

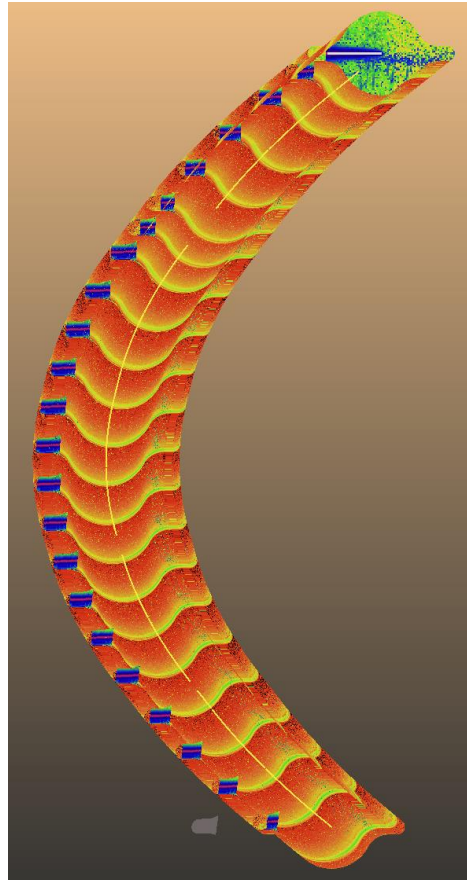


SYNCHROTRON RADIATION MANAGEMENT, PRESSURE PROFILES

Marion ADY, CERN

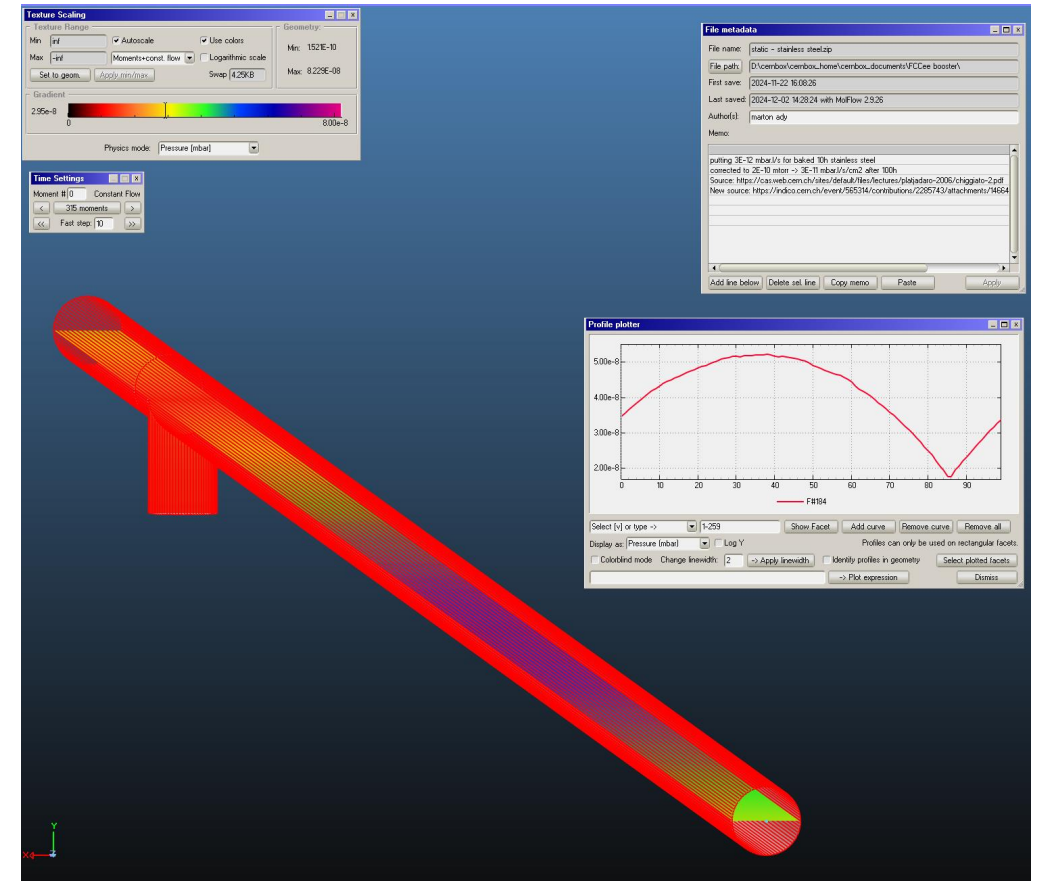
FCC Week, Vienna, 21-05-2025

Collider ring



Absorber placement study

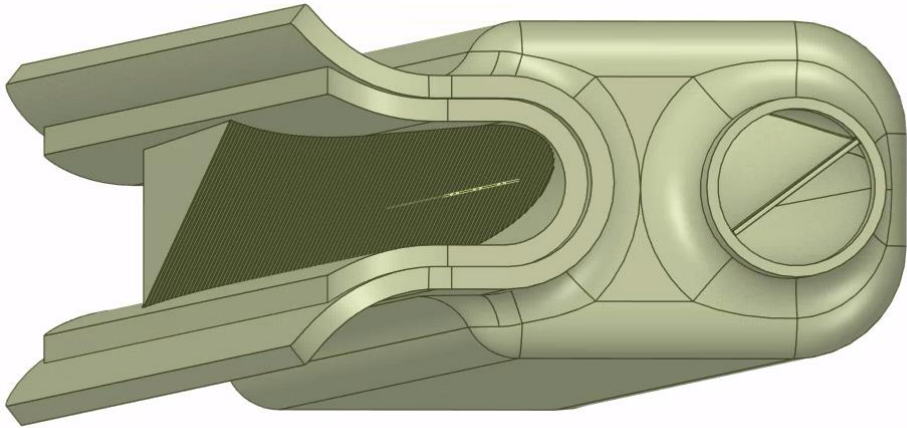
Booster ring



Dynamic and static pressures

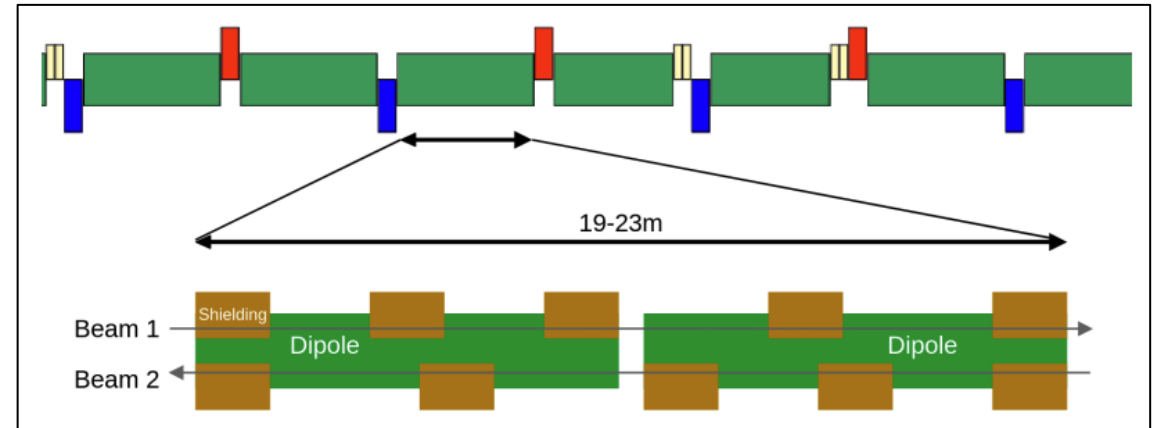
The task

~50MW/beam synchrotron radiation



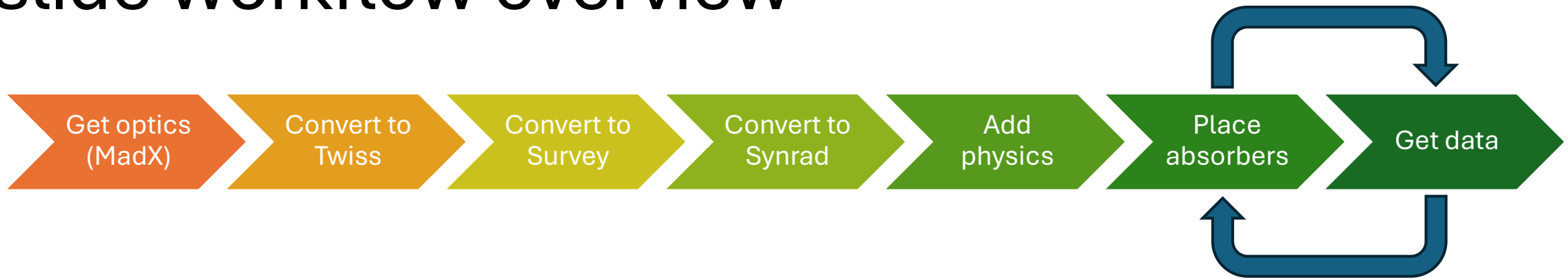
place discrete absorbers, 4 per magnet?

FCC consists of 130m “supercells” with 5 magnets



“Find absorber placement as periodic solution”

1-slide workflow overview



Survey file to SynRad+ converter

Export result to Synrad format | Aperture list | Sessions

Name	length (m)	DIPOLE: Bending angle [rad]	DIPOLE: Field (T)	QUADRUPOLE: Gradient (T/m)	QUAC
DRIFT_5134	0.3				
QD3_468	2.9			-10.9308023	-0.052
DRIFT_5135	0.3003188634				
B1S_658	21.44417655	0.001988600825	-0.05645071947		
DRIFT_5136	0.300322124				
SF26.9	1.4				
DRIFT_5137	0.1				
SF26.10	1.4				
DRIFT_5138	0.3				
QF4_468	2.9			10.93084694	0.0520
DRIFT_5139	0.3003188634				
B1_718	24.64417655	0.002285349111	-0.05645071946		
DRIFT_5140	0.300322124				
QD3_469	2.9			-10.9308023	-0.052

Reference element row: 2 | Set selected | Ref. X [m]: 0 | Ref. Z [m]: 0 | Ref. theta [rad]: 0

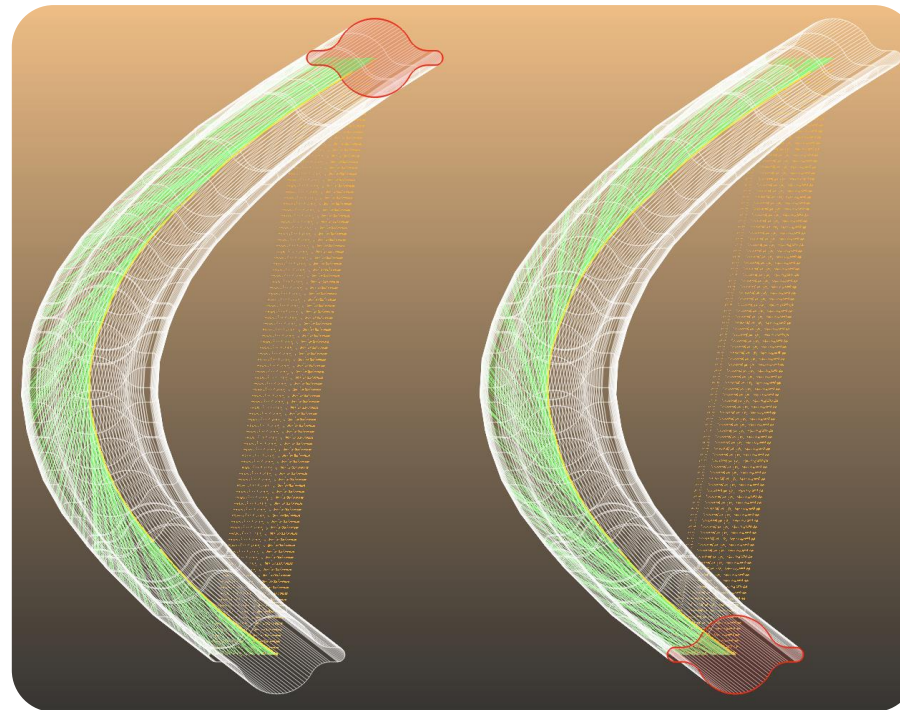
Search text: | Search beginning | Search end | Convert B<->Angle and Grad<->K1L

File output: Output dir: C:\Users\mszakaca\cse\box\WINDOWS\Desktop\export | Start row: 2 | Get Selected | End row: | Get Selected

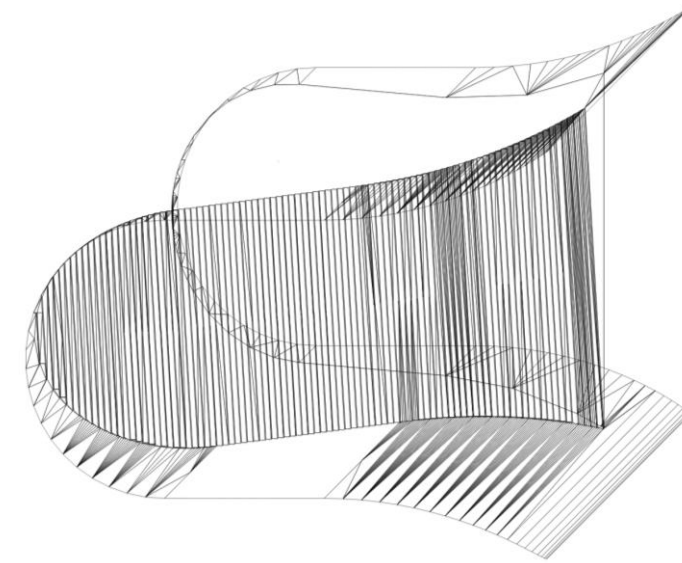
Beam properties | Synrad param files | Synrad/Molflow Geometry

Filename: Geometry.txt | Circle sides: 72 | Sticking factor: 1.0 | curve step every: 0.01 radians | Aperture transition: Continuous (aper) | Aperture facets: First and last (end caps) | Write geometry file

Opticsbuilder



Synrad geometry

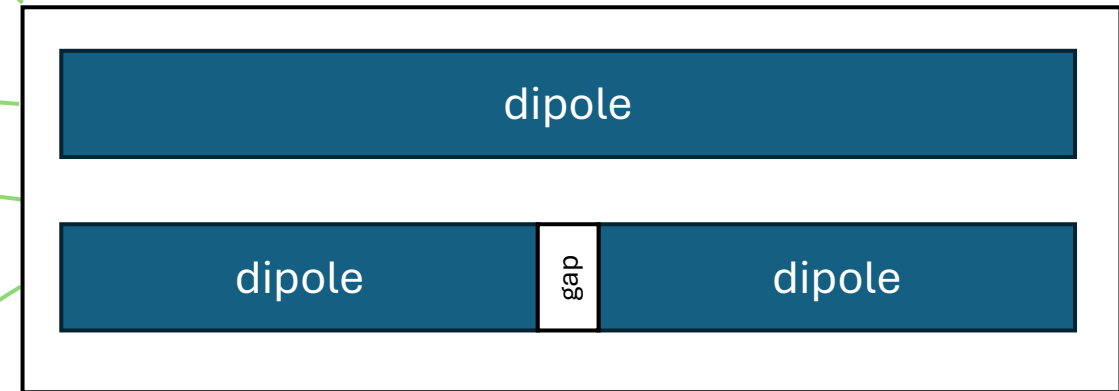


Absorbers ⁴

First step: manually edit magnets in OpticsBuilder

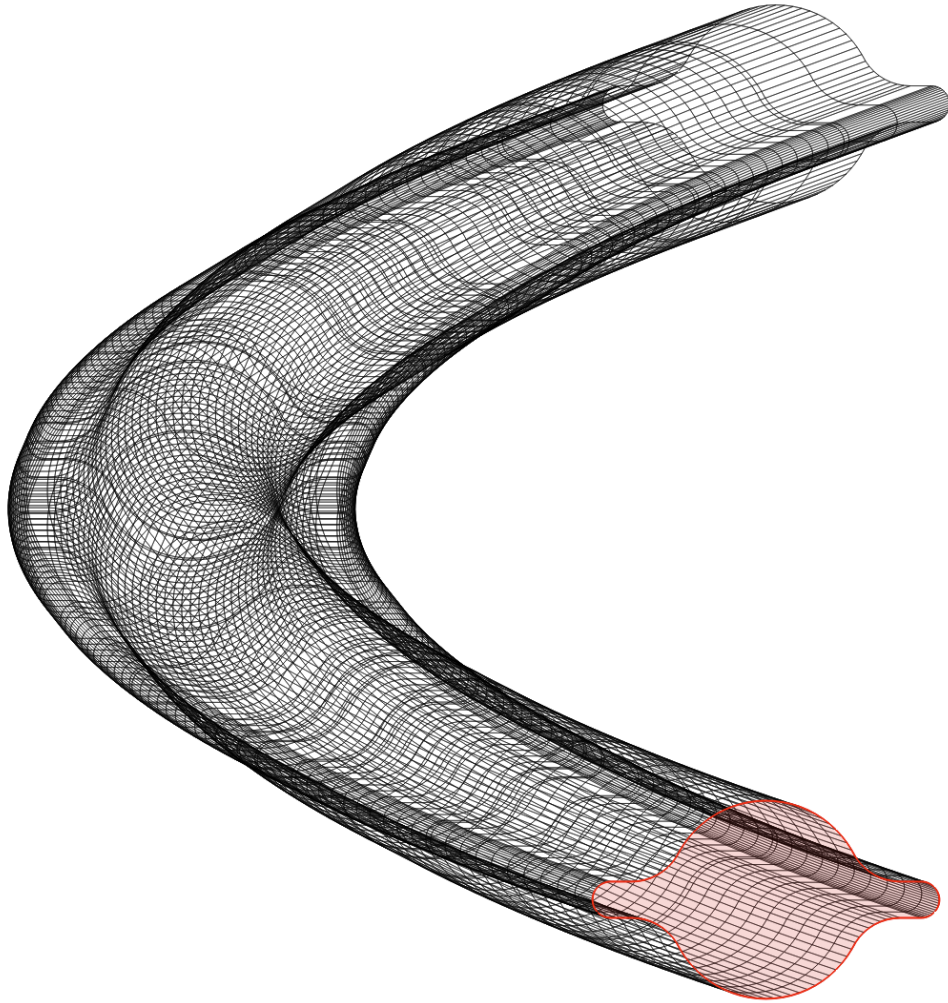
130.2m 5-cell pattern in OpticsBuilder:

