

Collimators for LHC IR3 dispersion suppressors

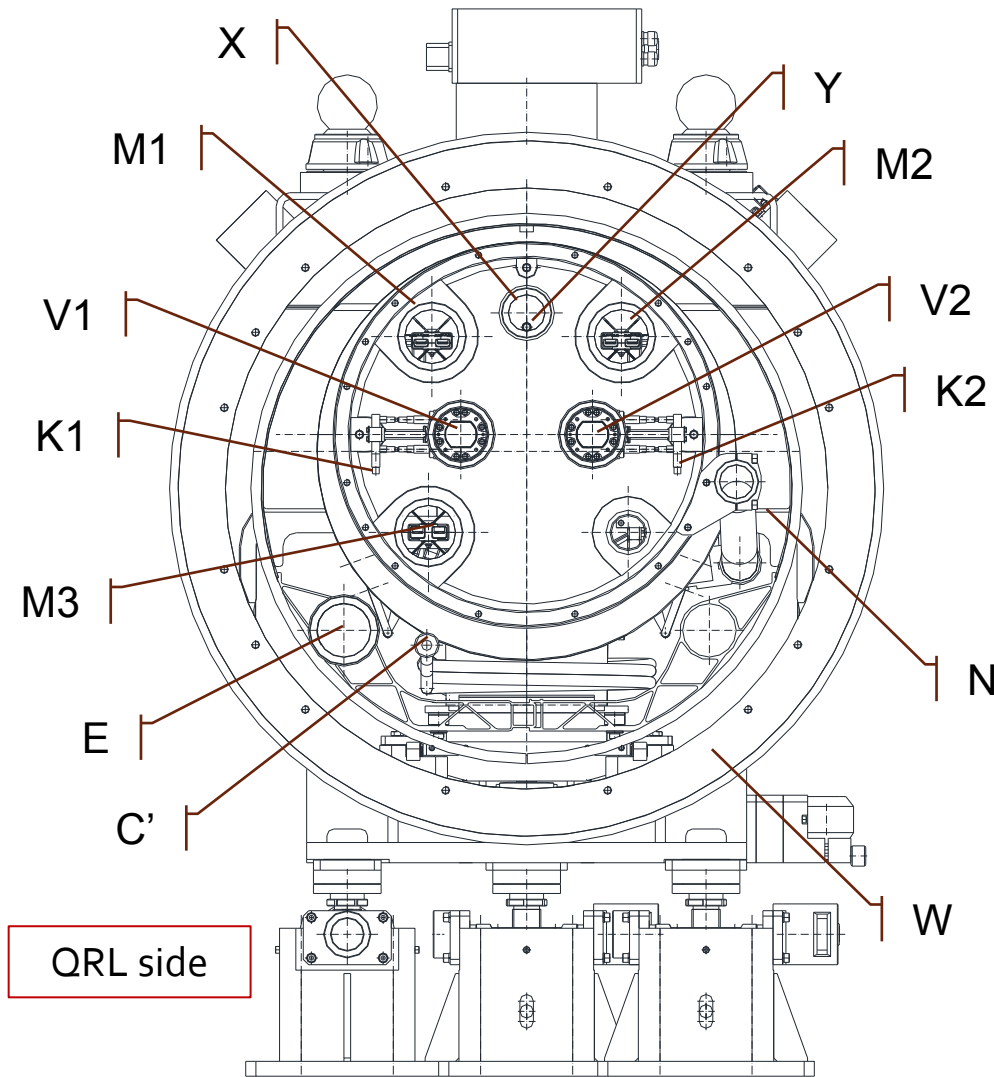
# QTC Bypass cryostat design

May 26, 2011

presented by D. Ramos

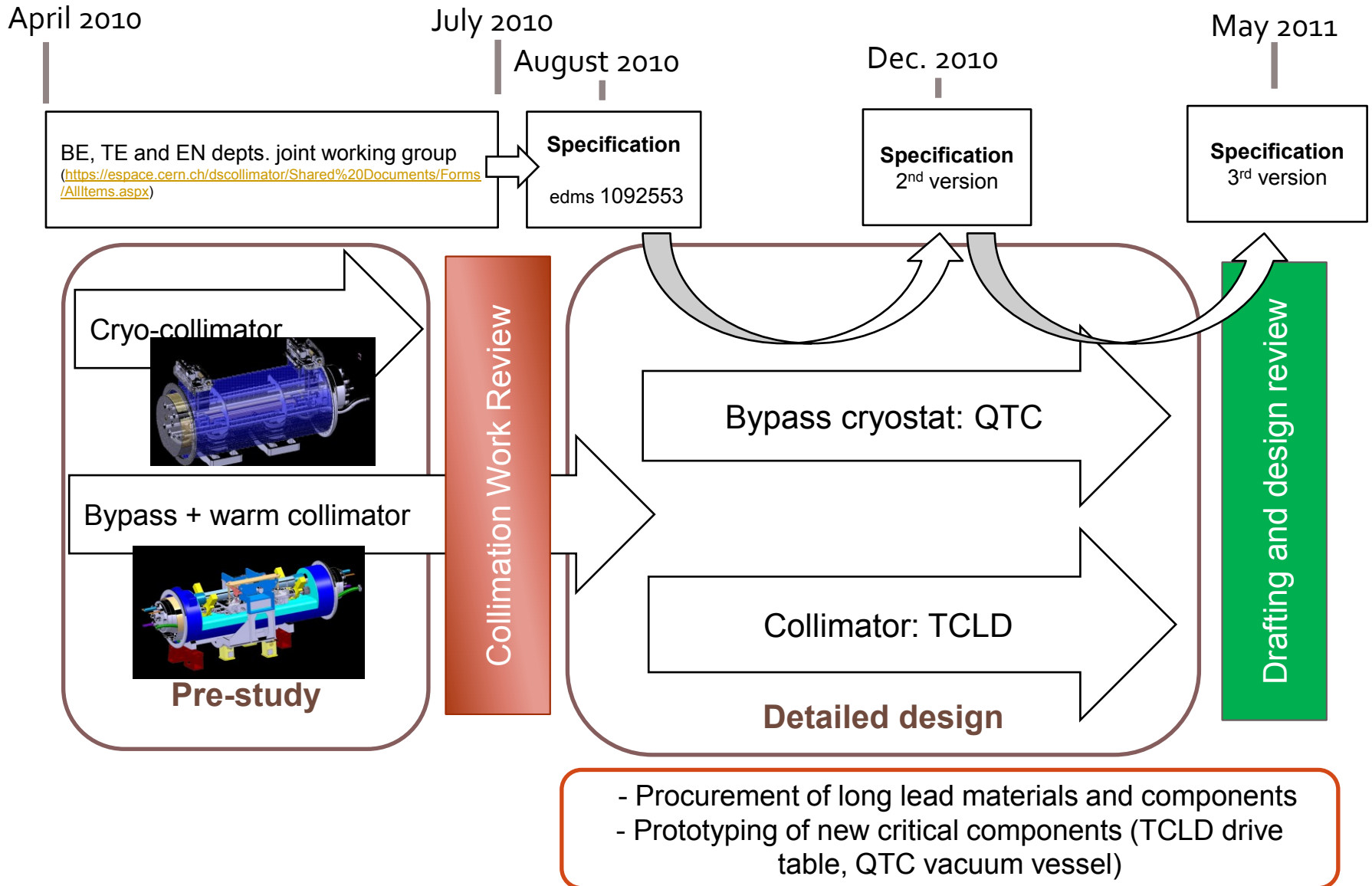
on behalf of a dedicated team: P. Minginette, L. Zuccalli, N. Chritin, D. Maciocha, L. Alberty, A. Bertarelli, A. Cherif, R. Claret, G. Favre, P. Moyret, M. Redondas, M. Timmins, L. Gentini, C. Mucher  
with input and contributions from: S. Chemli, P. Trilhe, T. Renaglia, R. Van Weelderren, V. Parma, A. Jacquemod, N. Bourcey, P. Bestmann, R. Principe, P. Fessia, V. Boccone, V. Baglin, P. Cruikshank, N. Provot, W. Maan, S. Sgobba, M. Polini, JM. Dalin, A. Gerardin, R. Denz, and many more...

