

International
UON Collider
Collaboration



MuCol



Collider magnet moving system status report

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mmWG 27/06/2024**

With input from many colleagues



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INTRODUCTION

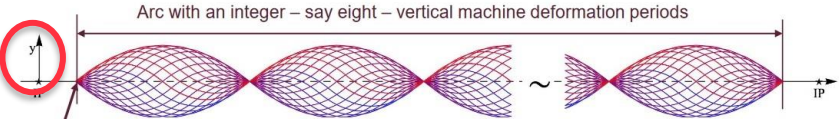
- Review of the work done so far – many points are already presented
- Mitigation requirements
- Collider magnets
- Moving the interconnections
- Support concepts
- Background:
 - [Mitigation concept IMCC 2022](#) by C. Carli
 - [Movers presentation IMCC 2023](#) by C. Accettura
 - [Neutrino radiation model IMCC 2024](#) by C. Ahdida

The concept for baseline

Mitigation by “Wobbling”

- Wobbling of machine in vertical direction – part of MAP proposal?
 - ♦ Time-dependent mechanical deformation of ring around arc (including chromatic compensation, matching section and FMC arc cells)
 - ♦ High precision movement system
 - ♦ Impact on optics?
- For 10 TeV com collider with 10 km circumference and say 4.8 km arcs



Arc with an integer – say eight – vertical machine deformation periods

Vertical bend
±16.7 Tm

- ♦ Combination of pieces of parabola – two pieces with opposite curvature one period
- ♦ Say 8 periods 660 m long periods generating angles between -1 mrad and + 1 mrad
- ♦ Magnetic field (average) bending in vertical ±0.11 T
- ♦ Excursion (maximum total) ±150 mm
- ♦ Replaces vertical Gaussian angle distribution with rms opening of ≈0.0086 mrad by about rectangular distribution within ±1 mrad

=> About two order of magnitude reduction of peak dose rates

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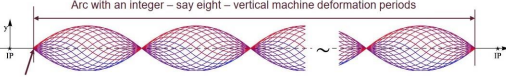
Mitigation fundamentals:

- **By C. Ahdida & J. Manczak**
- More than 100 steps leads to saturation(overlapping) within ±1 mrad range
- Range is 2 mrad, i.e. from +1 to -1 mrad per year
 - A period(two opposing parabolas) per two years
- This leads to appr. 48h between the steps(200 days of operation)
- Mitigation only applied vertically!(Y-axis on the image)

Questions:

- If 48h between the steps, is this acceptable in the most radiated area?(dose varies on the surface)
- Are there periods with no mitigation requirement?

The concept for baseline



Mitigation by “Wobbling”

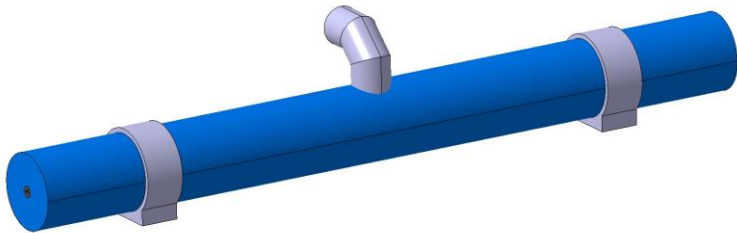
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Arc with an integer – say eight – vertical machine deformation periods

Vertical bend
 $\pm 16.7 \text{ Tm}$

- Combination of pieces of parabola – two pieces with opposite curvature one period
- Say 8 periods 660 m long periods generating angles between -1 mrad and $+1 \text{ mrad}$
- Magnetic field (average) bending in vertical $\pm 0.11 \text{ T}$
- Excursion (maximum total) $\pm 150 \text{ mm}$
- Replaces vertical Gaussian angle distribution with rms opening of $\approx 0.0086 \text{ mrad}$ by about rectangular distribution within $\pm 1 \text{ mrad}$

