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# Quark mixing model with $S_3$ modular symmetry and 3 Higgs doublets

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# Outline

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# Motivation

## Some background

- ▶ The Standard Model has been successful in describing interactions.
- ▶ There are issues such as the mixing pattern, neutrino masses, the composition of dark matter...
- ▶ A possible solution: extending the model with one or more symmetry groups.
- ▶ Finite permutation groups:  $S_3$  has provided a good approach to describe the mixing pattern.
- ▶ Finite groups based on modular symmetries have been proposed.

# Quark mixing matrix

$$V_{ckm} = \begin{pmatrix} V_{ud} & V_{us} & V_{ub} \\ V_{cd} & V_{cs} & V_{cb} \\ V_{td} & V_{ts} & V_{tb} \end{pmatrix}$$

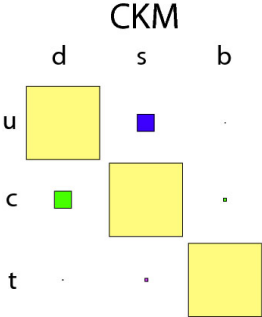


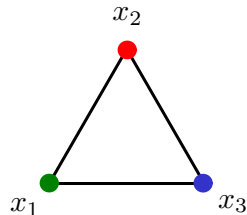
Figure 1: Quark mixing matrix pattern

# Symmetry groups: $S_3$ Group

## Permutation group of three elements

$$\begin{aligned}e &: \{x_1, x_2, x_3\} \rightarrow \{x_1, x_2, x_3\}, \\a_1 &: \{x_1, x_2, x_3\} \rightarrow \{x_2, x_1, x_3\}, \\a_2 &: \{x_1, x_2, x_3\} \rightarrow \{x_3, x_2, x_1\}, \\a_3 &: \{x_1, x_2, x_3\} \rightarrow \{x_1, x_3, x_2\}, \\a_4 &: \{x_1, x_2, x_3\} \rightarrow \{x_3, x_1, x_2\}, \\a_5 &: \{x_1, x_2, x_3\} \rightarrow \{x_2, x_3, x_1\},\end{aligned}$$

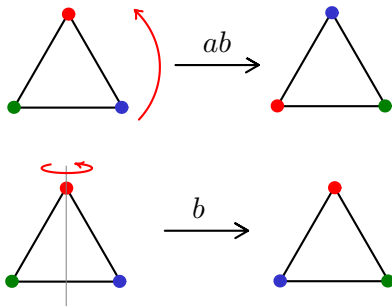
$$a_1 a_2 = a_5, \quad a_2 a_1 = a_4, \quad a_4 a_2 = a_2 a_1 a_2 = a_3.$$



If we redefine  $a_1 = a$  and  $a_2 = b$ , then all the elements of the group are defined as follows.

$$\{e, a, b, ab, ba, bab\}, \quad (1)$$

## Symmetry groups: $S_3$ Group



For the elements of  $S_3$ , it is also satisfied that

$$\begin{aligned} a^2 &= b^2 = (bab)^2 = \mathbf{1} \\ (ab)^3 &= (ba)^3 = \mathbf{1}, \end{aligned} \tag{2}$$

This allows us to group the elements into three conjugacy classes (identity, rotations, and reflections).

$$C_1 : \{e\} \quad C_2 : \{ab, ba\} \quad C_3 : \{a, b, bab\} \tag{3}$$

## Symmetry groups: $S_3$ Group

Matrix representation of  $S_3$

$$a = \begin{pmatrix} -1 & 0 \\ 0 & 1 \end{pmatrix}, \quad b = \begin{pmatrix} -\cos \theta & \sin \theta \\ \sin \theta & \cos \theta \end{pmatrix}, \quad bab = \begin{pmatrix} -\cos 2\theta & \sin 2\theta \\ \sin 2\theta & \cos 2\theta \end{pmatrix}, \quad (4)$$

$$ab = \begin{pmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{pmatrix}, \quad ba = \begin{pmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{pmatrix}, \quad e = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix},$$

## Modular Groups

The modular group is defined as

$$\Gamma = SL_2(\mathbb{Z}) = \left\{ \begin{pmatrix} a & b \\ c & d \end{pmatrix} \mid a, b, c, d \in \mathbb{Z}, ad - bc = 1 \right\}. \quad (5)$$

From this group, the fractional transformation is defined as

$$\Gamma(\tau) = \begin{pmatrix} a & b \\ c & d \end{pmatrix} (\tau) \rightarrow \frac{a\tau + b}{c\tau + d}. \quad (6)$$

with  $\begin{pmatrix} a & b \\ c & d \end{pmatrix} \in \Gamma$ .

