glazing

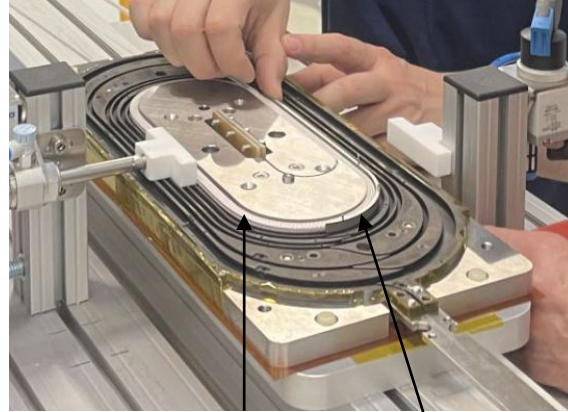
# Subscale – Winding

spool



former

Rotating beam



After 1<sup>st</sup> coil block

rib



Before pushing down



After pushing down



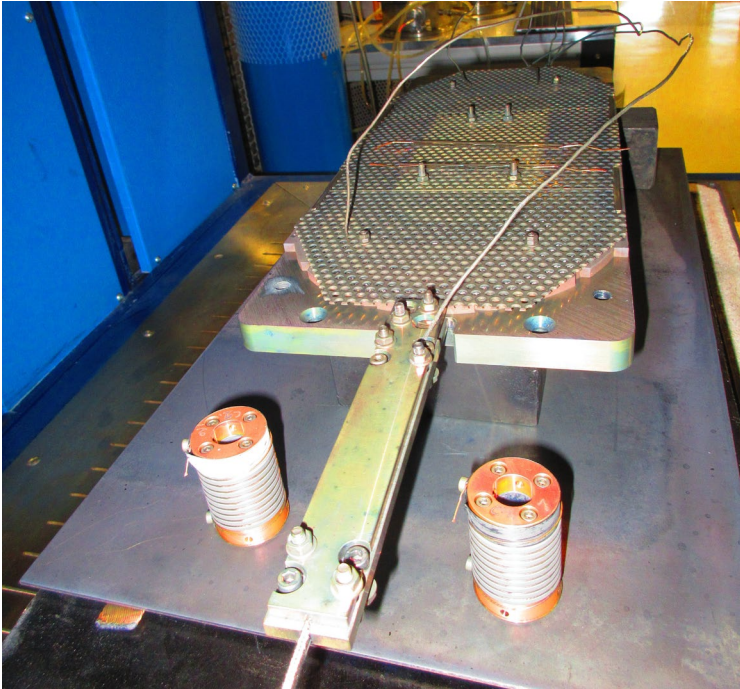
# Subscale – Winding: not proud of...



Re-machining former holes during the winding

Cutting a screw because it couldn't be removed

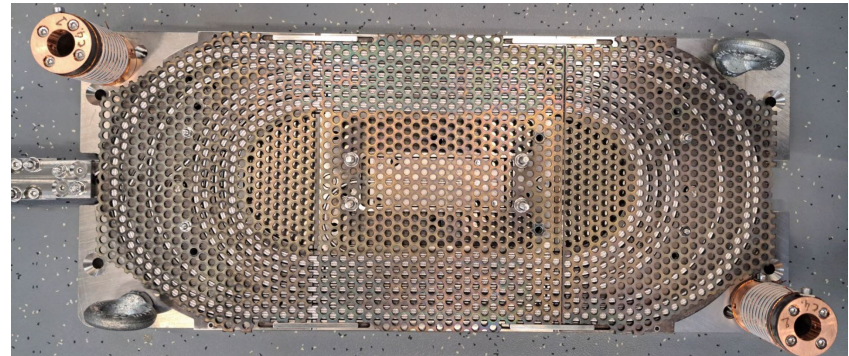
etc



Coil 1 – former 2  
Oxidation on barrels

RRR measurement of witness samples  
145 and 182 for the extracted strands

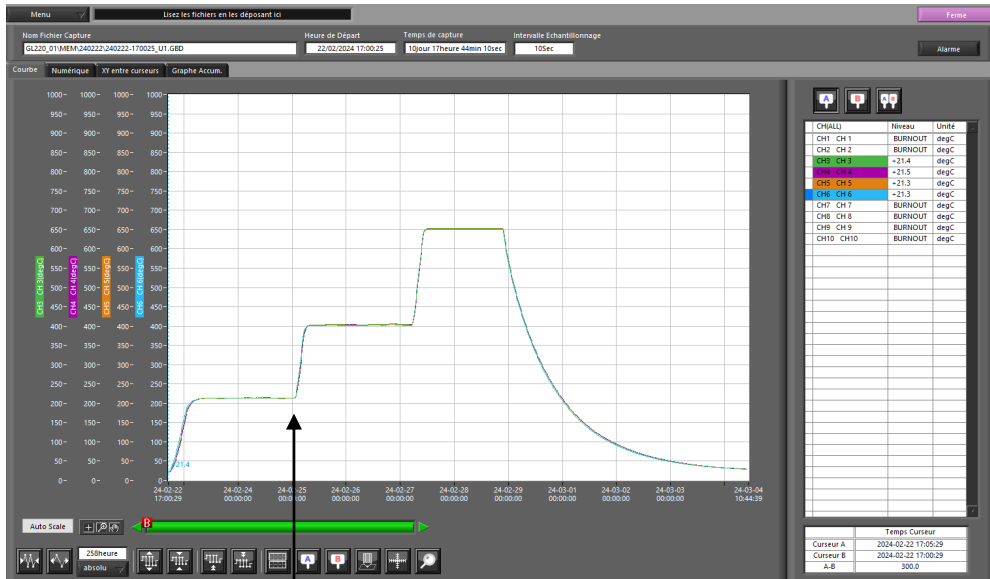
Status: waiting for barrels Ic measurements  
before the coil – former 1 reaction is launched



