# Emittance measurement with a Slit \& Grid system in high intensity hadron machine 

DITANET-High Intensity Proton Beam Diagnostics workshop<br>Massy-Palaiseau September $26^{\text {th }}-27^{\text {th }}$

## Outline

- Emittance measurement with a Slit \& Grid System
- Thermal load
- Space Charge effect
- Multiple Scattering effect


## Slit \& Grid system

Emittance measurement with moveable slit

## Issue on the slit design and emittance reconstruction

- The slit == beam dump
- High thermal load and high thermo-mechanical stresses
- The slit geometry and the global emittance meter design has an influence on the measurement resolution
- Multiple scattering effect on slit edges
- Space charge effect on the beamlet


## LINAC4 emittance meter



Diagram of the LINAC4 diagnostic test bench
-Will be installed in LINAC4 diagnostic test bench for commissioning phase -3 commissioning stages

$$
\begin{aligned}
& \text {-RFQ exit (3 MeV) } \\
& \text {-End of Chopper line (or MEBT) ( } 3 \mathrm{MeV} \text { ) } \\
& \text {-Exit of DTL tank } 1 \text { (12 MeV) }
\end{aligned}
$$

-Drift space between slit and grid equal to 3,5 meters

## Thermal load-LINAC4 example

| Commissioning <br> stage | Energy [MeV] | Intensity <br> $[\mathbf{m A}]$ | Pulse Lendth <br> $[\boldsymbol{\mu} \mathbf{s}]$ | $\boldsymbol{\sigma}_{\mathbf{x}}[\mathbf{m m}]$ | $\boldsymbol{\sigma}_{\mathbf{y}}[\mathbf{m m}]$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| MEBT | 3 | 65 | 100 | 3.64 | 3.61 |
| DTL | 12 | 65 | 100 | 1.21 | 1.8 |

- $4 \times 10^{13}$ particles per pulse
- @ 3MeV:
- Energy

$$
=>\quad 31 \mathrm{~J}^{2} \mathrm{~cm}^{-2}
$$

- Power (over pulse) $\quad=>\quad 0.31$ MW.cm ${ }^{-2}$
- @ 12 MeV :
- Energy
- Power (over pulse) $\quad=>\quad$ 7.56 MW.cm ${ }^{-2}$


## Thermal load

## The Material and geometry should be defined to reduce the thermal load and Mechanical stresses.

Energy deposition has been calculated with FLUKA
First estimation of the temperature with analytical model for the material choice and slit geometry
Energy deposition map from FLUKA used as input in ANSYS analysis

- Material suitable for the slit:
- Material with high Melting point (Tungsten, Tantalum, Graphite)
- Material with high Cp (Graphite, Beryllium)
- Material with High thermal conductivity (Copper)
- Geometry:
- Spread the energy deposition in a larger surface.


## Thermal load-Material of the slit

- For the largest beam power $12 \mathrm{MeV}, 65 \mathrm{~mA}$ and $100 \mu \mathrm{~s}$ and a given slit geometry (slit at $30^{\circ}$ w.r.t. the beam axis):

| Material | T surf [K] | T max [K] | Bragg peak <br> depth [ $\mu \mathrm{m}]$ | Density $[\mathrm{g} /$ <br> $\left.\mathrm{cm}^{3}\right]$ |
| :---: | :---: | :---: | :---: | :---: |
| Beryllium | 907 | 2148 | 537 | 1.85 |
| Graphite | 1327 | 3143 | 513 | 1.90 |
| Copper | 3091 | 7028 | 147 | 8.96 |
| Tantalum | 4076 | 5368 | 103 | 16.65 |
| Tungsten | 5660 | 7028 | 92 | 19.35 |

High density material not adapted despite their high melting point ( $\mathrm{Cu}, \mathrm{W}, \mathrm{Ta}$ )
The slit material must have a low density, high Cp and high melting point

## Graphite is the best candidate

## Thermal load-slit geometry

- The slit is tilted to spread the energy deposition on a largest surface.
- The angle w.r.t the beam axis is chosen in order to keep the thermal load below the Graphite limits.


Energy deposition along the $z$ axis for three slit angles at 3 MeV (MEBT), in case of a Graphite slit.

|  | SRIM | FLUKA |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Angle [deg] | 90 | 90 | $\mathbf{4 5}$ | $\mathbf{1 5}$ |
| MEBT | 2673 | 2613 | 2065 | 1696 |
| DTL | 4669 | 4594 | 3931 | 2790 |

Maximum in temperature for the three commissioning stages, as estimated by analytical model (SRIM) and numerical simulations (FLUKA) when considering a 65 mA, 100 s pulse.