The generators of  $\Gamma(\tau)$  are

$$S : \tau \rightarrow -\frac{1}{\tau} \quad \text{and} \quad T : \tau \rightarrow \tau + 1, \quad (7)$$

which in  $\Gamma$  correspond to

$$S = \begin{pmatrix} 0 & -1 \\ 1 & 0 \end{pmatrix} \quad \text{and} \quad T = \begin{pmatrix} 1 & 1 \\ 0 & 1 \end{pmatrix} \quad (8)$$

and satisfy in  $\Gamma$

$$S^2 = \mathbf{1} \quad \text{and} \quad (ST)^3 = \mathbf{1}. \quad (9)_{8/34}$$



## Modular Groups

The congruence subgroup is defined as

$$\Gamma(N) = \left\{ \begin{pmatrix} a & b \\ c & d \end{pmatrix} \in \Gamma : \begin{pmatrix} a & b \\ c & d \end{pmatrix} = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} \pmod{N} \right\}. \quad (10)$$

It is worth noting that

$$\bar{\Gamma} \simeq PSL_2(\mathbb{Z}) = SL_2(\mathbb{Z})/\{I, -I\}. \quad \text{and} \quad \bar{\Gamma}(N) \simeq \Gamma(N)/\{I, -I\} \quad (11)$$

The finite modular group is defined as

$$\Gamma_N \equiv \bar{\Gamma}/\bar{\Gamma}(N). \quad (12)$$

Some isomorphisms of the finite modular groups are

$$\begin{aligned} \Gamma_2 &\simeq S_3 & \Gamma_3 &\simeq A_4 \\ \Gamma_4 &\simeq S_4 & \Gamma_5 &\simeq A_5. \end{aligned} \quad (13)$$

It can be proof that

$$\begin{aligned} S^2 &= \mathbf{1} \\ (ST)^3 &= \mathbf{1} \\ T^N &= \mathbf{1}. \end{aligned} \quad (14)$$

# Modular Groups

$$\Gamma_2 \simeq S_3$$

$$S^2 = \mathbf{1}$$

$$(ST)^3 = \mathbf{1}$$

$$T^2 = \mathbf{1}.$$

$$a^2 = \mathbf{1}$$

$$(ab)^3 = \mathbf{1},$$

$$b^2 = \mathbf{1}$$

# Modular Groups

Under  $\bar{\Gamma}$ , modular forms of weight  $k$  are defined as holomorphic functions  $f(\tau)$  that satisfy

$$f(\tau) \rightarrow (c\tau + d)^k f(\tau), \quad (15)$$

forms of weight zero are invariant under  $\Gamma$ .

It can be shown that modular forms can be organized into multiplets that, under a finite group  $\bar{\Gamma}$ , transform as

$$\vec{f}(\tau) \rightarrow (c\tau + d)^k \rho(\gamma) \vec{f}(\tau), \quad (16)$$

where  $\rho(\gamma)$  is a unitary representation of  $\bar{\Gamma}$ .

# Elements for Model Construction

Extended the group with  $\Gamma_2$

$$SU(3)_C \times SU_L(2) \times U_y(1) \times \Gamma_2 \quad (17)$$

$$\phi \rightarrow (c\tau + d)^{k_\phi} \phi \quad (18)$$

It is assumed as a hypothesis that modular symmetry is a residual symmetry of a more fundamental group at low energies.

Fields are not modular forms.

# Elements for Model Construction

- ▶ Define the basis of  $S_3$ .
- ▶ Establish the assignments under  $S_3$  and the modular weights of the fields.
- ▶ Construct the modular forms of  $S_3$  with weight 2 and 4.
- ▶ Calculate the Lagrangian of the Yukawa sector.

## Base definition

Base of  $S_3$  for  $\theta = 4\pi/3$

$$\begin{aligned} e &= \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix}, & a &= \begin{pmatrix} -1 & 0 \\ 0 & 1 \end{pmatrix}, & b &= \begin{pmatrix} \frac{1}{2} & -\frac{\sqrt{3}}{2} \\ -\frac{\sqrt{3}}{2} & -\frac{1}{2} \end{pmatrix}, \\ ab &= \begin{pmatrix} -\frac{1}{2} & \frac{\sqrt{3}}{2} \\ -\frac{\sqrt{3}}{2} & -\frac{1}{2} \end{pmatrix}, & ba &= \begin{pmatrix} -\frac{1}{2} & -\frac{\sqrt{3}}{2} \\ \frac{\sqrt{3}}{2} & -\frac{1}{2} \end{pmatrix}, & bab &= \begin{pmatrix} \frac{1}{2} & \frac{\sqrt{3}}{2} \\ \frac{\sqrt{3}}{2} & -\frac{1}{2} \end{pmatrix}. \end{aligned} \quad (19)$$