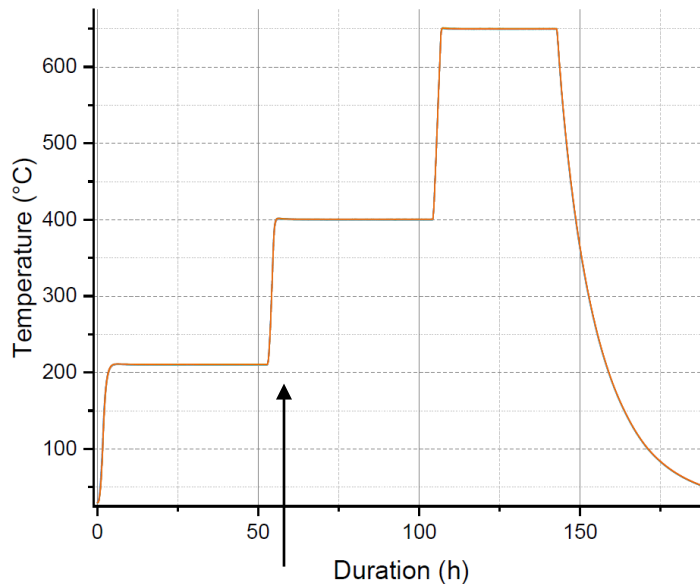
Coil 4 – former 4

CERN/927

PSI CHART/MagDev



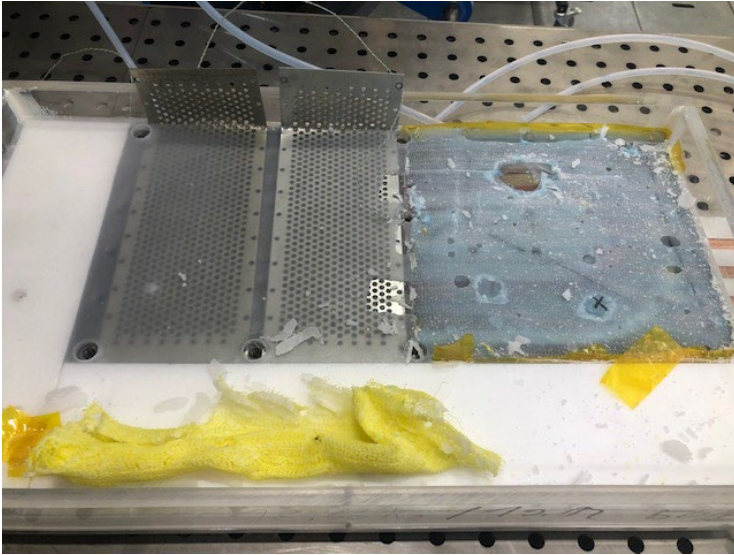
~ 50 °C/h



~ 100 °C/h



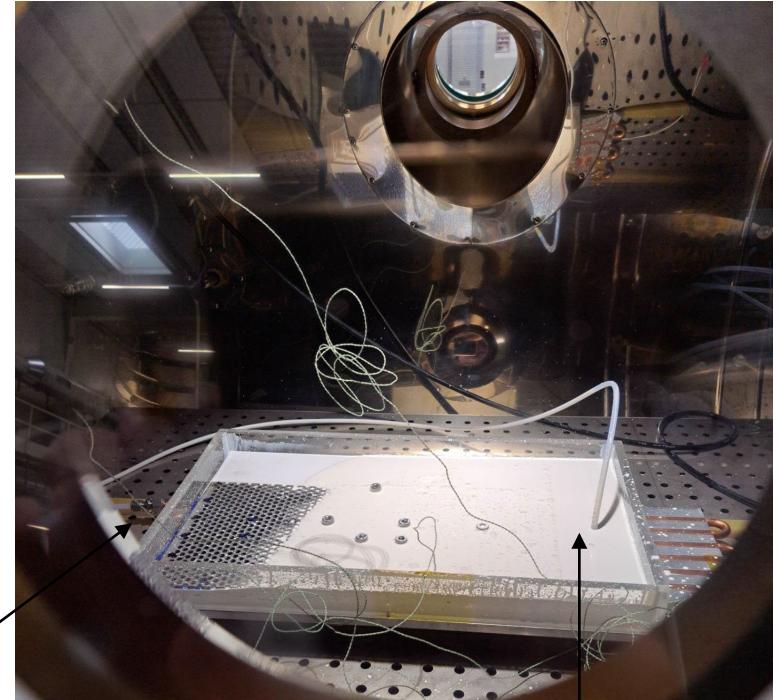
# Subscale: Impregnation trials



One-piece mold with insulated copper cable

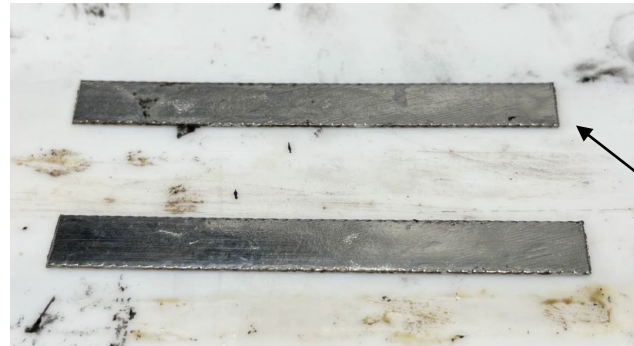
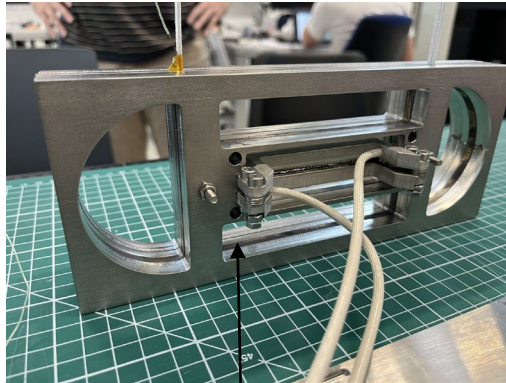
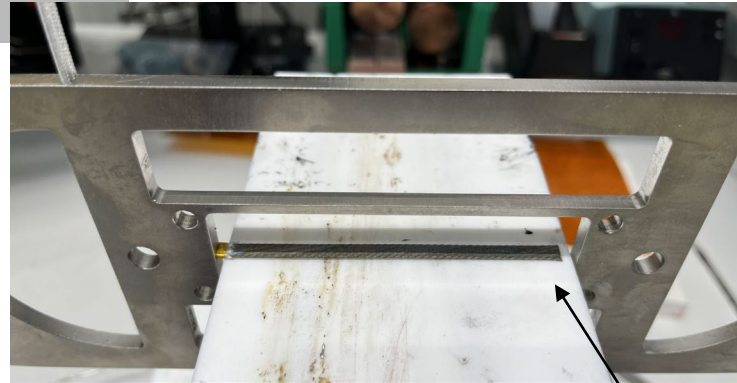
Metallic and non-metallic mesh trials

