

2nd Workshop on efficient RF Sources

High Efficiency Klystrons



23-25 September 2024, Toledo, Spain



Ultimate efficiency in linear beam devices.
Electro-vacuum technologies for FCC_{ee}

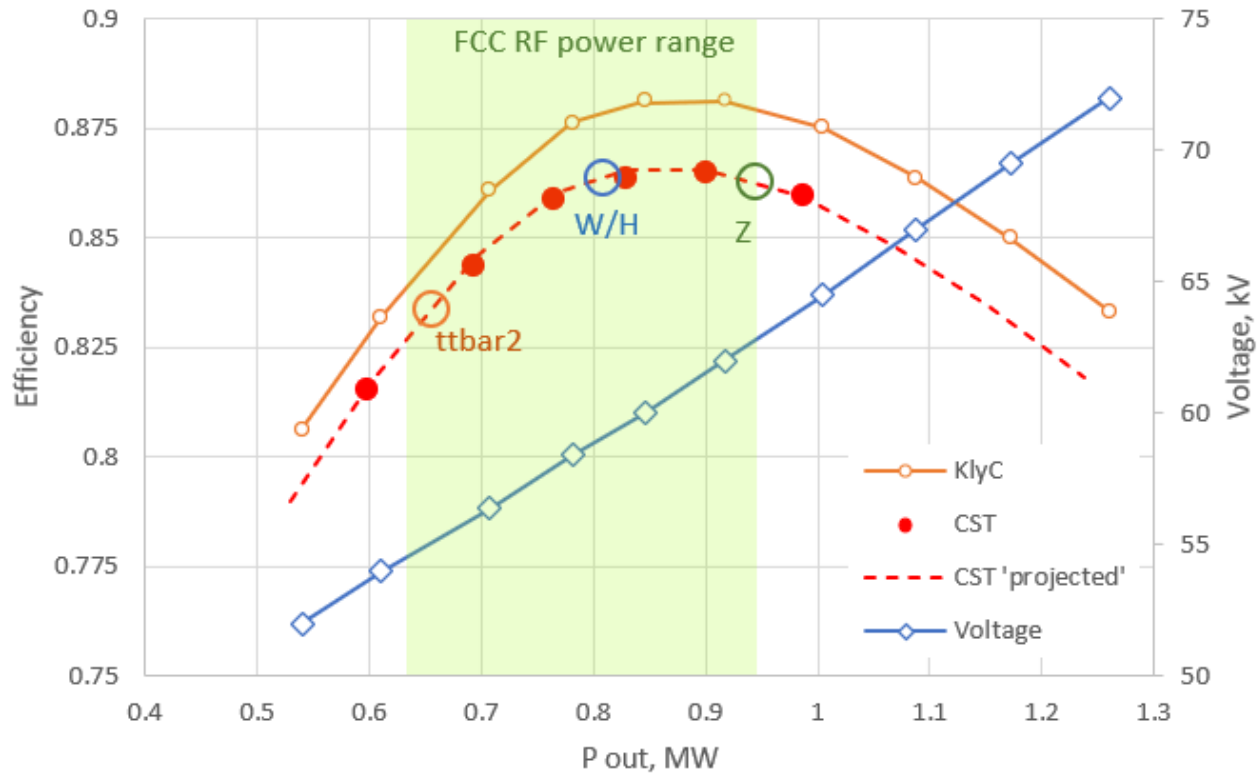
I. Syratchev, CERN

Novel 400 MHz, 1MW HE Two-Stages MBK for FCC_{ee}. Performance summary.

High Efficiency Klystrons

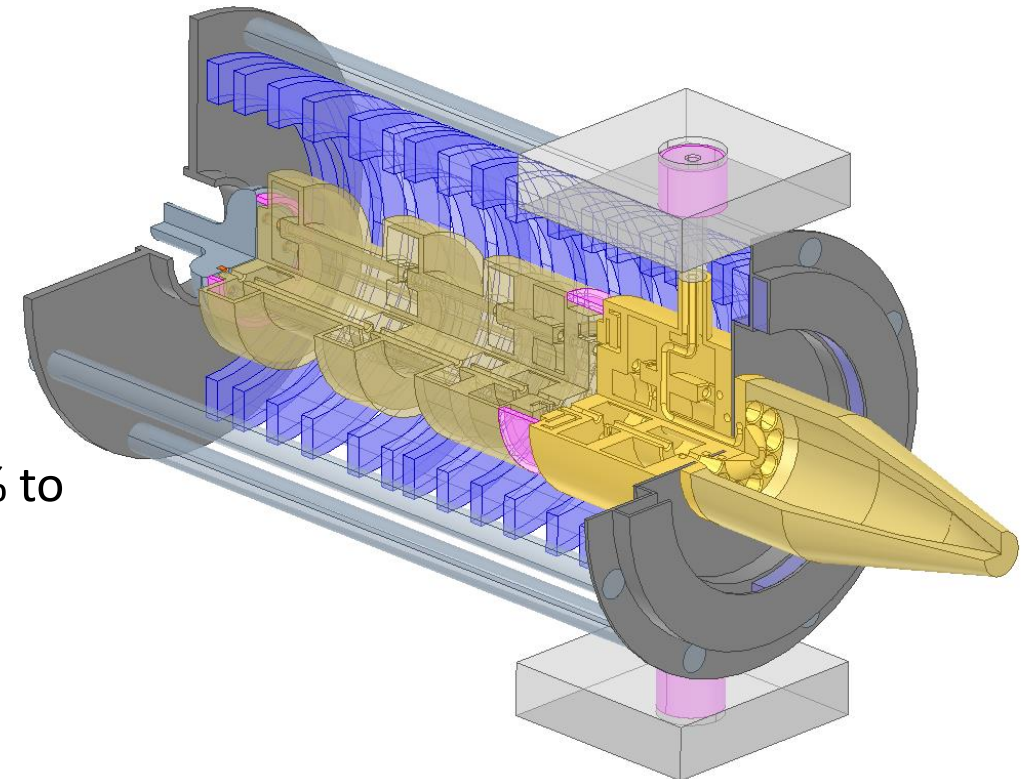


Efficiency vs. saturated RF power at different klystron voltages



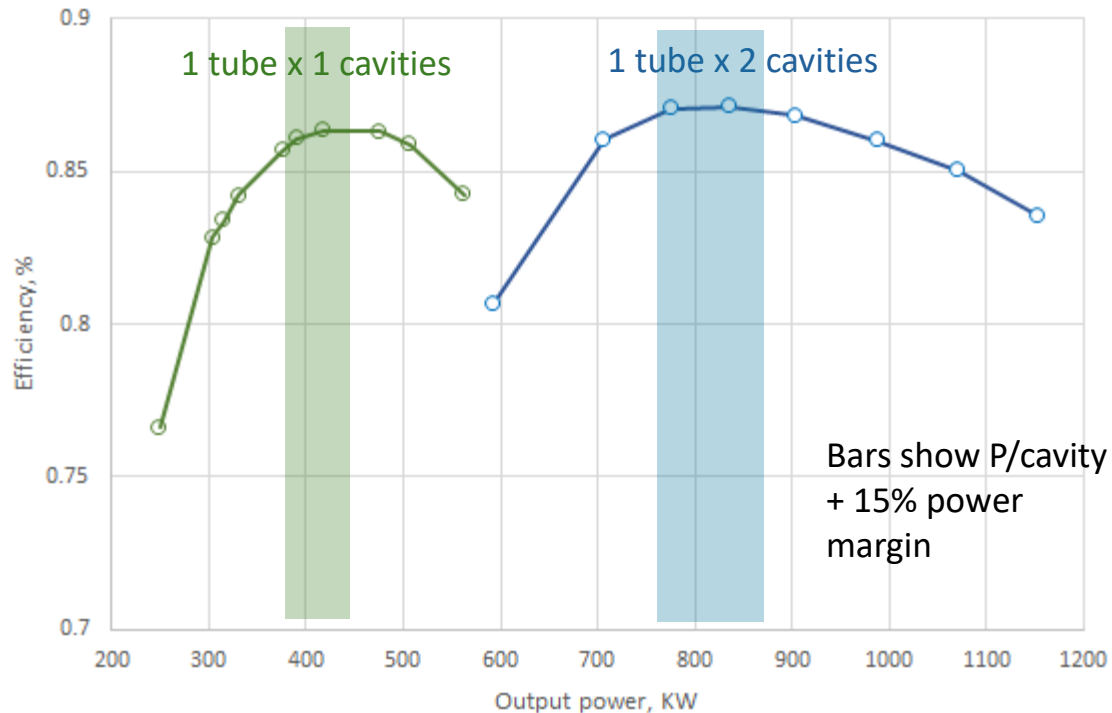
Featured:

- **Very efficient.** 86% @ Z,W,H and 83% @ ttbar2.
- **Compact.** Total length <3m.
- **Low Voltage.** Up to 64kV @ 1 MW.
- **High RF power gain.** 43dB @ 1MW.
- **Broadband.** 3.5 MHz @ -1dB.
- **Robust.** Can handle mismatch up to -15dB.



