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CIRCULAR  
COLLIDER

# Overview of and Challenges for the FCC-ee Fast Pulsed Beam Transfer Systems

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# Outline

- ❑ Outcome from feasibility study and kicker design outline
  
- ❑ Challenges and need for R&D/prototyping
  - Stripline kicker + Inductive adder
  - Lumped inductance kicker + generator
  - Other considerations
  
- ❑ Conclusions

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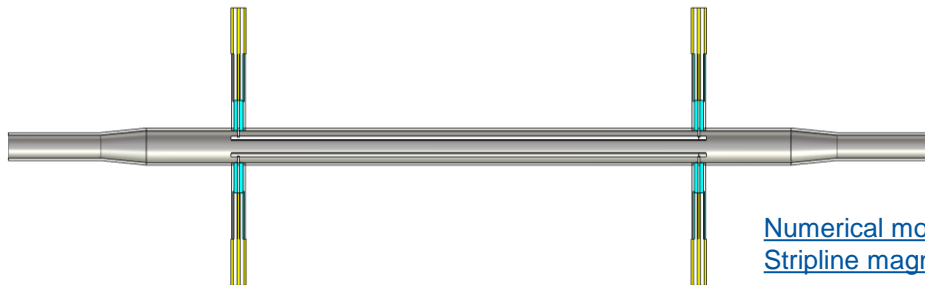
# Feasibility study

- Kicker systems are designed based on the following **key considerations**:
  - Optics design
  - Cost, power consumption & environmental impact
  - Integration
  - Ionizing dose levels
  - Machine protection impact
  - Operational needs
  - Collective effects
- **Multiple system specification changes** have required a reconsideration of the design choices or design reiterations
- **Some parameters remain undefined** or to be confirmed:
  - Beam stay clear region
  - Rise and fall time definition
  - Flat top quality
- **No major showstoppers**, but several challenges have been identified

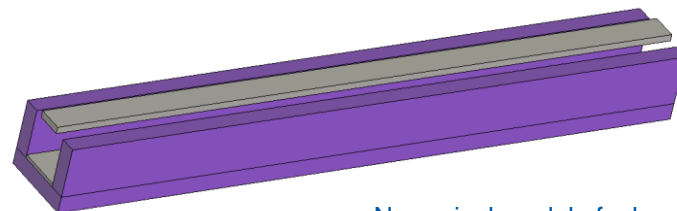
Operation

# Kicker systems outline

	Damping ring	Booster injection	Booster extraction	Booster Dump	Collider injection	Collider dump
<b>Magnet topology</b>	Stripline	Stripline	Lumped inductance	Lumped inductance	Lumped inductance	Lumped inductance
<b>Generator topology</b>	Inductive adder	Inductive adder	Marx generator	LBDS-like generator	Marx generator	LBDS-like generator
<b>Element under vacuum</b>	Yes	Yes	No	No	No	No
<b>Elements / Systems</b>	2/4	1/2	14/2	9/2	6/2	9/2
<b>Novel technology</b>	Yes	Yes	Yes	No	Yes	No
<b>R&amp;D required/ Prototyping required/ Conventional technology</b>	R&D - prototype required	R&D - prototype required	R&D - prototype Required	Prototype required	R&D - prototype required	Prototype required



