

Progress in the Design of Magnets for a Muon Collider

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on behalf of the IMCC

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A **Muon Collider (MuC)** has tremendous potential as a future Higgs factory in terms of footprint, operating costs, and physics reach!

- Given this potential and in response to recommendation from the European Strategy Group, the **IMCC** was formed in 2022 to provide a baseline concept, critical R&D demonstrators, and assess key risks and cost and power consumption drivers of a MuC
- We are considering a fast-track 3 TeV MuC and a 10 TeV MuC



Magnet Technologies are a crucial technology for all parts of a MuC complex

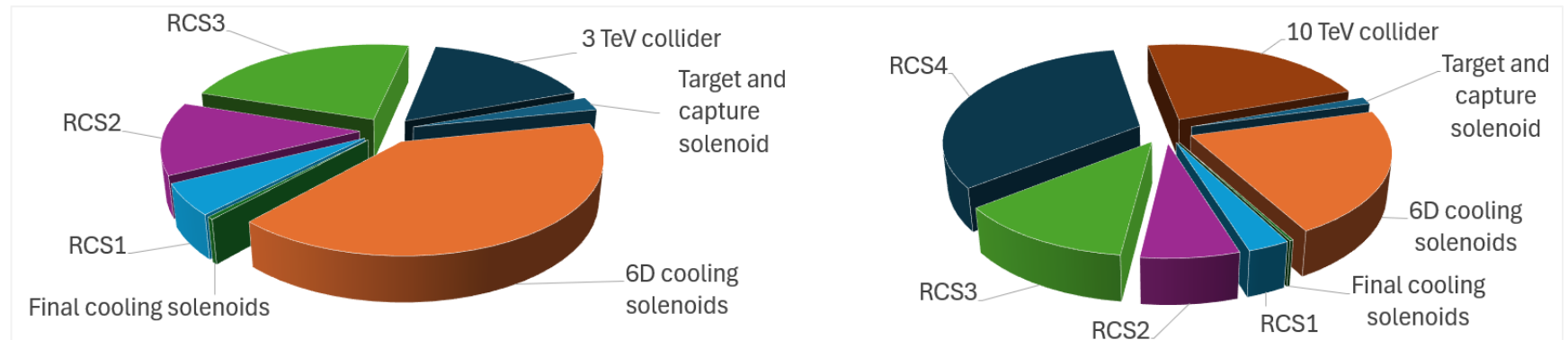
- The U.S. MAP program (2011-2016) provided a baseline MuC magnet configuration
- Focus on **HTS** technologies to enable higher field reaches and other considerations (next slide)

Recent outcomes for magnet and powering systems :

Technically limited schedule



Percentage cost contributions considering cost of materials, consumables, and labor



Motivations/Considerations for HTS Technologies



2020 update to the European Strategy for Particle Physics:
“...A detailed plan for the **minimisation of environmental impact** and for the **saving and re-use of energy** should be part of the **approval process for any major project.**”

→ **Energy efficient cryogenics! Temperature levels as high as possible**

6'600 kt of helium WW estimated reserve according to USGS report in 2021. EU assessment 2023 → **Critical Raw Material**

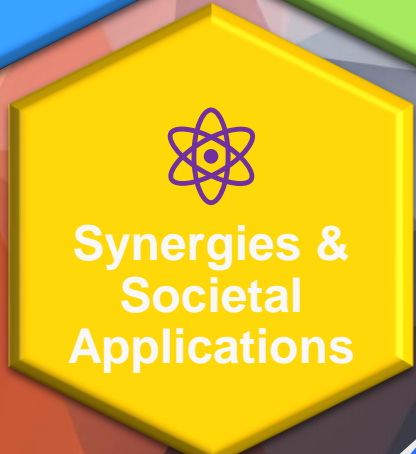


- A large component of the magnet cost is the **amount of superconductor**
- Cost depends on **material**: High-field superconductors are (significantly) more expensive than Nb-Ti

Reduce magnet cost

Reduce the coil cross section (increase J !)

Reduce the unit conductor cost



Developing **HTS Technologies** = enabling higher field reaches + being more compact!

- Thermonuclear Fusion
- MRI Technology
- High Field Science (e.g. NMR)

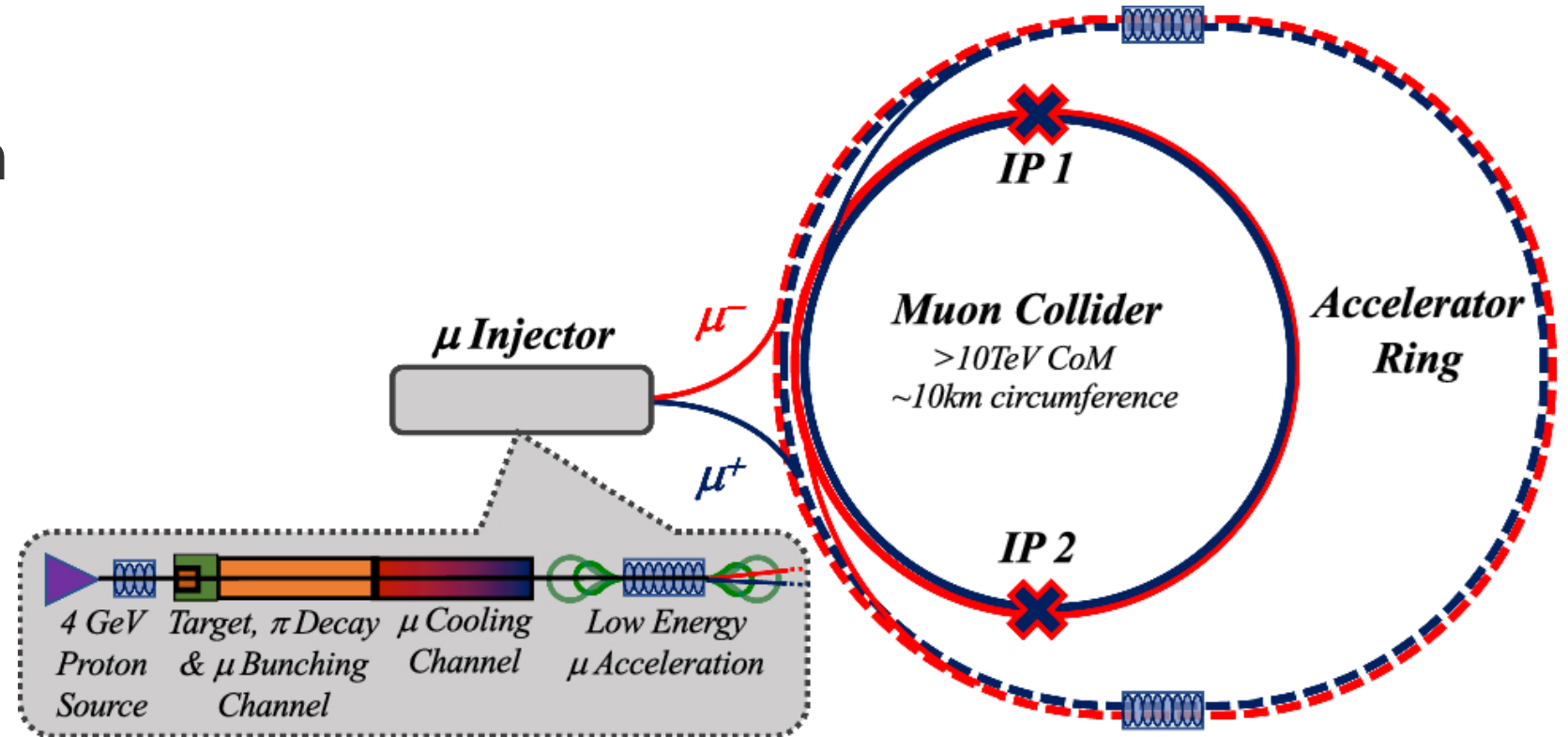
<https://www.iter.org/mach/Magnets>
<https://news.mit.edu/2021/MIT-CFS-major-advance-toward-fusion-energy-0908>

Key Challenges

- I. **Short muon (2.2 μs) lifetime**, helped by relativistic time dilation (at 5 TeV, lifetime $\rightarrow \sim 100$ ms)
 - Rapid production and acceleration of the beam, short collider circumference
- II. **Production of bright muon beams:** Luminosity $\propto \bar{B} * (N_{\mu^+} N_{\mu^-}) / (\varepsilon_{\perp})$, where \bar{B} is avg. bending field, N_{μ^+} and N_{μ^-} are the final number of muons per bunch in the collider, and ε_{\perp} is the transverse emittance.
 - Large fields at target to maximize number of captured muons, low final emittance before acceleration, large bending fields in collider
- III. **Radiation from their decay products:** ($\mu^+ \rightarrow \nu_{\mu} + \nu_e + e^+$ and $\mu^- \rightarrow \nu_{\mu} + \bar{\nu}_e + e^-$)
 - Large bore magnets to allow for protective shielding, combined function magnets to minimize straight sections in collider so as not to produce collimated beams of neutrinos

Key Magnet Systems

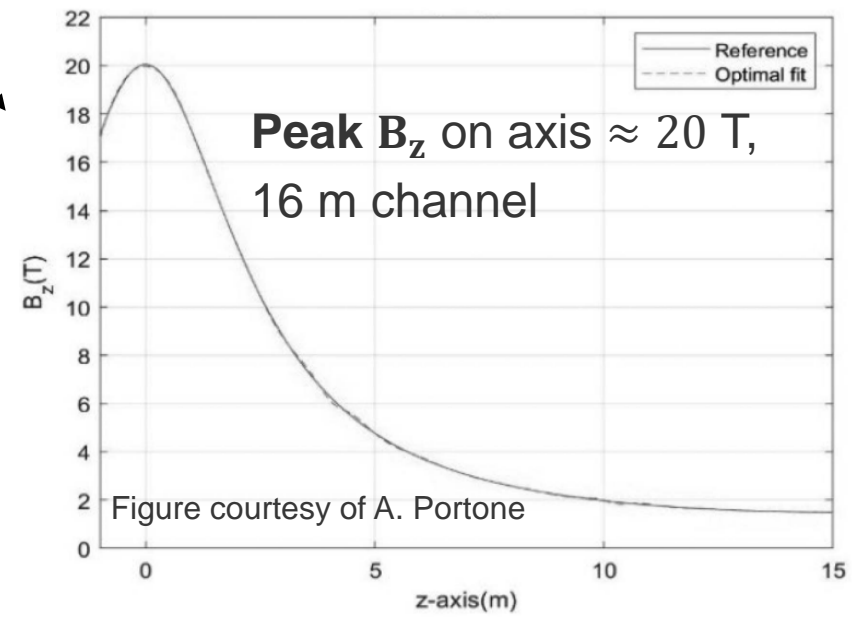
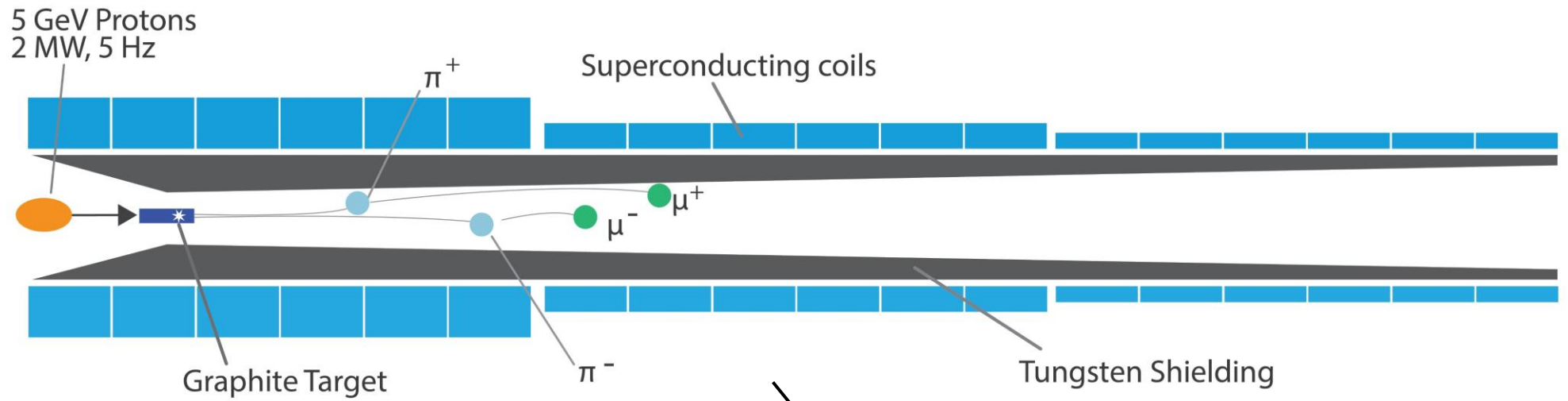
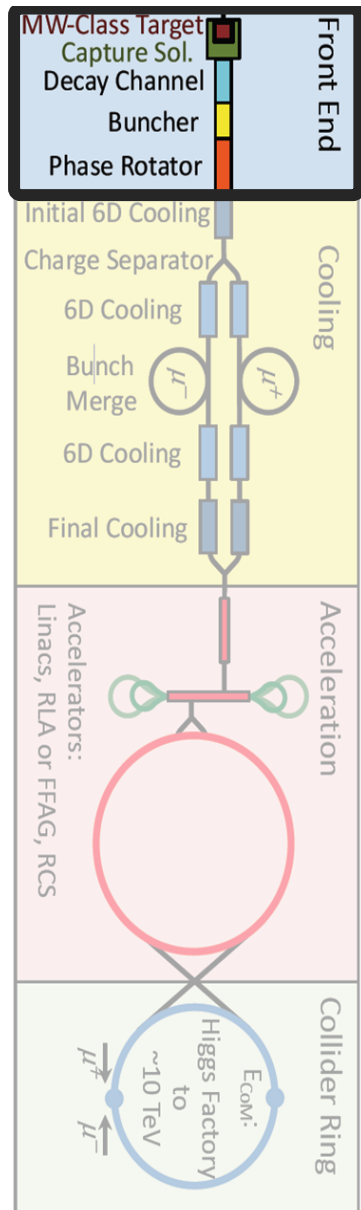
- Target, decay and capture channel
- Cooling
- Acceleration
- Collision