For FCC_{ee}, such an efficiency improvement from conventional 65% to 85% will allow to save 38MW of the grid electric power. That is compatible to the electric power needed for the entire FCC_{ee} cryogenic system (40MW).

The new layout with one unique two-gaps cavity for Z,W,H poles, opens options of using one power source per single, or two cavities. Performance of the TS klystron is now optimized for both options with almost identical efficiency.



With reduced power per klystron:

- Reduced by ~50% collector volume.
- Improved beam extraction quality into collector.
- Reduced by 10% RF circuit length.
- Reduced from 62kV to 47 kV operating voltage.
- Reduced power in solenoid
- Improved x2 life- time.
- Single RF output.
- With chosen technology, cost saving will be rather modest – no more than 20% when moving from 1MW tube to 0.5MW tube.
- Will need x2 more klystrons.

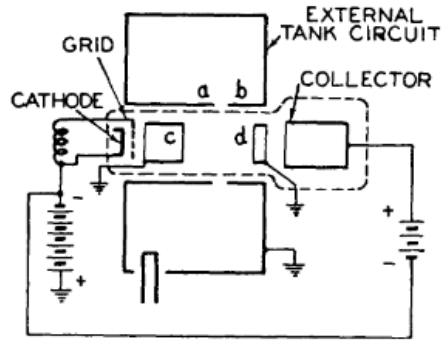
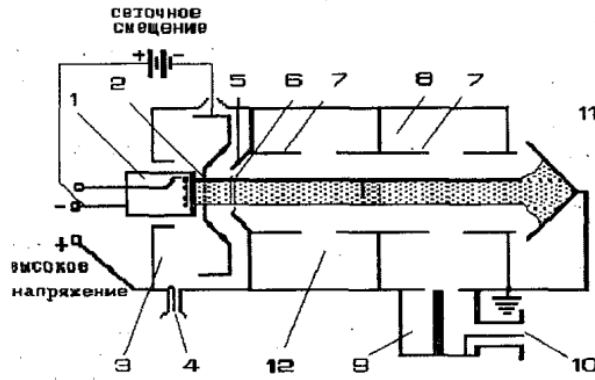


Fig. 2—Diagram of an inductive-output amplifier with an external output circuit.

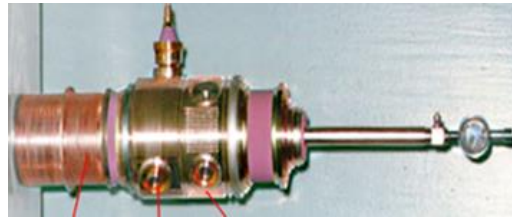
IOT (A. Haeff, 1939)

Klystrode

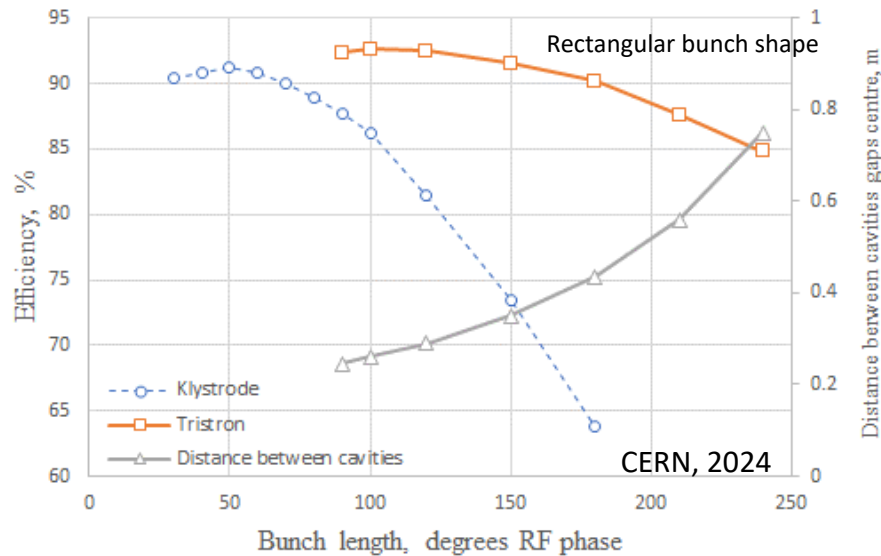
(H. Priest and M.B. Shrader 1982)



Tristron (A.D. Sushkov et. al. 1967)
MB Prototype tested in 1997, V. Tsarev:

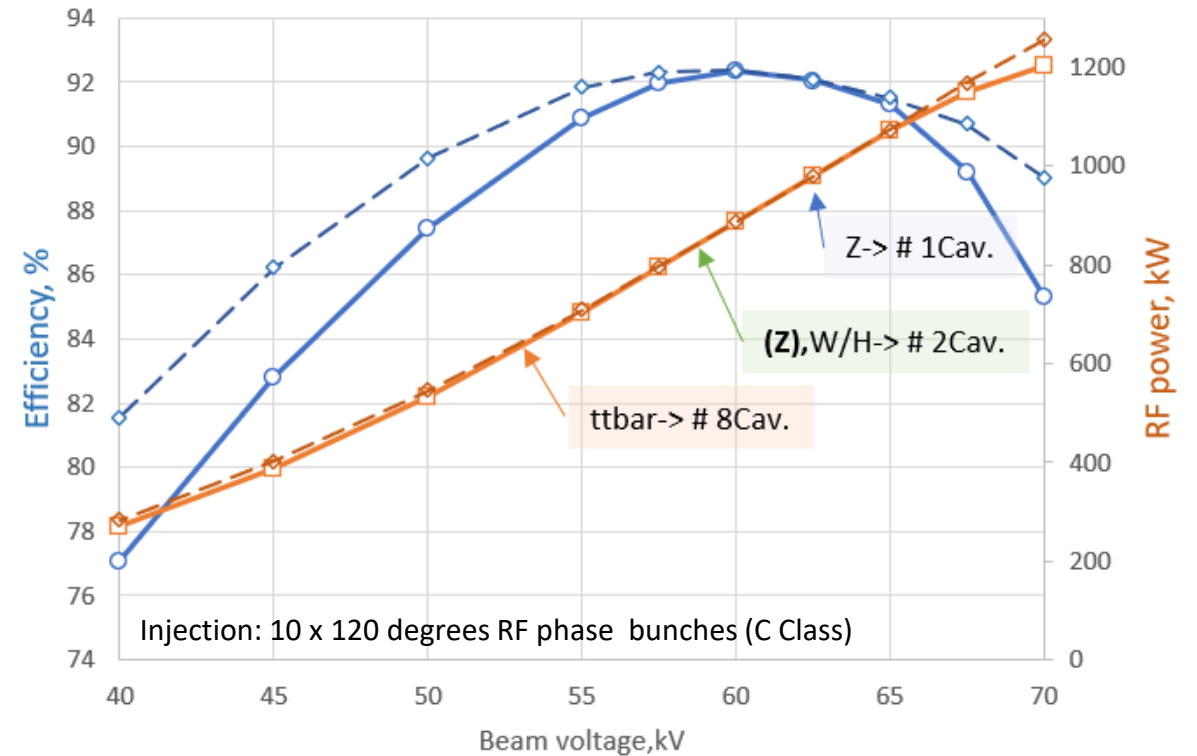


FCC_{ee} 1MW, 400 MHz 10 beams gridded tubes performance (KlyC simulations)