Tensor products of  $S_3$

$$\begin{aligned} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix}_{\mathbf{2}} \otimes \begin{pmatrix} y_1 \\ y_2 \end{pmatrix}_{\mathbf{2}} &= (x_1y_1 + x_2y_2)_{\mathbf{1}} \oplus (x_1y_2 - x_2y_1)_{\mathbf{1}'} \oplus \begin{pmatrix} x_1y_2 + x_2y_1 \\ x_1y_1 - x_2y_2 \end{pmatrix}_{\mathbf{2}} \\ \begin{pmatrix} x_1 \\ x_2 \end{pmatrix}_{\mathbf{2}} \otimes (y')_{\mathbf{1}'} &= \begin{pmatrix} -x_2y' \\ x_1y' \end{pmatrix}_{\mathbf{2}} \\ (x')_{\mathbf{1}'} \otimes (y')_{\mathbf{1}'} &= (x'y')_{\mathbf{1}}. \end{aligned} \quad (20)$$

# Higgs potential

Three Higgs doublets potential invariant under  $S_3$

$$\begin{aligned} V = & \mu_1^2 \left( H_1^\dagger H_1 + H_2^\dagger H_2 \right) + \mu_0^2 \left( H_s^\dagger H_s \right) + \frac{a}{2} \left( H_s^\dagger H_s \right)^2 + b \left( H_s^\dagger H_s \right) \left( H_1^\dagger H_1 + H_2^\dagger H_2 \right) \\ & + \frac{c}{2} \left( H_1^\dagger H_1 + H_2^\dagger H_2 \right)^2 + \frac{d}{2} \left( H_1^\dagger H_2 - H_2^\dagger H_1 \right)^2 + e f_{ijk} \left( \left( H_s^\dagger H_i \right) \left( H_j^\dagger H_k \right) + h.c. \right) \\ & + f \left\{ \left( H_s^\dagger H_1 \right) \left( H_1^\dagger H_s \right) + \left( H_s^\dagger H_2 \right) \left( H_2^\dagger H_s \right) \right\} + \frac{g}{2} \left\{ \left( H_1^\dagger H_1 - H_2^\dagger H_2 \right)^2 + \left( H_1^\dagger H_2 + H_2^\dagger H_1 \right)^2 \right\} \\ & + \frac{h}{2} \left\{ \left( H_s^\dagger H_1 \right) \left( H_s^\dagger H_1 \right) + \left( H_s^\dagger H_2 \right) \left( H_s^\dagger H_2 \right) + \left( H_1^\dagger H_s \right) \left( H_1^\dagger H_s \right) + \left( H_2^\dagger H_s \right) \left( H_2^\dagger H_s \right) \right\}; \end{aligned} \quad (21)$$

$$v_1^2 = 3v_2^2,$$

where the VEVs are denoted as

$$\langle 0 | H_1 | 0 \rangle = \frac{1}{\sqrt{2}} v_1; \quad \langle 0 | H_2 | 0 \rangle = \frac{1}{\sqrt{2}} v_2; \quad \langle 0 | H_s | 0 \rangle = \frac{1}{\sqrt{2}} v_3, \quad (22)$$

## Assignments in $S_3$ and modular weights

	$(Q_1, Q_2)$	$(q_1, q_2)$	$Q_3$	$q_3$
$SU(2)$	2	1	2	1
$S_3$	2	2	1	1
$k$	-2	-2	0	0
	$(H_1, H_2)$	$H_s$	$(Y_1^{2(4)}(\tau), Y_2^{2(4)}(\tau))$	$Y_s^{(4)}(\tau)$
$SU(2)$	2	2	1	1
$S_3$	2	1	2	1
$k$	0	0	2(4)	4

**Table 1:** Charges, assignments, and modular weights of  $SU(2)$  and  $S_3$ . The superindex (4) on the modular forms indicates that they are of modular weight 4. The subindex  $s$  indicates that it is the symmetric singlet of the modular form of weight 4.



