

# Beam Diagnostics

Anne Dabrowski  
CERN PH/CMX

Material in these slides included from

T. Lefevre, E. Bravin, (DITANET instrumentation school 2009)  
R. Jones, U. Raich (CAS 2008 & ASP2010 school)  
H. H. Braun (CAS 2008), P. Frock (CAS 2008) M. Minty (CAS 2003)

[http://cas.web.cern.ch/cas/CAS\\_Proceedings.html](http://cas.web.cern.ch/cas/CAS_Proceedings.html)

<http://www.liv.ac.uk/ditanet/events/>

<https://espace.cern.ch/juas/SitePages/Home.aspx>



→ Why do we need diagnostics

→ What do we need to measure?

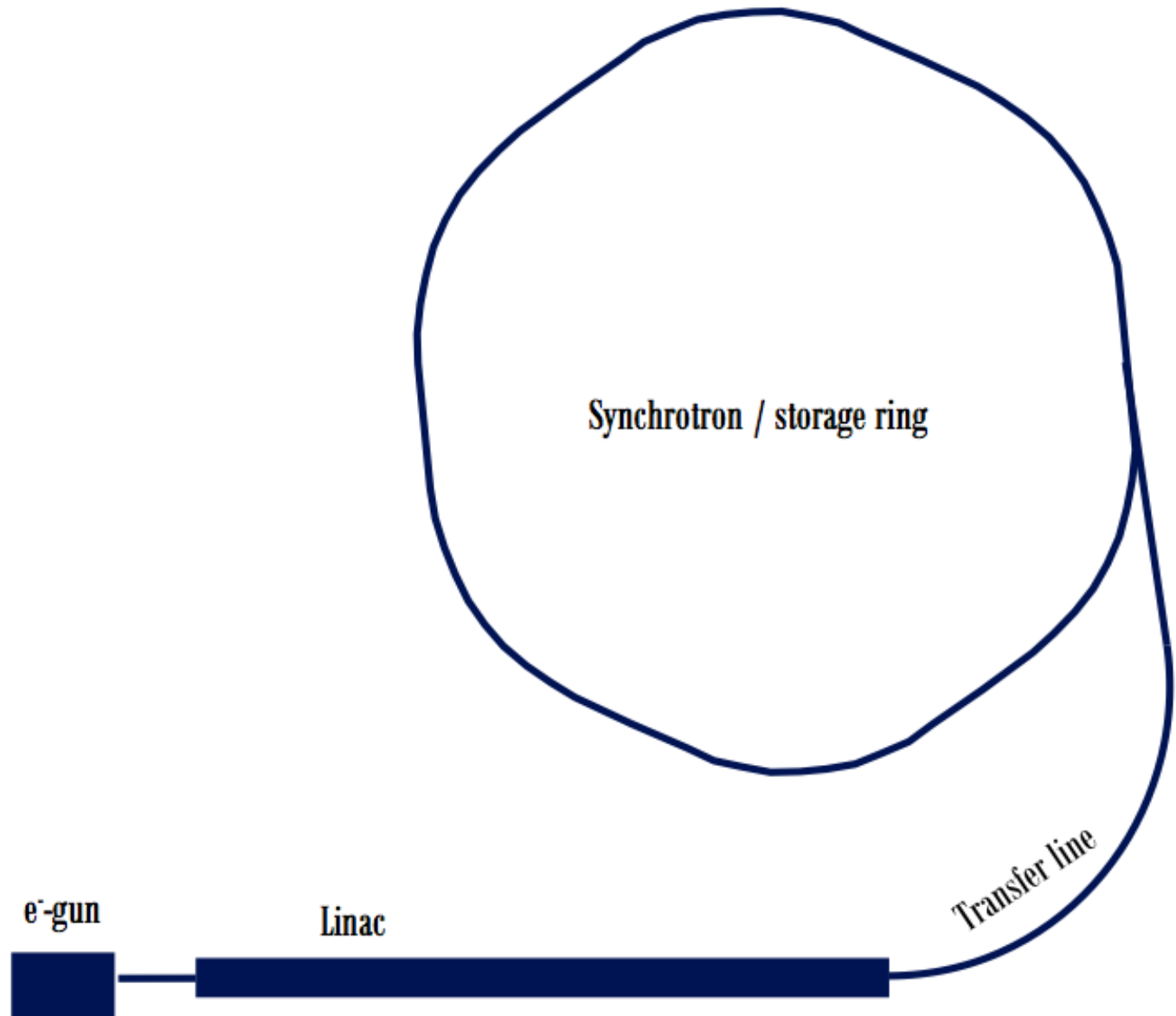
- Position
  - Capacitive BPM
- Current
  - Wall current monitor
  - Faraday Cup
- Transverse Profile (emittance, TWISS ( $\alpha\beta\gamma$ ) parameters)
  - Intercepting methods
    - » Scanning wires
    - » Radiative screens
    - » Scintillation screens
    - » Cerenkov targets
  - Non intercepting methods
    - » Synchrotron light
- Longitudinal Profile
  - Streak Camera
  - RF deflector
  - Electro optical techniques
  - RF power measurements and spectroscopy
- Luminosity Detectors
- Beam Loss Detectors

First  
Lecture

Second  
Lecture

→ Discuss diagnostics developments needed for new machines

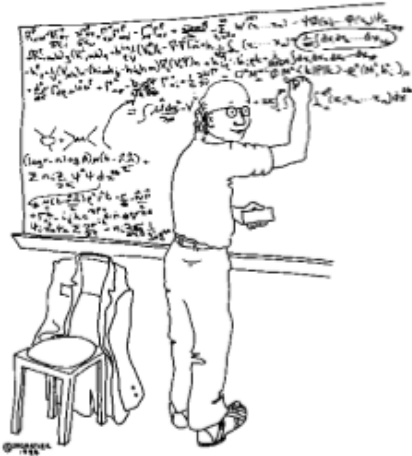
# Why do we need diagnostics?



H. H. Braun (CAS 2008)

# Why do we need diagnostics?

**Accelerator design relies on well established physics !**



## Magnets, RF cavities

Maxwell's equations

$$\nabla \cdot \vec{D} = 4\pi\rho$$

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{E} = -\frac{1}{c} \frac{\partial \vec{B}}{\partial t}$$

$$\nabla \times \vec{H} = \frac{4\pi}{c} \vec{J} + \frac{1}{c} \frac{\partial \vec{D}}{\partial t}$$

## Beam dynamics

Lorentz Force

$$\vec{F} = e(\vec{E} + \vec{\beta} \times \vec{B})$$

Newton's 2<sup>nd</sup> law  
+ special relativity

$$\frac{d}{dt} \left( \frac{mc\vec{\beta}}{\sqrt{1-\vec{\beta}^2}} \right) = \vec{F}$$

tron / storage ring

## Cathode

Richardson-Dushman  
equation

$$J = CT^2 e^{\frac{-\phi}{kT}}$$

e-gun

Linac

## Synchrotron radiation

Lienard-Wiechert potentials  
and Planck's energy quanta

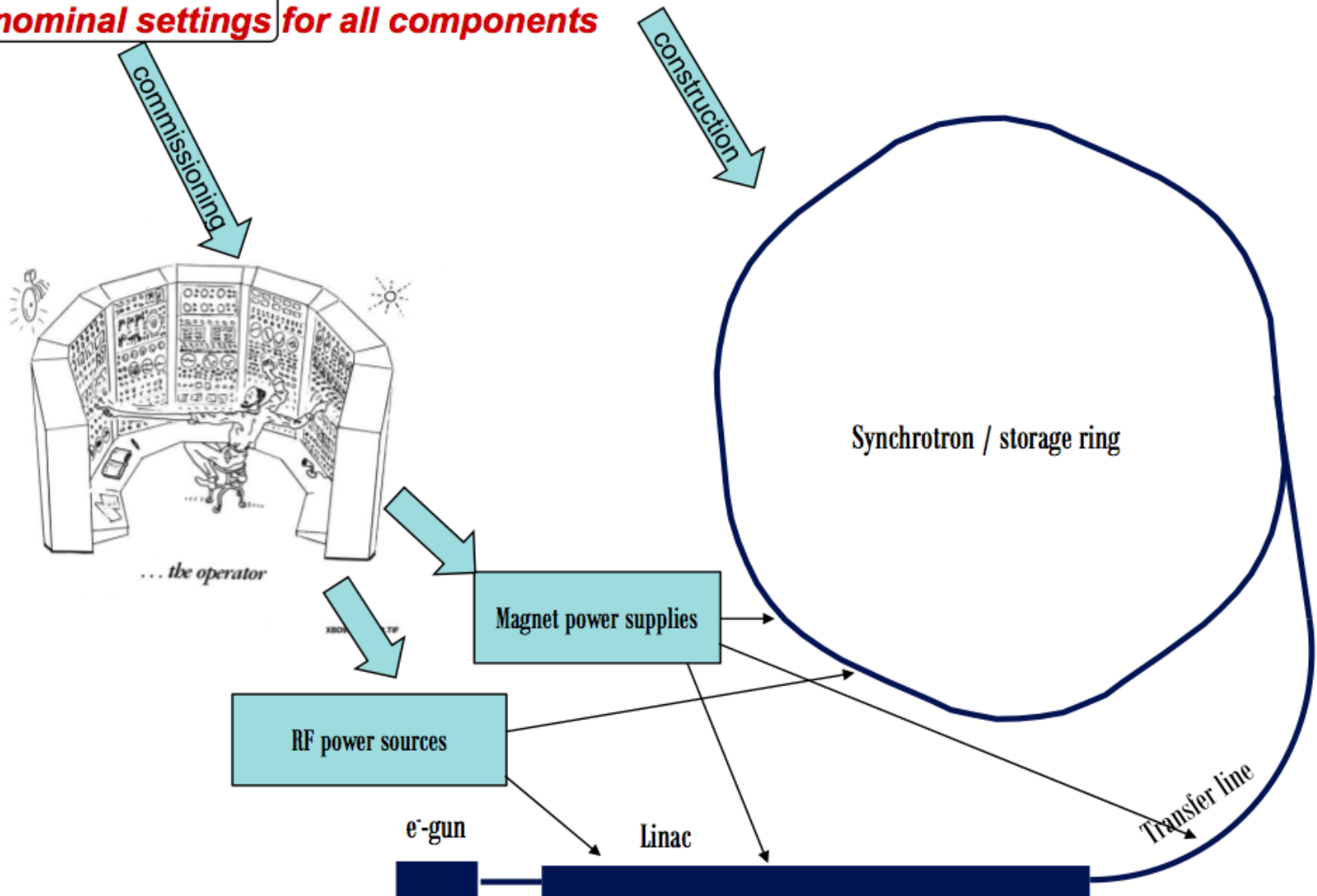
$$\phi(t) = \frac{e}{4\pi\epsilon_0} \left\{ \frac{1}{r(1-\hat{n} \cdot \vec{\beta})} \right\}_{ret}$$

$$\vec{A}(t) = \frac{\mu_0 e}{4\pi} \left\{ \frac{\vec{\beta} c}{r(1-\hat{n} \cdot \vec{\beta})} \right\}_{ret}$$

$$E = \hbar\omega$$

# Why do we need diagnostics?

**Machine design provides specifications and nominal settings for all components**



H. H. Braun (CAS 2008)

# Protection & monitoring of machine

Modern accelerators are expensive, powerful and can contain many components

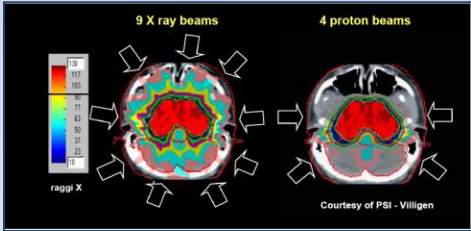
LHC contains > 1600 superconducting magnets and connections

Collateral damages due to pressure rise

Monitor changes in the temperature and pressure throughout the machine diagnose a problem and correct for it

kW of power from x-rays produced by synchrotron radiation in a light source at BNL

Medical treatment with beams



Damage to accelerator components or screens due to **high charge density CTF3 (CERN)**

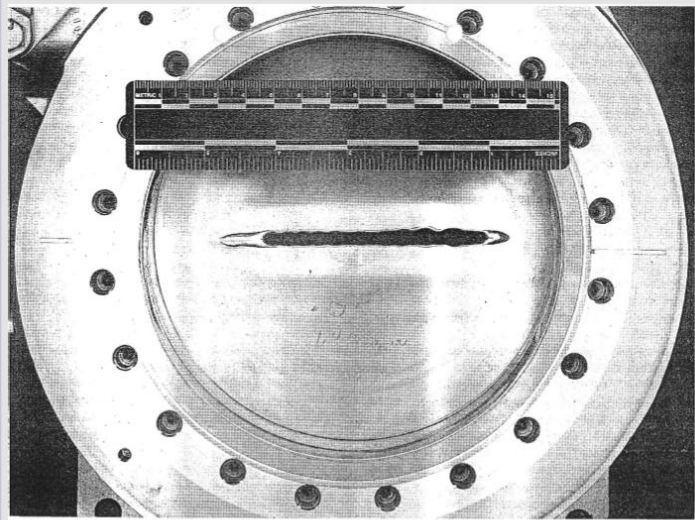
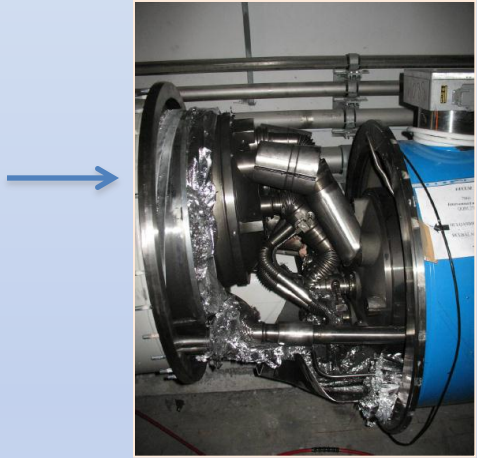
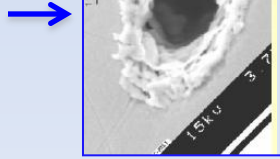


Fig. 12. Damaged X-ray ring front end gate valve. The power incident on the valve was approximately 1 kW for a duration estimated to 2-10 min and drilled a hole through the valve plate.

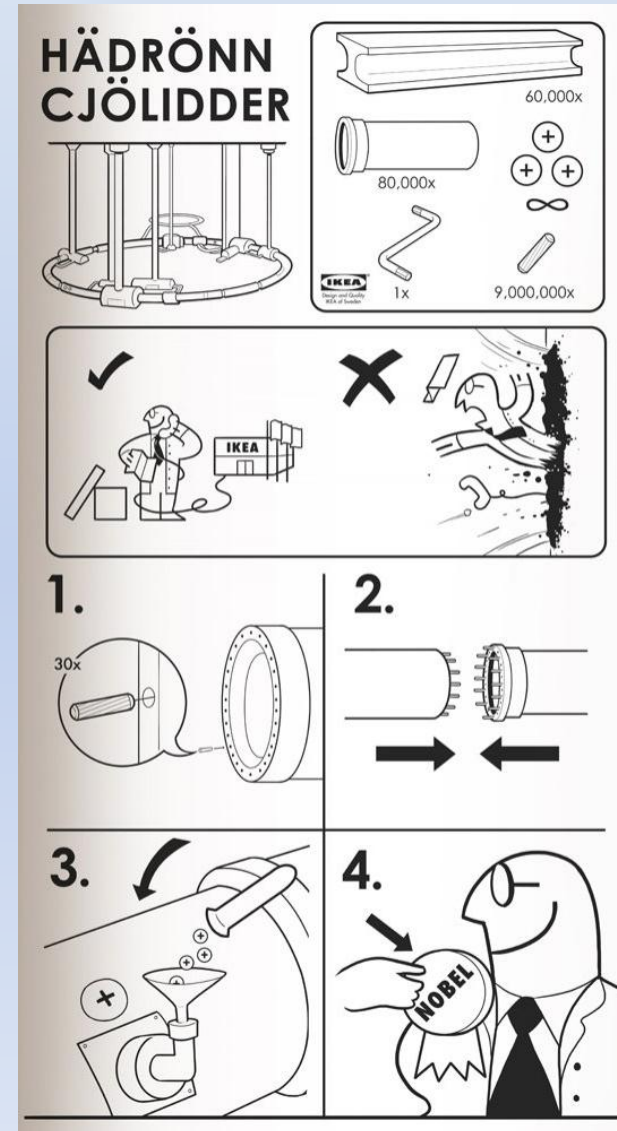


# Mistakes during building and integration

- Connect magnet polarity with the wrong polarity



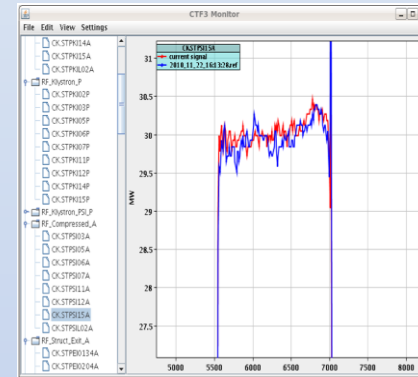
- Cables connected to the wrong equipment
- Wrong values in the controls database .. etc



# Why do we need diagnostics?

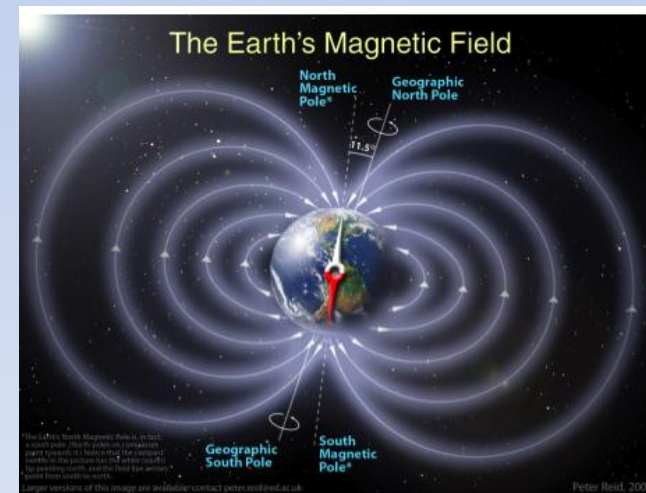
## Component tolerances and random errors

- Magnet field has been measured with a finite error
- The survey people have aligned relatively the center of neighboring magnets with a finite transverse and angular (roll) error
- The RF wave amplitude has a ripple due to another ripple from a high voltage power supply
- The resonance frequency of an accelerating structure has drifted due a temperature increase (expansion by a few microns)
- ...



## Correct for environmental effects

- Earth's magnetic field
- Mechanical vibrations induced by water flow
- Seismic vibrations
- Vibrations due to trains / airplane landing
- Stray fields from neighboring instruments or magnets
- ...