High Power Gridded Tubes

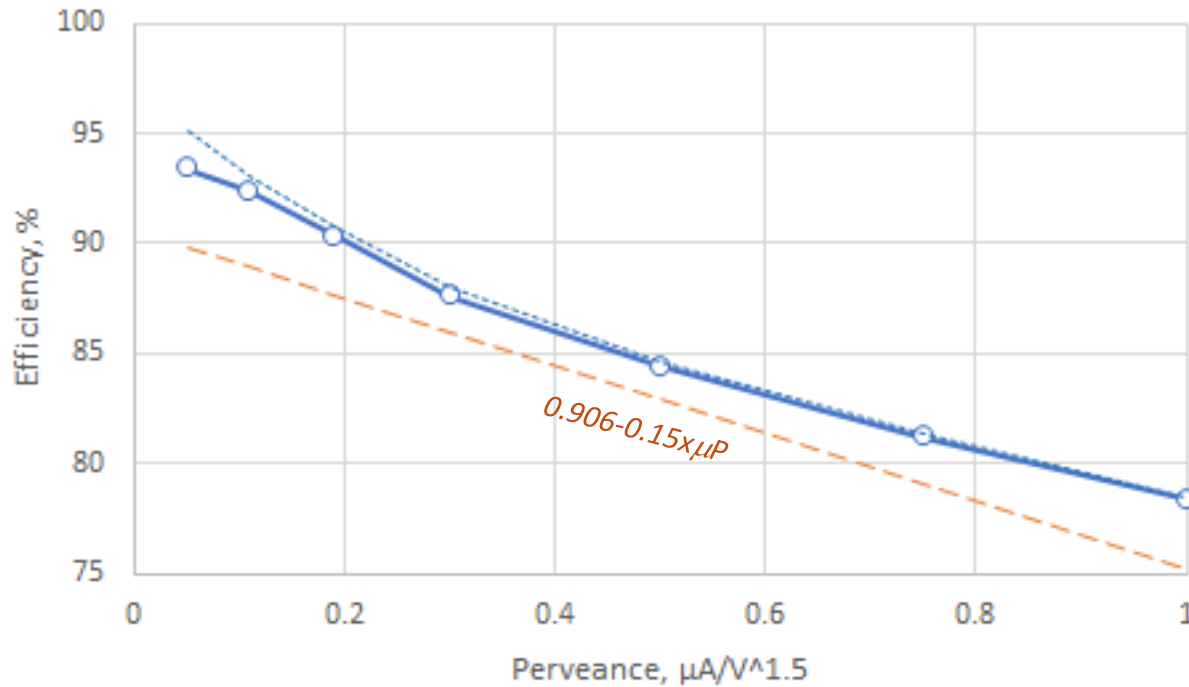
1 MW, MB Tristron power-efficiency capabilities



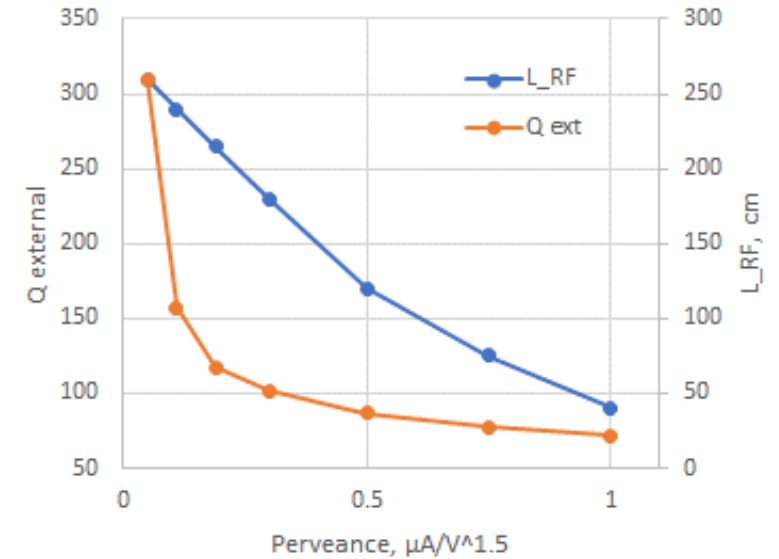
"Il n'y a de nouveau que ce qui est oublié". Marie Antoinette (1785)

Tristron efficiency vs. beam perveance

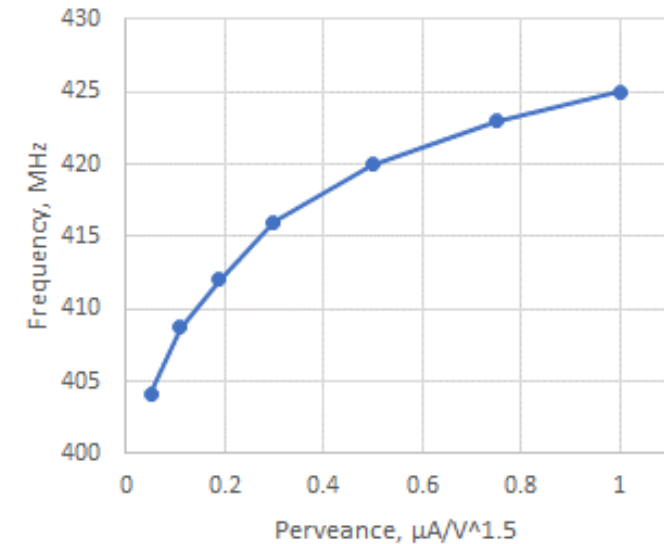
Optimized for bunch length of **120** degrees RF phase
and fixed beam power (960 KW)



Overall, tristron demonstrated excellent performance in terms of the ultimate efficiency in a wide range of operating perveance.



Penultimate cavity tuning



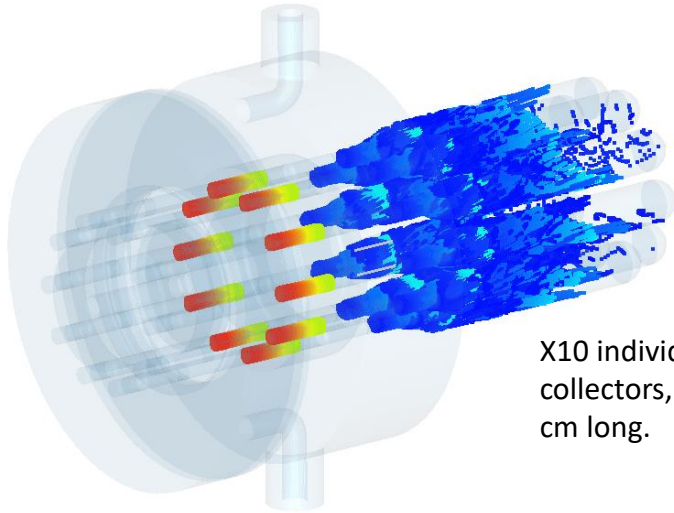
10 beams (1.6A, 60kV each)

Bz: 0.032T

Beam power 960kW

RF power: 880kW

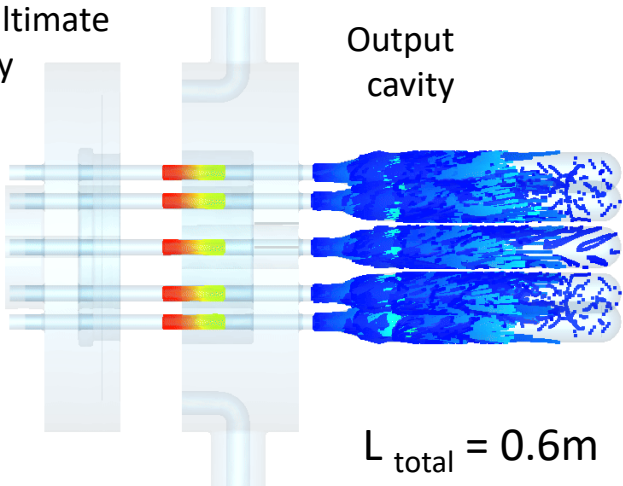
Efficiency: 91.4%



X10 individual collectors, each 30 cm long.

Penultimate cavity

Output cavity



$L_{total} = 0.6m$

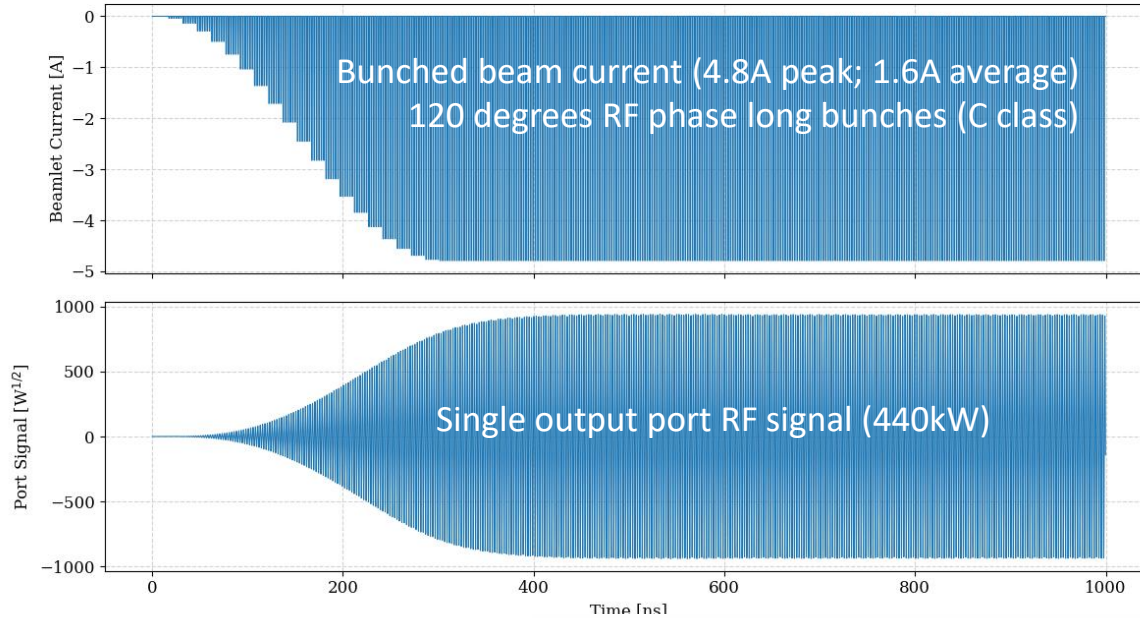
Tristron 3D CST PIC simulations.