# Outline



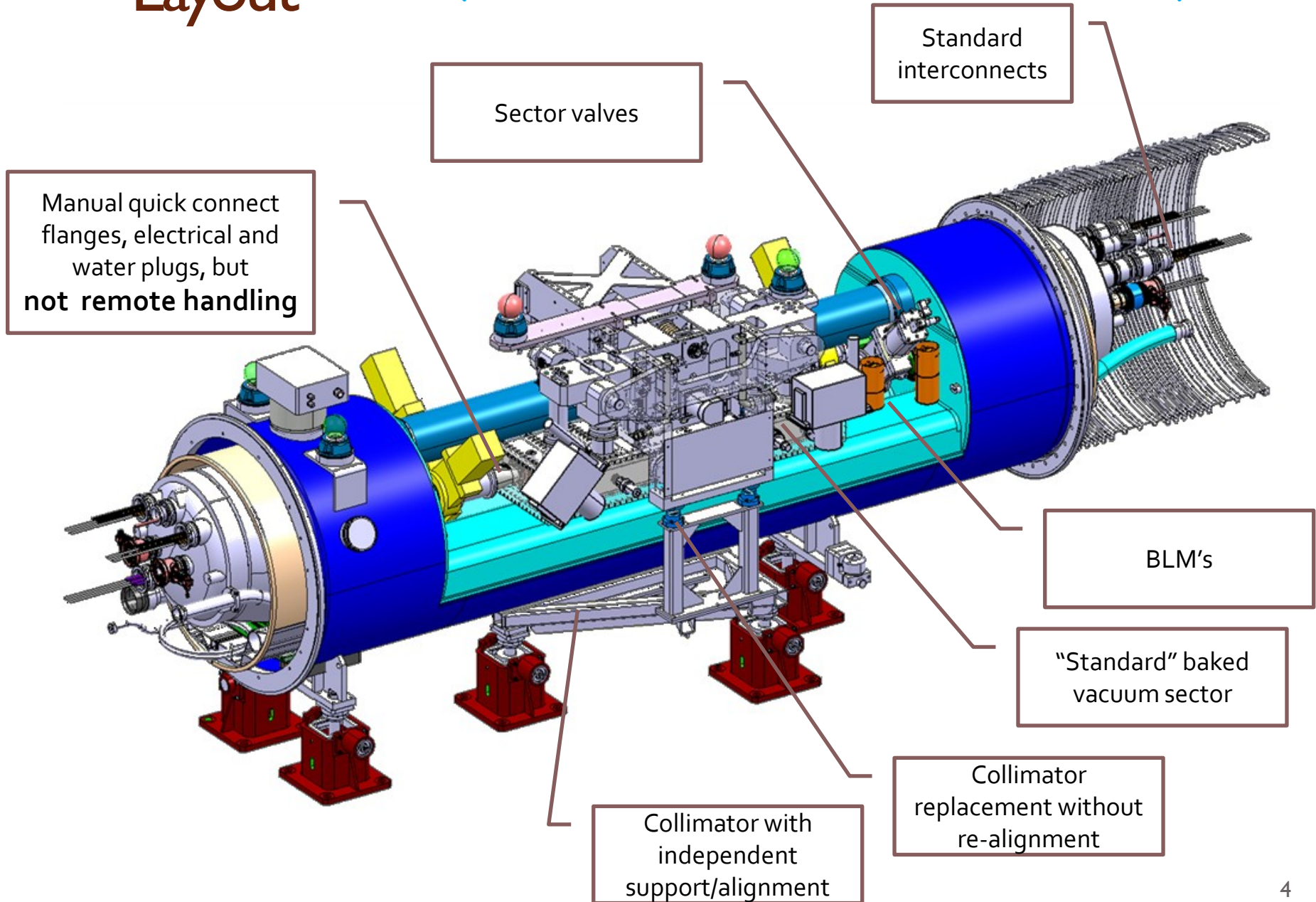
- Overview
- Busbars (M1, M2, M3)
- 1.9 K He II vessel and HX
- 4.6 to 20 K lines (C', K)
- 50 to 75 K level (E, thermal shield)
- Insulation vacuum vessel (W)
- Beam vacuum (V1, V2)
- Supports (cold feet, jacks)
- Conclusion

# Project timeline

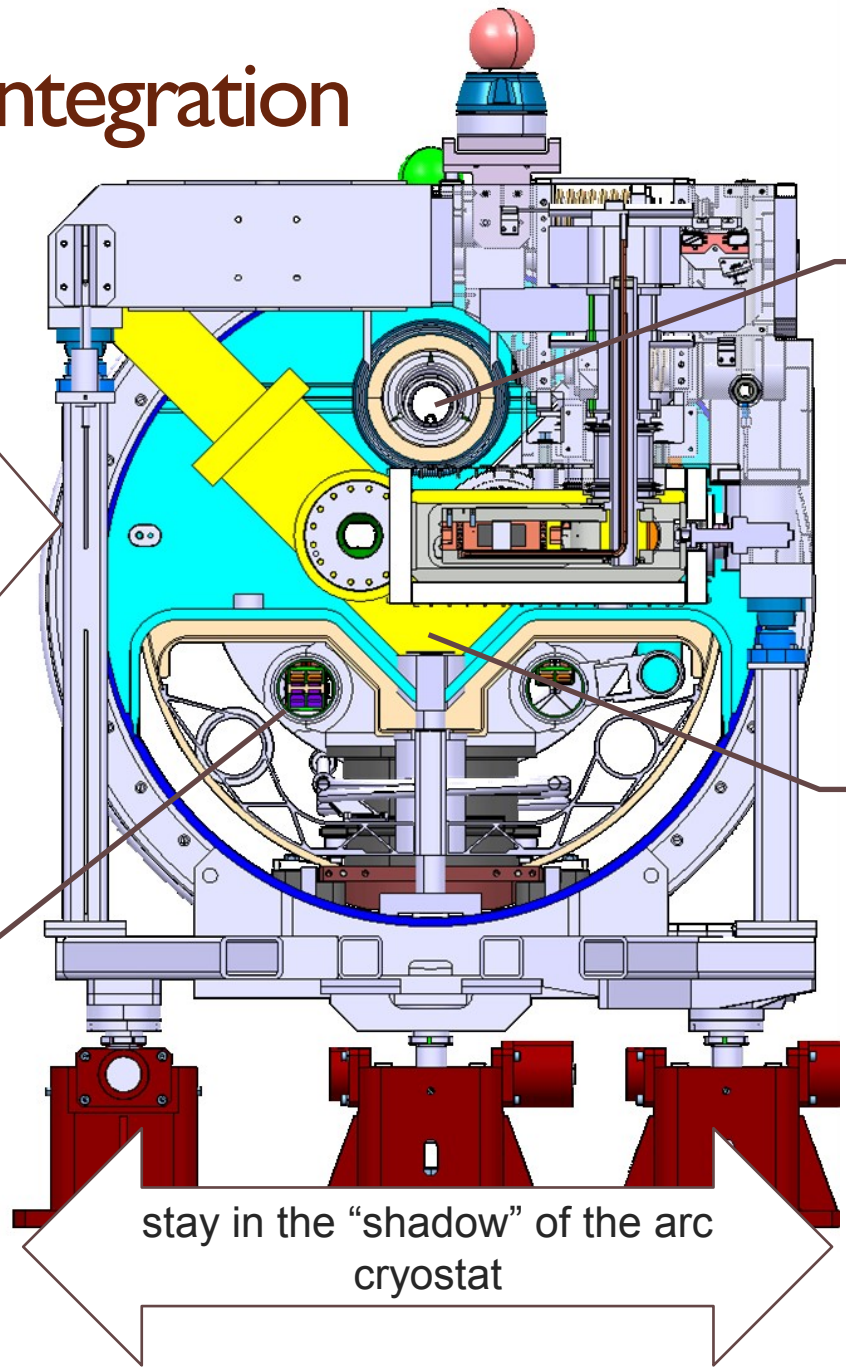


# Layout

4.0 m + 0.5 m interc. = **4.5 m** installation length



# Collimator integration



$\Sigma$  jaw,  
vacuum tank,  
bakeout jacket,  
assy. tolerances,  
installation gap

No bypass for two-  
phase He flow

RF-shielded sector  
valves

Room for only two  
bypass tubes  
→M<sub>1</sub>& M<sub>3</sub> grouped.

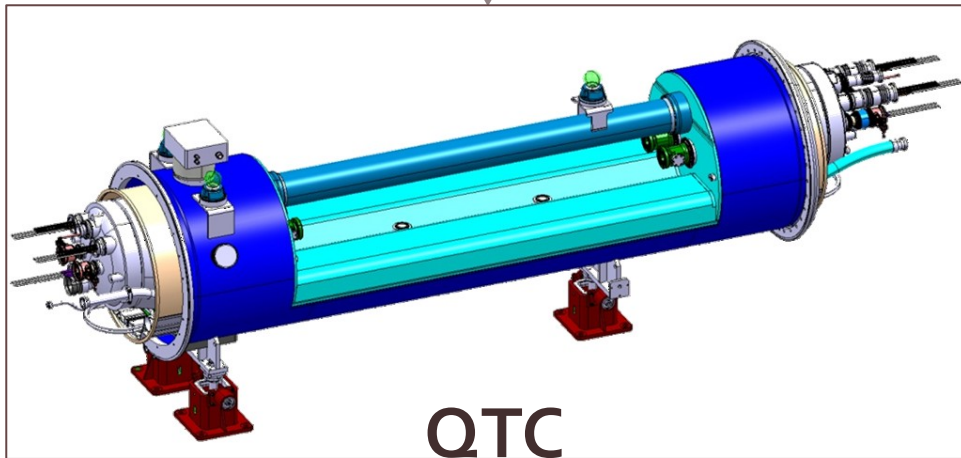
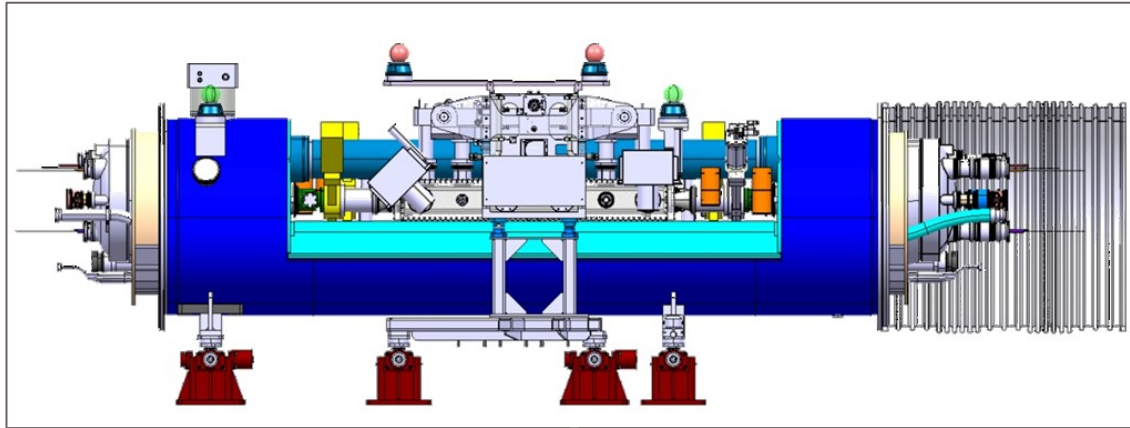
Cross-talk addressed  
by R. Denz:  
not an issue

See A. Siemko's pres.