Controlled mold heaters and cooling circuit



Matrix: Filled Wax

## Intra-layer splice

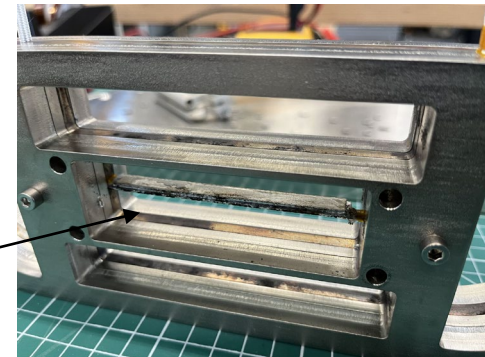


splice mock-up  
NbTi pre-thinned

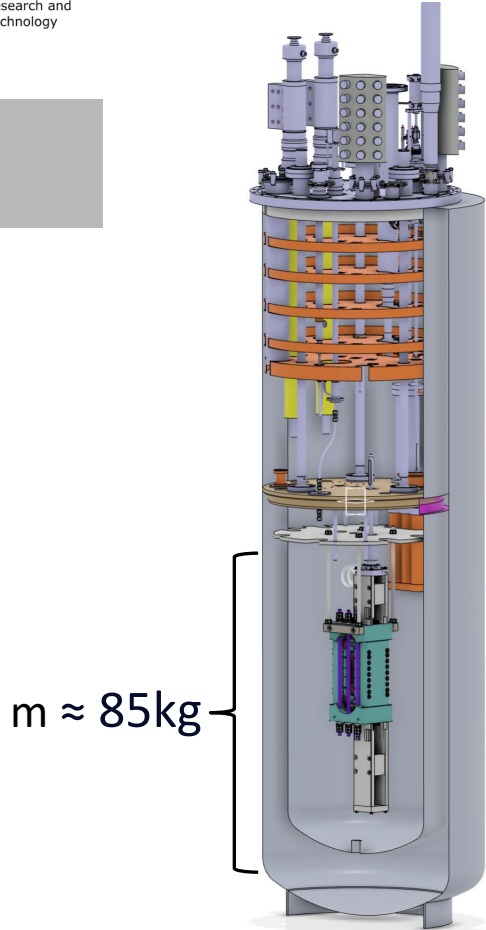
Heaters

Test setup

After splicing



# Subscale: Integration



Magnet Support Plate, 15mm

Top Mount

Subscale SM-CC Magnet

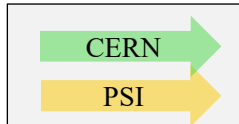
Bottom Mount

Drive Shaft

Top Adjuster





















Rot. Coil Shaft

Bottom Adjuster





# Subscale: coils manufacturing status, components delivery date and final assembly

	Winding	HT	Instrumentation	Impregnation	Splicing
Coil 1 – former 2					
Coil 2 – former 1					
Coil 3 – former 3					
Coil 4 – former 4					

Magnet structural

May/June 2024

Components delivery date

Final assembly and pre-load

June 2024

**Siegtal** and rotating coil  
integration parts status

Finalizing the drawings

# Acknowledgment

- CHART: B. Auchmann, A. Brem, T. Michlmayr, C. Müller, J. Schmidt
- PSI magnet section: R. Felder
- LBNL: D. Arbelaez, I. Pong, P. Ferracin, S. Prestemon
- CERN: E. Ravaioli, M. Wozniak, A. Verweij
- CERN: T. Boutboul, S. Hopkins, A. Bonasia
- CERN: F-J. Mangiarotti, C. Petrone, J. Feuvrier, S. Russenschuck
- CERN: F-O. Pincot, J-C. Perez, A. Haziot, E. Todesco, A. Milanese
- CERN: L. Gentini

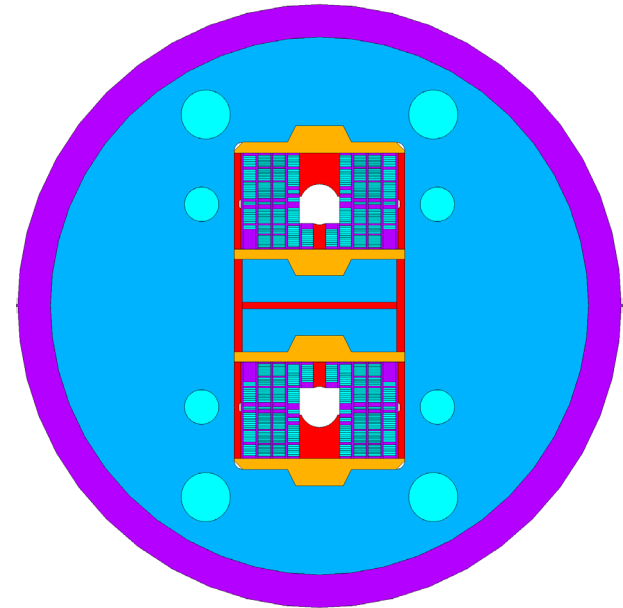
# Stress-Managed Asymmetric Common-Coils (SMACC) - Cross-Section

The asymmetric common-coils magnet has an intra-beam distance of 250 mm, 50 mm **bore**, **yoke** diameter of 660 mm and 40 mm thick stainless-steel **shell**.

The magnet has 4 different types of coils (layer 1, layer 2, layer 3,4 and layer 5) and **10 coils in total (for a double aperture magnet)**. The coils are placed in the stress-management **formers**. The preload is transferred towards the inner-most layers through the **ribs**.

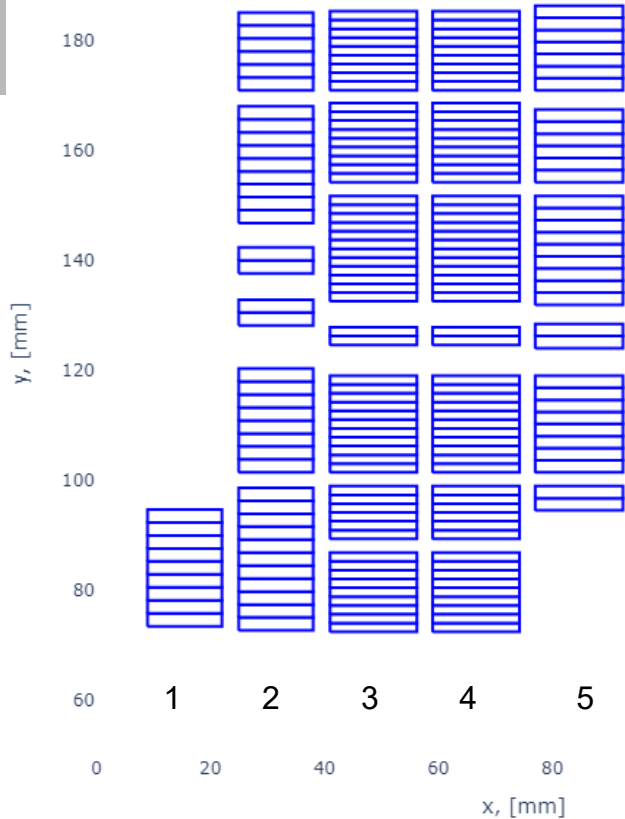
The **iron pole**, combined with the asymmetric concept, helps on the balance vertical force balance.