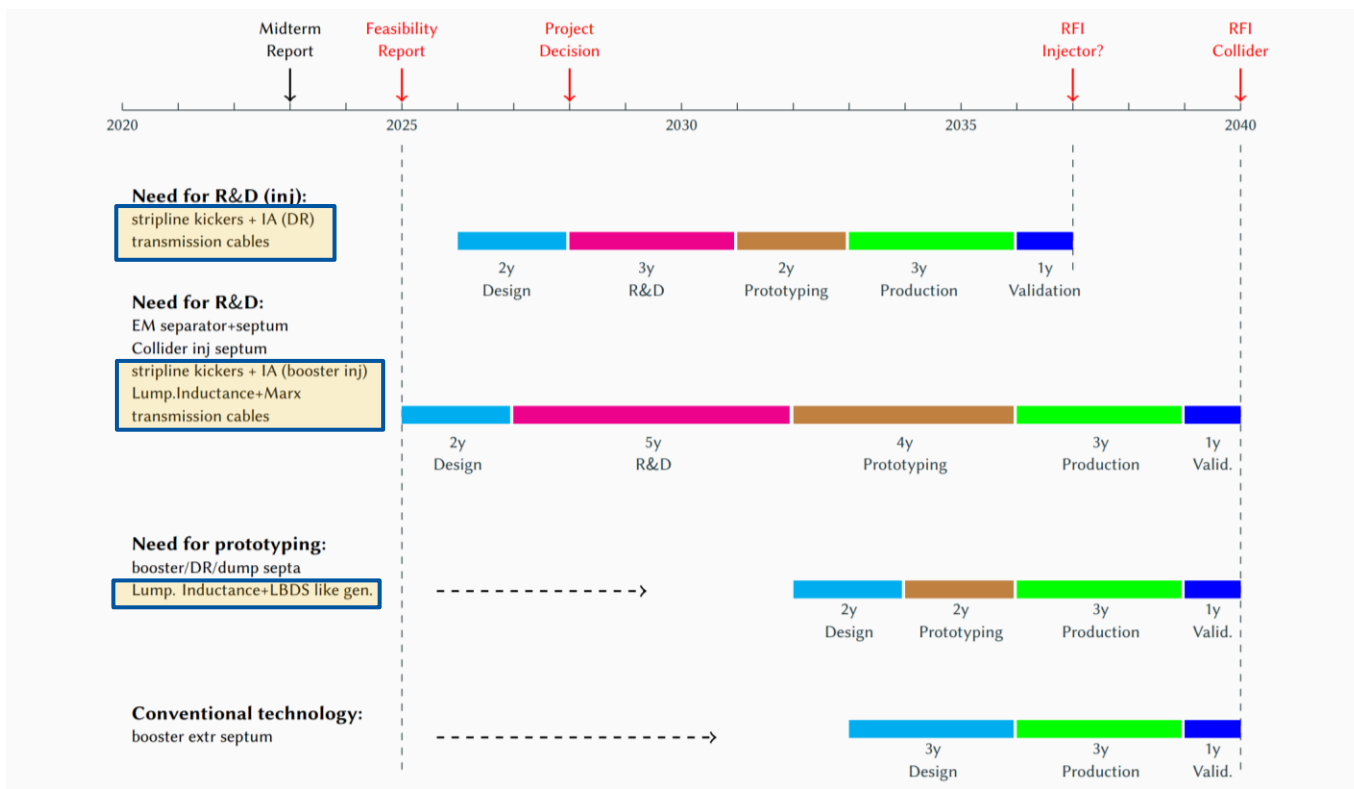
Numerical model of a Stripline magnet



Numerical model of a lumped inductance magnet

# R&D and prototyping timeline

- R&D and prototyping activities have been planned and a timeline has been established to ensure a timely systems readiness



# Kicker systems design choice criteria

- ❑ Magnets and generator topologies have been designed to be cost-efficient, simplify their maintenance and improve machine protection aspects. Priorities are:
  - Standardization of equipment
  - Limited generator voltage solutions
  - Avoidance of oil-filled generators or SF6 cables
  - Limited power dissipation and cooling requirements
  
- ❑ Looking back:
  - Profited of LEP experience and considered similar kicker solutions
  
- ❑ Looking ahead:
  - Considered **benefits and long-term availability of novel technologies**
  - i.e. solid state switches favoured over thyratrons; modular solutions preferred due to easier maintenance

# Outline

❑ Outcome from feasibility study and kicker design outline

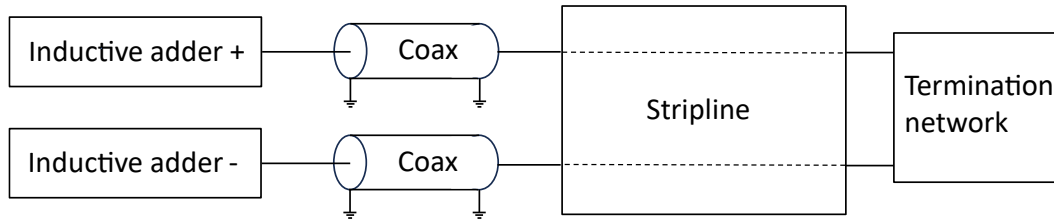
❑ Challenges and need for R&D/prototyping

- Stripline kicker + Inductive adder
- Lumped inductance kicker + generator
- Other considerations

❑ Conclusion

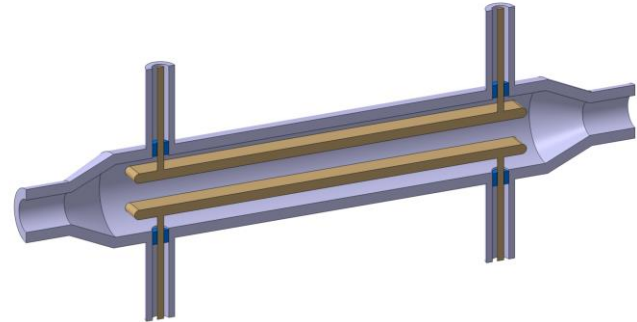
# Stripline + Inductive Adder

- ❑ **Kicker:** Stripline to satisfy fast rise and fall time requirements
- ❑ **Generator:** Inductive adder can provide the short flat top and the required homogeneity
- ❑ The coaxial cable length is based on integration constraints, but **≤30m** needed to achieve rise time and field homogeneity



