



*This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 951754.*

# FCC WEEK 2025

## Semi-Dry Cavity Cooling of SRF Cavities at Temperatures above 4.5 K

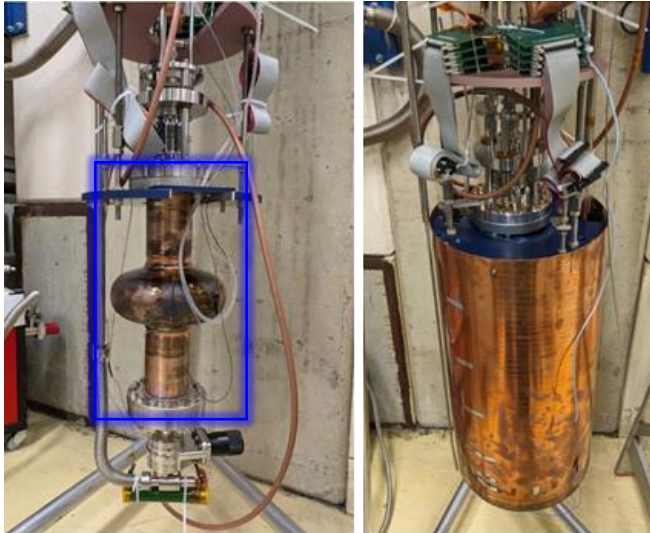
*Torsten Koettig, Maria Chioteli, Guillaume Rosaz, Pierre Maurin, Marco Garlasche,  
Alan Saillet, Vittorio Parma, Walter Venturini*

# Content

- **Concept of “semi-dry” cooling SRF cavities**
- **Experimental setup**
- **Results from the “cryocooler standalone and boosted operation” 1.3 GHz cavity**
- **Integrated cooling features in the cavity surface – cavity wall mock-up**
- **Grooved cavity production**
- **Summary**

# Standard cryomodule vs. dry cavity cooling

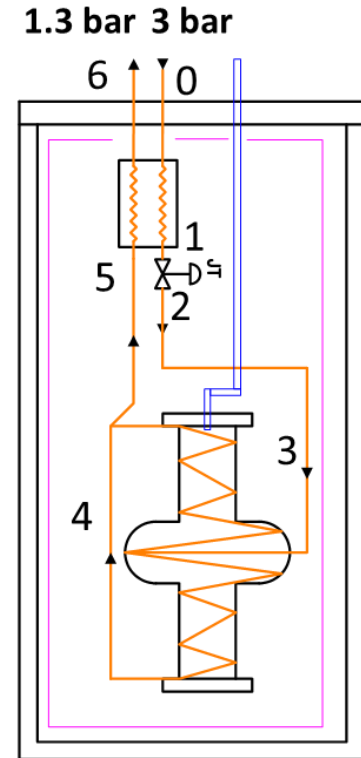
## LHe bath cooling



Use of a thermal shield in He gas for slow  $T_c$  cooldown from 20 K

## Pros vs. Cons.

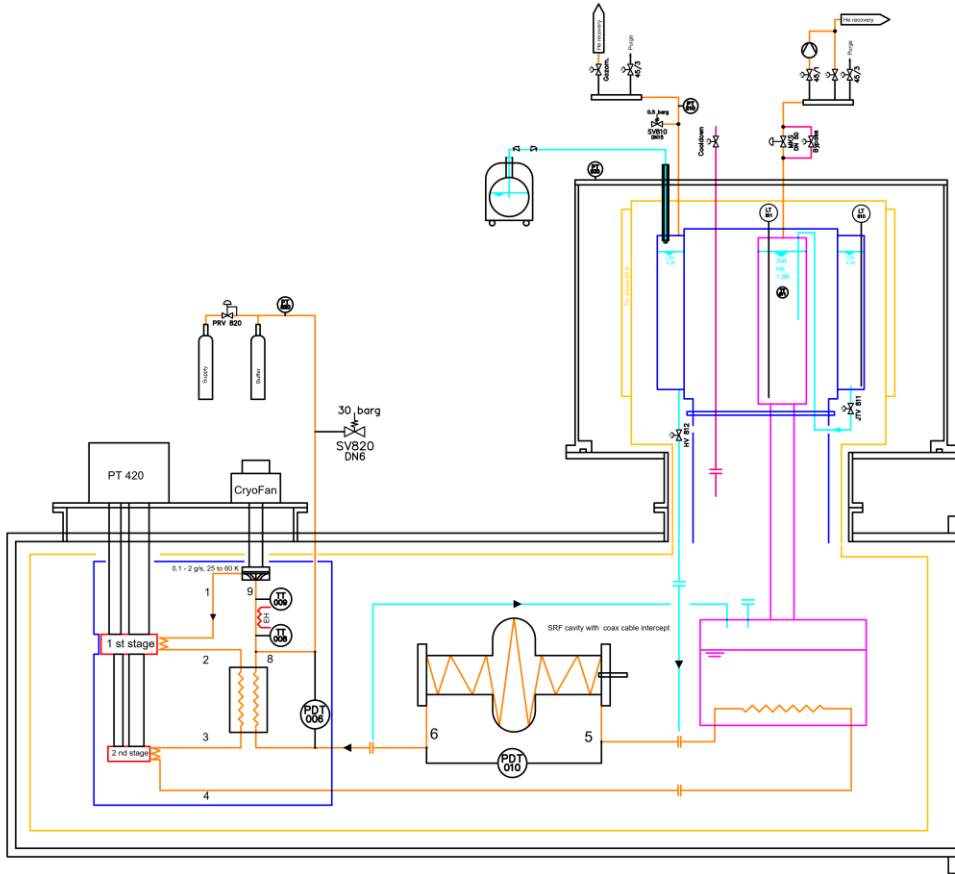
- LHe content (reduced safety hazards)
- Pressure safety of the vessel
- Material transitions
- $T_c$  transition front => trapped flux\*
- Temperature profile
- Cooling performance  
=> free conv. vs. forced flow
- Add. cooling features vs. no He vessel
- Mechanical tuners at cold
- Option for cavity cooling for FCC?