The magnet concept is based on **bladder & keys technology** for room temperature preload.





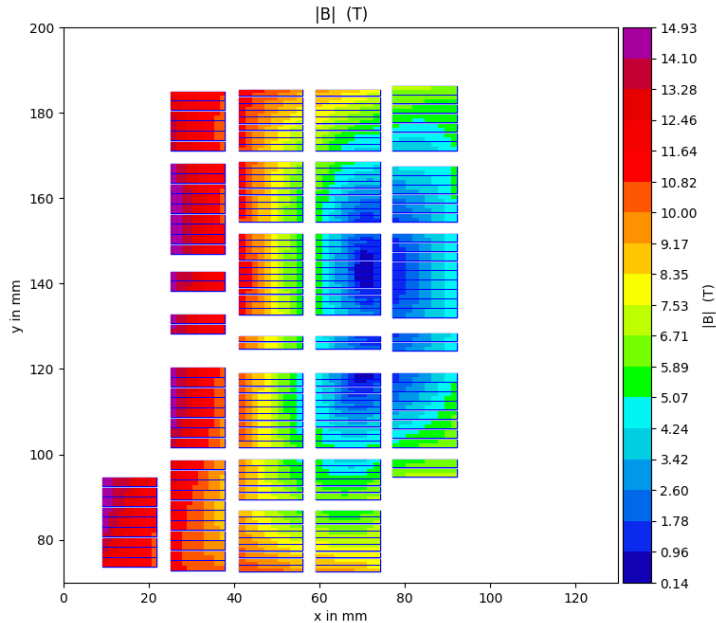
# Stress-Managed Asymmetric Common-Coils (SMACC) – Hybrid Nb<sub>3</sub>Sn / NbTi – v2



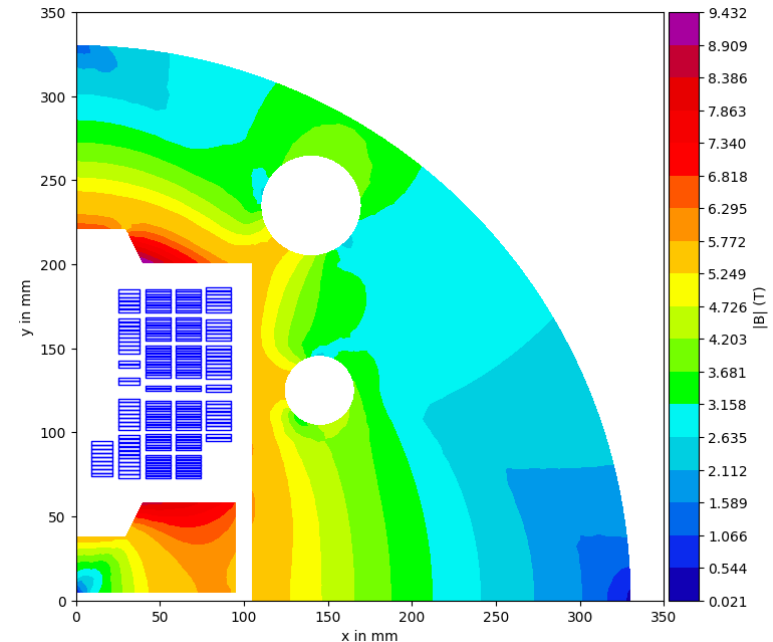
Layers	1	2	3/4	5
Wire type	Nb <sub>3</sub> Sn RRP® 162/169	Nb <sub>3</sub> Sn RRP® 162/169	Nb <sub>3</sub> Sn RRP® 78/91	NbTi
N wire x dia in mm	21 x 1.1	21 x 1.1	40 x 0.7	28 x 1.065
Cu/nCu	0.9	0.9	1.2	1.0
Bare Cable dimensions in mm	12.74 x 2.06	12.74 x 2.06	14.94 x 1.3	15.10 x 1.90
Insulation thickness in mm	0.155	0.155	0.155	0.155
Number of turns	9	38	58/58	34

# Stress-Managed Asymmetric Common-Coils (SMACC) – Hybrid Nb<sub>3</sub>Sn / NbTi – v2 - 14 T

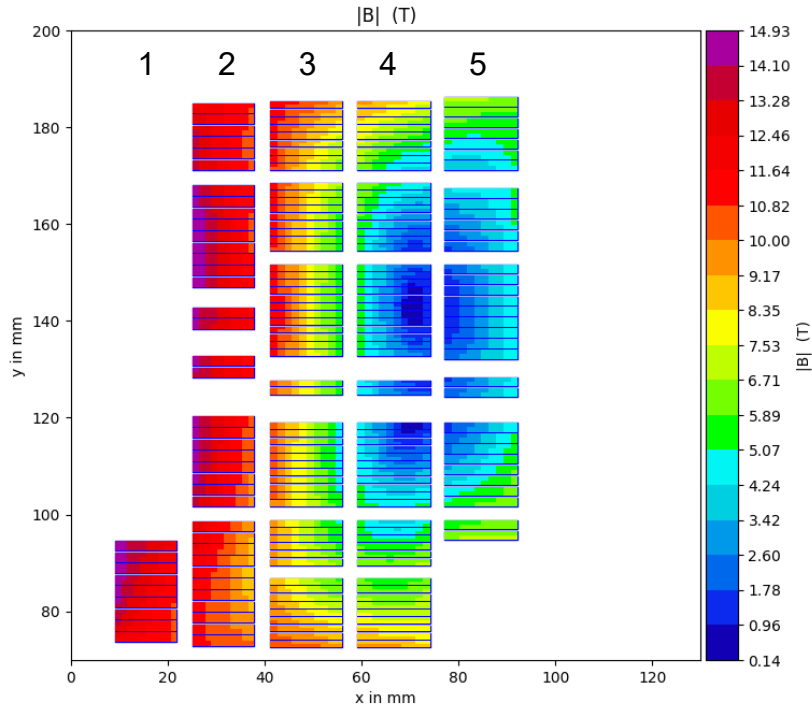
Ribs and spar thickness were optimized for mechanics. Field quality is < 20 units spread between injection (1 T) and nominal field 14 T operation and < 12 units at nominal (to be further optimized after the final cable definition).  $I_{op} = 12.48$  kA



