



# Conductor and Cable Summary and Comparison of MQXFB07 Witness Sample Results

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# Cable and Coil Overview

Coil	Cable <sup>1</sup>	Cabling Report	HT	Witness Report	Cable NCRs	Strand Contract <sup>2</sup>	Billets
<a href="#"><u>CR138</u></a>	<a href="#"><u>H16OC0410A</u></a>	<a href="#"><u>2772486</u></a>	765	<a href="#"><u>3012883</u></a>		F663/Am4 (22) F663/Am5 (18)	AO08S00295 (6) AO08S00443 (8) AO08S00559 (8) AO08S00592 (7) AO08S00633 (11)
<a href="#"><u>CR145</u></a>	<a href="#"><u>H16OC0454A</u></a>	<a href="#"><u>3058659</u></a>	791	<a href="#"><u>3101766</u></a>		F663/Am4 (21) F663/Am5 (19)	AO08S00470 (11) AO08S00565 (10) AO08S00627 (10) AO08S00630 (9)
<a href="#"><u>CR146</u></a>	<a href="#"><u>H16OC0417A</u></a>	<a href="#"><u>2822508</u></a>	802	<a href="#"><u>3132280</u></a>		F663/Am3 (11) F663/Am4 (10) F663/Am5 (19)	AO08S00222 (11) AO08S00477 (10) AO08S00635 (9) AO08S00640 (10)
<a href="#"><u>CR147</u></a>	<a href="#"><u>H16OC0452A</u></a>	<a href="#"><u>2963109</u></a>	814	<a href="#"><u>3132282</u></a>	<a href="#"><u>2957863</u></a>	F663/Am4 (16) F663/Am5 (24)	AO08S00296 (9) AO08S00568 (7) AO08S00621 (8) AO08S00622 (9) AO08S00636 (7)

<sup>1</sup> MQXF cable specification, [EDMS 1863790](#)

<sup>2</sup> MQXF wire specification, LHC-MQXF-CI-0001, [EDMS 1419924](#)

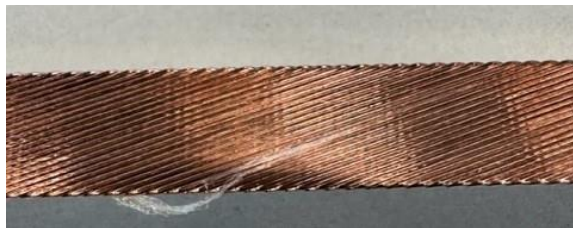
# Nonconformities

- NCRs affecting the cable are summarised below and in the following slides
- Witness samples (coil heat treatments)
  - Any damage to witness sample test pieces did not impact testing for the present coils
  - For CR138, one extremity of the furnace reached 675 °C, resulting in reduced RRR on CoC
  - No indication of a significant performance impact from minor coil HT NCRs

Coil	HT	Cable NCRs	Coil NCRs Implicating Cable	Coil HT NCRs
<a href="#">CR138</a>	765		<a href="#">2974448</a>	<a href="#">2961736</a>
<a href="#">CR145</a>	791			<a href="#">3073728</a> , <a href="#">2884016</a>
<a href="#">CR146</a>	802		<a href="#">3083049</a>	<a href="#">3088822</a>
<a href="#">CR147</a>	814	<a href="#">2957863</a>		<a href="#">3101915</a> , <a href="#">2884016</a>