Name	length (m)	DIPOLE: Bending angle [rad]	DIPOLE: Field (T)
B1S.156	19.70537223	0.001966470217	-0.01517874778
DRIFT_811	0.3		
QD1.11	2.9		
DRIFT_812	0.2		
SD22.1	1.3		
DRIFT_813	0.2		
B1L.40	21.15537223	0.00211117095	-0.01517874777
DRIFT_814	3.4		
B1.198	22.65537223	0.002260861364	-0.01517874777
DRIFT_815	0.3		
QF2.11	2.9		
E.ARC	0		
DRIFT_816	0.2		
B1.199	22.65537223	0.002260861364	-0.01517874777
DRIFT_817	6.35		
B1S.157	19.70537223	0.001966470217	-0.01517874778
DRIFT_818	0.3		
QD1.12	2.9		
DRIFT_819	3.15		

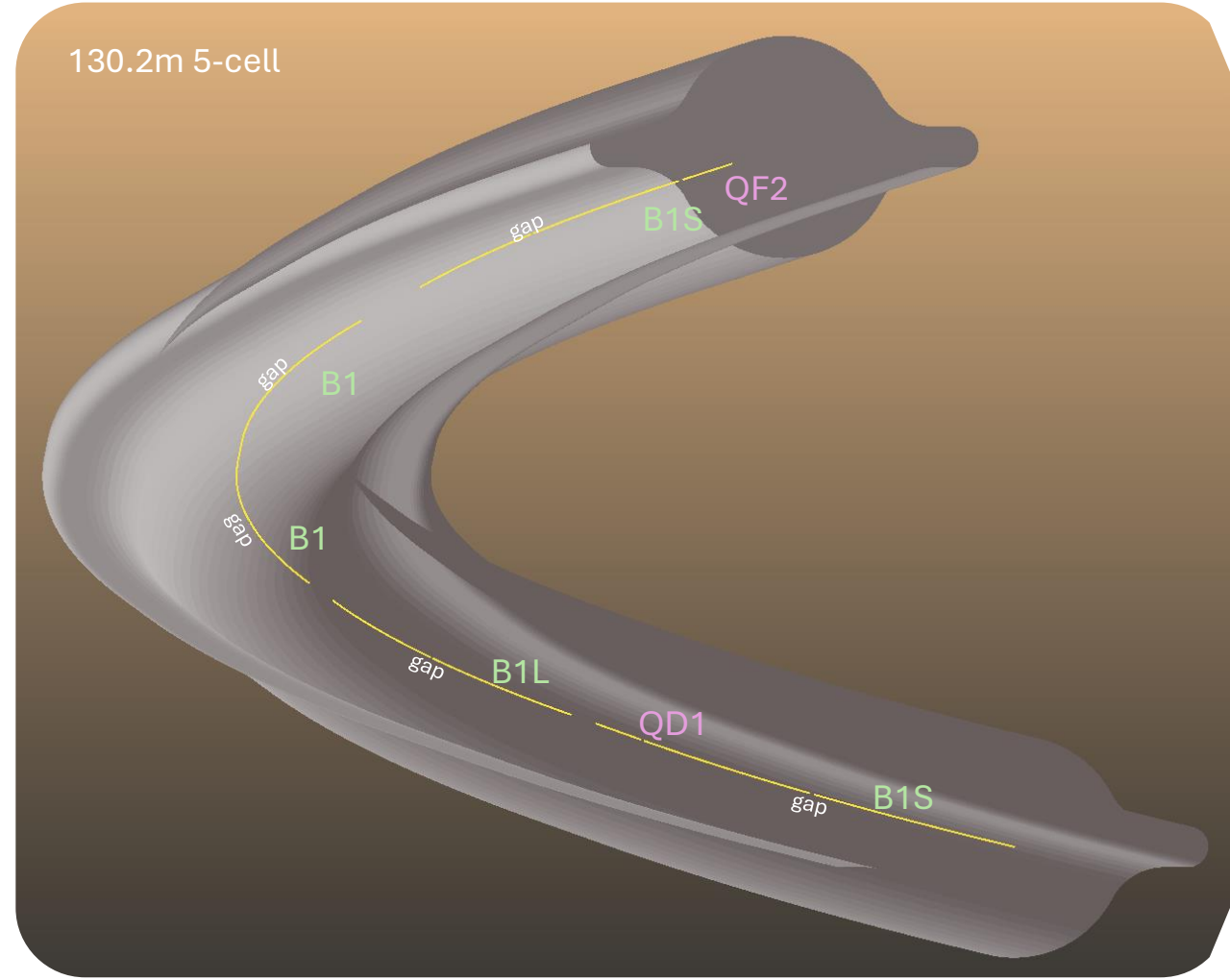


Lattice functions kept the same

Generate SynRad geometry and optics

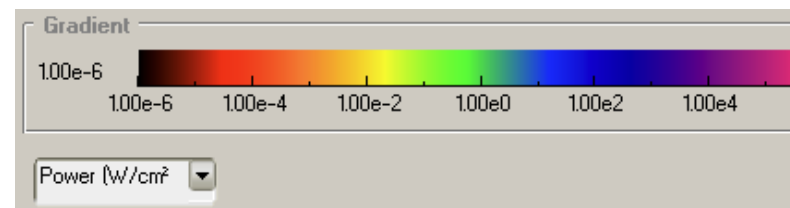
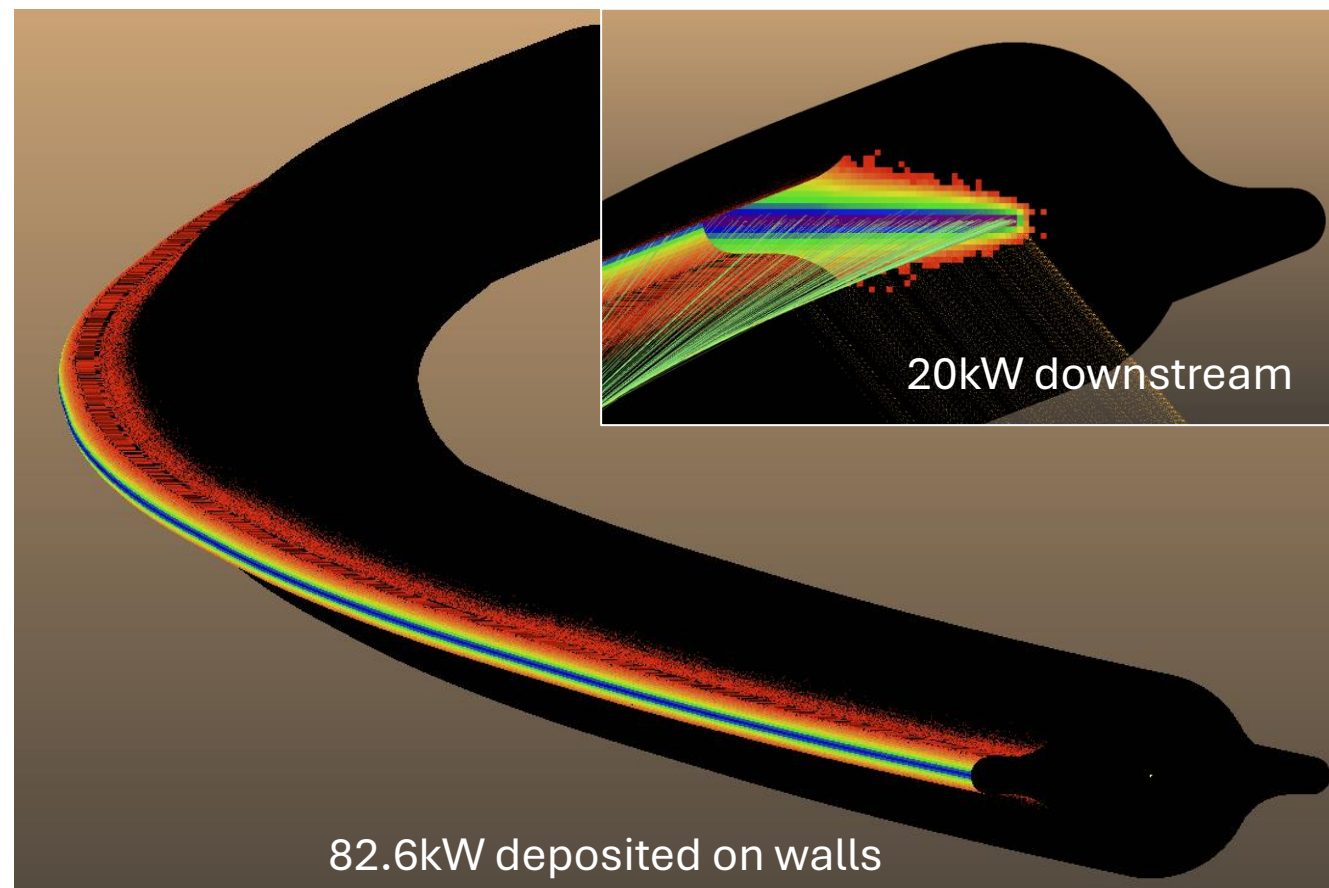
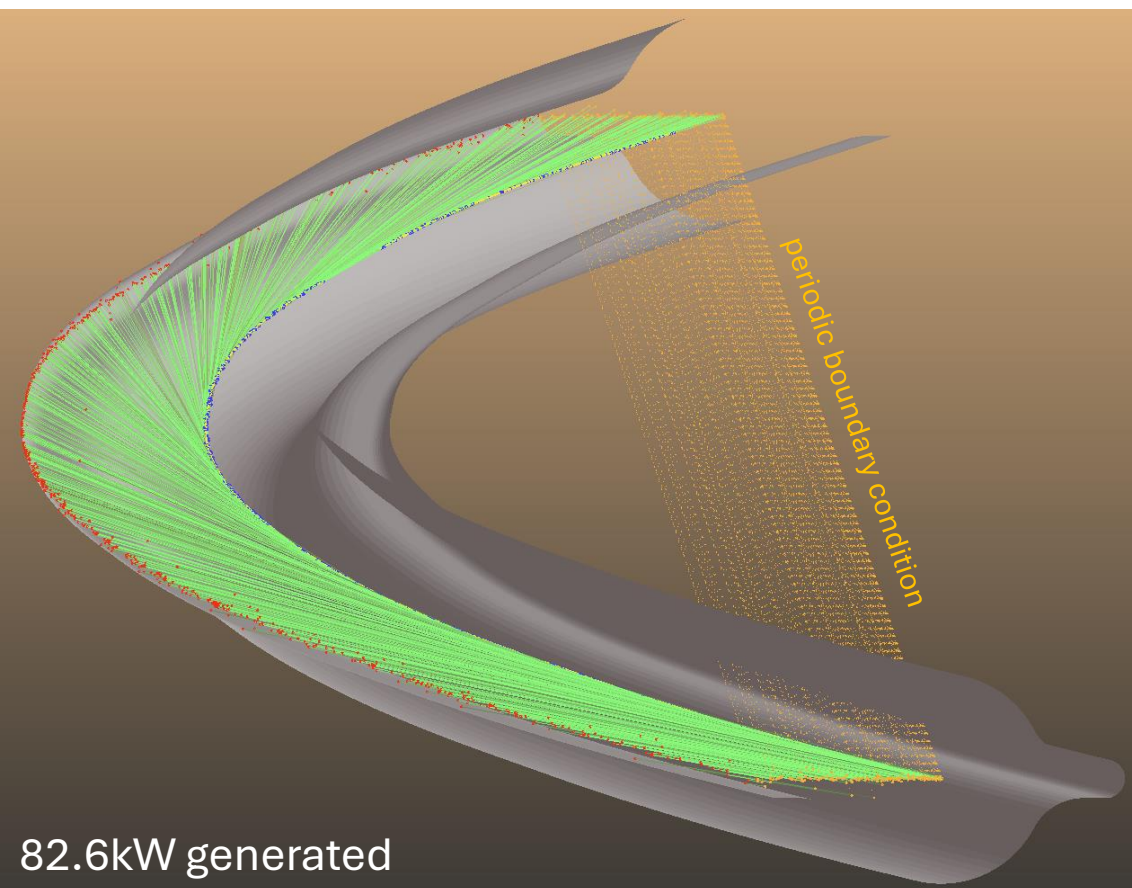


Geometry: 17100 polygons

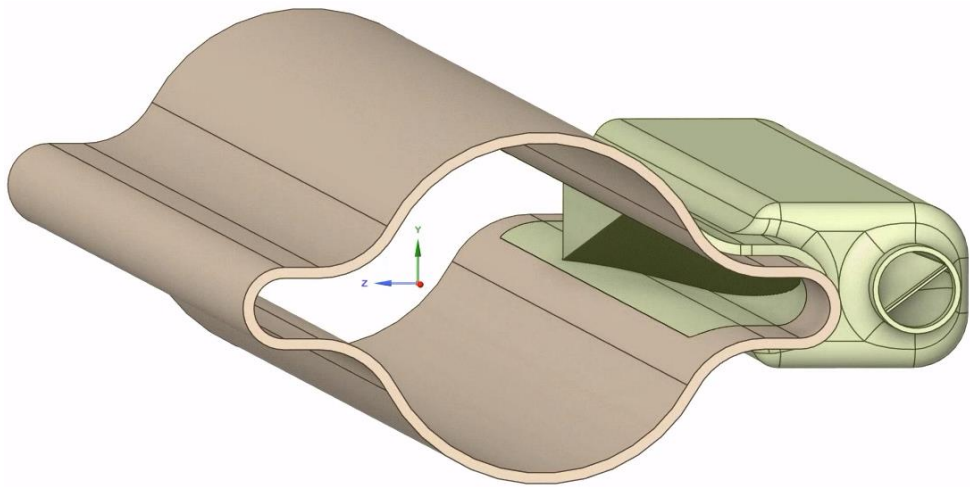


adding optics

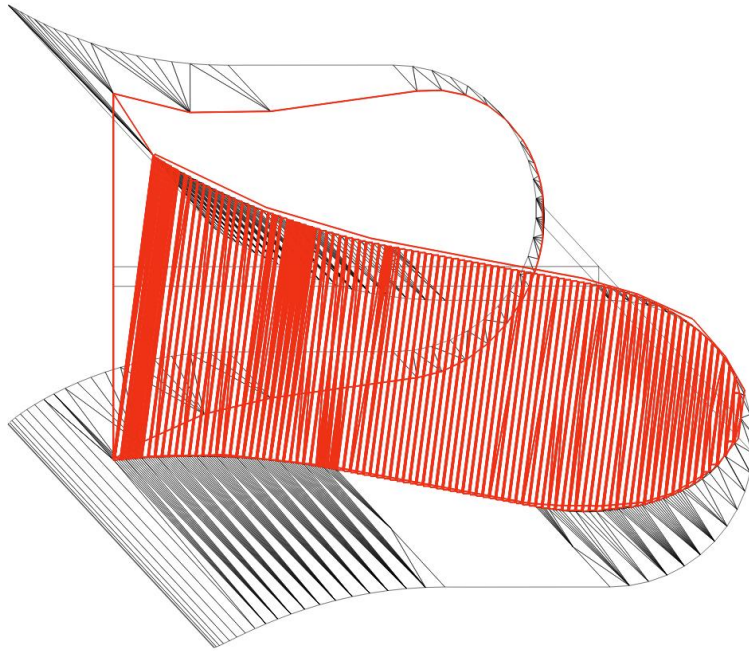
Simulation: verifying photon generation (no absorbers)