	Damping ring	Booster injection
<b>Requirements</b>		
Energy [GeV]	2.86	20
Kick angle per unit [mrad]	1.5	0.09
Rise / fall time [ns]	82	25
Flat top length [ns]	80	80
Flat top quality [%]	±0.5	±0.7
Repetition rate [Hz]	100	100
Available length [m]	1.5	5.5
<b>Design parameters</b>		
N. Of Magnets/ System(s)	2 / 4	1 / 2
Impedance [ $\Omega$ ]	50	50
Current [A]	640	260
Voltage [kV]	±32	±13.4
Plate separation [mm]	30	30
Integrated E-field [MV]	3	0.9
Integrated B-field [mT.m]	7.1	3
Effective length [m]	1	1
Physical length [m]	1.5	1.5

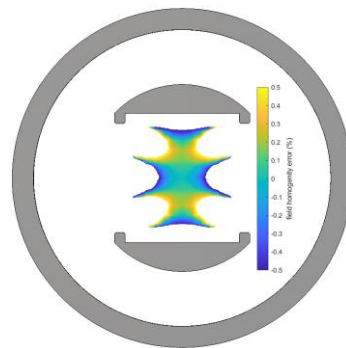
# Stripline kicker



- Relatively simple and compact kicker design

- A preliminary design has been developed, with main challenges being identified:

- **Field homogeneity**
  - Optimized electrodes shape design
- **HV issues**
  - HV limited to  $< 50\text{kV}$
  - SR impact?
- **Operational experience**
  - Magnet topology already prototyped for CLIC, but not currently operated
  - Learn from other electrons laboratory' experience
- **Impedance matching**



# Stripline kicker – Impedance matching

- ❑ Stripline kickers work in two operating modes, with two different characteristic impedances
  - **Odd mode**
    - Seen by the bipolar pulse from the generators when kicker is on
    - Reflections affect the pulse quality
  - **Even mode**
    - Seen by the beam when kicker is off
    - Reflections affect the beam coupling impedance
  
- ❑ An optimization process is required to achieve the field tolerances and limit the beam impedance
  - One impedance is matched by the terminations at the expense of the other
  - Beam impedance limits not yet specified
  
- ❑ A more complex matching network might be needed if a good compromise can't be found:
  - Need to design a termination element between the electrodes
    - in-vacuum: complex design due to concerns about power losses and vacuum compatibility
    - outside-vacuum: would be prone to mismatches at the feedthroughs
  - **R&D and prototyping is needed!**

# Inductive adder

- ❑ Compact and modular design and only solid-state switches used
- ❑ No operational experience
  - Generator topology already prototyped but not yet implemented at CERN
- ❑ A lot of know-how has been acquired from previous prototyping
- ❑ The unprecedented specifications (<25ns rise time and 30m connecting cable length) **require dedicated R&D and prototyping**



## Requirements

	Booster injection	Damping ring	CLIC PDR-DR
Energy [GeV]	20	2.86	2.86
Kick angle per unit [mrad]	0.09	1.5	2-1.5
Rise / fall time [ns]	25	82	700-1000
Flat top length [ns]	80	80	160
Flat top quality [%]	±0.5	±0.5	±0.01
Repetition rate [Hz]	200	100	50

# Lumped inductance kicker – Generator

- ❑ **Kicker:** a ferrite-loaded lumped-inductance magnet can still comply with the most recent and more stringent fast rise and fall time requirements
- ❑ **Generator:**
  - Marx generator for booster extraction and collider injection
  - LBDS-type generator for dump systems, due to more relaxed flat-top homogeneity requirements
- ❑ The length of the cable connecting the generator to the beamline elements is presently **hundreds of meters:**
  - Resulting from the current integration scheme
  - Impact on kicker pulse quality

