

# Acoustic Calibration for the KM3NeT Pre-Production Module

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## Abstract

The proposed large scale Cherenkov neutrino telescope KM3NeT will carry photo-sensors on flexible structures, the detection units. The Mediterranean Sea, where KM3NeT will be installed, constitutes a highly dynamic environment in which the detection units are constantly in motion. Thus it is necessary to monitor the exact sensor positions continuously to achieve the desired resolution for the neutrino telescope. A common way to perform this monitoring is the use of acoustic emitters and receivers based on the piezoelectric effect. The acoustic receivers are attached to detection units whereas the emitters are located at fixed positions on the sea floor. There are complete commercial systems for this application with sufficient precision. But these systems are limited in the use of their data as they were designed to perform only this single task. Several working groups in the KM3NeT consortium are cooperating to custom-design a positioning system for the specific requirements of KM3NeT. This leads to extended capabilities of already existing sensor types as well as to some new developments like small piezoelectric elements equipped with preamplifiers inside the same housing as the optical sensors. Most of the studied solutions hold the possibility to extend the application area from positioning to additional tasks like acoustic particle detection or monitoring of the deep-sea acoustic environment. The KM3NeT Pre-Production Module (PPM) is a test system to verify

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the correct operation and interoperability of the major involved hardware and software components developed for KM3NeT. In the context of the PPM, alternative designs of acoustic sensors will be tested. These will be described in this article.

*Keywords:* Acoustic sensors, Calibration, KM3NeT, Neutrino detection

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## 1. Introduction

KM3NeT[1] is a planned large scale neutrino telescope which will be located in the deep-sea environment of the Mediterranean. It will consist of flexible structures, the detection units (DU), anchored to the sea bed to instrument a water volume exceeding  $1 \text{ km}^3$ . This size is necessary to detect high energy neutrinos as the expected flux of these particles strongly decreases with their energy. KM3NeT is designed as a deep-sea water Cherenkov neutrino telescope following the predecessor experiments ANTARES<sup>1</sup>[2], NEMO<sup>2</sup>[3] and NESTOR<sup>3</sup>[4]. The experience gained in these projects benefit all activities related to KM3NeT. Particle detection based on the Cherenkov effect, i.e. the light emission of charged particles travelling faster than the light group velocity in its surrounding dielectric medium, requires sensitive optical sensors with inter sensor spacings of the order of 100 m corresponding to the absorption length of the relevant light wavelength. Neutrinos, being neutral particles, do not emit Cherenkov radiation so their detection is based on the detection of a muon generated in a neutrino interaction. The arrival times of light signals “seen” by the optical sensors can be used to reconstruct the particle track assuming a correct attribution of the muon to a high energy neutrino. The relative arrival time of a photon at the photo-sensor can be reconstructed with a precision of the order of 1 ns, see e.g. [5]. It is thus mandatory for this track reconstruction to know the exact position of the optical sensor to a precision of about 20 cm (the

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<sup>1</sup>Astronomy with a Neutrino Telescope and Abyss environmental RESearch