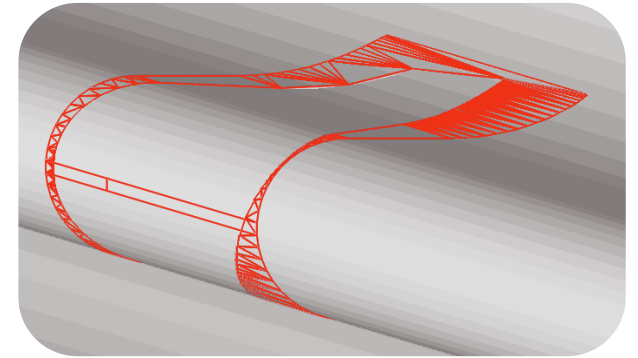
Adding the sawtooth* absorbers



Model (Fabrice Santangelo, TE-VSC)



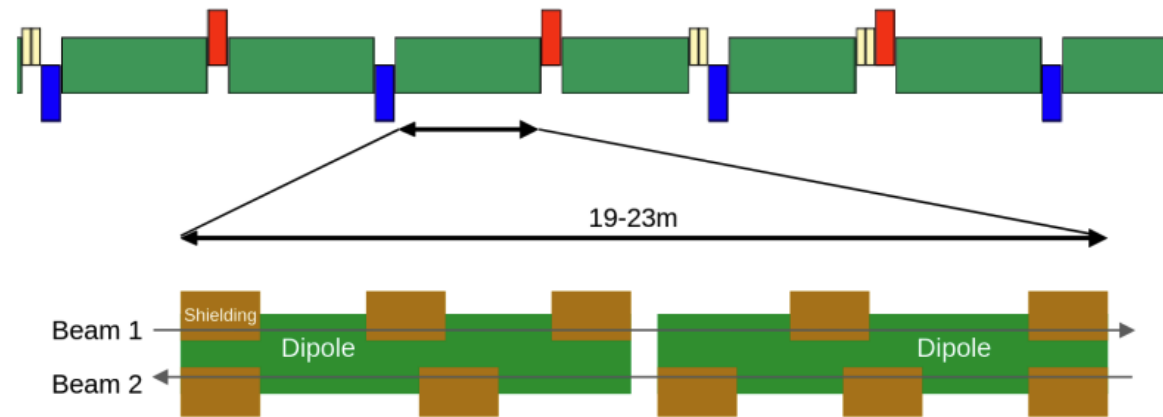
1134 polygons
sawtooth modeled as-is



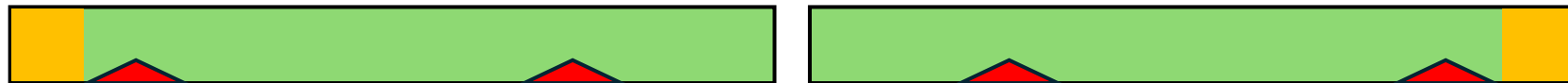
transparent facets help align

* Sawtooth details: see talks of Marco Morrone and Stefania Grozavu in this session

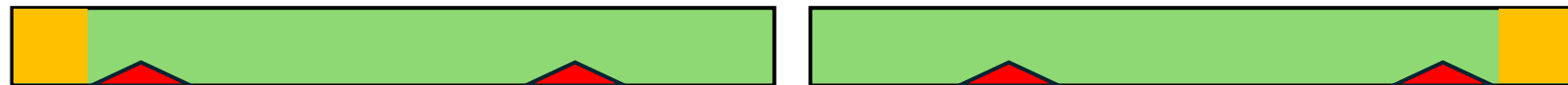
Add absorbers: first attempt – equal spacing



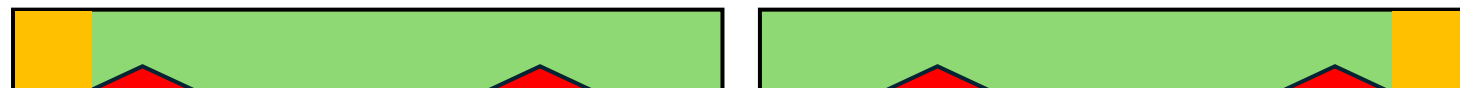
B1 (22.655m)



B1L (21.155m)

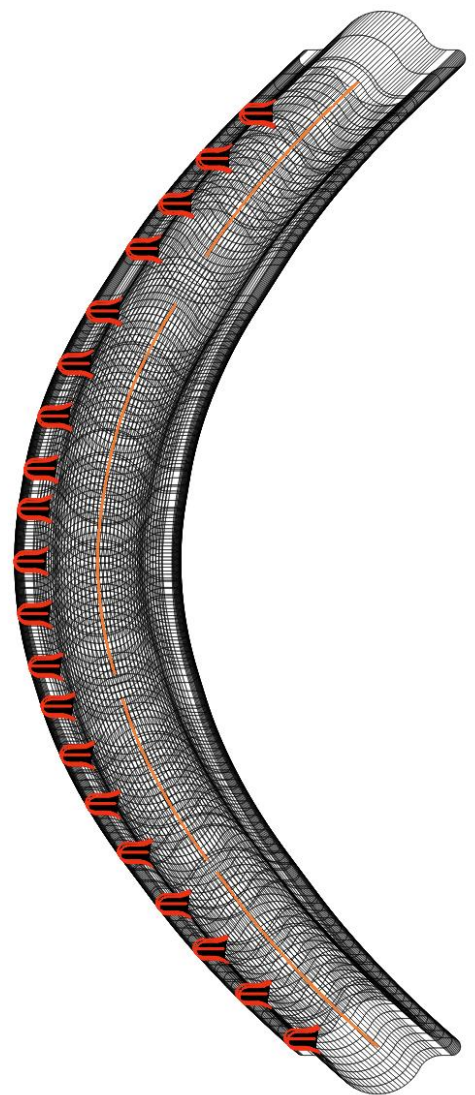


B1S (19.7m)

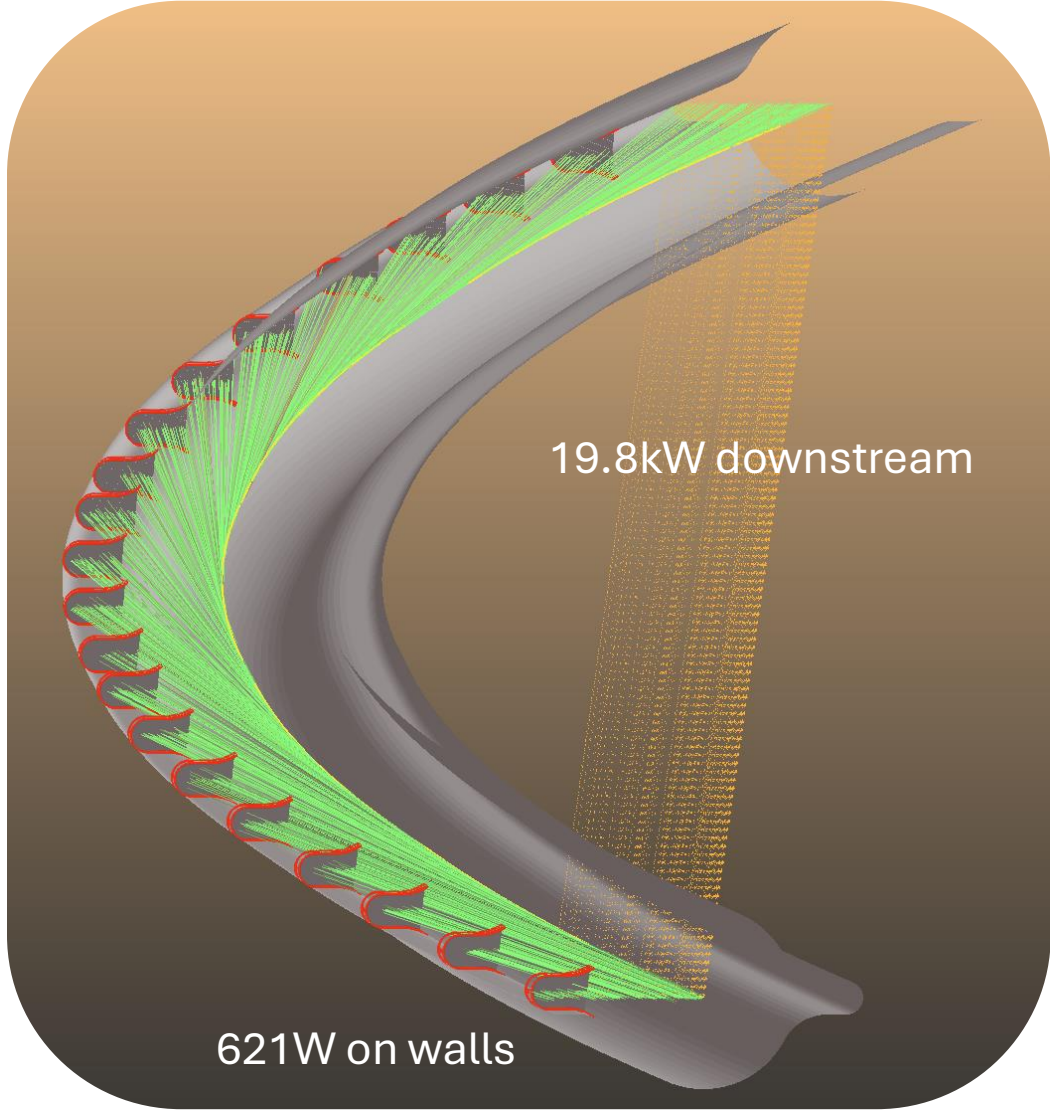


55cm / 75cm reserved for shielding

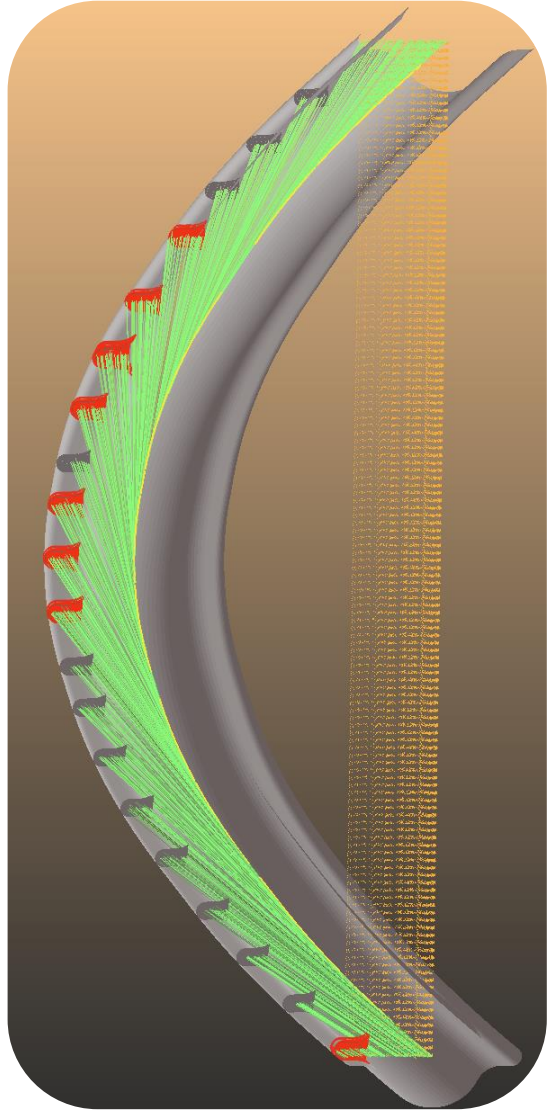
Simulation: equal spacing



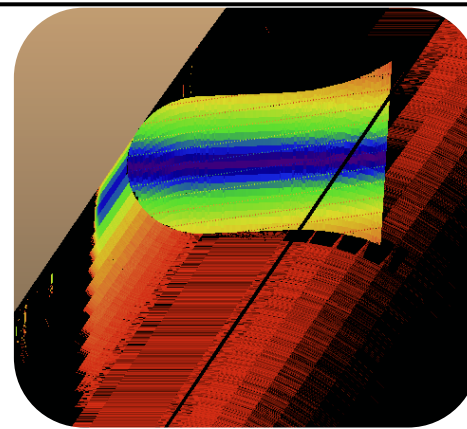
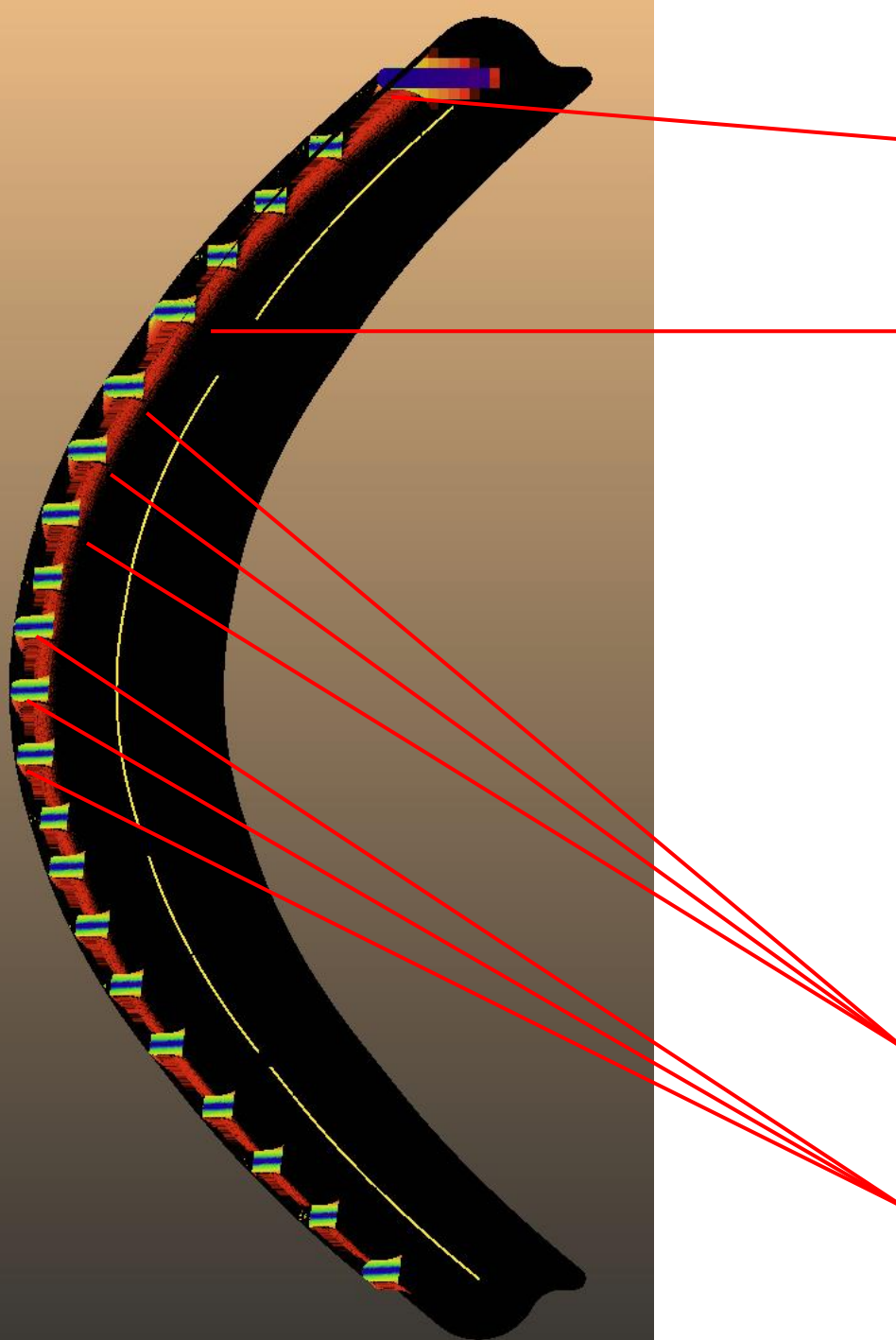
5 dipoles * 4 absorbers = 20 total