## Requirements

## Design Paramets

	Booster extraction	Collider injection	Booster dump	Collider dump		Booster extraction	Collider injection	Booster dump	Collider dump
Energy [GeV]	45 – 182.5	45 – 182.5	45 – 182.5	45 – 182.5	N. Of Magnets/ System(s)	14 / 2	8 / 4	9 / 2	9 / 2
Kick angle per unit [mrad]	0.014	0.013	0.033	0.033	Impedance [ $\Omega$ ]	10	10	10	10
Rise / fall time [ns]	600	600	600	600	Current [kA]	0.7	0.7	1.7	1.7
Flat top length [us]	304	304	304	304	Voltage [kV]	7	7	17	17
Flat top quality [%]	$\pm 0.6$	$\pm 1.5$	$\pm 20$	$\pm 20$	Integrated B-field [mT.m]	3	8.12	21	21
Repetition rate [Hz]	0.3	0.3	1	0.1	Element aperture [mm]	70	70	70	70
Beam aperture [mm]	60	60	60	60	Effective length [m]	0.7	0.7	0.7	0.7
Available length [m]	TBD	TBD	TBD	TBD					

# Lumped inductance kicker

- ❑ Simple and robust magnet, which can be operated out-of-vacuum
  - Easier maintenance
  - Reduced machine protection issues
  
- ❑ Design re-iterations were needed as well as an increased number of magnets to adapt to the new 600ns abort gap requirement
  - Impact on cost and integration
  
- ❑ Beam impedance or Electron Cloud instabilities can be addressed employing surface coating:
  - Dedicated simulations needed to assess coating impact, considering the faster rise time requirements
  - Need to clarify beam impedance requirements

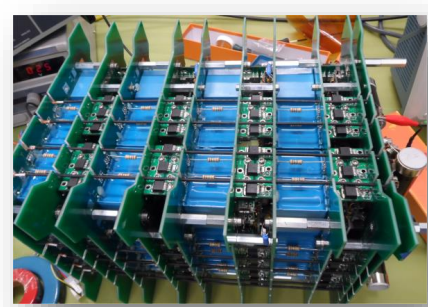
# Generator for LI kicker

## □ Marx generator (Booster extraction, Collider injection)

- Compact and modular design using only solid-state switches
- No operational experience but know-how acquired from previous prototyping
- Unprecedented very challenging long flat top, combined with long cable length  
→ Requires tests on real equipment, to eventually develop compensation solutions
- **Need of R&D and prototyping of a LI magnet driven by a Marx generator!**

## □ LBDS like generator (Booster and Collider dump)

- Driven by a main capacitor discharge stage sustained by a droop compensation stage
- Prototyping is necessary given the unprecedented requirements



# Other considerations

❑ Other studies, supported by R&D are foreseen on:

- F-Gas free insulation solutions
- Radiation impact on components
- Control development for highly reliable systems
- Automatized maintenance and repair
- Interlock systems and/or absorbers for machine protection

❑ Detailed integration studies needed

FCC-ee Integration Requirements for Injection-Extraction Equipment, D. Standen

- Review space requirements: accounting for magnets, generators, control systems, and any additional equipment facilitating maintenance, including spares  
→ Cold spares vs Warm spares?
- Establish final length for cables connecting beamline elements to generators

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# Conclusions

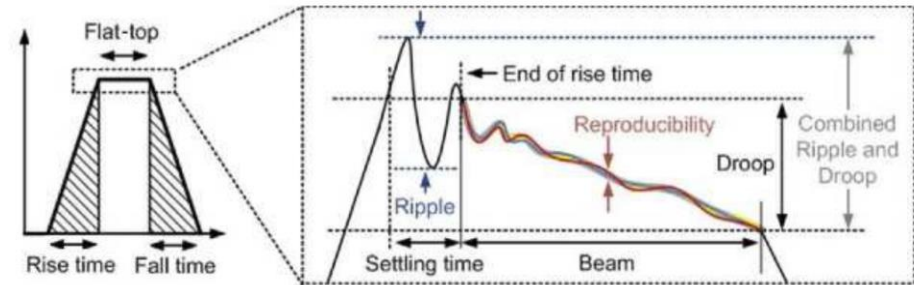
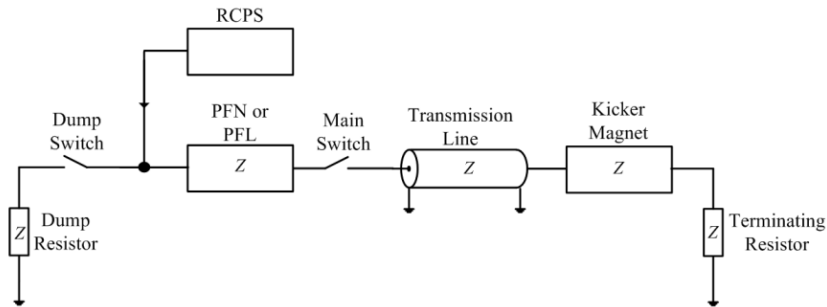
- ❑ Kicker systems have been designed accounting for cost, availability, reliability, and address integration, operational and radiation constraints
- ❑ Design choices have been detailed in the FSR
- ❑ The main design challenges have been identified and mitigating solutions already considered
- ❑ Given the unprecedented specifications, R&D and prototyping are planned to develop new technologies and optimize existing ones to achieve target parameters

Thank you for your attention!