\*coated cavities want small thermal gradients during transition: Seebeck vs. Meissner  
bulk Nb looking for fast cooldown through  $T_c$  expel magnetic flux

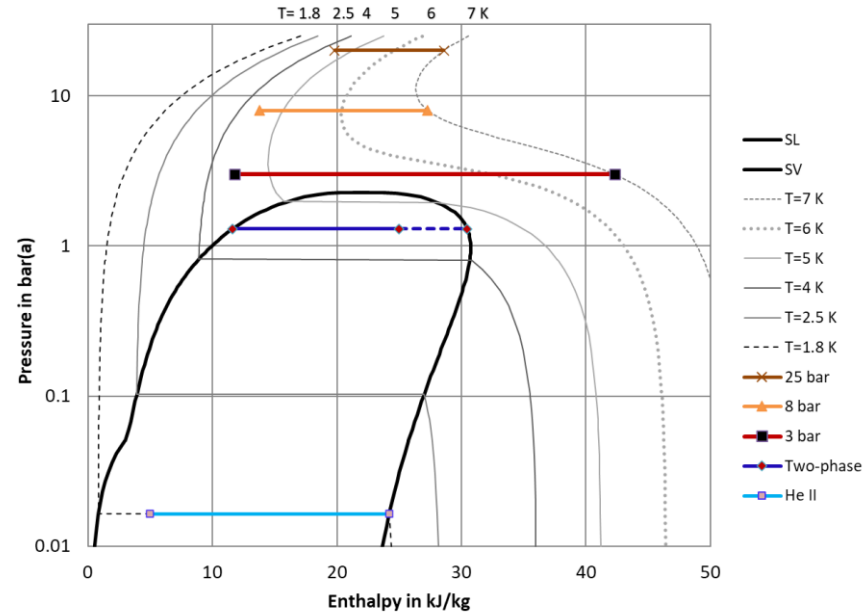


# P&ID with LHe booster HEX



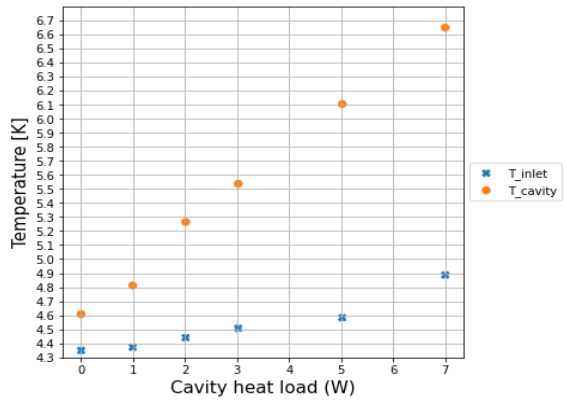
## Possible fluid conditions

- LHe two-phase flow
- Supercritical He @ 3 bara, 4.5 K
- GHe @ 8 bara, 4.5 K
- GHe @ 25 bara, 4.5 K