82kW on absorbers (4.1kW avg, 4.8kW max)

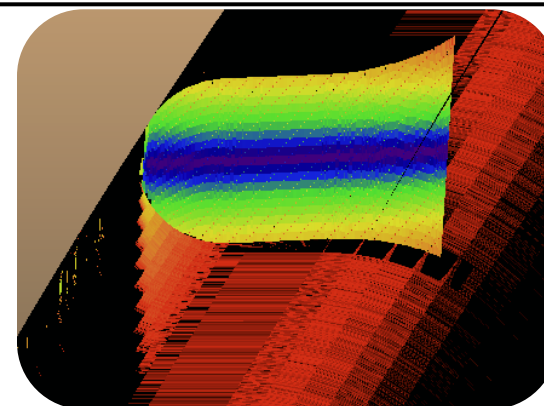


8 abs > 4.5kW

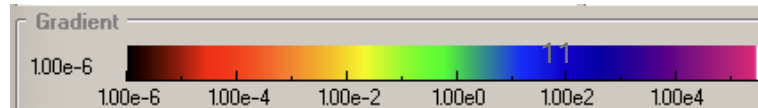


B1.199_second_half	11.177686115	0.001130430682	-0.01538244039
DRIFT_817	6.35		
B1S.157_first_half	9.702686115	0.0009832351085	-0.0154134057
B1S.157_second_half	9.702686115	0.0009832351085	-0.0154134057
DRIFT_818	0.3	} 6.35m	
QD1.12	2.9		
DRIFT_819	3.15		

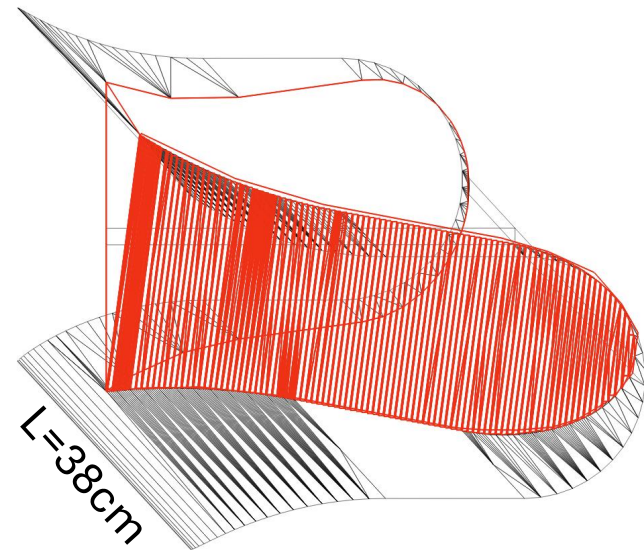
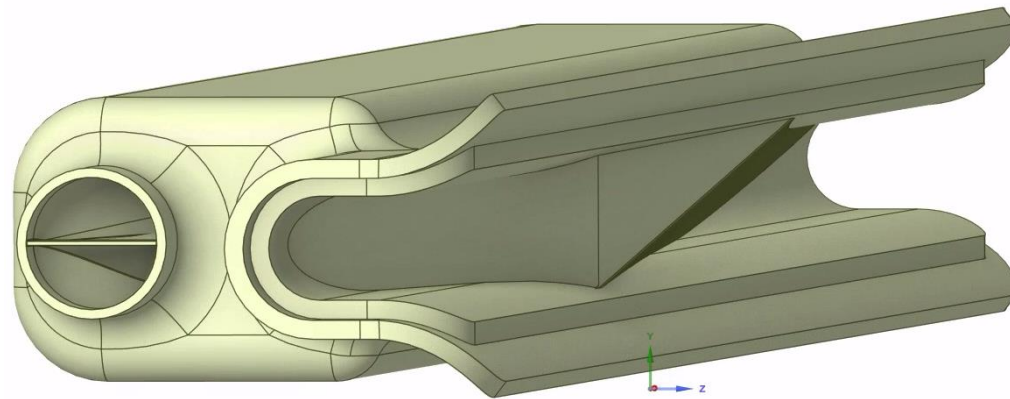
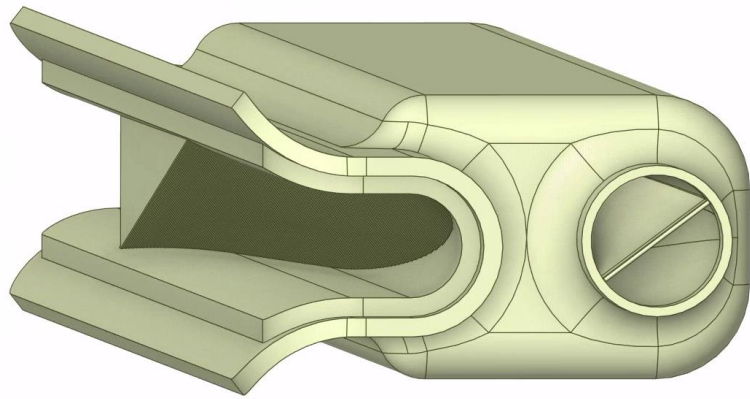
Expected problems (>6m drift)



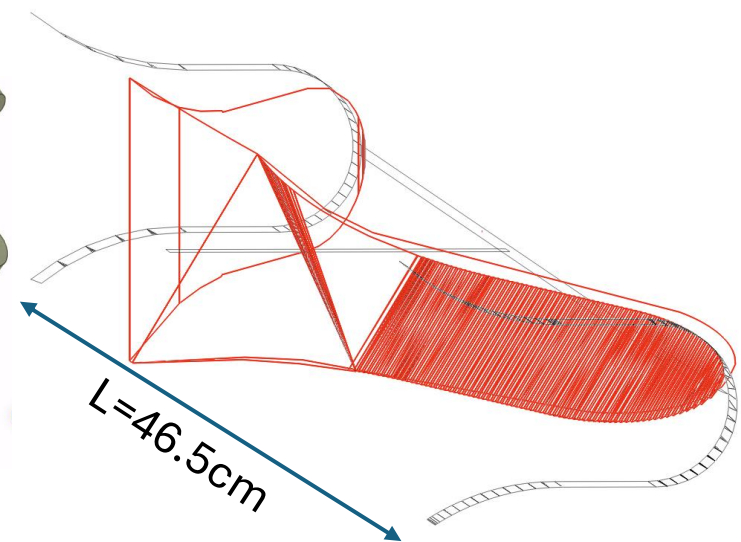
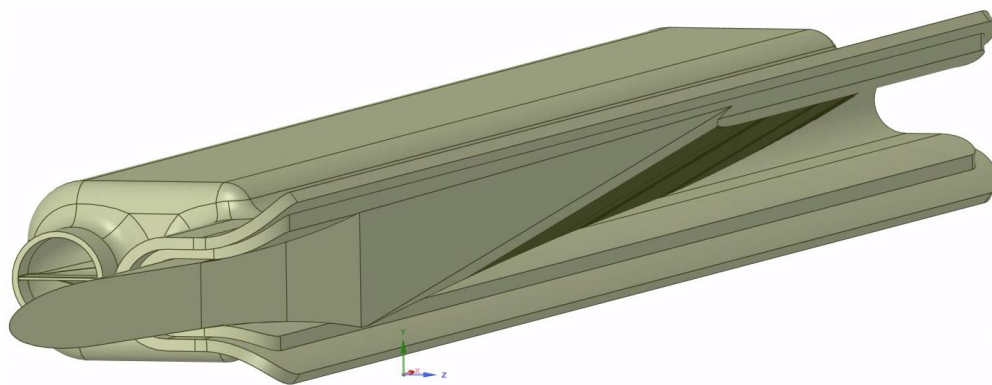
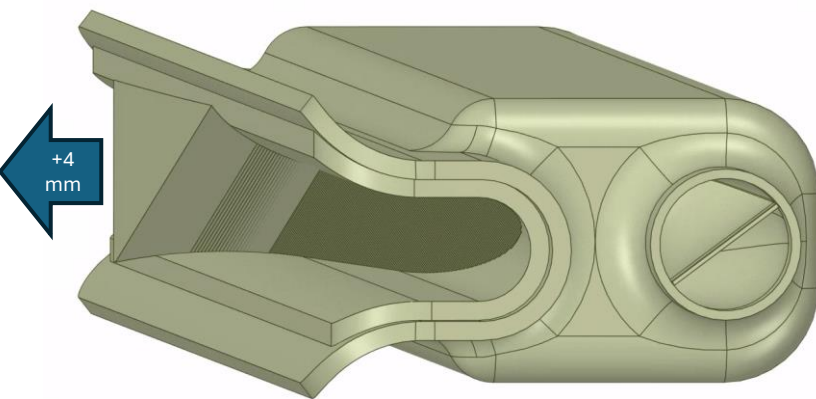
B1 magnets: too sparse spacing



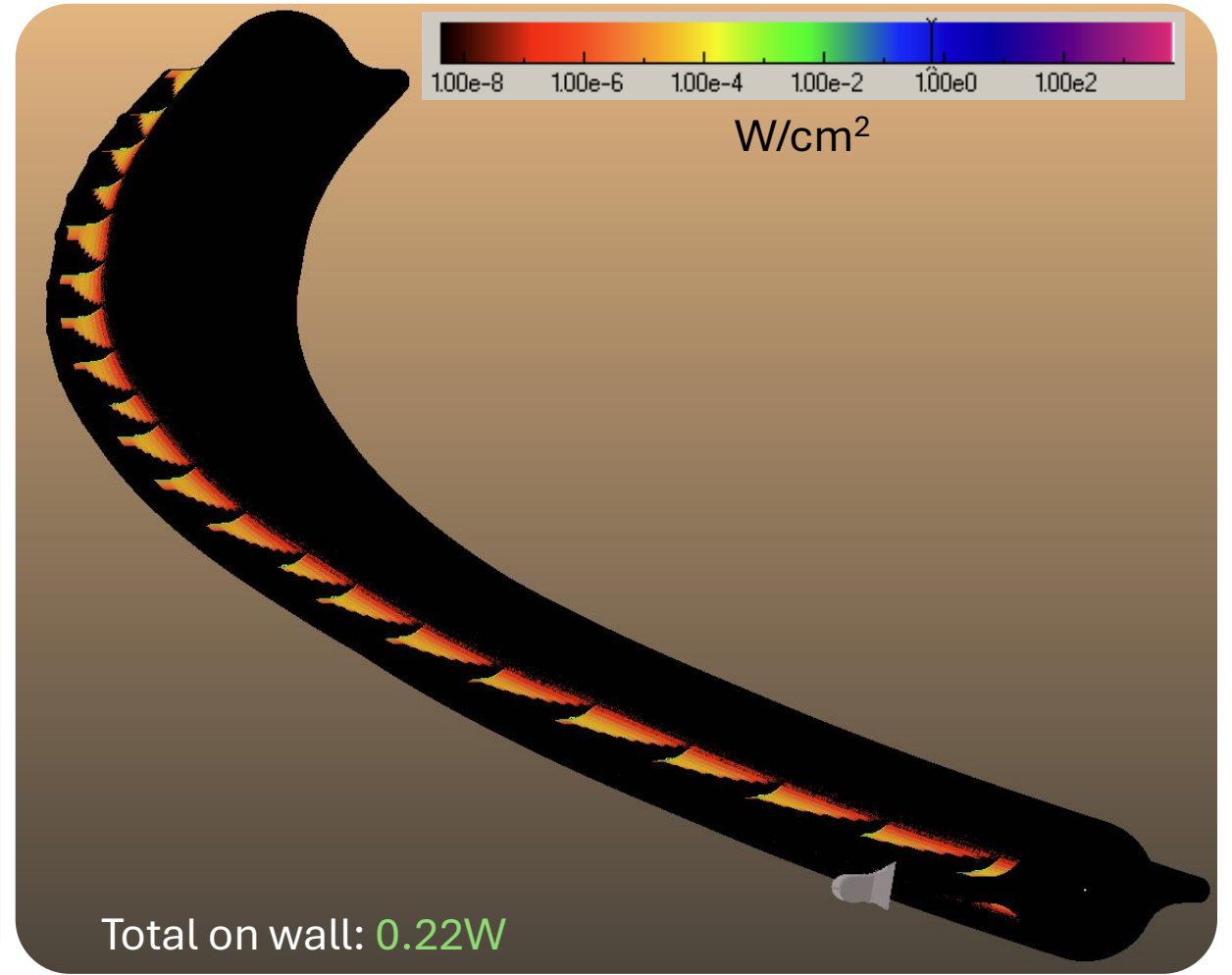
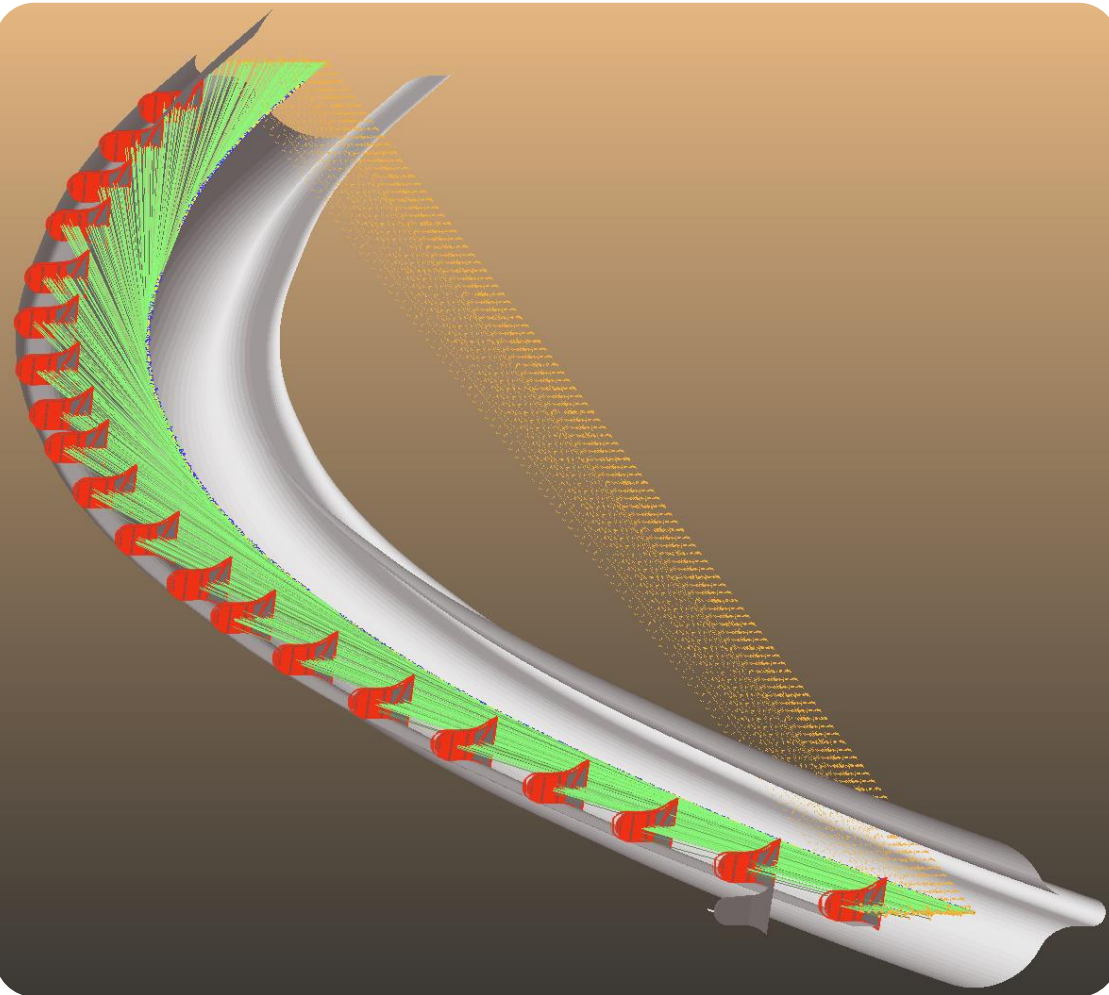
Original sawtooth absorber model (F. Santangelo)