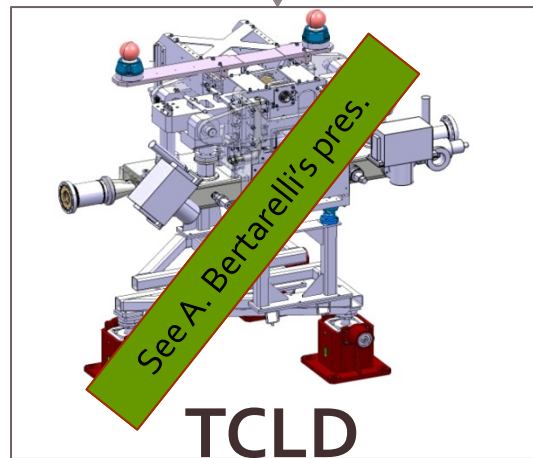
stay in the "shadow" of the arc  
cryostat



# Equipment breakdown

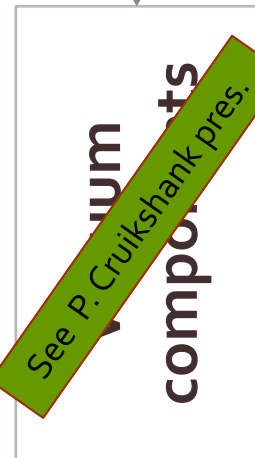


QTC



See A. Bertarelli's pres.

TCLD



See P. Cruikshank pres.  
um  
ts  
components

# Busbars

See A. Siemko's pres.

Radiation damage studies on-going (V. Boccone)

New equipment:  
→ voltage taps on 13 kA busbars  
→ IFS (capillary routing to be designed)

Busbar bending in-situ w/ cable already tinned

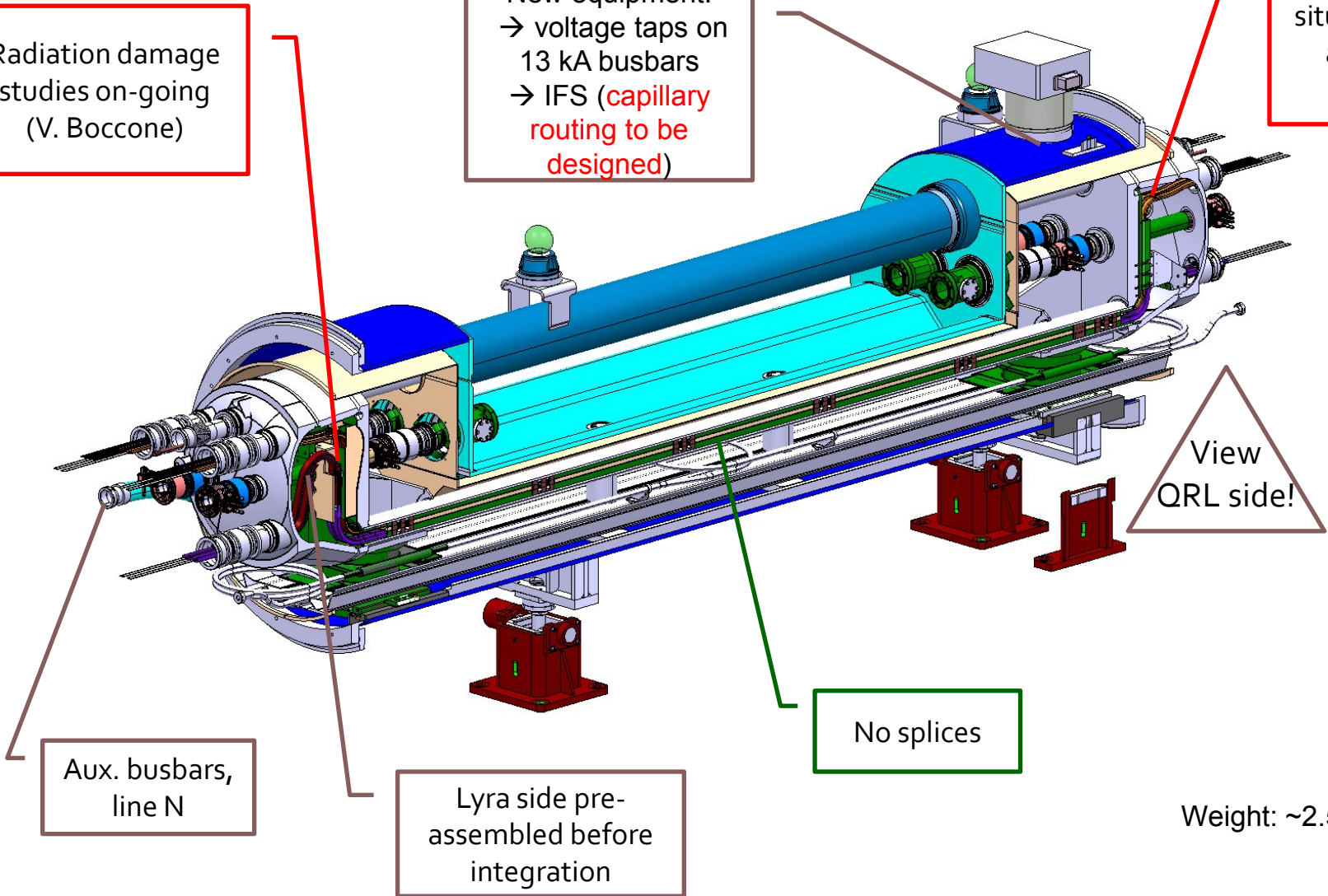
View QRL side!

No splices

Aux. busbars, line N

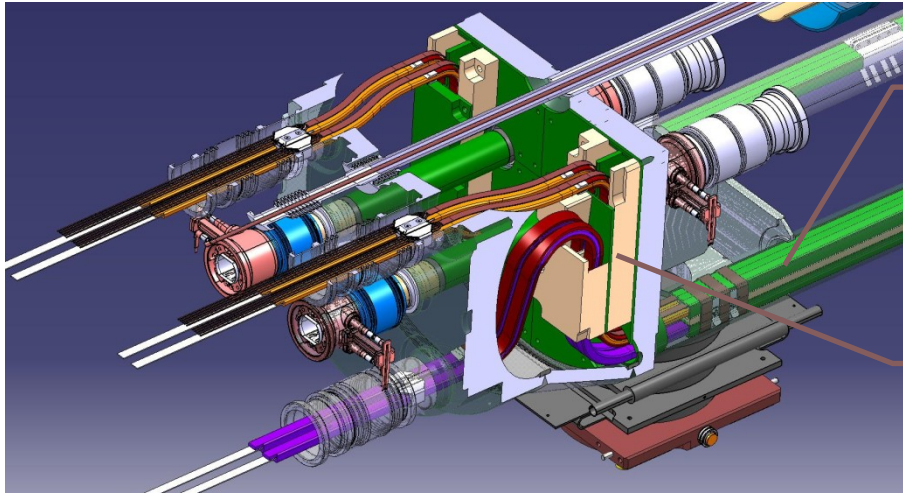
Lyra side pre-assembled before integration

Weight: ~2.5 ton



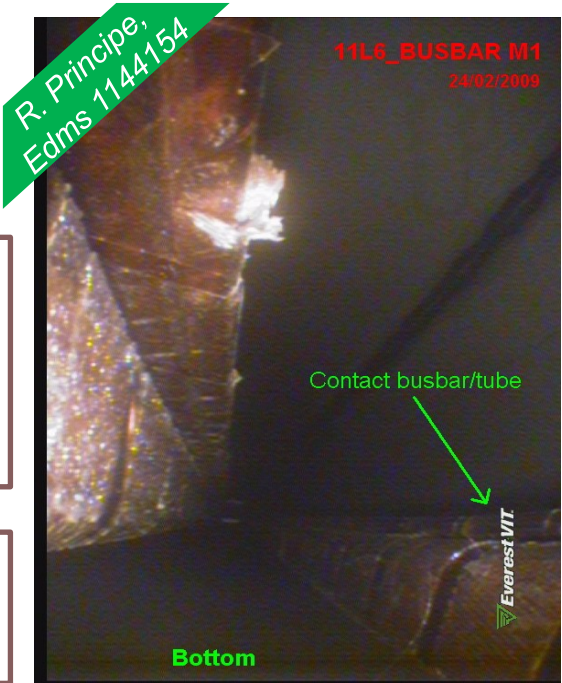
# Busbar insulation

Lyra



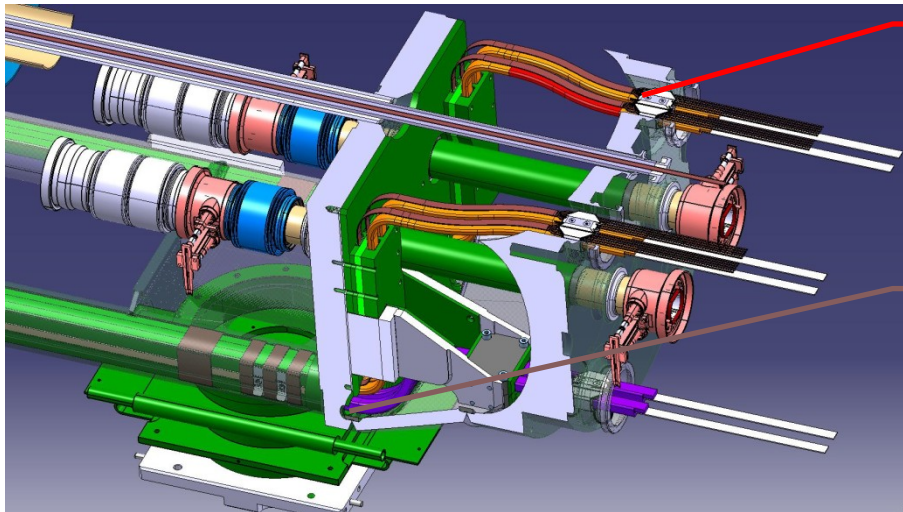
Full length insulation and Lorentz force support (200 kgf/m)