## Constantly need to measure and adjust the beam orbit

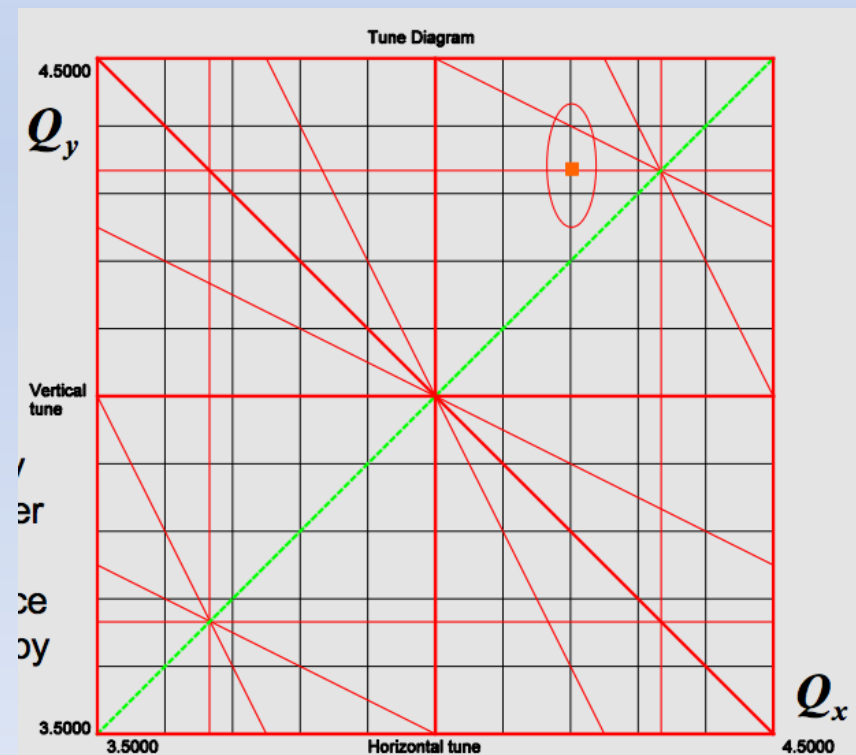
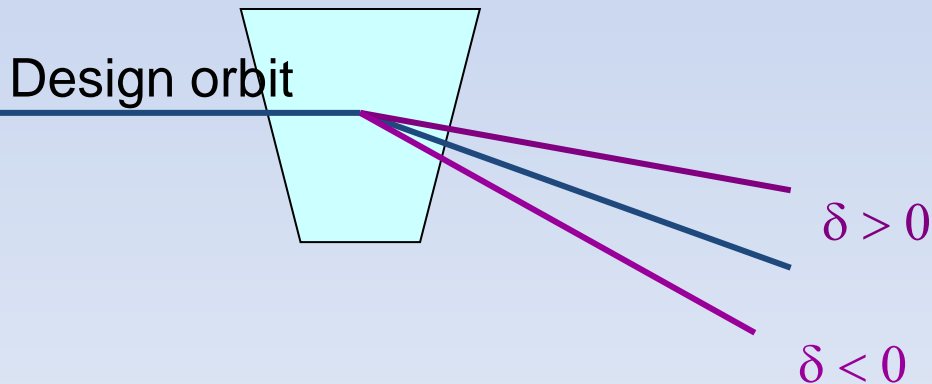


# Why do we need diagnostics?

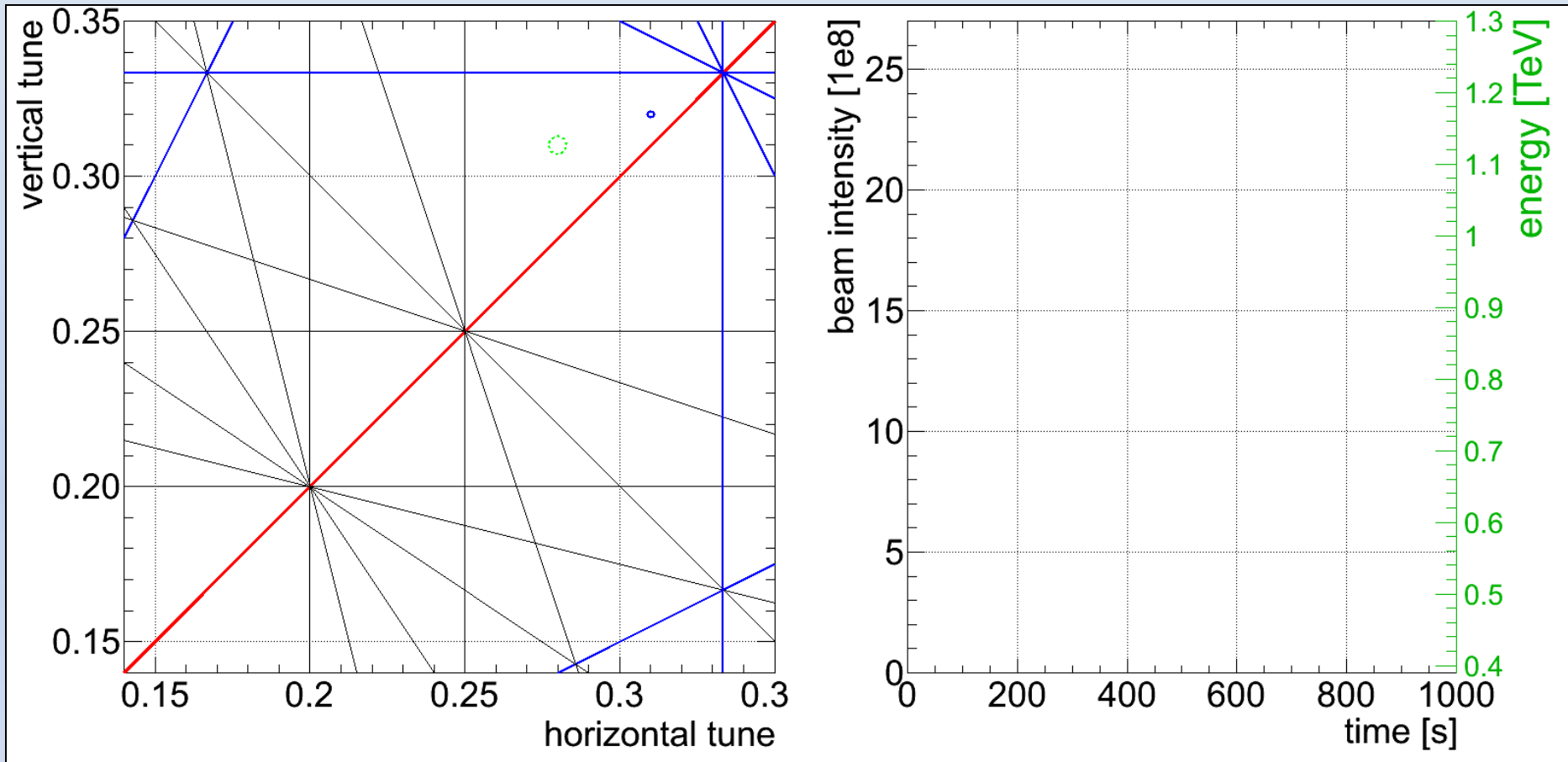
## Verification of optics model with beam based measurements

- Measure the difference between predicted trajectory / angle and measured trajectory
- Measure the dispersion pattern in the machine
- Keeping the beam within  $< 100 \mu\text{m}$  for many hours (billions of km) in a modern storage ring
- Verify you are staying away from a tune resonance
- Understand why you loose the beam ...
- Etc ...

$$x_{\max}(s) = \boxed{D_x(s) \cdot \delta} + \boxed{\sqrt{\epsilon_x \beta_x(s)}}$$

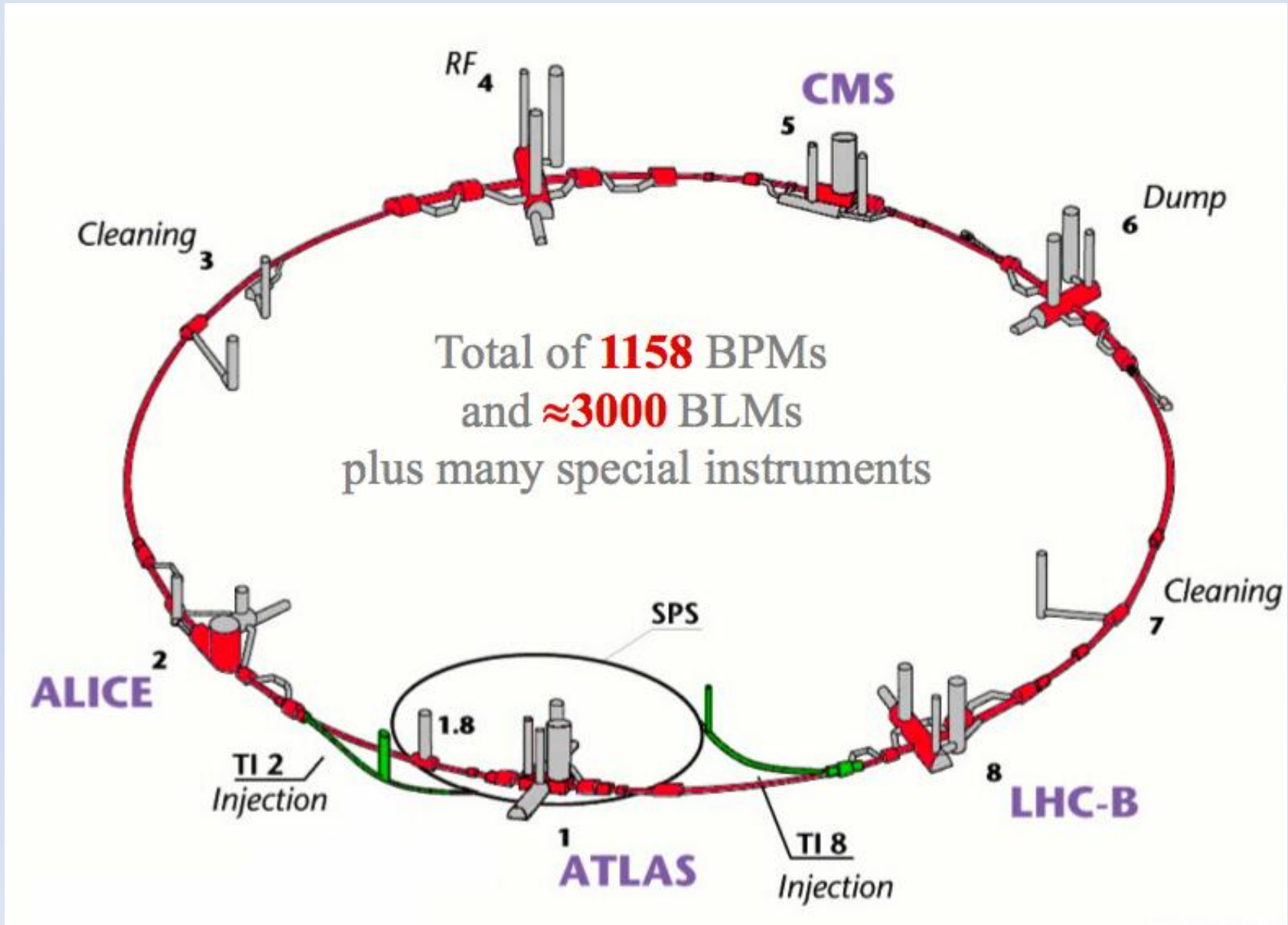


# LHC Ramp Commissioning

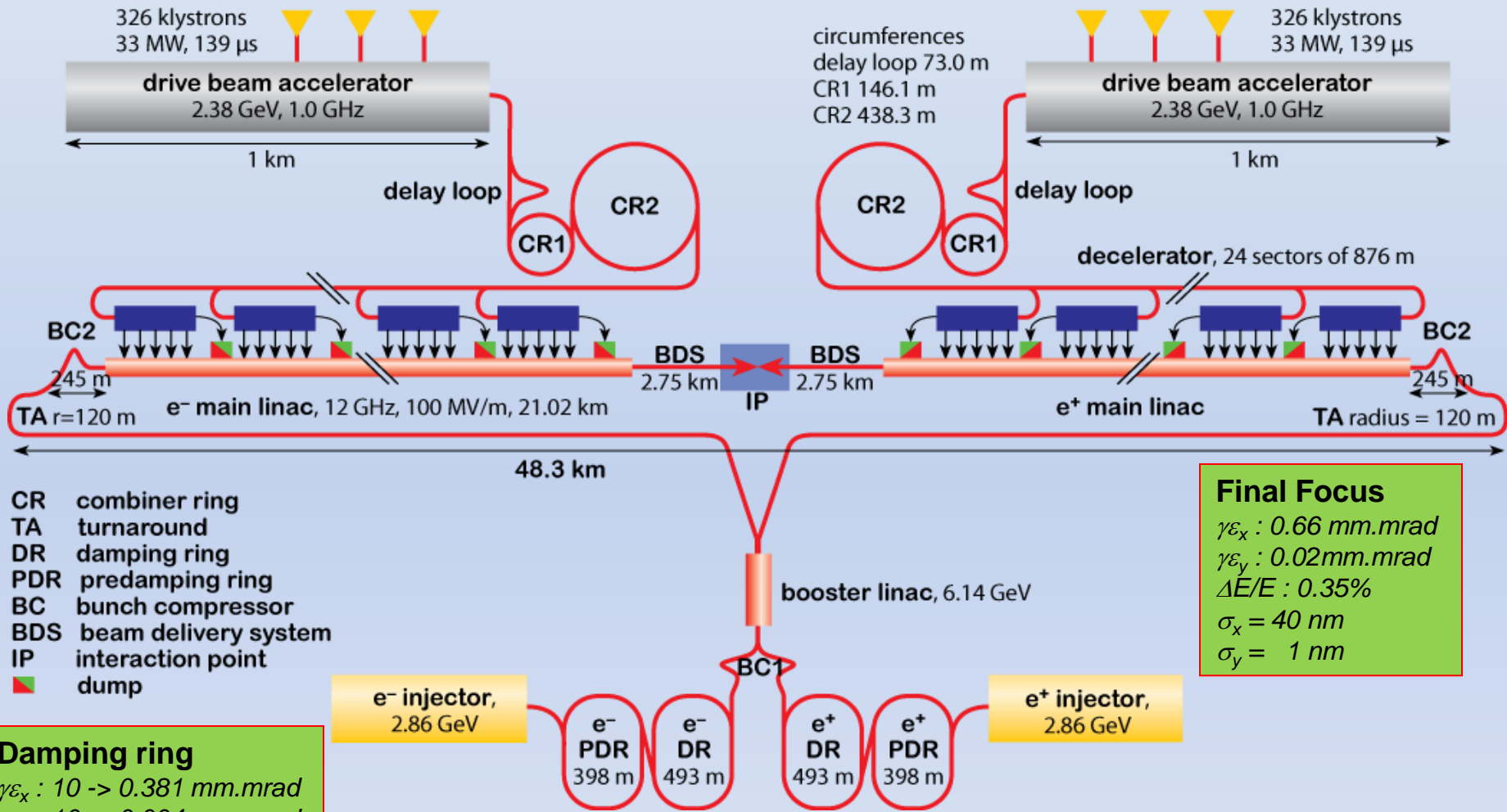


- Tune diagnostics throughout the ramp
  - Early ramps had poor tune control
  - Beam loss observed every time tune crossed resonance line

# LHC Beam Diagnostics



# Instrumentation for CLIC



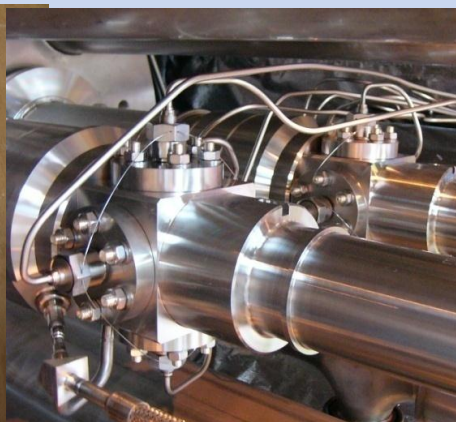
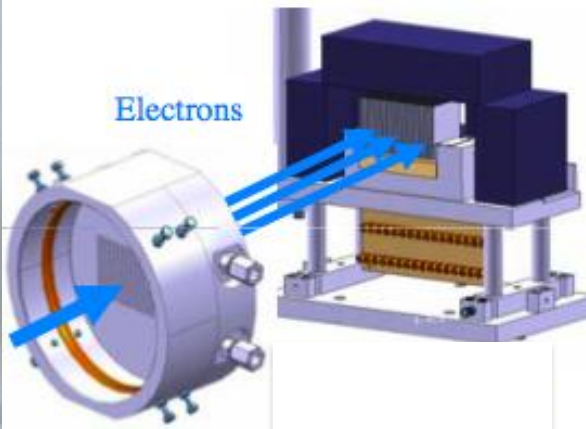
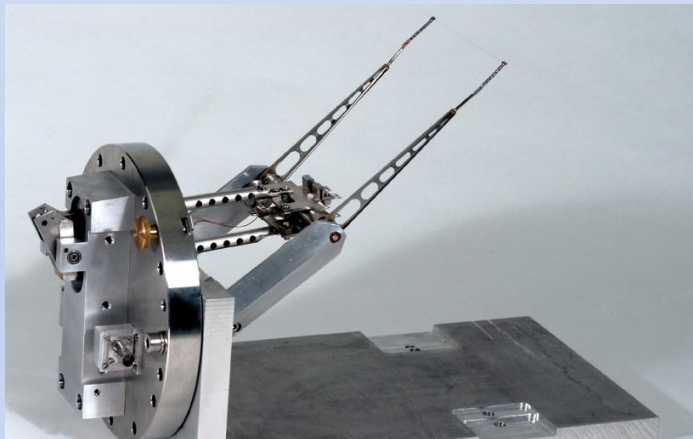
More than 200kms of beamline requiring > **50 000 instruments**

T. Lefevre

# What do we need to measure?

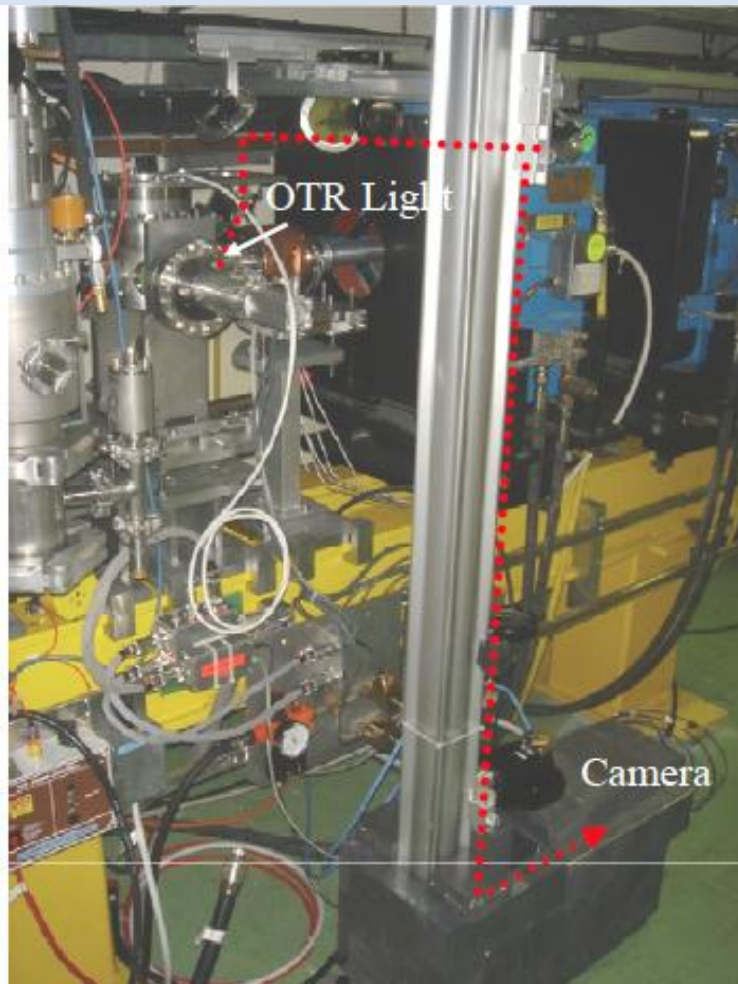


Position; Current; Energy; Transverse Profile (emittance and TWISS parameters); Longitudinal Profile (Bunch length, Bunch shape, Bunch spacing); Beam Loss ...





# What skills are needed?



C. Welsch

- Beam Instrumentation == “eyes” of the machine operators
  - i.e. the instruments that observe beam behaviour
  - An accelerator can never be better than the instruments measuring its performance!
  
- What does work in beam instrumentation entail?
  - Design, construction & operation of instruments to observe particle beams
  - R&D to find new or improve existing techniques to fulfill new requirements
  - A combination of the following disciplines
    - Applied & Accelerator Physics;
      - Material science, thermodynamics, Electro-magnetism, Optics, Mechanics, Electronics, Nuclear Physics, Controls and Software engineering ...
  - A multi-disciplinary field!



