



FUTURE
CIRCULAR
COLLIDER

ABT: Hardware design for beam transfer equipment and related challenges

G. Favia on behalf of SY-ABT
CERN, Geneva, Switzerland

Outline

- Baseline design for kickers and septa
- Challenges and main design criteria
- R&D and prototyping
- Conclusion

Outline

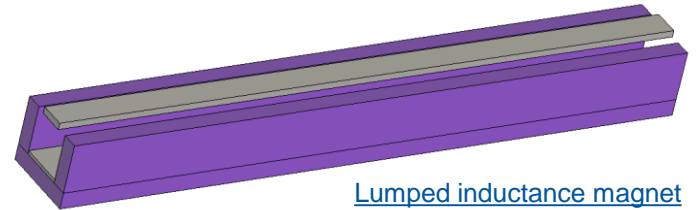
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Kickers

| | Damping ring | Booster injection | Booster extraction | Booster Dump | Collider injection | Collider dump |
|--|-----------------|-------------------|--------------------|---------------------|--------------------|---------------------|
| Magnet topology | Stripline | Stripline | Lumped inductance | Lumped inductance | Lumped inductance | Lumped inductance |
| Generator topology | Inductive adder | Inductive adder | Marx generator | LBDS-like generator | PFN/Marx generator | LBDS-like generator |
| Magnet under vacuum | Yes | Yes | No | No | No | No |
| Elements / Systems | 2/4 | 1/2 | 10/2 | 6/2 | 4/2 | 6/2 |
| Physical length [m] | 3 | 1.5? | 12 | 12 | 4 | 12 |
| Novel technology | Yes | Yes | No | No | No | No |
| R&D required/ Prototyping required/ Conventional technology | R&D required | R&D required | R&D required | Prototype required | R&D required | Prototype required |



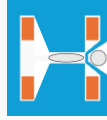

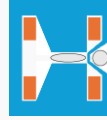
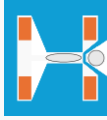
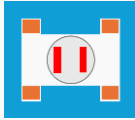


Stripline magnet



Lumped inductance magnet

Septa

| | Booster injection | Booster extraction | Booster Dump | Collider injection | Collider dump | Separator septum | E-M separator |
|---|---|---|---|---|---|---|---|
| Diagram |  |  |  |  |  |  |  |
| Magnet topology | Under vacuum Lambertson | Outside vacuum Direct Drive | Low Power outside vacuum | Under vacuum Direct Drive | Low Power outside vacuum | Low Power outside vacuum | |
| Operation | DC | Pulsed | DC (ramped) | Pulsed | DC | DC | |
| Magnet under vacuum | partially | no | no | yes | no | no | partially |
| Elements / Systems | 2/2 | 1/2 | 3/2 | 6/2 | 2/2 | 10/2 | 10/2 |
| Physical length [m] | 6 | 3 | 5.4 | 7.2 | 4 | 25 | |
| Novel technology | Yes | No | Yes | No | Yes | No | yes |
| R&D required / Prototyping needed / conventional technology | Prototype required | Conventional technology | Prototype required | R&D required | Prototype required | Prototype required | R&D urgently required |

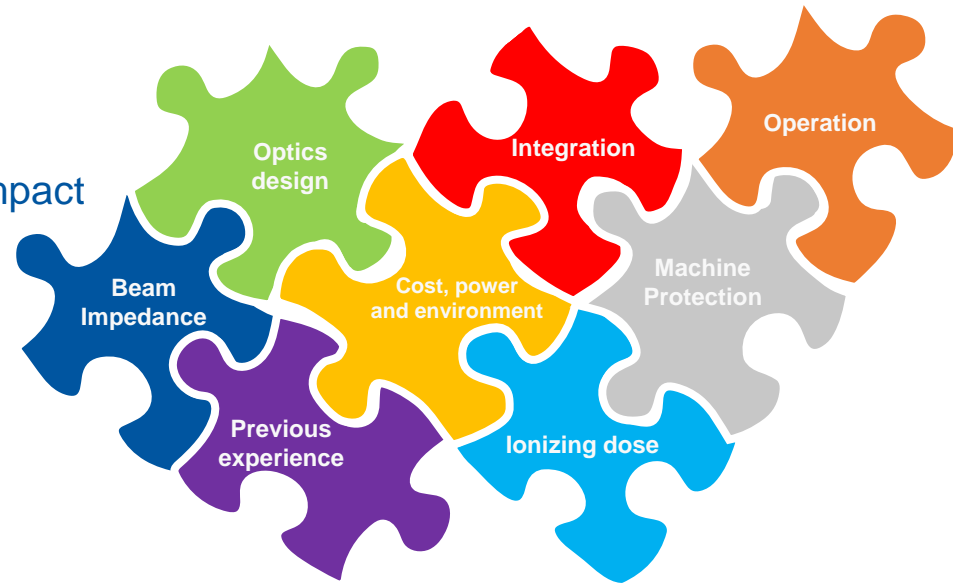
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Feasibility study