## Modular forms in $S_3$

The modular forms will be constructed from the following expression.

$$\sum_i \frac{d}{d\tau} \log f_i(\tau) \rightarrow \sum_i (c\tau + d)k_i c + \sum_i (c\tau + d)^2 \frac{d}{d\tau} \log f_i(\tau). \quad (23)$$

A useful type of modular form is

$$\eta(\tau) = q^{1/24} \prod_{n=1}^{\infty} (1 - q^n), \quad q = e^{2\pi i\tau} \quad (24)$$

## Modular forms in $S_3$

Under the generators of the modular group,  $\eta(\tau)$  transforms as

Under T

$$\begin{aligned}\eta(2\tau) &\rightarrow e^{i\pi/6}\eta(2\tau), \\ \eta(\tau/2) &\rightarrow \eta((\tau + 1)/2), \\ \eta((\tau + 1)/2) &\rightarrow e^{i\pi/12}\eta(\tau/2).\end{aligned}\tag{25}$$

Under S

$$\begin{aligned}\eta(2\tau) &\rightarrow \sqrt{-i\tau/2}\eta(\tau/2), \\ \eta(\tau/2) &\rightarrow \sqrt{-i3\tau}\eta(2\tau), \\ \eta((\tau + 1)/2) &\rightarrow e^{-i\pi/12}\sqrt{-i\tau}\eta((\tau + 1)/2).\end{aligned}\tag{26}$$

## Modular Forms in $S_3$

The general modular form in terms of the functions  $\eta(\tau)$  can be written as

$$Y(\alpha, \beta, \gamma|\tau) = \frac{d}{d\tau} \left( \alpha \log \eta \left( \frac{\tau}{2} \right) + \beta \log \eta \left( \frac{\tau+1}{2} \right) + \gamma \log \eta(2\tau) \right), \quad (27)$$

which satisfies

$$\begin{aligned} \alpha + \beta + \gamma &= 0 \\ Y(\alpha, \beta, \gamma|\tau) &\xrightarrow{S} \tau^2 Y(\gamma, \beta, \alpha|\tau) \\ Y(\alpha, \beta, \gamma|\tau) &\xrightarrow{T} Y(\beta, \alpha, \gamma|\tau) \end{aligned} \quad (28)$$

with the generators of  $S_3$  for the representation **2**

$$\rho(S) = \frac{1}{2} \begin{pmatrix} 1 & -\sqrt{3} \\ -\sqrt{3} & -1 \end{pmatrix}, \quad \rho(T) = \begin{pmatrix} -1 & 0 \\ 0 & 1 \end{pmatrix}, \quad (29)$$

## Modular Forms in $S_3$

The system of equations generated by is solved

$$\begin{aligned}\alpha + \beta + \gamma &= 0 \\ Y(S\tau) &= Y(-1/\tau) = \tau^2 \rho(S) Y(\tau) \\ Y(T\tau) &= Y(\tau + 1) = \rho(T) Y(\tau)\end{aligned}\tag{30}$$

The modular forms of weight 2 for  $S_3$ , with  $C_1 = i/2\pi$ , are

$$\begin{aligned}Y_1(\tau) &= \frac{\sqrt{3}i}{4\pi} \left( \frac{\eta'(\tau/2)}{\eta(\tau/2)} - \frac{\eta'((\tau+1)/2)}{\eta((\tau+1)/2)} \right), \\ Y_2(\tau) &= \frac{i}{4\pi} \left( \frac{\eta'(\tau/2)}{\eta(\tau/2)} + \frac{\eta'((\tau+1)/2)}{\eta((\tau+1)/2)} - \frac{8\eta'(2\tau)}{\eta(2\tau)} \right),\end{aligned}\tag{31}$$

$$\begin{pmatrix} Y_1 \\ Y_2 \end{pmatrix} \otimes \begin{pmatrix} Y_1 \\ Y_2 \end{pmatrix} = Y_s^{(4)} + \begin{pmatrix} Y_1^{(4)} \\ Y_2^{(4)} \end{pmatrix},$$

$$\begin{aligned}Y_s^{(4)} &= Y_1^2 + Y_2^2 \\ Y_1^{(4)} &= 2Y_1 Y_2 \\ Y_2^{(4)} &= Y_1^2 - Y_2^2.\end{aligned}$$

## Yukawa Sector

To compress the notation, the doublets of  $S_3$  can be redefined as

$$Q = \begin{pmatrix} \bar{Q}_1 \\ \bar{Q}_2 \end{pmatrix}; \quad u = \begin{pmatrix} u_{1R} \\ u_{2R} \end{pmatrix}; \quad H = \begin{pmatrix} H_1 \\ H_2 \end{pmatrix}; \quad Y^{(4)} = \begin{pmatrix} Y_1^{(4)} \\ Y_2^{(4)} \end{pmatrix}; \quad Y^{(2)} = \begin{pmatrix} Y_1^{(2)} \\ Y_2^{(2)} \end{pmatrix};$$