## → What do we need to measure?

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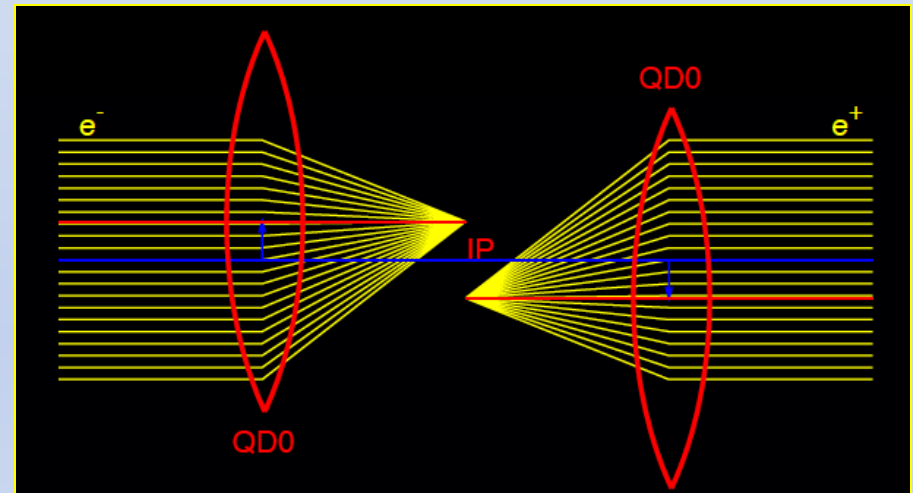
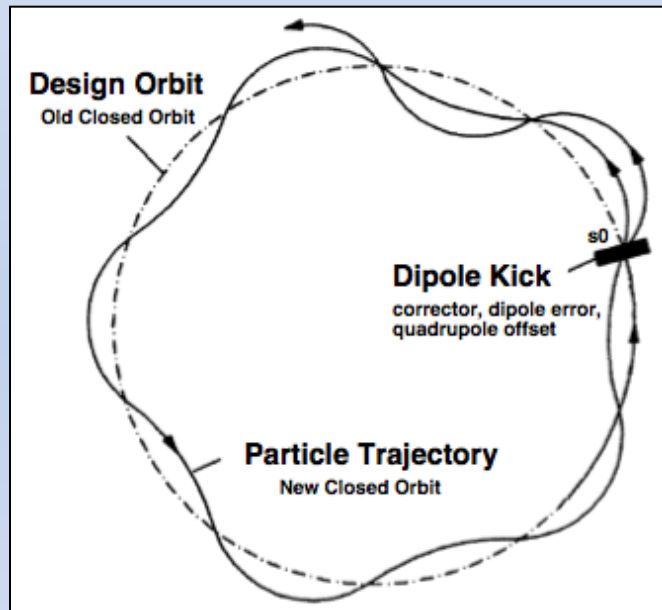
First  
Lecture

Second  
Lecture

## → Discuss diagnostics developments needed for new machines

# Position Measurements

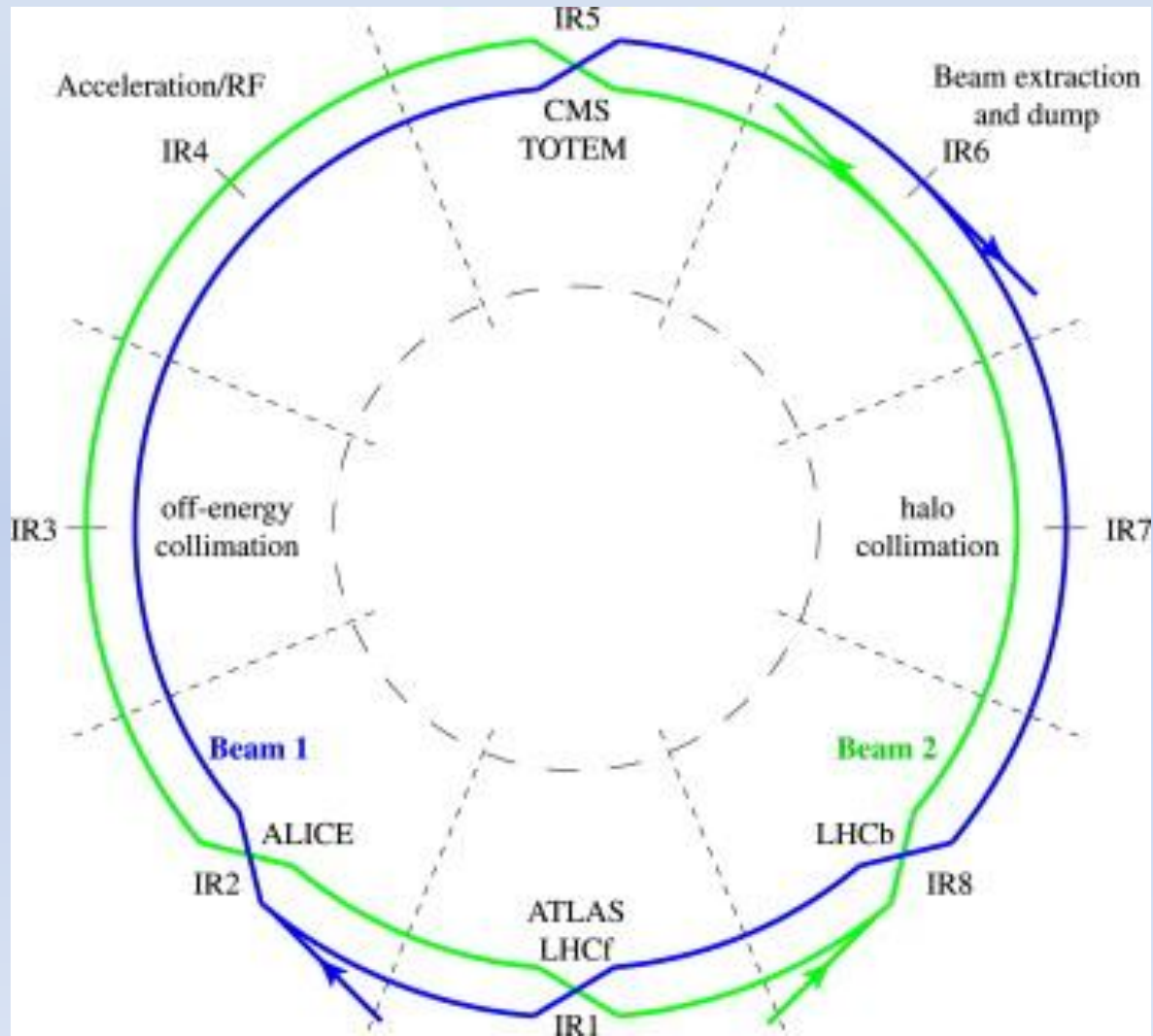
- In a modern storage ring particles travel billions of km within  $< 100 \mu\text{m}$  of the ideal orbit
- In linear colliders nano-beams from independent accelerators must be made to collide
- Must employ stability principles for beam dynamics and accurate components and diagnostics



QD0 should be stabilized to  $0.15 \text{ nm}$  for frequencies above  $4 \text{ Hz}$

- At the SLS 73 “button” BPMs measure orbit deviations to better than  $1 \mu\text{m}$  @  $4 \text{ kHz}$  sampling rate.
- LHC BPM resolution  $\sim 5 \mu\text{m}$  (depending on location in machine & measurement purpose)
- CLIC BPMs, resolution requirements:
  - $100 \mu\text{m}$  (injectors) down to  **$3 \text{ nm}$  (at IP)**

# LHC Beam Diagnostics

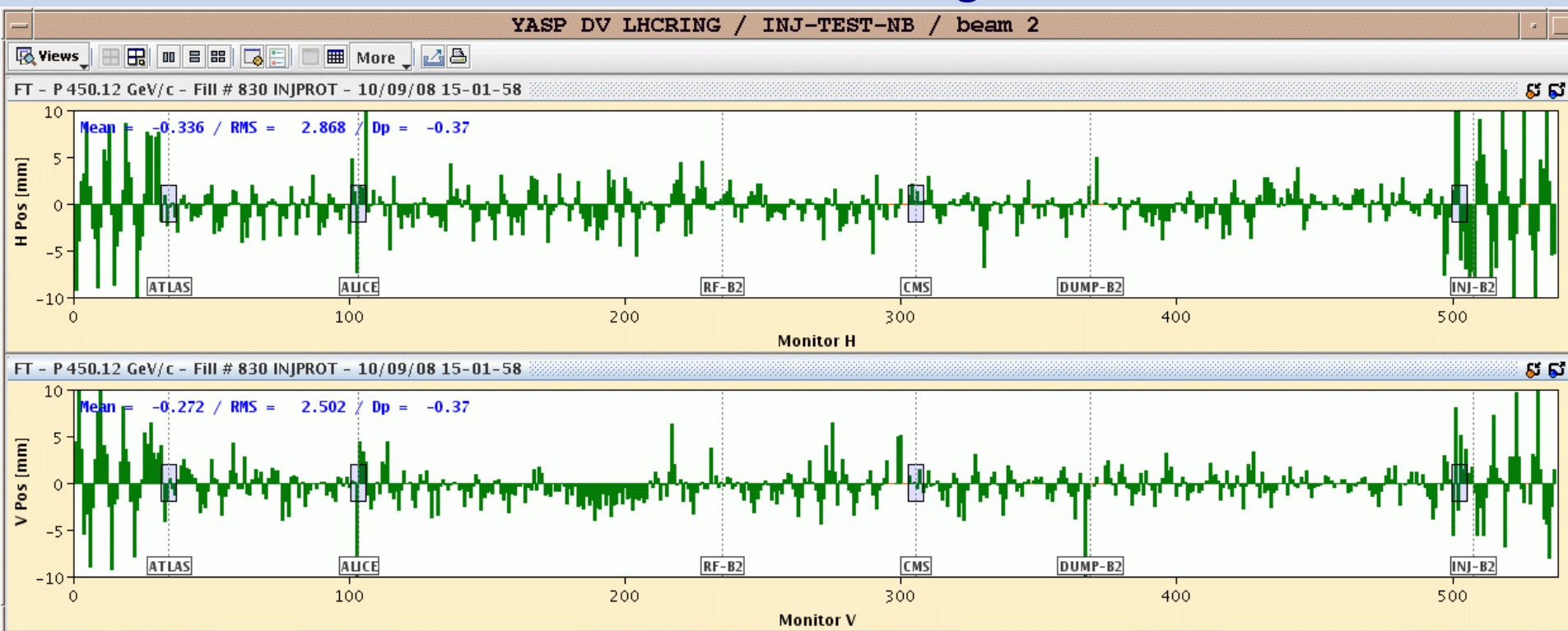


# Position Measurement for Beam Threading

- Threading the beam round the LHC ring
  - One beam at a time, one hour per beam.
  - Collimators were used to intercept the beam (1 bunch,  $2 \times 10^9$  protons)
  - Beam through 1 sector (1/8 ring)
    - correct trajectory, open collimator and move on.

BPM availability ~ 99%

Beam 2 threading



R. Jones

# Transfer matrix between two points

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The transfer matrix between two arbitrary point in the machine

$$\begin{pmatrix} x \\ x' \end{pmatrix}_2 = M_{1 \rightarrow 2} \begin{pmatrix} x \\ x' \end{pmatrix}_1$$

**Measure:**

- **Position**
- **Angle**

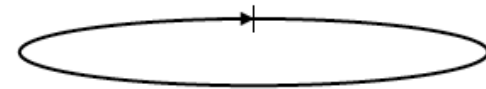
With beam position monitor at point 1 (2) using at least 2 beam position monitors

Adjust  
machine  
parameters

# Stability of transverse (betatron) oscillations

The transfer matrix of a beamline that consists of elements with individual matrices  $M_1, M_2, \dots, M_n$   $\mathbf{M}_{\text{tot}} = \mathbf{M}_n \cdot \dots \cdot \mathbf{M}_2 \cdot \mathbf{M}_1$  (N.B. the order in which matrices are multiplied!)

- Full turn matrix  $M$



$$\begin{pmatrix} x \\ x' \end{pmatrix}_n = M^n \begin{pmatrix} x \\ x' \end{pmatrix}_0$$

- After  $n$  turns must remain finite for arbitrarily large  $n$

L. Rivkin

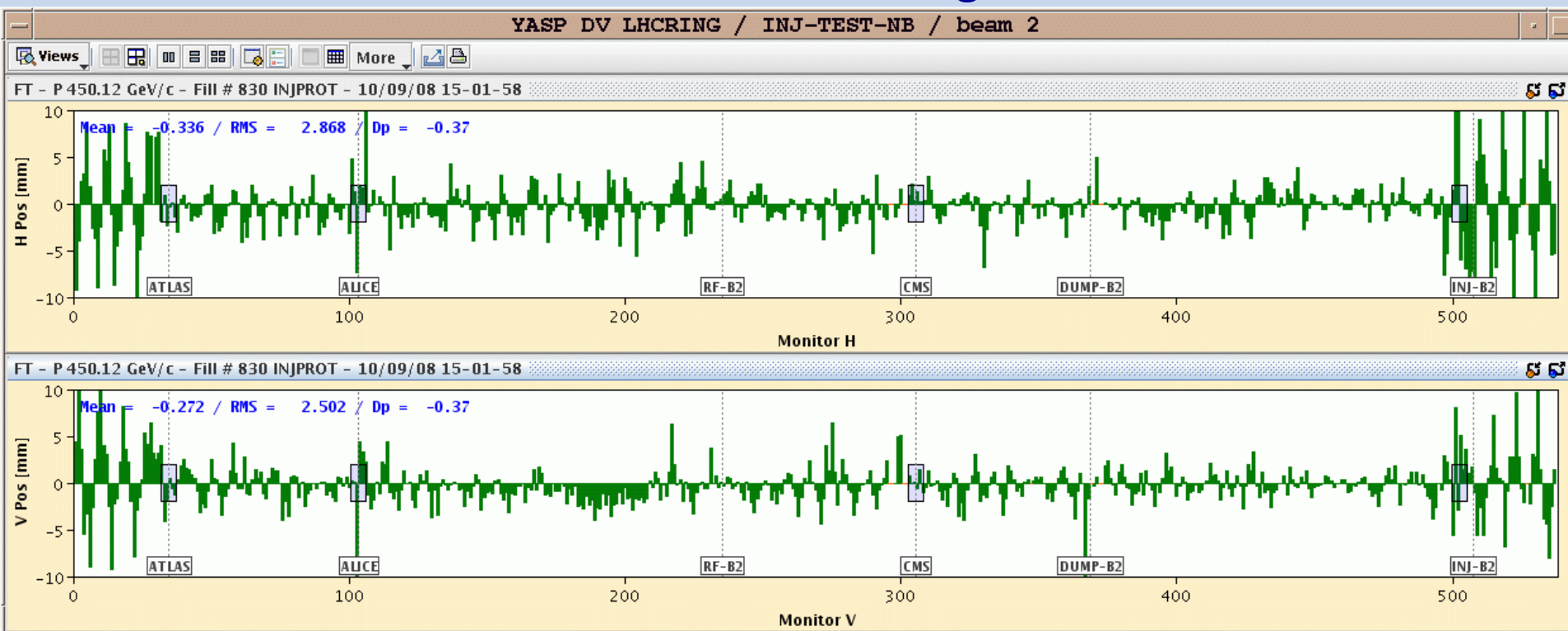


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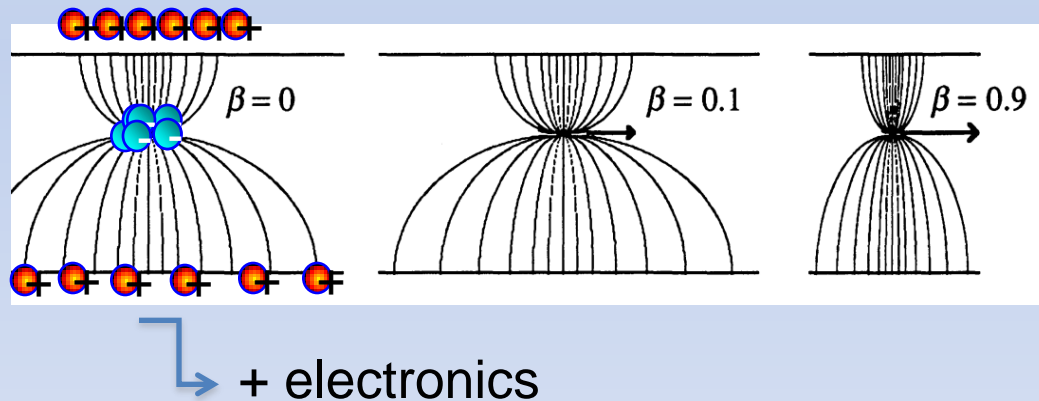
Beam 2 threading



R. Jones

## Physics : Electricity and magnetism

- Relativistic beams:
  - Measure the relative difference in the strength of the electric field (image charge density on beam pipe) moving in disk with and at right angles to the beam's velocity direction
  - (other method's too – e.g. cavity BPMs)



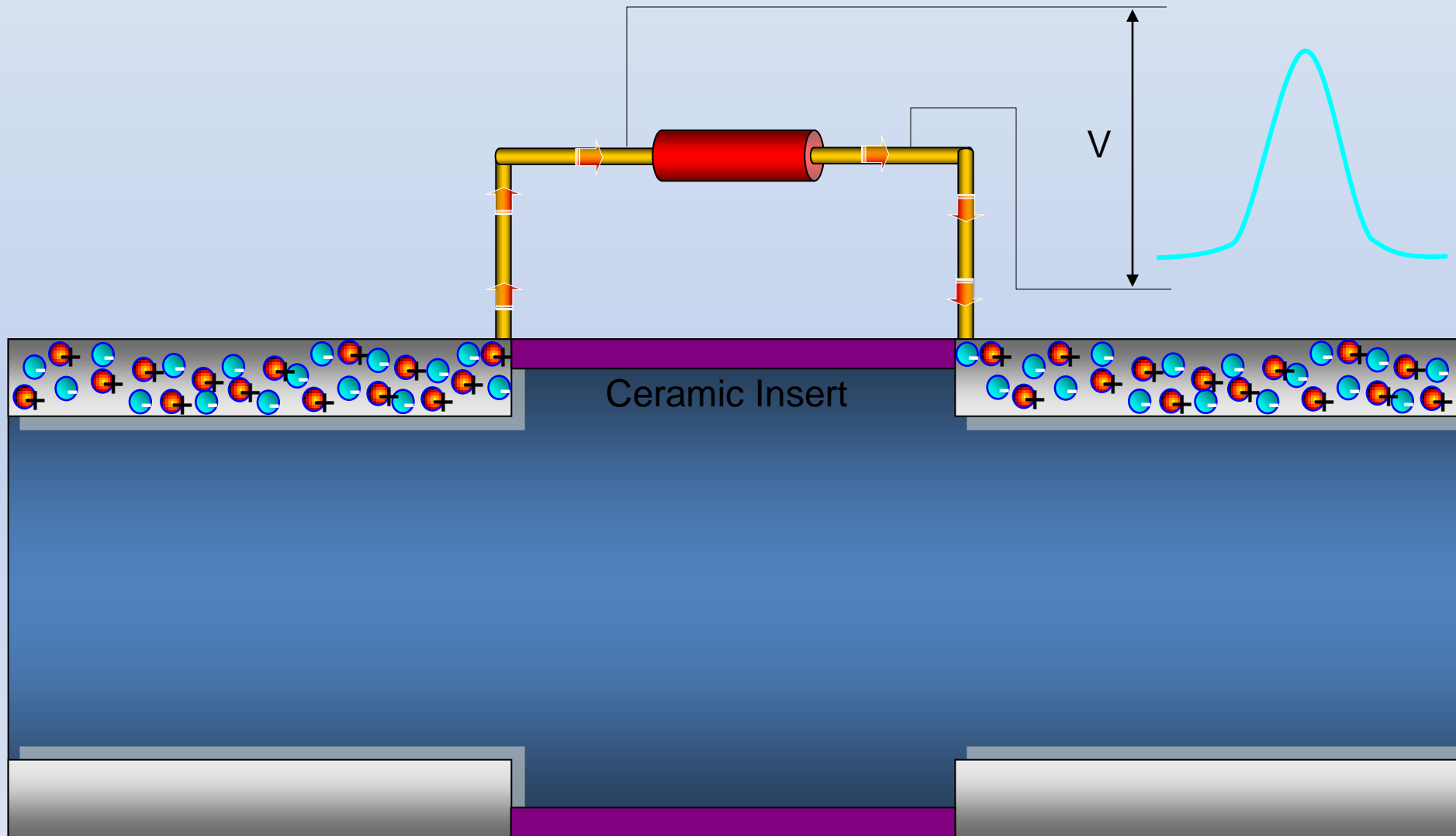
Basic principle exploited in inductive and electrostatic BPMs and wall current monitors