Kickers and septa magnets are designed based on the following key considerations:

- Optics design
- Cost, power consumption & environmental impact
- Integration
- Ionizing dose levels
- Machine protection impact
- Operational needs
- Collective effects



The main challenge lies in maintaining a well-balanced final design that accounts for all these factors and their interdependencies, like solving a complex puzzle

Optics design

- ❑ The specifications for kickers and septa are primarily determined by the lattice design
- ❑ Any changes to these parameters necessitate a re-evaluation of the feasibility study and a reconsideration of the design choices for the kickers and septa systems
- ❑ Foresee lattice design iterations where the kicker or septa design may fail to meet required parameters due to technical limitations
- ❑ Some parameters remain undefined or to be confirmed:
 - Beam stay clear region
 - Rise and fall time definition
 - Flat top quality
 - Beam line length

Cost, power consumption & environmental impact

❑ Cost considerations:

- **Standardization of equipments:** implementing standardized solutions across all systems reduces costs and simplifies maintenance
- **Limited generator voltage:** it improves reliability and enhances long-term performance while reducing maintenance costs
 - **Avoiding oil-filled generators** mitigates (environmental) risks and maintenance complexities
 - **Out-of-vacuum magnets** can lower costs and are less complex to maintain

❑ Power efficiency and environmental impact:

- **Avoidance of "difficult" materials:** like gas or liquid filled cables (e.g., SF6, FC-77)
- **Electrical consumption and heat load limitation:** to enhance energy efficiency, reduce cooling requirements and decrease the environmental footprint
- **Energy recovery:** Exploring energy recovery options for generators can significantly lower operational costs

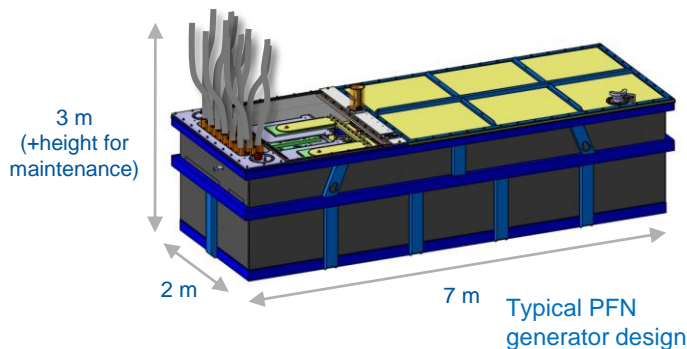
Integration

❑ Magnet length considerations:

- The length of the magnet must account for the space required for the tank or flanges, ensuring proper installation and functionality

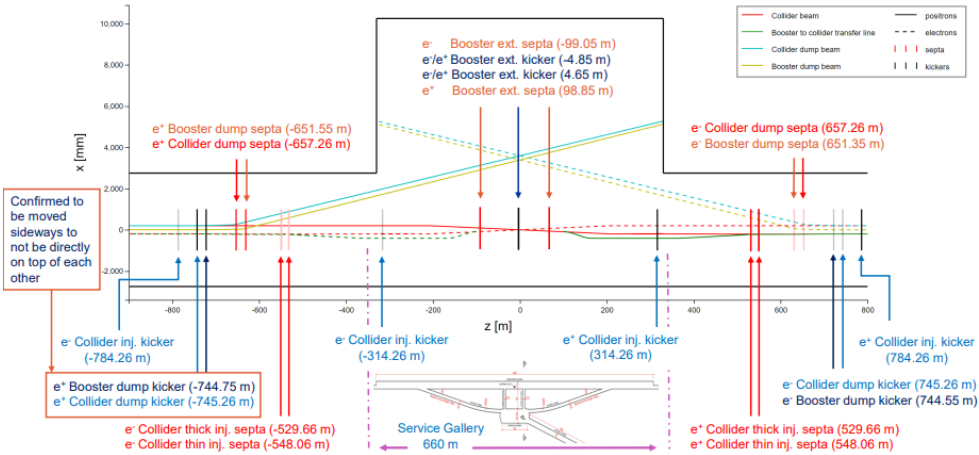
❑ Services galleries:

- **Radiation sensitivity:** all radiation-sensitive components, such as generators and controls, cannot be installed directly in the tunnel
- **Cable length implications:** the location of the service galleries directly affects the length of cables required between the magnet and the generator
- **Space requirements:** adequate space must be estimated for the generator, control systems, and any additional equipment facilitating maintenance, including spares



| FCCee POINTB (mostly) KICKERS and SEPTA Footprints | | | | | | | | | |
|--|--------------------|---|---------------------|----------------------|------------------------|---------------------------------|---|--|-----------------|
| KICKERS | Cable length (m) | Generator type | No. per beam | Total for FCC (e/e-) | Hot spares generators | Generator Footprints (m) | Racks per generator | Total racks per beam + control racks | Inc. hot spares |
| Collider injection | 250 | PFN BL DIS | 2 + 2 (2 alcoves) | 8 | 1 per alcove | 2x3.5x2.9h | 2 | 4 + 4 (+4 per alcove) | 6 + 4 |
| Collider dump | 250 | M/D generator | 6 | 12 | 2 | 1 x 2 x 3h | 2 | 12 + 3 | 16 + 3 |
| Booster injection | 30 | Inductive adder | 1 | 2 | 1 | 2 x 2 | 2 | 2 + 3 | 4 + 3 |
| Booster extraction | 100 | Main generator | 10 | 20 | 4 per beam or 6 shared | 7 x 2 x 3h | 2 | 20 + 3 | 28 + 3 |
| Booster dump | 250 | M/D generator | 6 | 12 | 2 | 1 x 2 x 3h | 2 | 12 + 3 | 16 + 3 |
| | | Unconfirmed / new iteration | | | | | | standard size of rack is 600x1000x2400mm | |
| SEPTA | Cable length (m) | Generator type (power converter) | No. per beam | Total for FCC (e/e-) | Hot spares generators | Power converter racks footprint | Additional equipment near magnet | | |
| Collider injection | 120 aim 150 max | Combined racks per magnet | 6 (1 thin, 5 thick) | 12 | N/A | 4w x 0.9d x 2.2h | Transformer (1m ³) | | |
| Collider dump | 500 | Combined racks | 1 | 2 | N/A | 2.5w x 0.9d x 2.2h | Water-cooling (0.25w x 1.5 x 1.2h) | | |
| Booster injection | 150 (reasonable) | Combined racks | - | - | N/A | - | - | | |
| Booster extraction | 120 aim 150 max | Combined racks | 1 | 2 | N/A | 4w x 0.9d x 2.2h | Transformer (1m ³) No Water-cooling? | | |
| Booster dump | 150 (reasonable) | Combined racks Beam energy tracking system | 1 | 2 | N/A | 0.8w x 0.9d x 2.2h | Water-cooling (0.25w x 1.5 x 1.2h) | | |
| BM Separator | Many 100s | Combined high voltage racks HV switches | 2 (+ & -) | 4 | N/A | 4w x 0.9d x 2.2h | Decoupling resistors and ground switches | | |
| | | Combined high current racks | | | | 3.2w x 0.9d x 2.2h | 2x0.35w x 0.8d x 1.5h per tank | | |