Key Magnet Systems

Target

Configuration Concept



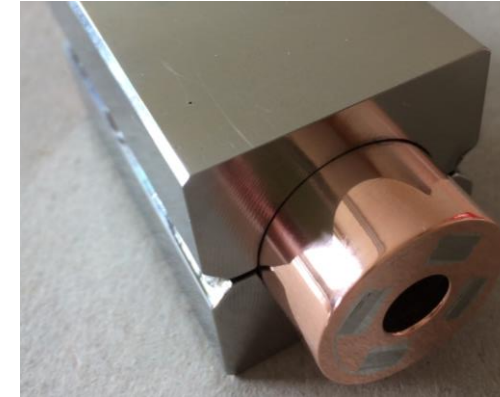
Key Magnet Systems

Target

Proposed Design Solution

- **23** HTS, ReBCO-based solenoids
- **Peak B_z** on axis ≈ 20 T, 16 m channel
- ~ 1.2 m **bore** diameter
- All coil **currents** $I \cong 61$ kA
- Operating at **20-30 K**
- Total coil weight \sim **100 tons**
- System stored energy \sim **1 GJ**
- Power consumption of \sim **1 MW**

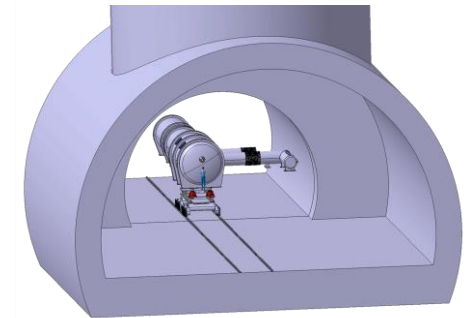
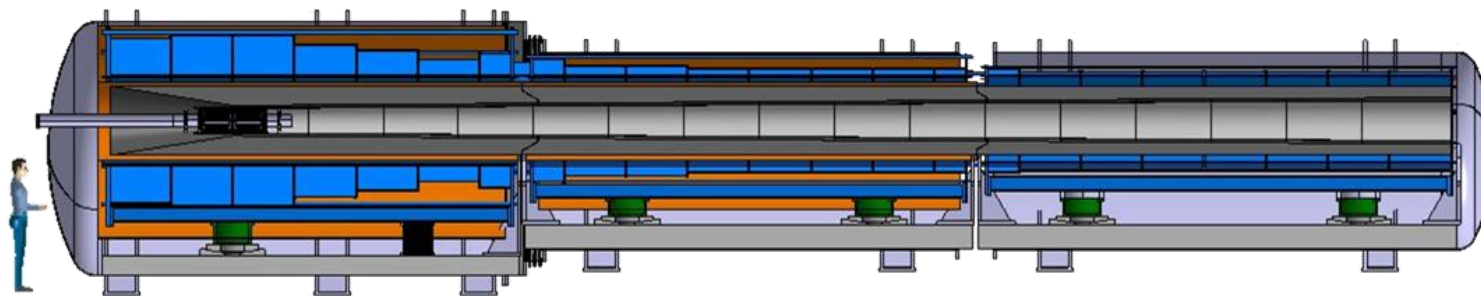
Current proposed conductor: MIT "VIPER"



$$I_{op} = 61 \text{ kA}$$

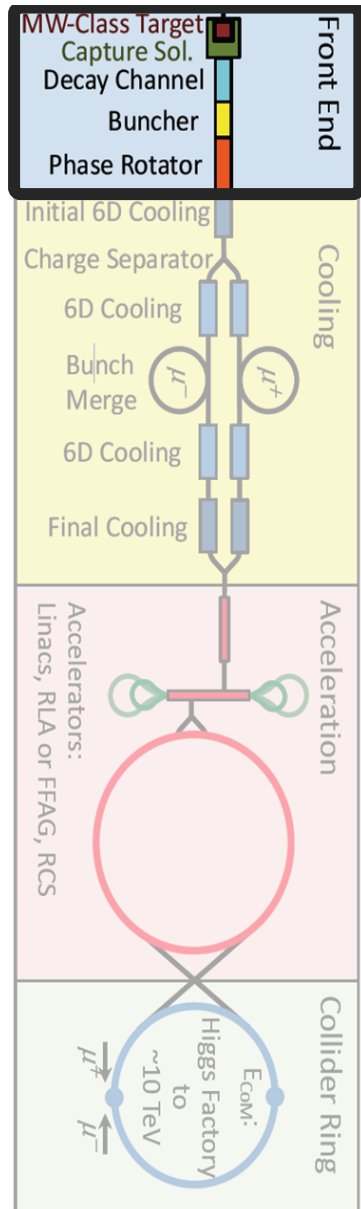
$$B_{op} = 20 \text{ T}$$

$$T_{op} = 20 \text{ K}$$



Figures and design by A. Portone, L. Bottura et. al
Accettura, C., et al. "Conceptual design of a target and capture channel for a Muon Collider.", 2024

- ✓ Magnetic Design
- ✓ Detailed structural & local analyses
- Design integration work

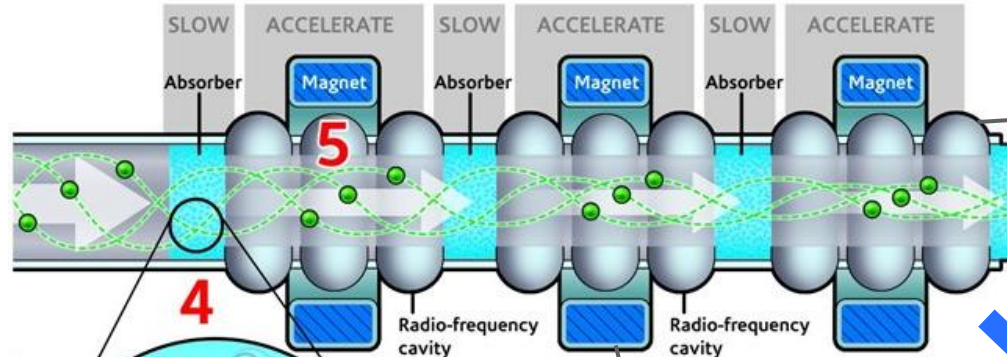
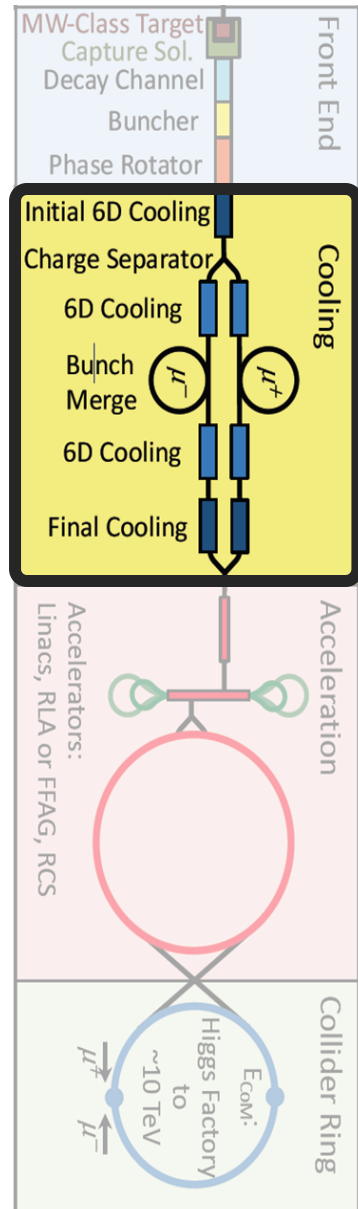


Key Magnet Systems

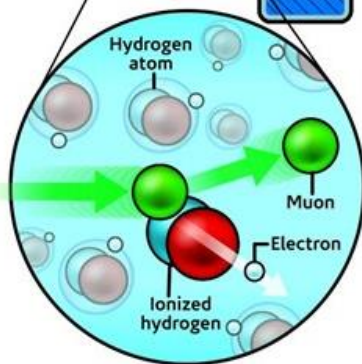
Cooling – 6D

Concept

Cooling system goal is to reduce the normalized rms transverse emittance of the beam by ~ 3 orders of magnitude to roughly $30 \mu\text{m} \cdot \text{rad}$



RF cavities re-accelerate muons in longitudinal direction



Infographic: STFC, Ben Gilliland

Solenoids confine muons radially

Absorbers slow muons down in all directions

Cooling Cell Example

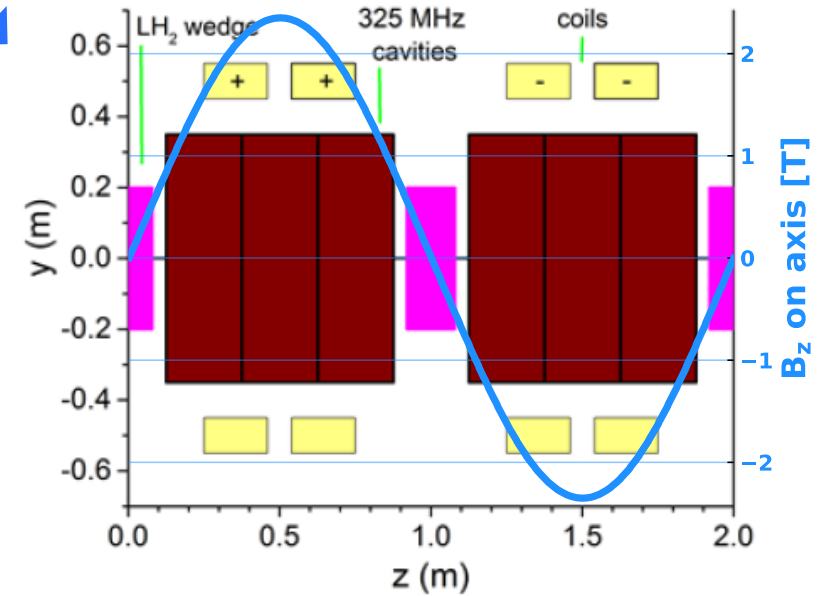


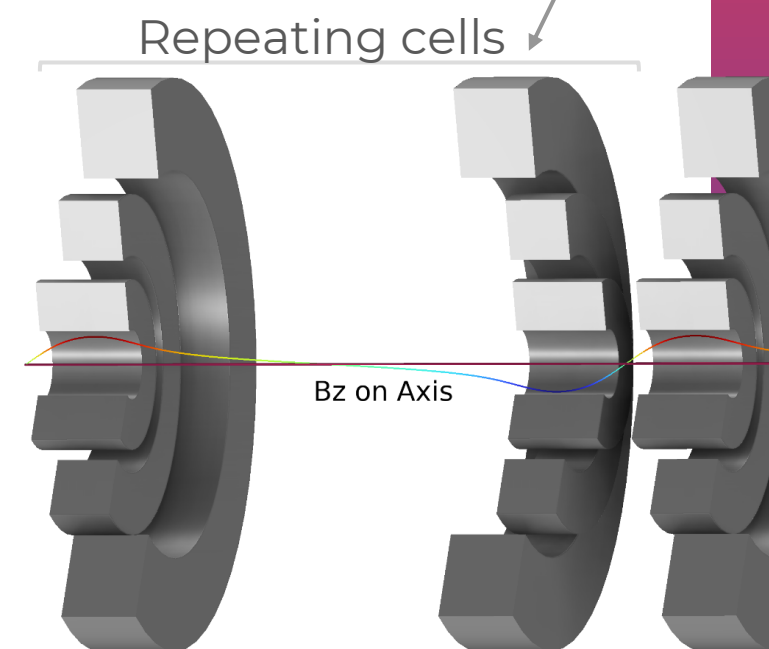
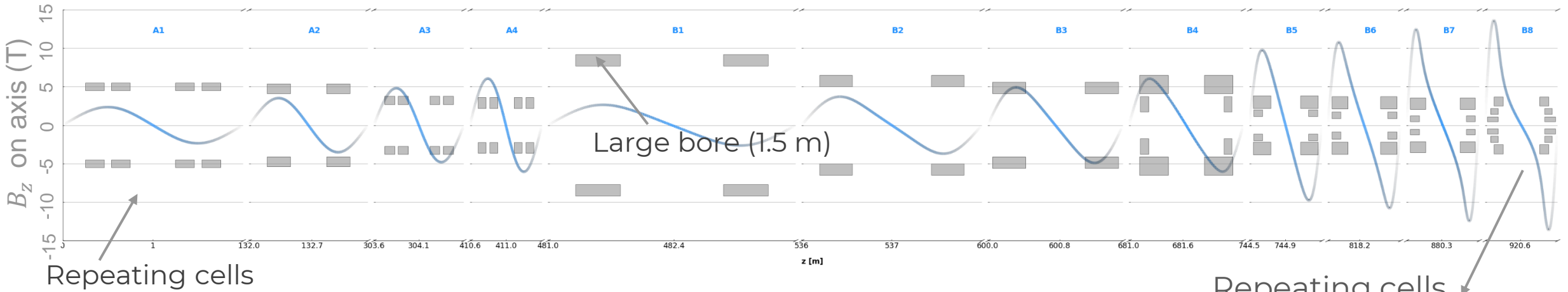
Image from Stratakis, Diktys et al "Rectilinear six-dimensional ionization cooling channel for a muon collider: A theoretical and numerical study." *Physical Review Special Topics-Accelerators and Beams* 18.3 (2015): 031003.