# Measuring Beam Position – The Principle



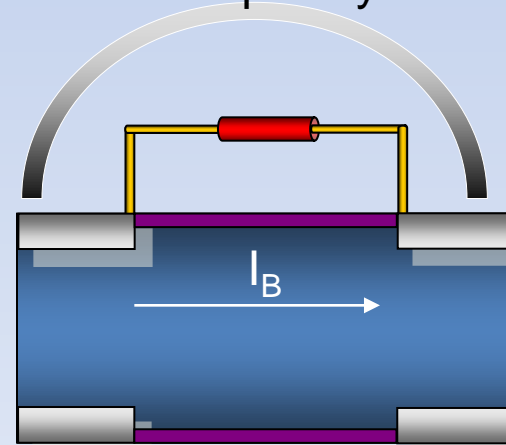
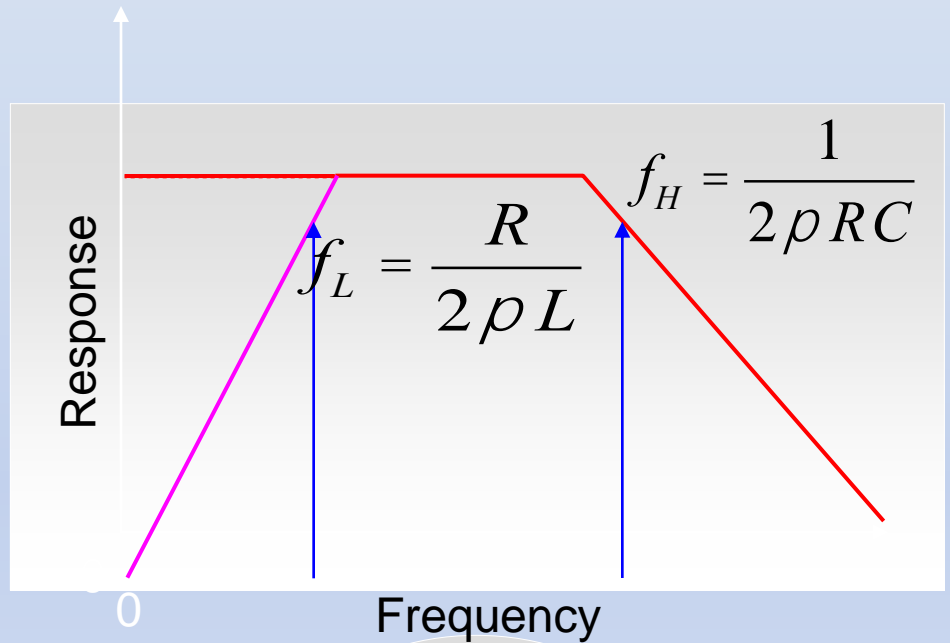
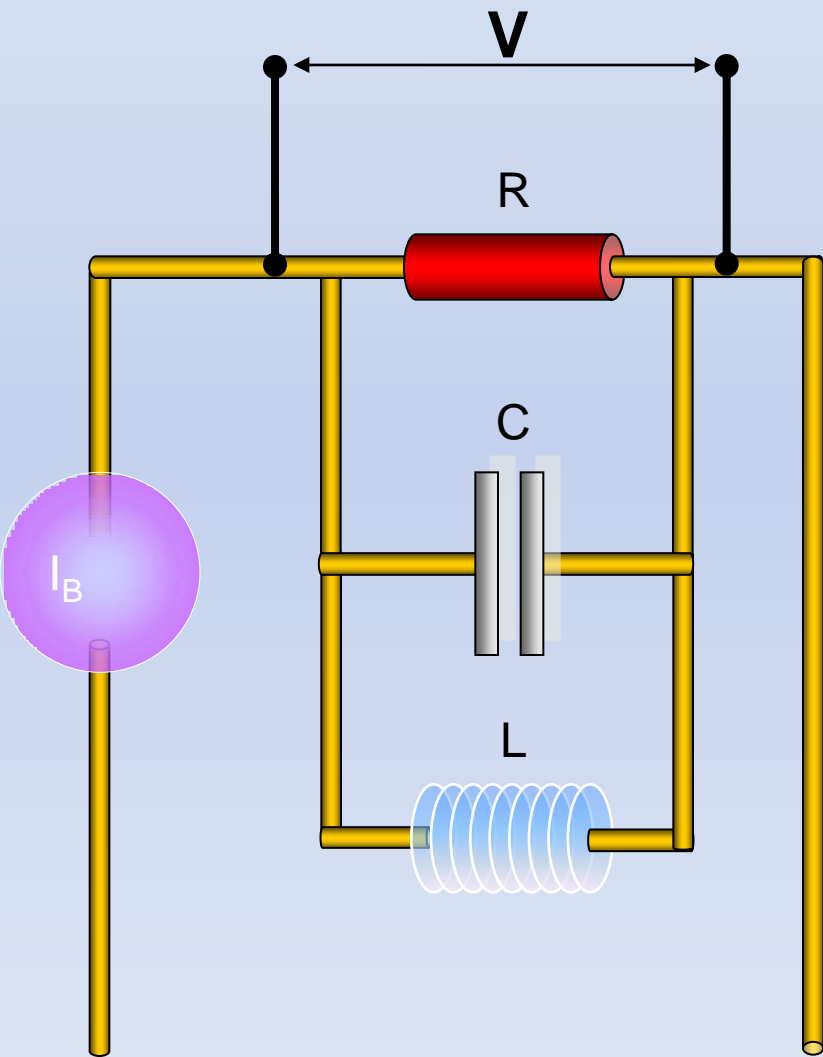
Slide by R. Jones

# Wall Current Monitor – The Principle

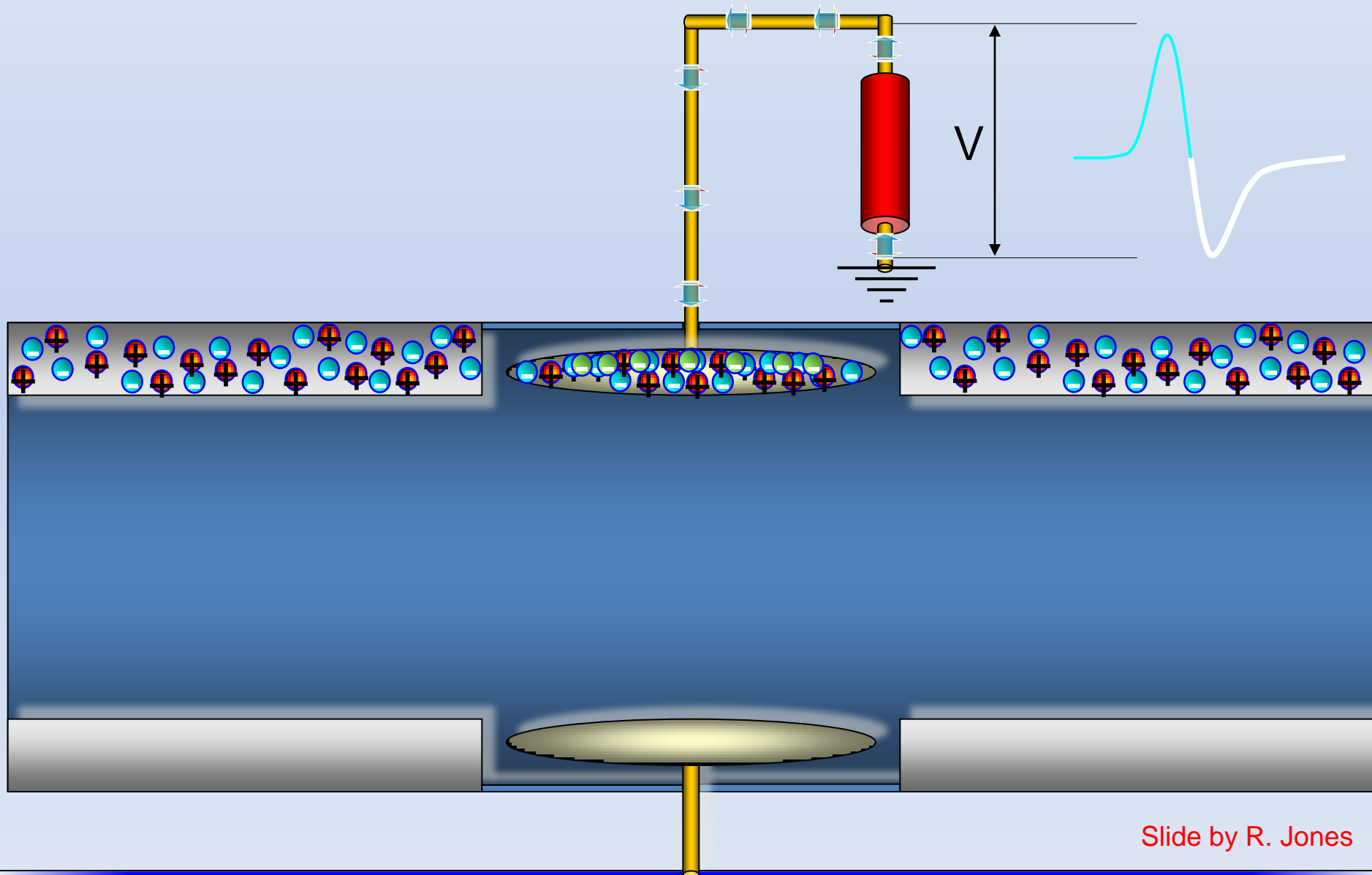


Slide by R. Jones

# Wall Current Monitor – Beam Response



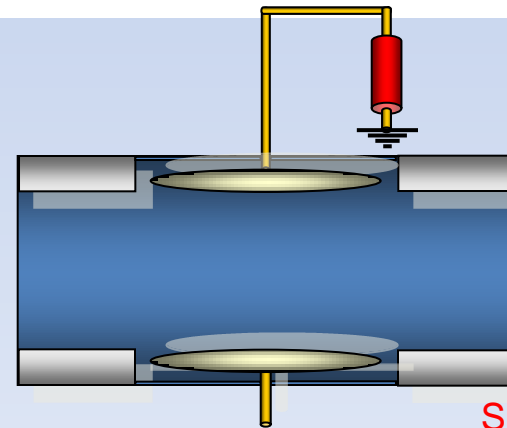
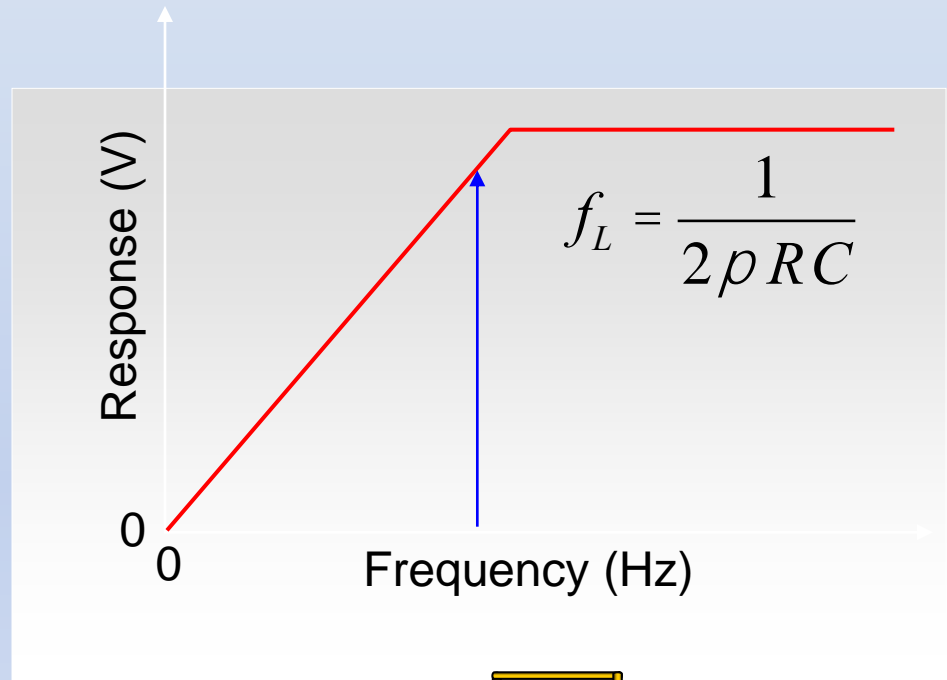
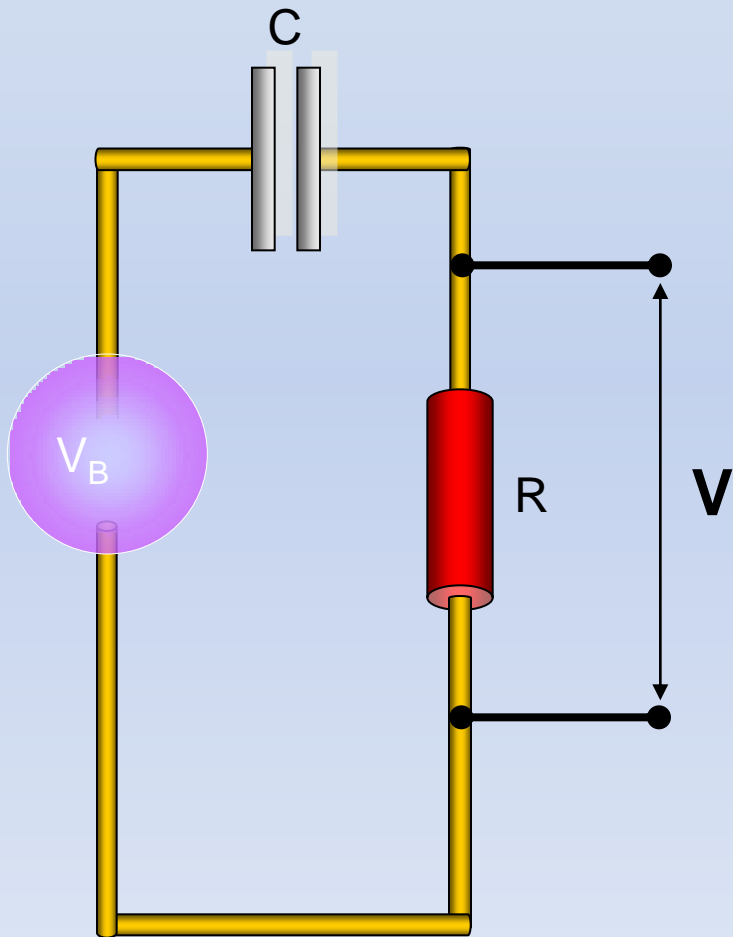
Slide by R. Jones



Slide by R. Jones



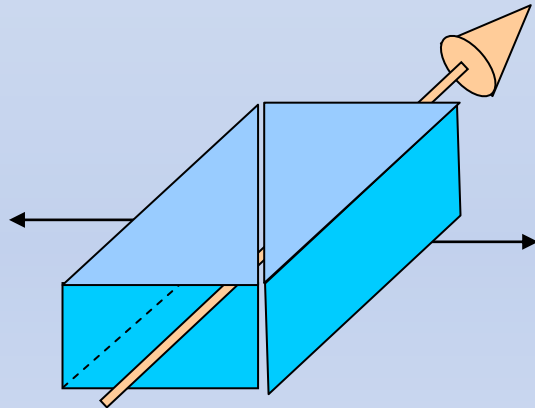
# Electrostatic Monitor – Beam Response



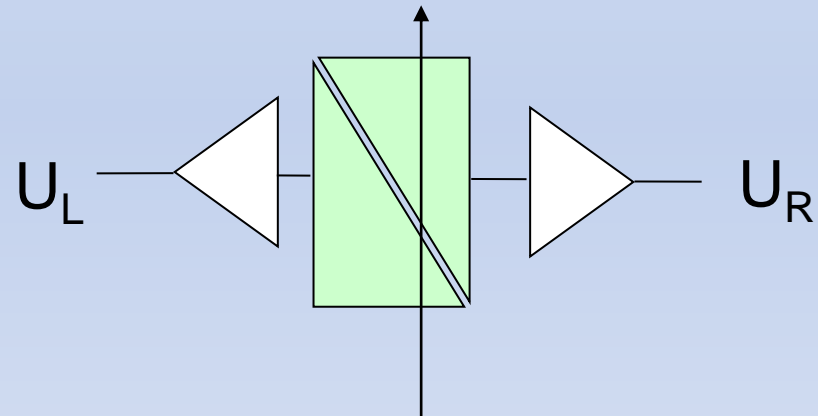
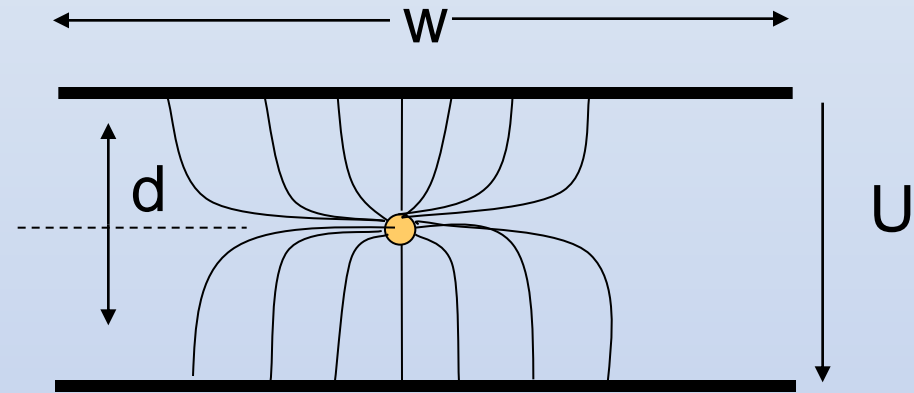
Slide by R. Jones

# Shoebox pick-up

Bunch length should be smaller than the shoebox length,  $w$  to be linear



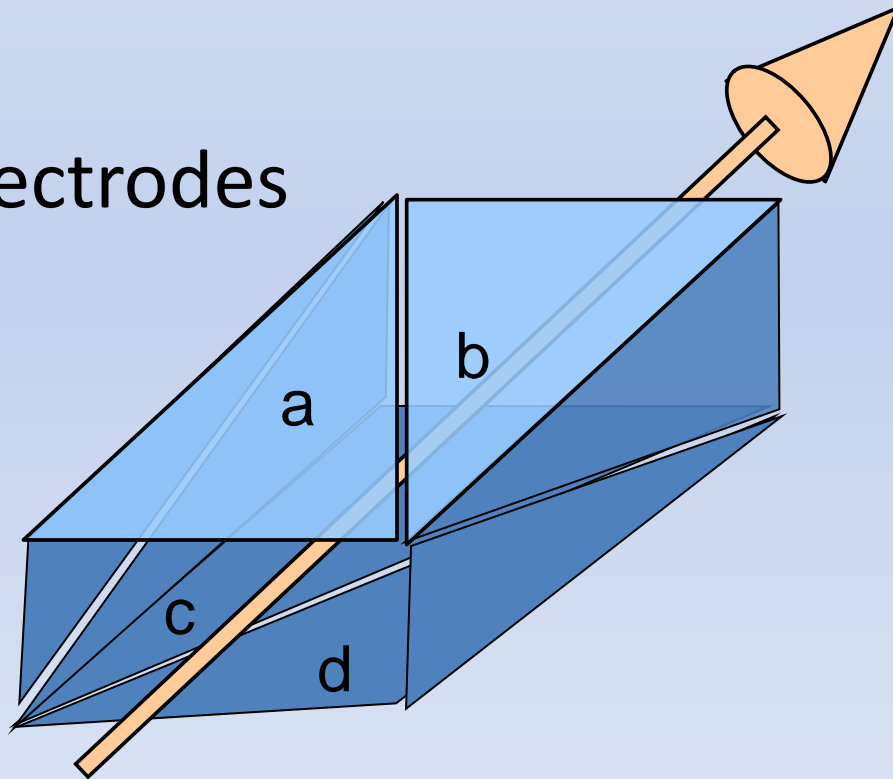
Linear cut through a shoebox



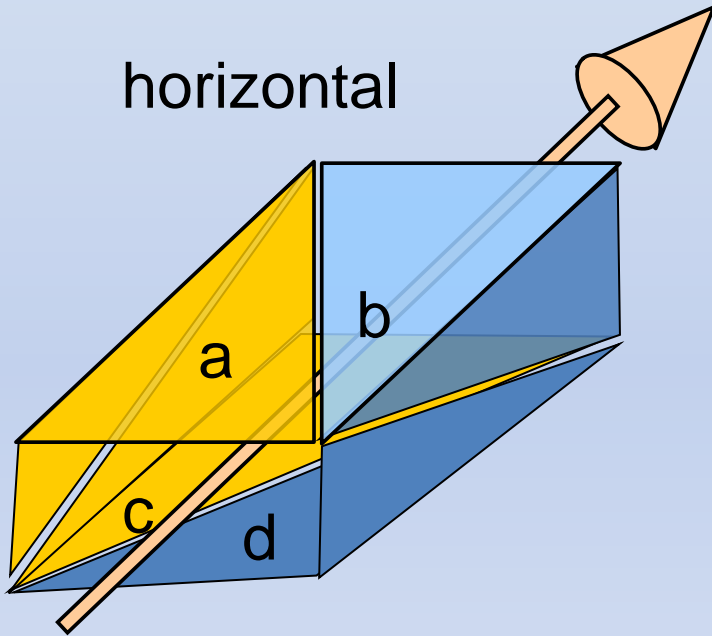
$$X \propto \frac{U_L - U_R}{U_L + U_R} = \frac{D}{S}$$