Even with $15^{\circ}$, thermal load is too high for DTL case.
Move the slit 1 m downstream beam sizes increase by a factor 1.5 Temperature drops to 1520 K

## Thermal load-ANSYS*



Temperature increases on Graphite plate with cooling circuit in Copper for DTL case. (Courtesy of A. Dallocchio and F. Carra).


Evolution of the temperature with external cooling on Graphite plate at 12 MeV . (Courtesy of A. Dallocchio and F. Carra).

Cooling by conduction and effect of cooling system implemented in ANSYS.


- Maximum temperature reduced by 250 K in $100 \mu \mathrm{~s}$
- Equilibrium reached after few pulses, $\mathrm{T}_{\max }=1400-1500 \mathrm{~K}$
*Simulations done by CERN EN group.


# Space charge effect on emittance reconstruction 

- Full emittance scan simulated with PATH
- Gaussian beam generated with the expected Twiss parameters
- Particles tracking with and without space charge effect
- Two slit aperture simulated (100 and $200 \mu \mathrm{~m}$ )


Emittance reconstruction error due to space charge, considering two slit apertures

## Multiple scattering effect

- Effect of the slit geometry on the amount of scattered particles estimated with FLUKA


Simulation parameters:

- $2,5 \mathrm{MeV}$ proton beam
- Gaussian beam source generated with PATH
- Graphite as slit material (penetration depth $75 \mu \mathrm{~m}$ )
- 3 slit thicknesses simulated ( 0,50 and $100 \mu \mathrm{~m}$ )
- 2 slit apertures simulated ( 100 and $200 \mu \mathrm{~m}$ )

Schematic diagram of the slit used in the simulations.
Scattered and non scattered particles position scored on a screen $35,2 \mathrm{~cm}$ downstream the slit.


Beamlet profile reconstruction

## Effect of the slit thickness



Simulated distribution of the particles at the profile monitor location.


## Effect of the aperture



- Amount of scattered particles almost independent of the slit aperture
- Large slit apertures provide better non scattered/ scattered particles ratio


## Summary

- Thermal analysis
- Graphite is the best material choice
- Slit angle of $15^{\circ}$
- From ANSYS the maximum temperature is about 1400 K



## Mechanical limit of graphite reached

- Error on emittance reconstruction
- Space charge $=>$ small slit aperture
- Multiple scattering => large slit thickness and large slit aperture


> Effect of scattering can be reduced in offline analysis $\Rightarrow>$ Small aperture to keep error less than few $\%$

## Outlook-L4 design

Slit design also influenced by other parameters (space available, mechanics....)


- Graphite plates clamped on a copper block
- Slit aperture adjustable at the assembly ( 100 or $200 \mu \mathrm{~m}$ )
- Slit thickness equal to 3 mm .


## EXTRA SLIDE

Specific heat capacity models :


## EXTRA SLIDE

Temperature profile along the longitudinal axis, for the DTL case.


Graphite slit


Tungsten slit

## EXTRA SLIDE

Temperature History


Evolution of the temperature with internal cooling by conductivity only, on a Graphite plate at 12 MeV . (Courtesy of A. Dallocchio and F. Carra).

## EXTRA SLIDE

- Effect of Multiple scattering on emittance reconstruction assuming the same weight for scattered and non scattered particles.

Threshold [\%]

|  | 0 |  |  |  |  |  | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thickness $[\mu \mathrm{m}]$ | $\varepsilon_{\text {norm }}[\pi . \mathrm{mm} . \mathrm{mrad}]$ | Error [\%] | $\varepsilon_{\text {norm }}[\pi$.mm.mrad] | Error [\%] |  |  |  |
| 0 | 1.41 | 516 | 1.28 | 467 |  |  |  |
| 10 | 1.41 | 516 | 1.28 | 467 |  |  |  |
| 50 | 0.72 | 214 | 0.23 | 0.62 |  |  |  |
| 100 | 0.31 | 36 | 0.22 | -0.58 |  |  |  |
| 500 | 0.33 | 44 | 0.22 | -1.11 |  |  |  |
| PATH | 0.23 | 0 | 0.23 | 0 |  |  |  |