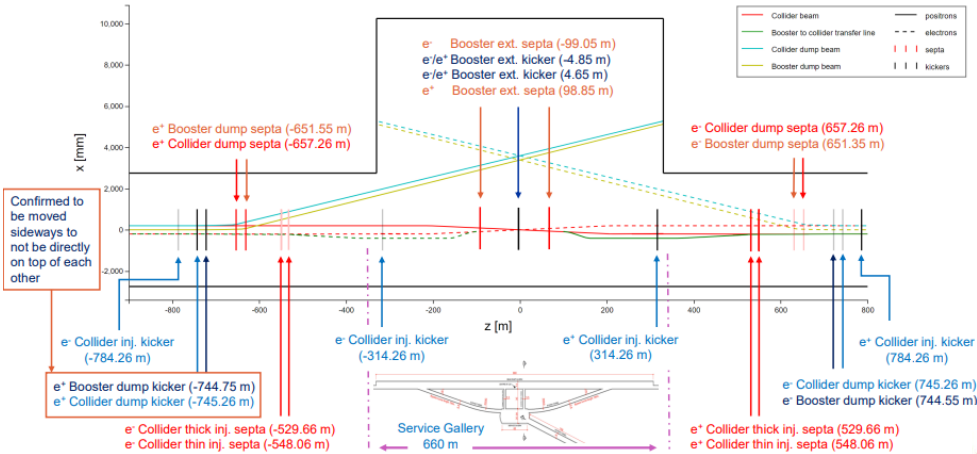
Integration – Point B



❑ Space requirements for kickers and septa estimated in **point B**

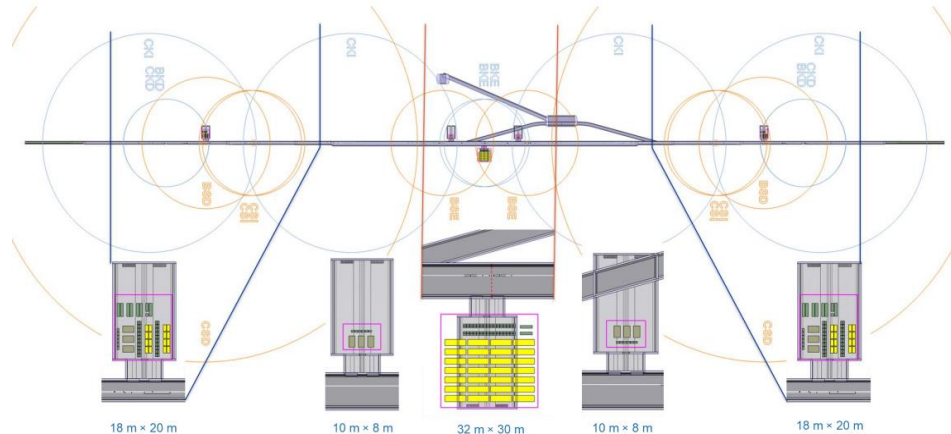
❑ Integration considerations should be initiated in **Point A** for the Booster

Integration – Point B



❑ Space requirements for kickers and septa estimated in **point B**

❑ Integration considerations should be initiated in **Point A** for the Booster



FCC-ee Underground Structure at point B

❑ As result of detailed study and more iterations, we **relaxed cable length specifications** where feasible to ease integration.

❑ Proposed alcoves layout as an **alternative to the baseline**

Ionizing dose levels

□ Use of solid-state generators and semiconductor switches:

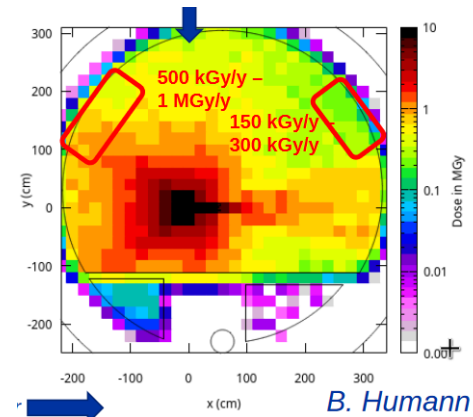
- Significant concern on the availability of high voltage thyatron switches
- Need service areas or dedicated low-radiation space

□ Synchrotron light effects:

- To be accounted for during design phases, i.e for EM separator and stripline magnet electrodes
- Dedicated mask required for EM Separator
- Electrostatic septa now avoided as too sensitive to X-ray impact, which leads to break downs

➤ Need for reliable radiation mapping:

- Straight section doses to be estimated
- Choice of components, i.e. cables, isolators
- Radiation tests prior to installation to ensure component suitability



Machine Protection

- ❑ Machine protection concerns start at booster extraction and Z-mode is the most critical
- ❑ Failure types and probability depend on magnet kind and operational conditions:
 - They are typical for high voltage fast pulsed systems (breakdown, erratic, missing, mis-kick)
 - Additional challenges are introduced by synchrotron radiation, high stored energy and energy density
 - Iteration needed at design phase to find best trade-off between magnets performance, reliability, availability and machine protection aspects
- ❑ Mitigations consist of:
 - Redundancy, monitoring and fast reaction to failures, passive protection, retriggering mechanism etc.
 - Rad-hard electronics where needed
 - Segmentation and voltage reduction to reduce risk and consequence of failures
 - Out of vacuum magnets, minimum beam coupling impedance design, etc.
 - New concepts like sacrificial absorbers (for ultra-fast failures), chunk extraction etc. have to be considered (in booster extraction/dump, booster-to collider TL, collider injection and extraction)

FCC-ee operational model

The design of kickers and septa systems is based on the new FCC operational model, which aims to maximize availability and reliability, while reducing maintenance and intervention needs, enhancing automation and AI integration.

Summary



FCC-ee requires to rethink how to operate and maintain particle accelerators.
Emerging technologies (i.e. AI) will make operating FCC-ee (financially) feasible.

→ run FCC-ee like a space telescope.

- We can learn from their approaches

It means:

- Maximising availability and physics time at constant number of personnel
- → Redundancy and margin
- → Full remote diagnostics and control
- → Full automation
- And also: Overall system engineering, analysis and coordination