=> About two order of magnitude reduction of peak dose rates



MAGNETS

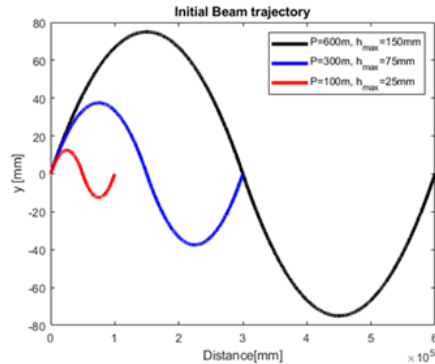
Magnet details:

- [B. Caiffi et al: Collider magnets study](#)
- Assumes 5 m dipole
- Beam aperture (5σ): $\text{Ø}47 \text{ mm}$
- Magnet movers based so far on 10 m dipole –
 - The shorter the magnet, the more motors and cabling
 - The shorter the magnet, the smaller the movements for lay-out change
- $m \approx 2450 \text{ kg/m}$ (HL-LHC D2 & W-shield)
- Supports at $1/6 * L$ from the ends
- Reducing stroke, and thus period length, requires increase of vertical field by the same factor w.r.t. the baseline
- Vacuum barrier anchoring on a moving magnet

Questions:

- Can two beam lay-outs fit one magnet position?
 - Half the number of physical magnet movements
- Position tolerance of the magnets?

INTERCONNECTIONS



Interconnection details:

- Bellows see angular movement, < 1 mrad, and offset, appr. 0.13 – 0.9 mm, depending on the magnet position on the period, due to lay-out change (100 m period, 10 m magnet)
 - Movement based on same speed for all jacks
 - Jacks can be also driven with different speed
- Leads and splices over the interconnection see the same movement – design with care but is feasible
- Running magnets into opposite extreme positions will destroy bellows! (and leads, splices)
 - Can be solved mechanically
 - Can be solved with control system

Questions:

- Other features of the interconnection?

Assumptions based on the LHC interconnections!

CRYOGENICS

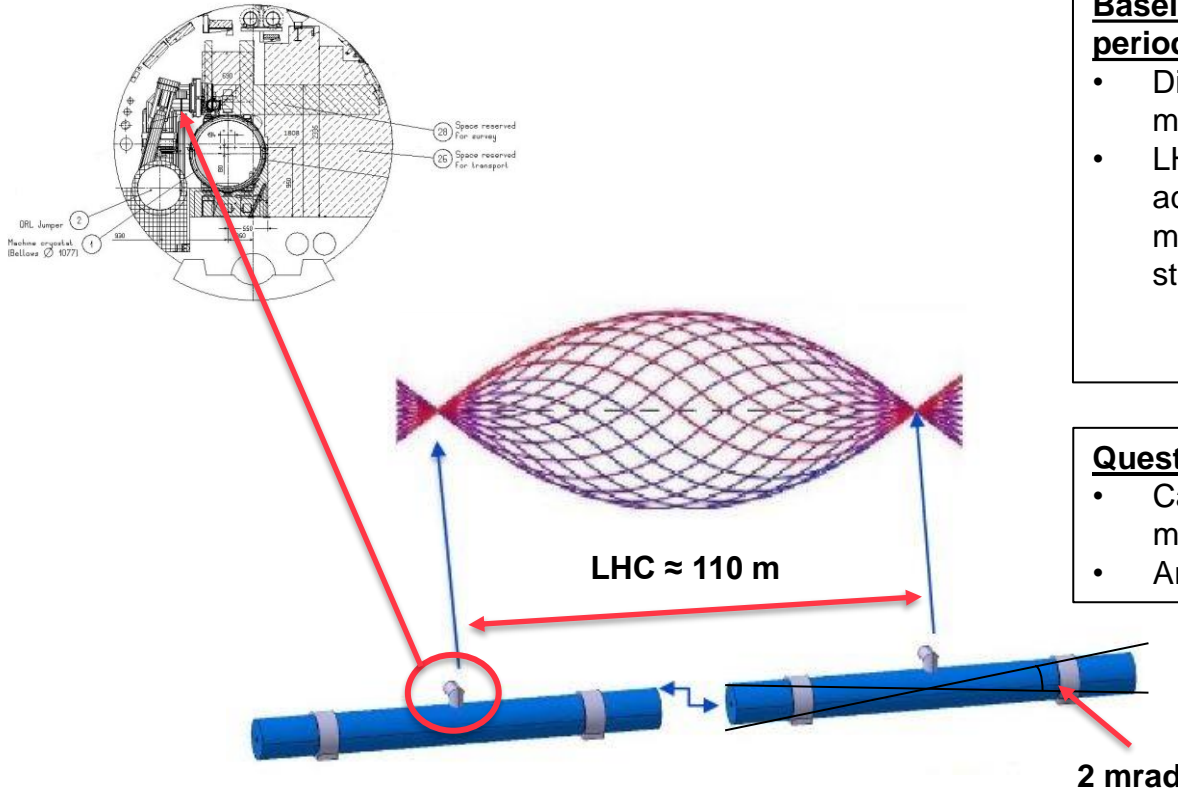
Baseline is LHC-type cryogenic line with periodic connections to magnets:

- Distance between connections (the “jumper”) at most appr. 100 m
- LHC design for the jumper cannot accommodate magnet height change as in the muon collider arc – must be placed at period start and end points.
 - It must be able to accept angular movements! (± 1 mrad)

Questions:

- Can the jumper accommodate angular movement? Can it be designed for that?
- Are there other options for the cryogenic line?

Based on the LHC!



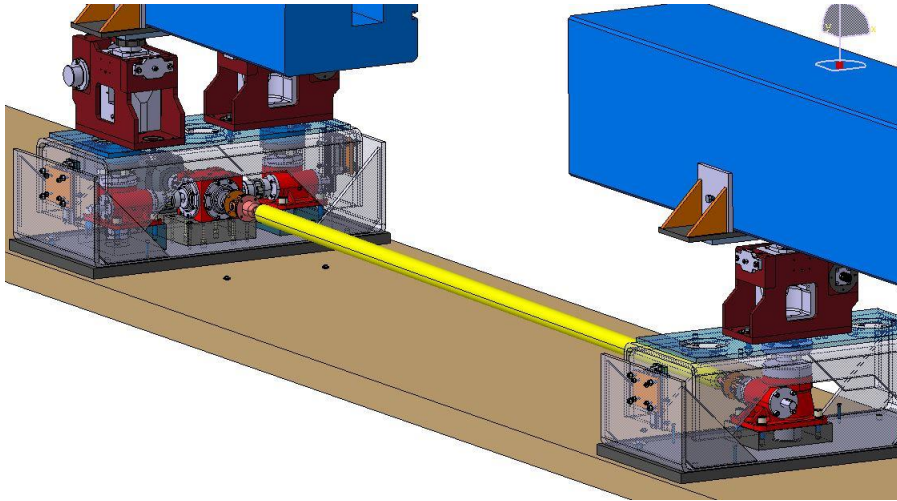
CONCEPT SPECIFICATION

collection of input from previous slides

BASELINE FOR THE MOVER SYSTEM:

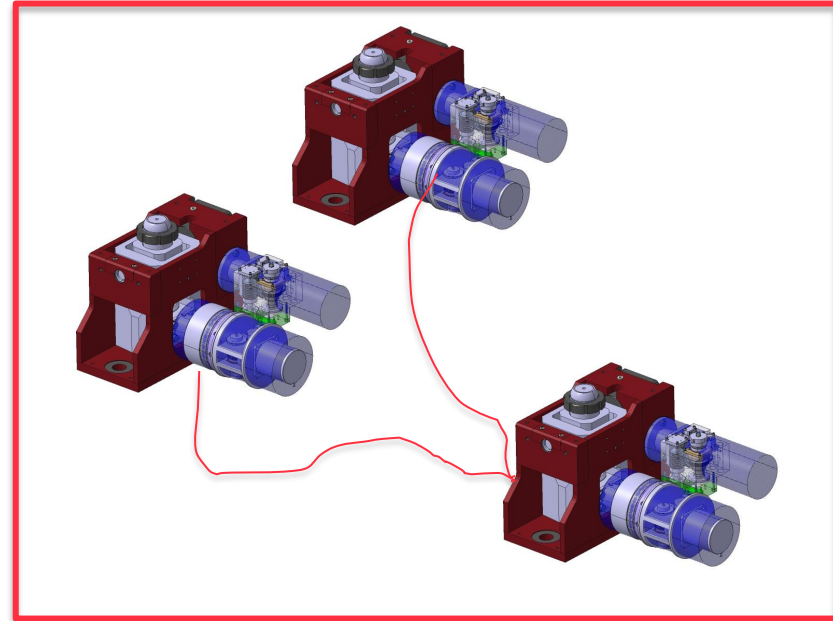
- 100 steps for the beam per year (0.02 mrad) = every 2 days with 200 days of operation
- Fitting 2 beam lay-outs per physical magnet position -> physical movement every 4 days
 - Loss of operation = movement time/96 hours -> time in hours for movement \approx percentage of operation. **Target value?**
- Steps for magnet = 2 mrad/50 (= 0.04 mrad)
 - For 10 m dipole on a 100 m period, the angular movement leads into a minimum vertical step of 133 μm .
 - **Tolerance of magnets' positions after movement? (0.004 mrad = 13 μm on a jack)**
- Period length defined by cryogenic supply would be appr. 100 m
 - 1/6 of the original period
 - Leads to 6x the original vertical field, 0.11 T -> 0.67 T
 - Leads to 1/6 of the original stroke, thus to ± 25 mm vertical stroke
- Interconnection must be protected from the vertical deviation

HOW TO PROTECT THE INTERCONNECTION?



Option 1: Mechanical protection

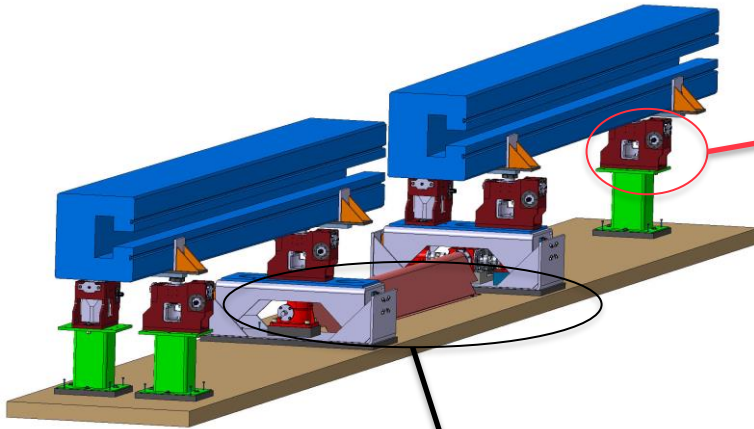
- Connect vertical jacks across the interconnection
- Use common platform
- Mechanical stoppers across the interconnection



Option 2: Control system based or “mixed”

- Movement monitoring
- Limit switches
- Deformation measurement for rigid connection