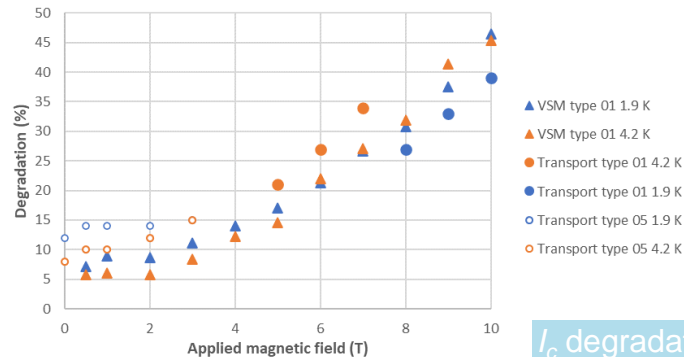
# NCR: Plastic Entrapped in Cabling

- During production of cable **H16OC0452A** for **CR147**, the inspection system identified fragments of material at positions 686, 746 and 755 m:
  - Identified as polyethylene film (23  $\mu\text{m}$  thick) used to wrap wire spools
  - Similar film applied by the manufacturer is removed for inspection and sampling, and replaced by CERN for storage
- The cable was thoroughly inspected and all plastic removed
- All standard tests were performed, and the cable geometry and extracted strand  $I_c$  and RRR were in specification: no impact on this cable expected
- Respooling procedures were revised to prevent recurrence:
  - Reduced speed and tension for removing plastic wrap
  - Heightened vigilance during unwrapping and respooling, with inspection by a second operator
- A blue coloured wrap will be used when wrapping future stock for storage, to increase visibility of any fragments



# NCR: Overheating During Impregnation

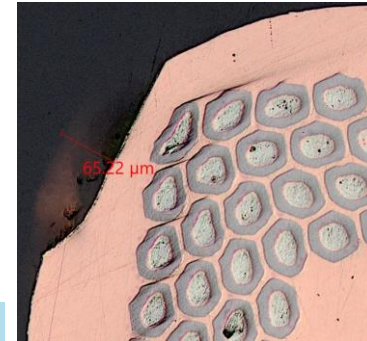
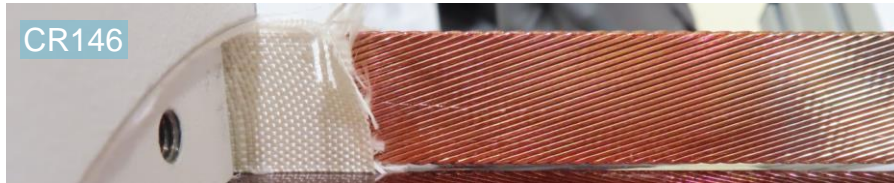
- During impregnation of reacted coil **CR138**, thermocouples were not connected and an uncontrolled temperature increase potentially up to 300 °C for 24 h occurred
- Transport  $I_c$  and VSM tests (see [EDMS 3007813](#)) following application of a simulated heat treatment to reacted samples suggested negligible impact on both Nb-Ti and Nb<sub>3</sub>Sn performance
  - For Nb-Ti leads,  $I_c$  degradation increases with applied field, but is modest (~10 %) in operating conditions, and RRR increases
  - For Nb<sub>3</sub>Sn, VSM data suggest no degradation of  $I_c$



$I_c$  degradation of Nb-Ti samples

# NCR: Cable Mechanical Damage

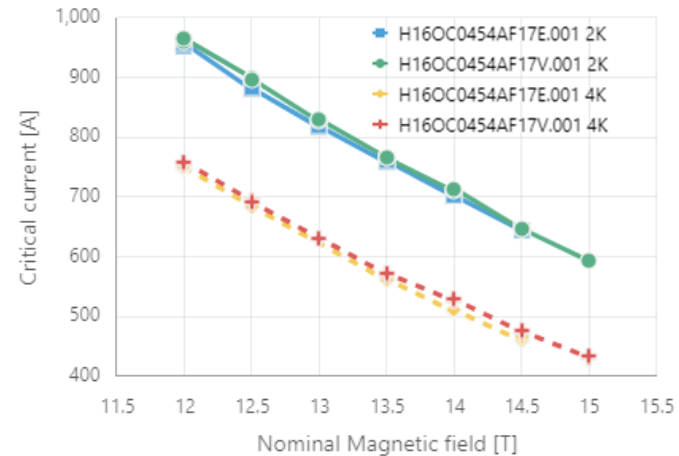
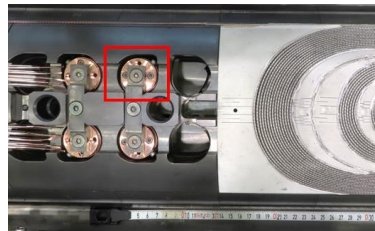
- For **CR146**, the cable of the inner connection was lightly scratched with tooling during the removal of cable insulation
- The scratch does not appear to penetrate beyond the copper, with estimated depth 22  $\mu\text{m}$
- Not specifically evaluated at cable level, but a study is ongoing to simulate the effects of mechanical damage following a more severe case for coil CR141 (MQXFB06)
  - Initial findings showed no degradation of RRR even for severe simulated defects:
    - ~60  $\mu\text{m}$  depth, applied compressively by a straight edge or rolling (indenting) with a 60  $\mu\text{m}$  wire
  - $I_c$  samples recently reacted: due for measurement in ~2 weeks