# Spare slides

# Kicker system design

- A kicker magnet is designed to provide a required field magnitude, duration, rise and fall time and homogeneity
- The pulse generator provides a certain current and voltage output to match the requirements for the needed pulse
- Critical parameters are:
  - current and voltage values
  - system impedance
  - pulse rise time and fall time, droop, flat-top stability, pulse-to-pulse stability
  - repetition rate

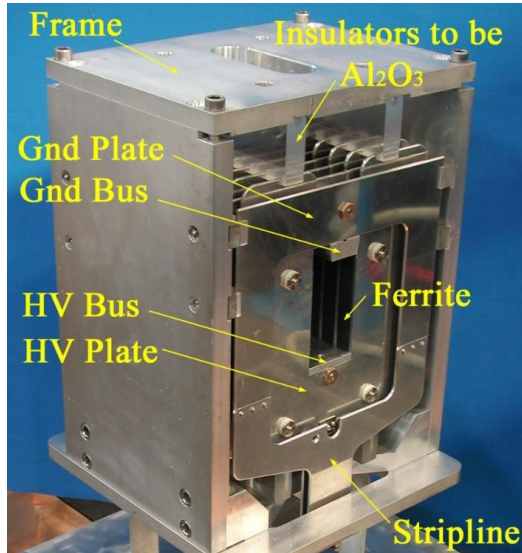


# Magnet topologies

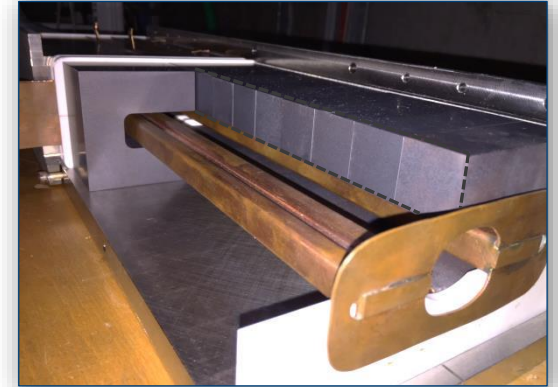
	PRO	CONS
<b>Stripline</b>	<ul style="list-style-type: none"> <li>▪ Compact design</li> <li>▪ Very fast rise time (few ns)</li> <li>▪ Low beam coupling impedance</li> </ul>	<ul style="list-style-type: none"> <li>▪ Weaker deflection</li> <li>▪ Impedance matching important</li> <li>▪ Challenging flat-top stability</li> <li>▪ More power consumption</li> </ul>
<b>Transmission line</b>	<ul style="list-style-type: none"> <li>▪ Fast rise time <math>\ll 1\mu\text{s}</math></li> <li>▪ Strong deflecting field</li> </ul>	<ul style="list-style-type: none"> <li>▪ Voltages up to 80 kV</li> <li>▪ Complex to manufacture and costly</li> <li>▪ Impedance matching important</li> <li>▪ High beam coupling impedance</li> </ul>
<b>Lumped inductance</b>	<ul style="list-style-type: none"> <li>▪ Strong deflecting field</li> <li>▪ Simple and robust magnet design</li> <li>▪ Can be out of vacuum</li> </ul>	<ul style="list-style-type: none"> <li>▪ Needs minimizing interconnection inductance</li> <li>▪ Suitable for rise time <math>\geq 1\mu\text{s}</math></li> <li>▪ High beam coupling impedance</li> </ul>