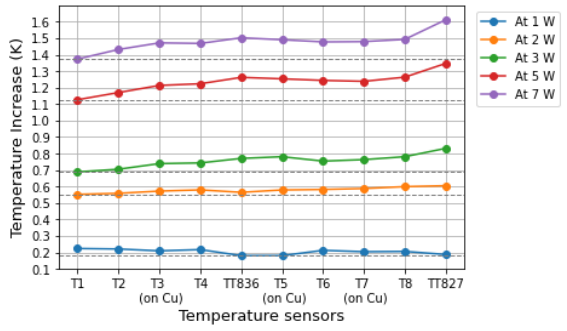


# Inlet & Cavity temperature distribution supercritical He flow condition

### Cavity & inlet temperature at each heat load level for the optimal system performance at 3-4 bar He flow



### Local temperature increase across the entire length of the cavity 3-4 bar He flow



- Temperature gradient < 20 mK up to 2 W
- As the heat load increases, the temperature rise becomes slightly more pronounced, reaching around 220 mK at 7 W

✓ Copper effectively maintains an almost uniform temperature rise over the length of the cavity with added heat load.

**For no introduced heat load – 0 W**

**Inlet Temperature:** 4.35 K ± 20 mK

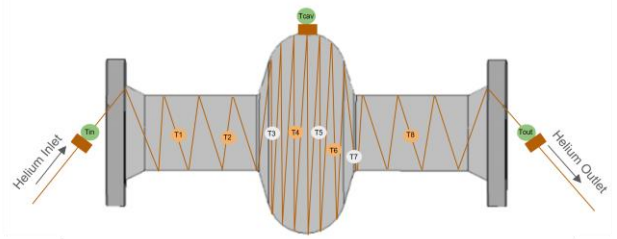
**Cavity Temp range:** 4.60 K ± 20 mK

**At 7 W introduced heat load**

**Inlet Temperature:** 4.90 K ± 20 mK

**Cavity Temp range:** 6.65 K ± 20 mK

Residual heat load of approximately 1 W



- (TVO) **Tin** located on the capillary (inlet)
- (TVO) **Tcav** located on the cavity equator, measuring the average centured temperature
- (TVO) **Tout** located on the capillary (outlet)
- (Allen Bradley) **T1,T2,T4,T6,T8** located on the capillary
- (Allen Bradley) **T3,T5,T7** located on the Cu cavity surface

$$\alpha_{He2tube} / \lambda_{tube} = 1/9$$

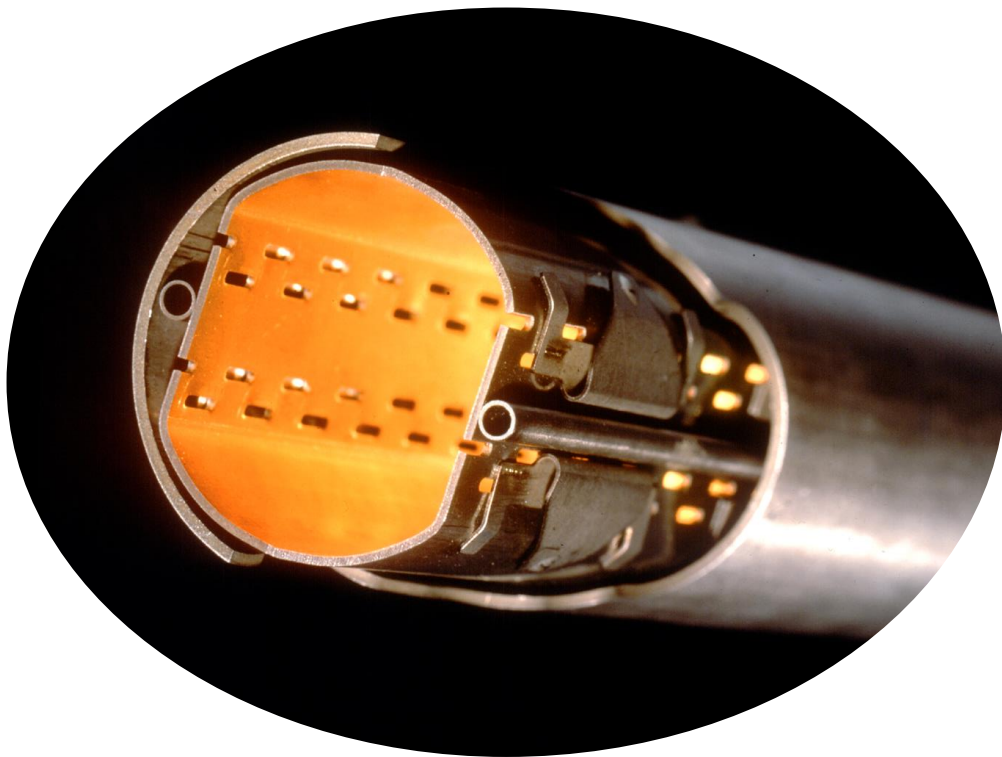
$$\lambda_{tube} / \lambda_{cav} = 1/4$$

