

# [HI-ECN3 BDF Target & target complex initial review]: Looking ahead – Target alternative designs

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# **HI-ECN3 BDF target initial review**

- Baseline design.
- > Alternative designs:
  - 1. Removed water channels.
  - 2. The full W target.
  - 3. The full W target exploring other options.
  - 4. In-beam tests

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Conclusions.



# WP3 – BDF Target design Baseline design



Target will become an extremely radioactive device! ~100 Sv/h after few hours of cool-down Baseline beam parameters of the BDF Target operation.

Proton momentum (GeV/c)	400
Beam intensity (p <sup>+</sup> /cycle)	$4 \times 10^{13}$
Cycle length (s)	7.2
Spill duration (s) ~ 4.0×10 <sup>10</sup> P <sup>13</sup>	1.0
Beam dilution pattern	Circular
Beam sweep frequency (turns/s)	4
Dilution circle radius (mm)	50
Beam sigma (H, V) (mm)	(8, 8)
Average beam power (kW)	356
Average beam power deposited in target (kW)	305
Average beam power during spill (MW)	2.3



Baseline design is robust with thorough design report
 <u>https://doi.org/10.23731/CYRM-2020-002</u>,
 representative in-beam tests, PIE plus HIP & other testing.

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# WP3 – BDF Alternative Target design requirements

### Now is an opportunity to explore alternative designs.

### **Physics drivers**

- Particle production •
  - Want particle interactions with High Z materials, especially in the shower region –large effect. W > TZM > Cu . -Replacing upstream TZM with W would be beneficial, even if this needs more cooling channels
    - Overall density of target (including water channels) is not so important
- Background signal •
  - Capture all electromagnetic shower particles in the target Need sufficient target ø and density •

### **Operations drivers**

- Activation products of water •
  - Reduce volume of water, especially in the beam & shower Production of Hydrogen

### Thermal management & engineering drivers

- Want lots of cooling channels in the shower region! (reduces overall p) •
- Want lots of high thermal conductivity materials in the shower region, eq copper (reduces  $\rho \& Z$ ) •
- Want to reduce target ø. •
- Want to reduce plate thicknesses (reduces overall p) •
- Want improved Tungsten grain structure ٠



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### Alternative design – proven concepts



![](_page_4_Picture_3.jpeg)

![](_page_4_Picture_4.jpeg)

![](_page_4_Picture_5.jpeg)

# WP3 – BDF Target design Alternative designs

 $\rightarrow$  Using what the section's learnt experience

![](_page_5_Figure_2.jpeg)

### **Drivers:**

- Reduce the amount radiolysis-produced free hydrogen gas (ATEX)
- Reduce activation of the water (less water) and of the target (less Ta), and decay heat (less Ta)
- Reduce contamination risk of water & W spallation products -(stronger and thicker external shroud instead of thin cladding)
- Shorter target will simplify waste packaging and disposal.
- Increase physics performance. (overall denser without water channels)

![](_page_5_Picture_9.jpeg)

# WP3 – BDF Target design Alternative design – Initial approach

1. Is it beneficial to have the blocks in contact or not?

2. Diluted or sweep beam?

**PREMATURE MODELS** with assumptions and simplifications

![](_page_6_Figure_3.jpeg)

... These options were explored in the 26<sup>th</sup> SHiP Collaboration Meeting, by T.Griesemer

![](_page_6_Picture_5.jpeg)

![](_page_7_Figure_0.jpeg)

with assumptions and simplifications Steady State + One Pulse 35mm centre beam

![](_page_7_Figure_2.jpeg)

PREMATURE MODELS

![](_page_7_Figure_3.jpeg)

Cooling water at circumference uses 10 000 W/m<sup>2</sup>.K calculated using original water flow rate of baseline.

Contact (perfectly bonded): the stress distribution along the beam axis is homogeneous. On average, the equivalent stresses are lower.

**Contact** (not

bonded)

- Contact (not bonded): High stress gradients in single blocks.
- Gap (not bonded): Higher temperatures, stress reduction is negligible compared to the perfectly bonded case.

 $\rightarrow$  Having the blocks bonded is best option

Gap

(not bonded)

![](_page_7_Picture_9.jpeg)

![](_page_7_Picture_10.jpeg)

**Contact** (perfectly

bonded)

## WP3 – BDF Target design Alternative design – TZM&W blocks, TZM shell

![](_page_8_Figure_1.jpeg)

![](_page_8_Picture_2.jpeg)

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**PREMATURE MODELS** with assumptions and simplifications

**PREMATURE MODELS** with assumptions and simplifications

# WP3 – BDF Target design

## Alternative design – Initial approach

- The sweep significantly reduces the peak temperature compared to the diluted beam (Δ200°C)
- The sweep reduces peak equivalent stresses by 70 MPa (down to 130 MPa) compared to diluted centrebeam

✓ It is beneficial to have the blocks in contact.
 ✓ The swept beam reduces the peak temperatures & stresses.
 How would a full W target behave using this design?...