# Magnet topologies

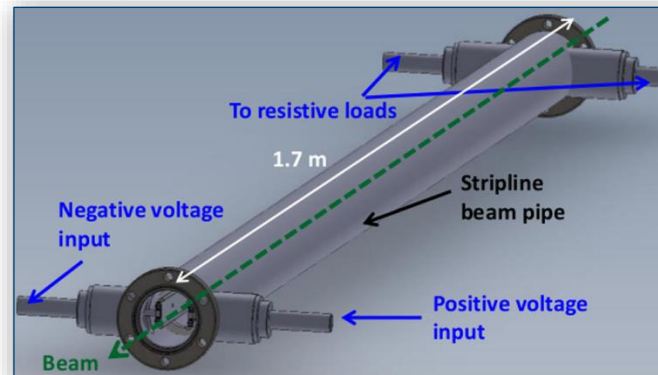
## Transmission line



## Lumped inductance



## Stripline



# Generator topologies

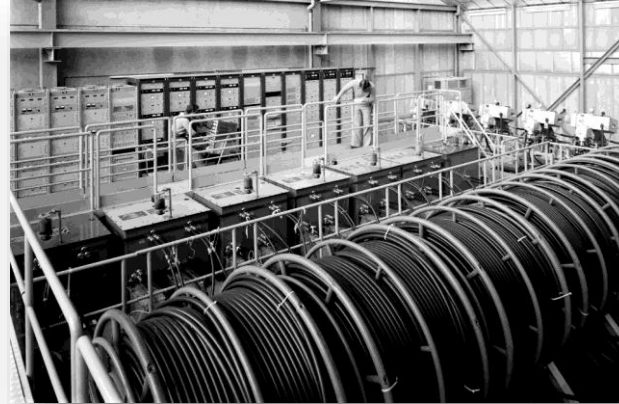
	PRO	CONS
<b>PFN</b>	<ul style="list-style-type: none"> <li>▪ Compact design</li> <li>▪ Low droop and long pulses <math>&gt; 3\mu\text{s}</math></li> <li>▪ Voltage up to 80 kV</li> </ul>	<ul style="list-style-type: none"> <li>▪ Complex constructions</li> <li>▪ Risetime limited by cells cut-off frequency</li> <li>▪ Pulses are prone to ripples - may require cells adjustment</li> <li>▪ Require high voltage capacitors</li> </ul>
<b>PFL</b>	<ul style="list-style-type: none"> <li>▪ Simple design</li> <li>▪ Short pulses <math>&lt; 3\mu\text{s}</math></li> <li>▪ Ripple-free (flat) pulses</li> </ul>	<ul style="list-style-type: none"> <li>▪ Significant droop in pulses <math>&gt; 3\mu\text{s}</math></li> <li>▪ Above 40 kV SF6 used at CERN</li> <li>▪ Bulky: <math>3\mu\text{s}</math> pulse 300 m of cable</li> </ul>
<b>Marx Generator</b>	<ul style="list-style-type: none"> <li>▪ Long duration pulse capability</li> <li>▪ High repetition-rate</li> <li>▪ Low-voltage components</li> <li>▪ Modular</li> </ul>	<ul style="list-style-type: none"> <li>▪ Sensitive to radiation</li> <li>▪ Complex triggering system</li> </ul>
<b>Inductive adder</b>	<ul style="list-style-type: none"> <li>▪ Short and precise pulses</li> <li>▪ Modular, redundant, scalable</li> <li>▪ Easier triggering circuits</li> </ul>	<ul style="list-style-type: none"> <li>▪ Available pulse duration is affected by magnetic material (<math>&lt; 3\mu\text{s}</math>)</li> <li>▪ Sensitive to radiation</li> </ul>