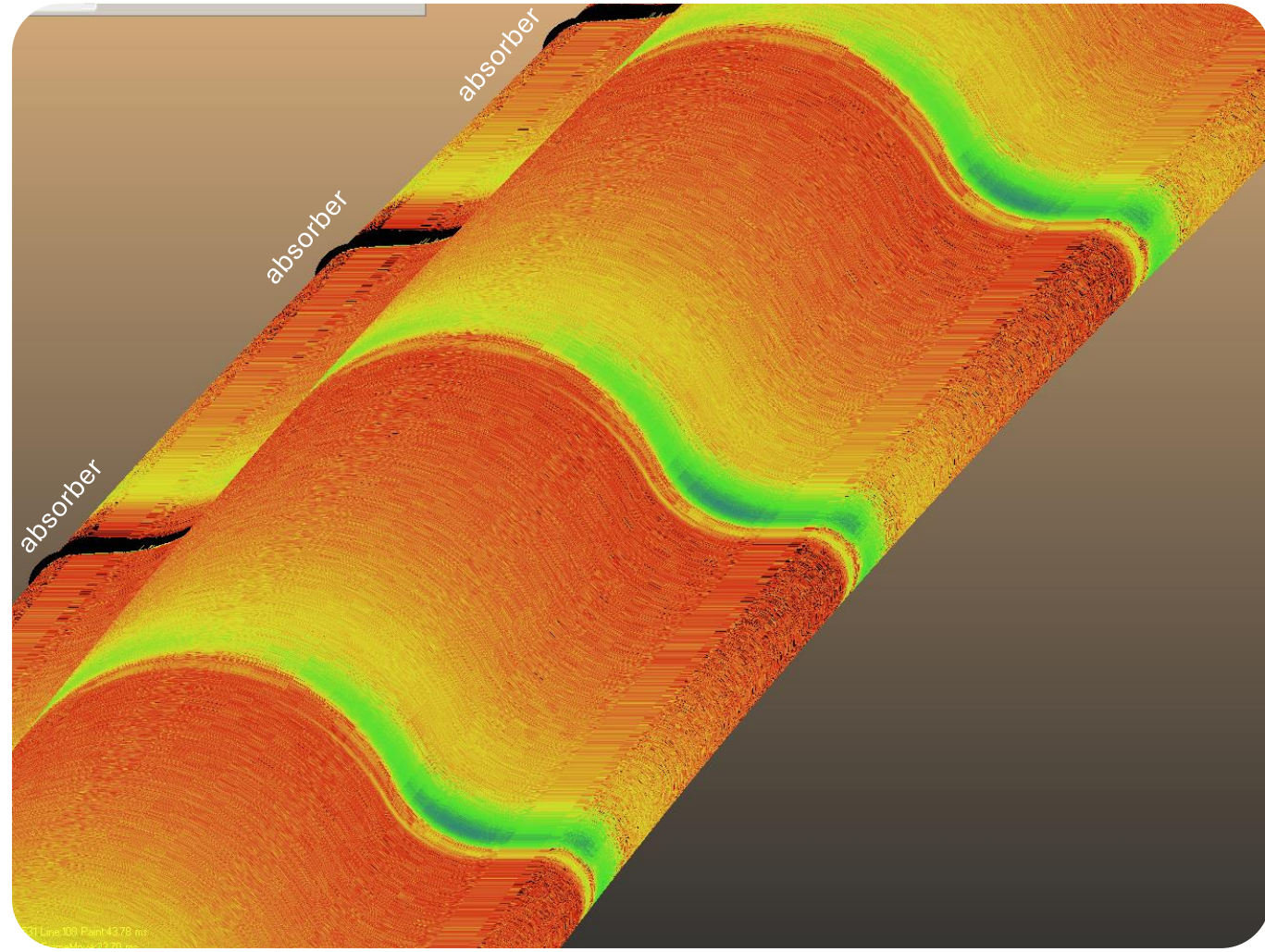
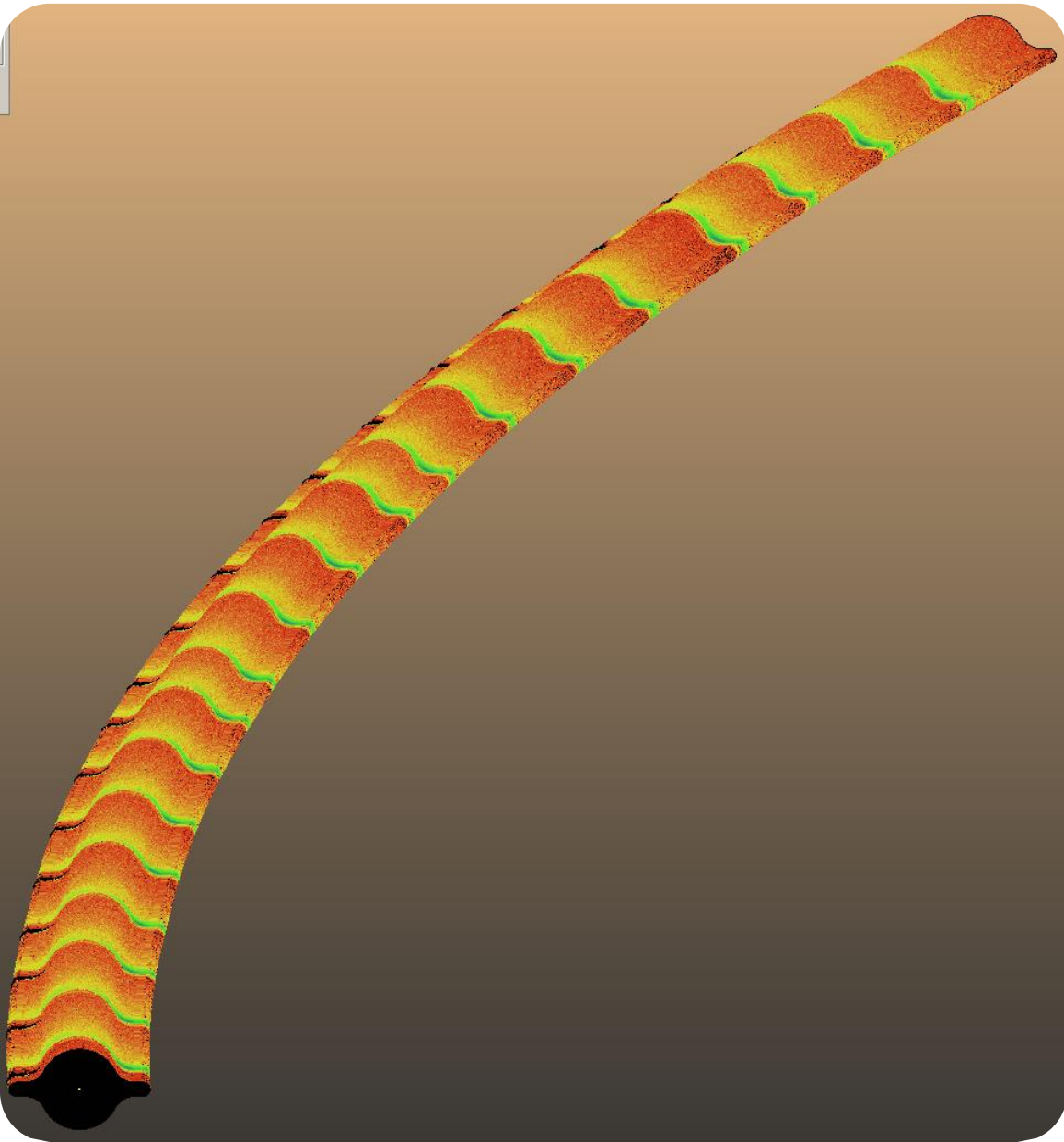
Modification (preliminary, partial sawtooth)



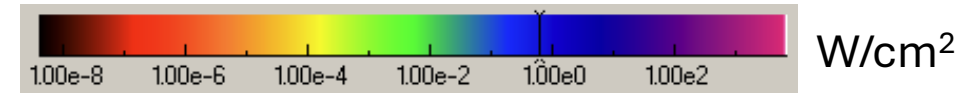
Larger absorbers: Negligible direct hits on outer walls



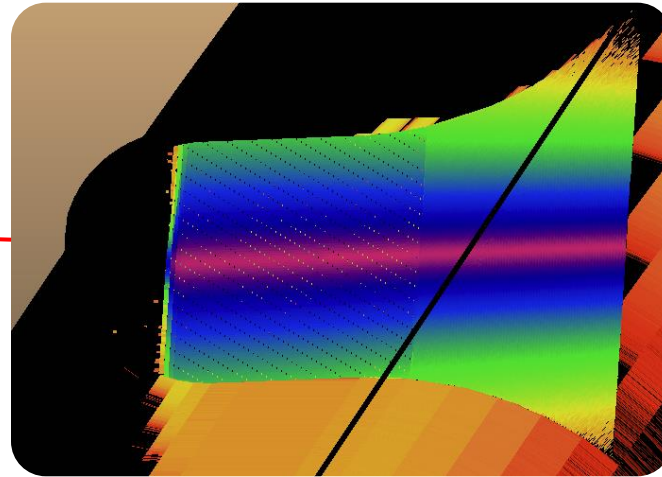
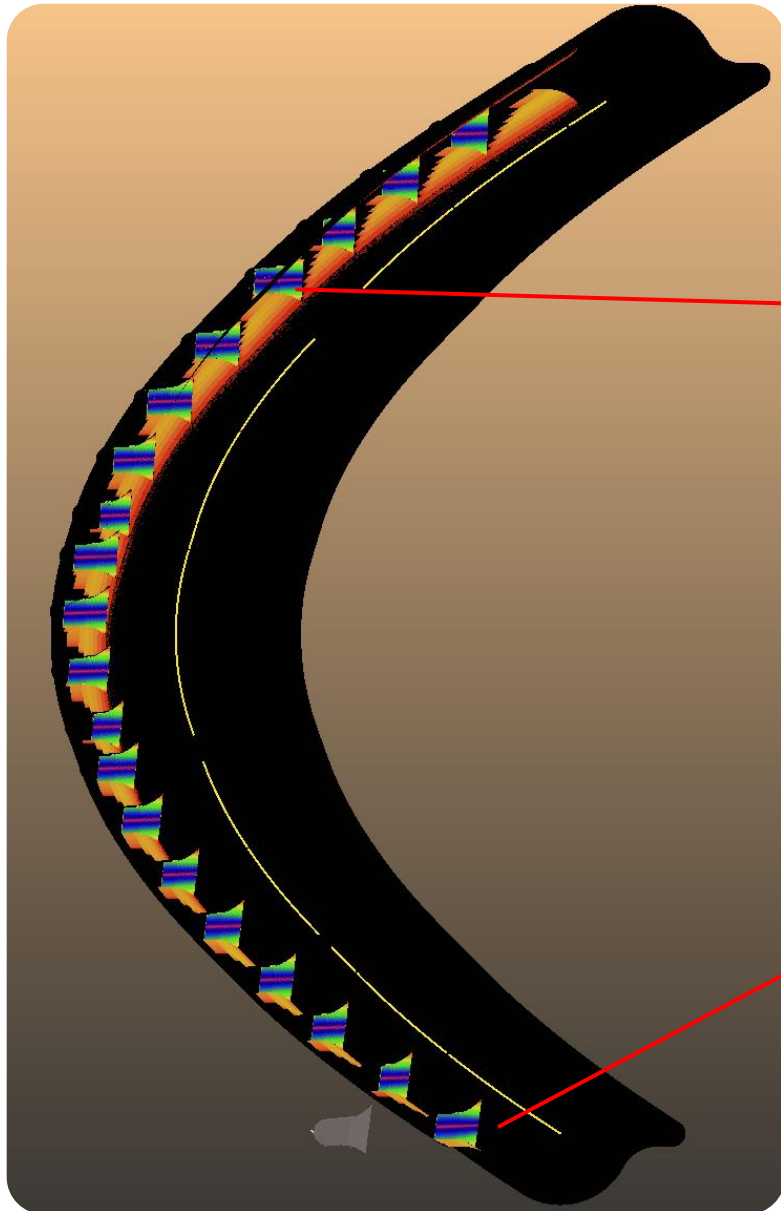
Secondaries: 380W (2.9W/m) on walls



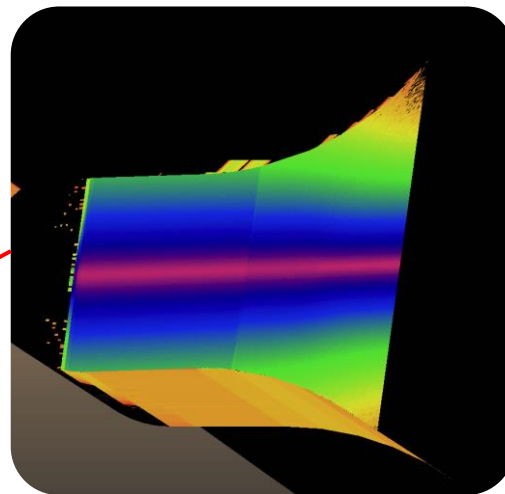
Largest load opposite absorbers



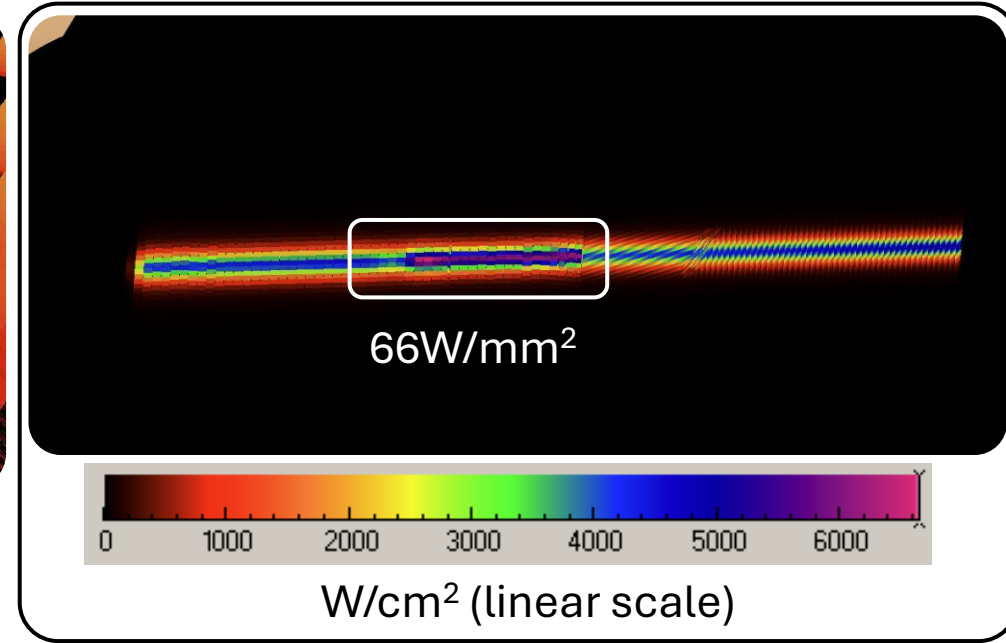
Load on absorbers: largest after drifts



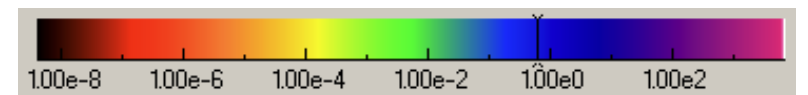
5200W



4580W



66W/mm²



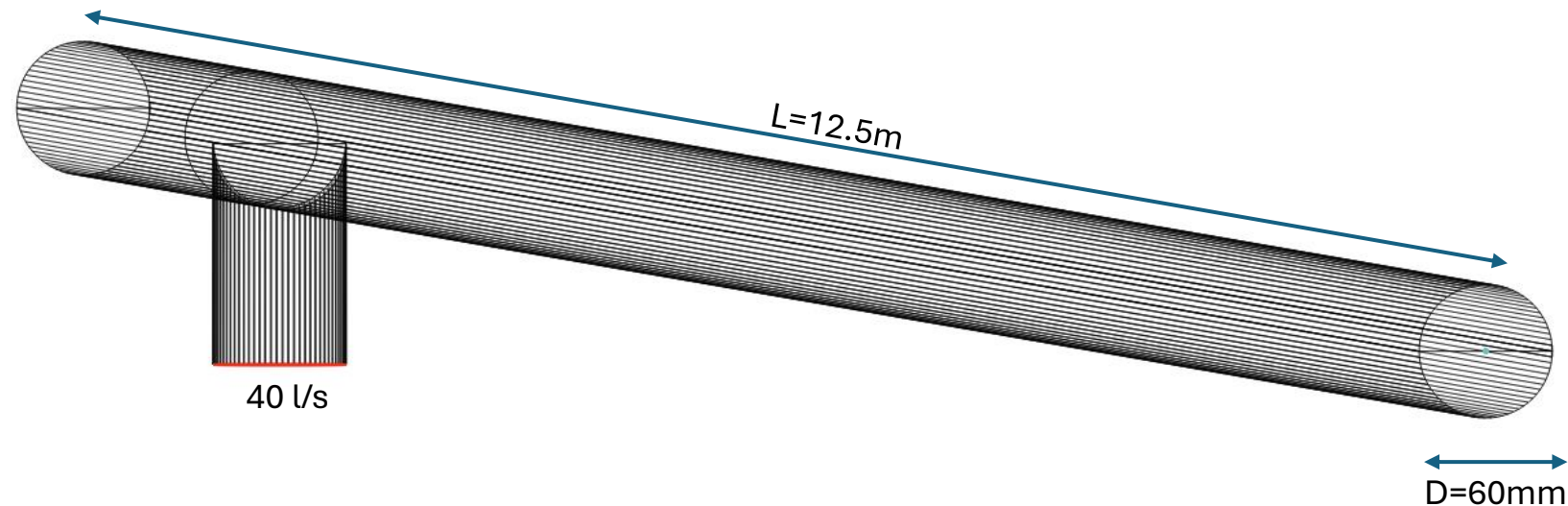
W/cm²

Conclusion (collider SR management)