An operational model for the FCC, RAWG, V. Kain, 18-June-2024

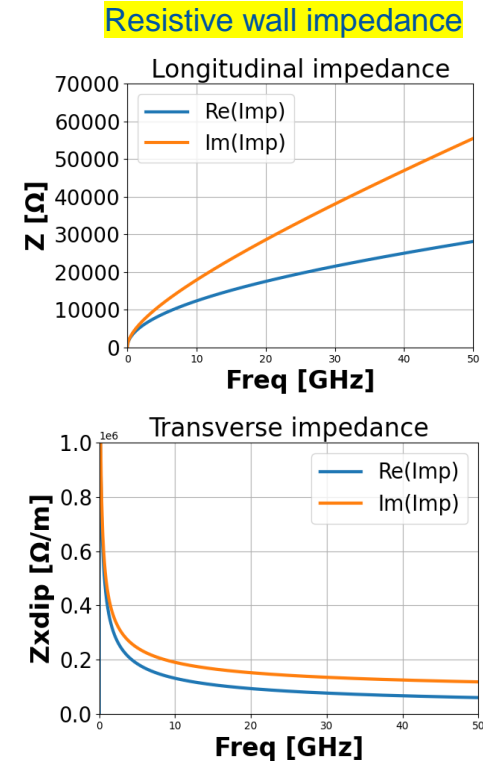
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Courtesy of V. Kain



Collective effects

- ❑ Magnet design requires optimization to limit beam coupling impedance and e-cloud:
 - Coating foreseen in lumped inductance magnets
 - Stripline needs proper design to minimize impedance or integration of a resistive network
 - EM separator requires proper electrode design
 - Beam stay clear region needs to be defined, as it largely affects impedance
 - Vacuum requirements and equipment integration need to be clarified for septa to assess impedance impact
- ❑ Resistive wall impedance presently used as target ($\ll 10x$):
 - Beam induced heating needs dedicated study to design proper beam screens
 - Complete magnet design needed for accurate prediction at high frequencies



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Future work: R&D and prototyping

□ Kickers

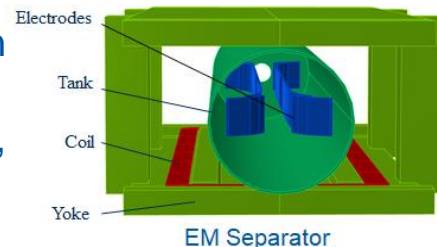
- **Stripline magnet driven by an inductive adder:** to optimize the design, balancing the trade-off between impedance matching and beam coupling
- **Lumped inductance magnet driven by a PFN or Marx generator:** it requires the development of proper compensations for such long cable connection to achieve rise time and flat-top specifications for long pulse durations

□ Septa

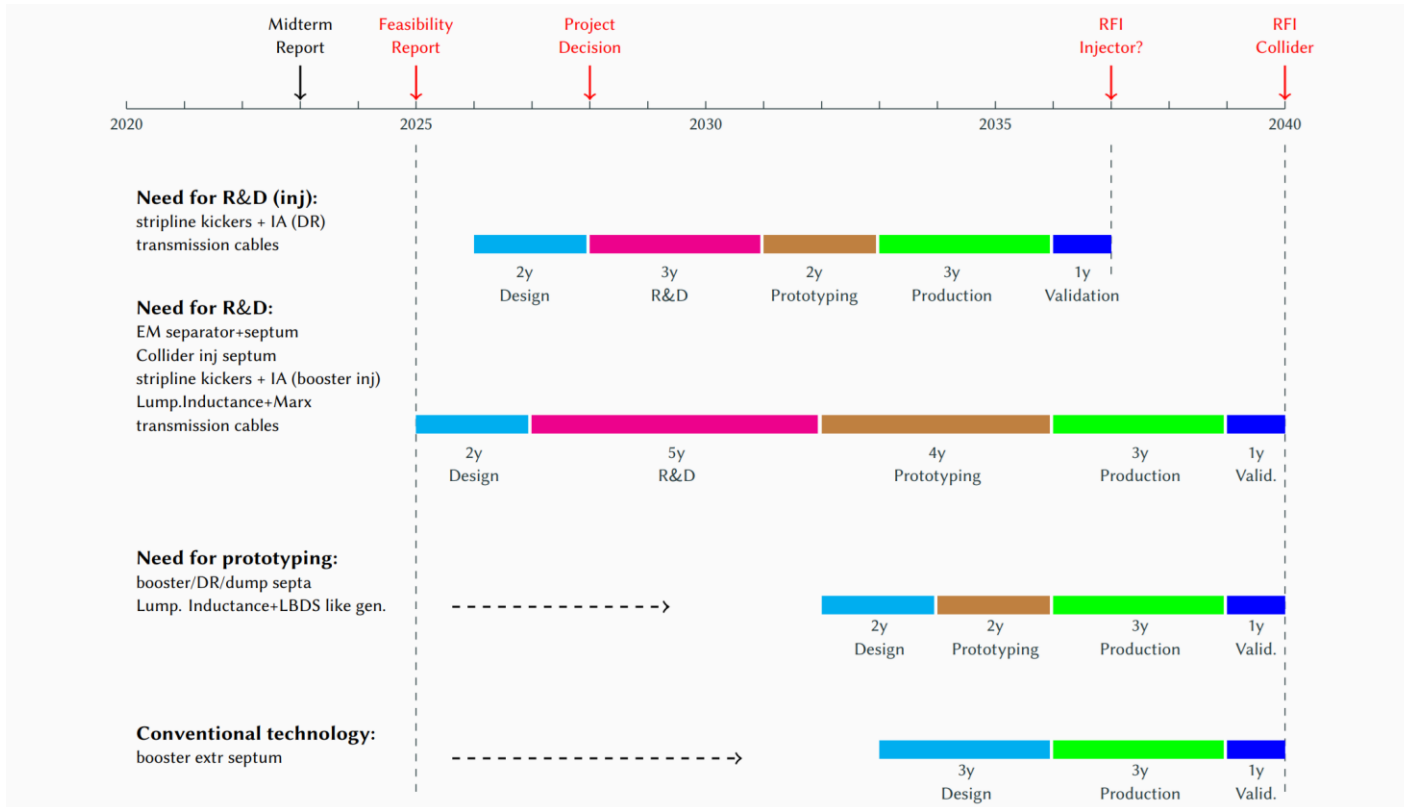
- **Lambertson septa** close to the design limit of the septum thickness. Bake-out requirements to be clarified from early on in the project.
- Robustness of **direct drive septa** for Collider injection to be confirmed. May require novel cooling concepts