## Example from the LEP water cooled cavities



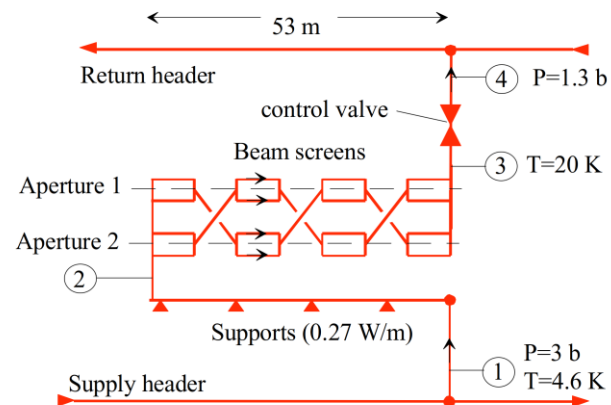
Cu cavity with water cooling circuits

## Example from the LHC operation - Beam Screen cooling



LHC beam screen cooling with two-parallel capillaries of  $d_i=3.7$  mm

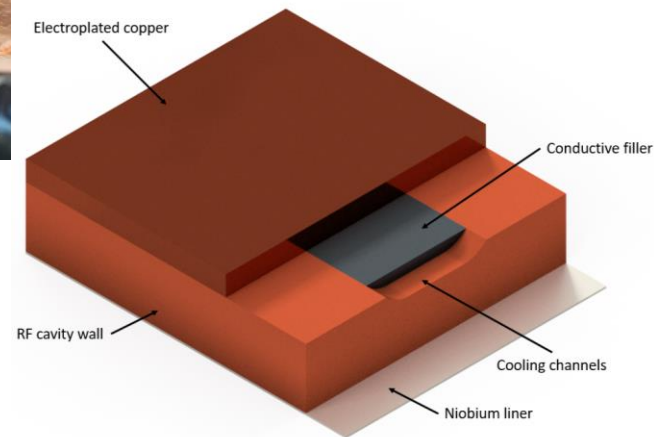
Supercritical He flow at 3 bar a, 4.5 K



# Integration of cooling channels in the Cu cavity wall => grooves

## Procedure:

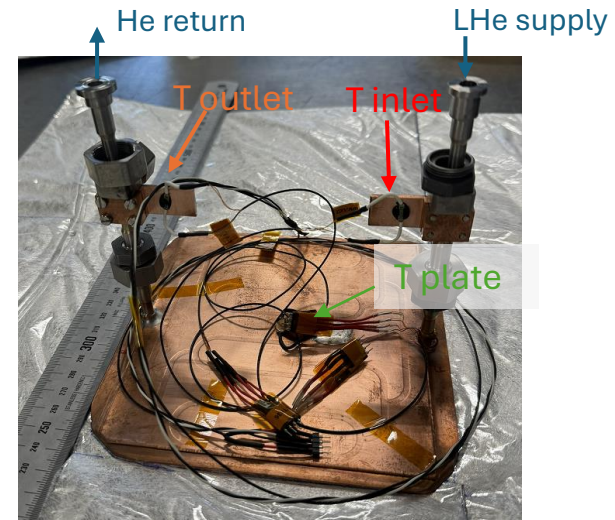
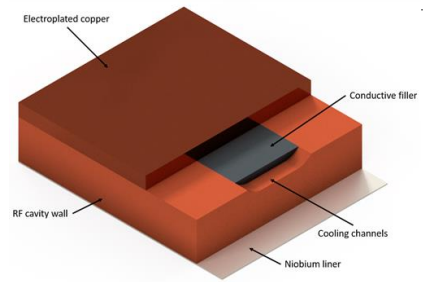
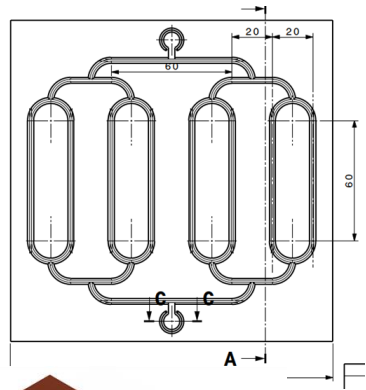
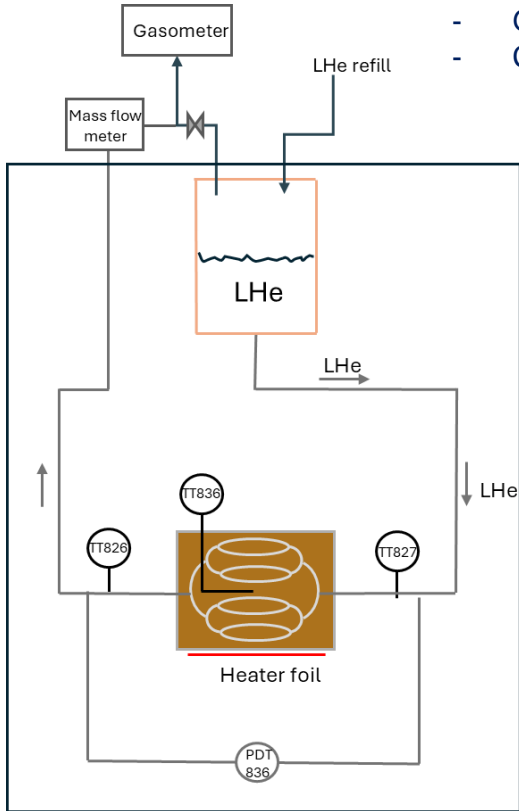
- Groove machining
    - Filling with conductive wax
    - 20-50% graphite charged
  - Hard wax (jewellers wax)
  - Removal of excess material
  - Cleaning
  - Electroplating with copper
  - Machining
  - Connections
- 
- Testing with LHe two-phase and supercritical flow