Independently guided lyra displacements



Bottom

Fixed point



New spiders to be designed

HD polyethylene covering all critical regions



New lyra design: see Edms 1137872



# He II inner vessel

## Pressure vessel

- CERN GSI-M3 special equipment
- EN 13458:2002 parts 1 and 2, Cryogenic vessels – Static vacuum insulated vessels
- **PS = 20 bar, Ptest = 25 bar**
- *Overpressure safety relies on existing quench valves*

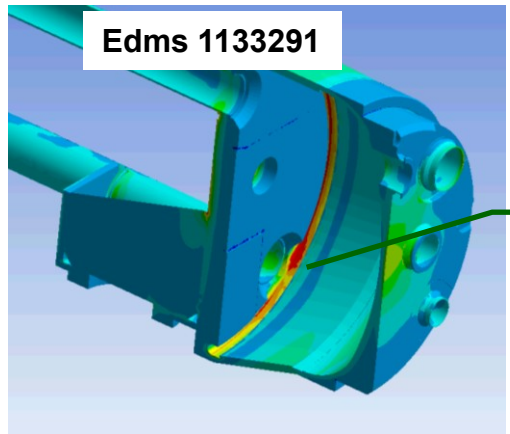
Dipole end covers

Pre-installed X-line shield and vacuum enclosure pipes

H

Flat covers for minimum length

Bypass pipes as structural elements



$2 \times T_{M13}$   
 $T_N$

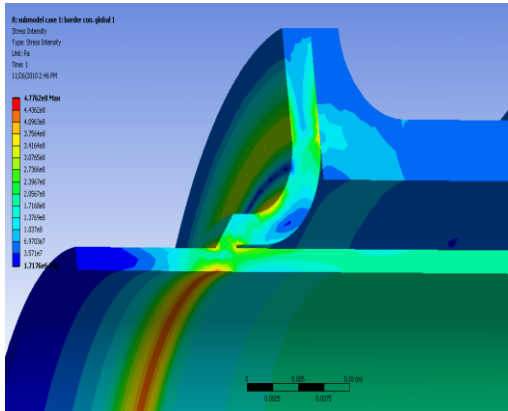
Low stresses, design driven by deformations

Cold bore tubes: installed after vessel closure to avoid welding distortions

See R. Van Weelderen's pres. for details on instrumentation

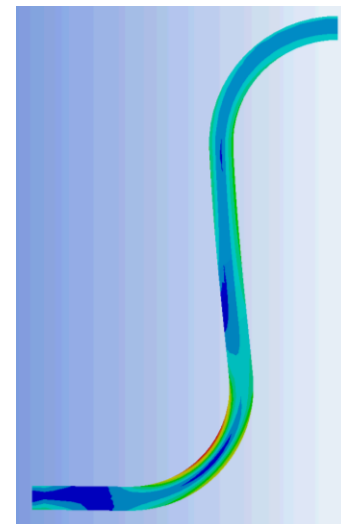
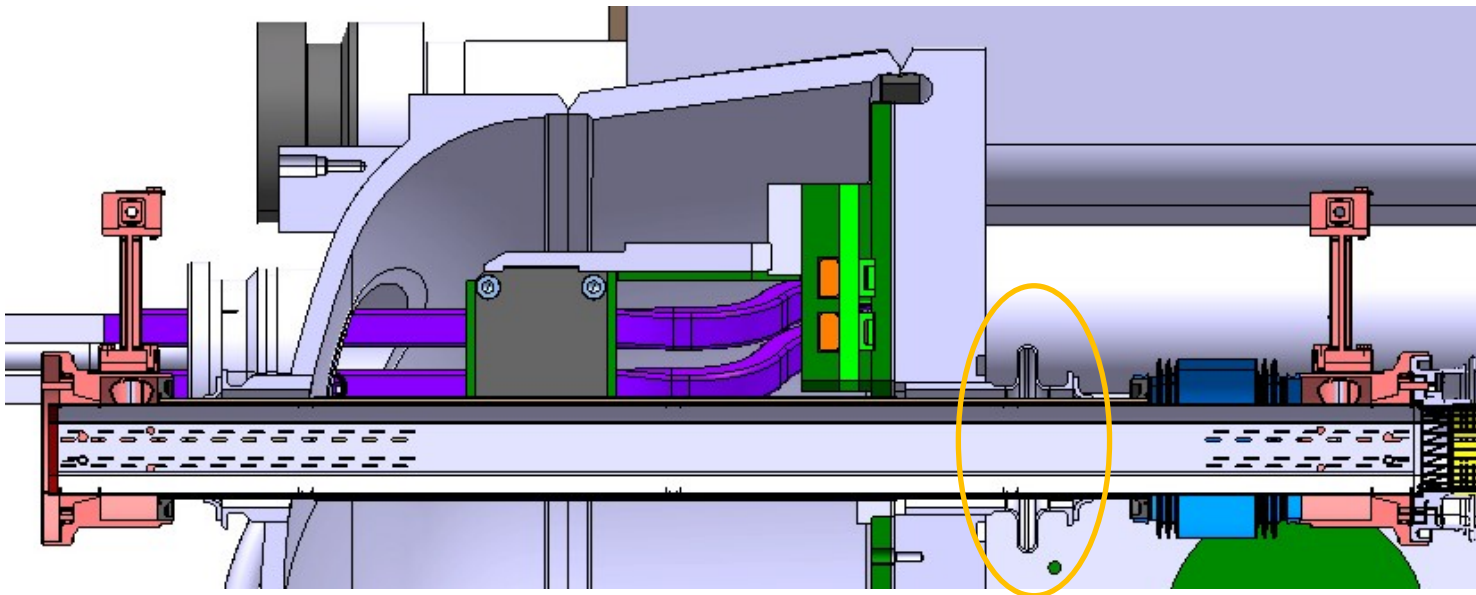
Draft fabrication specification Edms 1132997

# Interface with cold bore tube



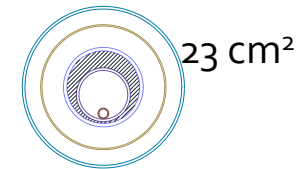
## Short cold bore tube

- Flat cover deflection and short cold bore → High stress
- Solution: Membrane for longitudinal flexibility
- Compromise between pressure strength and flexibility: **Design close to maximum allowance**
- Maintain lateral stiffness for cold bore alignment (64 kN/mm)

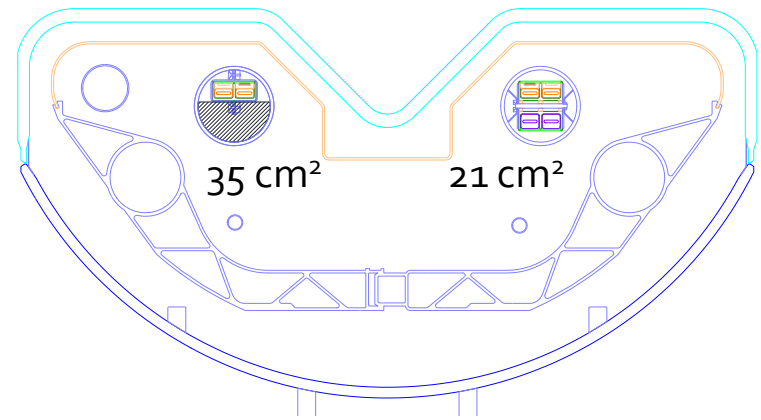


# Hydraulic and thermal continuity

- Pressure drop analytical estimations:
  - He flow 6 kg/s, 6 K, 20 bar
  - Specification: Pressure drop of a 50 mm smooth pipe: **4.3 kPa/m**
  - Pressure drop QTC: **3.1 kPa/m** ( $\epsilon=0.2$  mm)
  - *Conservative results according to CFD analysis by H. Alain TE-CRG*