<sup>2</sup>NEutrino Mediterranean Observatory

<sup>3</sup>Neutrino Extended Submarine Telescope with Oceanographic Research

22 refractive index is about 1.33 in sea water). The detection units are exposed to  
23 a highly dynamic deep-sea environment with sea currents varying both in ve-  
24 locity and direction and thus the detection units are constantly changing their  
25 positions/orientations compared to the undeflected equilibrium position. This  
26 necessitates a continuous monitoring of the exact sensor positions. The monitor-  
27 ing with the help of electromagnetic waves is impractical due to the large signal  
28 absorption and attenuation in sea water which implies a huge amount of mon-  
29 itoring devices to cover several  $\text{km}^3$  volume. Instead acoustic waves constitute  
30 a well established way to perform the position calibration of the detector. The  
31 attenuation length of sound waves in sea water is of the order of 1 km (frequency  
32 dependent) what makes it possible to receive the signals from an emitter at the  
33 sea floor at the top of a DU. The viability of acoustic calibration strongly de-  
34 pends on the feasibility to emit well defined signals and to detect these pressure  
35 differences (sound waves) besides a high ambient pressure of about  $10^7$  Pa per  
36 1000 m water depth. In addition the calibration signals should be long ranged  
37 to allow for enhanced sensor spacings but with sufficient protection for the bio-  
38 sphere, e.g. lowest possible signal amplitudes. A set of dedicated emitters and  
39 receivers are necessary for this method. The emitters will be located at fixed  
40 positions on the sea floor to ensure a known position over the whole operation  
41 period of the detector. The anchors of the detection units are well suited po-  
42 sitions for emitters as there will be no need for additional infrastructures to  
43 power and control these devices. The exact position of the emitters has to be  
44 determined only once, e.g. from a ship above the detector. The receivers of  
45 the acoustic signals will be attached to the detection units to determine their  
46 positions relative to the different emitters. This is done by triangulation of the  
47 different signal arrival times at the detection units with respect to the known  
48 emitter positions and emission times. It is not necessary to equip each opti-  
49 cal sensor with an acoustic receiver as it is possible to interpolate the sensor  
50 positions between two distant acoustic receivers using a model of the shape of  
51 the DU. It is possible to use either complete commercial systems or to combine  
52 different emitters and receivers to a dedicated system. These systems offer more

53 flexibility concerning signal amplitudes, frequencies and signal shapes whereas  
54 commercial ones are characterised by a sophisticated and reliable design. The  
55 use of a dedicated system is preferred as it allows for more diverse applications  
56 and studies. The devices used for this kind of applications, both for emission  
57 and reception, are mostly based on the piezoelectric effect. These devices are  
58 capable of withstanding the high ambient pressure of the deep sea while still  
59 offering a simple and reliable design without mechanical parts. The long term  
60 stability of piezoelectric ceramics, hereafter called piezos, ensures the operabil-  
61 ity of the acoustic calibration system over the whole lifetime of the detector.  
62 In this article a short overview is given of different possible types of piezos to  
63 be used for acoustic calibration as well as a more detailed description of a new  
64 development in this field at ECAP<sup>4</sup>[6]. Some of these devices will be tested  
65 on the Pre-Production Module (PPM) of KM3NeT in order to find the best  
66 solution to monitor the positions of the detection units.

## 67 **2. Sensor types**

68 All sensors to come into consideration comprise a piezo and are thus based  
69 on the piezoelectric effect. If such a piezoelectric crystal is exposed to external  
70 pressure/force variations, it accumulates electrical charge on its surfaces (de-  
71 pending on the polarisation of the crystal and the direction of the variation).  
72 The resulting difference in potential between those surfaces can be measured  
73 as a voltage signal. This voltage signal is proportional to the applied force.  
74 The voltage signal resulting from the deformation is very small and has to be  
75 amplified prior to its analysis. This effect is reversible and in this way a piezo  
76 can be used as acoustic emitter as well if it is exposed to an external electrical  
77 field. A sufficiently large high voltage signal has to be applied to the emitter to  
78 generate a useful signal amplitude in this case. The sensitivity and directivity  
79 of the piezo strongly depends on the used material as well as on its geometry

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Figure 1: A short description of these three sensor types is given in the text.

80 and polarisation. There is a variety of ultrasonic devices designed especially for  
 81 acoustic calibration as well as for other different applications.