Courtesy: CERN EN-MME

# Dry Cavity Cooling: Mock-up plate results in two-phase flow

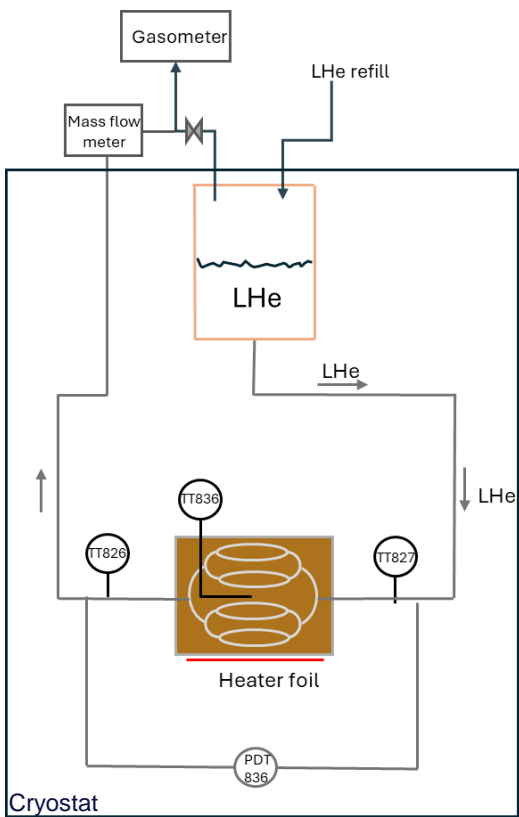
- Grooves are machined into the Cu substrate (cavity wall) and electroplated
- Cryo performance with low pressure LHe two-phase flow @ 4.3 K in the Cryolab



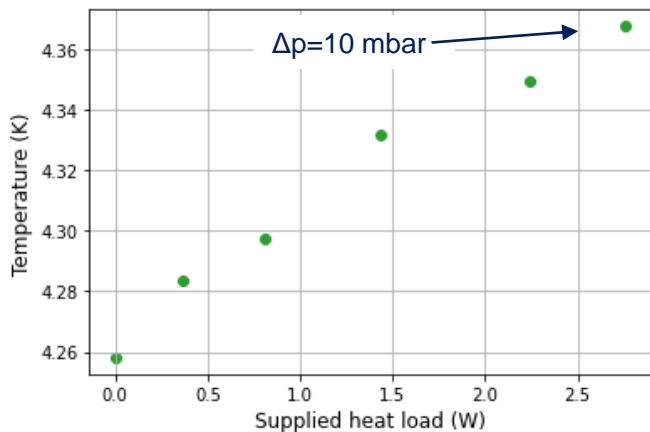
### Two ways for controlling the mass flow rate:

1. Supplying liquid helium from reservoir, flow driven by hydrostatic pressure differences: → Helium supply:  $p=1$  bar / 4.2 K
2. Pressurising the supply reaching a higher mass flow rate → Helium supply:  $p=1.1$  bar / 4.3 K