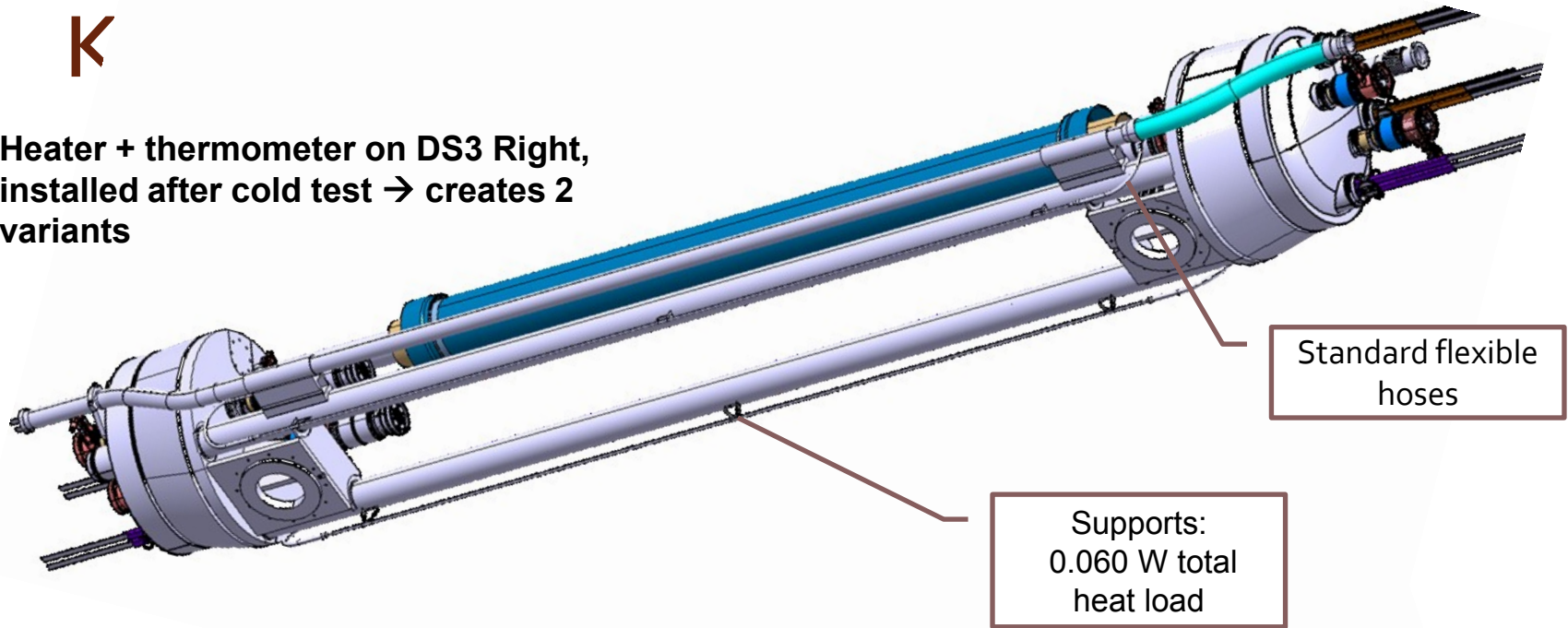


- He II free cross section:
  - **79 cm²** > specification: **60 cm²**

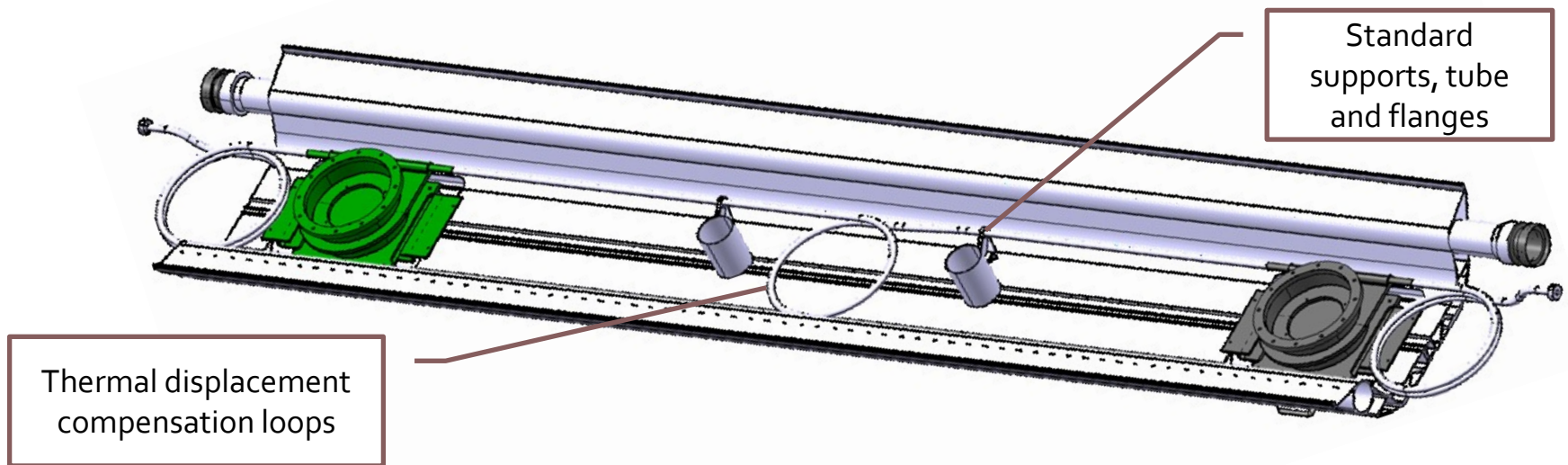


K

Heater + thermometer on DS3 Right,  
installed after cold test → creates 2  
variants



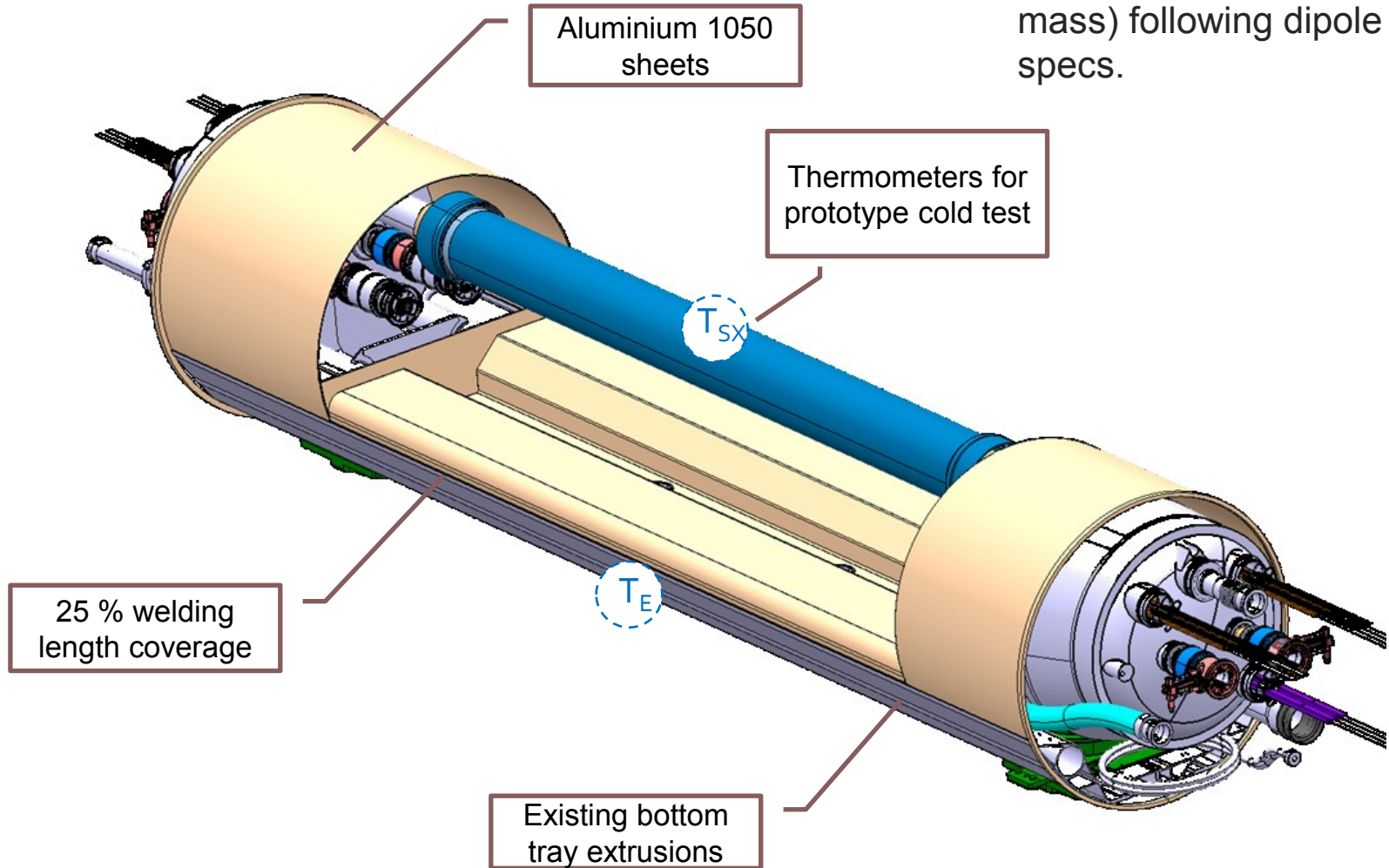
## C'-line: support post thermalisation





# Thermal shield

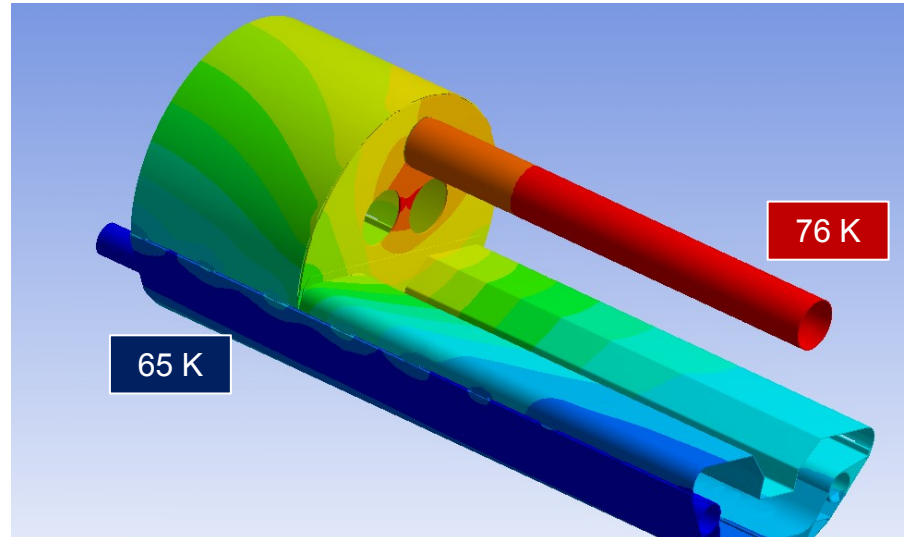
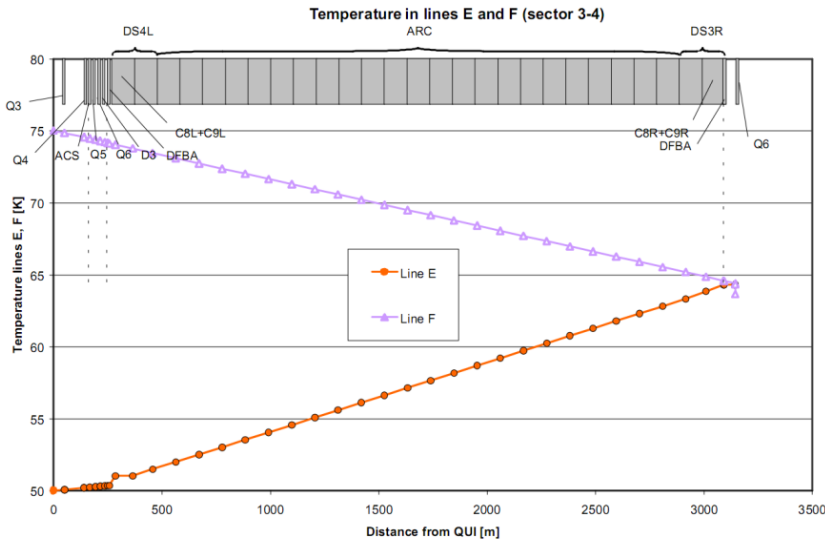
- Subcontracted design and fabrication of MLI blankets (including cold mass) following dipole specs.