82 Figure 1 shows an exemplary set of acoustic sensors. The first one on the left  
 83 side is a hydrophone from High Tech, Inc.[7] as used in the AMADEUS<sup>5</sup> test  
 84 setup[8]. These hydrophones comprise a hollow piezo cylinder and a preampli-  
 85 fier moulded together in polyurethane. They are almost equally sensitive over a  
 86 frequency range from 10 kHz to 50 kHz. This is the frequency range of interest  
 87 for acoustic neutrino detection. These hydrophones are used for investigations  
 88 of acoustic particle detection, positioning (and marine science). The acous-  
 89 tic sensor in the middle, c.f. Figure 1, is a “Free Flooded Ring” (FFR) from  
 90 SensorTech[9]. This transceiver can be used either as emitter or as receiver as it  
 91 is not equipped with a preamplifier. This sensor type is studied at IGIC-UPV<sup>6</sup>.  
 92 It is planned to use this devices as emitters for the KM3NeT acoustic position-  
 93 ing system. Its use as receiver is also under investigation. In the latter case the  
 94 FFRs are equipped with a preamplifier to detect small pressure variations. The  
 95 third sensor type seen in Figure 1 is a hydrophone from SMID[10] equipped with  
 96 a preamplifier. This hydrophone was developed in cooperation with INFN<sup>7</sup> and  
 97 is designed to work in the frequency range from 10 Hz to 70 kHz. These sensors

<sup>5</sup>ANTARES Modules for Acoustic DETection Under the Sea

<sup>6</sup>IGIC-Universitat Politècnica de València

<sup>7</sup>Istituto Nazionale di Fisica Nucleare

98 are used in the NEMO Phase II framework and are also under consideration for  
99 the use in KM3NeT. The above mentioned devices constitute examples for a  
100 variety of different devices available for calibration purposes and other deep-sea  
101 applications. The acoustic monitoring of the deep sea environment or long-run  
102 monitoring of the sea in general is a multidisciplinary task which also can be  
103 adressed with these types of sensors. Almost all of these devices and their elec-  
104 tronics are moulded into a single housing, e.g. in polyurethane, to protect them  
105 from the sea water, the high ambient pressure and other environmental influ-  
106 ences. Polyurethane is a frequently-used material for underwater acoustics as  
107 its acoustic impedance can be matched with the one of the surrounding water.  
108 This ensures the best performance for emission and reception while still protect-  
109 ing the device. Another possibility to protect the acoustic receiver is presented  
110 in the next section.

### 111 **3. Opto-Acoustical Modules (OAMs)**

112 The so-called Acoustic Modules (AMs) deployed in the AMADEUS test  
113 setup represent a different approach to the aforementioned moulding of acoustic  
114 sensors. These modules consist of two bare piezos glued to the inside of pressure  
115 resistant glass spheres, identical to those used for optical modules. Each piezo  
116 is connected to a preamplifier which is located inside a copper tube together  
117 with the piezo to shield the resulting sensor from electromagnetic influences.  
118 The major difference compared to the use of dedicated receivers is the possi-  
119 ble combination of acoustic sensor and optical sensor inside the same housing.  
120 The resulting Opto-Acoustical Module (OAM) would combine all features of a  
121 standard optical module, the key building blocks of the detection units, with  
122 the ability to determine its position with respect to a set of dedicated emitters  
123 without the need for additional calibration devices. This reduces the required  
124 underwater connectors and feedthrough to a minimum as one connection is suf-  
125 ficient to connect the OAM. Underwater connectors and feedthrough always  
126 constitute potential points of failure with water ingress in the worst case. There