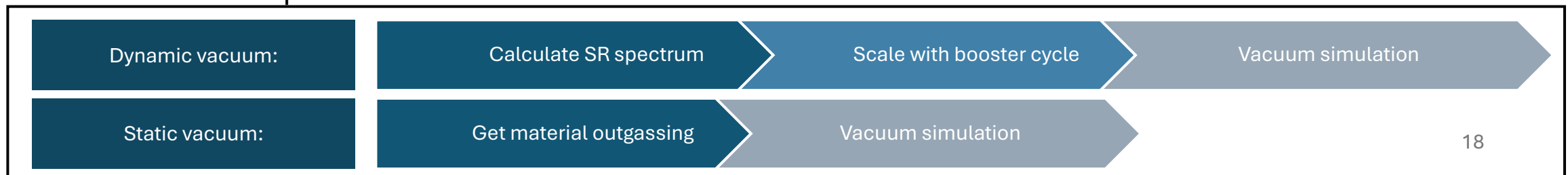
- Increasing the absorber protrusion shows complete shadowing
- Should be repeated with real sawtooth (0.9mm sides)
- Total power (5.3kW) – check with cooling simulations
- Power density: decrease angle and make longer?
- 46.5cm too long for 3D printer
- Impedance validation required
- If above passed, 4 absorbers/magnet feasible

Second part: booster ring pressure profiles

- Can we build the booster ring without bakeout and without NEG coating?
- A representative 12.5 m-long "half-cell" model with a 60 mm inner diameter was analyzed, featuring a single 40 l/s ion pump placed between the dipole and quadrupole magnets (lumped pumps in absence of NEG)



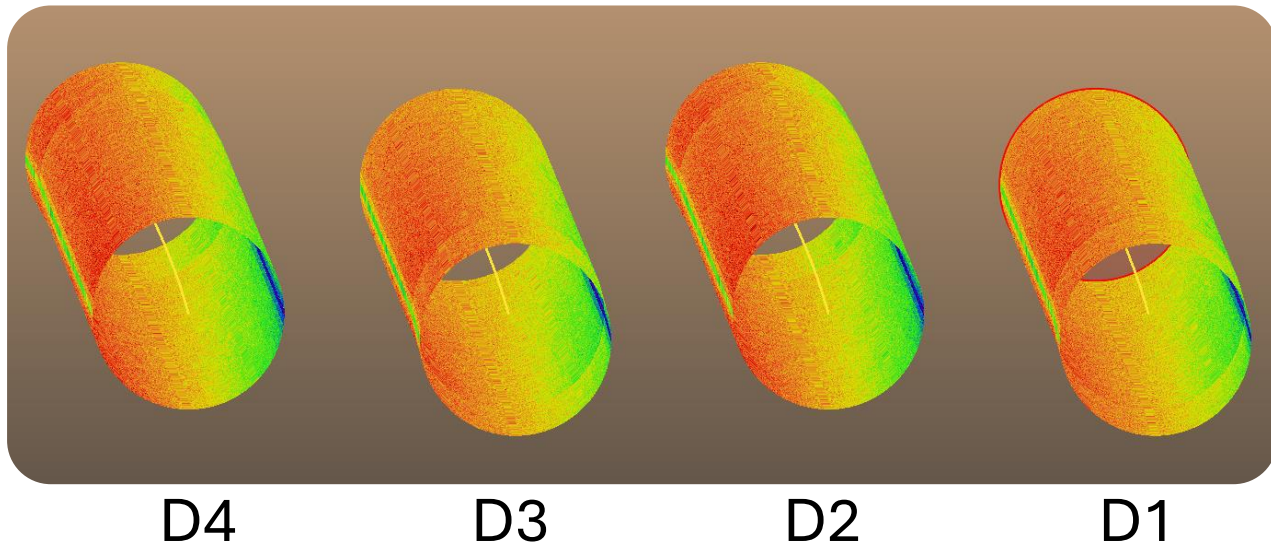
Calculation steps



Dynamic vacuum

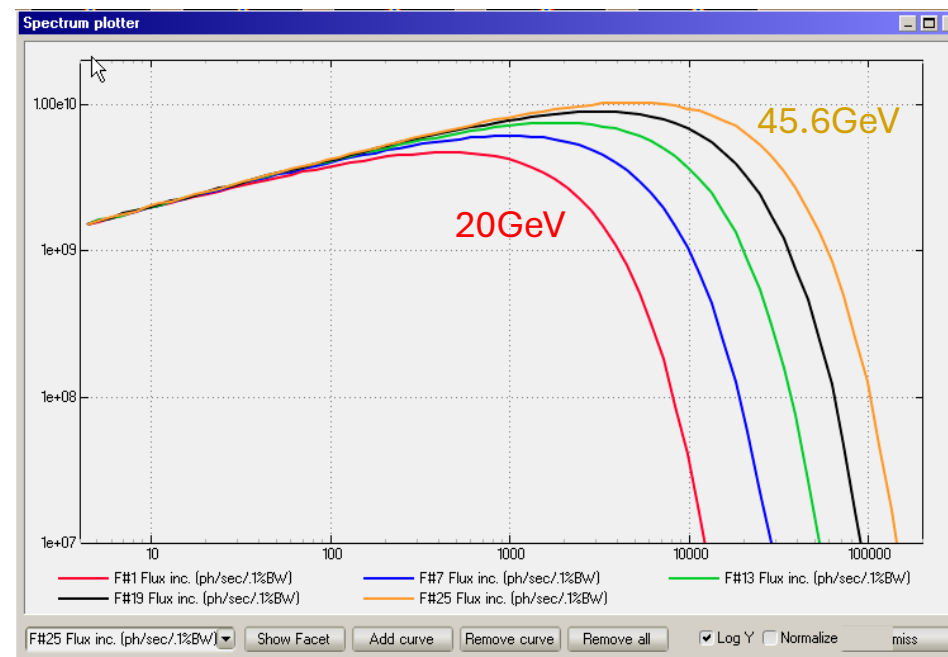
Step1: Estimate synchrotron radiation

Dipoles



Magnet parameters:

- B=6.5mT at 20GeV
- I=14.83mA*
- L=4*11m



Part of SR above 4eV ("SR_factor"):

- 20 GeV: 83%
- 45.6GeV: 92%
- took the average

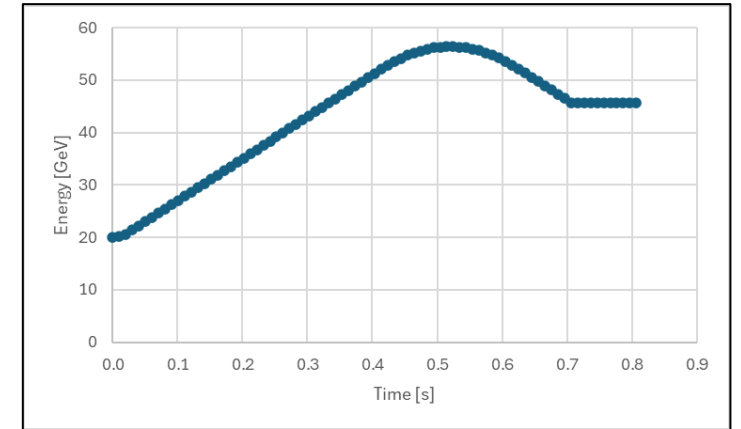
Practical formula: Flux = $8.08E17 * E[GeV] * I[mA] * SR_factor * Ring_fraction = 2.36E17$ photons/s (at mid-energy, full current)

SynRad result: $2.24E17$ photons/s

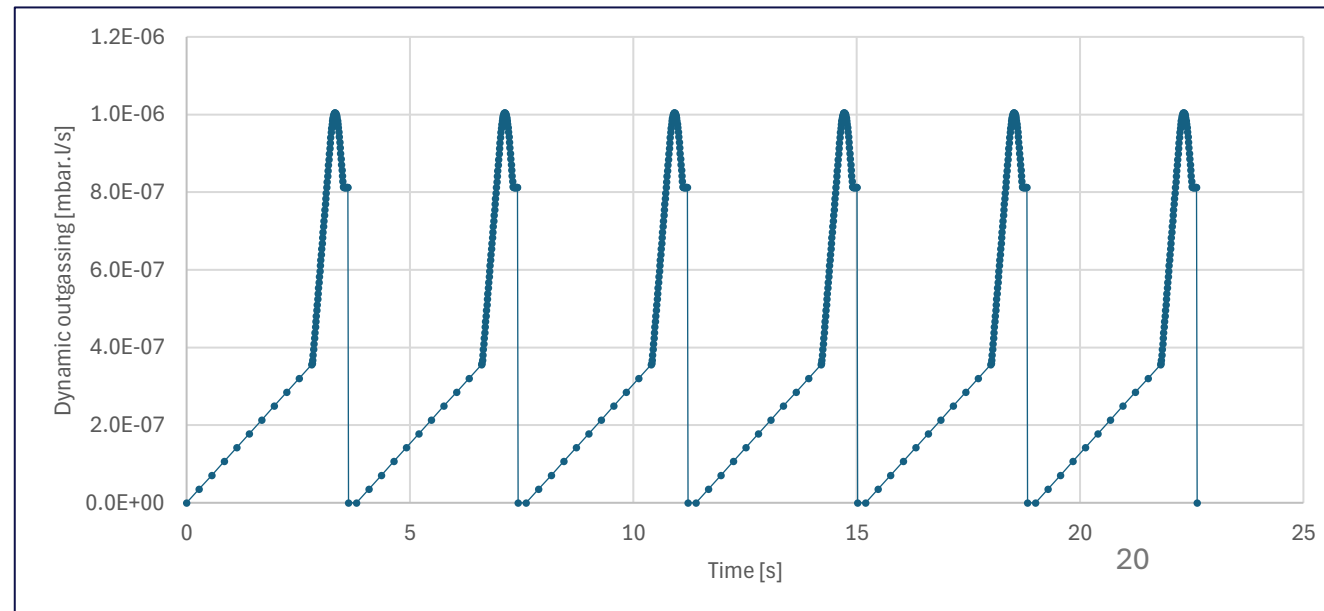
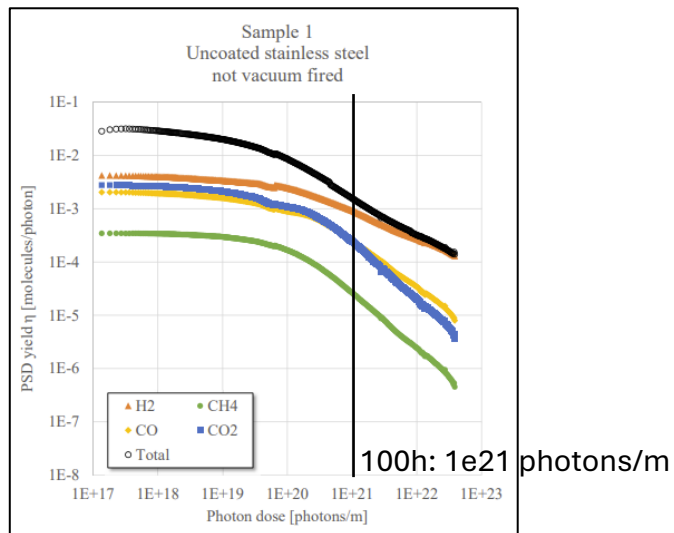
Dynamic vacuum

Step2: construct dynamic outgassing for vacuum simulation

- Representative booster cycle (Z mode):
 - 2.8s accumulation: 0 to 14.83mA linear current increase
 - 0.8s ramp-up cycle with energy overshoot
 - 0.2s magnet ramp-down
- Flux = $8.08E17 * E[GeV] * I[mA]$
- Outgassing: $PSD_yield * Flux$
 - Choose $\eta=3E-4$ mol./photon for CO



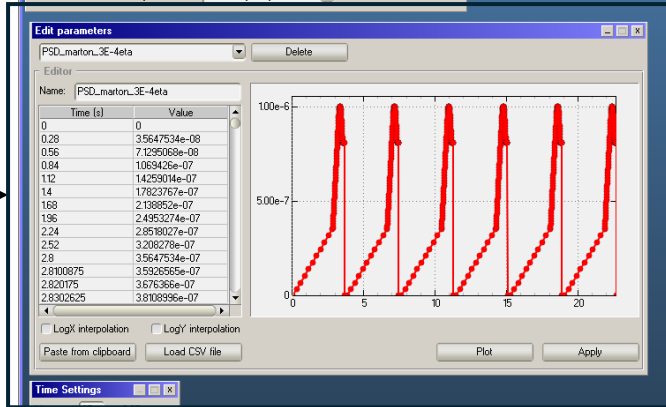
digitized data: Antoine Chance (CEA)