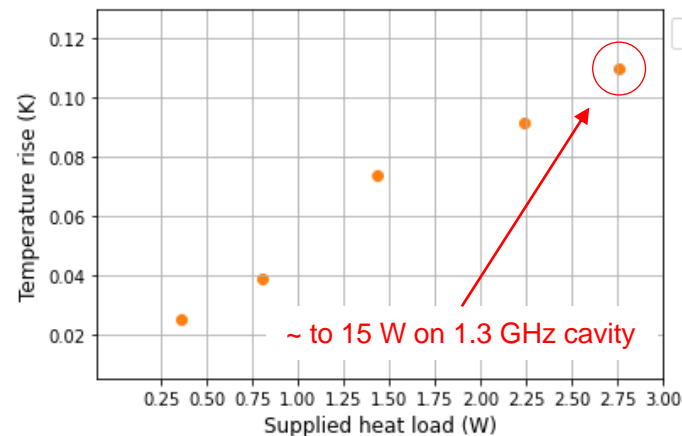
- Grooves are machined into the Cu substate (cavity wall) and electroplated
- Cryo performance is measured with:
  - **Low pressure LHe two-phase flow @ 4.25 K in the CERN Cryolab**
  - High pressure supercritical He flow @ 3-4 bar and 8-9 bar



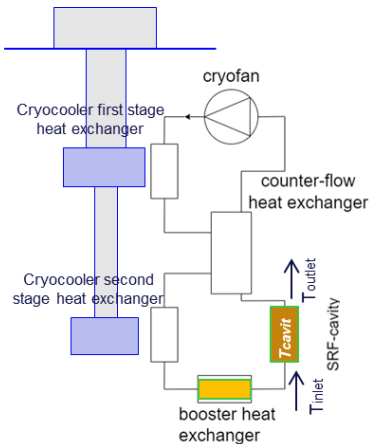
Temperatures at each heat load level



Temperature rise at each heat load level

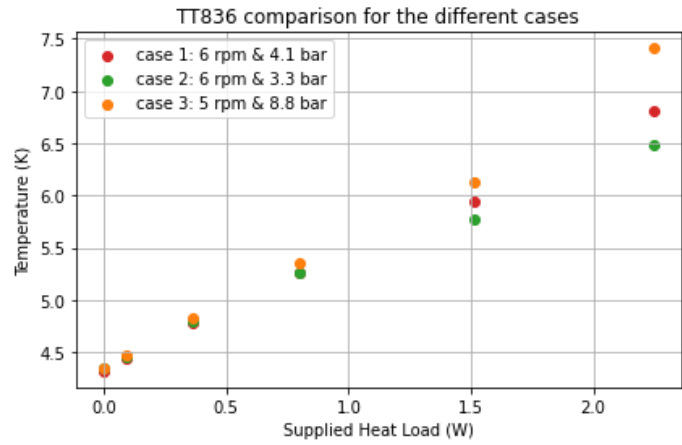


Accuracy estimation: Pressure drop:  $\pm 0.35$  mbar, Temperature:  $\pm 0.045$  K, Temperature rise:  $\pm 0.01$  K

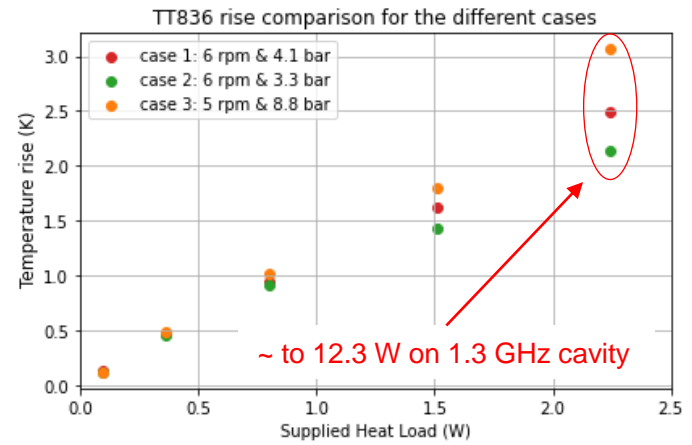


- Grooves are machined into the Cu substate (cavity wall) and electroplated
- Cryo performance is measured with:
  - Low pressure LHe two-phase flow @ 4.25 K in the CERN Cryolab
  - **High pressure supercritical He flow @ 3-4 bar and 9 bar**