More severe simulated defect not causing RRR degradation

# Witness Sample Damage

- Recap from MQXFB06:
  - For CR141, two virgin witness samples were found to be damaged after heat treatment
  - Modifications were made to the mica sheet in the mould assembly for CR144 onwards
- For **CR145**, an extracted witness sample from strand 17 appeared to be damaged
  - Not the same form as previous defects, and no apparent contact with mica sheet
- On testing, no degradation of  $I_c$  was found
  - No indication that further changes to reaction tooling are required

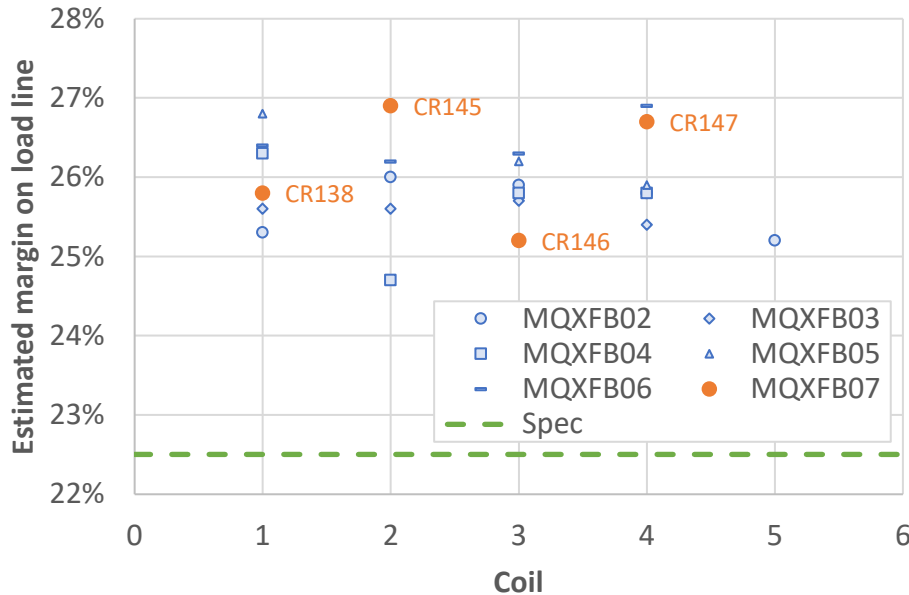


# Testing Anomalies

- For CR138, extracted sample WE13 was degraded, probably due to sample damage
  - Excluded from analysis
  - No correlation with furnace position, so not caused by heat treatment anomalies
- For CR146, the 60 cm voltage taps were not measurable for extracted strand WE15. Results for this sample were not included in the analysis
  - Values measured on the 90 cm voltage taps are consistent with the general behaviour and intermediate between other samples, so any effect on coil evaluation is negligible
- For CR145 and CR147, **cable qualification** samples were re-measured because of a concern with magnetic field calibration of a test station at the time of the original measurement
  - The cabling report was issued using only the **second** measurement to calculate cabling degradation
  - The witness reports plot results from the **first** measurement, but degradation values were confirmed with the **second** measurement
  - The heat treatment evaluation is not affected, as this is on the basis of virgin verification samples
  - The cause of the unexpected magnetic field behaviour has been identified and repaired