OPTION 1: TWO JACK SYSTEMS



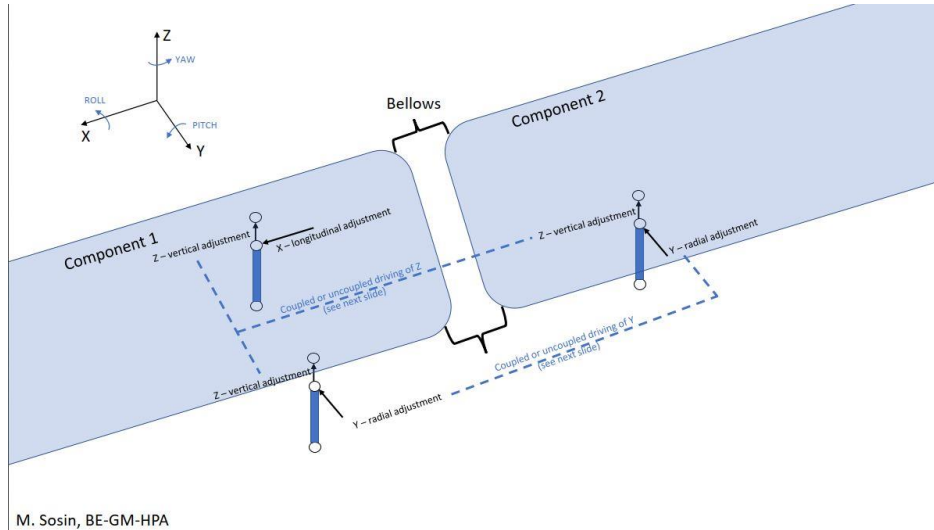
- Three jack system to drive interconnection height change with one motor
 - This system cannot offset magnet ends
 - One 0.12 kW motor
 - Commercial components
 - **Height around 400 mm**

- 6 D-o-F alignment and corrections by HL-LHC jack
 - Sufficient for required movement
 - No development cost
 - 6 motors per magnet for corrections
 - May be 5 if longitudinal is not required
 - HL-LHC jack small motorized movement protects interconnection

Pros and cons:

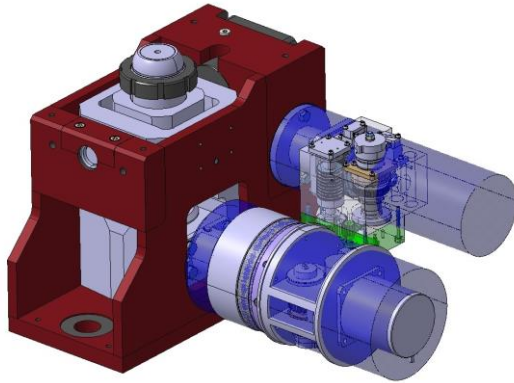
- + No jack development
- + May require only one motor for lay-out change
- Space penalty
- Steel structures for HL-LHC jacks
- May require 5 or even 6 motors for corrections, altogether 6 or 7 motors per magnet

OPTION 2: NEW JACK CONCEPT



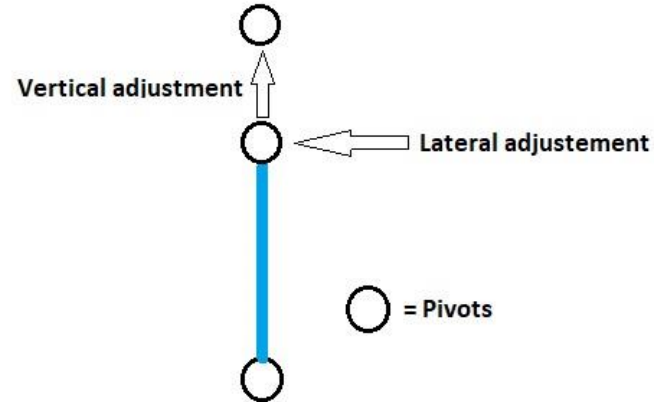
- Concept proposal by Mateusz Sosin CERN BE-GM
- Mechanically connected jacks for vertical movement
 - Drive with one motor
 - Add **clutches** to allow correction for height and tilt driven by same motor
- Add one motor for longitudinal and two for lateral corrections
 - 4 motors in total, 3 if radial alignment can be coupled and 2 if no longitudinal correction is required

NEW JACK OPTIONS



Option 2A: Modified LHC jack

- + Designed for similar loads
- + Coupling motions results in max 4, min 2 motors
- Modify vertical movement
- Modify for connected vertical movement



Option 2B: New jack development

- + Can be designed to specification from start
- + Coupling motions results in max 4, min 2 motors
- + External design possible
- Complete development program = time

TO BE STUDIED

- Design of most promising solution
- Mechanical behavior
 - Between steps
 - Friction
 - Wear
 - Done with the mock-up
- Level of control system for the required accuracy
 - Including the measurement system
 - Done with the mock-up
- Leads and splice behaviour?
 - With separate test set-up
- EMC compatibility
 - Testing of individual components(unless already certified)
- Radiation compatibility
 - Testing of individual components?(unless already certified)