Thus, the Lagrangian in the Yukawa sector is

$$\begin{aligned} \mathcal{L}_y^{(u)} = & C_1 \bar{Q} \otimes u \otimes \tilde{H} \otimes Y^{(4)} + C_2 \bar{Q} \otimes u \otimes \tilde{H} \otimes Y_s^{(4)} \\ & + C_3 \bar{Q} \otimes u \otimes \tilde{H}_s \otimes Y^{(4)} + C_4 \bar{Q} \otimes u \otimes \tilde{H}_s \otimes Y_s^{(4)} \\ & + C_5 \bar{Q} \otimes u_{3R} \otimes \tilde{H} \otimes Y^{(2)} + C_6 \bar{Q} \otimes u_{3R} \otimes \tilde{H}_s \otimes Y^{(2)} \\ & + C_7 \bar{Q}_3 \otimes u \otimes \tilde{H} \otimes Y^{(2)} + C_8 \bar{Q}_3 \otimes u \otimes \tilde{H}_s \otimes Y^{(2)} \\ & + C_9 \bar{Q}_3 \otimes u_{3R} \otimes \tilde{H}_s + \text{h.c.} \end{aligned} \tag{32}$$

Only the  $S_3$  invariant terms are allowed, and their modular weight must be zero.

# Yukawa Sector

## Matrix elements

$$\begin{aligned}M_{11}^{(u)} &= (\alpha + \gamma)v_1Y_1^{(4)} + (\alpha - \gamma)v_2Y_2^{(4)} + C_2v_2Y_s^{(4)} + C_3v_sY_2^{(4)} + C_4v_sY_s^{(4)} \\M_{12}^{(u)} &= (\beta + \gamma)v_2Y_1^{(4)} + (\gamma - \beta)v_1Y_2^{(4)} + C_2v_1Y_s^{(4)} + C_3v_sY_1^{(4)} \\M_{13}^{(u)} &= C_5(v_2Y_1^{(2)} + v_1Y_2^{(2)}) + C_6v_sY_1^{(2)} \\M_{21}^{(u)} &= (\beta + \gamma)v_1Y_2^{(4)} + (\gamma - \beta)v_2Y_1^{(4)} + C_2v_1Y_s^{(4)} + C_3v_sY_1^{(4)} \\M_{22}^{(u)} &= (\alpha + \gamma)v_2Y_2^{(4)} + (\alpha - \gamma)v_1Y_1^{(4)} - C_2v_2Y_s^{(4)} - C_3v_sY_2^{(4)} + C_4v_sY_s^{(4)} \\M_{23}^{(u)} &= C_5(v_1Y_1^{(2)} - v_2Y_2^{(2)}) + C_6v_sY_2^{(2)} \\M_{31}^{(u)} &= C_7(v_2Y_1^{(2)} + v_1Y_2^{(2)}) + C_8v_sY_1^{(2)} \\M_{32}^{(u)} &= C_7(v_1Y_1^{(2)} - v_2Y_2^{(2)}) + C_8v_sY_2^{(2)} \\M_{33}^{(u)} &= C_9v_s.\end{aligned}\tag{33}$$

In this model, the free parameters are  $v_1$ ,  $v_2$ ,  $v_s$ ,  $\alpha$ ,  $\beta$ ,  $\gamma$ ,  $C_2$ ,  $C_3$ ,  $C_4$ ,  $C_5$ ,  $C_6$ ,  $C_7$ ,  $C_8$ ,  $C_9$  y  $\tau$ ,

## $V_{CKM}$ Matrix

The goal is to construct a matrix of the form

$$\begin{pmatrix} 0 & a & 0 \\ a^* & b & c \\ 0 & c^* & d \end{pmatrix}, \quad (34)$$

Known as texture zeros.