Key Magnet Systems

Cooling – 6D

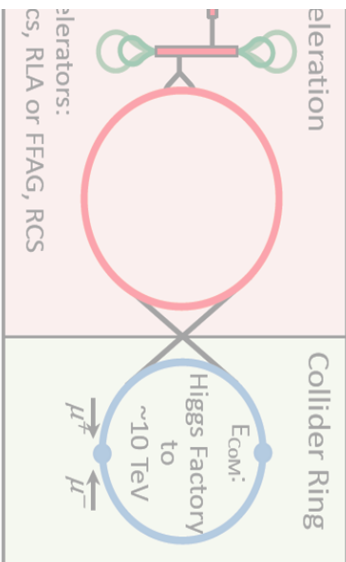
Baseline Reference (MAP) Evaluation

~3000 solenoids per ~1 km long cooling chain | 18 unique solenoid types
 On axis field 2.4 T to 13.6 T | Bore size from 90 mm to 1.5 m



Un-optimized from engineering perspective

- Large average **hoop stresses** (peak 340 MPa)
- Tensile **radial stresses** (peak 20 MPa)
- Large stored **magnetic energies** (up to 45 MJ in one coil)
- Largest contributor to **cost** of magnets & powering in 3 TeV machine

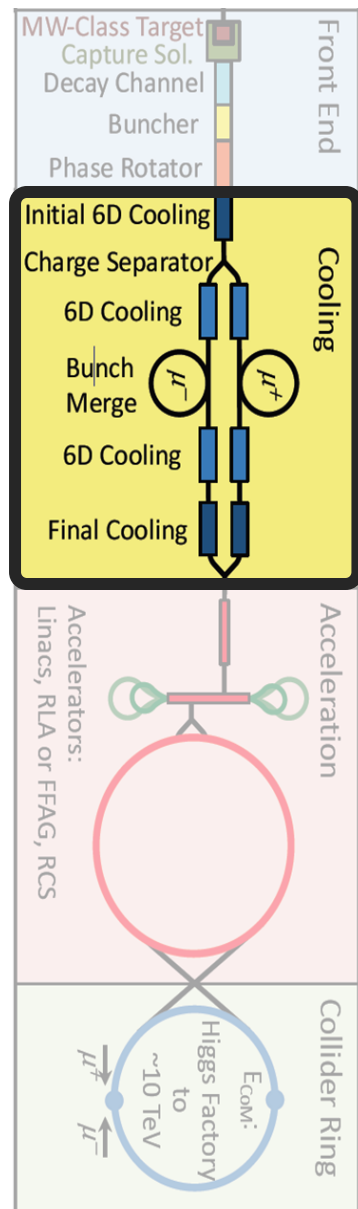
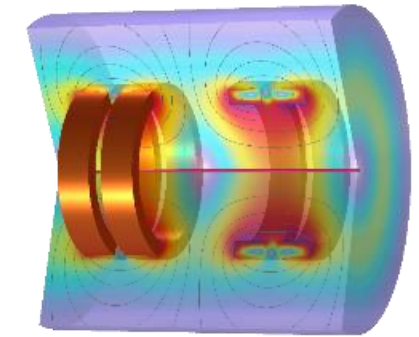
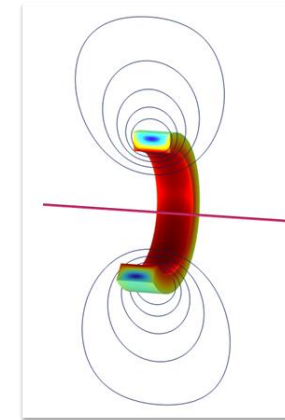


Key Magnet Systems

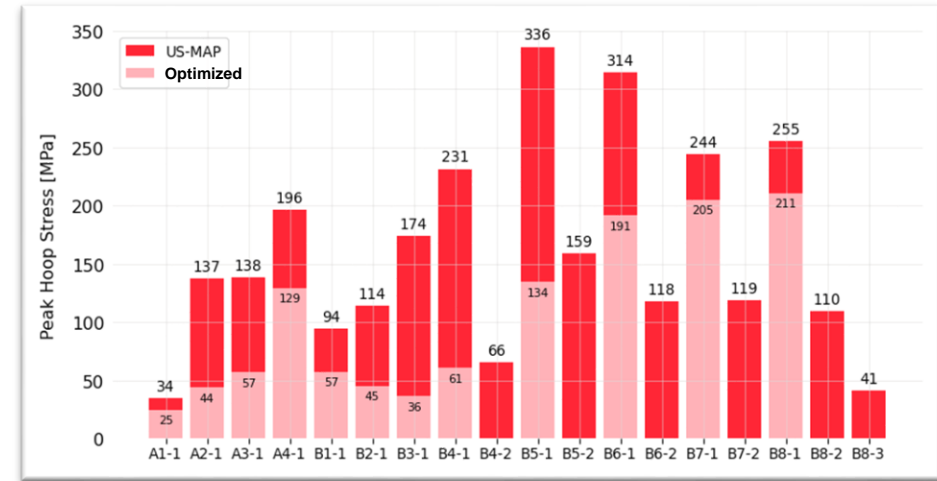
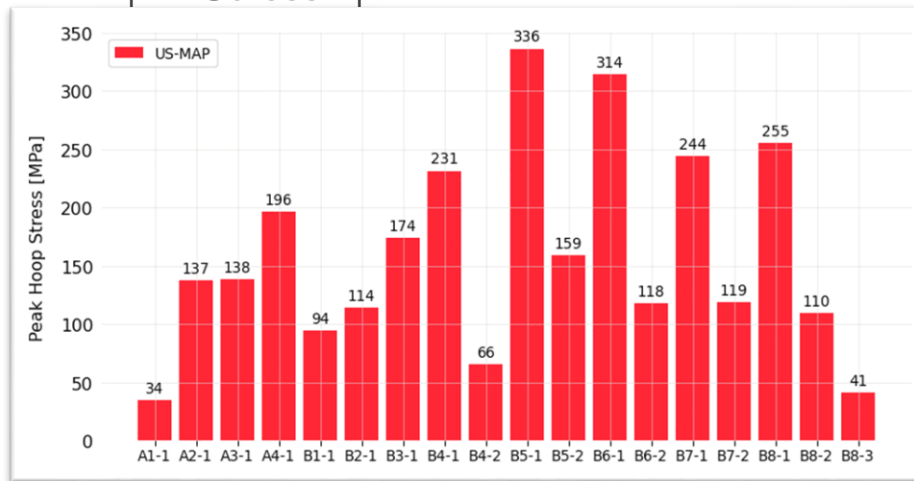
Cooling – 6D

Unique Problem: Numerical Optimization Routine

- Input**
- Desired field on axis + some tolerance
 - Constraints (\mathbf{J} , cell length, search resolution, ...)
- Output**
- Many solenoid combination solutions and properties (single coil stresses, peak fields, etc.)



Example: **Stress** optimization



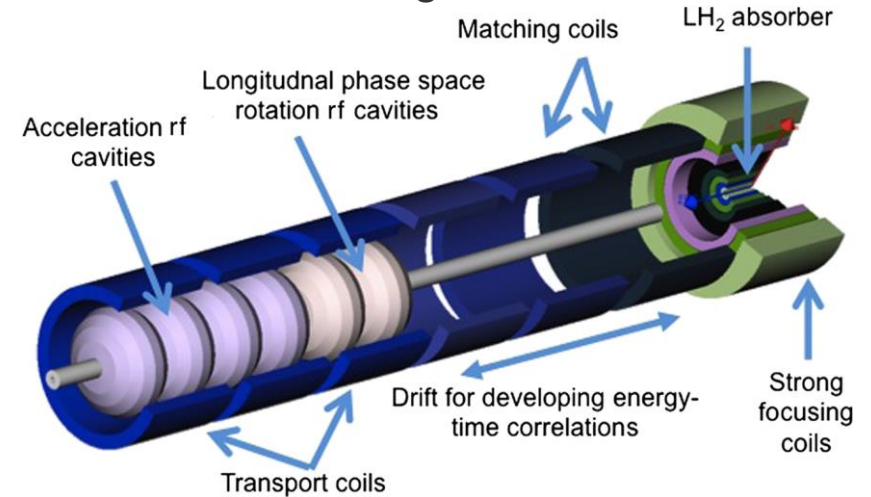
- **Optimization** is an ongoing iteration with beam optics to improve and realize a realistic solenoid configuration
- Integrated **cooling cell demonstrator**

Final **emittance** of muon beam is inversely proportional to final cooling solenoid field strength → considering 14 **very high field** Final Cooling Solenoid Cells

Current Design

- Magnetic field $B_z \geq 40 \text{ T}$
- Bore diameter **50 mm**
- Not/Metal-Insulated (N/M-I) HTS solenoids
- Field homogeneity w/in 1% over 0.5 m central axis
- Energizing time ≤ 6 hrs, persistency 0.1 Units/s

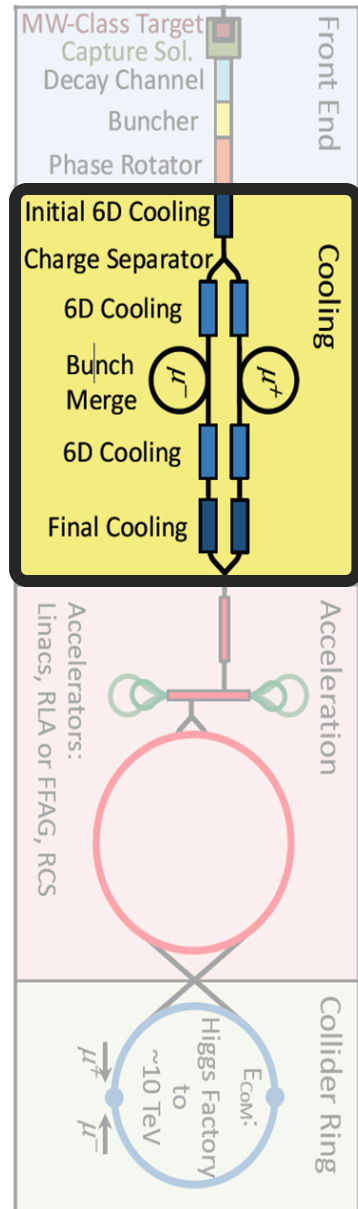
Final Cooling Cell Schematic



Sayed et al. Phys. Rev. ST Accel. Beams **18**, 091001

Critical design parameters:

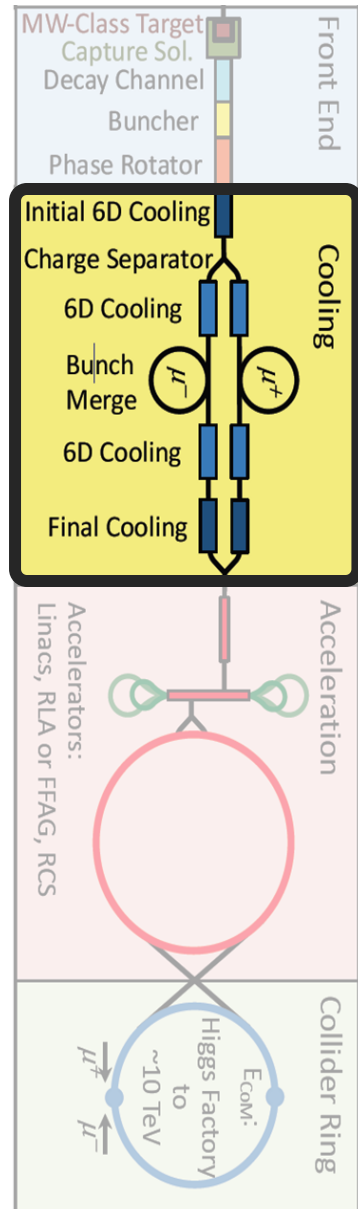
- Stress state (no tensile radial stress, hoop stress 600 MPa peak)
- Transverse resistance – low enough for quench protection, but high enough to enable a full ramp < 6 hours



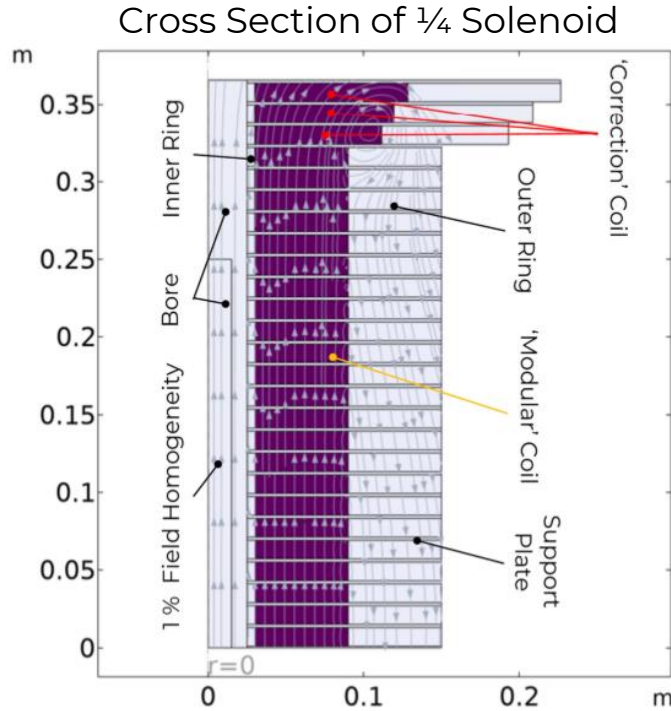
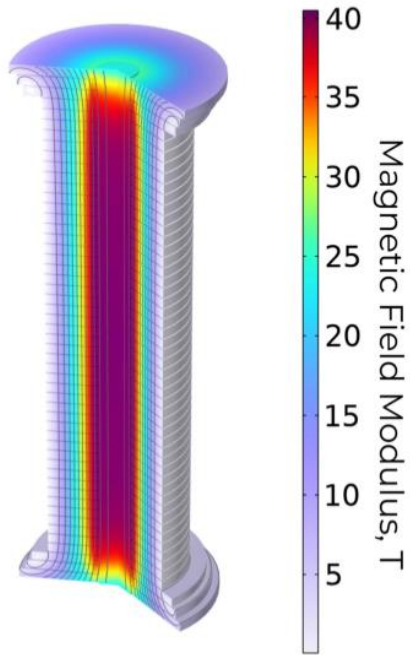
Key Magnet Systems

Cooling – Final

Proposed Design Solution



lines represent the field direction



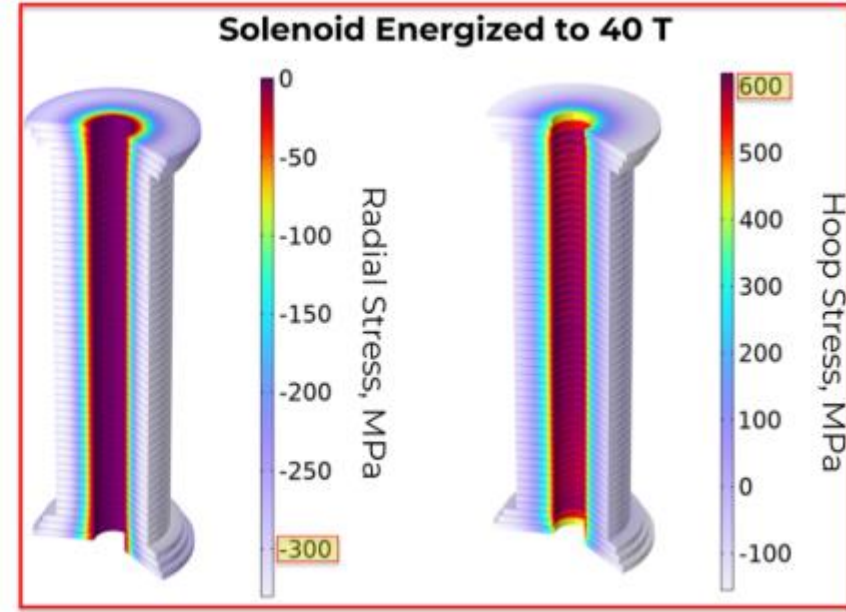
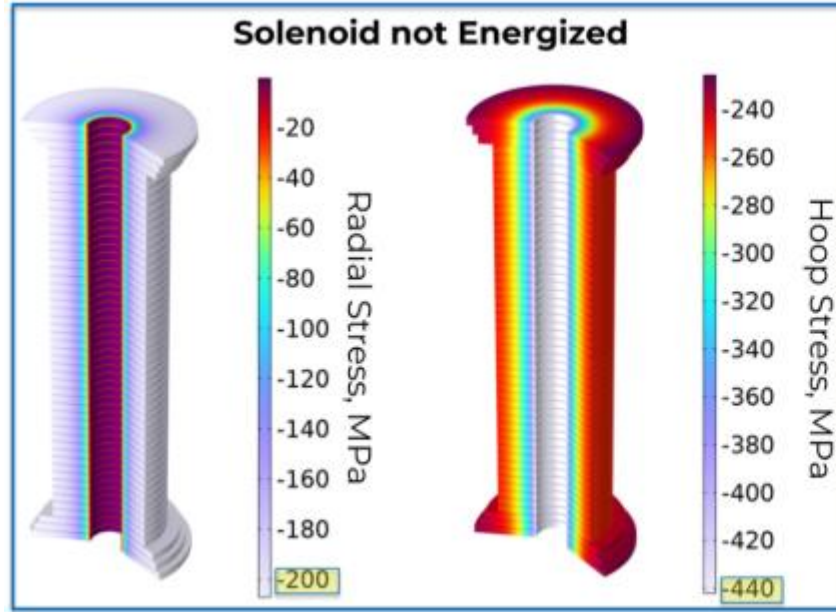
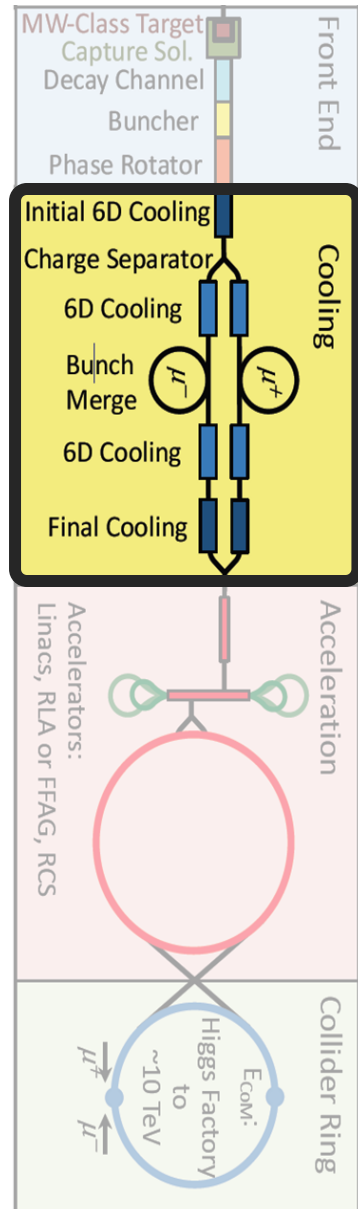
- Modular pancake design
- Supporting outer ring and plates to manage hoop, radial and vertical stresses
- Stack of soft-soldered pancakes
- Outer radius 150 mm
- $J = 650 \text{ A/mm}^2$
- 12 mm wide tape

Figures courtesy of B. Bordini, CERN. Bordini, B., et al. "Conceptual Design of a ReBCO Non/Metal-Insulated Ultra-High Field Solenoid for the Muon Collider." 2024

Key Magnet Systems

Cooling – Final

Proposed Design Solution



Figures courtesy of B. Bordini, CERN. Bordini, B., et al. "Conceptual Design of a ReBCO Non/Metal-Insulated Ultra-High Field Solenoid for the Muon Collider." 2024

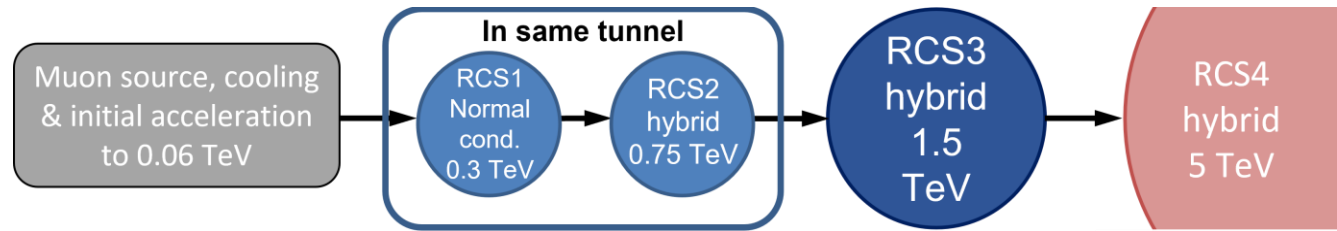
A **radial precompression of at least ~ 200 MPa** is essential to limit the conductor hoop stress to acceptable values and to prevent tensile radial stress.

- Detailed thermo-electromagnetic design and tests are in progress to validate the concept and analyze the coil in transient conditions like quench or ramp-up.
- Significant R&D required, however contributes only <0.5% to cost of magnets and powering systems of a MuC!

Key Magnet Systems

Acceleration

Concept



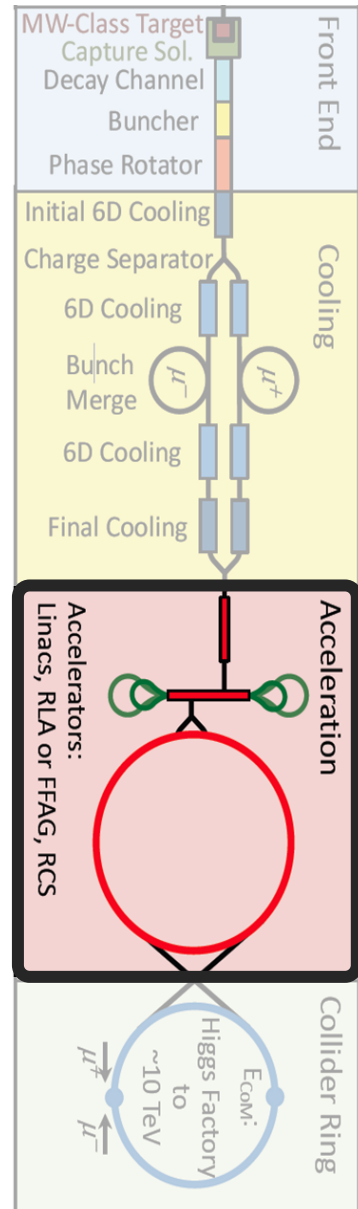
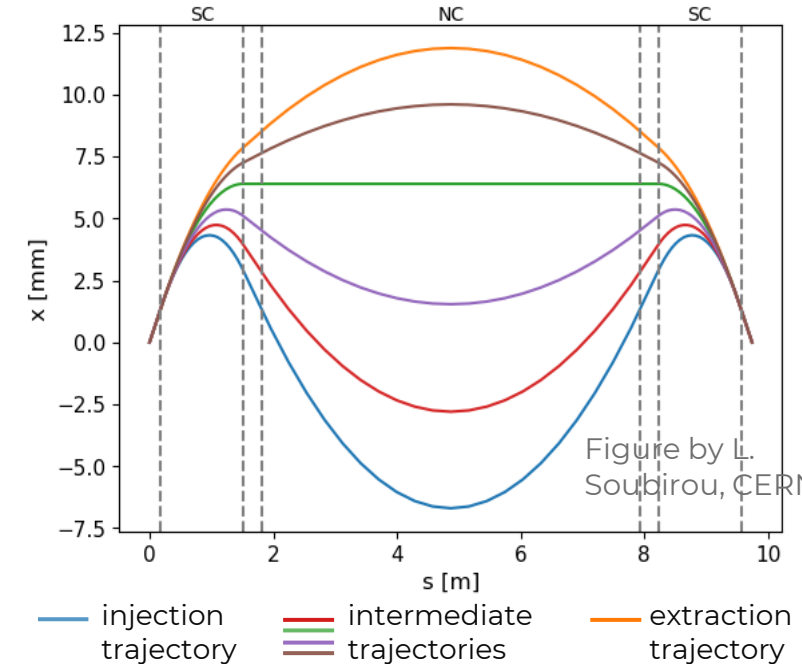
- Linear accelerator
- Rapid-cycling synchrotron (**RCS**)
 - NC fast-ramping magnets sweep from injection to extraction field levels 0.36 to 1.8 T within 0.35 ms (4 kT/s)
- Hybrid Cycling Synchrotrons (**HCS**)
 - Static SC magnets establish field offset of 10 T (or assumed 16 T in final HCS)
 - NC fast-ramping magnets swing from -1.8 to 1.8 T in ramp rates up to 3.3 kT/s

10 T steady state, +/- 1.8 T up to 4 kT/s
30x100 mm aperture

Challenges

- I. **Management of the power** (10s of GW) in the resistive dipoles,
 - Minimize stored magnetic energy (minimizes the stored power)
 - Efficient energy storage and recovery
 - **Limit the total losses** (iron hysteresis, eddy currents, etc.)
- II. **Cost:** Magnets + powering in accelerators is largest cost contribution!