# Doubly cut shoebox

- Can measure horizontal and vertical position at once
- Has 4 electrodes

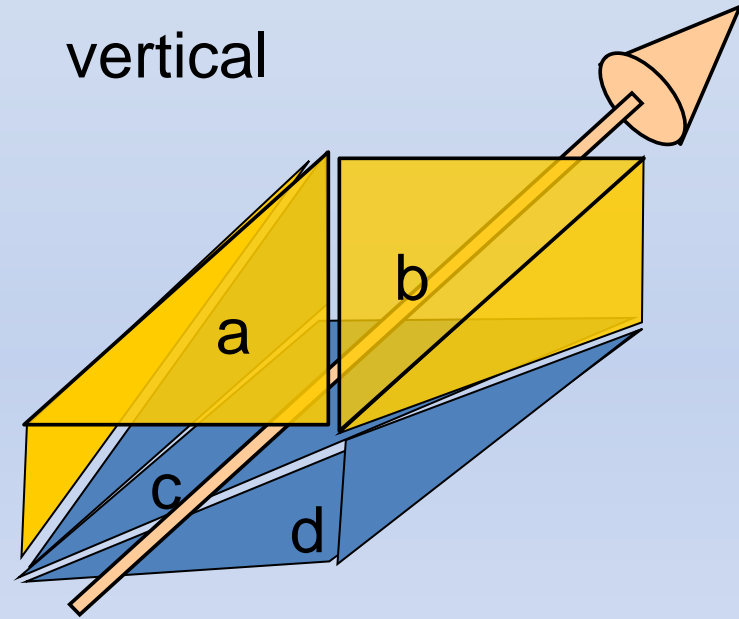


horizontal



$$X = \frac{(U_a + U_c) - (U_b + U_d)}{SU}$$

vertical



$$Y = \frac{(U_a + U_b) - (U_c + U_d)}{SU}$$

Slide by R. Jones

## Important Effects:

- Non-linearity
- Geometrical center  $\neq$  electrical center
- Errors in difference of small numbers
  - Amplification before sum and difference
- System bandwidth –
  - Convolution of the transfer impedance and frequency response of the cables, amplifier, filters, ADC
- Saturation
- Sampling resolution of ADC
- Noise on electronics
- Average position measurement or single shot
- Goodness of calibration circuit
- Cross talk between adjacent electrodes

$$X = \frac{1}{S_x} \frac{(U_a + U_c) - (U_b + U_d)}{SU} + d_x$$

$$Y = \frac{1}{S_y} \frac{(U_a + U_b) - (U_c + U_d)}{SU} + d_y$$

## Important Concepts:

- Accuracy, Resolution, Analog Bandwidth, Acquisition bandwidth, Dynamics range, Signal-to-noise ratio

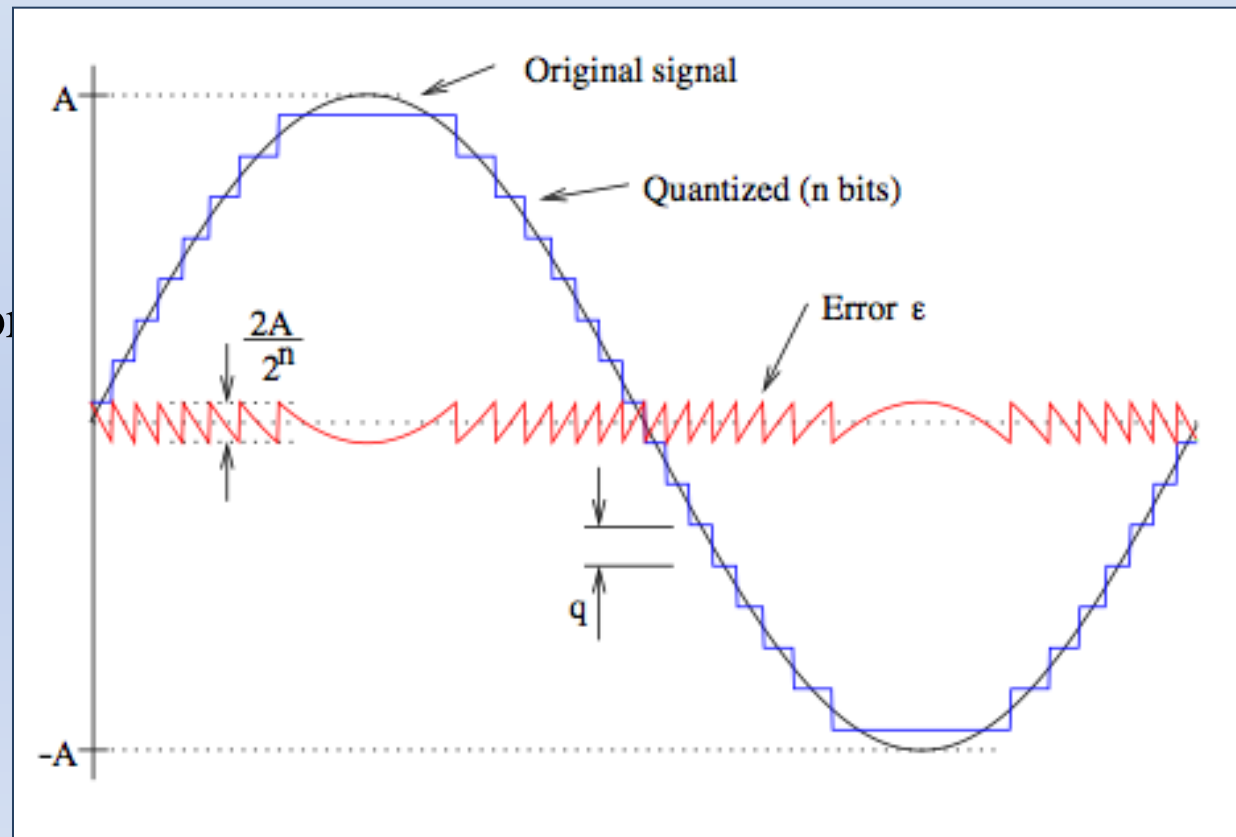
Excellent Lecture “Analog to Digital” at CAS2008 School by Belleman

## Amplitude Quantization

$$q = \frac{2A}{2^n} = A \cdot 2^{-(n-1)}$$

Maximum quantization error

$$e = \frac{\pm q}{2} = A \cdot 2^{-n}$$

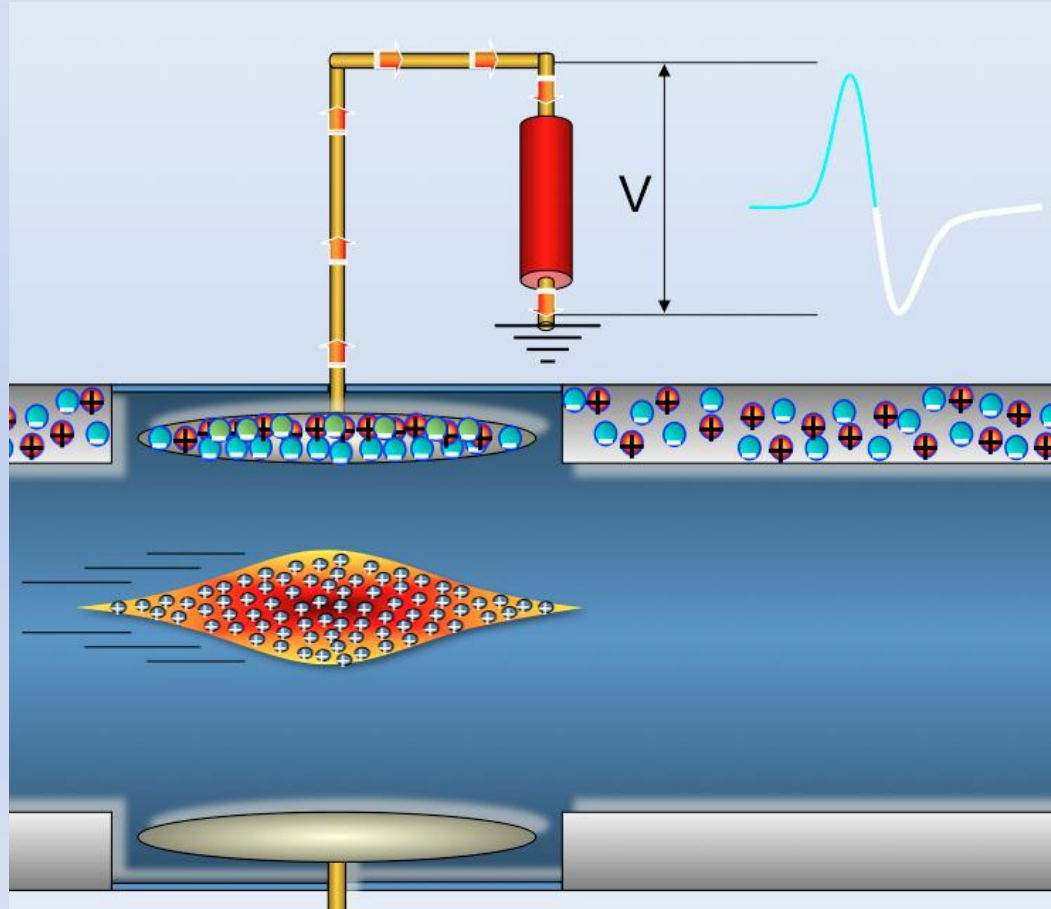


- Digital electronics - contributes to the resolution
- Appears now in most diagnostics
- Important subject in itself – requires dedicated lecture



# Current Measurements, cont ..

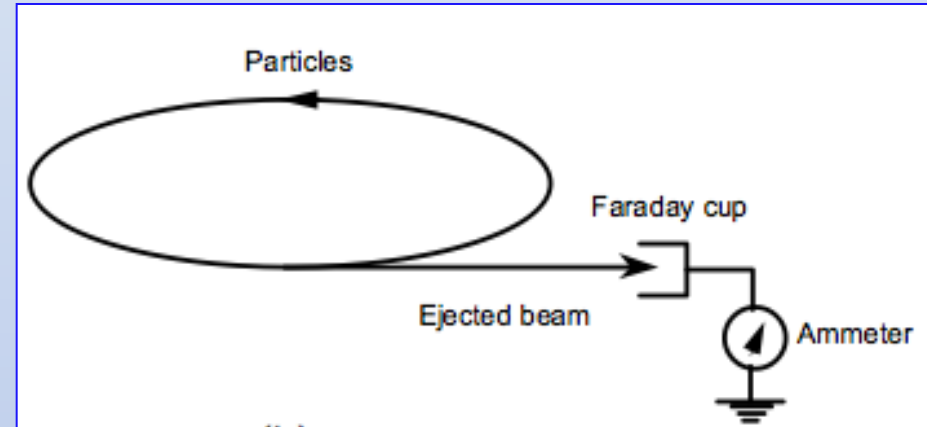
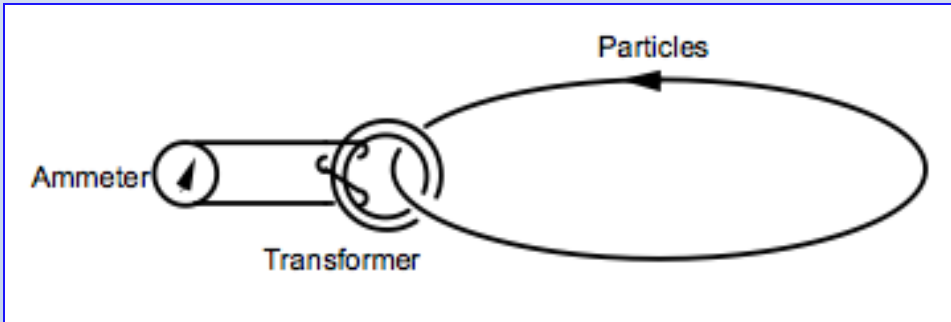
From this BPM signal – how do you measure the current?



Any other way to measure the current? ....

# Current Measurements, cont ..

Rate at which charge passes a fixed point

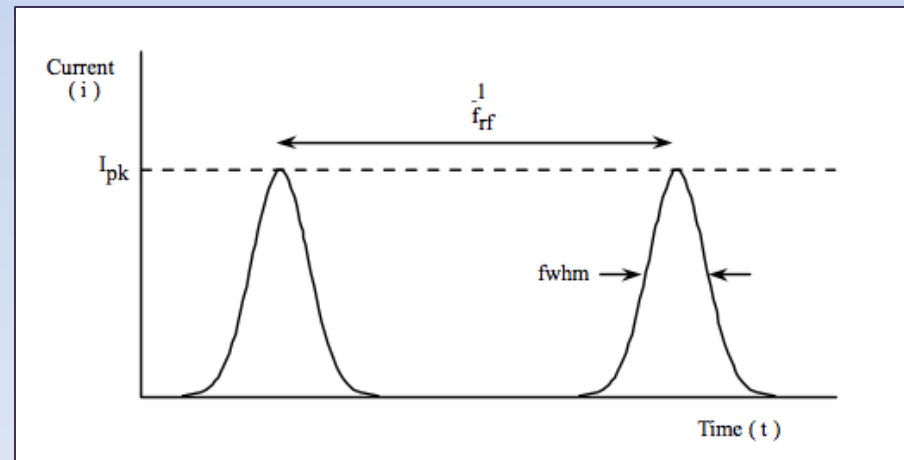


## DC current transformer

(Measures magnetic field produced by the current)

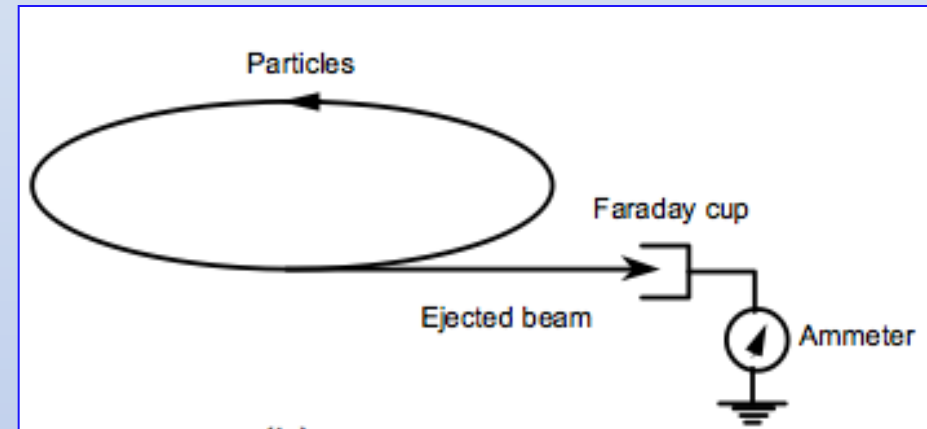
## Faraday cup

(measured the total beam charge)



# Current Measurement – Faraday Cup

- At very low energies and low intensities the Faraday Cup is an often used device for intensity measurements.
- It acts as a beam stopper and is therefore fully destructive
- Very low intensities down to a few pA can be measured, even for a DC beam, with low noise current to voltage amplifiers

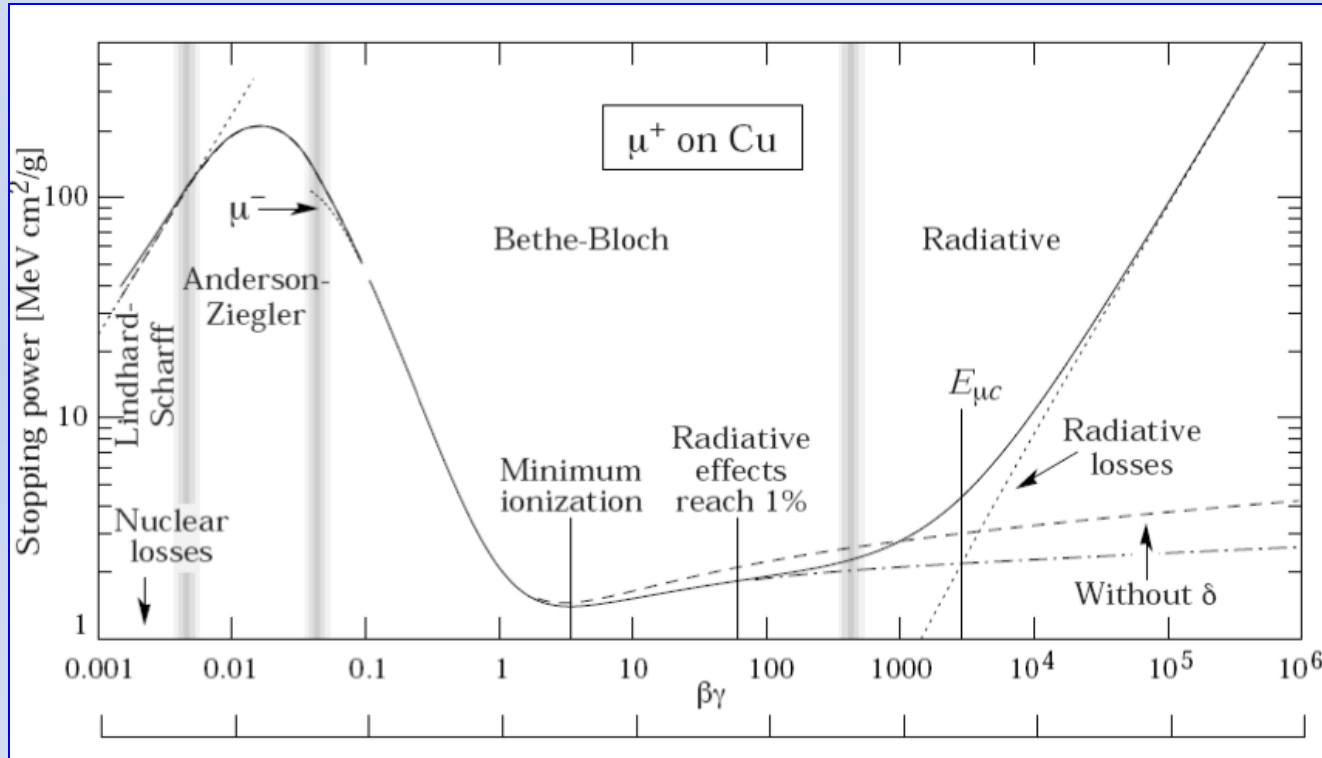


# Current Measurement – Faraday Cup

## Physics : Understanding particles interact with matter

Measure directly the stopped charge as a current in a metallic block

To measure the full charge → must stop the full beam



## Bethe Bloch formula: Stopping Power $dE/dz / \rho$

$$-\frac{dE}{dx} = 4\rho N_A r_e^2 m_e c^2 \frac{Z_T}{A_T} r \frac{Z_p^2}{b^2} \left[ \ln \frac{2m_e c^2 g^2 b^2}{I} - b^2 \right]$$

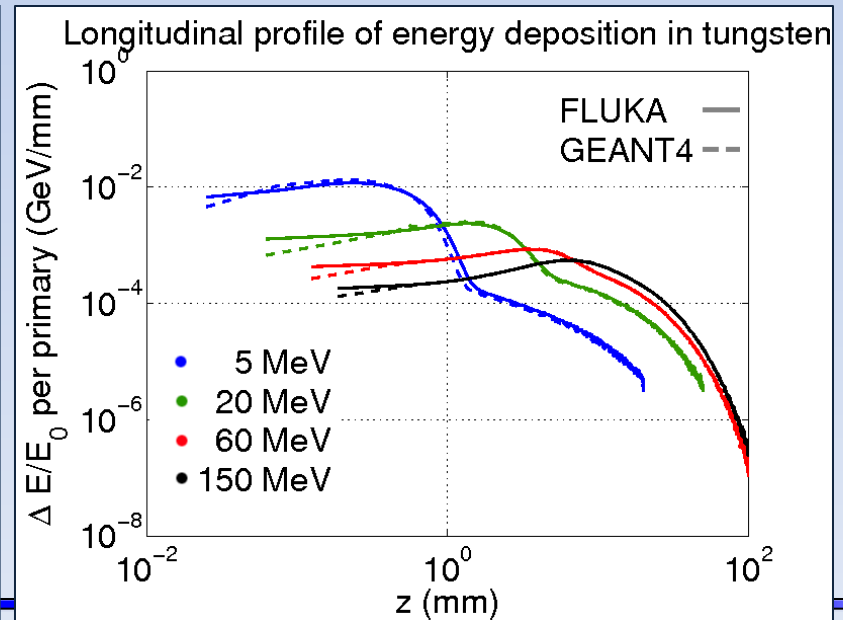
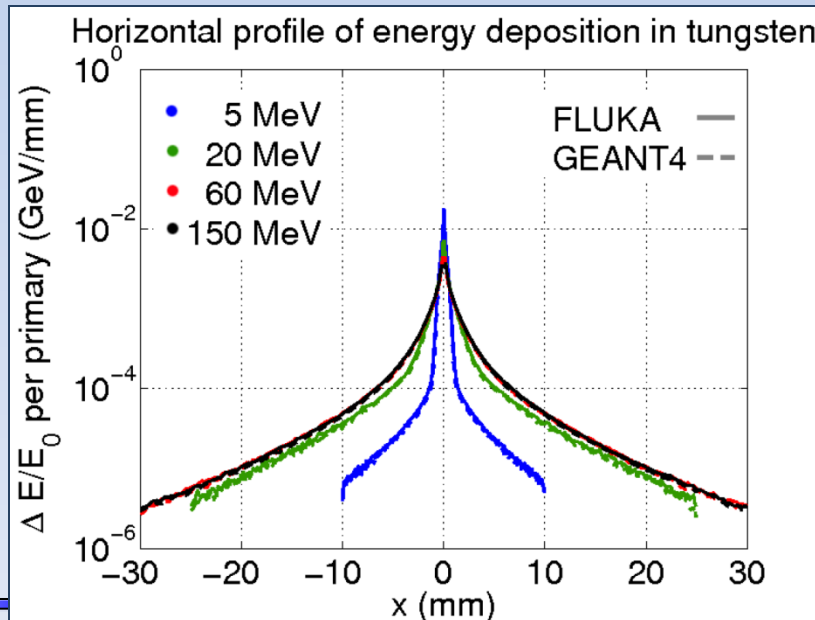
## Variables in design:

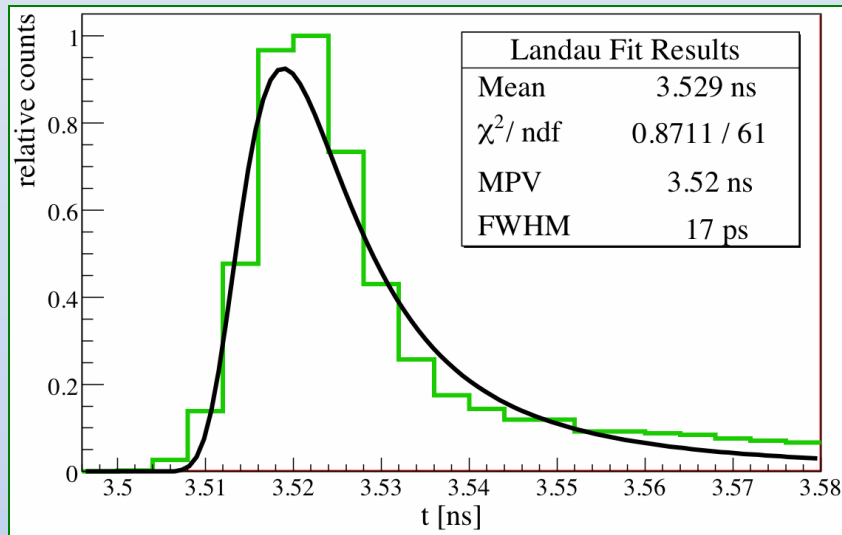
- $\rho$ : material density
- $A_T$  and  $Z_T$ : the atomic mass and nuclear charge
- $Z_p$ : particle charge
- $\beta$ : the particles velocity and  $\gamma$   $g = \frac{1}{\sqrt{1 - \beta^2}}$

## Detector Size:

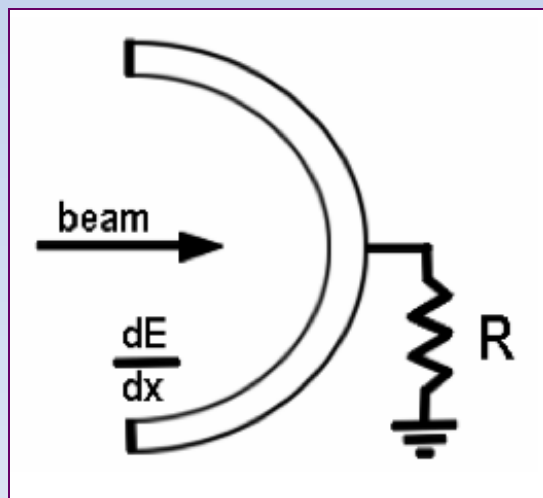
Chose conducting material to fully the particles and contain the beam shower

Example for various electron beam energies into a tungsten sample



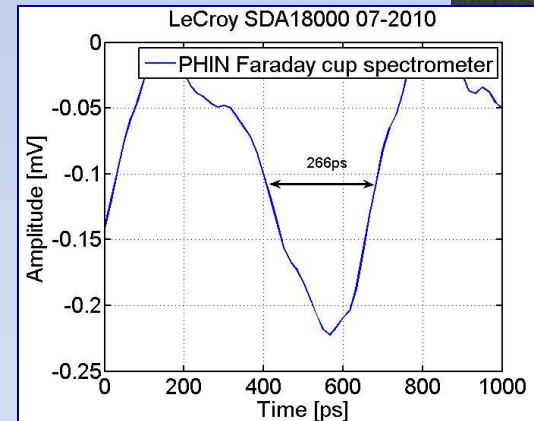
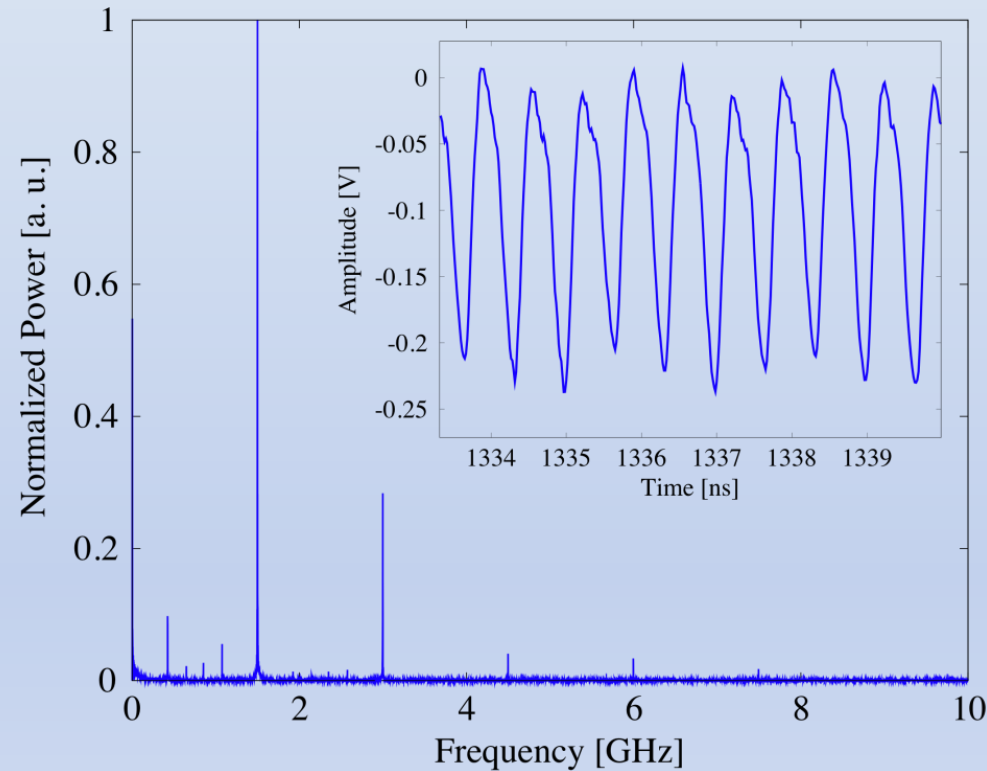


Simulation of time to stop particles GEANT 4



- Beam charge converted into a current
  - The voltage measured across resistor R to ground
- The time response** → design of signal transmission line:
- Resistance R
  - The capacitance C of the cables ( $\sim 100\text{pF/m}$ )
  - The inductance H of the cables ( $\mu\text{H/m}$ )
  - The length of the cable
  - Bandwidth of connectors
  - Sampling rate of ADC / scope

# Current Measurement – Faraday Cup – Electron Beam

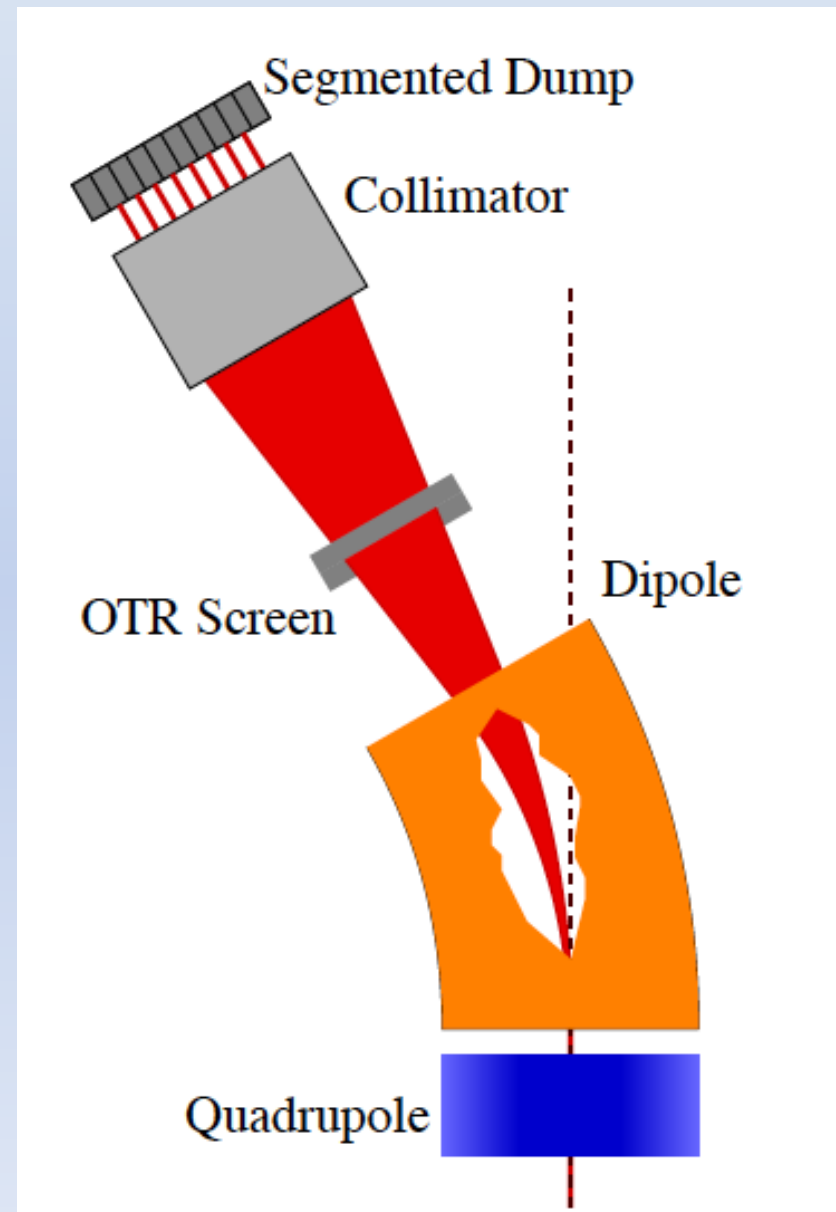
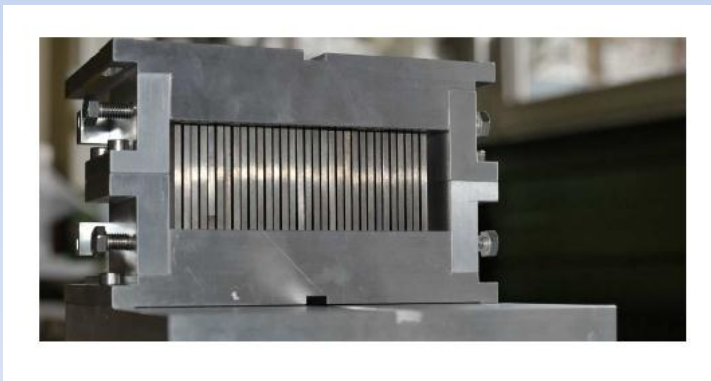


## Scope Trace:

- Bunch current
- Bunch spacing
- Bunch length (in reality it is shorter, limited by the time resolution of the Faraday cup + RC circuit by cables ... need better diagnostics for bunch length measurement)

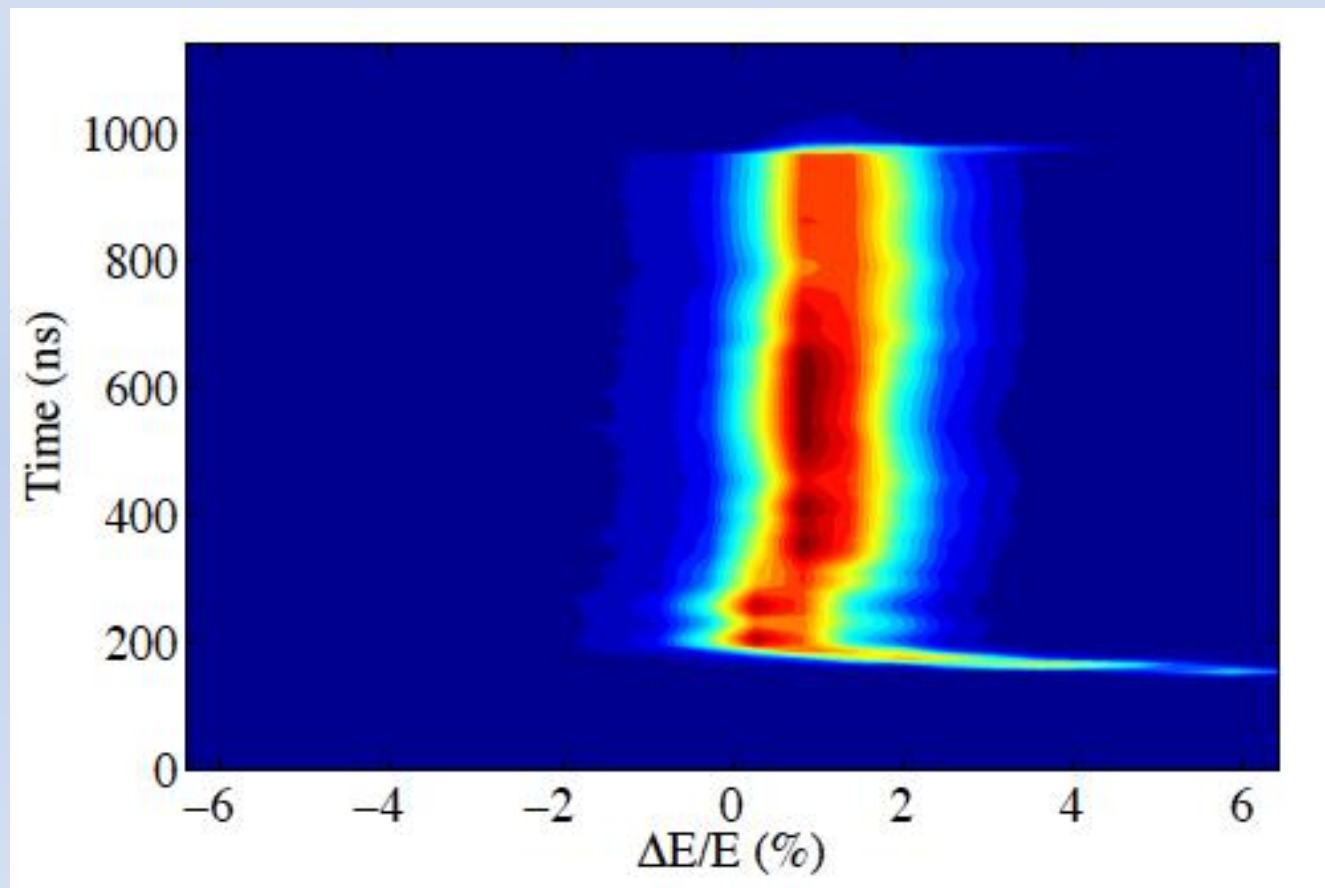


# What if you segmented the faraday cup, and put it after a dipole magnet?

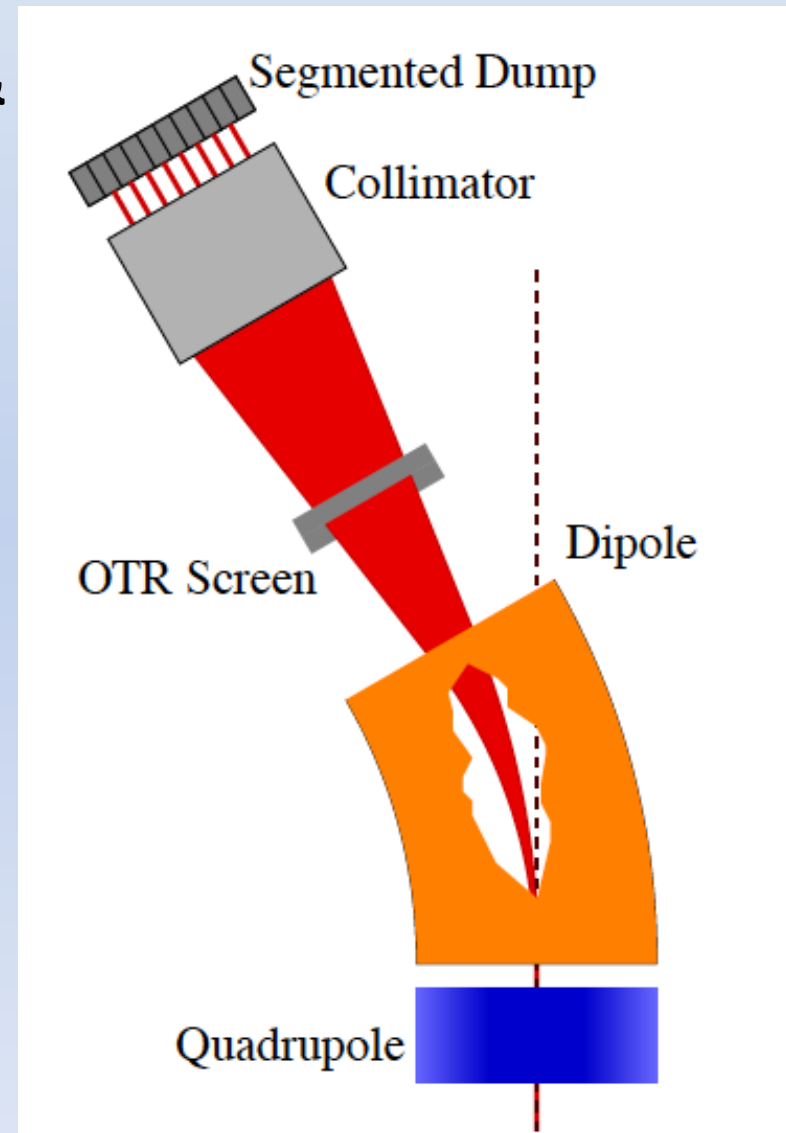
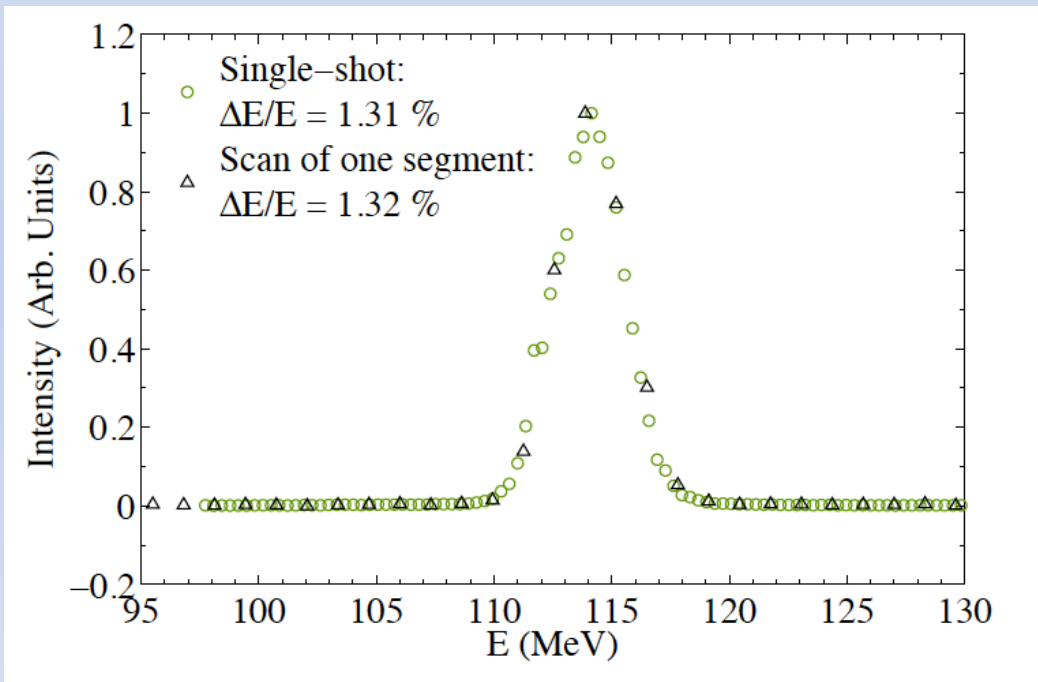