# Generator topologies

**PFN**



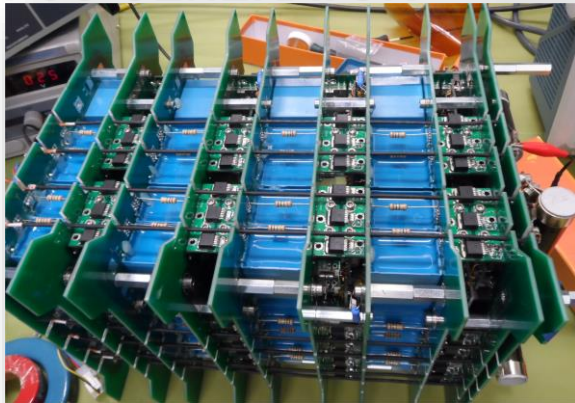
**PFL**



**INDUCTIVE ADDER**

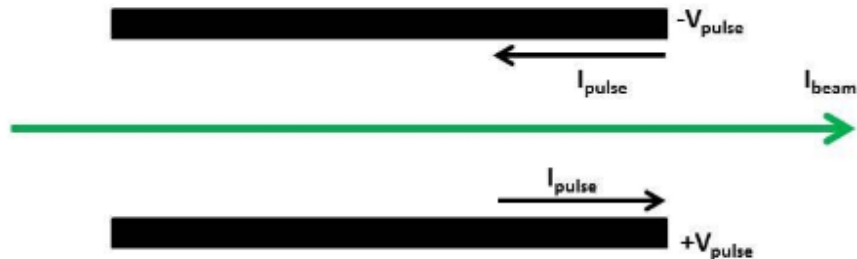


**FCC GENERATOR**



# Cross Section Design

## KICKER ON



## KICKER OFF

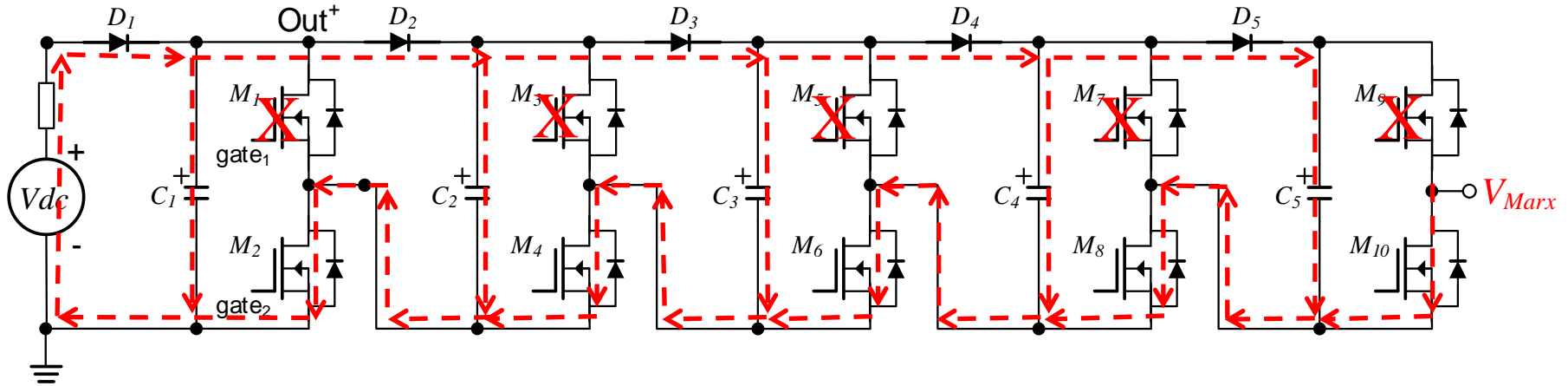


**KICKER ON = ODD MODE**  
**KICKER OFF = EVEN MODE**

- When the electrodes are excited with opposite polarity voltages, the current flow is in opposite directions in each stripline electrode: this is the **odd mode**.
  - an electromagnetic field is created between the electrodes, giving a transverse kick to the beam
- When un-kicked circulating beam passes through the aperture of the striplines, it induces image currents in the electrodes: the direction of current flow is the same in both electrodes – this is the **even mode**.
  - this generates an electromagnetic field, which gives a longitudinal kick to the beam and can produce beam instabilities.

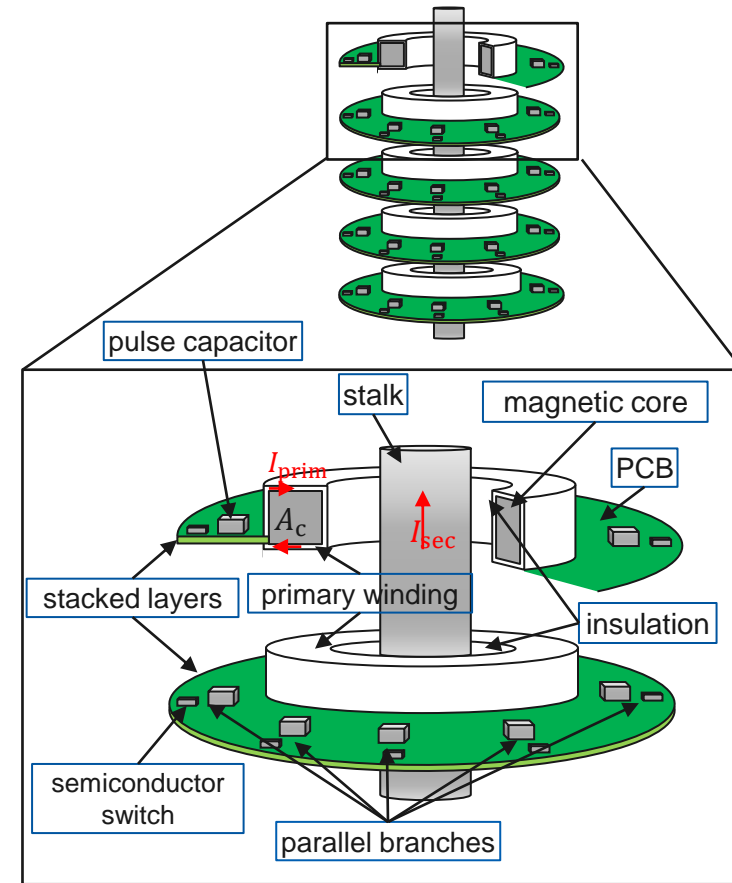
# Marx generator

- In a Marx generator  $n$  capacitors are charged in parallel from a relatively low-voltage DC power supply, and discharged in series into the load
- The output voltage pulse has an amplitude approximately equal to the number of stages ( $n$ ) times the input voltage ( $V_{dc}$ ),  $V_{Marx} = n \cdot V_{dc}$
- 16 kV, 2.6 kA, 75 ns rise and fall prototype developed for FCC-hh