Hybrid Cycled Synchrotron



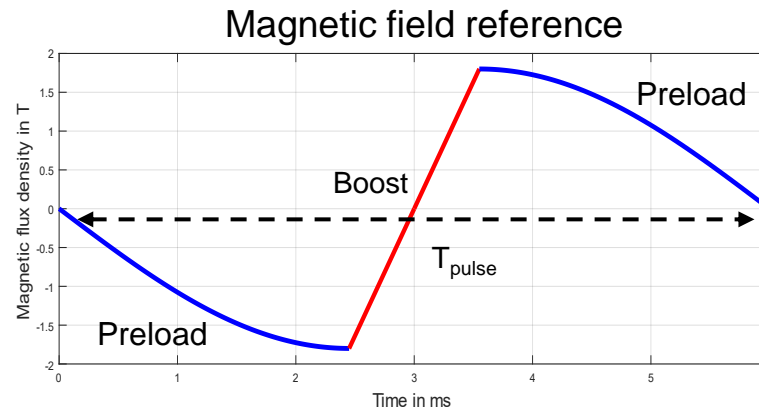
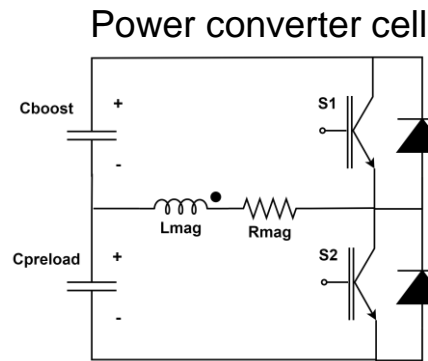
Key Magnet Systems

Acceleration

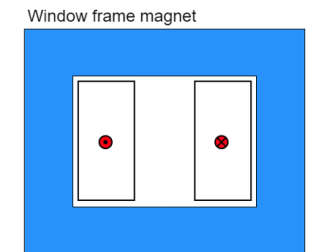
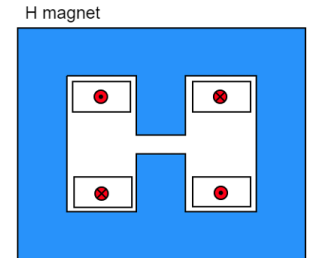
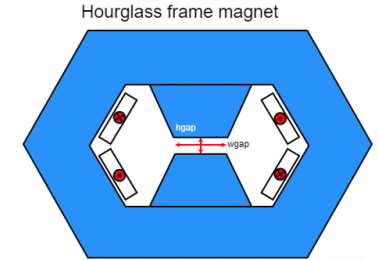
Ongoing Designs

Breschi, M., et al. "Comparative analysis of resistive dipole accelerator magnets for a Muon Collider", 2024

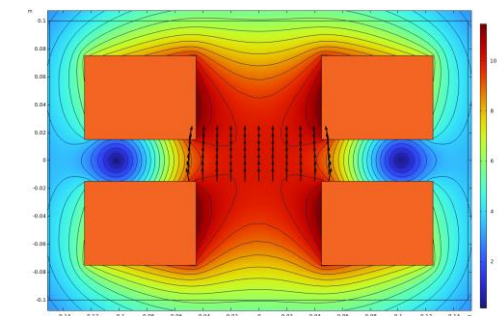
1. **NC Dipole Configuration Optimization** in Matlab (and FEMM) carried out to minimize the stored energy and losses while maintaining the best field homogeneity, considering different configurations, iron cross-sections, materials and current densities.
 - Best compromise b/w stored energy, losses and manufacturing simplicity is the **H-type magnet**.
2. **Powering system cost optimization carried out** in Python, considering different power converter options

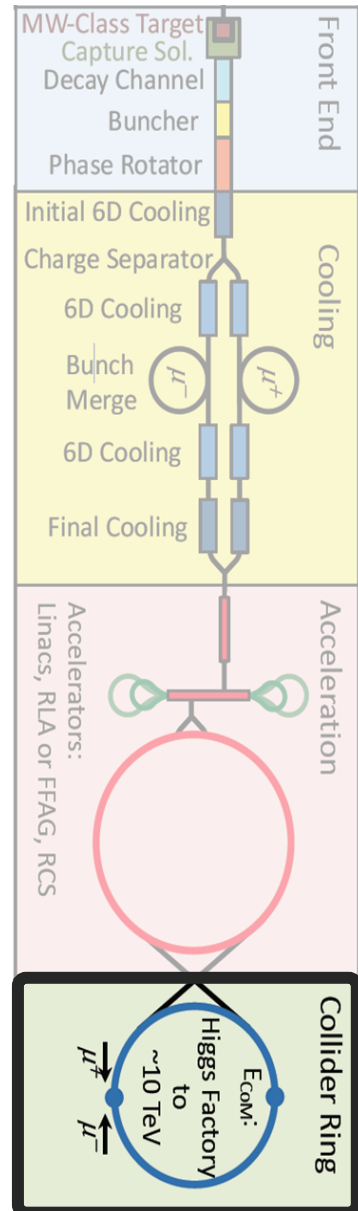


3. **SC Dipole Optimization Routine** in progress for rectangular aperture HTS racetrack coils with a target field of 10 T while minimizing cost for a target field quality.



Figures courtesy of M. Breschi, F. Boattini, et al.





Main bending dipoles

- 16 T, 158 mm aperture
- 5 m length
- 1200 magnets

Arc

- Combined function dip. + sext, $B_1 + B$
 $B_1 \sim 14$ T, $G \sim \pm 7100$ T/m², 100 mm aperture
- Combined function dip. + quad., $B_1 \sim 8$ T,
 $G \sim \pm 320$ T/m, 100 mm aperture

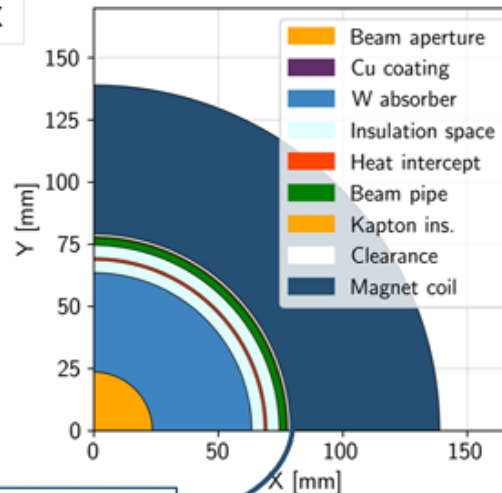
IR

- Quads $G \sim \pm 300$ T/m, aperture ~ 120 mm
- Quads $G \sim \pm 110$ T/m, aperture ~ 300 mm
- Combined function dip. + quad., $B_1 \sim 8$ T, $G \sim \pm 100$ T/m, 280 mm aperture

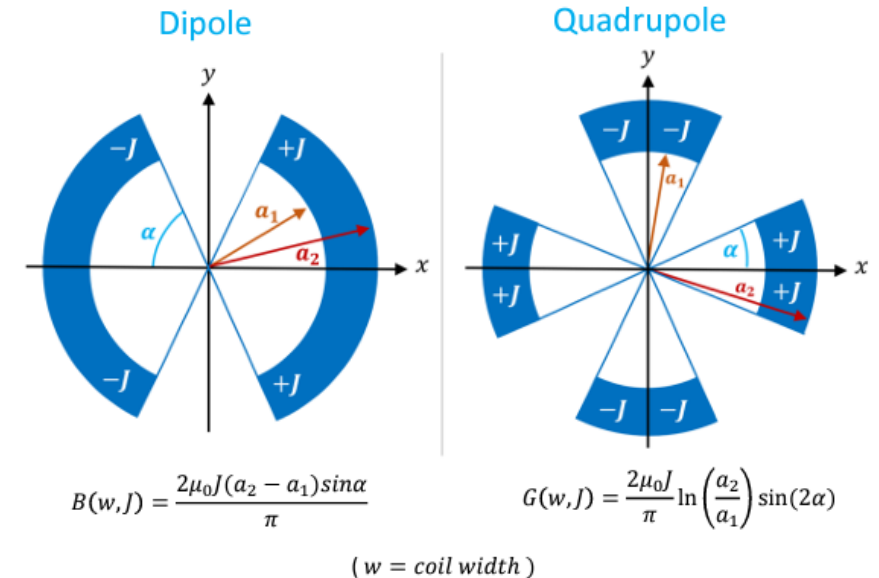
Assuming 10 TeV machine and coil at 4.5 K

- Beam aperture (5σ) 23.5 mm radius
 - Cu layer beam screen 0.01 mm thick
 - Tungsten absorber 40 mm thick
 - Insulation space 5 mm thick
 - Heat intercept 1 mm thick
 - Insulation space 5 mm thick
 - Beam pipe 3 mm thick
 - Kapton insulation 0.5 mm thick
 - Clearance 1 mm thick
 - Coil pack* (60 mm thick)
- *thickness TBD, placeholder

Courtesy of Patricia Borges de Sousa
<https://indico.cern.ch/event/2125007/contributions/5357594/>



Analytic Design Study sector coil approximation dipole and quadrupole



Figures courtesy of D. Novelli, INFN-Genoa

Key Magnet Systems

Collision

Analytic design study

Novelli, Daniel, et al. "Analytical evaluation of dipole performance limits for a Muon Collider."

Ongoing study considering operating margins, peak stress, quench protection and total cost limit, assuming sector coil geometry with

- NbTi at 1.9 K
- Nb₃Sn at 4.5 K
- HTS (ReBCO) at 4.5 and 20 K (*operating at higher temp. also can reduce absorber thickness!)

Summarized into Aperture vs Bore field (AB) plots.