Direct benchmarking with CERN made fast 1.5D computer code KlyC

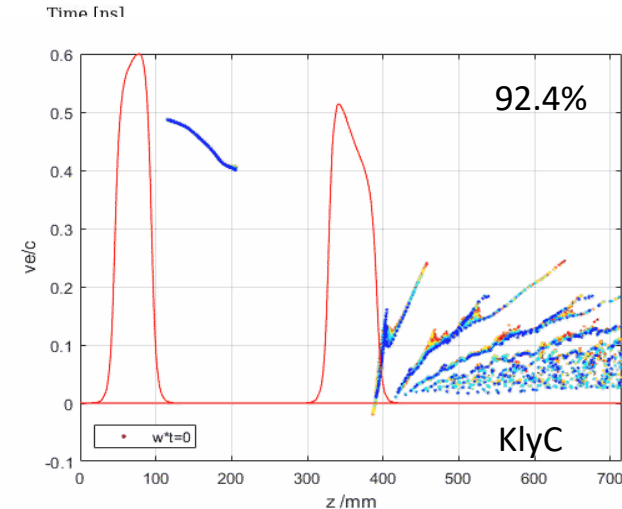
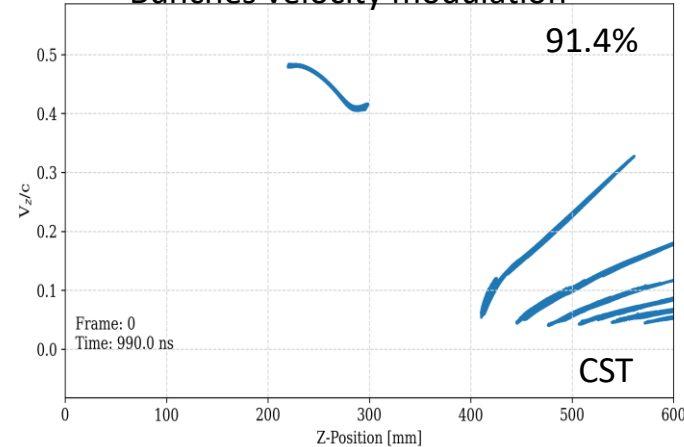
High Efficiency Klystrons



klystrode_pic_1000ns_300nsSineUp_analyticalB

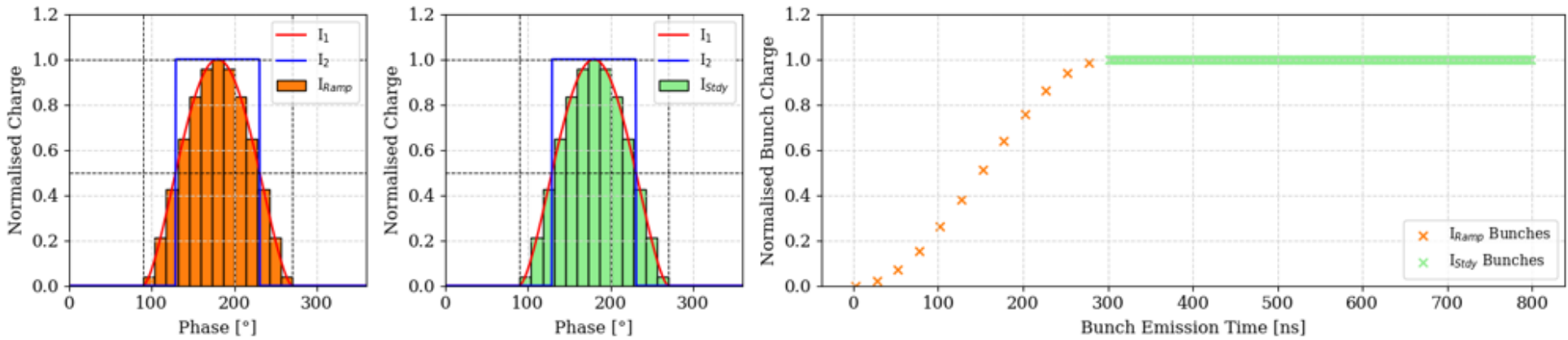


Bunches velocity modulation

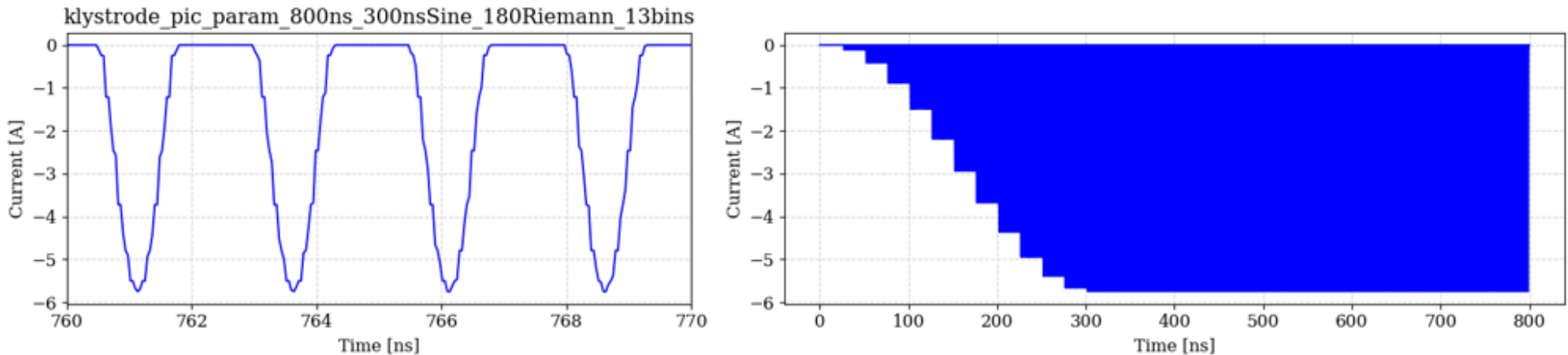


Emission Current – 180° Bunch $I(t) = I_0 \times (U_{bias} + U_{RF} \times \sin(\omega t))^{1.5}$