$|B|$  including self-field



# Stress-Managed Asymmetric Common-Coils (SMACC) – Hybrid Nb<sub>3</sub>Sn / NbTi – v2



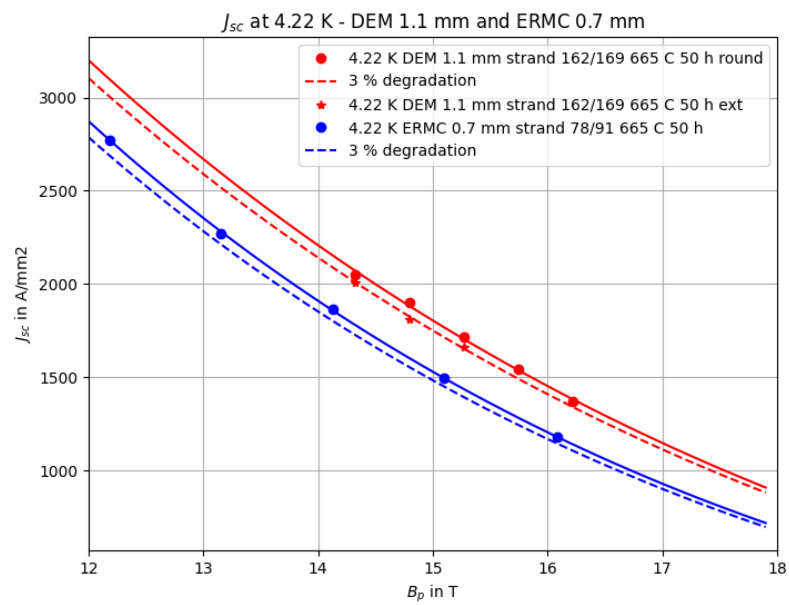
$B_0$ in T	$B_{peak}$ in T	$T_{op}$ in K	% Margin	$I_{op}$ in kA
14	14.93	4.22	8.5	12.48

Layer	$B_{peak}$ in T	% Margin	$J_{sc}$ in A/mm <sup>2</sup>	$J_{cu}$ in A/mm <sup>2</sup>	$J_{eng}^*$ in A/mm <sup>2</sup>
1	14.82	9.0	1188.2	1320.2	405.5
2	14.93	8.5			
3	11.64	13.4	1783.6	1486.3	511.8
4	9.43	25.7			
5	7.05	10.9	1000.7	1000.7	368.4

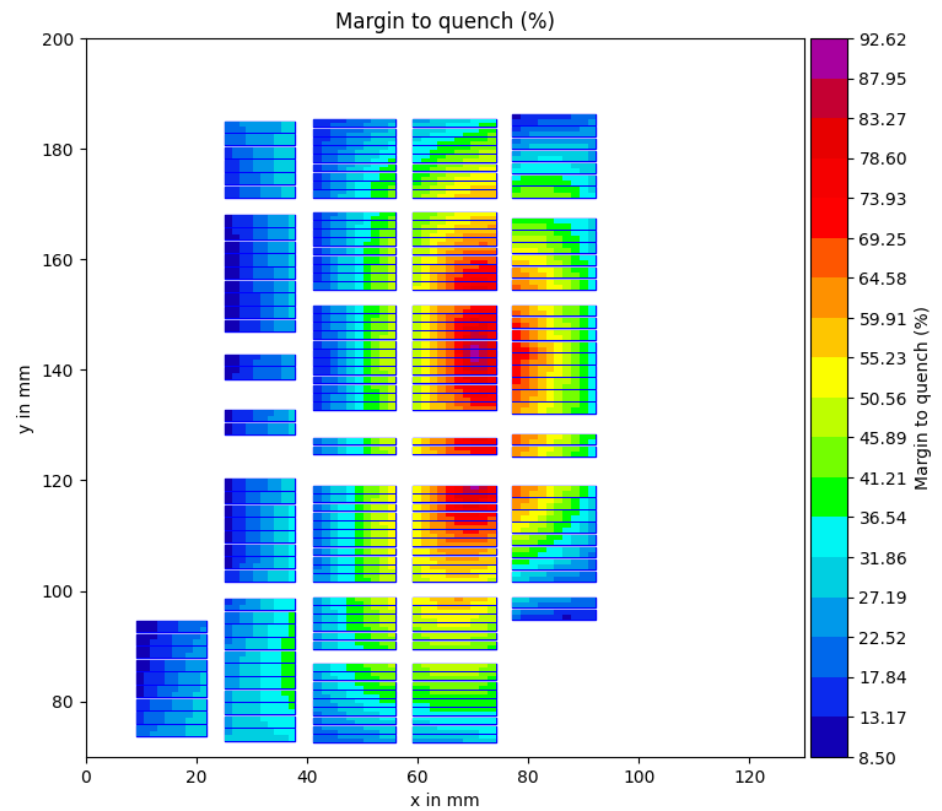
\* Including insulation area



# Stress-Managed Asymmetric Common-Coils (SMACC) – Hybrid Nb<sub>3</sub>Sn / NbTi – v2 - 14 T



High-Field and Low-Field strand fitting

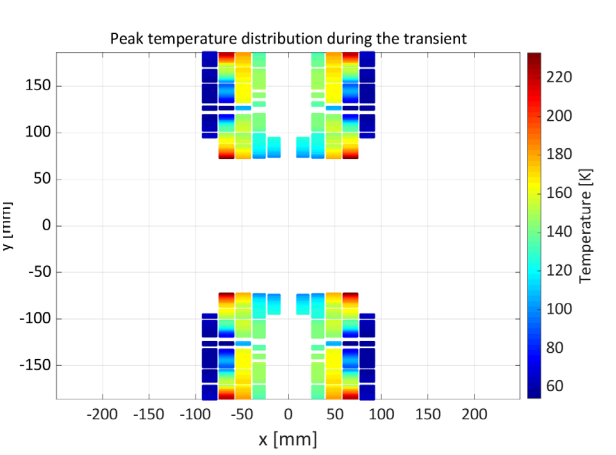
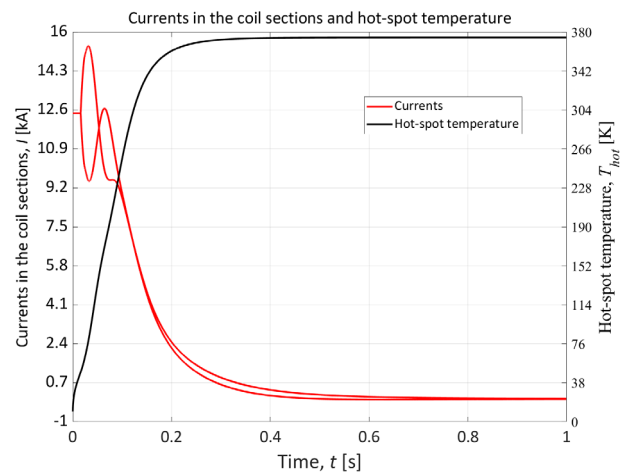
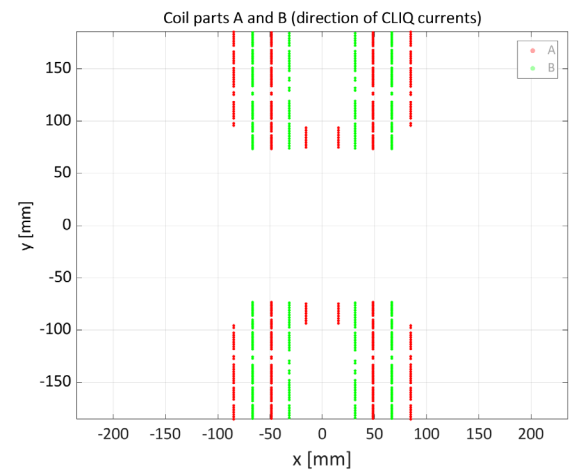