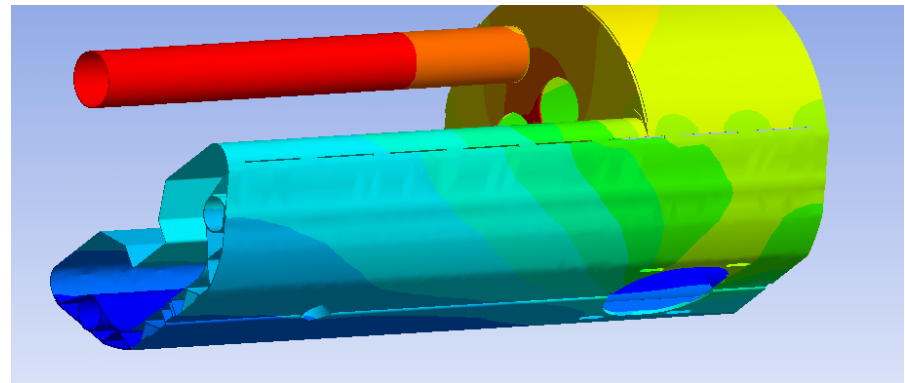
# Temperature gradient

- Heat loads
  - Radiation:  $1.5 \text{ W/m}^2$ (\*)
  - Supports:  $7.1 \text{ W}^{(**)}$  p/unit
  - CWT:  $6 \text{ W}$  p/unit
  - Total:  $52 \text{ W}$
- Cooling
  - $T_{\text{He}} = 65 \text{ K}$
  - $h = 489 \text{ W/m}^2 \text{ K}$
- 25% welding coverage
  - $\sim 2 \text{ K}$  increase wrt full welded length

Temperature profiles for sector 3-4 : lines E and F



assuming  $80\text{K} \rightarrow \sim 0.008 \text{ W/m}$ ,  $100\text{K} \rightarrow 0.020 \text{ W/m}$  to the X line enclosure pipe, w.r.t  $0.350 \text{ W/m}$  avg. static heat load in DS (R. van Weelderren)\*\*\*

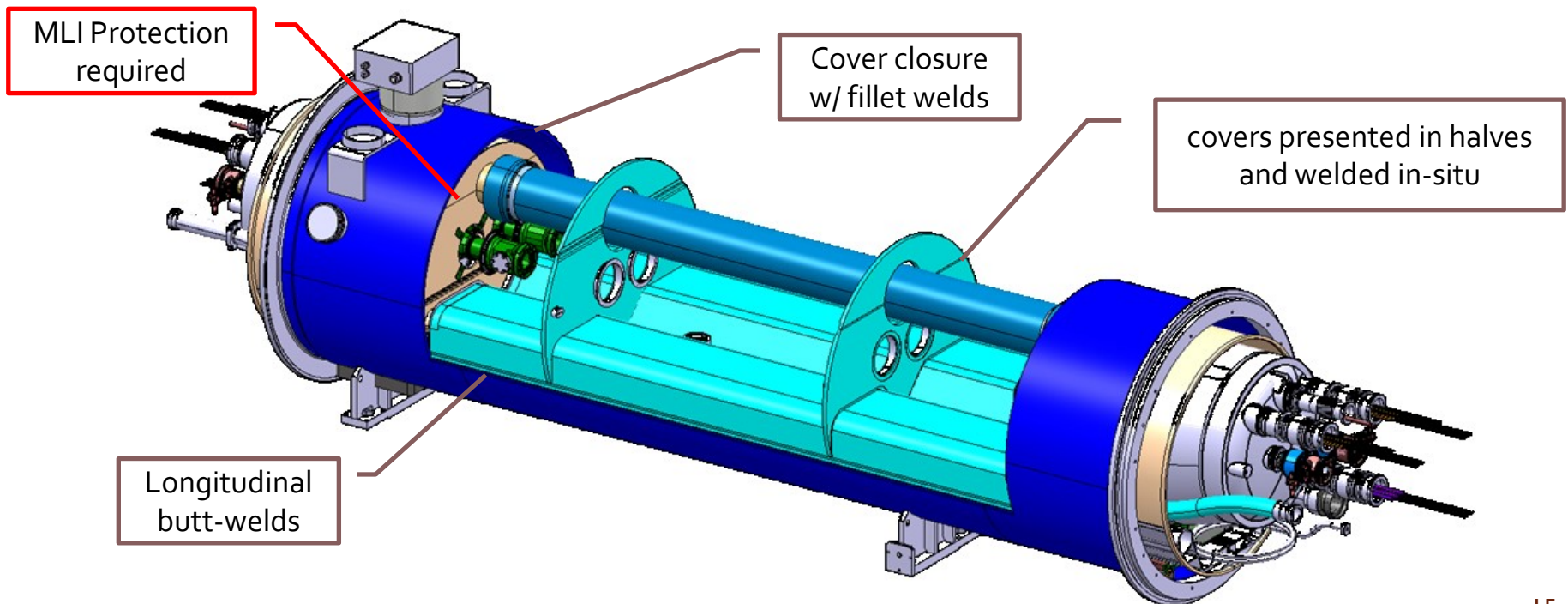


\* Typical heat load from 290K, MLI 30 layers, pressure < 1 mPa. average from DS3 and DS7 total load is  $1.2 \text{ W/m}^2$   
 \*\* M. Castoldi et al. LHC project report 335  
 \*\*\*Calculated without MLI, Al foil on cold surface ( $e=0.01$ ), Al shield as delivered ( $e=0.12$ ). Total heat load:  $0.020 \text{ W}$  (80K) static +  $0.420 \text{ W}$  dynamic (FLUKA, 10\$)

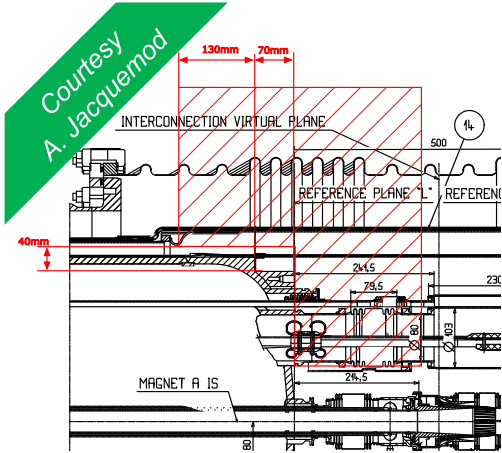
# Vacuum vessel design

An assembly challenge!

- Can only be finished after cryostating
- Dealing with **welding distortions** is a major issue
  - **Mock-up** under fabrication for welding tests
  - **Adjustment of cold mass supports** is required
  - Elaborated assembly procedure
- Material: magnetic shielding for collimator LVDT accuracy
  - Charpy test min. **27 J at -50 °C** test temperature (as LHC dipoles)
  - P355NL2 chosen for low temp. resilience and availability