To satisfy this form in the mass matrix, the following conditions must be imposed

$$M_{11} = 0 \quad M_{12} = M_{21}^* \quad M_{32} = M_{23}^* \quad M_{13} = M_{31} = 0. \quad (35)$$

$$\begin{aligned} M_{13}^{(u)} &= C_5(v_2 Y_1^{(2)} + v_1 Y_2^{(2)}) + C_6 v_s Y_1^{(2)} = 0, \\ M_{31}^{(u)} &= C_7(v_2 Y_1^{(2)} + v_1 Y_2^{(2)}) + C_8 v_s Y_1^{(2)} = 0, \end{aligned} \quad (36)$$

Using the relation from the minimization of the Higgs potential

$$Y_2^{(2)}(\tau) - \sqrt{3}Y_1^{(2)}(\tau) = 0. \quad (37)$$

## $V_{CKM}$ Matrix

We make the texture zeros matrix if

$$\begin{array}{lll} \operatorname{Re}(\beta) = 0 & C_3 = 0 & \gamma = -(1/2)(v_s/v_2)C_4 \\ \alpha = -C_2 \in \mathbb{R} & C_6 = -4(v_2/v_s)C_5 & C_8 = -4(v_2/v_s)C_7 \\ C_5 = C_7^* & \tau = i & C_9, v_{1,2}, v_s \in \mathbb{R} \end{array}$$

For  $\tau = i$  we have

$$y_2 = \sqrt{3}y_1 \quad y_1^{(4)} = 2\sqrt{3}y_1^2 \quad y_2^{(4)} = -2y_1^2 \quad y_s^{(4)} = 4y_1^2, \quad (38)$$

with  $y_k = Y_k(i)$ . The mass matrix takes the form.

For simplify the notation, we have defined the parameters as

$$\begin{aligned} C' &= 4\sqrt{3}v_2y_1^2(C_2 + \beta), \\ C'_4 &= 8y_1^2(C_4v_s - C_2v_2), \\ C'_5 &= -4\sqrt{3}v_2y_1C_5, \\ C'_9 &= C_9v_s \end{aligned} \quad M^{(u)} = \begin{pmatrix} 0 & C' & 0 \\ C'^* & C'_4 & C'_5 \\ 0 & C'_5^* & C'_9 \end{pmatrix}, \quad (39)$$



The information about the phase is extracted through the matrix

$$P_f = \text{diag}(1, e^{i\phi_1}, e^{i(\phi_1 - \phi_2)}) \quad (40)$$

where  $\phi_1$  is  $C'$  phase and  $\phi_2$  is  $C'_5$  phase.

$$M^{(u)} = P_f^\dagger \bar{M}^{(u)} P_f, \quad (41)$$

Therefore,

$$\bar{M}^{(u)} = \begin{pmatrix} 0 & |C| & 0 \\ |C| & C'_4 & |C'_5| \\ 0 & |C'_5| & C'_9 \end{pmatrix}, \quad (42)$$

## $V_{CKM}$ Matrix

If we relate the mass matrix  $M_D = \text{diag}(\tilde{\sigma}_1, -\tilde{\sigma}_2, 1)$  and using the invariants of a matrix, one obtains

$$|C| = \sqrt{\frac{\tilde{\sigma}_1 \tilde{\sigma}_2}{C'_9}}$$

$$C'_4 = (\tilde{\sigma}_1 - \tilde{\sigma}_2 + 1 - C'_9) \quad (43)$$

$$|C'_5| = \sqrt{\frac{(1 - C'_9)(C'_9 - \tilde{\sigma}_1)(C'_9 + \tilde{\sigma}_2)}{C'_9}}.$$

where  $\tilde{\sigma}_i = \sigma_i/\sigma_3$ , con  $i = 1, 2$ .

This calculation applies to both up and down quarks.