M. Olvegaard et al Nuclear Instruments and Methods in Physics Research A, Volume 683, p. 29-39.

# Measure current as a function of x- position

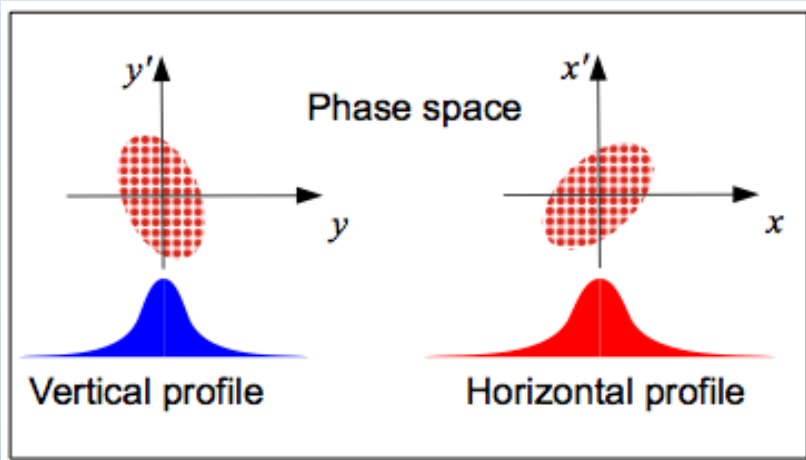


Know the calibration of dipole magnet  
 Measure the average **central energy** &  
**energy spread**



M. Olvegaard et al Nuclear Instruments and Methods in Physics  
 Research A, Volume 683, p. 29-39.

# Transverse Phase Space and Beam Profile



$$X' = \frac{\partial X}{\partial s}$$

$$y' = \frac{\partial y}{\partial s}$$

s is the longitudinal co-ordinate

$e_{x(y)}$  = area in  $[x(y); x'(y')]$  plane occupied by beam particles divided by  $\rho$

$$e_x^{rms} = \frac{1}{b_x(s)} \left[ S_x^2(s) - \left( D(s) \frac{Dp}{p} \right)^2 \right]$$

$$e_y^{rms} = \frac{1}{b_y(s)} \left[ S_y^2(s) \right]$$

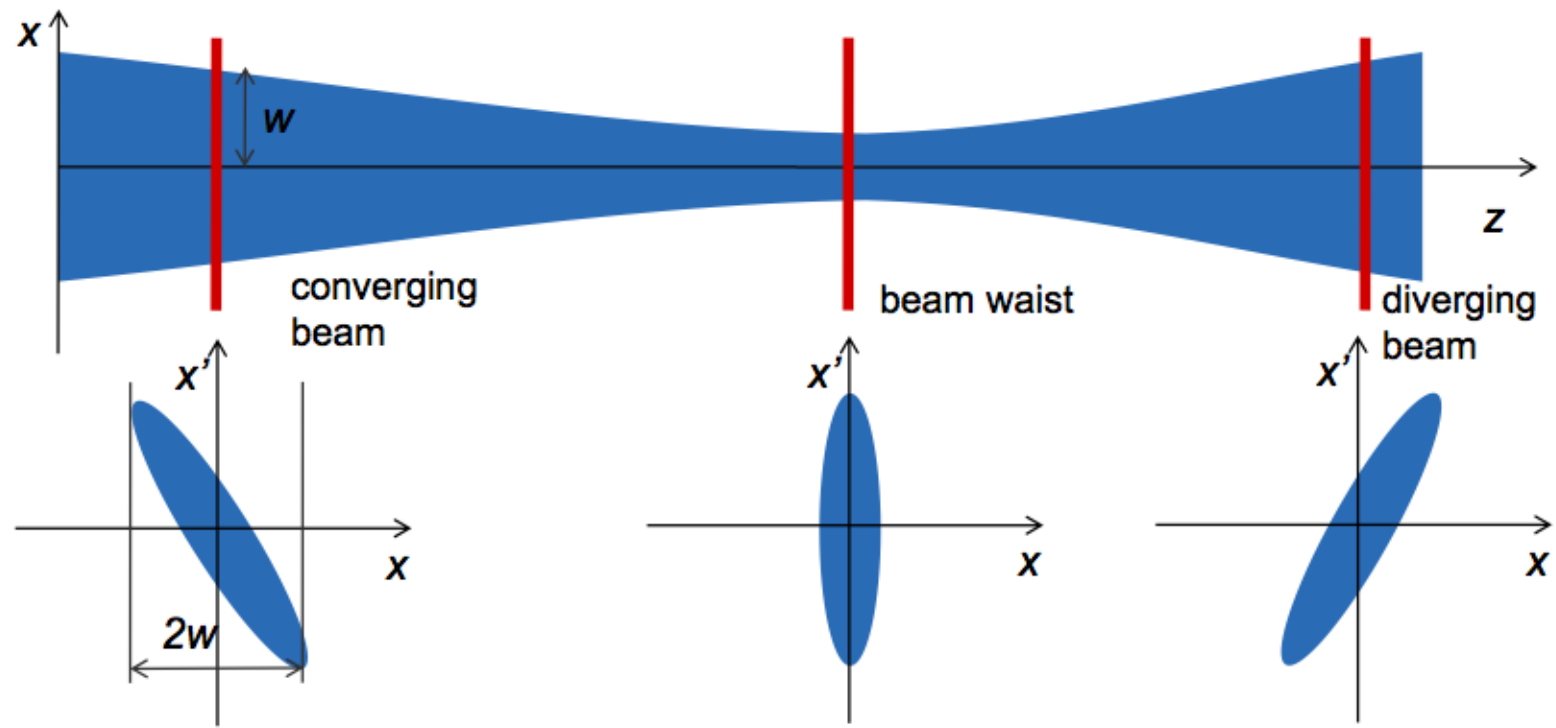
measure:  $S_x^2(s_i)$

know the optics:  $b_x(s_i); D(s) \frac{Dp}{p}$

calculate the emittance

# Transverse Profile

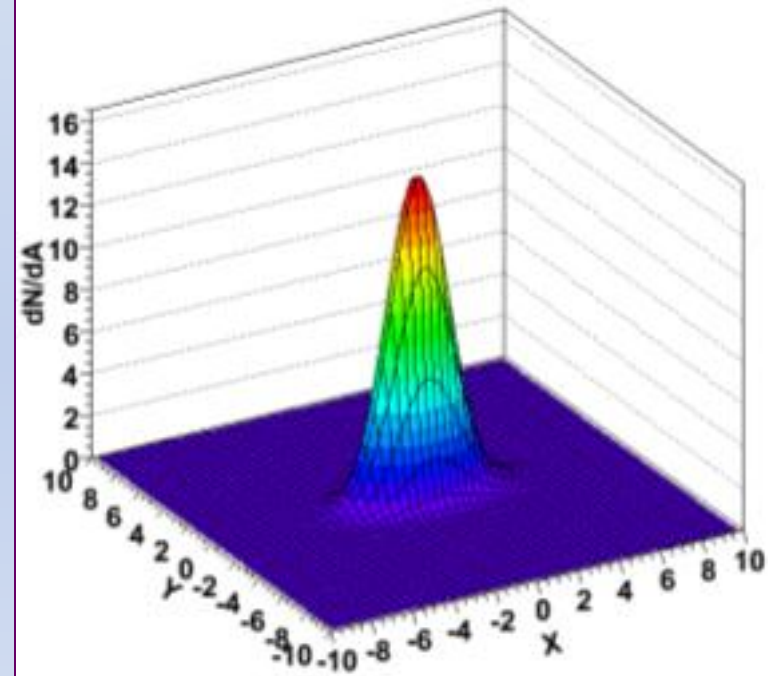
Beam envelope along beamline



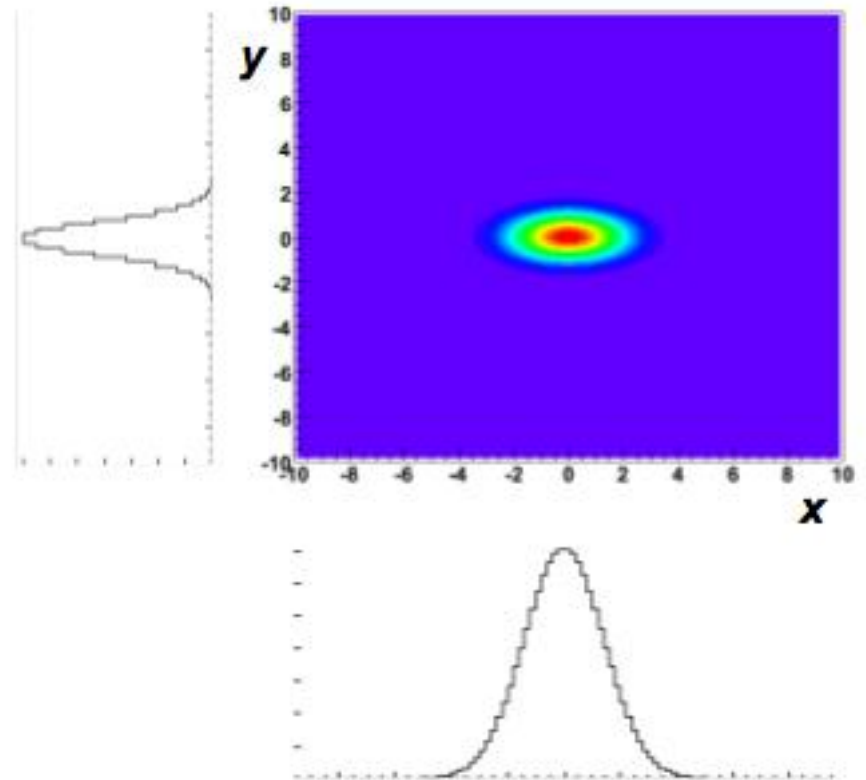
Along a beamline the orientation and aspect ratio of beam ellipse in  $x, x'$  plane varies, but area  $\pi\mathcal{E}$  remains constant

# Transverse Profile Measurement

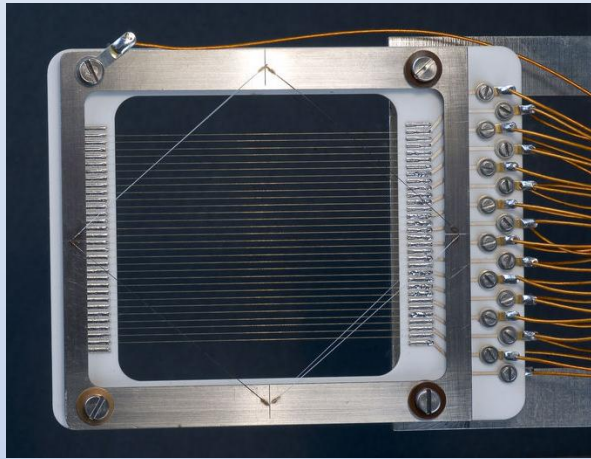
Particles Distribution



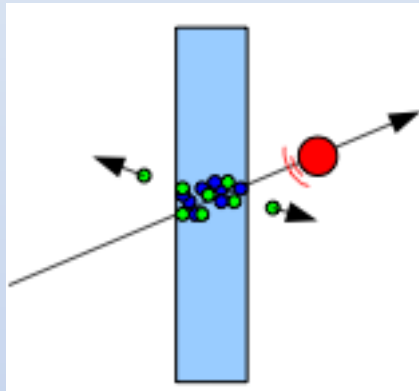
Profiles



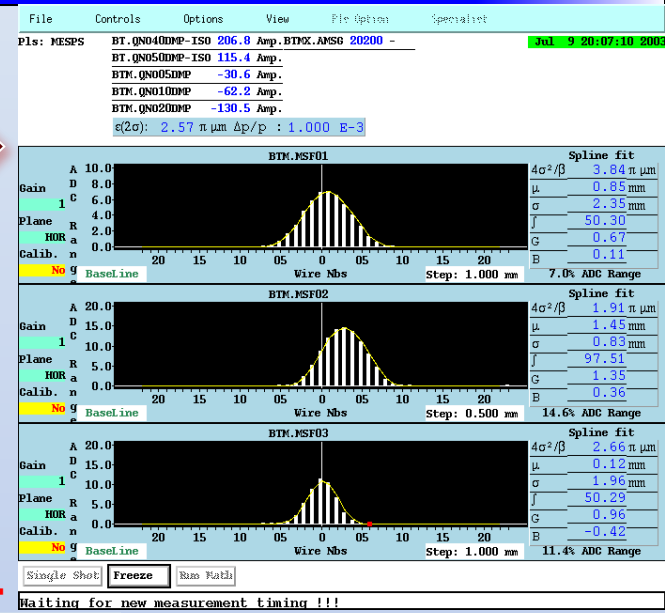
# SEM (secondary emission) grids



**Detector:**  
SEM grid (parallel wires)

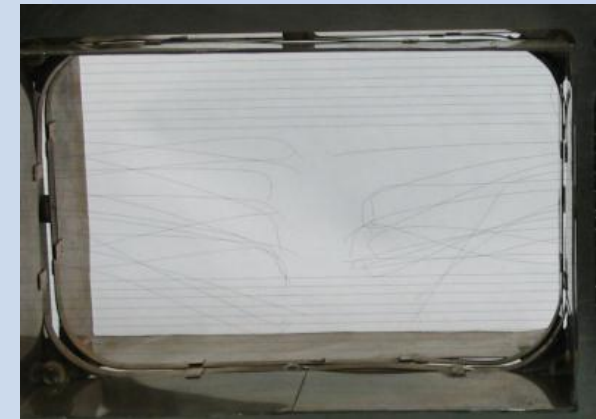


**Physics process:**  
Secondary emission or e-



Waiting for new measurement timing !!!

## Single shot profile



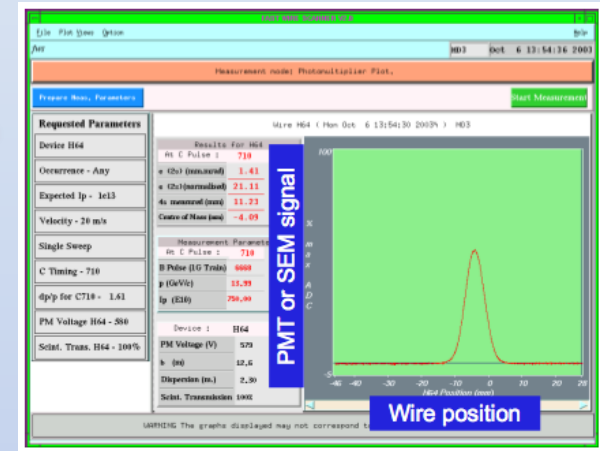
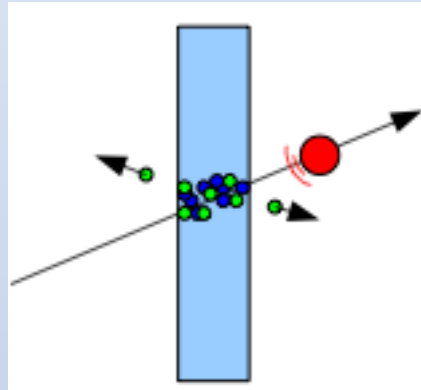
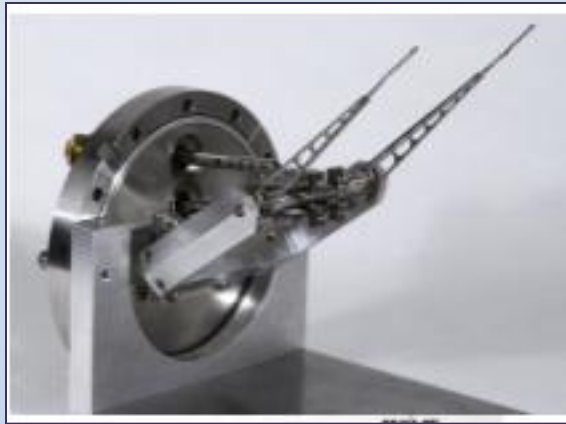
## Complex mechanical assembly:

- Insert grid into the beam, in vacuum
- Single shot
- Profile scale determined by wire position
- Profile sampling determined by distance between wires, wire thickness
- Wires stretched tight

## Wire signal detection:

- Current flowing back onto the ribbons is measured
- Electrons ejected are taken away by polarization voltage
- One amplifier / ADC per channel

# Wire scanner



**Detector:**  
**Wire Scanner**

**Physics process:**  
**Secondary emission or e-**

**Reconstruct transverse profile**

## Complex mechanical assembly:

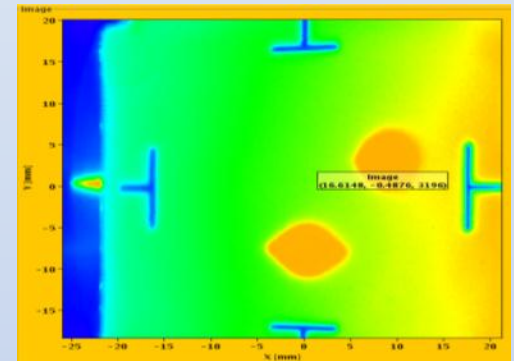
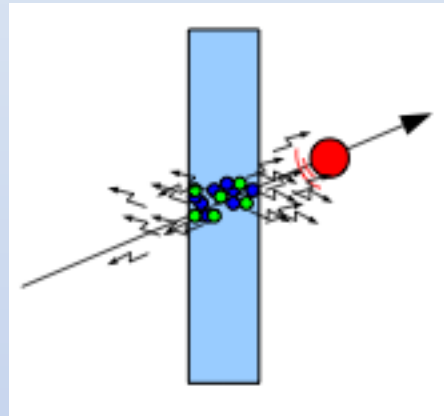
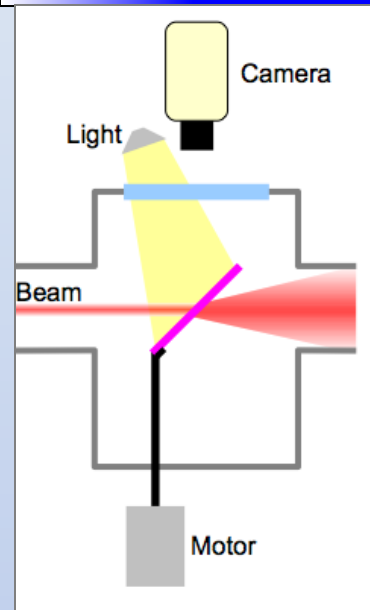
- Scan wire, across beam, in vacuum
- Speeds up to 20 m/s!
- Profile scale determined by wire position
- Profile sampling determined by speed of the wire w.r.t. frequency of beam
- Perturbs the beam, not suited to follow the emittance evolution

## Wire signal detection:

- Either measure the current from wire
- Or deflect (capture) secondary electrons, create photons, image the photons



# Scintillating screen



First full turn as seen by the BTV 10/9/2008

## Single shot profile

**Physics process:**  
**Scintillation, photons are emitted due to the excitation, and de-excitation of atomic states**

**Detector:**  
**Insert screen + optical system**

## Image detection:

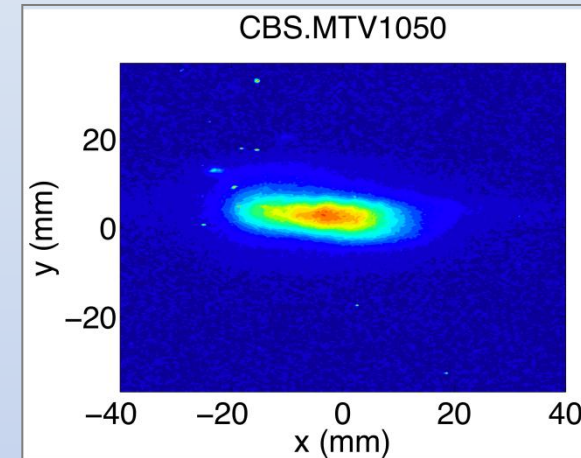
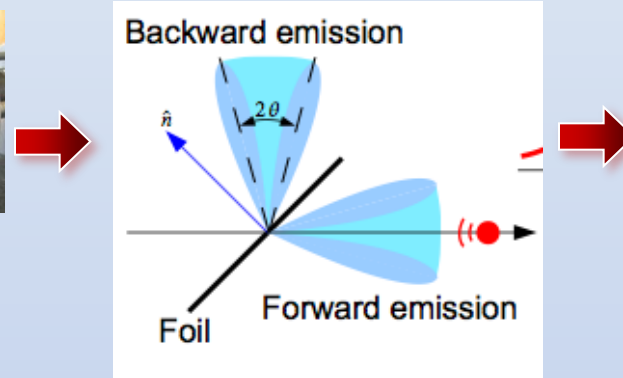
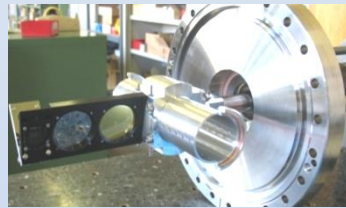
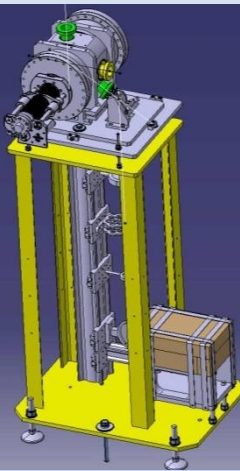
- Image the light of the screen
- Multiple scattering in screen increase beam size
- Emission of photons ns to micro seconds
- Calibrate optical system with known target
- Correct for optical aberrations (screen 45 degrees)