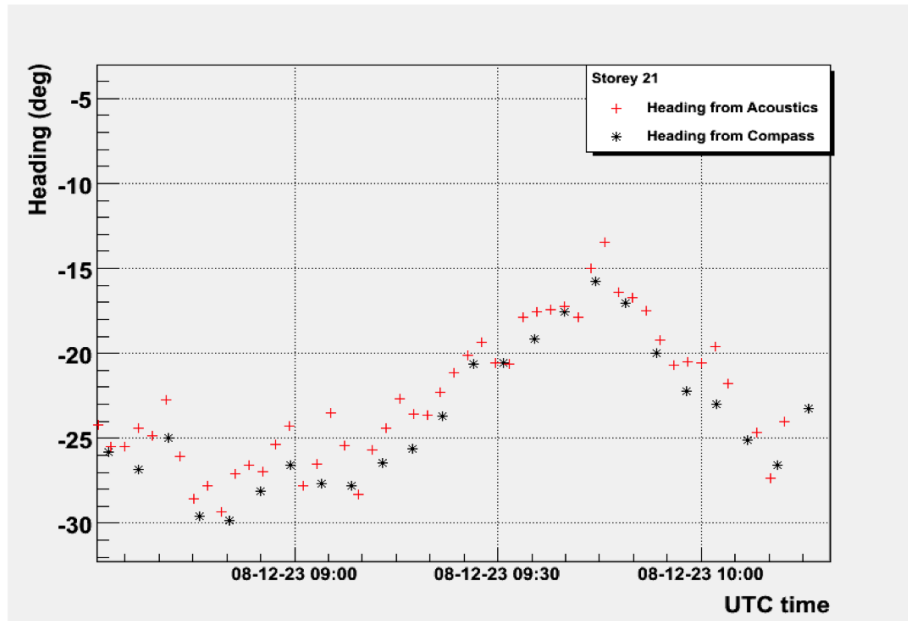


Figure 2: The graph depicts heading measurements carried out for an ANTARES storey holding AMs. The data obtained from a dedicated compass board are in good agreement to the heading reconstructed with the AM data.

127 is no need to further protect the acoustic sensor against environmental influ-  
 128 ences as it is perfectly protected by the glass sphere. The results obtained with  
 129 the AMs prove the principal concept to operate this type of acoustic sensor. A  
 130 result comparing exemplary the reconstructed heading of the storey compris-  
 131 ing AMs with the one obtained through dedicated compass devices is shown in  
 132 Figure 2.

133 The results prove the possibility to determine the position of the AMs to a  
 134 sufficient precision. A study of the angle dependence of a piezo glued to a glass  
 135 sphere can be found in [11]. The biggest obstacle is expected from the high  
 136 voltage necessary to operate a photomultiplier inside the module. The high  
 137 voltage itself or its transformation from a lower supply voltage might lead to a  
 138 “noisy” environment interfering with the signal path of the acoustic device. On  
 139 the other hand the acoustic device with its amplifiers might influence the PMT

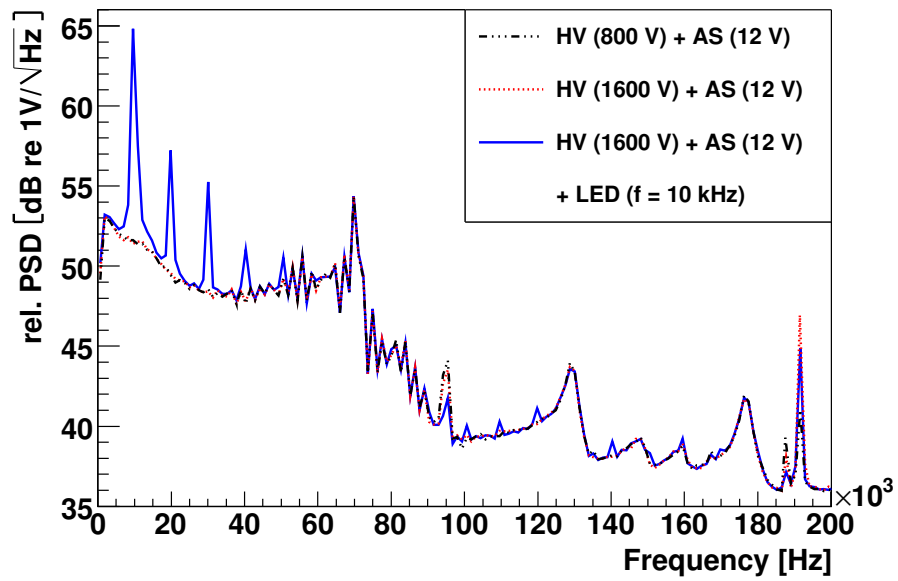


Figure 3: The figure shows the results of noise measurements for a first OAM prototype and different settings given in the legend. This test in a simplified setup shows some prominent features. These can be attributed to the poor shielding of the acoustic sensor as well as to the power supply. “HV” shows the high voltage between cathode and anode of the PMT. “AS” stands for the acoustic sensor which was powered by 12 V and “LED” gives the frequency of a flashing LED inside the test setup.