*TT836 / Plate Temperature comparison for the different cases*

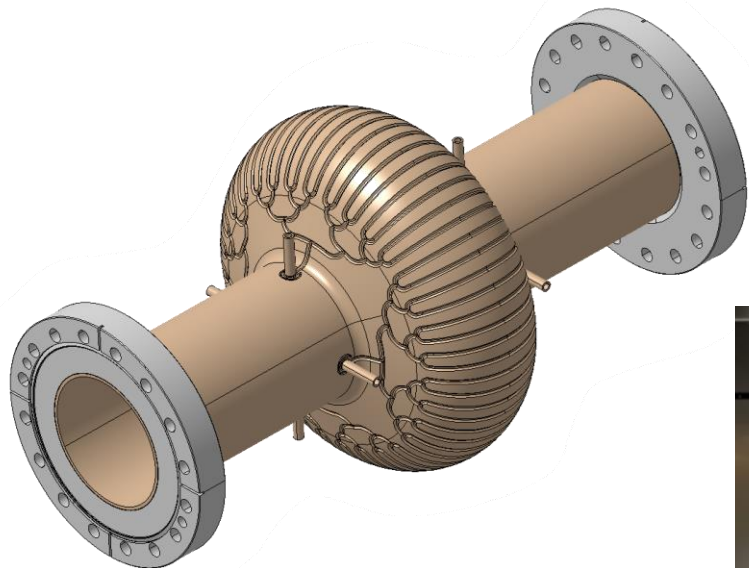


*TT836 / Plate Temperature rise from 0 to 2.25 W comparison for the different cases*

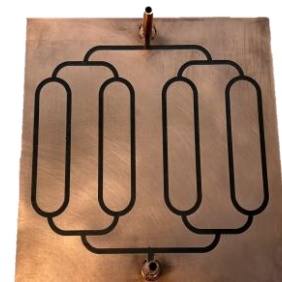
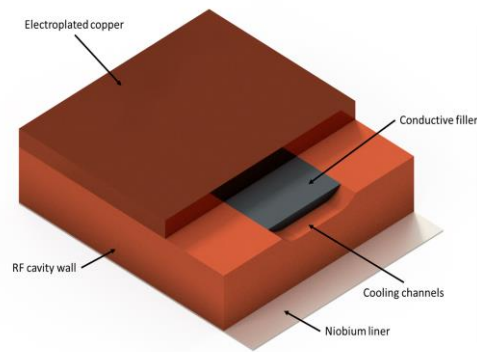


Accuracy estimation: Pressure drop:  $\pm 0.35$  mbar, Temperature:  $\pm 0.045$  K, Temperature rise:  $\pm 0.01$  K

## Application to an R&D 1.3 GHz cavity



Design of integrated cooling channels in a 1.3 GHz cavity wall.



Design and fabricated Cu mock-up plate, wax filled grooves.



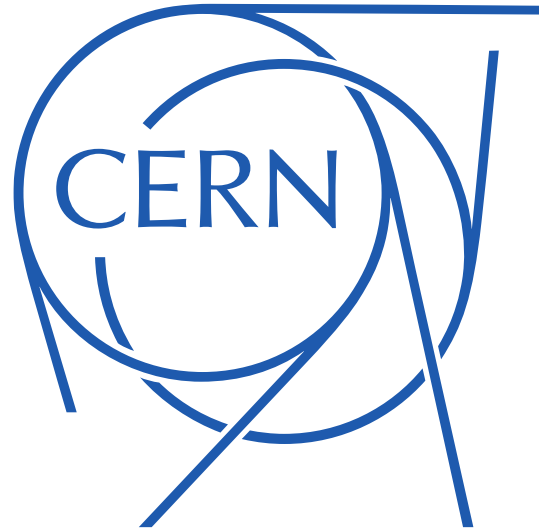
First manufacturing steps in the CERN main workshop.

# Conclusion and Status May 2025

- Combination of three very promising technologies:
  - Semi-dry cavity cooling
  - A15 coatings like Nb<sub>3</sub>Sn on Cu
  - Electroforming or integrated channel manufacturing
- Huge impact on possible CM designs, drastically reduced He content (30-50x)
- Cavity cooling => feasibility of remote cooling systems, reaching cooling requirements with supercritical flow.
  - ✓ **6.5 K** cavity temperature @ **1 W** + residuals / Cryocooler standalone operation
  - ✓ **6.6 K** cavity temperature @ **7 W** + residuals / Booster heat exchanger integrated operation
- Groove mock-up:
  - ✓ tested in two-phase flow, leak tight at cold with 1.3 bar, small temperature rise, pressure drop OK
  - ✓ tested in supercritical flow, leak tight at cold with up to 10 bar, smallest  $\Delta T=2.1$  K for 3.3 bar (QRL like)