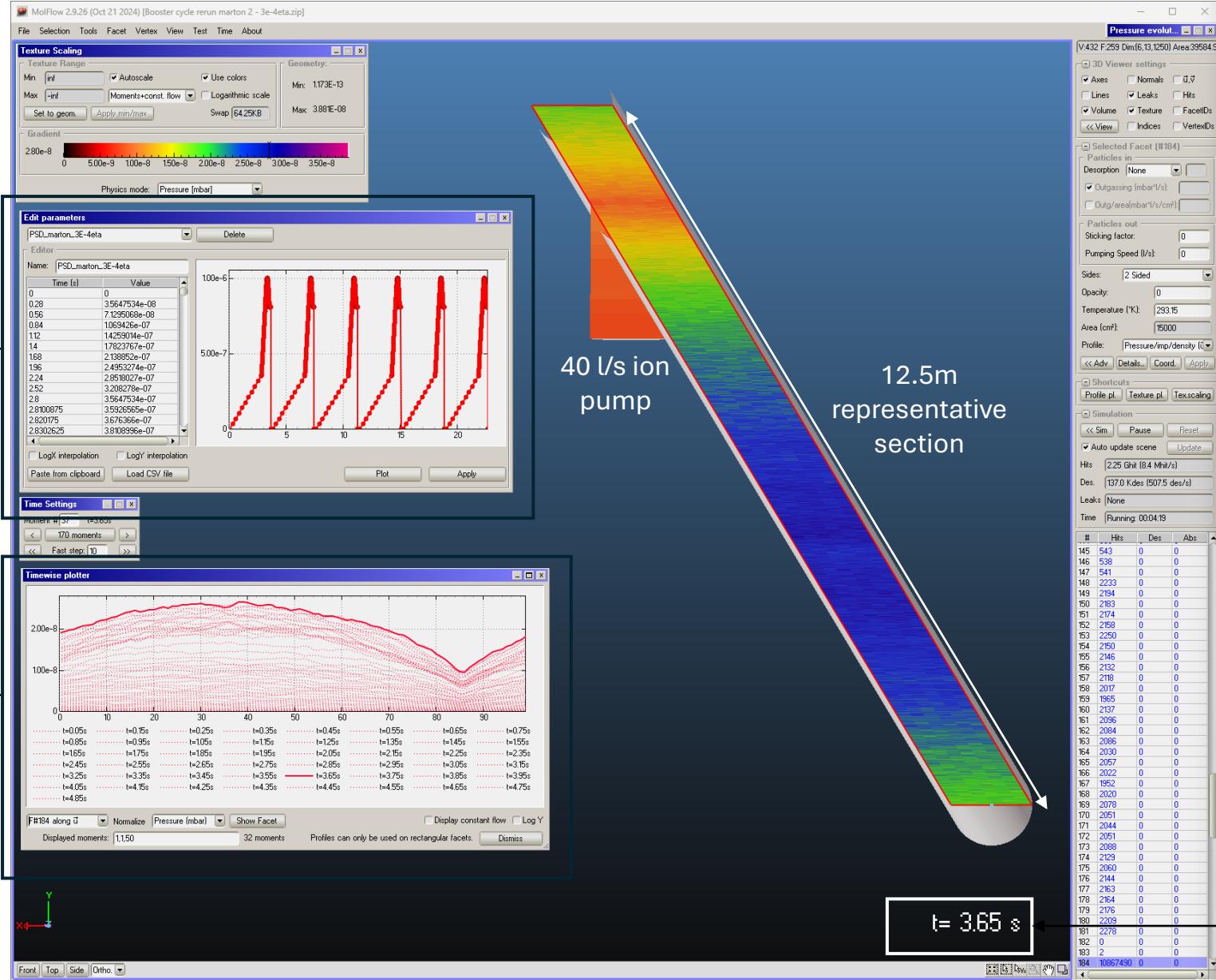
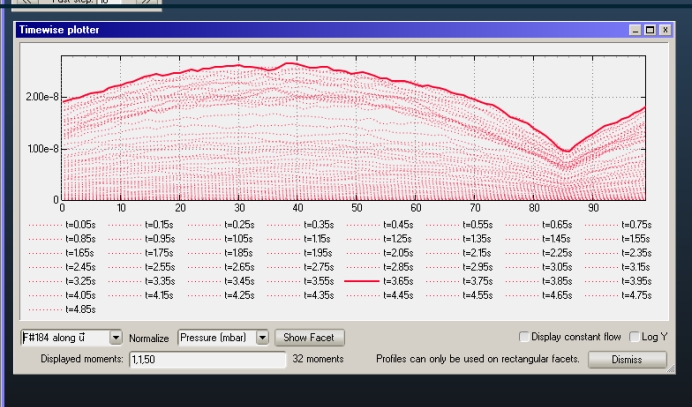
Dynamic vacuum

Step3: vacuum simulation

Time-dependent outgassing



Pressure profiles at different moments



Mass: 28 (CO)
Temp: 300K



Typically, the gas species are (ordered per fraction): H₂, CO, CO₂, CH₄ (baked system), plus H₂O (if unbaked), which can initially be the predominant gas specie

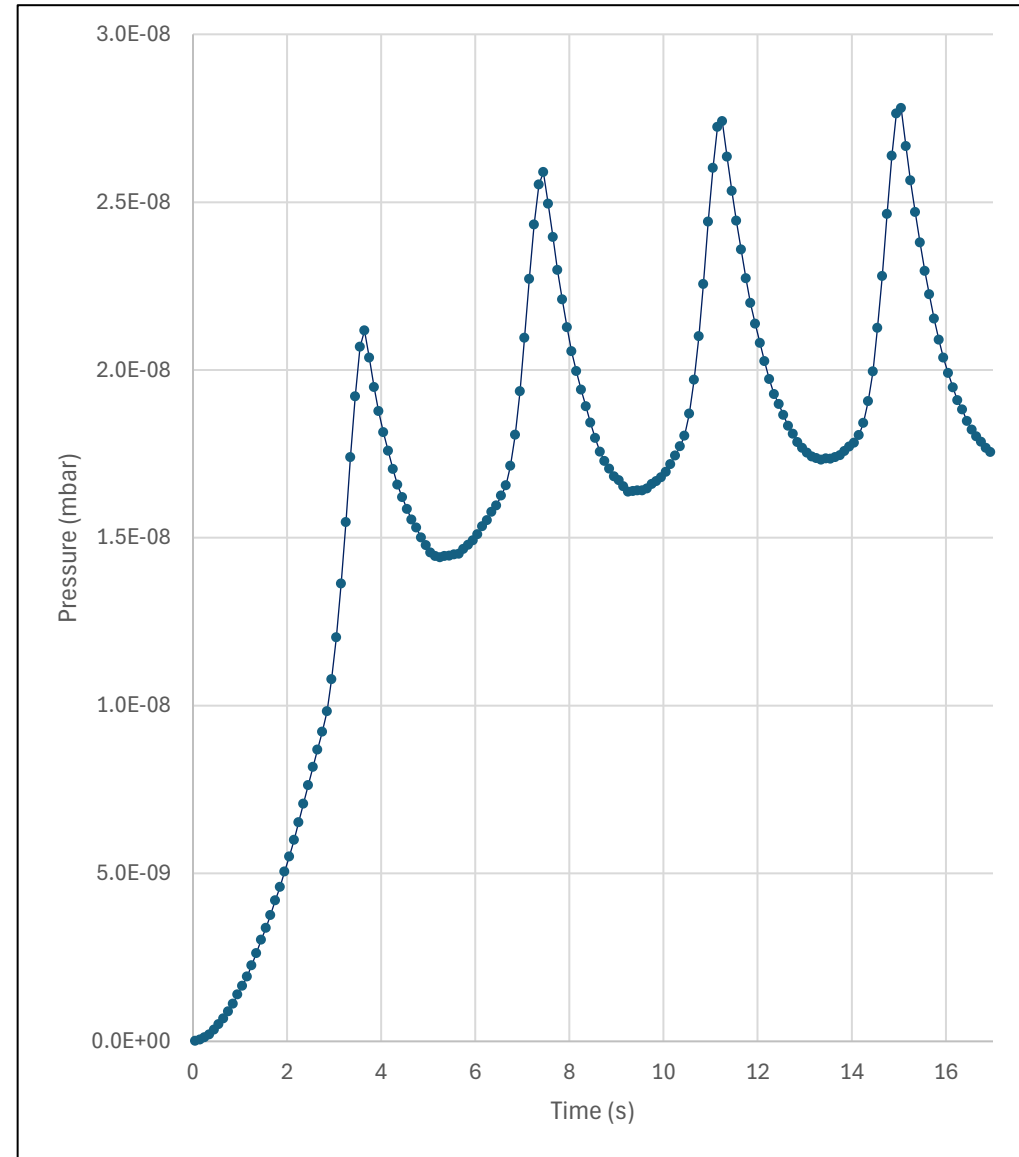
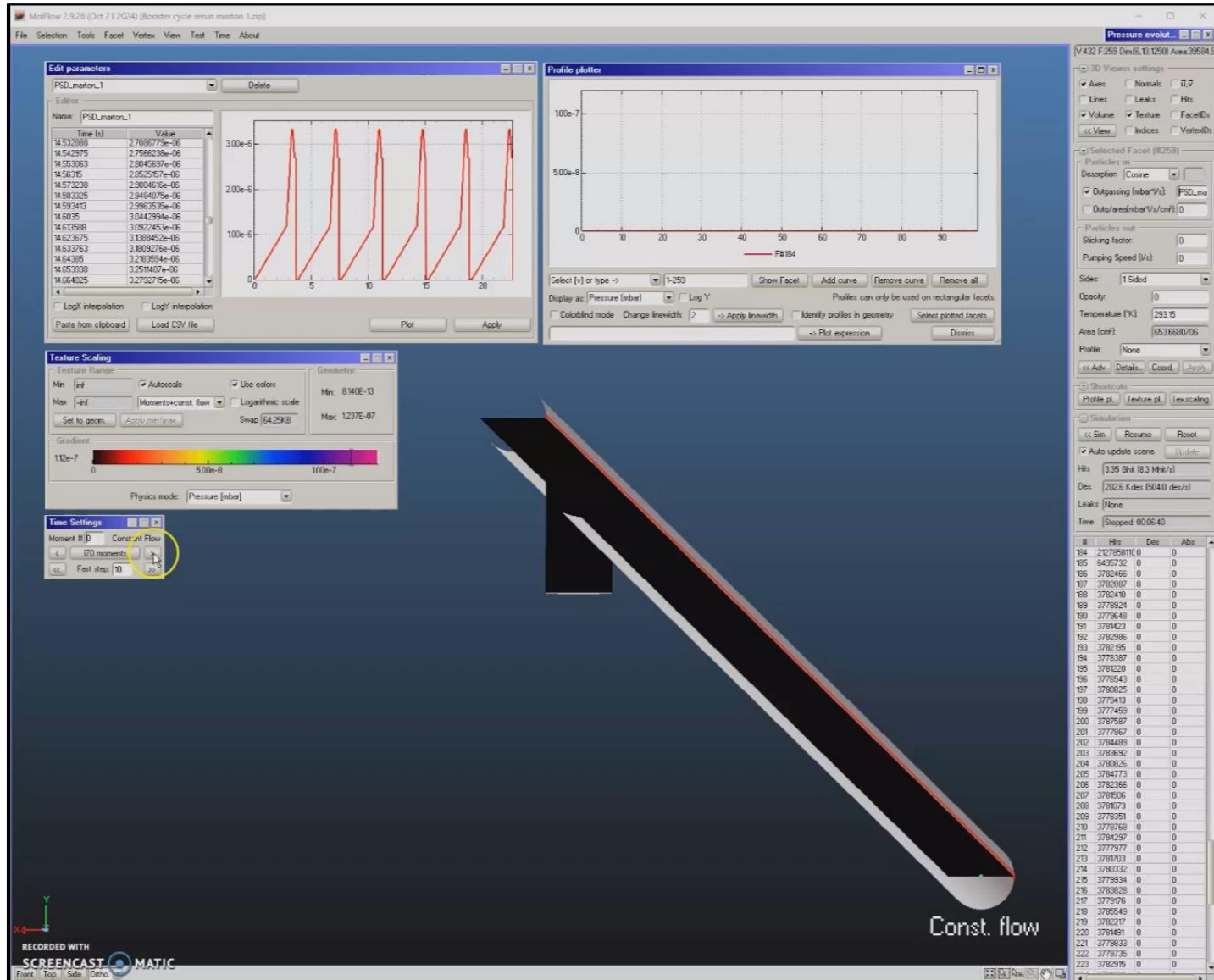
➤ We have considered CO because it has an atomic number much higher than that of hydrogen, and therefore its effect in terms of beam bremsstrahlung (BS) is ~15x bigger than for H₂... (Z_{eff}²(Z_{eff}+1) dependence for BS, Z_{eff} = weighted effective atomic number for C and O)