140 operation. The latter case is unlikely and was not observed so far due to the  
141 low voltage ( $\sim 3.3\text{ V}$  to  $5.0\text{ V}$ ) necessary to power the acoustic sensor but any  
142 parasitic influence has to be eliminated.

143 First tests as shown in Figure 3 demonstrated that PMTs and piezos can  
144 be operated within a single sphere. Some interference of the PMT operation  
145 with the piezo was observed, however this can be attributed to the very poor  
146 electromagnetic shielding of the first prototypes (no electromagnetic shielding  
147 was applied) and the pulsed LED (connected to the same power supply as both  
148 sensors). Some tests in cooperation with LNS-INFN<sup>8</sup>[12] were carried out to  
149 test the combined operation under more realistic conditions. In this context  
150 the NEMO Phase II infrastructure was used together with a new prototype  
151 of a piezo-preamp unit with better shielding and a different amplifier layout  
152 adapted to the operation conditions. In this configuration no drawbacks were  
153 visible during laboratory tests with the piezo mounted in the same 13'' sphere  
154 as the PMT next to a PMT powered almost at its nominal voltage with a dark  
155 count rate of several kHz. The small size of the acoustic sensor enables its  
156 integration into a variety of different optical module designs. See Figure 4 for  
157 the two designs currently pursued. The first one is the single PMT option used  
158 in the NEMO Phase II framework and the second one is a multi PMT (31 PMTs  
159 per module) option developed at Nikhef<sup>9</sup>[13] in Amsterdam and will be used for  
160 the PPM.

#### 161 4. Conclusions

162 The acoustic calibration is a way to determine the position and the orienta-  
163 tion of detecton units. The choice of the appropriate acoustic devices for this  
164 task strongly depends on the intended multiple uses as the positioning with  
165 the required precision can be realised with each of the presented devices. The  
166 KM3NeT Pre-Production Module provides the necessary infrastructure to test

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<sup>8</sup>Laboratori Nazionali del Sud - Istituto Nazionale di Fisica Nucleare

<sup>9</sup>Nationaal instituut voor subatomaire fysica

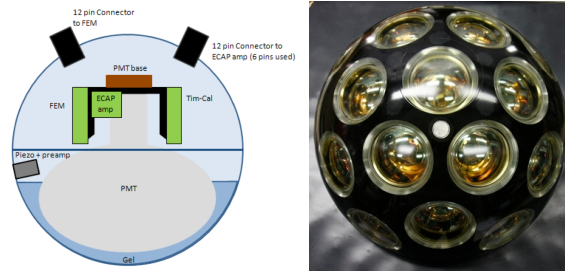


Figure 4: The figure on the left shows a schematic of a single PMT optical module equipped with an acoustic sensor to be used in NEMO Phase II. The picture on the right shows the exterior of a prototype multi PMT detection unit. The PMTs are clearly visible as well as a small circle, the metallised piezo surface.

167 different types of sensing devices to validate the positioning results and to figure  
 168 out potential incompatibilities in the final system. The various components are  
 169 developed at different KM3NeT member institutes all over Europe. The joint  
 170 tests in the different laboratory yielded a perfect compatibility of the differ-  
 171 ent sensor components. The final confirmation requires the fully-fledged PPM  
 172 evaluated under real conditions. The multidisciplinary research adressed with  
 173 general purpose devices becomes more and more important as the complexity  
 174 and efforts to maintain large scale detectors increase and have to be partitioned  
 175 among several institution not only from a single scientific subject. KM3NeT  
 176 could serve as an observatory where many natural sciences collaborate to better  
 177 understand our planet with its deep sea environment as well as our universe as  
 178 a whole.

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