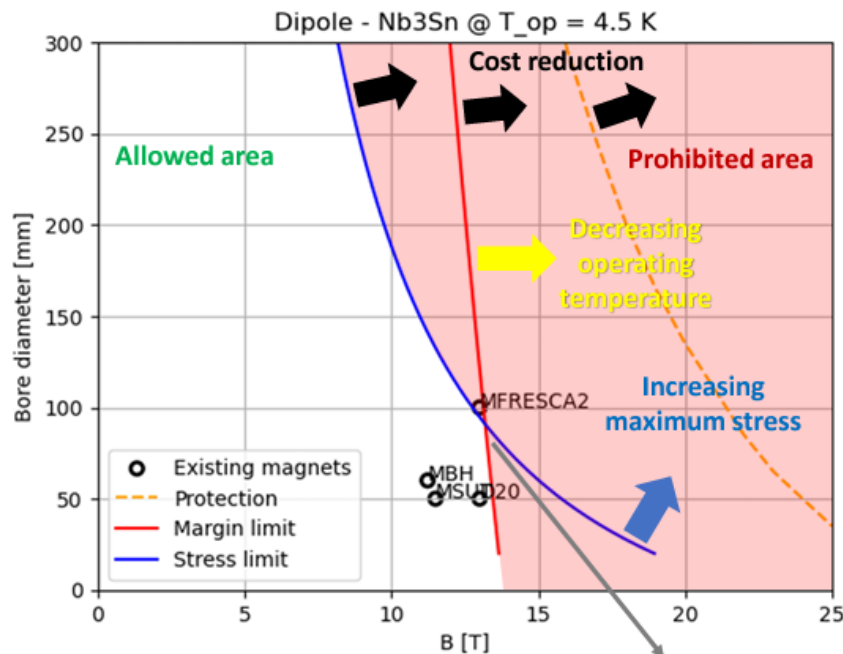
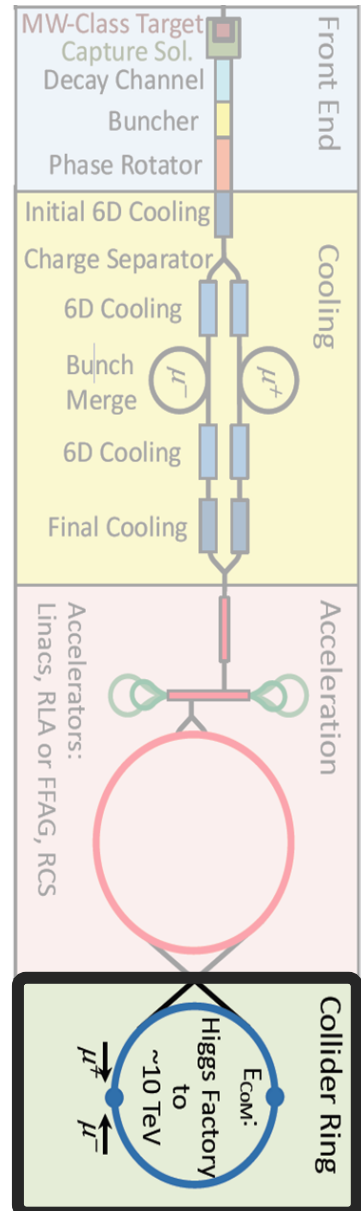


Figure courtesy of D. Novelli, INFN-Genoa

Conclusions so far (main bending dipoles):

- **Nb₃Sn**: limited by peak stress and operating margin, provides feasible solutions only up to 14 T (can be considered for a 3 TeV MuC)
- **Not/metal-insulated ReBCO at 20 K**: limited by balance between total cost of superconductor and quench protection. Two configurations can be 16 T, 100 mm or 14 T, 140 mm





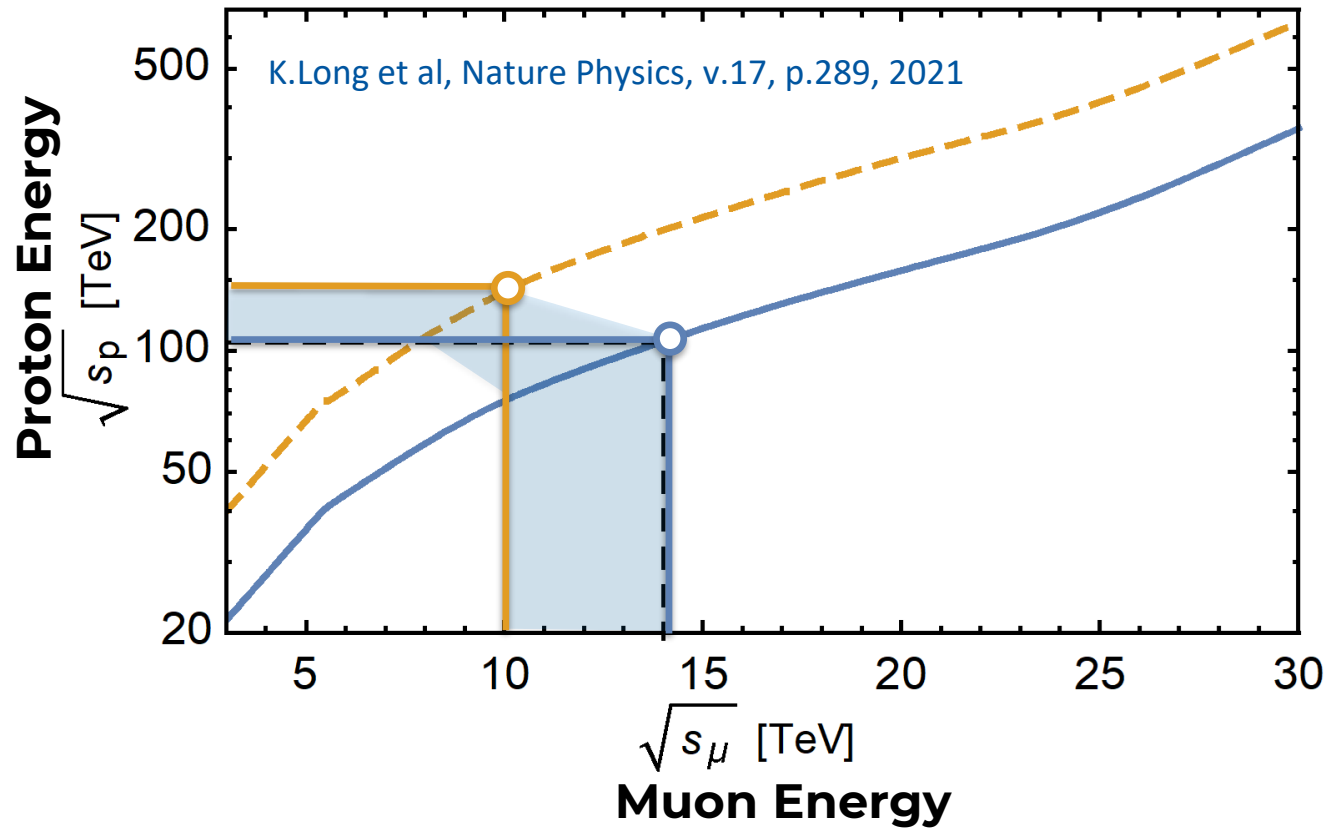
**Funded by
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Back-Up Slides

Motivation: Muon Collider – Physics Reach

Energy at which the proton (hadron) collider cross-section equals that of muon (lepton) collider for selected production and decay channels



--- comparable processes from muon and proton production
— possible QCD enhancement of production rates of a proton-proton collider

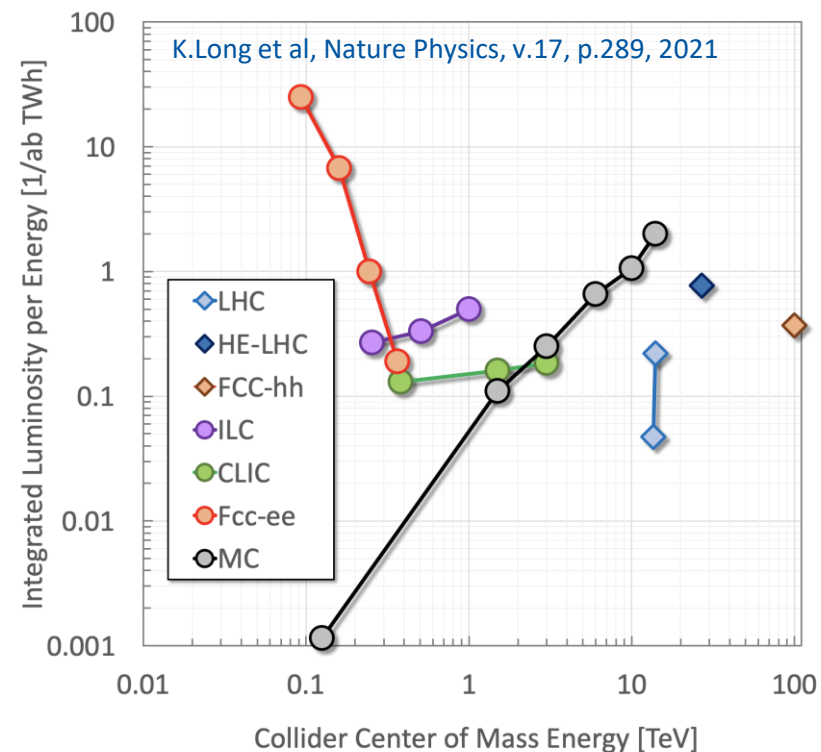
Muon collisions in the range of 10 TeV have comparable discovery potential to hadron collision in the range of 100 TeV

Future Considerations for the Next HEP Machine



V. Shiltsev et al, *Reviews of Modern Physics*, v.93, p.57, 2021

| Project | Type | Energy (TeV, c.m.e.) | N_{det} | \mathcal{L}_{int} (ab^{-1}) | Time (years) | Power (MW) | Cost | Cost/ \mathcal{L}_{int} (BCHF/ ab^{-1}) | \mathcal{L}_{int} /Power (ab^{-1} /TWh) |
|---------------|----------|----------------------|-----------|-----------------------------------|--------------|------------|---------------|--|--|
| ILC | e^+e^- | 0.25 | 1 | 2 | 11 | 129 | 4.8-5.3 BILCU | 2.7 | 0.24 |
| | | 0.5 | 1 | 4 | 10 | 163(204) | 8.0 BILCU | 1.3 | 0.4 |
| | | 1 | 1 | | | 300 | +(n/a) | | |
| CLIC | e^+e^- | 0.38 | 1 | 1 | 8 | 168 | 5.9 BCHF | 5.9 | 0.12 |
| | | 1.5 | 1 | 2.5 | 7 | 370 | + 5.1 BCHF | 3.1 | 0.16 |
| | | 3 | 1 | 5 | 8 | 590 | +7.3 BCHF | 2.0 | 0.18 |
| CEPC | e^+e^- | 0.091&0.16 | 2 | 16+2.6 | 2+1 | 149 | 5 B USD | 0.27 | 7.0 |
| | | 0.24 | 2 | 5.6 | 7 | 266 | +(n/a) | 0.21 | 0.5 |
| FCC-ee | e^+e^- | 0.091&0.16 | 2 | 150+10 | 4+1 | 259 | 10.5 BCHF | 0.065 | 20.5 |
| | | 0.24 | 2 | 5 | 3 | 282 | | 0.064 | 0.9 |
| | | 0.365 & 0.35 | 2 | 1.5+0.2 | 4+1 | 340 | +1.1 BCHF | 0.07 | 0.15 |
| LHeC | ep | 1.2 | 1 | 1 | 12 | (+100) | 1.37* BCHF | 1.37 | 0.14 |
| HE-LHC | pp | 27 | 2 | 20 | 20 | 220 | 7.2 BCHF | 0.36 | 0.75 |
| FCC-hh | pp | 100 | 2 | 30 | 25 | 580 | 17(+7) BCHF | 0.8 | 0.35 |
| FCC-eh | ep | 3.5 | 1 | 2 | 25 | (+100) | 1.75 BCHF | 0.9 | 0.13 |
| Muon Collider | $\mu\mu$ | 14 | 2 | 50 | 15 | 290 | 10.7* BCHF | 0.21 | 1.9 |

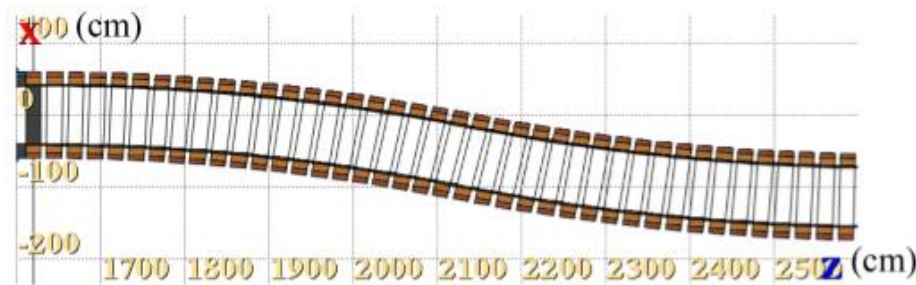
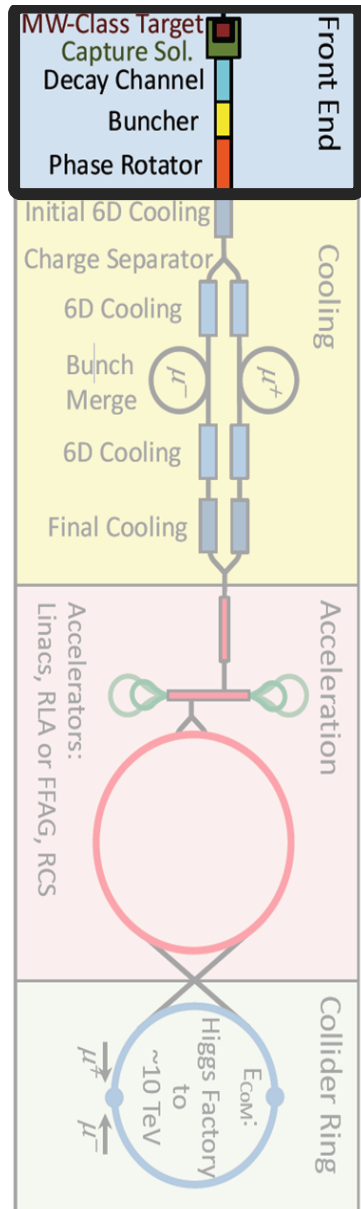
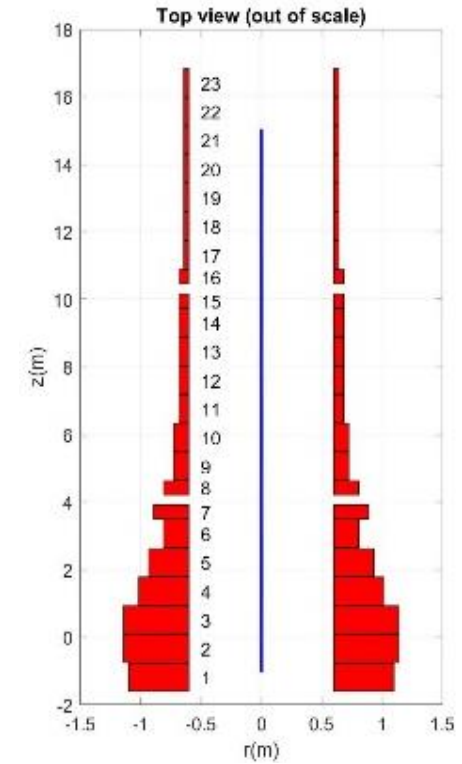