Emission Programme

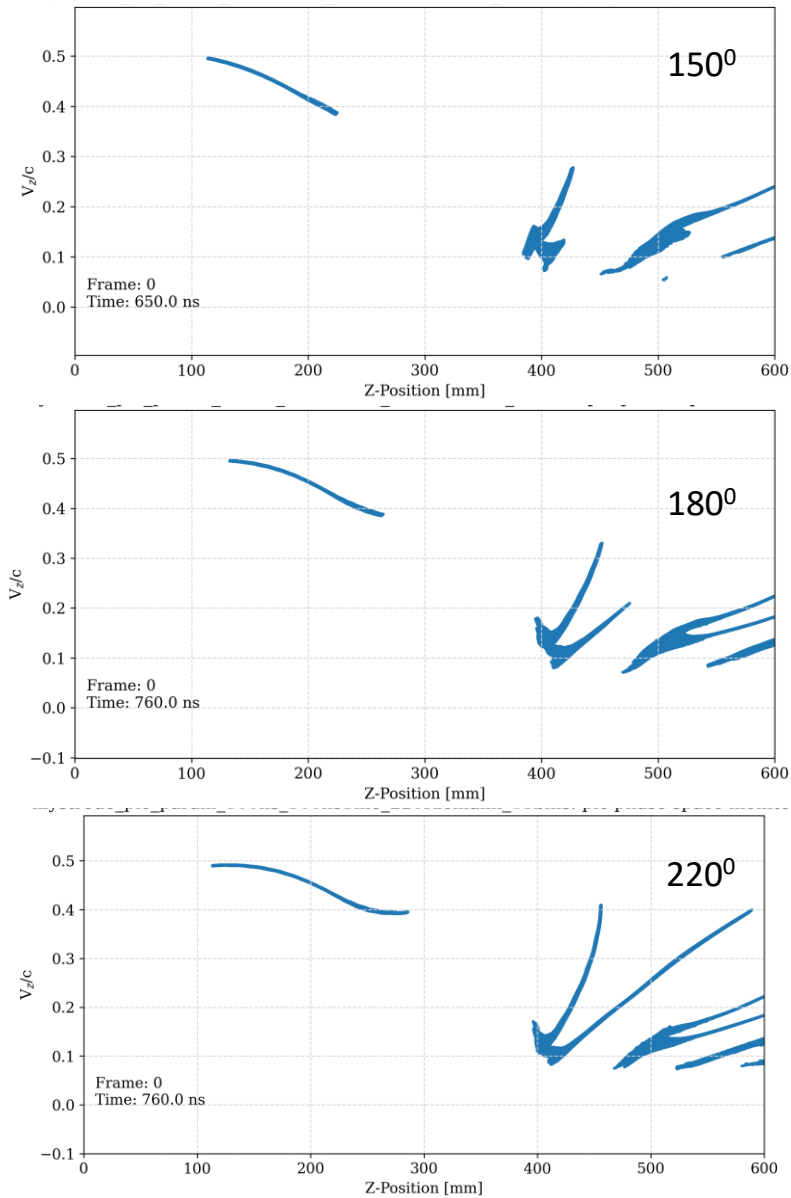


CST monitors

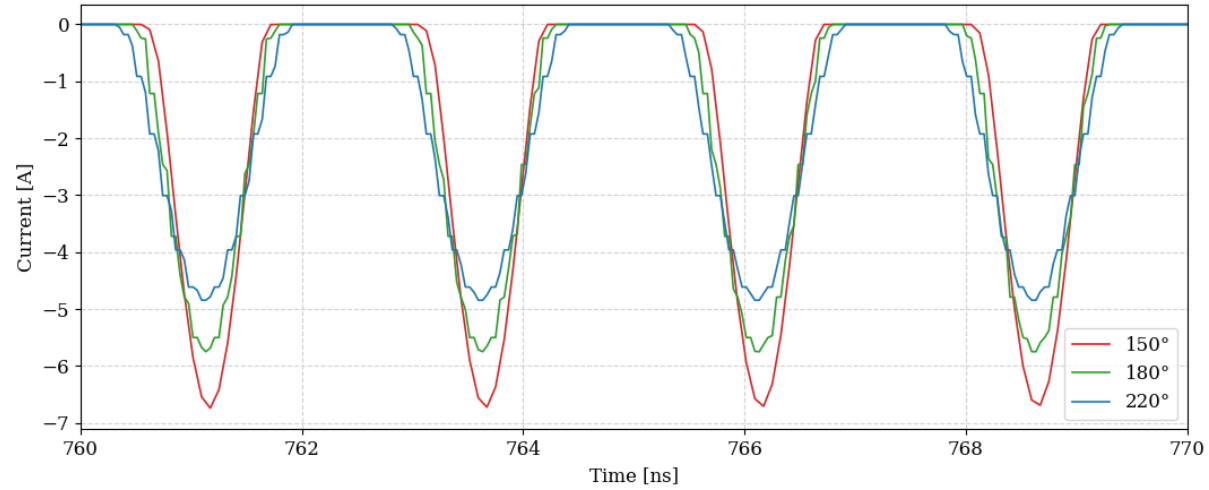


Realistic bunches in gridded tubes

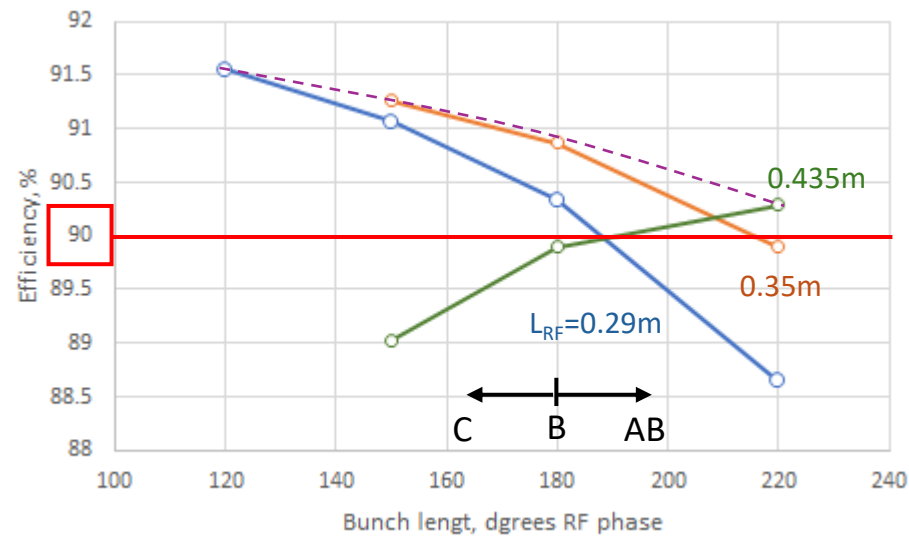
Particles velocity modulation ($L_{RF}=0.29m$)



Average current 1.6A/beam



1MW, MB Tristron efficiency (measured at RF port)

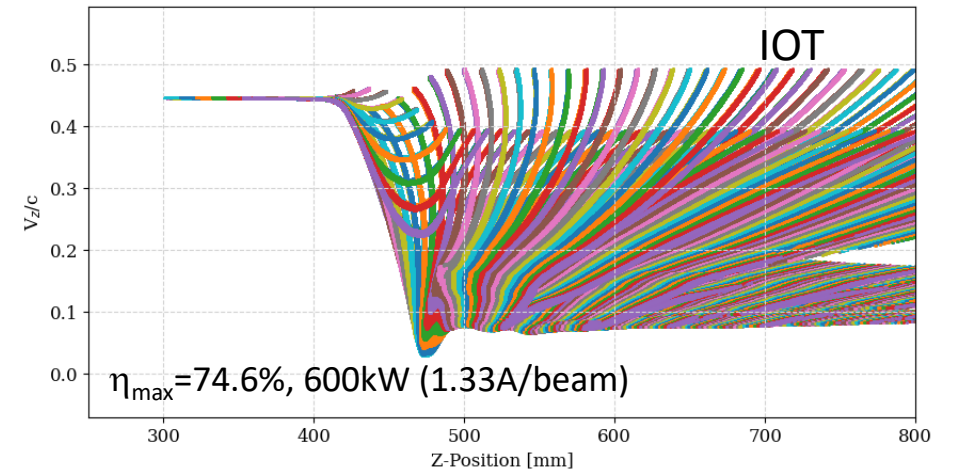
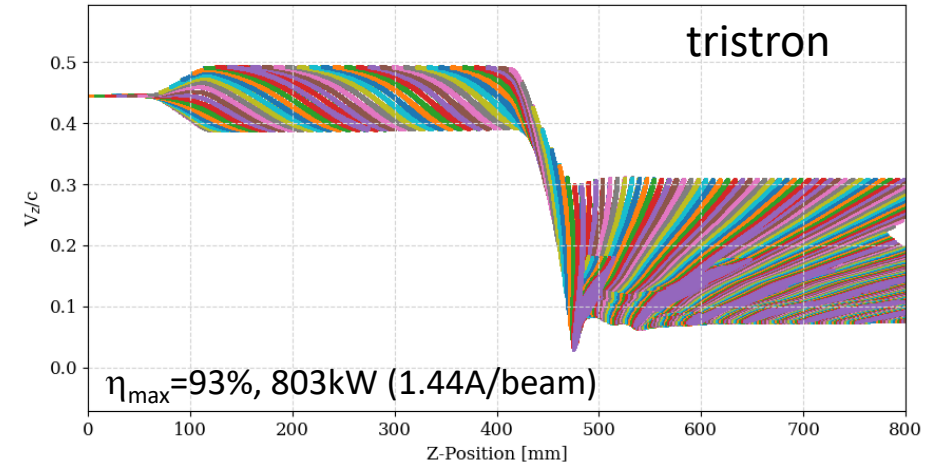
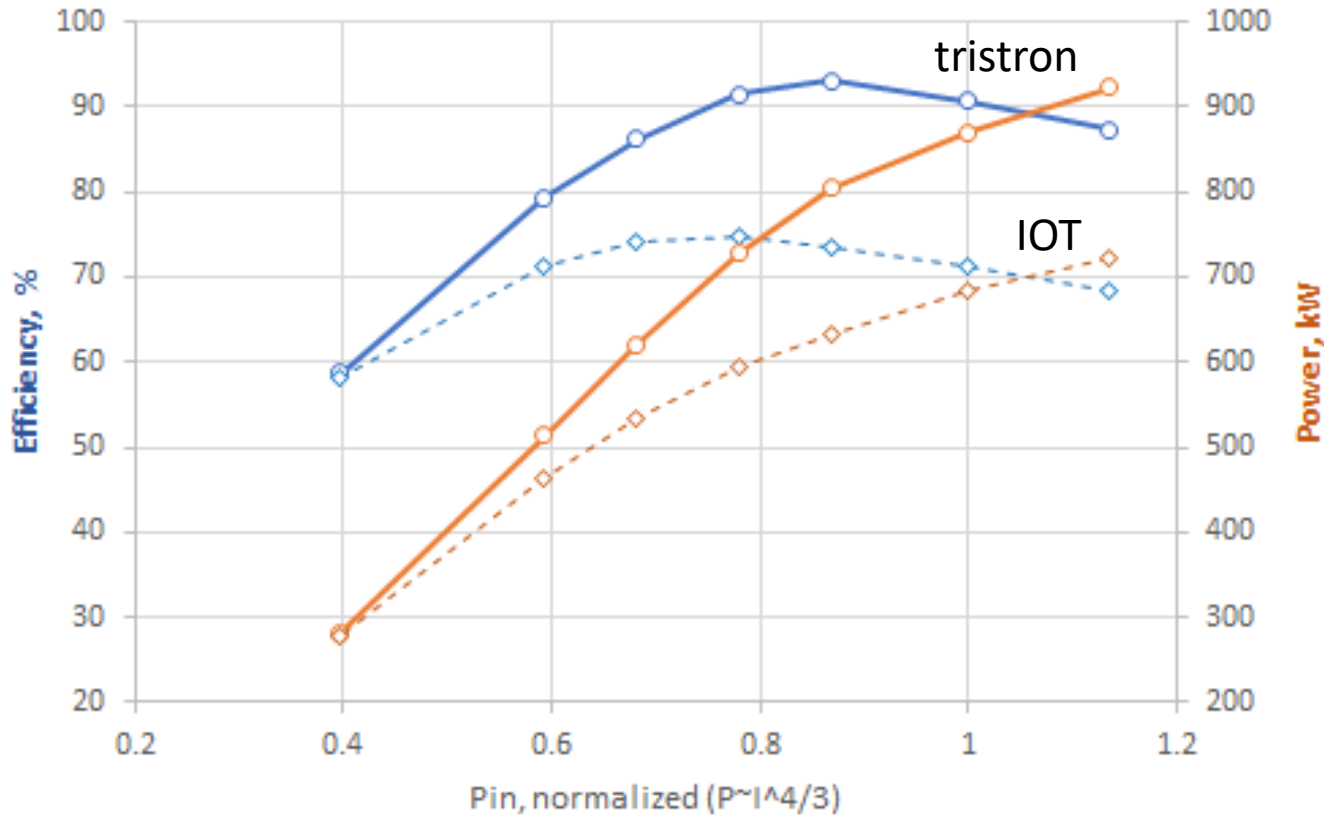