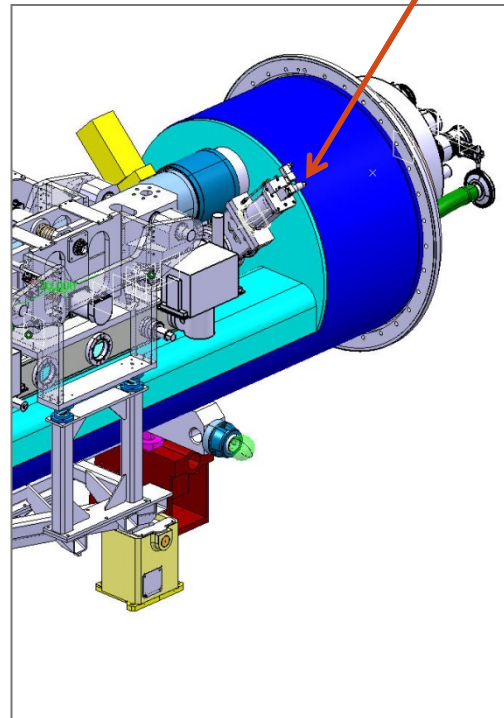
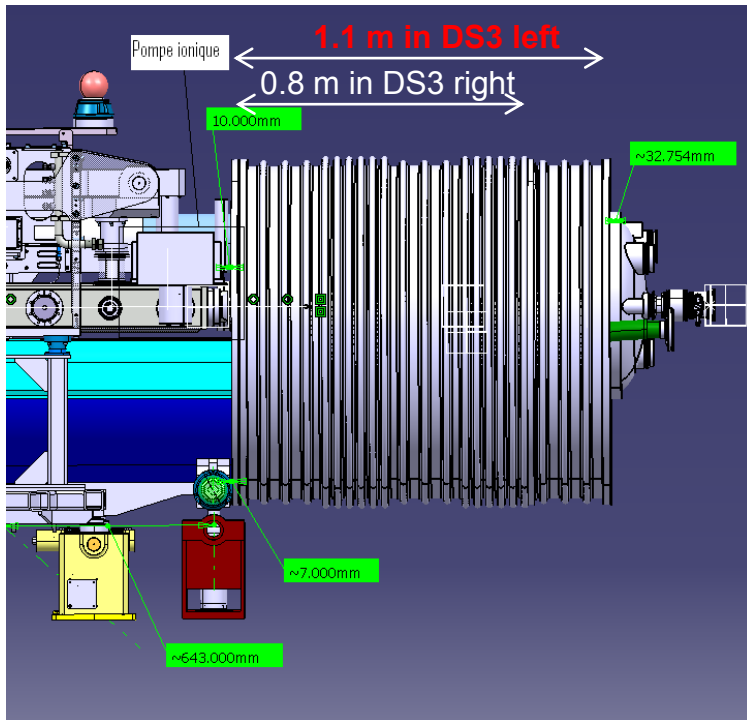
# Interconnect accessibility



Alternative support  
for the US welding  
machine required

All interconnect  
components remain  
standard

- Interference with sector valve
  - Valve actuator removed prior sleeve opening
  - Actuator removal test has proven the feasibility in closed position (W. Maan)

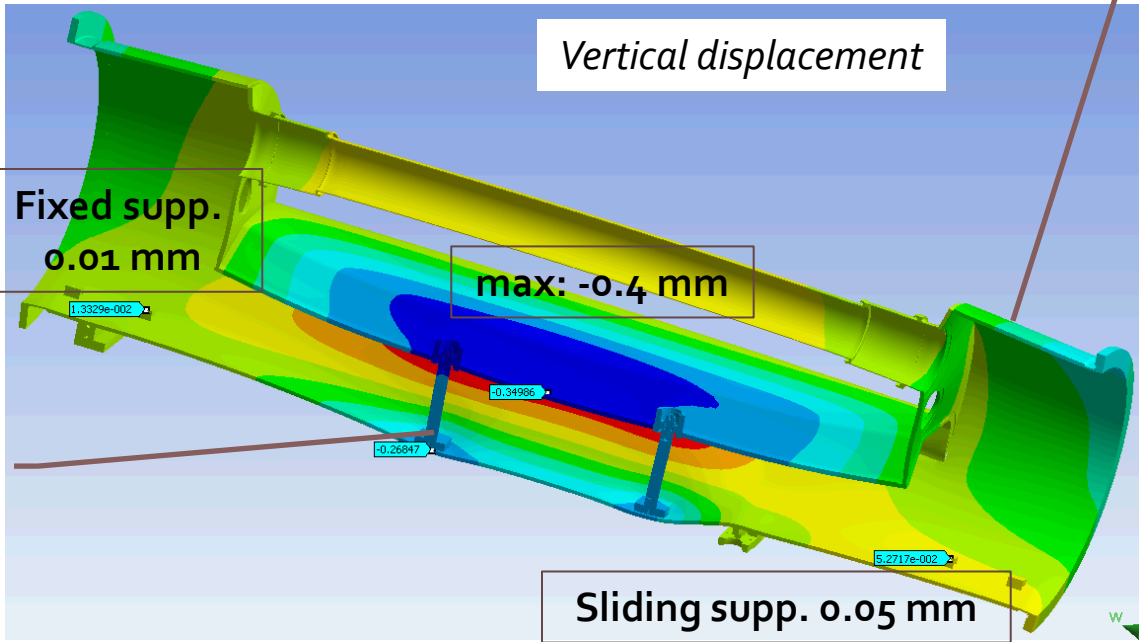


**Beam vacuum and  
insulation vacuum  
operations decoupled**

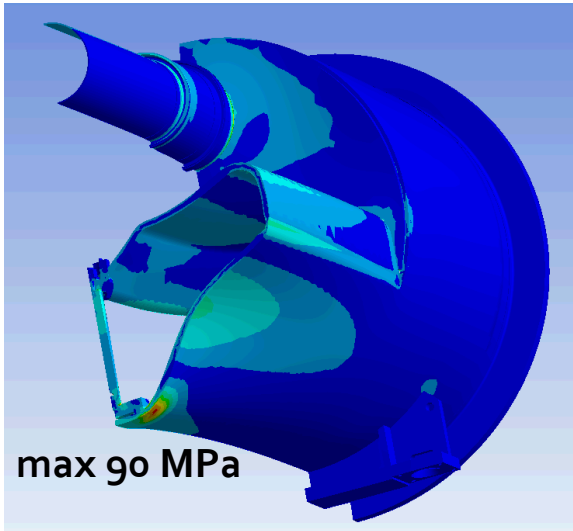
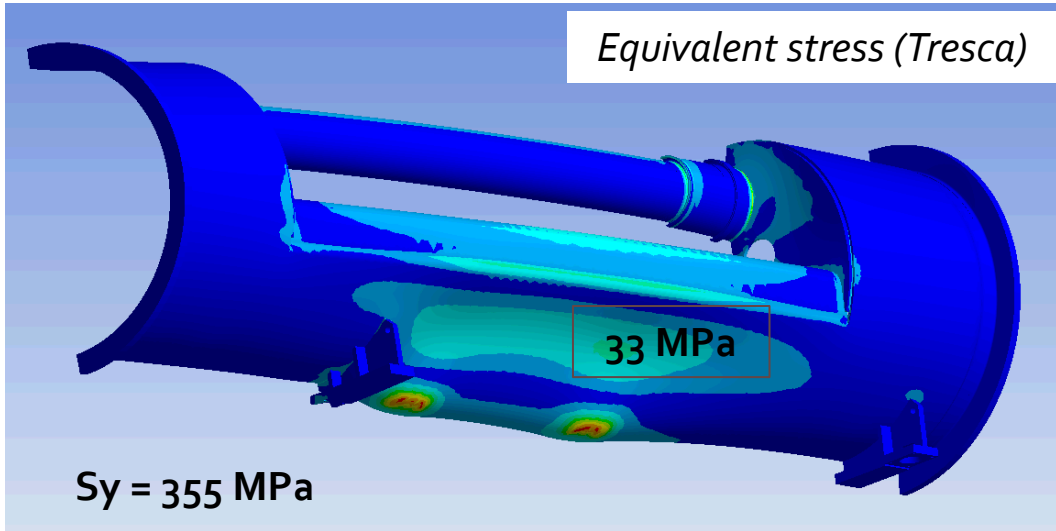


# Mechanical stability

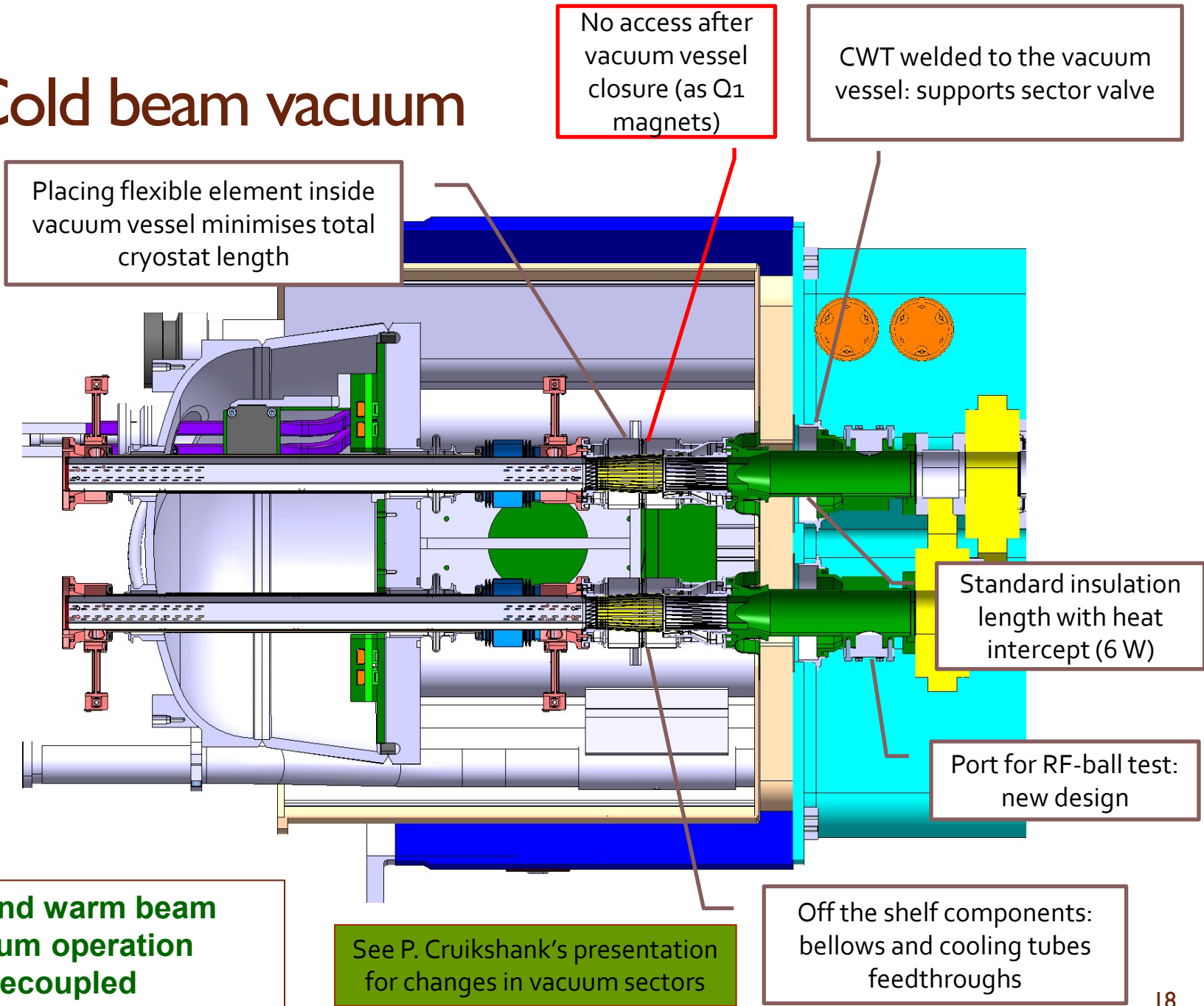
Cylindrical extremities for support base rigidity and flange flatness