Snapshot displayed on model

t = 3.65 s

Dynamic vacuum

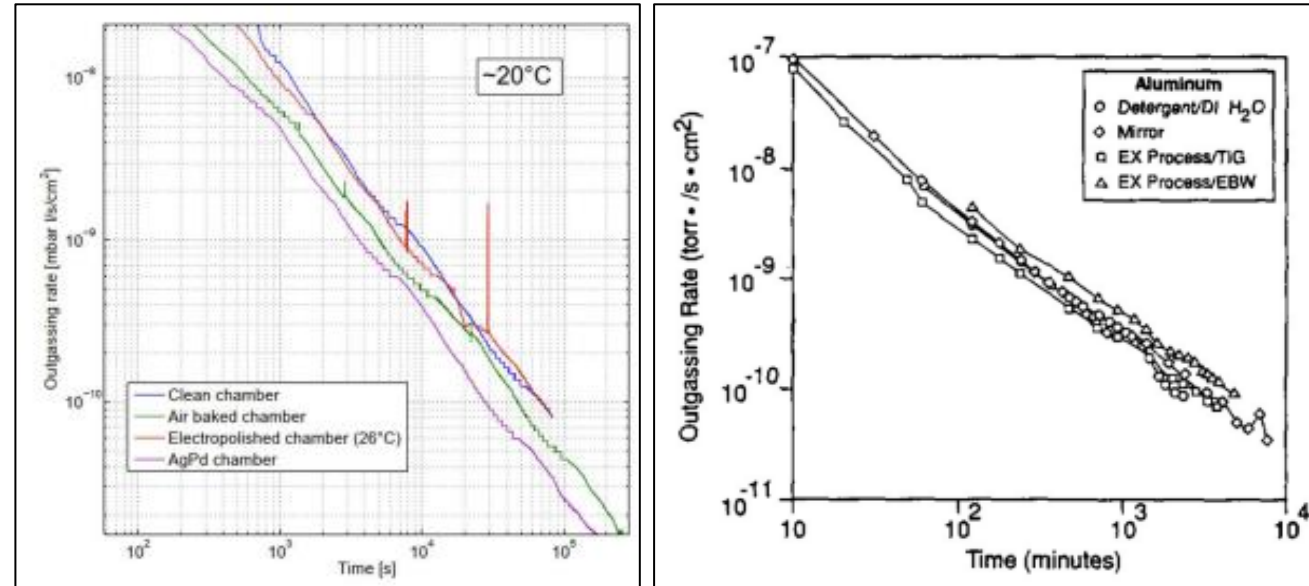
Step4: pressure results



Static vacuum

Step1: material outgassing rate

Unbaked materials: dominated by water vapor



4. Outgassing of water vapour from unbaked metal alloys

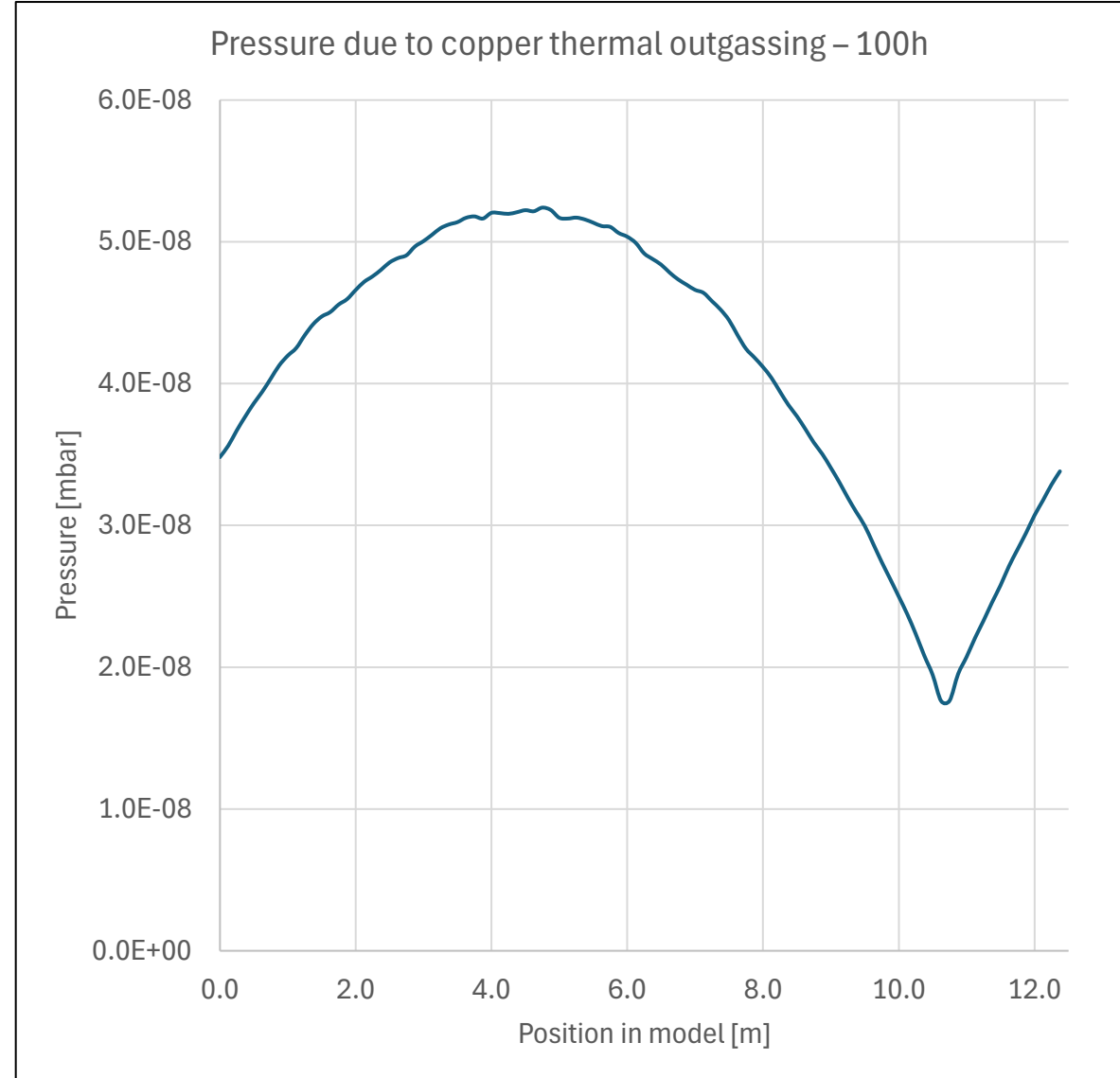
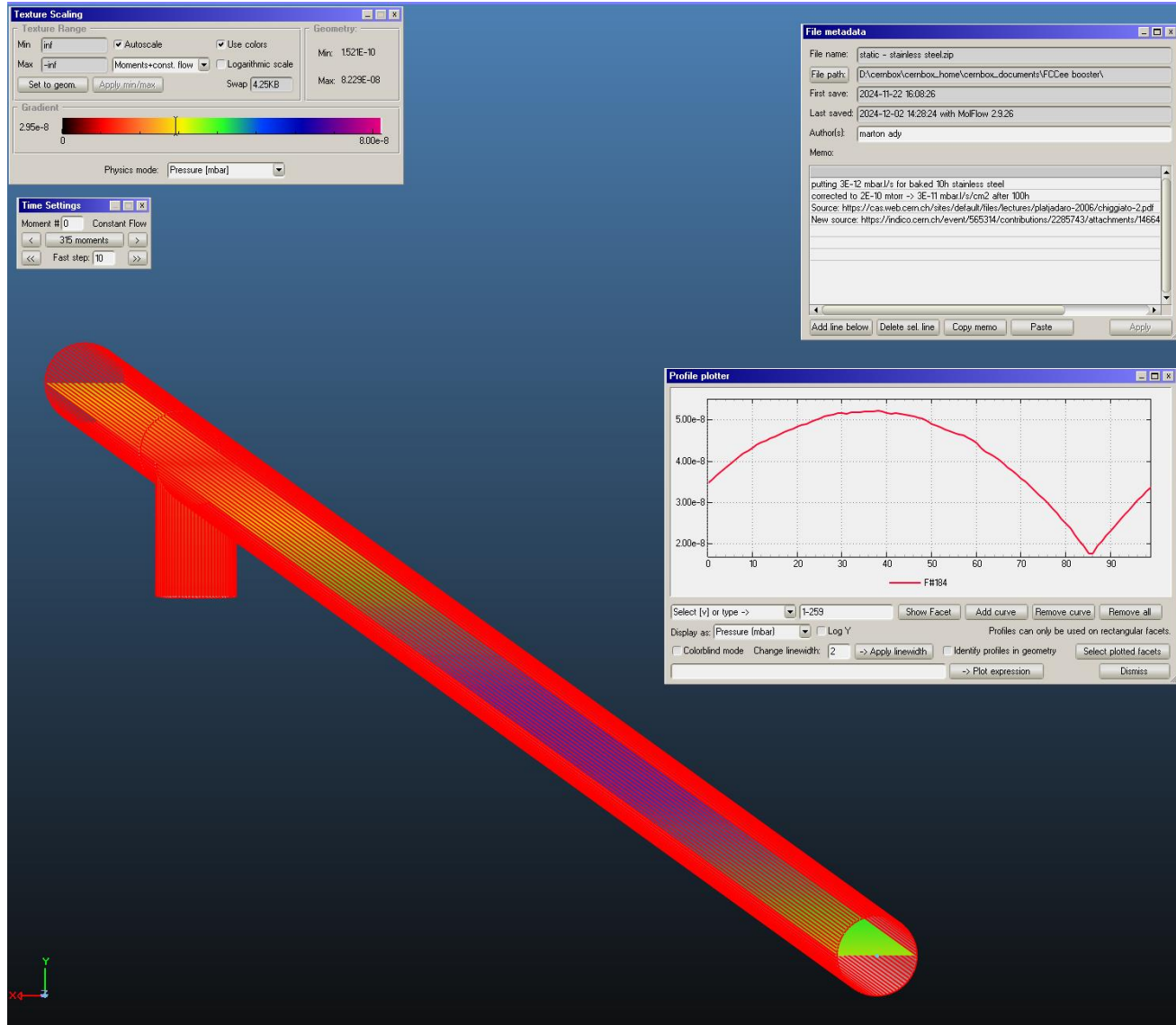
After thorough surface cleaning, water vapour dominates the outgassing process of metals in vacuum. For metal alloys, the outgassing rate is inversely proportional to the pumping time (t) and the empirical relationship of Eq. 13 is in general applied at CERN for design of vacuum systems.

$$q_{H_2O} \approx \frac{3 \times 10^{-9}}{t[h]} \left[\frac{\text{mbar l}}{\text{s cm}^2} \right] \quad (13)$$

After 100 hours:
3E-11 mbar.l/s/cm²

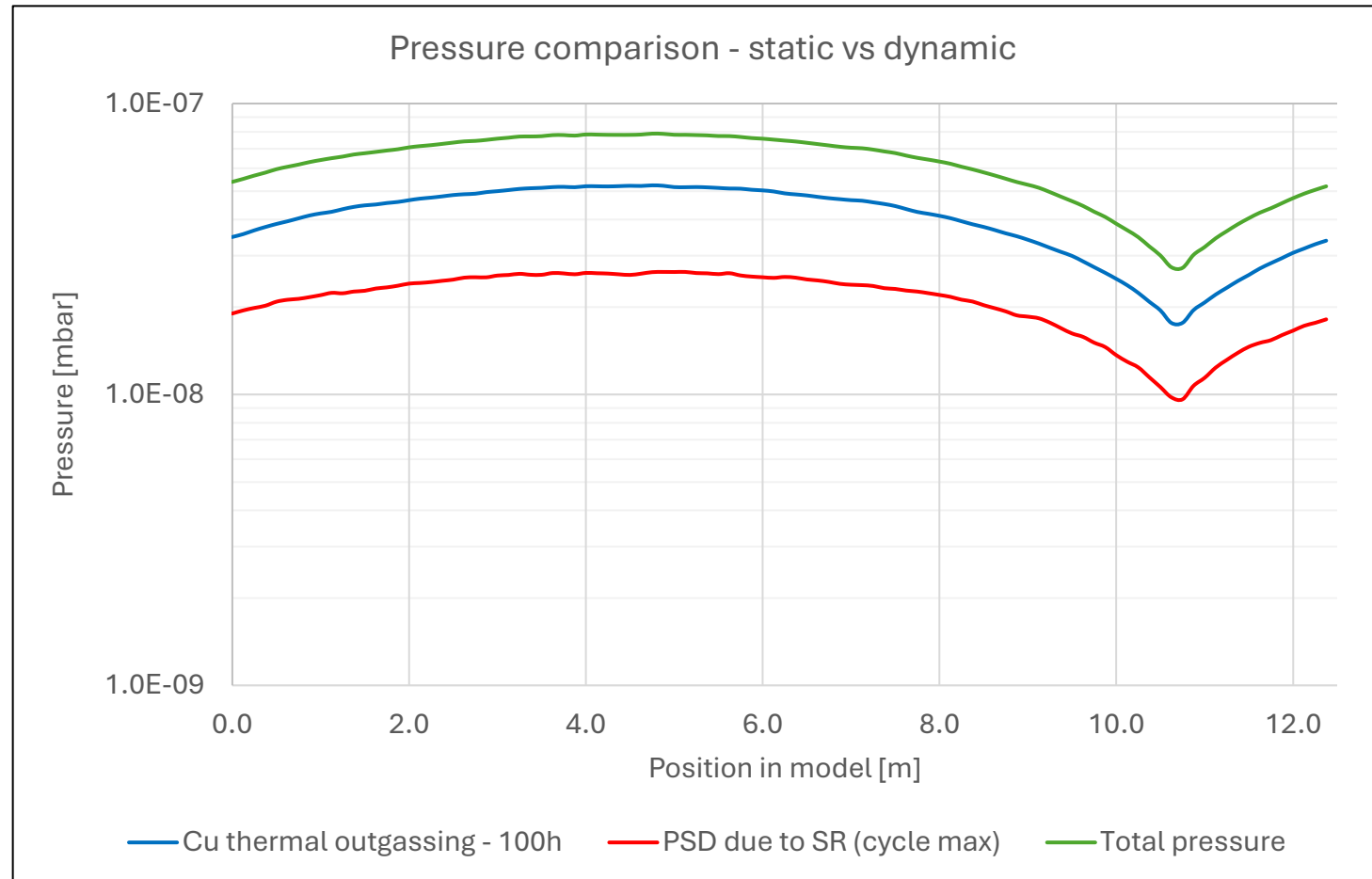
Static vacuum

Step2: static simulation



Static / dynamic pressure comparison

After 100h conditioning:

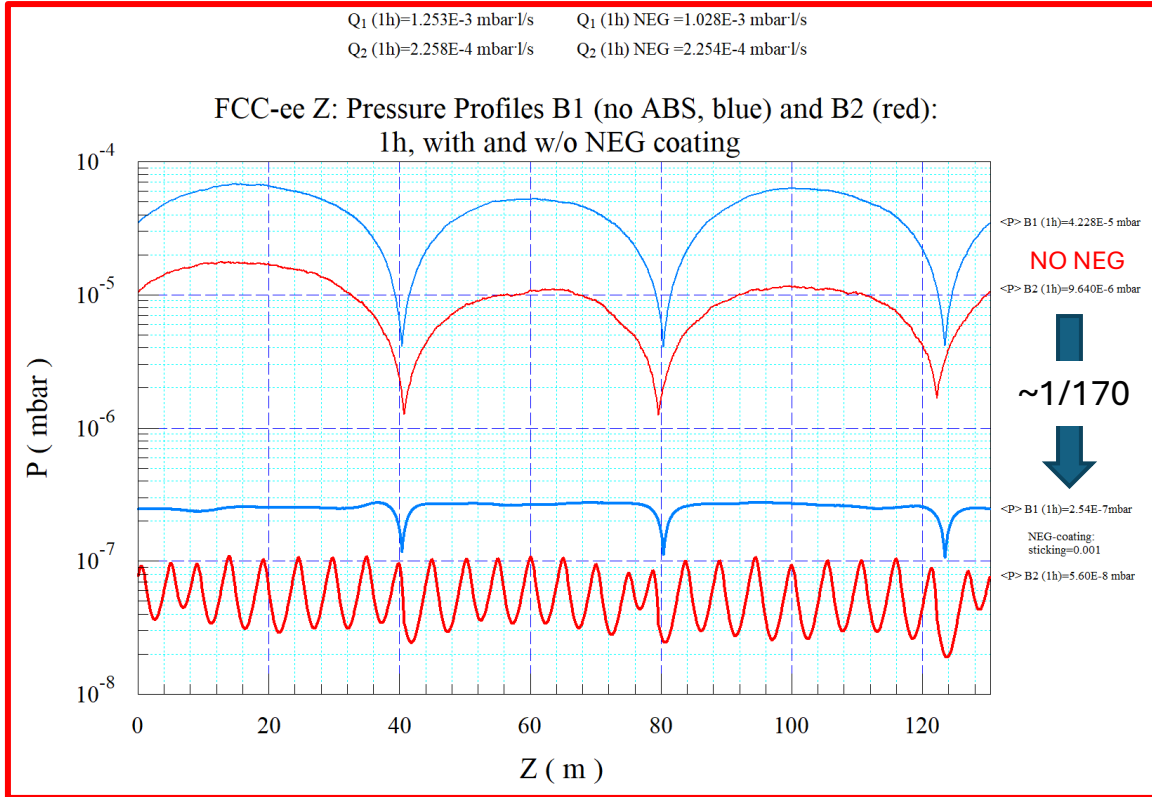


$$Q_{\text{thermal}} \sim t^{-1}$$

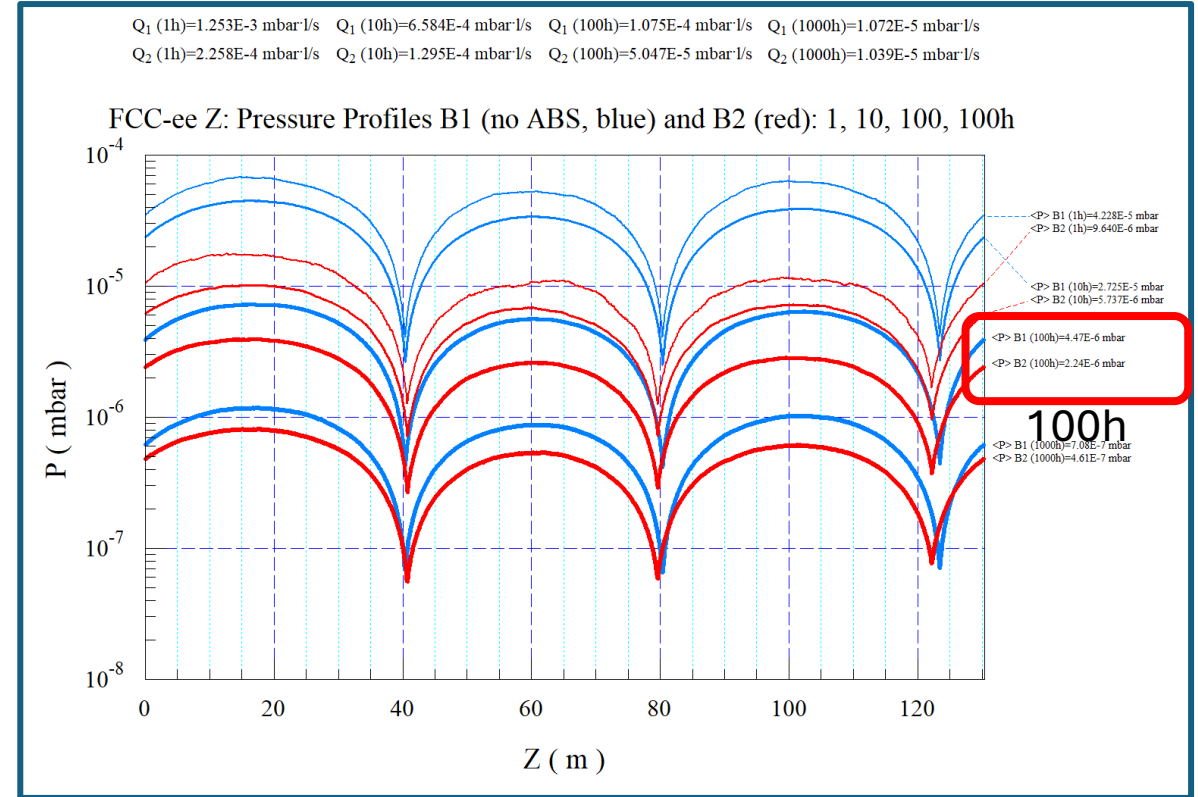
$$Q_{\text{PSD}} \sim t^{-0.6}$$

The case for NEG coating

Cedric Garion / Roberto Kersevan, FCC Week 2024:



- effect of NEG coating (1h case)



- The PSD pressure profiles have been calculated for 4 different beam doses, corresponding to times of 1 h, 10 h, 100 h, 1000 h at nominal current (1270 mA); Simulated gas: CO
- case with 3x 100 (l/s) lumped pumps/beam, and no NEG-coating

Conclusion (booster vacuum)

- The average pressure after around 100h (0.8Ah) of conditioning is around $3E-8$ mbar
- This is exactly the max. pressure by the latest beam-gas calculations*
- It would be preferable to have an in-situ bakeout system installed, and consequently NEG-coating of the vacuum chambers, as this would reduce the number of external pumps and their cabling by a factor of about 5
- Additionally, the NEG-coated solution would guarantee very fast reconditioning of any vacuum sector needing venting during operation.