□ EM-separator

- If break down rate limit (tbd) cannot be reached, single RF concept in the collider will need review. **Urgent R&D required**
- Requires local cancellation of the E and B field in one beam direction, while providing a homogeneous field in the opposite direction
- The desired installation moment to be clarified early in the project



Future work: R&D and prototyping



Given the extensive R&D and prototyping needed, it may be beneficial to consider initiating R&D studies in the near future

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Conclusion

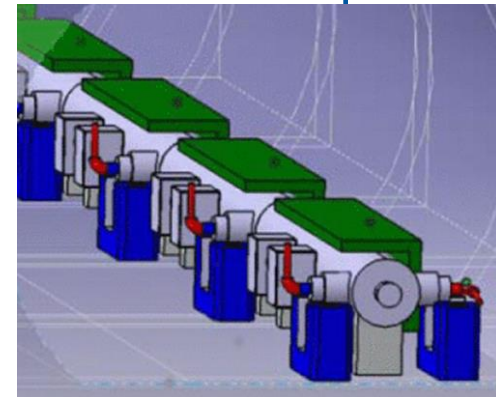
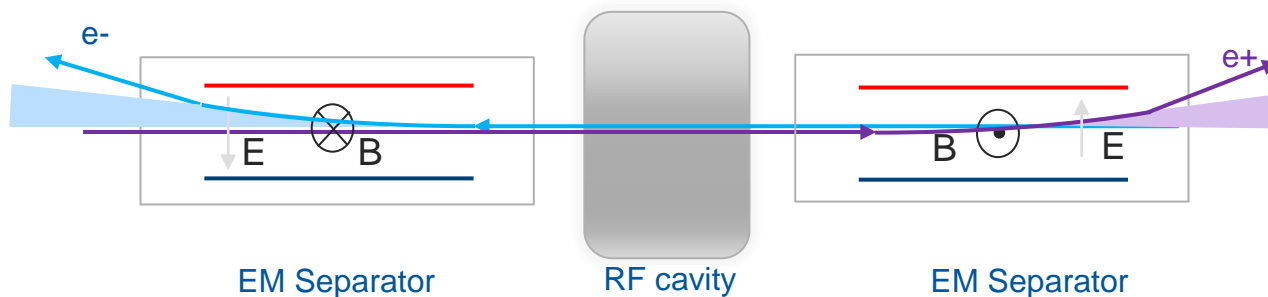
- ❑ The baseline design for kickers and septa has been established
- ❑ These designs are developed to optimize cost, availability, reliability, energy efficiency, and address integration, operational and radiation constraints
- ❑ New iterations are expected due to changing requirements; however, it is essential to adapt to the current hardware design in order to move forward with the next steps
- ❑ Given the unprecedented specifications, R&D and prototyping are envisaged to develop new technologies and optimize existing ones to achieve target parameters