Key Magnet Systems

Target

Back-Up Slide

- 21 T peak field on **HTS cable**
- Double pancake** winding
- Max **shear stress** in tapes $\tau \approx 30$ Mpa
- He coolant** ≈ 20 K, $P \approx 20$ bar
- 3 sections**, ~ 5.5 m long each, 0.48 m gaps
- Detection and dump strategy for **quenches**, hot spot limit ($T_{HS} \approx 150 - 200$ K), detection threshold in range of 10 mV, dump voltages w/in 5 kV,
- Max **field error** 4.2 %
- HTS cable length 9.65 km
- Tensile stress generally below 10 Mpa
- Dominantly affected by hoop stresses and axial compressive stresses from different coils

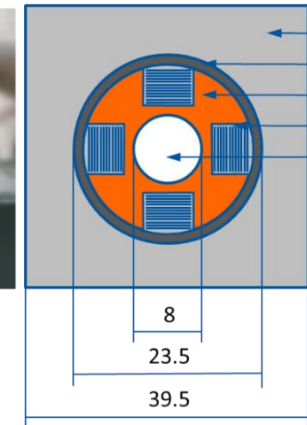


MIT "VIPER" conductor



M. Takayasu et al., IEEE TAS, 21 (2011) 2340
Z. S. Hartwig et al., SUST, 33 (2020) 11LT01

HTS conductor design



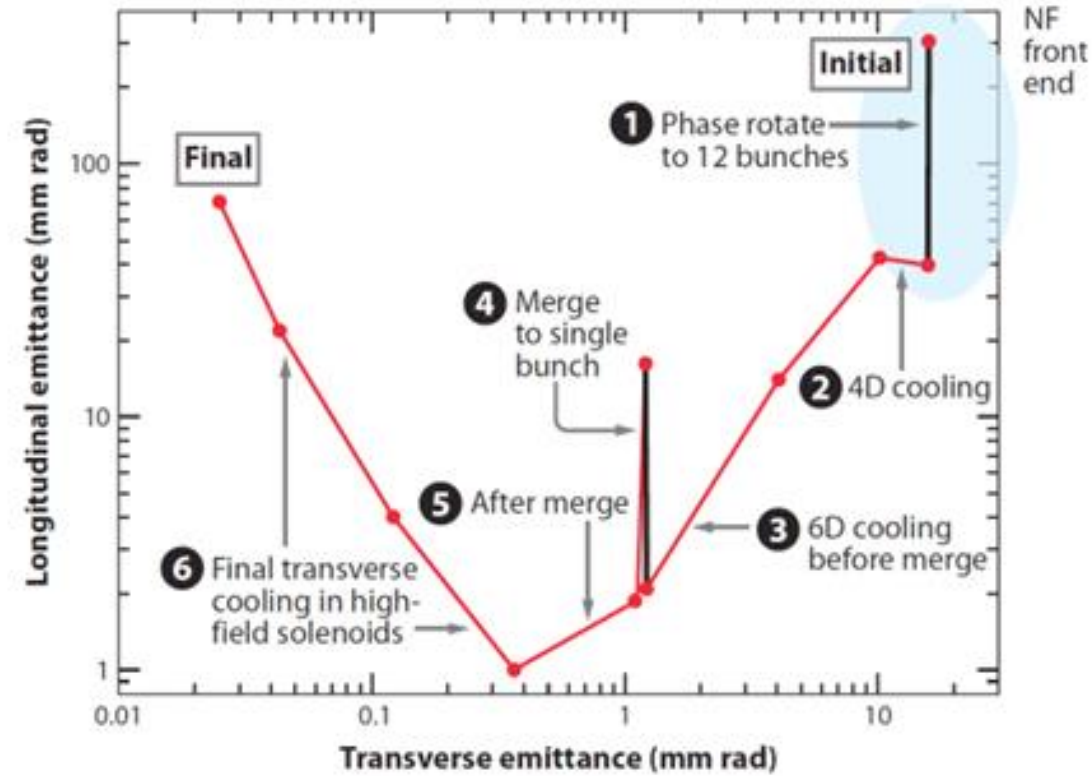
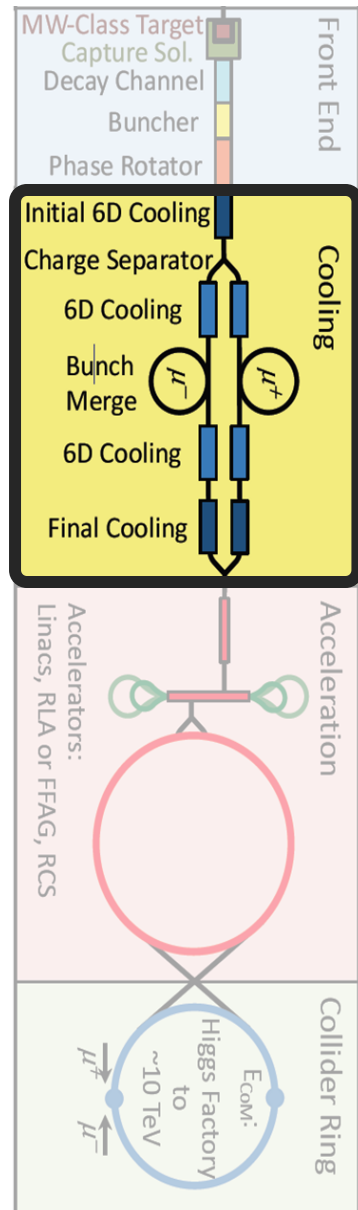
- Operating current: 58 kA
- Operating field: 20 T
- Operating temperature: 20 K
- STAINLESS STEEL JACKET
- STAINLESS STEEL WRAP
- COPPER FORMER
- SOLDERED HTS STACK
- COOLING CHANNEL



Key Magnet Systems

Cooling – 6D

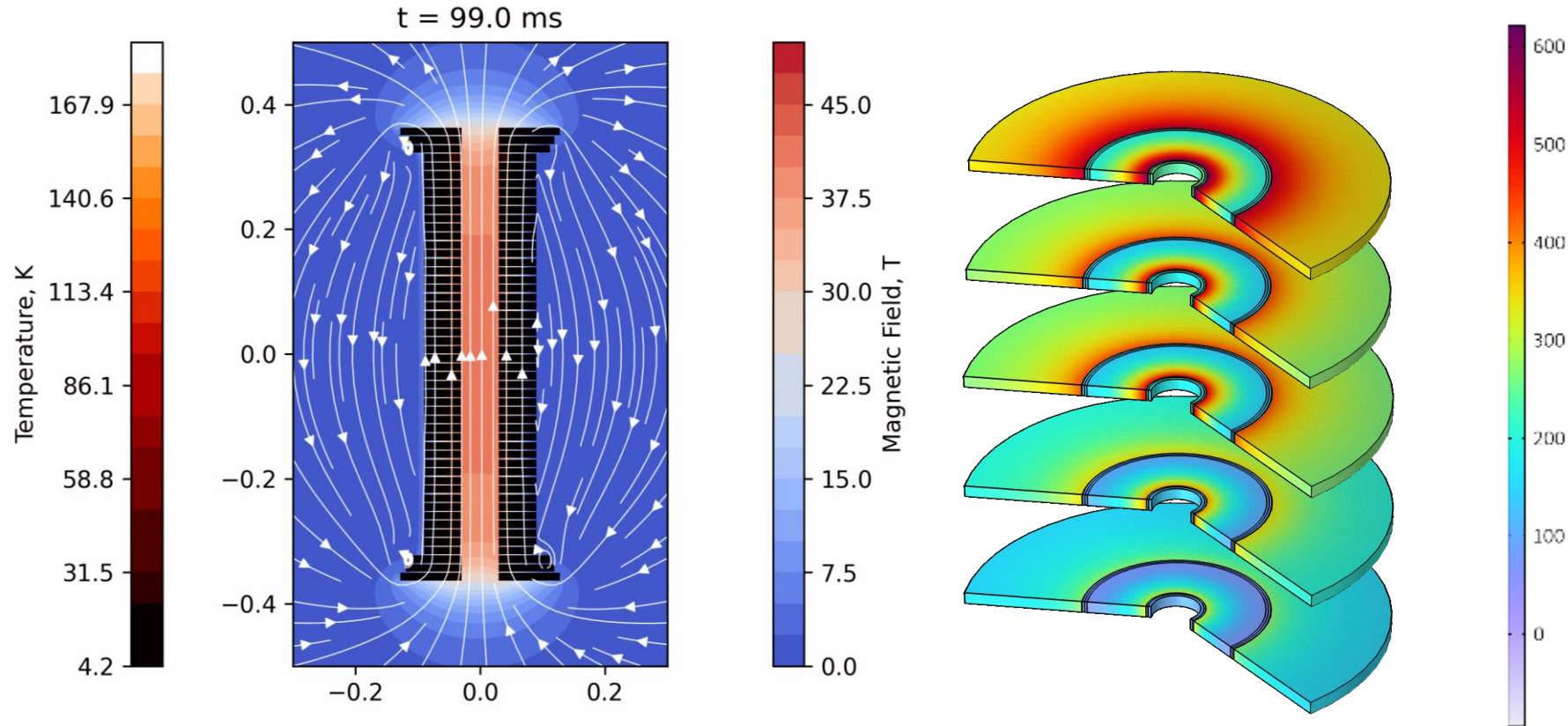
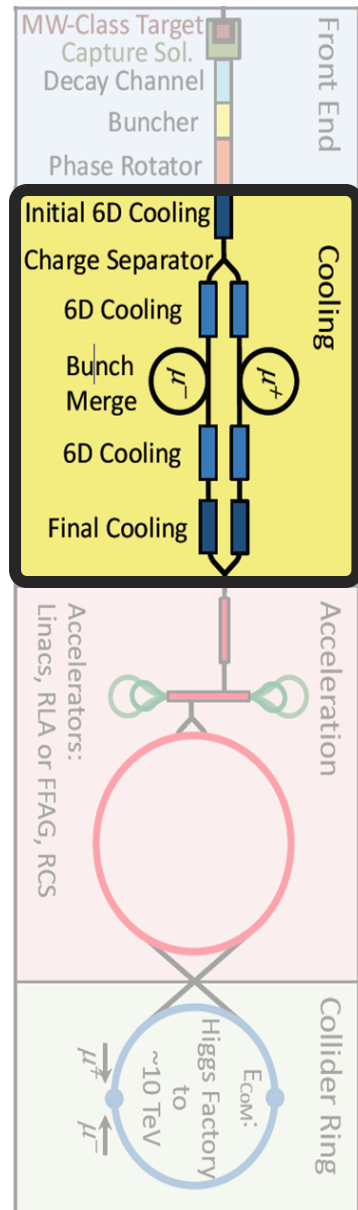
Concept