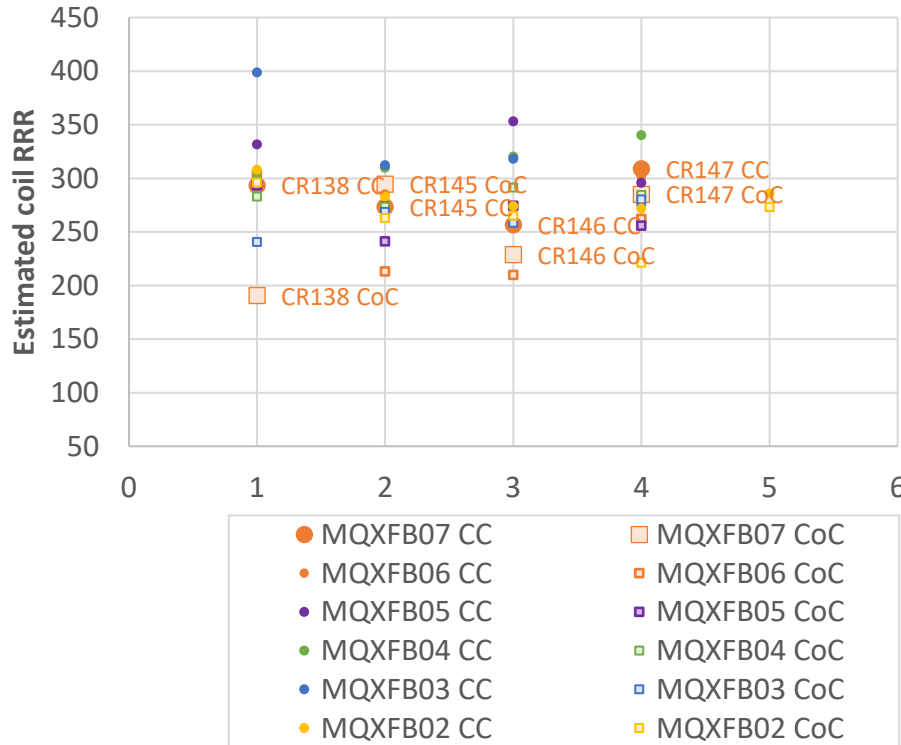


# Load Line Margin



- Large margin on load line of  $\sim 26.2\%$
- Consistent in mean and spread with recent coils