# Protecting 15 m long magnet with 1x 100 mF, 2 kV CLIQ unit

Red: Negative initial CLIQ  $di/dt$   
Green: Positive initial CLIQ  $di/dt$

Currents vs time  
Hot-spot temperature vs time

Temperature in the turns  
(hot-spot not shown here)



Hot-spot temperature	Peak voltage to ground	Peak CLIQ current
375 K	1950 V	5890 A

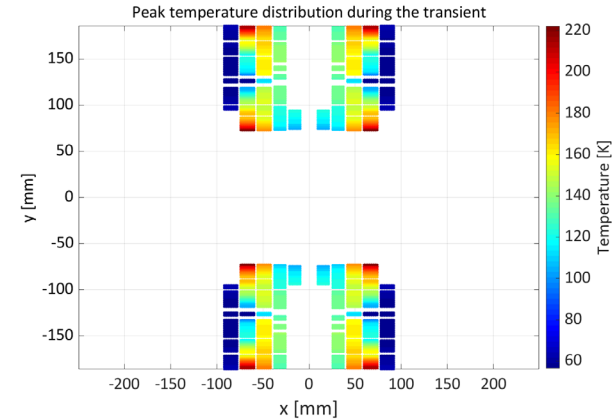
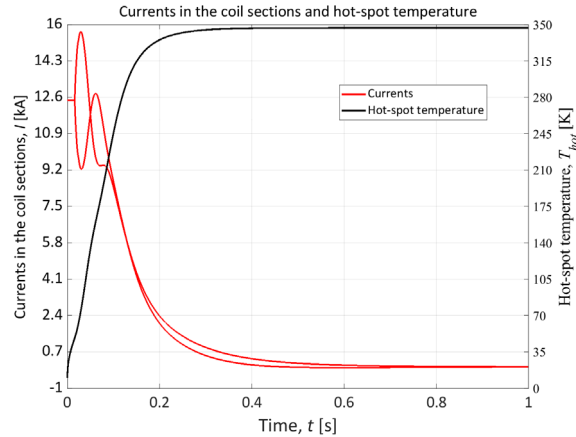
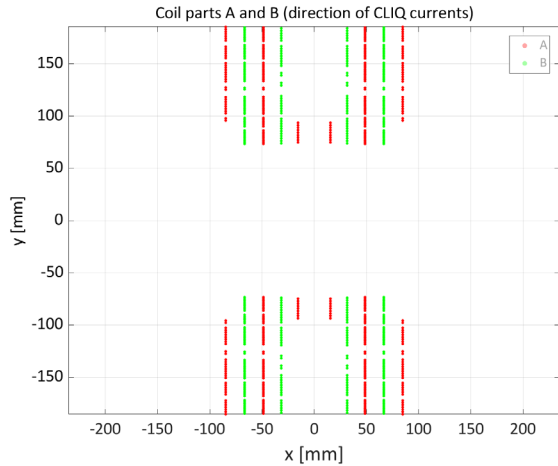
# Protecting 12 m long magnet with 1x 100 mF, 2 kV CLIQ unit

Red: Negative initial CLIQ  $di/dt$   
Green: Positive initial CLIQ  $di/dt$

Currents vs time

Hot-spot temperature vs time

Temperature in the turns  
(hot-spot not shown here)



Hot-spot temperature	Peak voltage to ground	Peak CLIQ current
347 K	1790 V	6430 A



# Protecting 0.8 m long magnet with 1x 100 mF, 0.5 kV CLIQ unit

Red: Negative initial CLIQ  $di/dt$

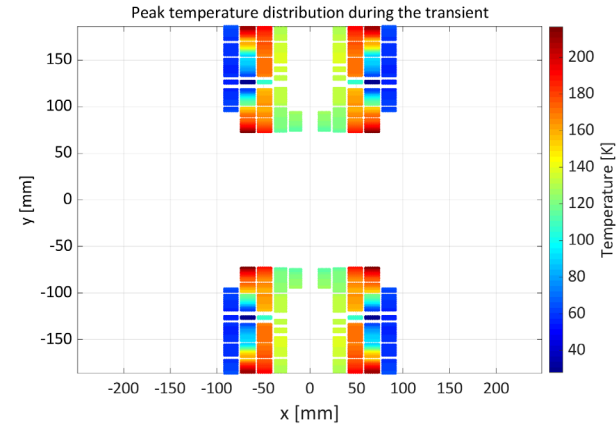
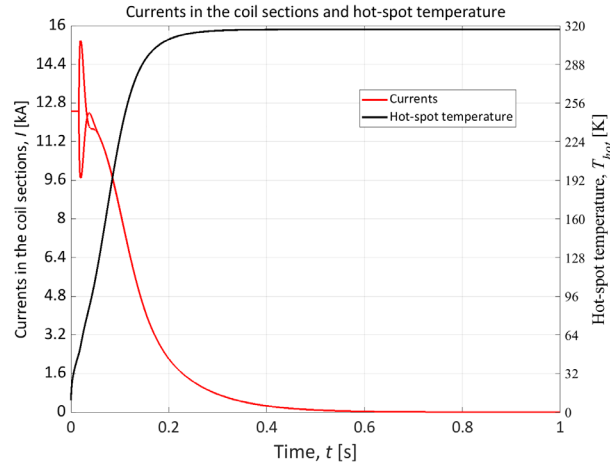
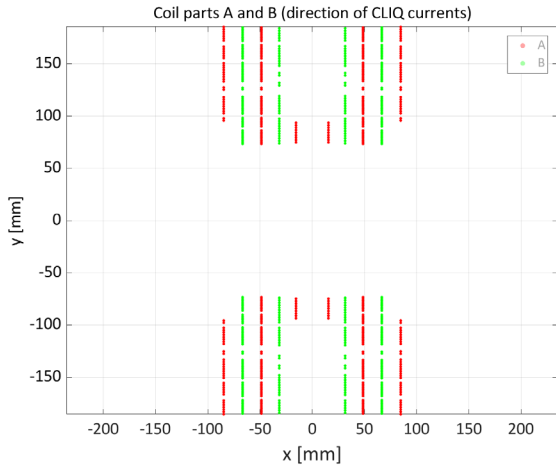
Green: Positive initial CLIQ  $di/dt$