Distance between the cavities (L_{RF}) and penultimate cavity tunings were taken from the ones optimized in KlyC for rectangular bunch shape (see page 4). *There is some space left for post-optimization*

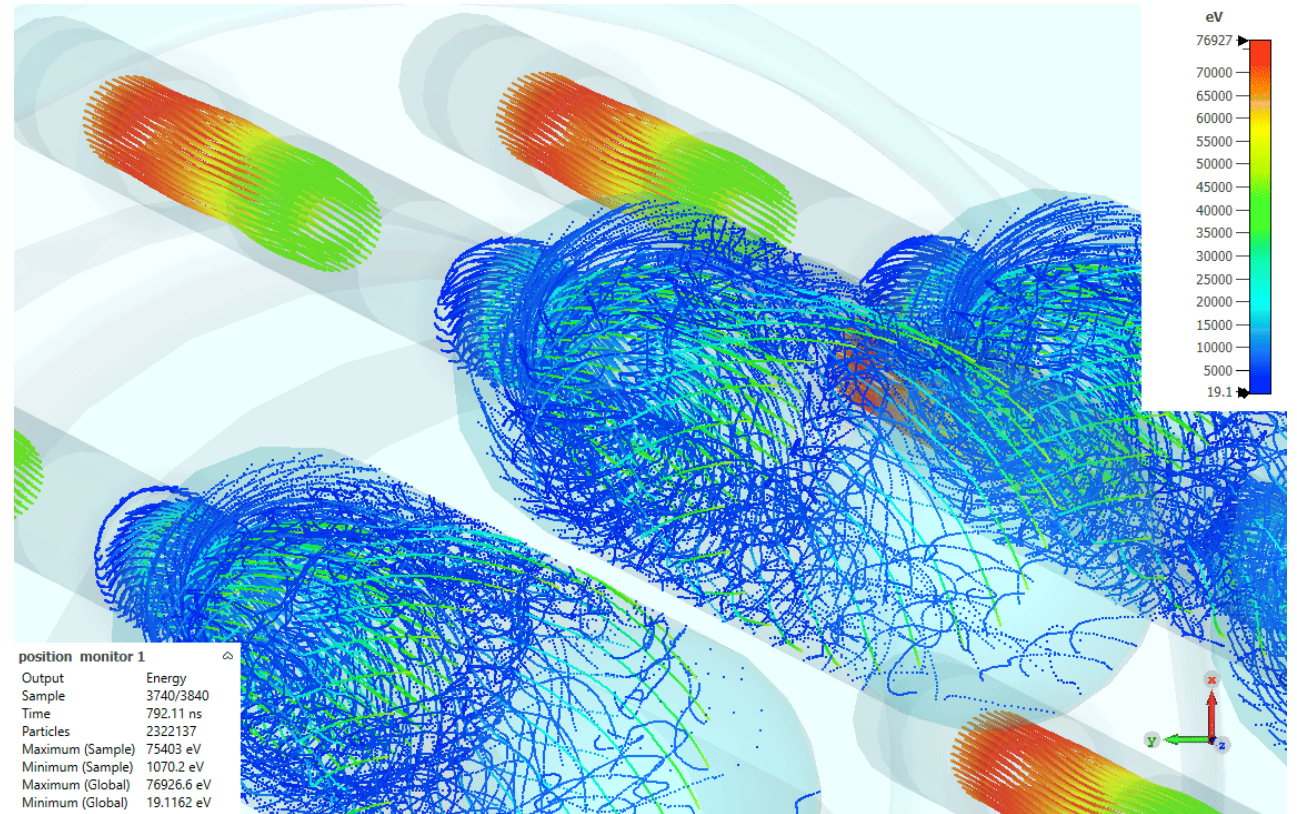
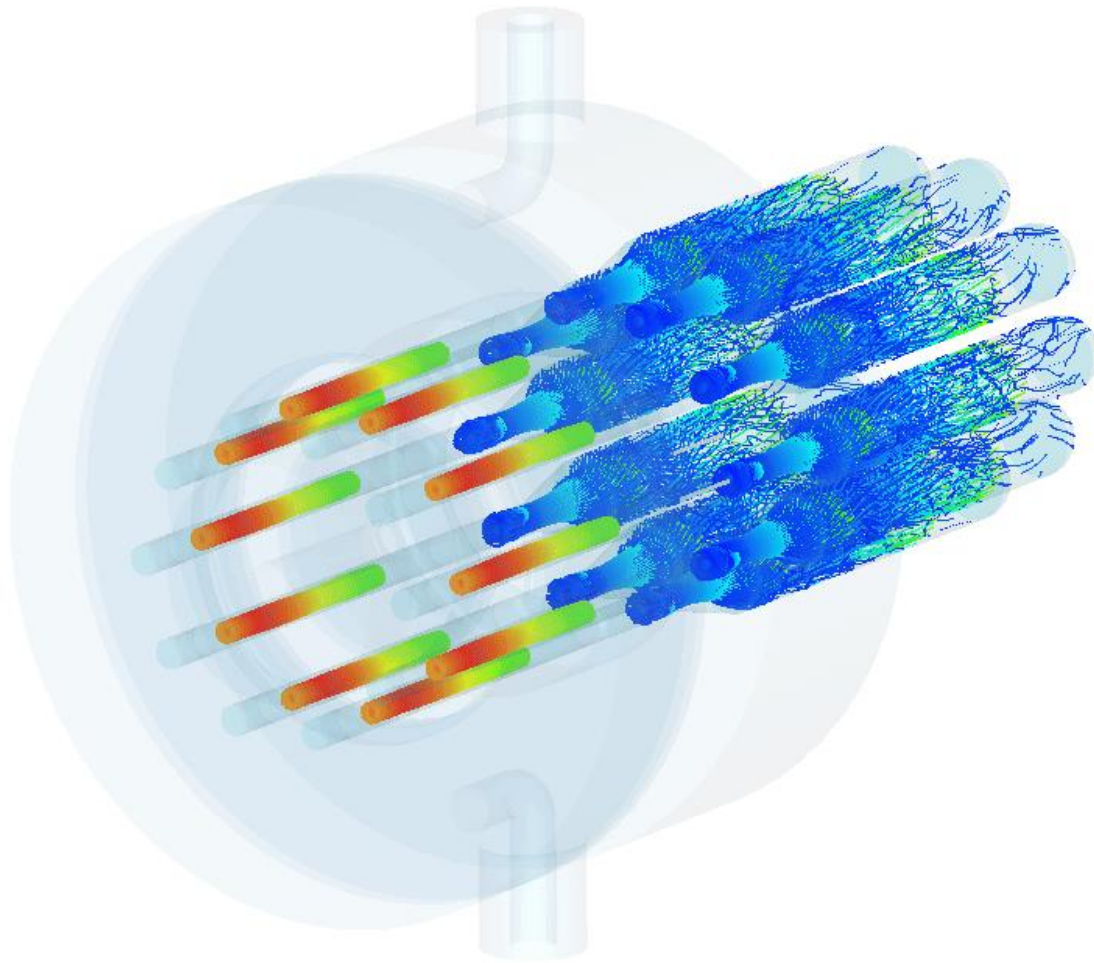
MB tristrion vs. IOT power gain curves