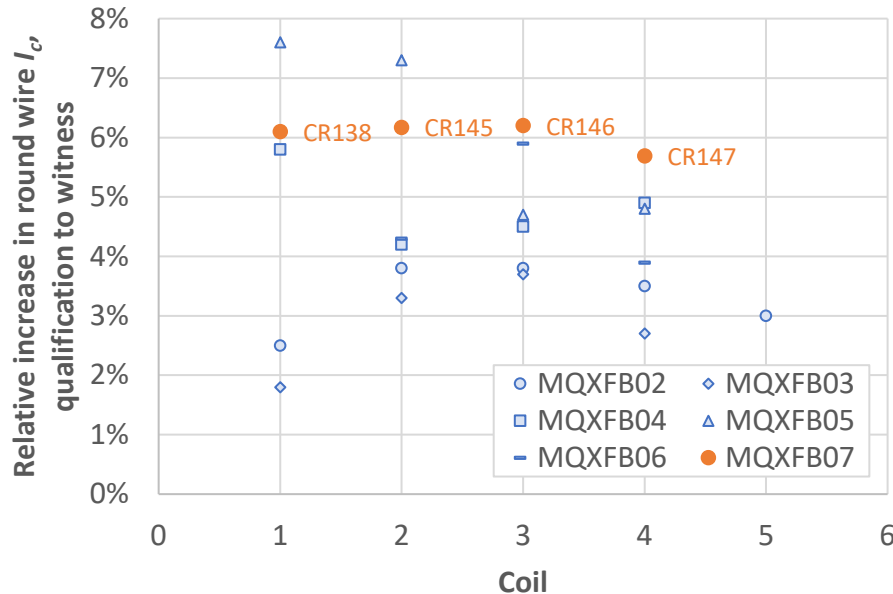
# Estimated Coil RRR



- Large RRR margin
- Connection side (CC) generally has higher RRR
- Low RRR of CR138 CoC due to HT NCR, but still well above specification limit
- All other values within the range of other recent coils

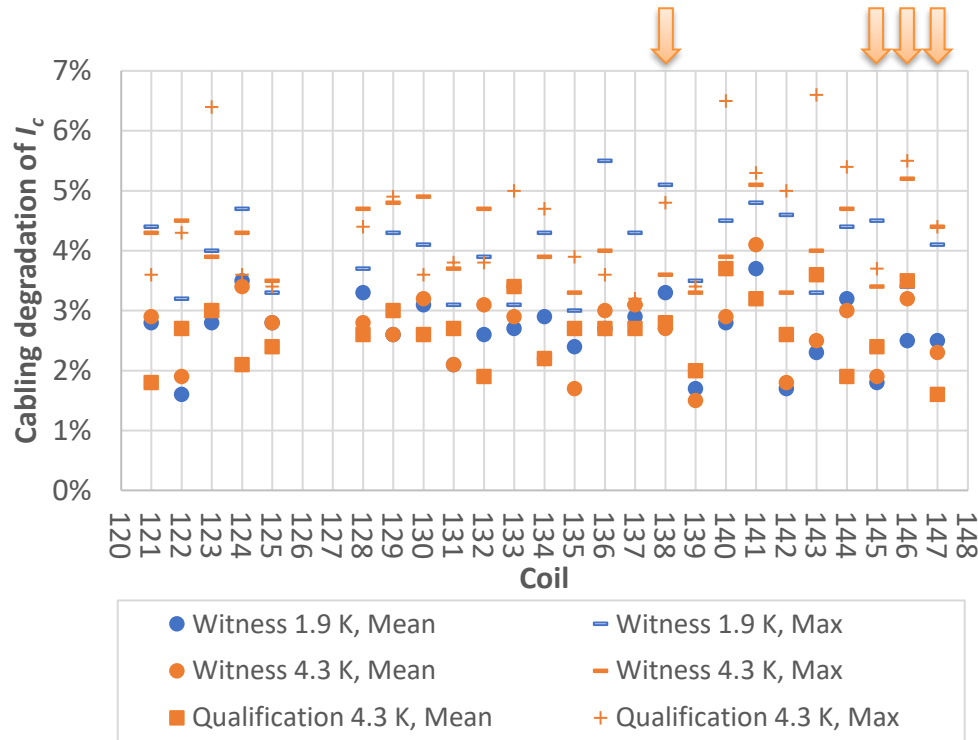
# Effect of HT/Furnace on Round Wire $I_c$

- $I_c$  of virgin **witness** samples (building 180) –  $I_c$  of virgin **qualification** samples (building 163)



- $I_c$  consistently slightly higher for witness samples (HT in building 180) than qualification samples (HT in building 163)
- Very consistent for recent coils (despite HT NCRs)

# Cabling Degradation of $I_c$



- Cabling degradation of  $I_c$  is within the 5 % specification for all coils
- Consistent and conforming degradation as assessed from witness samples across all recent production, both at 1.9 K and 4.3 K
- Mean cabling degradation ~3 %

# Summary

- Cable data in specification for all coils
- Good consistency between recent coils, and data in a comparable range to MQXFB02-06
- Systematic differences remain between small (building 163) and large (building 180) HT furnaces, and in RRR between CC and CoC



***Thank you for your attention!***