Currents vs time

Hot-spot temperature vs time

Temperature in the turns

(hot-spot not shown here)

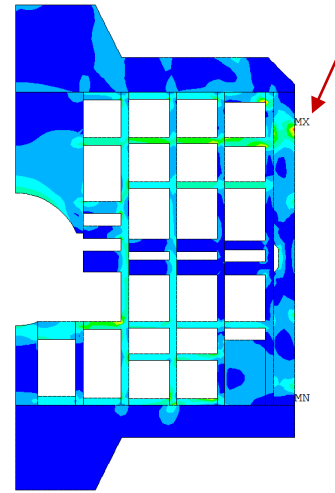


Hot-spot temperature	Peak voltage to ground	Peak CLIQ current
317 K	150 V	5680 A

# Mechanical Analysis

Von-Mises

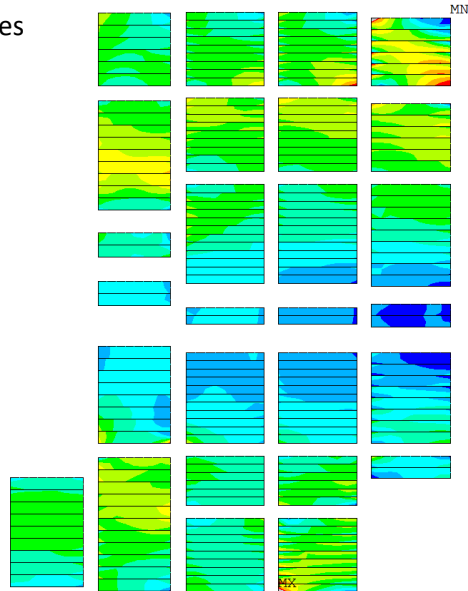
Pre-load with 0.75 mm interference on the keys.



ANSYS 2021 R1  
Build 21.1  
NODAL SOLUTION  
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EFACET=1  
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SMN =29.9604  
SMX =.793E+09

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.444E+09
.533E+09
.622E+09
.711E+09
.800E+09

Von-Mises



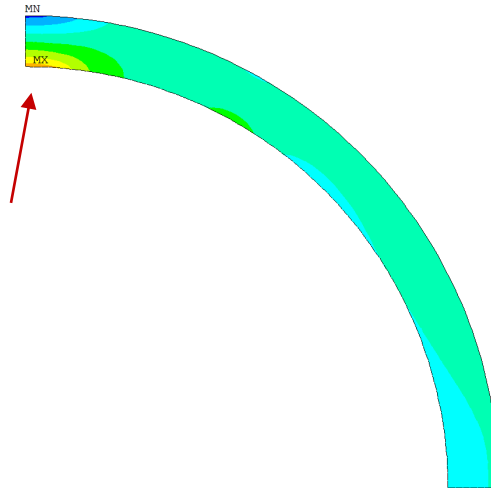
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.667E+08
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.889E+08
.100E+09

Keys

D. M. Araujo

Keys



Hoop Stress

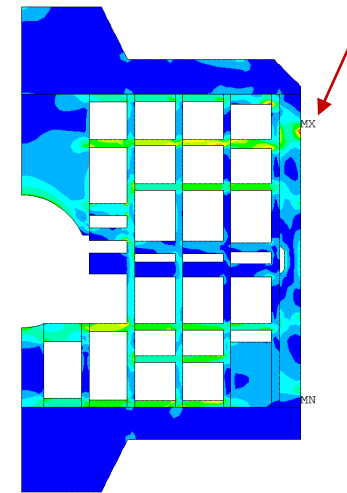
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Keys

# Mechanical Analysis

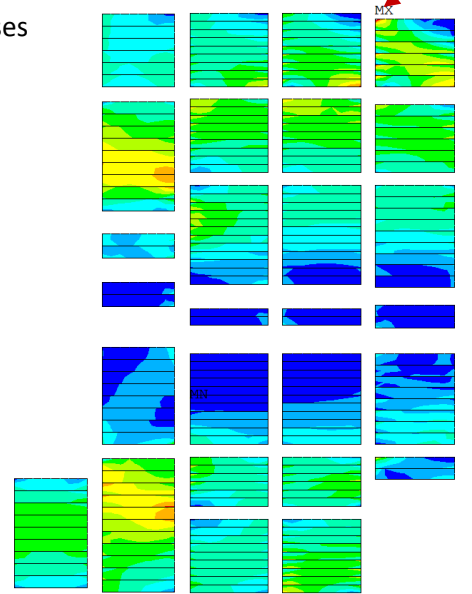
Von-Mises



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Von-Mises



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Cool-down

Hoop Stress

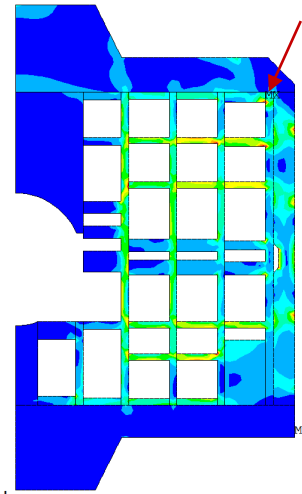


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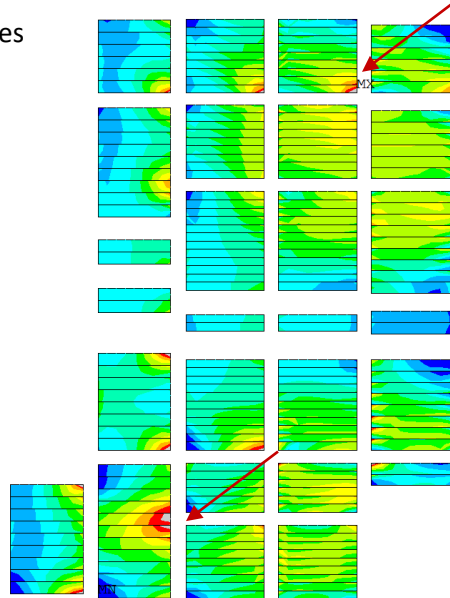
# Mechanical Analysis