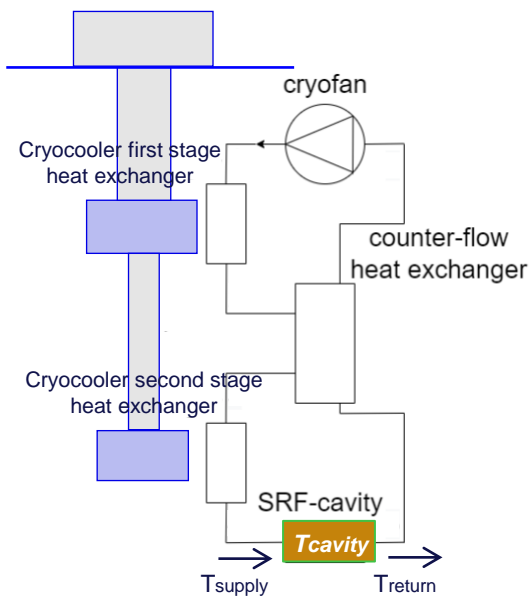
## Next steps:

- Proceed with a 1<sup>st</sup> full-scale 1.3 GHz machined cavity for thermal test
- Produce a coated 1.3 GHz cavity for full RF and thermal tests

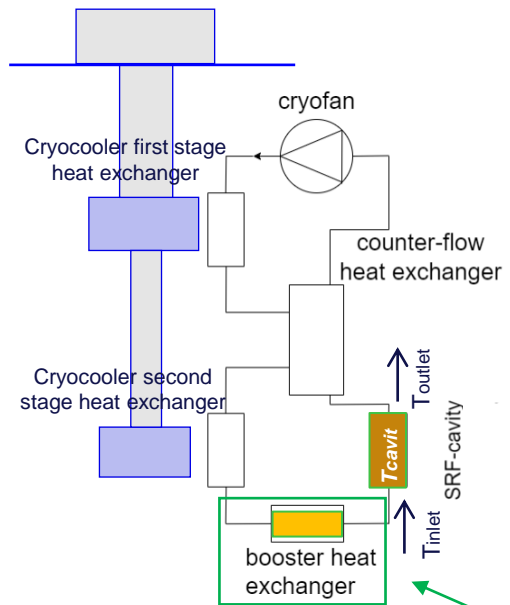


# Dry cavity cooling concept – cryocooler based for testing

*Cooling power is supplied by a **cryocooler** in combination with a **closed fluid circulation loop***



**Cryocooler standalone operation**



**Booster heat exchanger integrated operation**

Inside a 4.2 K liquid helium bath



*Radiofrequency (1.3 GHz) Cu cavity with soldered capillary*

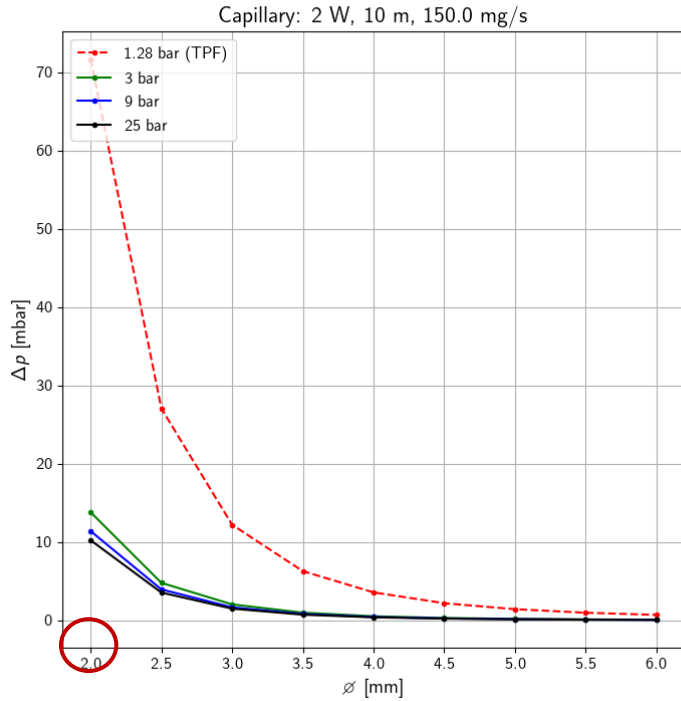


## Booster Heat Exchanger:

Will provide the necessary cooling to achieve a lower and constant inlet temperature to the cavity and to also achieve a lower cavity temperature with higher possible heat loads.

# Helium simulation code for capillary flow

Pressure drop He flow in the capillary



Temperature difference He flow to capillary wall