Key Magnet Systems

Cooling – Final

Design

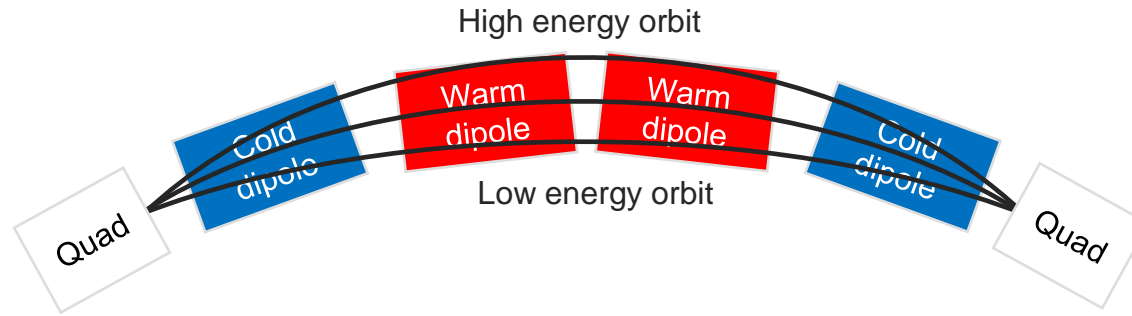
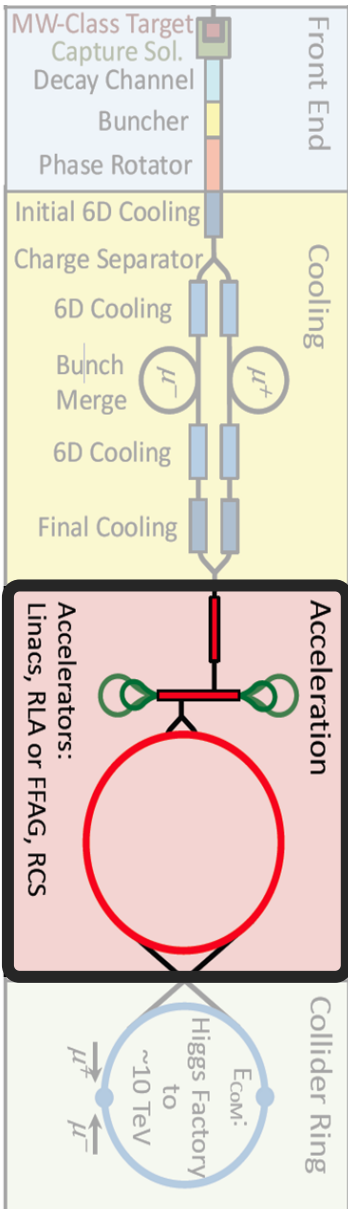


At this magnet scale (i.e. stored energy and size) a **non-insulated winding** seems to be a good option for quench management. Transverse resistance control in a range suitable for operation, balancing protection, mechanics, ramp time and field stability will be crucial (**priority R&D**)

Key Magnet Systems

Acceleration

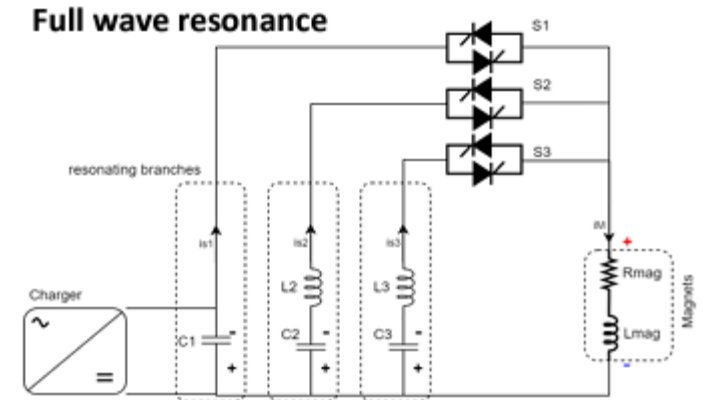
Backup Slide



| Parameter | RCS 1 | RCS 2 | RCS 3 | RCS 4 |
|------------------------------------|-------------|-------------|--------------|--------------|
| Circumference [m] | 5990 | 5990 | 10700 | 27600 |
| Normal-conducting magnet field [T] | 1.8 | 1.8 | 1.8 | 1.8 |
| Super-conducting magnet field [T] | 10 | 10 | 10 | 16 |
| Total transmission N_4/N_0 | | | ≥ 0.65 | |
| Maximum packing factor | 0.66 | 0.66 | 0.66 | 0.7 |
| Ejection energy [GeV] | [250; 450] | [500; 1100] | [1150; 3000] | [3500; 5000] |
| Transmission rate [-] | [0.8; 0.95] | [0.8; 0.95] | [0.8; 0.95] | [0.8; 0.95] |

Table 1: Parameters used for the "RCS 4 in LHC tunnel" optimization.

Different power converter options investigat



Commutated resonance (new)

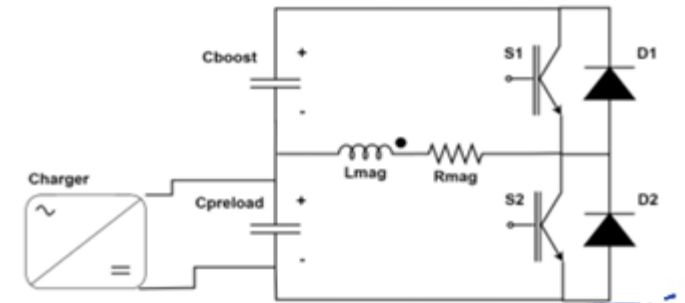


TABLE I. 10 TeV center of mass energy muon collider.

| Parameters | Symbol | Unit | 10TeV com mc |
|---|---------------------------------------|---|--------------|
| Particle energy | E | GeV | 5000 |
| Particle momentum | P_0 | GeV c ⁻¹ | 5000 |
| Luminosity per IP | \mathcal{L} | 10 ³⁴ cm ⁻² s ⁻¹ | 20 |
| Bunch population | N_p | 10 ¹² | 1.8 |
| Transverse normalized rms emittance | $\varepsilon_{nx} = \varepsilon_{ny}$ | μm | 25 |
| Transverse geometric rms emittance | $\varepsilon_{gx} = \varepsilon_{gy}$ | nm | 0.528 |
| Longitudinal emittance ($4\pi \sigma_E \sigma_T$) | ε_l | eVs | 0.314 |
| Longitudinal geometric emittance ($\frac{\varepsilon_l c}{4\pi E_0 \mu}$) | ε_{lg} | mm | 70 |
| Rms bunch length | σ_z | mm | 1.5 |
| Relative rms energy spread | δ | % | 0.1 |
| Beta function at IP | $\beta_x^* = \beta_y^*$ | mm | 1.5 |
| Power per beam with 5 Hz repetition rate | P_{beam} | MW | 7.2 |
| Linear beam-beam tune shift per IP | ξ | | 0.078 |

Key Magnet Systems

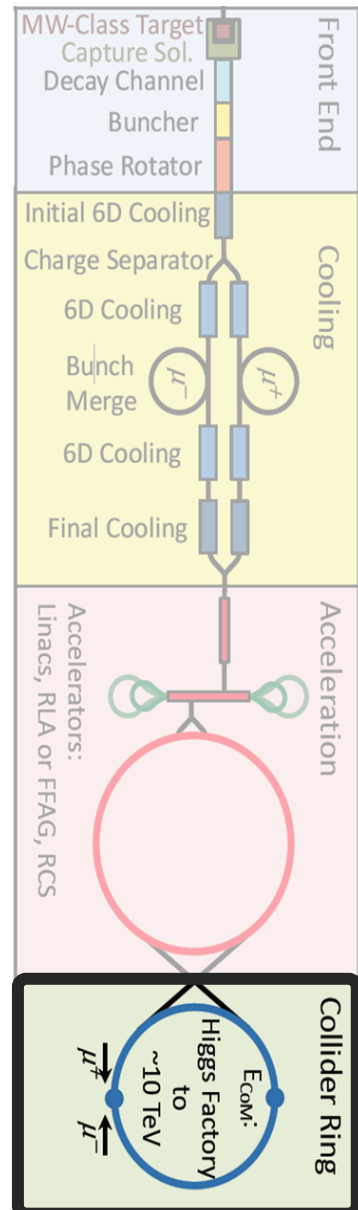
Collision

Analytic design study

Novelli, Daniel, et al. "Analytical evaluation of dipole performance limits for a Muon Collider."

Assumptions in Analytic Evaluations (see table)

- Quench protection system: quench heaters bring entire volume to resistive state; assumed 40 ms delay between initial quench and coils becoming resistive
- Total cost limit of 175 kEUR/m (FCC)
 - Assumed costs: Labour - 20 kEUR/m (LHC)
 - Other materials - 20kEUR/m
 - See table for conductor cost (*aspirational cost assumed future cost reduction factor of ~3)



| | Critical current fit source | Temp. Margins [K] | Stress Limit (MPa) | SC cost [EU/kg] | SC *aspirational cost [EU/kg] | Hot Spot Temperature Limit [K] |
|----------------------------|-----------------------------|-------------------|--------------------|-----------------|-------------------------------|--------------------------------|
| NbTi (1.9 K) | LHC | + 2 | 100 | 330 | | 350 |
| Nb3Sn (4.5 K) | FCC target performance | + 2.5 | 150 | 2000 | 700 | 350 |
| HTS (ReBCO) (4.5 and 20 K) | Fujikura FESC AP | + 2.5 | 300 | 8000 | 2500 | 200 |

Key Magnet Systems

Collision

Analytic design study

Novelli, Daniel, et al. "Analytical evaluation of dipole performance limits for a Muon Collider."

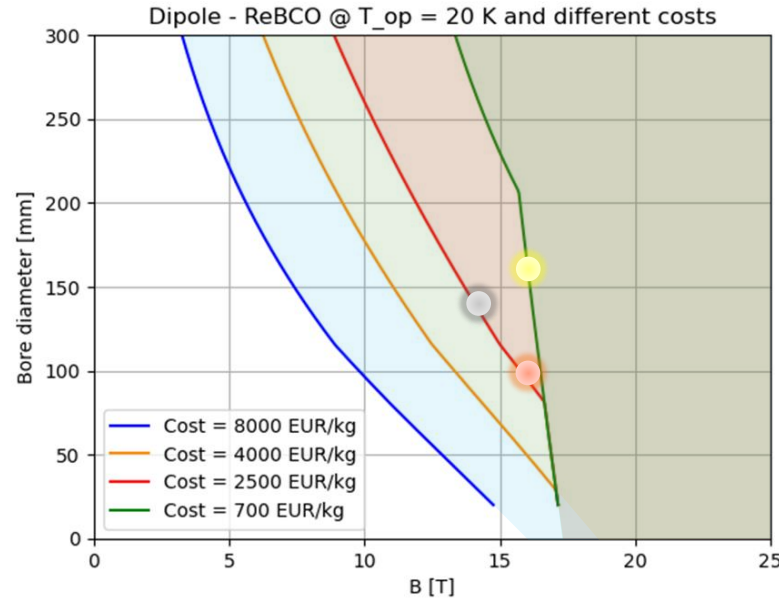
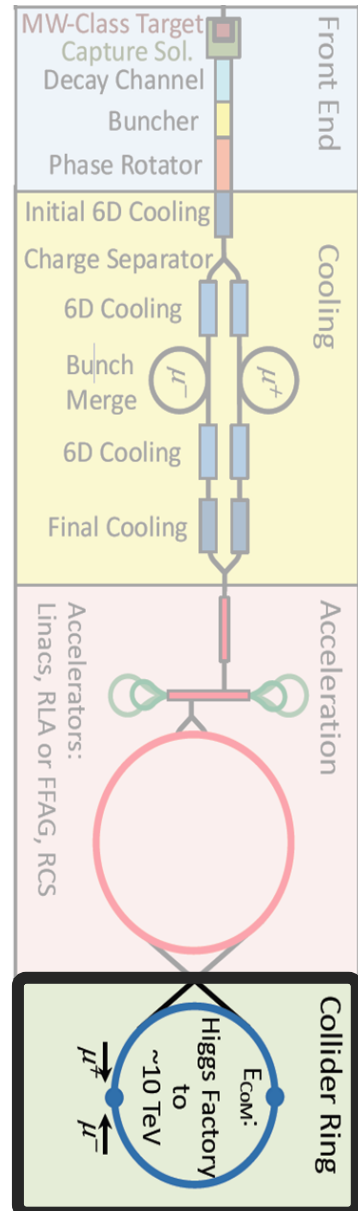


Figure by D. Novelli, INFN-Genoa

- The initial design target (● – 16 T, 158 mm) of the main dipoles.
- Two possible configurations can be 16 T, 100 mm (●) and 14 T, 140 mm (●).

| | 2 cm | 3 cm | 4 cm |
|-------------------------------------|-----------------------------|-----------------------------|-----------------------------|
| Beam aperture (radius) | 23.5 mm | 23.5 mm | 23.5 mm |
| Outer shielding radius | 43.5 mm | 53.5 mm | 63.5 mm |
| Inner coil aperture (radius) | 59 mm | 69 mm | 79 mm |
| Power penetrating tungsten absorber | 19.1 W/m (3.8%) | 8.2 W/m (1.6%) | 4.1 W/m (0.8%) |
| Peak power density in coils | 6.5 mW/cm ³ | 2.1 mW/cm ³ | 0.7 mW/cm ³ |
| Peak dose in Kapton (5/10 years) | 56/112 MGy | 18/36 MGy | 7/14 MGy |
| Peak dose in coils (5/10 years) | 45/90 MGy | 15/30 MGy | 5/10 MGy |
| Peak DPA in coils (5/10 years) | 8/16 × 10 ⁻⁵ DPA | 6/12 × 10 ⁻⁵ DPA | 5/10 × 10 ⁻⁵ DPA |

Power load and damage in arc magnets (10 TeV), as a function of radial tungsten absorber thickness – IMCC Interim Report 2024