Von-Mises



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Von-Mises

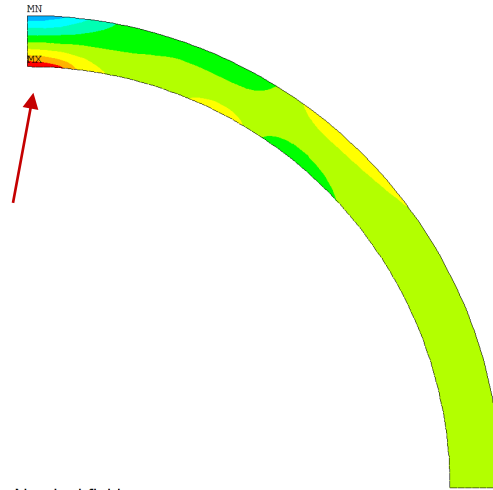


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.100E+09

Nominal field

D. M. Araujo

Nominal field

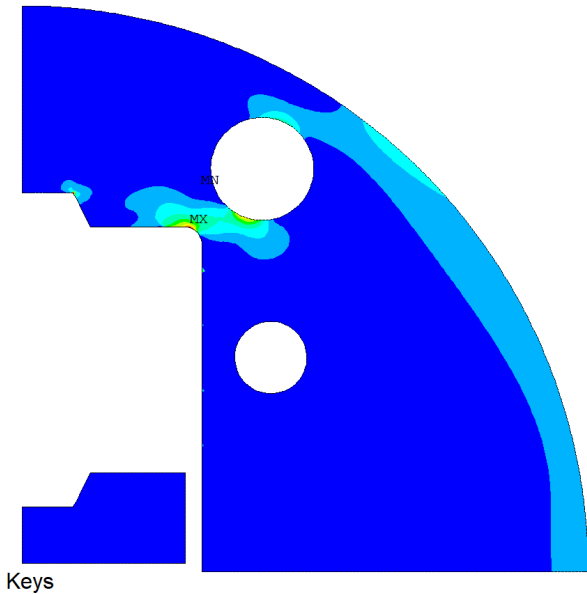


Hoop Stress

Nominal field

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.204E+09  
.255E+09  
.306E+09  
.357E+09  
.408E+09  
.459E+09

# Mechanical Analysis

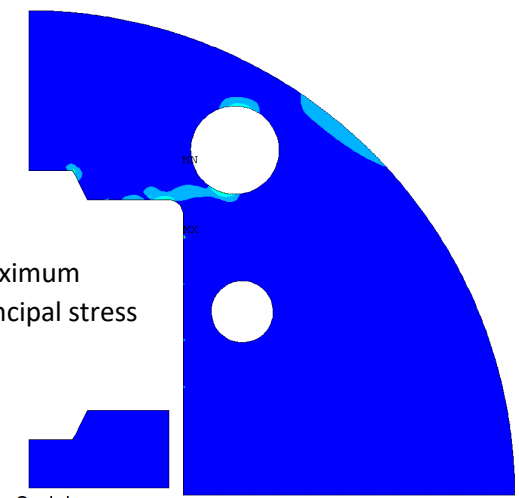


ANSYS 2021 R1
   
 Build 21.1
   
 NODAL SOLUTION
   
 STEP=1
   
 SUB =1
   
 TIME=1
   
 S1 (AVG)
   
 PowerGraphics
   
 EFACET=1
   
 AVRES=Mat
   
 DMX =.715E-03
   
 SMX =.300E+09

0
.333E+08
.667E+08
.100E+09
.133E+09
.167E+09
.200E+09
.233E+09
.267E+09
.300E+09

Keys

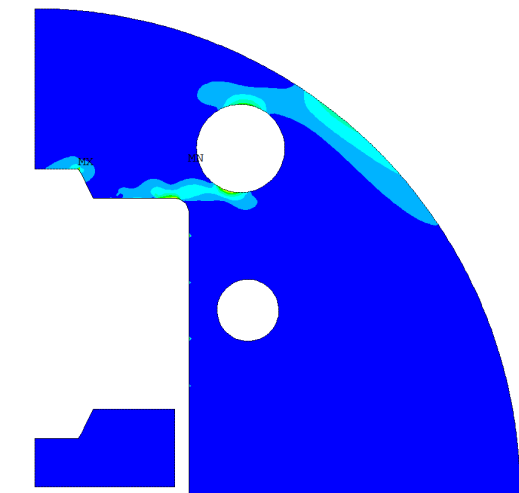
Maximum principal stress



ANSYS 2021 R1
   
 Build 21.1
   
 NODAL SOLUTION
   
 STEP=2
   
 SUB =1
   
 TIME=2
   
 S1 (AVG)
   
 PowerGraphics
   
 EFACET=1
   
 AVRES=Mat
   
 DMX =.994E-03
   
 SMX =.199E+09

0
.333E+08
.667E+08
.100E+09
.133E+09
.167E+09
.200E+09
.233E+09
.267E+09
.300E+09

Cool-down



Build 21.1
   
 NODAL SOLUTION
   
 STEP=3
   
 SUB =1
   
 TIME=3
   
 S1 (AVG)
   
 PowerGraphics
   
 EFACET=1
   
 AVRES=Mat
   
 DMX =.001072
   
 SMX =.214E+09

0
.333E+08
.667E+08
.100E+09
.133E+09
.167E+09
.200E+09
.233E+09
.267E+09
.300E+09

Nominal field

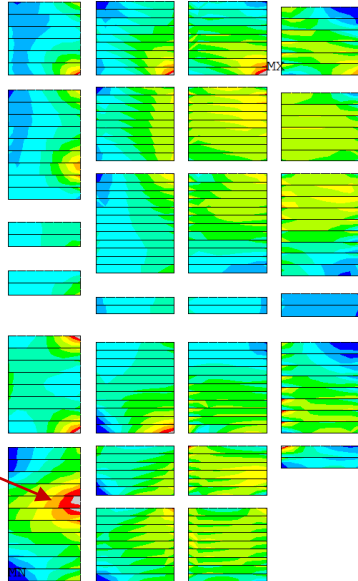


14 T operation

Stress on coils: **123 MPa on corners**, other else  
< 100 MPa

> 30% engineering margin on the peak of stress regions.

Von-Mises



Nominal field

ANSYS 2021 R1  
Build 21.1  
NODAL SOLUTION  
STEP=3  
SUB =1  
TIME=3  
SEQV (AVG)  
PowerGraphics  
EFACET=1  
AVRES=Mat  
DMX =.696E-03  
SMN =484723  
SMX =.123E+09  
0  
.111E+08  
.222E+08  
.333E+08  
.444E+08  
.556E+08  
.667E+08  
.778E+08  
.889E+08  
.100E+09

D. M. Araujo