# $V_{CKM}$ Matrix

$$\begin{aligned}
 V_{ud}^{th} &= \sqrt{\frac{\tilde{\sigma}_c \tilde{\sigma}_s \xi_1^u \xi_1^d}{\mathcal{D}_{1u} \mathcal{D}_{1d}}} + \sqrt{\frac{\tilde{\sigma}_u \tilde{\sigma}_d}{\mathcal{D}_{1u} \mathcal{D}_{1d}}} \left( \sqrt{(1-\delta_u)(1-\delta_d)} \xi_1^u \xi_1^d + \sqrt{\delta_u \delta_d \xi_2^u \xi_2^d} e^{i\phi_2} \right) e^{i\phi_1}, \\
 V_{us}^{th} &= -\sqrt{\frac{\tilde{\sigma}_c \tilde{\sigma}_d \xi_1^u \xi_2^d}{\mathcal{D}_{1u} \mathcal{D}_{2d}}} + \sqrt{\frac{\tilde{\sigma}_u \tilde{\sigma}_s}{\mathcal{D}_{1u} \mathcal{D}_{2d}}} \left( \sqrt{(1-\delta_u)(1-\delta_d)} \xi_1^u \xi_2^d + \sqrt{\delta_u \delta_d \xi_2^u \xi_1^d} e^{i\phi_2} \right) e^{i\phi_1}, \\
 V_{ub}^{th} &= \sqrt{\frac{\tilde{\sigma}_c \tilde{\sigma}_d \tilde{\sigma}_s \delta_d \xi_1^u}{\mathcal{D}_{1u} \mathcal{D}_{3d}}} + \sqrt{\frac{\tilde{\sigma}_u}{\mathcal{D}_{1u} \mathcal{D}_{3d}}} \left( \sqrt{(1-\delta_u)(1-\delta_d)} \delta_d \xi_1^u - \sqrt{\delta_u \xi_2^u \xi_1^d \xi_2^d} e^{i\phi_2} \right) e^{i\phi_1}, \\
 V_{cd}^{th} &= -\sqrt{\frac{\tilde{\sigma}_u \tilde{\sigma}_s \xi_2^u \xi_1^d}{\mathcal{D}_{2u} \mathcal{D}_{1d}}} + \sqrt{\frac{\tilde{\sigma}_c \tilde{\sigma}_d}{\mathcal{D}_{2u} \mathcal{D}_{1d}}} \left( \sqrt{(1-\delta_u)(1-\delta_d)} \xi_2^u \xi_1^d + \sqrt{\delta_u \delta_d \xi_1^u \xi_2^d} e^{i\phi_2} \right) e^{i\phi_1}, \\
 V_{cs}^{th} &= \sqrt{\frac{\tilde{\sigma}_u \tilde{\sigma}_d \xi_2^u \xi_2^d}{\mathcal{D}_{2u} \mathcal{D}_{2d}}} + \sqrt{\frac{\tilde{\sigma}_c \tilde{\sigma}_s}{\mathcal{D}_{2u} \mathcal{D}_{2d}}} \left( \sqrt{(1-\delta_u)(1-\delta_d)} \xi_2^u \xi_2^d + \sqrt{\delta_u \delta_d \xi_1^u \xi_1^d} e^{i\phi_2} \right) e^{i\phi_1}, \\
 V_{cb}^{th} &= -\sqrt{\frac{\tilde{\sigma}_u \tilde{\sigma}_d \tilde{\sigma}_s \delta_d \xi_2^u}{\mathcal{D}_{2u} \mathcal{D}_{3d}}} + \sqrt{\frac{\tilde{\sigma}_c}{\mathcal{D}_{2u} \mathcal{D}_{3d}}} \left( \sqrt{(1-\delta_u)(1-\delta_d)} \delta_d \xi_2^u - \sqrt{\delta_u \xi_1^u \xi_1^d \xi_2^d} e^{i\phi_2} \right) e^{i\phi_1}, \\
 V_{td}^{th} &= \sqrt{\frac{\tilde{\sigma}_u \tilde{\sigma}_c \tilde{\sigma}_s \delta_u \xi_1^d}{\mathcal{D}_{3u} \mathcal{D}_{1d}}} + \sqrt{\frac{\tilde{\sigma}_d}{\mathcal{D}_{3u} \mathcal{D}_{1d}}} \left( \sqrt{\delta_u (1-\delta_u)(1-\delta_d)} \xi_1^d - \sqrt{\delta_d \xi_1^u \xi_2^u \xi_2^d} e^{i\phi_2} \right) e^{i\phi_1}, \\
 V_{ts}^{th} &= -\sqrt{\frac{\tilde{\sigma}_u \tilde{\sigma}_c \tilde{\sigma}_d \delta_u \xi_2^d}{\mathcal{D}_{3u} \mathcal{D}_{2d}}} + \sqrt{\frac{\tilde{\sigma}_s}{\mathcal{D}_{3u} \mathcal{D}_{2d}}} \left( \sqrt{\delta_u (1-\delta_u)(1-\delta_d)} \xi_2^d - \sqrt{\delta_d \xi_1^u \xi_2^u \xi_1^d} e^{i\phi_2} \right) e^{i\phi_1}, \\
 V_{tb}^{th} &= \sqrt{\frac{\tilde{\sigma}_u \tilde{\sigma}_c \tilde{\sigma}_d \tilde{\sigma}_s \delta_u \delta_d}{\mathcal{D}_{3u} \mathcal{D}_{3d}}} + \left( \sqrt{\frac{\xi_1^u \xi_2^u \xi_1^d \xi_2^d}{\mathcal{D}_{3u} \mathcal{D}_{3d}}} + \sqrt{\frac{\delta_u \delta_d (1-\delta_u)(1-\delta_d)}{\mathcal{D}_{3u} \mathcal{D}_{3d}}} e^{i\phi_2} \right) e^{i\phi_1}.
 \end{aligned} \tag{44}$$