Internal pillars to limit displacements



# Cold beam vacuum

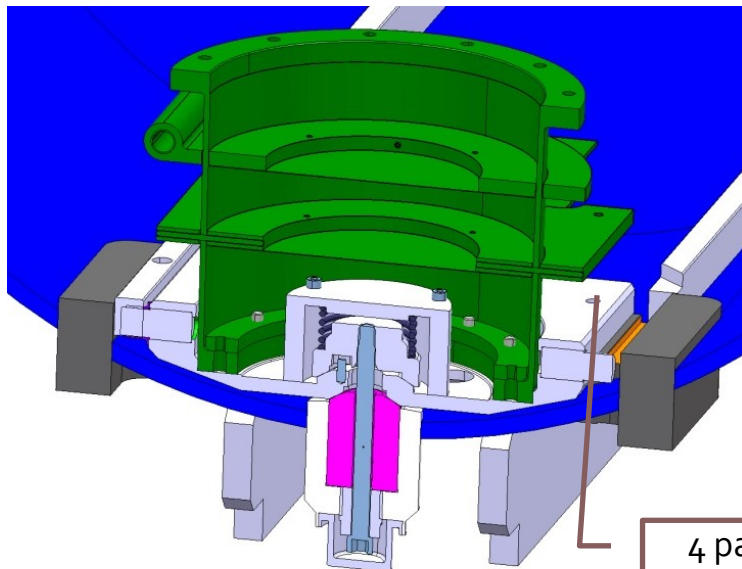


# Cold supports

Cold mass weight: ~1 ton

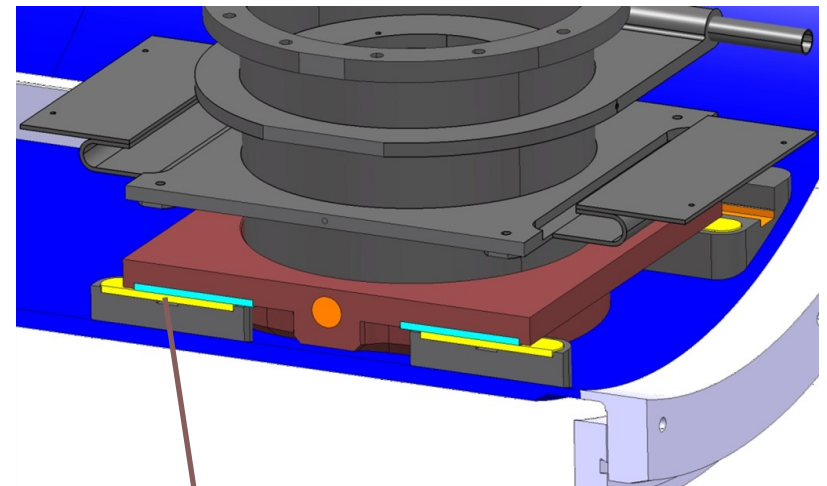
- Dipole type cold support posts
- Comparatively low cold mass weight (~5 kN/support):
  - Roll and lift must be restrained ( $|F_{\text{transv}}|=6.3 \text{ kN}$ ,  $M_{y,\text{max}}=5000 \text{ Nm}^*$ )
  - Support post additional inner ring for vertical restraint
- Compensation for displacements of support bases due to welding distortion
  - Intermediate base plates with angle adjustment

Fixed support



4 pairs of push/pull screws as anti-roll restraint ( $M_y$ )

Sliding support

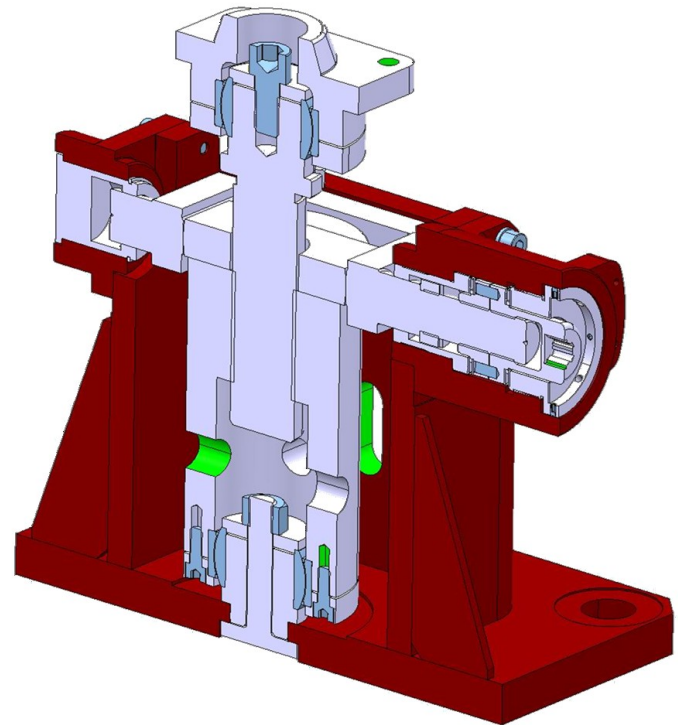
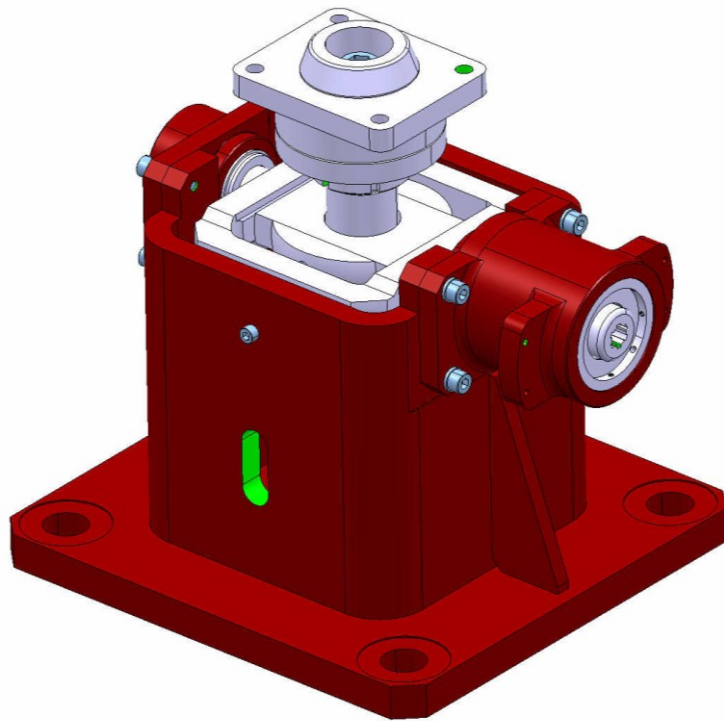


Sliding shims can be re-machined if needed

\* Per support post, including load safety factor 1.5

# Jacks

- Same alignment principle as LHC jacks
- Shorter design with additional **vertical restraint**
- Welded construction instead of forged block (small series)





# Remarks

- **Unique design** up to cold test, declines in 2 variants as installed (C' line circuit)
- Operation **independency of vacuum systems** is preserved
  - Sector valves between warm and cold beam vacuum
  - Insulation vacuum accessible with sector valves closed (but actuator must be demounted to open W sleeve)
  - RF-ball test of cold sectors possible without venting the collimator
- **Pressure limiting devices**
  - He volumes and lines: existing pressure relief valves in the QRL service modules
  - Beam vacuum: additional burst disks on SSS pumping ports
  - Insulation vacuum: DN200's on neighbouring dipoles
- **Flow and thermal continuity** of the cryogenic and vacuum systems is kept
- The design profits from **experience** with connection cryostats and DFBA shuffling modules
- **Busbar supports and insulation** design thoroughly studied

# Acknowledged challenges

- **Intricate assembly** procedure relying on good craftsmanship
- **Welding distortions** during vacuum vessel closure
- **MLI fire hazard** during vacuum vessel closure
- **Short gaps** between busbars insulation and He vessel walls (electrical insulation, damage during welding)
- **Access for repairs** may imply destruction of the vacuum vessel
- **Beam vacuum lines partly inaccessible** after cryostat closure
- **Cold test can reveal some possible defects but not all** (wear and fatigue damage, interaction with neighbouring magnets...)

- More detailed information
  - Edms hardware baseline
    - QTC <https://edms.cern.ch/nav/P:LHCPM001:V0/P:LHCPM065:V0>
    - TCLD <https://edms.cern.ch/nav/P:LHCPM001:V0/P:LHCPM076:V0>
  - Meeting minutes and working documents at

Project sharepoint site:

**[espace.cern.ch/dscollimator](https://espace.cern.ch/dscollimator)**

**Thank you for your attention!**