FUTURE ACTIONS

- Specification definition AND approval
 - Followed by concept selection
- Launch detailed design of the concept
 - Mechanical system design can be launched following concept selection
- Control and measurement system definition
- Testing campaign for the mover mechanical system components
 - Individual components, interconnection mock-up to test the mechanical components together
 - Investigate the possibilities of a full system study with digital twin
- Design verification and production drawings for mechanical system (– five years cumulated from design launch)
 - [Collider magnet development time is much higher](#)
- Production + software
 - Time for the development of the measurement system not known!
- Series system testing
 - Fully representative mock-up for mechanical system, use also with magnet testing in string

CONCLUSIONS

- How often beam must be replaced? Every 48 h?
- How often we have to move the magnets? Every 96 h?
- The period length is 100 m?
- What is the required movement and the required accuracy?
- Developing a new jack system is most space efficient
- Collider magnet development takes much longer – delivery in 17 – 26 years
- We need a realistic mock-up to test the system behaviour
- Measurement system depends on the required accuracy – thus may be substantial development and cost

Thank you for your attention!

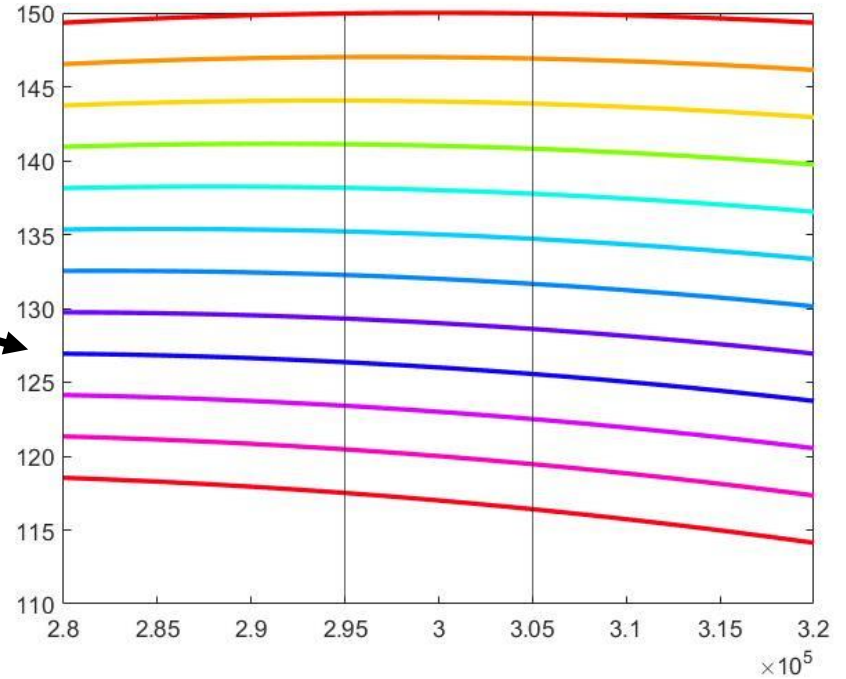
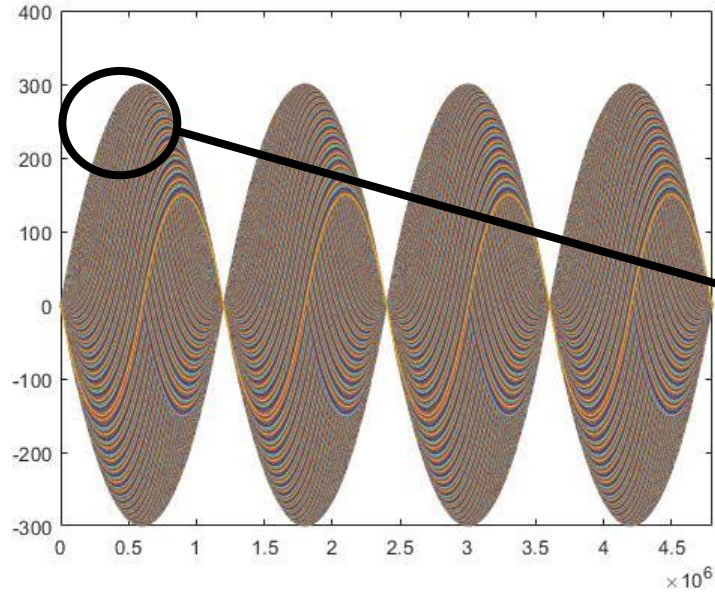
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Your questions please?