where it has been defined

$$\begin{aligned}\delta_{u,d} &= 1 - C'_{9u,d} \\ \xi_1^{u,d} &= 1 - \tilde{\sigma}_{u,d} - \delta_{u,d}, \\ \xi_2^{u,d} &= 1 + \tilde{\sigma}_{c,s} - \delta_{u,d}, \\ \mathcal{D}_{1(u,d)} &= (1 - \delta_{u,d})(\tilde{\sigma}_{u,d} + \tilde{\sigma}_{c,s})(1 - \tilde{\sigma}_{u,d}), \\ \mathcal{D}_{2(u,d)} &= (1 - \delta_{u,d})(\tilde{\sigma}_{u,d} + \tilde{\sigma}_{c,s})(1 + \tilde{\sigma}_{c,s}), \\ \mathcal{D}_{3(u,d)} &= (1 - \delta_{u,d})(1 - \tilde{\sigma}_{u,d})(1 + \tilde{\sigma}_{c,s}).\end{aligned}\tag{45}$$

## $V_{CKM}$ Matrix

The comparison is made with the  $\chi^2$  function defined as

$$\chi^2 = \sum_{i=u,c,t} \sum_{j=d,s,b} \frac{(|V_{ij}^{\text{th}}| - |V_{ij}|)^2}{\sigma_{V_{ij}}^2} \quad (46)$$

Parameters	Values in the fit
$C'_{9u}$	0.816393
$C'_{9d}$	0.828604
$\phi_{1u}$	1.63797
$\phi_{1d}$	0
$\phi_{2u}$	0.0981477
$\phi_{2d}$	0
$\chi^2$	0.00070

**Table 2:** Values of the free parameters for the adjustment with the values of the ratios of the masses fixed in their central value and the respective obtaining of  $\chi^2$ .

## Matriz $V_{CKM}$

VCKM matrix for this fit

$$V_{CKM}^{th} = \begin{pmatrix} 0.97435 & 0.2250 & 0.00369 \\ 0.22486 & 0.97349 & 0.04182 \\ 0.00857 & 0.04110 & 0.999118 \end{pmatrix}, \quad (47)$$

# Conclusions and Perspectives

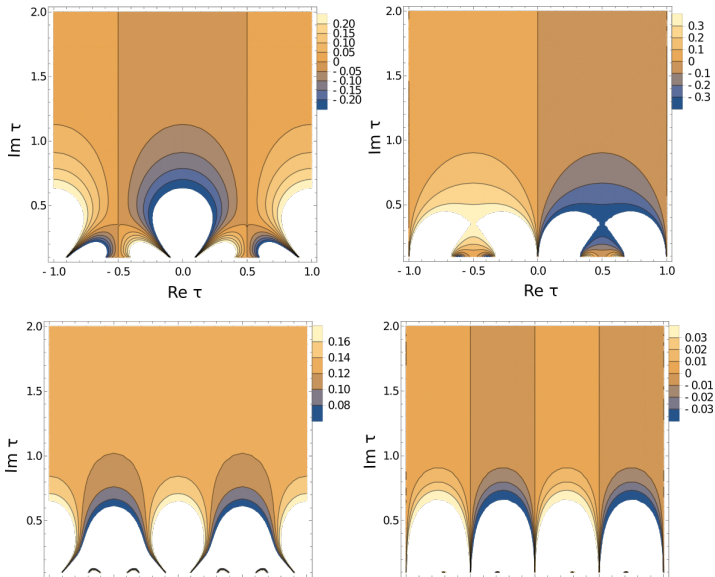
- ▶ When we use  $S_3$  (alone) it's difficult to obtain a proper  $V_{ckm}$  matrix. However, with  $S_3$  derived from a modular symmetry the constraints vanish and we obtain an accurate  $V_{ckm}$  matrix.
- ▶ In this framework, the Yukawa's are modular functions that can be obtained from the modular symmetry.
- ▶ It is possible to test other assignments or symmetry groups based on modular symmetry.
- ▶ New models can be constructed by combining some symmetry groups and modular groups.

Thank you for your attention!!!



# Modular forms in $S_3$

Real and imaginary part of the modular form



	$\chi_1$	$\chi_{1'}$	$\chi_2$
$C_1$	1	1	2
$C_2$	1	1	-1
$C_3$	1	-1	0