B class (180 degrees bunches)
V beam=60kV



More particles animations (AB Class)



RF power limit in CW UHF/L-band gridded tubes

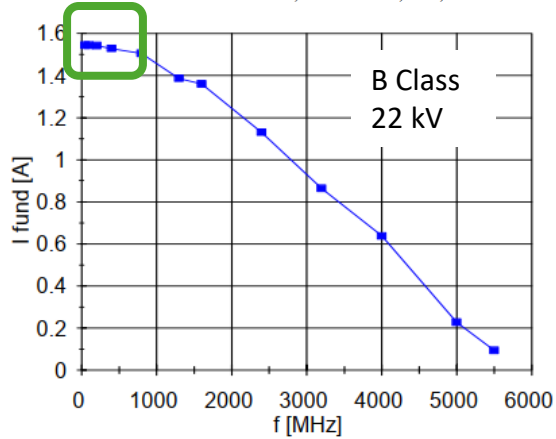
Proceedings of LINAC 2004, Lübeck, Germany

CHARACTERIZATION OF A KLYSTRODE AS A RF SOURCE FOR HIGH-AVERAGE-POWER ACCELERATORS*

D. Rees, D. Keffeler, W. Roybal, and P. J. Tallerico
Los Alamos National Laboratory, Los Alamos, NM 87545 USA

IOT RF POWER SOURCES FOR PULSED AND CW LINACS

H. Bohlen, Y. Li, R. Tornøe,
CPI Eimac Division, San Carlos, CA, USA

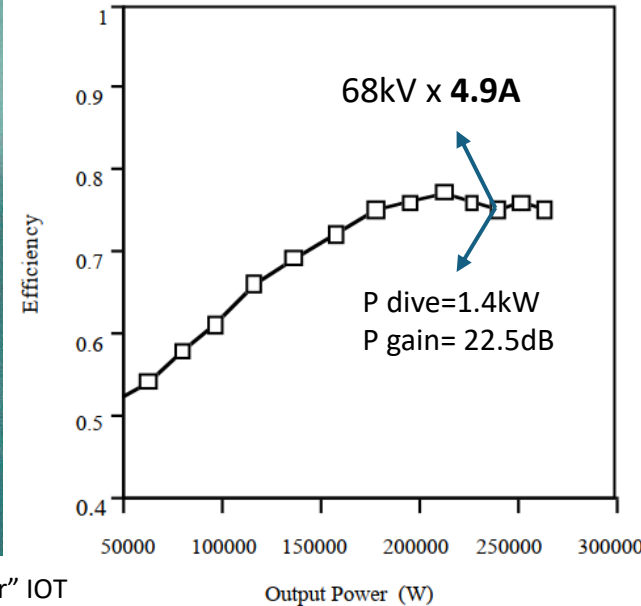


30 kW CW L-Band (1.3GHz) IOT by CPI / Eimac

Voltage (kV)	Current (A)	Drive (W)	Output (kW)	Gain (dB)	Eff (%)
24	0.79	208	10.0	17	52.7
25	1.10	203	15.1	19	54.9
26	1.46	183	20.6	21	54.3
32	1.35	192	25.7	21	59.5
34	1.39	253	30.2	21	63.8



250kW, 267 MHz CW "Chalk River" IOT



"...We have approximately 664 high-voltage hours on the 250-kW CW klystron at Los Alamos, and we have had to process the grid at least three times to remove material deposited on the grid by the cathode. We are afraid that the cathode is being overheated by the RF drive power and that the result will be a reduced tube life..."

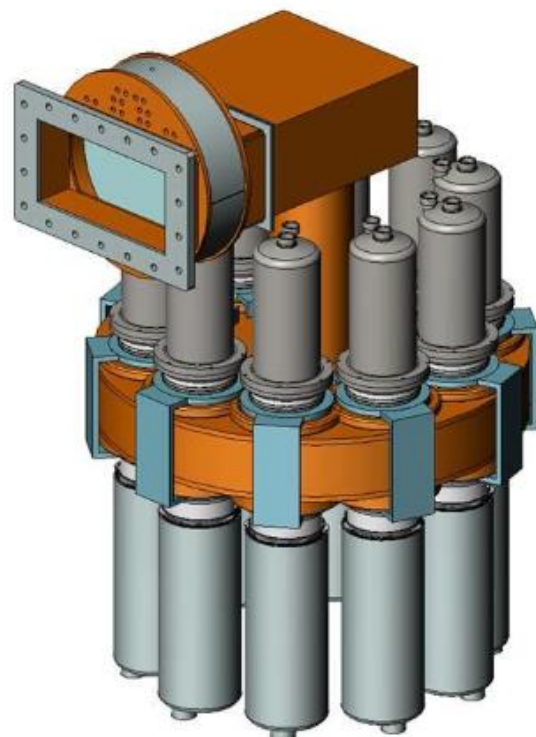
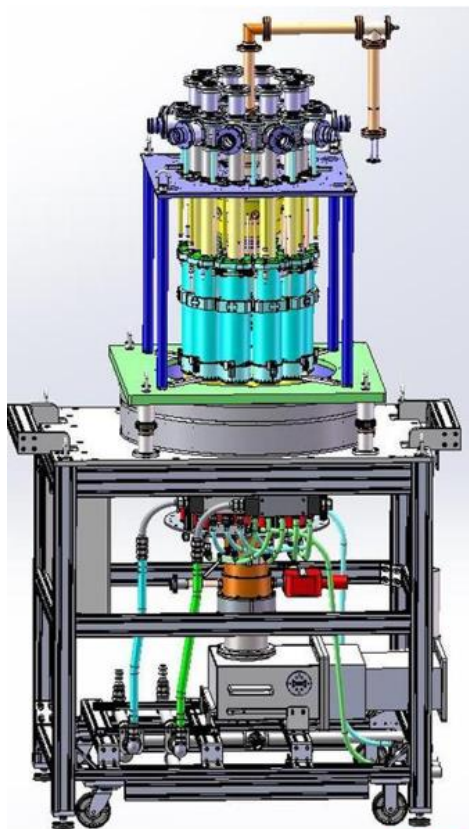
In the gridded tubes CW RF power level will be limited by:

- The average beam current (current interception on the grid - direct heating).
- Cathode overheating by the drive power (material deposition on the grid).
- More?

In MB tubes, the current and drive power per beam can be controlled/adjusted by beams number. In the FCC_{ee} MB tristrion designs:

- 10 beams, 60kV, Pout 880kW; beam current is 1.6 A, P dive/beam = 440W (P gain=23 dB)
- 10 beams, 47kV, Pout 440kW; beam current is 1.0 A, P drive/beam = 220W (P gain=23dB).

Both cases look like a feasible options.



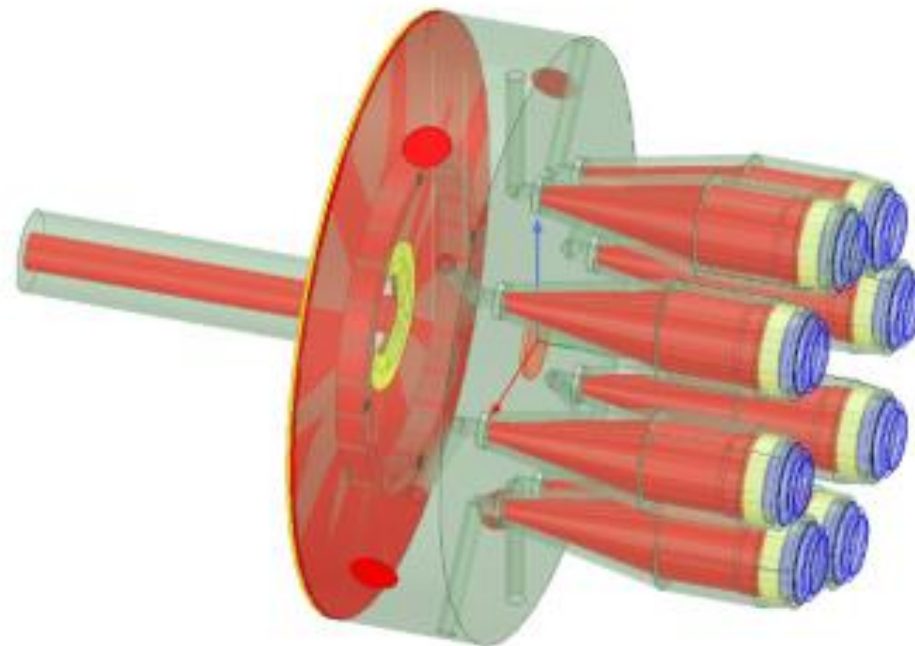
COMPREHENSIVE DESIGN AND WHOLE-CAVITY SIMULATION OF A MULTI-BEAM INDUCTIVE OUTPUT TUBE USING A 3rd HARMONIC DRIVE ON THE GRID