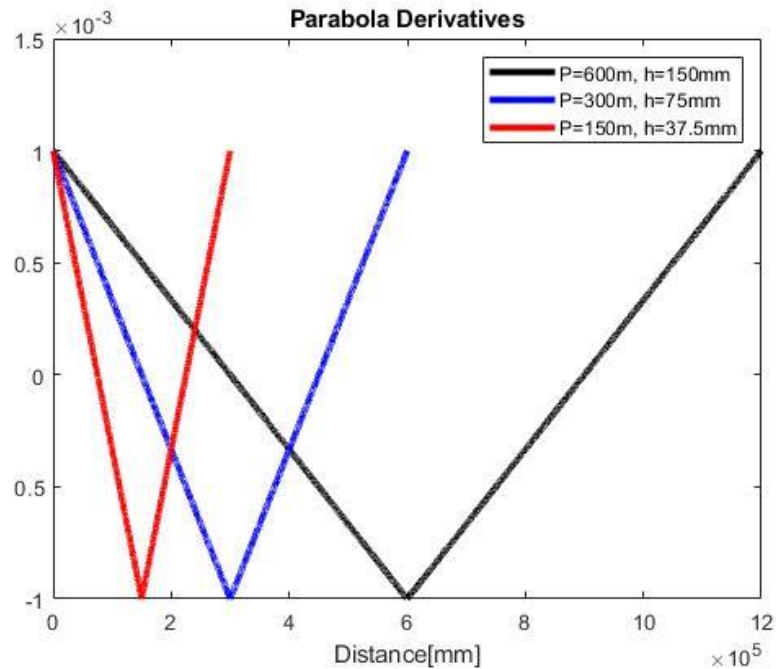
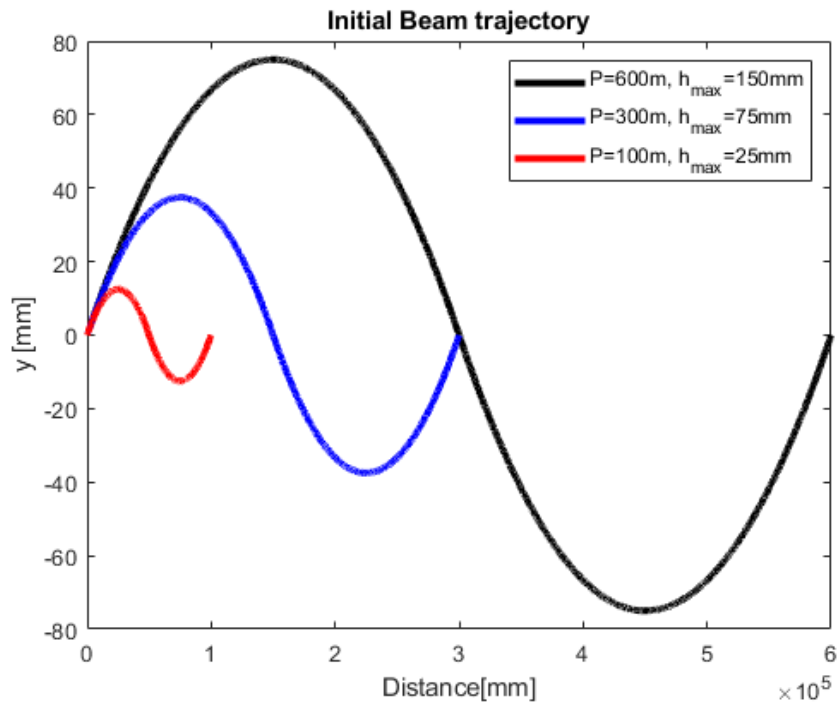