# Inductive adder

- The IA is a solid-state modulator, which can provide relatively short and precise pulses
- An inductive adder consists of multiple parallel layers (also known as stages), each of which has a 1:1 transformer
- The single turn primary totally encloses a magnetic core; hence, the leakage inductance of this geometry is negligible
- The secondary winding of each of these transformers is connected in series: hence a step-up voltage ratio of 1:N is achieved by using N-layers, with adequate voltage isolation



# Thyratrons vs semiconductor switches

Semiconductor switches can be used in fast high current pulsed power accelerator applications to replace thyatrons and PFLs.

## Thyratrons

- + Radiation resistant
- + Generally reliable
- + Robust (fault tolerant)
- + Relatively high voltage
- + Relatively high current
- Long term availability
- Spontaneous turn on
- Can only be turned on

*Versus:*

## Solid-state

- + Cost-effective
- + Easy to use
- + Off-the-shelf
- + Flexible
- + Modular
- + Maintainability
- Relatively low voltage
- Relatively low current

But.... Semiconductors have limited voltage and current rating. Hence, requires **series and parallel connection of power semiconductors** to achieve high pulsed power.

# Machine Protection

- ❑ Machine protection concerns start at booster extraction and Z-mode is the most critical
- ❑ Failure types and probability depend on magnet kind and operational conditions:
  - Iteration needed at design phase to find best tradeoff between magnets performance, reliability, availability and machine protection aspects
- ❑ Potential failures have been estimated:
  - They are typical of high voltage fast pulsed systems (see next slides)
  - Additional challenges are introduced by synchrotron radiation, high stored energy and energy density
- ❑ Mitigations consist in:
  - ❑ Redundancy, monitoring and fast reaction to failures, passive protection, retriggering mechanism etc.
  - ❑ Rad-hard electronics
  - ❑ Segmentation and voltage reduction to reduce risk and consequence of failures
  - ❑ Out of vacuum magnets, minimum beam coupling impedance design, etc.
  - ❑ New concepts like sacrificial absorbers (for ultra-fast failures), chunk extraction etc. have to be considered (in booster extraction/dump, booster-to collider TL, collider injection and extraction)

# Machine Protection – Booster Failures

Failure	Consequence	# affected bunches
Asynchronous extraction	xx bunches swept in the machine aperture	It depends on <b>reaction, re-triggering</b> and <b>rise time</b> (e.g. 44 for 1.1 us and 60 for 1.5 us)
Large ripples of extraction kickers	bunches extracted with oscillations, losses at the septum, septum mask and/or the transfer lines, poor transmission to the collider, large injection oscillations and losses in the collider	It depends on <b>the waveform shape</b> but in principle up to all (1120 for Z mode)
Up to 100XX extraction kickers missing .or. 100YY extraction septa not pulsing at nominal strength (0-100%)	mis-kicked bunches → oscillations in TL, losses (also possible at one single location), poor or no transmission, injection oscillations and losses in the collider	All (1120 for Z mode)

# Machine Protection – Colliders Failures

Failure	Consequence	# affected bunches
Asynchronous extraction	xx bunches swept in the machine aperture	It depends on <b>reaction, re-triggering</b> and <b>rise time</b> (e.g. 44 for 1.1 us and 60 for 1.5 us)
Large ripples of extraction kickers	bunches extracted with oscillations, losses at the septum, septum mask and/or the transfer lines	It depends on the <b>waveform shape</b> but in principle up to all (11200 for Z mode)
Up to 100XX extraction kickers .or. 100YY extraction septa not pulsing at nominal strength (0-100%)	mis-kicked bunches → oscillations in TL, losses (also possible at one single location)	All (11200 for Z mode)
100XX missing injection bumpers .or. pulsing with higher current than nominal	miss-kicked circulating bunches → oscillations (bump amplitude/xx) and losses at collimators, septum and septum mask.	All (11200 for Z mode)
100YY septum not pulsing at nominal strength (0-100%)	injected bunches mis-kicked → injection oscillations and losses in the collider	All (1120 for Z mode)
Sparks in electromagnetic separator	large kicks to the full circulating beam and ultra-fast losses	All (56 for ttbar and 380 for ZH modes)

# FCC Point B Magnet location (midpoint)