![](_page_9_Figure_6.jpeg)

![](_page_9_Picture_7.jpeg)

## WP3 – BDF Target design Alternative design – The full W target

![](_page_10_Figure_1.jpeg)

![](_page_10_Picture_2.jpeg)

## Alternative design – The full W target

![](_page_11_Figure_2.jpeg)

- Full W compact target, encased in an actively cooled TZM shell.
- The TZM discs in the baseline design are replaced with W. Good for physics
- The water-cooling channels in the baseline design are removed. Good for operations
- To achieve efficient heat evacuation, the W slices and the TZM shell are diffusion bonded by means
  of hot isostatic pressing (HIP). better grain structure for mechanical properties
- The thickness of the W slices is limited to the maximum capability through cold rolling.

# WP3 – BDF Target design Alternative design – The full W target

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# Steady state simulations!

![](_page_12_Figure_3.jpeg)

![](_page_12_Picture_4.jpeg)

# WP3 – BDF Target design Alternative design – The full W target

A full W target core has improved physics performance... ..but the temperature in the W discs, and the beam-induced mechanical stresses must be reduced

- Currently, we are exploring alternatives to optimize the design of the full W target...

![](_page_13_Picture_3.jpeg)

Alternative design – The full W target (exploring other options)

![](_page_14_Figure_2.jpeg)

### Alternative designs: Full W core

![](_page_14_Figure_4.jpeg)

Single core W-target TZM

<u>shell</u> To improve the mechanical behavior in the W core.

#### W-target – Ta shell

To improve the mechanical behavior in the shell.

<u>W-target – TZM shell</u> <u>+ Upstream cooling</u> To reduce the upstream temperatures and therefore, beam-induced stresses.

![](_page_14_Picture_10.jpeg)

![](_page_14_Picture_11.jpeg)

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Alternative design – The full W target (exploring other options)

![](_page_15_Figure_2.jpeg)

Alternative design – The full W target (exploring other options)

![](_page_16_Figure_2.jpeg)

Alternative designs: Full W core with internal sheets

![](_page_16_Figure_4.jpeg)

<u>Gold sheets in peak energy</u> <u>density deposition</u> Enhance heat evacuation with two gold sheets in the location with the highest peak energy density deposition, while keeping the interaction length.

<u>1-mm Copper slices between</u> <u>each W sheet</u> Enhance the heat evacuation in the upstream of the target

#### The full Gold target

Enhance heat evacuation a full gold target while increasing the interaction length

![](_page_16_Picture_9.jpeg)

![](_page_16_Picture_10.jpeg)

Alternative design – The full W target (exploring other options)

![](_page_17_Figure_2.jpeg)

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Alternative design – The full W target (exploring other options)

![](_page_18_Figure_2.jpeg)

### <u>Ta pipe in the center with</u> <u>Water cooling</u> To enhance the heat evacuation by introducing a HIP Ta pipe in the center of the target.

#### **Copper insert in the center**

To conduct the heat towards the downstream of the target, where it could be evacuated by means of alternative cooling systems.

![](_page_18_Picture_6.jpeg)

![](_page_18_Picture_7.jpeg)

Alternative design – The full W target (exploring other options)

![](_page_19_Figure_2.jpeg)

![](_page_19_Picture_3.jpeg)

![](_page_19_Picture_4.jpeg)

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# WP3 – BDF. More Alternative Target designs -Helium cooling

W (non-clad) helium cooled, or mix of Helium and Water cooling

![](_page_20_Figure_2.jpeg)

#### Helium cooled blocks

- Removes need for cladding
  - In baseline design, Tantalum has high stress: residual from HIPing + thermal expansion in beam •
  - Tantalum bad for accident cases
- Allows higher next-to surface local coolant temperatures (no risk of boiling)
- -But HTC is lower than water
- -Added cooling system complexity and cost
- Studies are ongoing

![](_page_20_Picture_11.jpeg)

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![](_page_20_Picture_12.jpeg)

# **Target Alternative Designs testing**

Scaled representative target(s) will be tested in 400GeV beam in 2025. Using the Test Stand base, and design of Test Stand top from the Baseline test in 2024 Option exists to test multiple alternative designs in beam.

![](_page_21_Figure_2.jpeg)

Alternative options for test/stand in 2025

![](_page_21_Picture_4.jpeg)

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Device

## Conclusions

- > New alternative designs are being explored.
- > Target with increased W has improved physics
- > The elimination of the water cooling channels between the core discs:
  - High stresses in cladding & issues of water in beam (with water channels) will have to be balanced against higher W temperatures and stresses in W (without water channels)
- > The introduction of high thermal conductivity materials such as Copper or Gold:
  - > Promising to reduce the temperature within the core.
  - Issues of thermal expansion mismatch, gold has cost implication
- We are also exploring "exotic" designs, such as cooling from the centre, or with helium. These studies are in a preliminary phase and may not be viable.
- > Variations on beam sigma & sweep radius, and target diameter will also be explored.

![](_page_22_Picture_10.jpeg)

![](_page_23_Picture_0.jpeg)

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