Optics design – Parameters table

| | Damping Ring | Booster injection | Booster extraction | Booster dump | Collider injection | Collider dump |
|---|-----------------------|-----------------------|-----------------------|-----------------|--------------------|----------------|
| Energy [GeV] | 2.86 | 20 | 45 – 182.5 | 45 – 182.5 | 45 – 182.5 | 45 – 182.5 |
| Beam line length [m] | tbc | 5.5 (tbc) | 15 (tbc) | 15 (tbc) | 15 (tbc) | 15 (tbc) |
| Total kick angle [mrad] | 3 | 0.09 | 0.2 | 0.3 | 0.08 | 0.3 |
| Aperture (beam stay clear) (\varnothing) [mm] | 30 | 30 | 60 | 60 | 60 | 60 |
| Rise / fall time [ns] | 82.5 | 25 | 1100 | 1100 | 1100 | 1100 |
| Flat top length [μ s] | 0.08 | 0.08 | 30 – 304 | 304 | 30 – 304 | 304 |
| Rise and fall time definition | 0.5% - 99.5% (tbc) | 0.7% - 99.3% (tbc) | 0.6% - 99.4% (tbc) | (tbc) | (tbc) | (tbc) |
| Flat top quality [%] | ± 0.5 (tbc) | ± 0.7 (tbc) | ± 0.6 (tbc) | ± 1.5 (tbc) | ± 20 (tbc) | ± 20 (tbc) |
| Repetition rate [Hz] | 100 | 100 | 0.3 | 1 | 0.3 | 0.1 |

Collider: Electric-Magnetic (EM) separator

- Installed upstream and downstream of RF section in tbar mode in point H.
- Used to assure both beams pass through centre of RF cavities, while avoiding synchrotron light hits the cavities.
- Magnetic field is cancelled by the electric field before entering the cavity, while adding up for particles the cavities.
- The 2 families of 10 EM separators [6] will be powered in series (magnet) and parallel (separator), limiting the power converter footprint.



Machine Protection – Booster Failures

| Failure | Consequence | # affected bunches |
|---|--|--|
| Asynchronous extraction | xx bunches swept in the machine aperture | It depends on reaction, re-triggering and rise time (e.g. 44 for 1.1 us and 60 for 1.5 us) |
| Large ripples of extraction kickers | bunches extracted with oscillations, losses at the septum, septum mask and/or the transfer lines, poor transmission to the collider, large injection oscillations and losses in the collider | It depends on the waveform shape but in principle up to all (1120 for Z mode) |
| Up to 100XX extraction kickers missing .or. 100YY extraction septa not pulsing at nominal strength (0-100%) | mis-kicked bunches → oscillations in TL, losses (also possible at one single location), poor or no transmission, injection oscillations and losses in the collider | All (1120 for Z mode) |

Machine Protection – Colliders Failures

| Failure | Consequence | # affected bunches |
|---|---|--|
| Asynchronous extraction | xx bunches swept in the machine aperture | It depends on reaction, re-triggering and rise time (e.g. 44 for 1.1 us and 60 for 1.5 us) |
| Large ripples of extraction kickers | bunches extracted with oscillations, losses at the septum, septum mask and/or the transfer lines | It depends on the waveform shape but in principle up to all (11200 for Z mode) |
| Up to 100XX extraction kickers .or. 100YY extraction septa not pulsing at nominal strength (0-100%) | mis-kicked bunches → oscillations in TL, losses (also possible at one single location) | All (11200 for Z mode) |
| 100XX missing injection bumpers .or. pulsing with higher current than nominal | miss-kicked circulating bunches → oscillations (bump amplitude/xx) and losses at collimators, septum and septum mask. | All (11200 for Z mode) |
| 100YY septum not pulsing at nominal strength (0-100%) | injected bunches mis-kicked → injection oscillations and losses in the collider | All (1120 for Z mode) |
| Sparks in electromagnetic separator | large kicks to the full circulating beam and ultra-fast losses | All (56 for ttbar and 380 for ZH modes) |

Thyratrons vs semiconductor switches

Semiconductor switches can be used in fast high current pulsed power accelerator applications to replace thyatrons and PFLs.

Thyratrons

- + Generally reliable
- + Robust (fault tolerant)
- + Relatively high voltage
- + Relatively high current
- Long term availability
- Spontaneous turn on
- Can only be turned on

Versus:

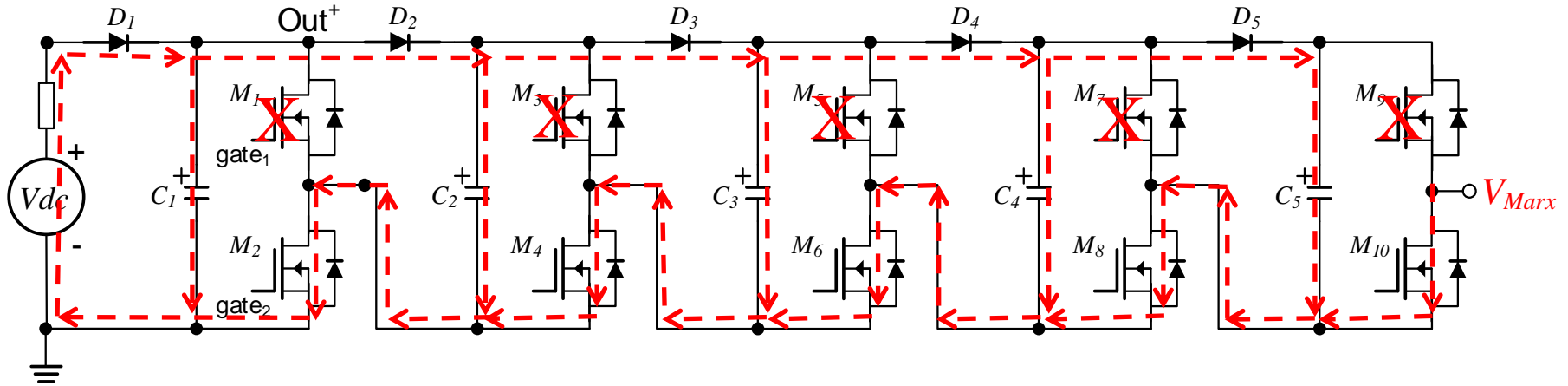
Solid-state

- + Cost-effective
- + Easy to use
- + Off-the-shelf
- + Flexible
- + Modular
- + Maintainability
- + **Can be turned on and off (thus PFL/PFN is not required)**
- Relatively low voltage
- Relatively low current

But.... Semiconductors have limited voltage and current rating. Hence, requires **series and parallel connection of power semiconductors** to achieve high pulsed power.

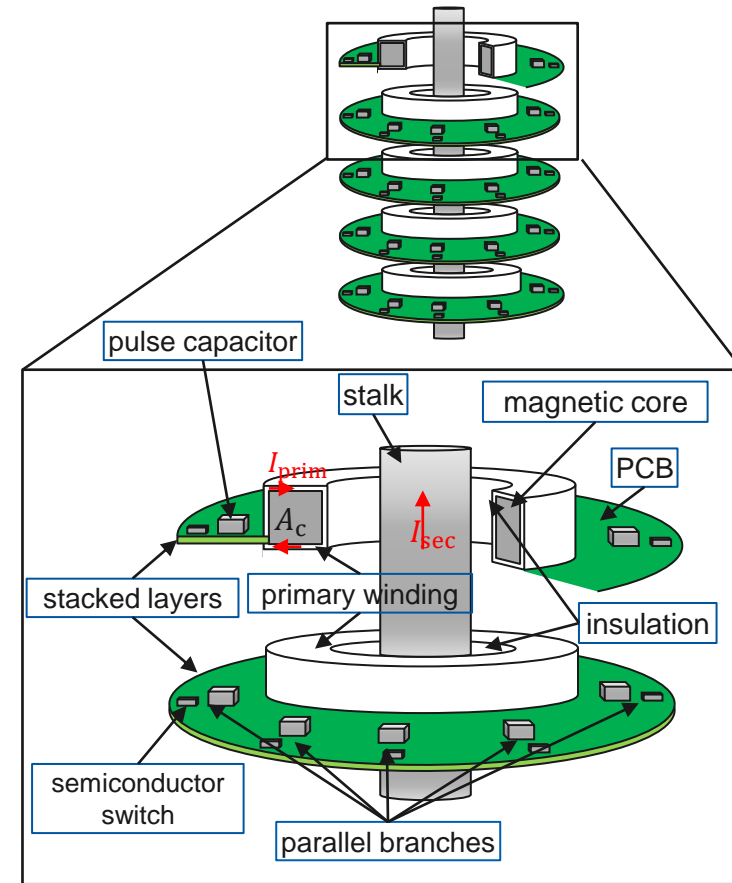
Marx generator

- In a Marx generator n capacitors are charged in parallel from a relatively low-voltage DC power supply, and discharged in series into the load
- The output voltage pulse has an amplitude approximately equal to the number of stages (n) times the input voltage (V_{dc}), $V_{Marx} = n \cdot V_{dc}$
- 16 kV, 2.6 kA, 75 ns rise and fall prototype developed for FCC-hh



Inductive adder

- The IA is a solid-state modulator, which can provide relatively short and precise pulses
- An inductive adder consists of multiple parallel layers (also known as stages), each of which has a 1:1 transformer
- The single turn primary totally encloses a magnetic core; hence, the leakage inductance of this geometry is negligible
- The secondary winding of each of these transformers is connected in series: hence a step-up voltage ratio of 1:N is achieved by using N-layers, with adequate voltage isolation



Previous experience

□ LEP:

- Experience from LEP serves as a valuable reference for the new design
- However, higher synchrotron radiation power is expected due to the use of top-up injection

□ CLIC:

- A stripline kicker magnet driven by an inductive adder was studied and prototyped for the CLIC Damping Ring
- While the specifications are similar to those for the FCC damping ring, further optimization is required to meet new requirements