SPARE SLIDES

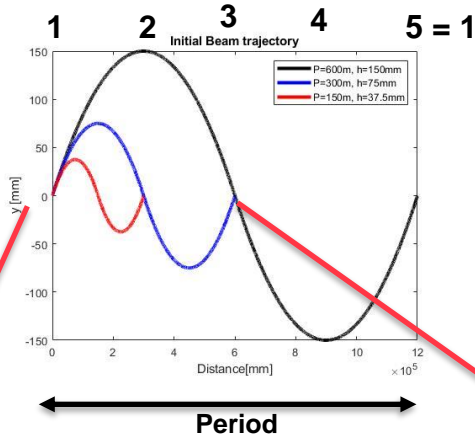
BEAM TRAJECTORIES vs. MAGNET MOVEMENTS



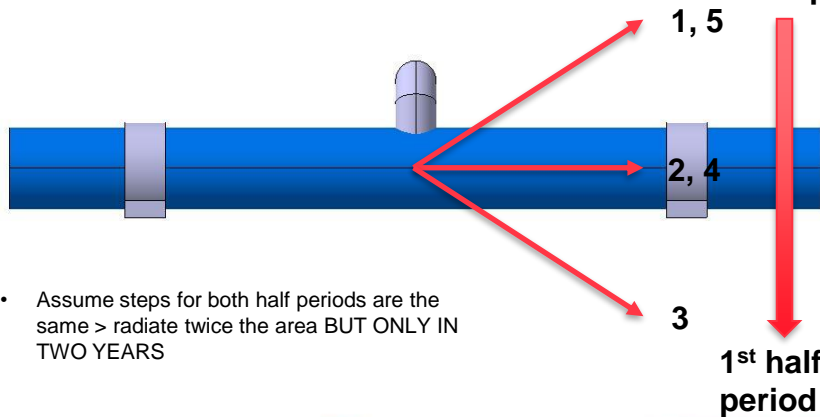
To be studied: how many beam trajectories could be fit into one magnet lay-out



MAGNET MOVEMENTS

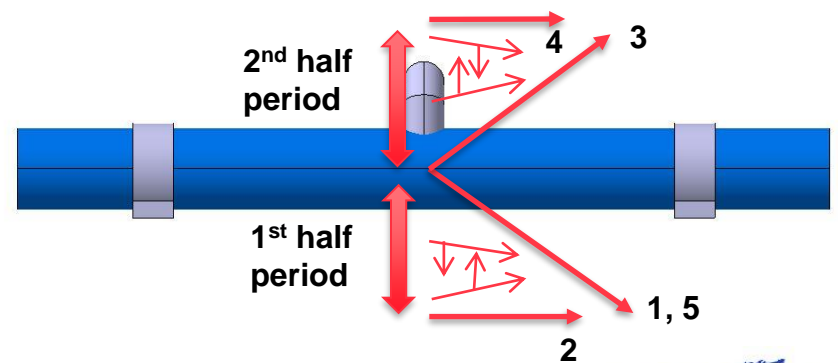


Magnets at period start/end



- Assume steps for both half periods are the same > radiate twice the area BUT ONLY IN TWO YEARS

Magnets at period mid-point



LAY-OUTS

Period	Steps	Magnet	Angular step magnet	Min jack step	Max jack step	Jack range
100 m	50	10 m	0.04 mrad	0.133 mm	0.9 mm	± 25 mm
100 m	100	10 m	0.02 mrad	0.067 mm	0.45 mm	± 25 mm
100 m	100	5 m	0.02 mrad	0.033 mm	0.23 mm	± 25 mm
600 m	50	10 m	0.04 mrad	0.133 mm	6 mm	± 150 mm