H.P. Freund,^{1,2,3} T. Bui,¹ R.L. Ives,¹ T. Habermann,¹ and M. Read¹

¹Calabazas Creek Research, Inc., San Mateo, CA 94404

²Institute for Research in Electronics and Applied Physics, University Maryland, College Park, Maryland 20742

³University of New Mexico, Albuquerque, New Mexico, 87131



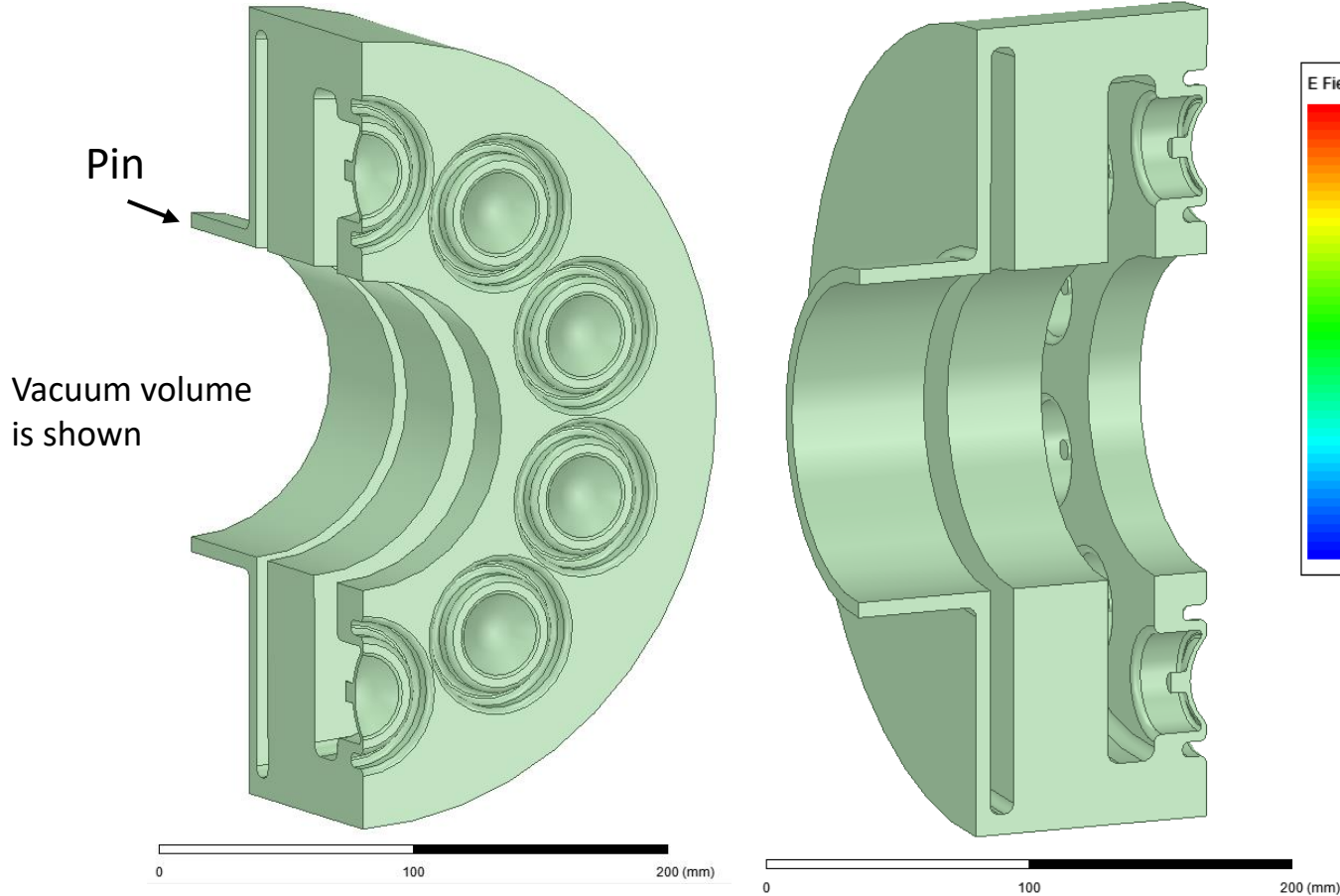
THALES



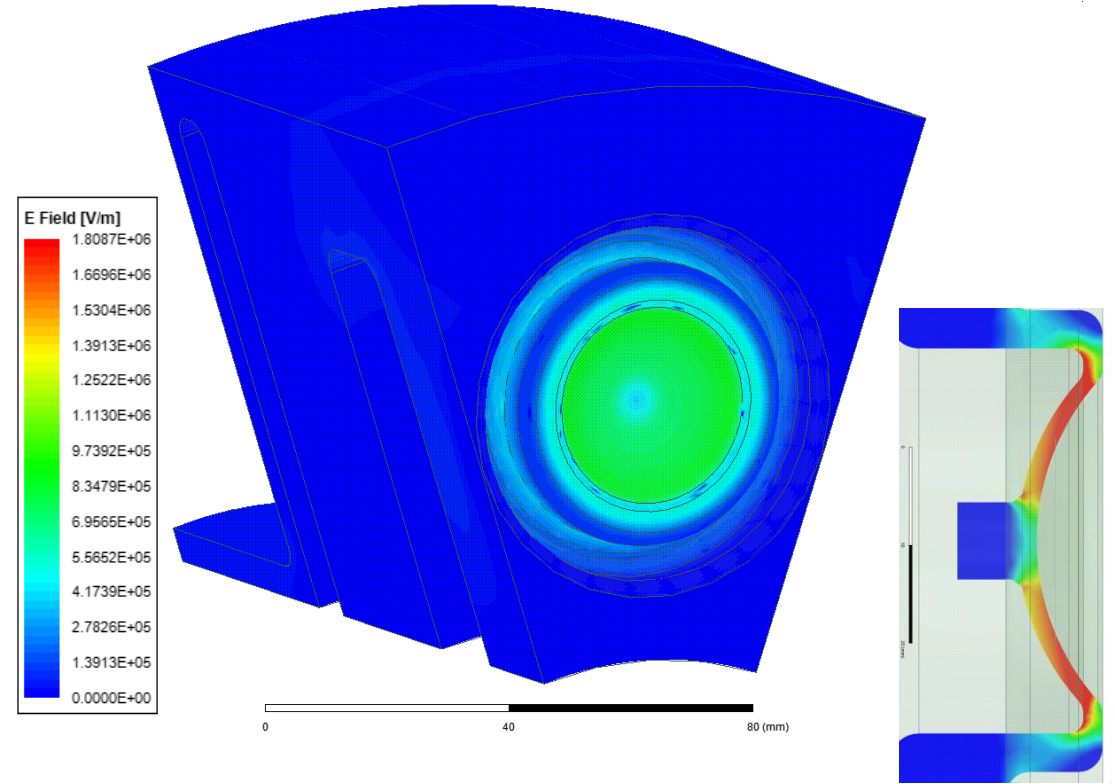
From ESS MB IOT experience, input cavity can be rather expensive and complicated if composed of many individual cavities (coupled or not). It will be useful to investigate more compact and reliable solution with a 'common' volume (one of the concepts is shown above on the right).

400MHz Double-gap coaxial compact cavity **concept** (CERN).

grid-cathode distance = 2mm



$Q_0=3080$, $Q_{ext}=61.5$ (Ohmic losses $\sim 2\%$)



With $P_{RF}=880\text{kW}$, assuming 23 dB power gain ($P_{in}=4.4\text{kW}$) and $Q_{ext}=61.5$, average gap field is $\sim 0.7\text{MV/m}$. With 2mm gap distance, the gap RF voltage is about 1.4 kV.

The MB Tristron has a remarkable potential as an FCC_{ee} RF power source, both in terms of power handling and attainable efficiency – above 90%.

Compared to its TS MBK counterpart operated in similar conditions, it has numerous advantages:

- Very compact (shorter by factor 3) – less than 1m long.
- Reduced power in solenoid (factor ~ 10) due to the lower magnetic field and shorter RF circuit
- Very compact and simple collector (factor ~6 in volume).
- Reduce by factor 10 cooling capacity need (Tristron will never be operated in DC diode mode).
- The cost of MB Tristron will be about 0.5 (or less) of those for TS MBK.
- Directly scalable to 200 kW, 800MHz.

Tristron development is already planned as a part of the future CERN-Thales collaboration.