Type	Composition	Decay Time	
		Decay of Light Intensity from 90 % to 10 % in	Decay of Light Intensity from 10 % to 1 % in
P 43	Gd <sub>2</sub> O <sub>2</sub> S:Tb	1 ms	1,6 ms
P 46	Y <sub>3</sub> Al <sub>5</sub> O <sub>12</sub> :Ce	300 ns	90 μs
P 47	Y <sub>2</sub> SiO <sub>5</sub> :Ce,Tb	100 ns	2,9 μs
P 20	(Zn,Cd)S:Ag	4 ms	55 ms
P 11	ZnS:Ag	3 ms	37 ms

*1MeV e<sup>-</sup> on 5μm P43 yields ~ 60 ph.*

**Mechanical assembly move screen into vacuum chamber:**

# Transition Radiation



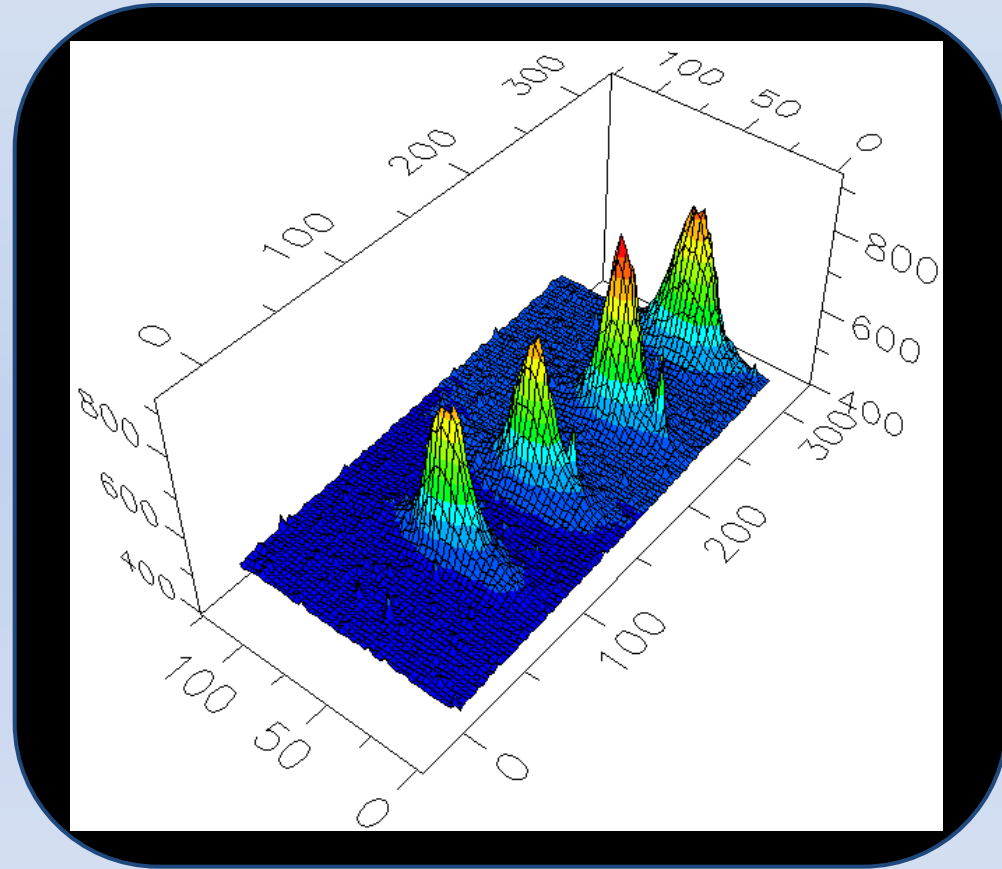
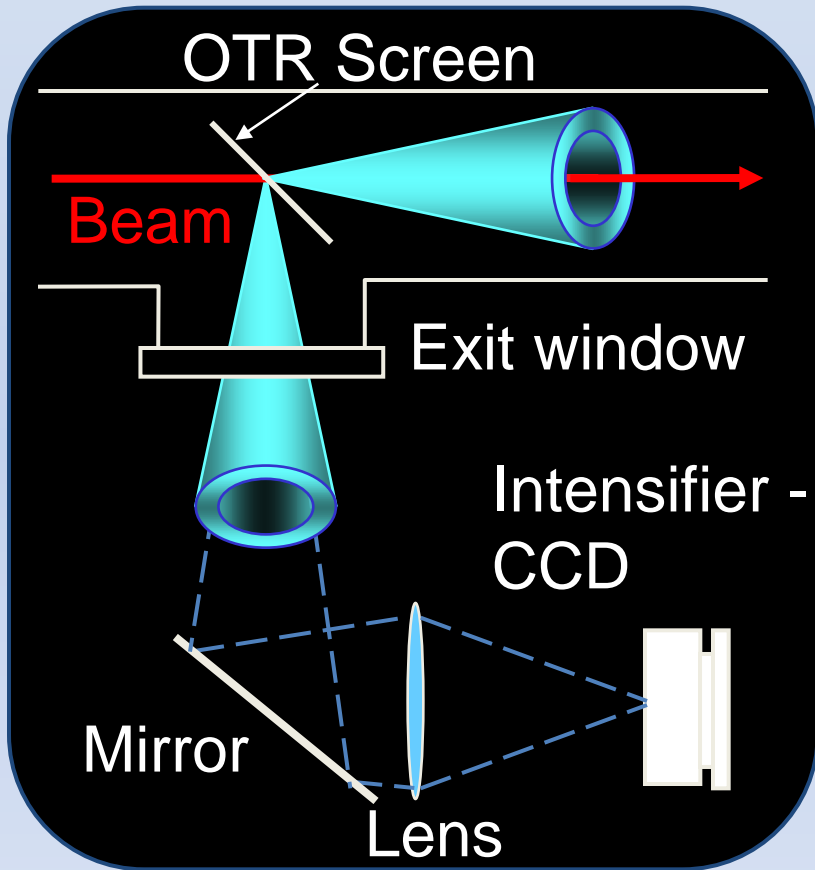
**Physics process:**  
 Radiation emitted when a charged particle crosses a material with a different dielectric constant

$$\frac{d^2W}{d\Omega d\omega} \approx \frac{Nq^2}{\pi^2 c} \left( \frac{\theta}{\gamma^{-2} + \theta^2} \right)^2$$

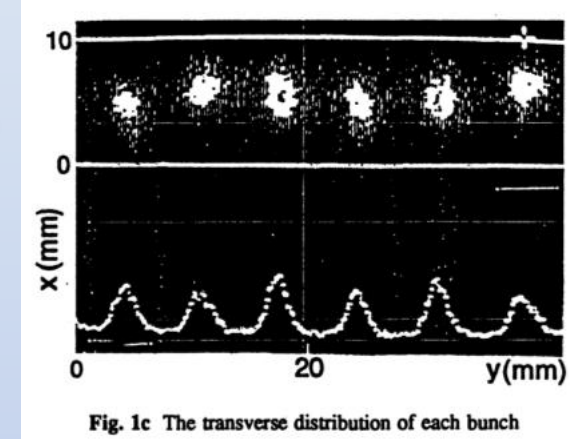
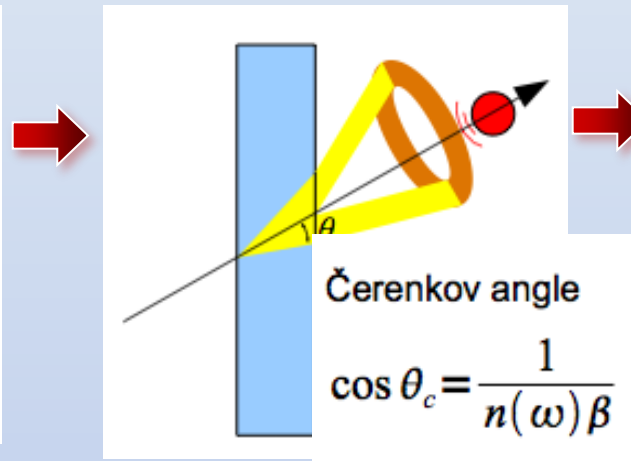
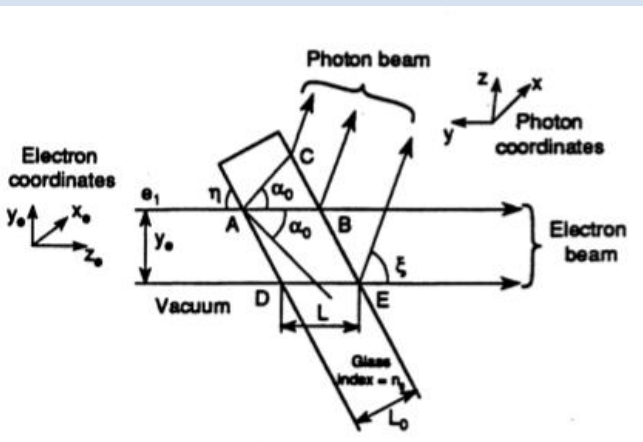
**Detector:**  
 Insert radiator  
 (e.g. thin Al foil / SiC wafer) +  
 optical system

## Image detection:

- Image the light at the focus of the screen
- Screen can be thin & emission instantaneous
- Angular pattern of emission depends on beam energy
- Thermal damage to screen charge density > 10<sup>6</sup>nC/cm<sup>2</sup>
- Number of photons emitted depends on electron energy ~0.3 photons/electron (50 MeV), 0.001 photon/electron (100 keV) [400 – 600 nm]



# Cerenkov Radiation



## Detector:

Insert radiator, with index of refraction matching beam energy requirements, with correct optical system

## Image detection:

- Threshold effect
- Fast emission – charged beam polarizes material, then de-excites back to ground state
- Emitted light travels slower than charged particles (source dispersion)
- Good light production yield-  
Sent to Streak Camera

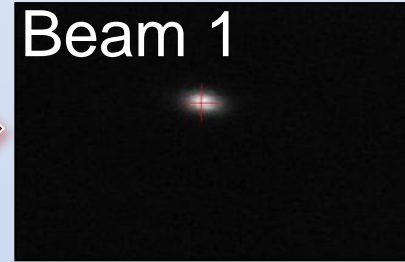
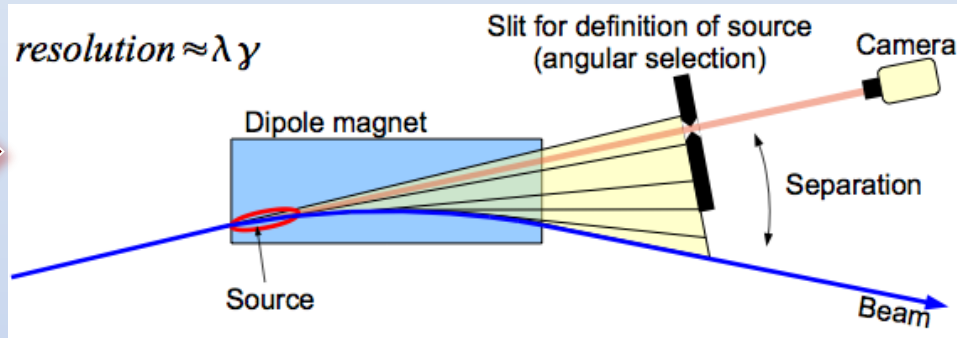
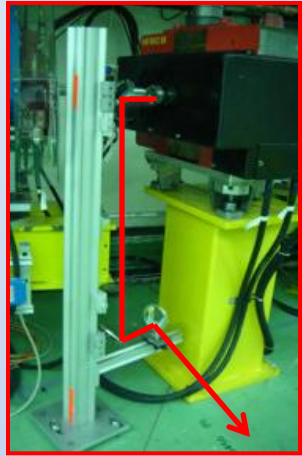
**Physics process:**  
 Radiation emitted when a charged particle crosses a material, when

$$b.n(\omega) > 1$$

Radiation has a defined angular distribution, not very suitable for transverse imaging

$$\frac{d^2 N}{dx d\omega} = \frac{\alpha z^2}{c} \sin^2 \theta_c(\omega) = \frac{\alpha z^2}{c} \left( 1 - \frac{1}{\beta^2 n^2(\omega)} \right)$$

# Synchrotron Light

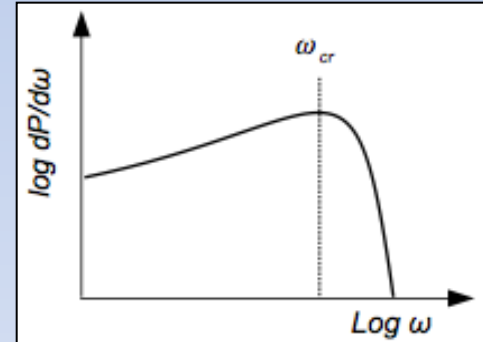


## Physics process:

Charge particles emit electromagnetic radiation when accelerated

Synchrotron radiation: change in direction

$$P = \frac{1}{4\pi\epsilon_0} \frac{2}{3} \frac{ce^2\gamma^4}{\rho^2}$$



$$\omega_c = \frac{3}{2} \frac{c\gamma^3}{\rho}$$

## Detector:

Extract light from a dipole magnet (or undulator or wiggler)

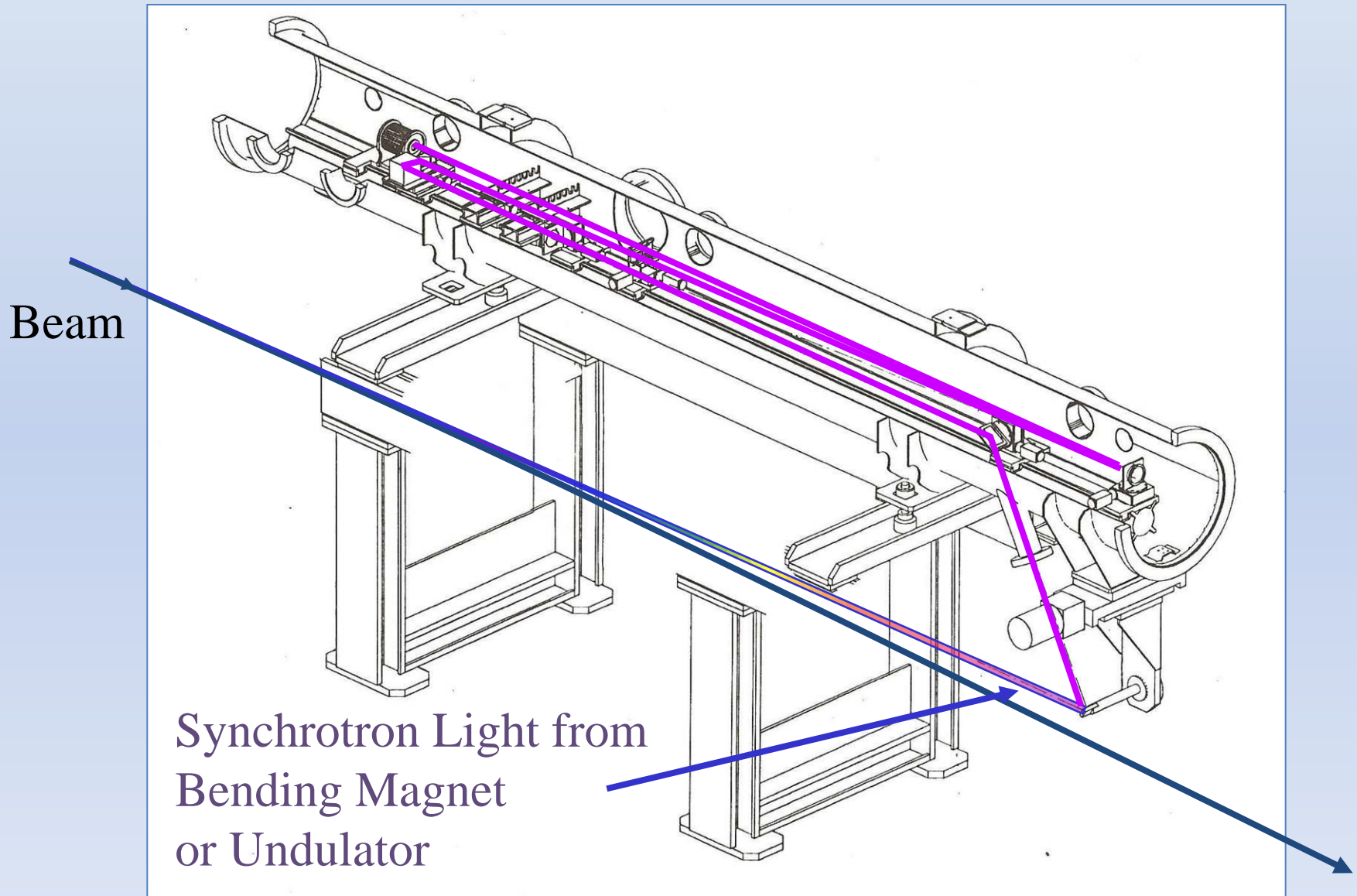
Optical system + camera /PMT

## Image detection:

- Image the light from the entrance or entrance edge of the magnet - higher frequency components, edge radiation
- Must implement a “virtual” target to image the source of the radiation in the magnet
- Resolution limited by diffraction

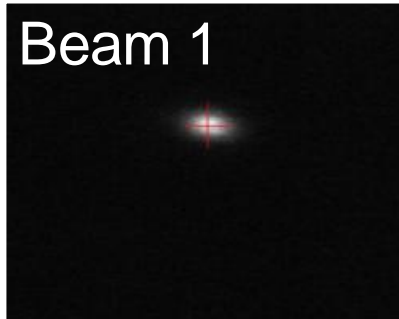


# The Synchrotron Light Monitor

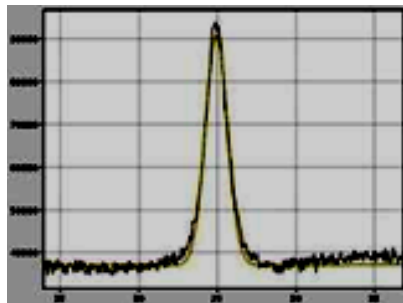


# The Synchrotron Light Monitor

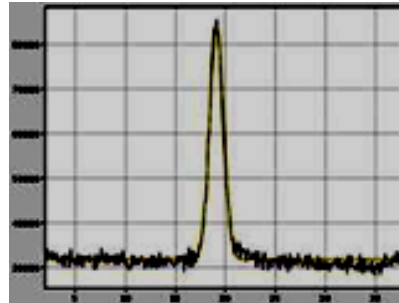
Beam 1



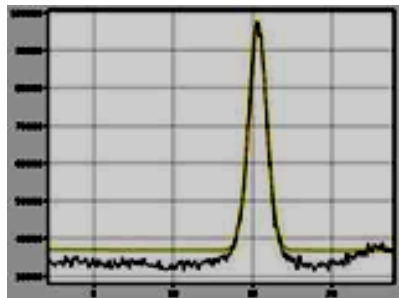
Beam 2



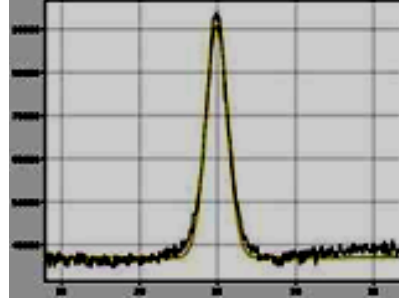
$$\sigma_h = 0.68\text{mm}$$



$$\sigma_h = 0.70\text{mm}$$



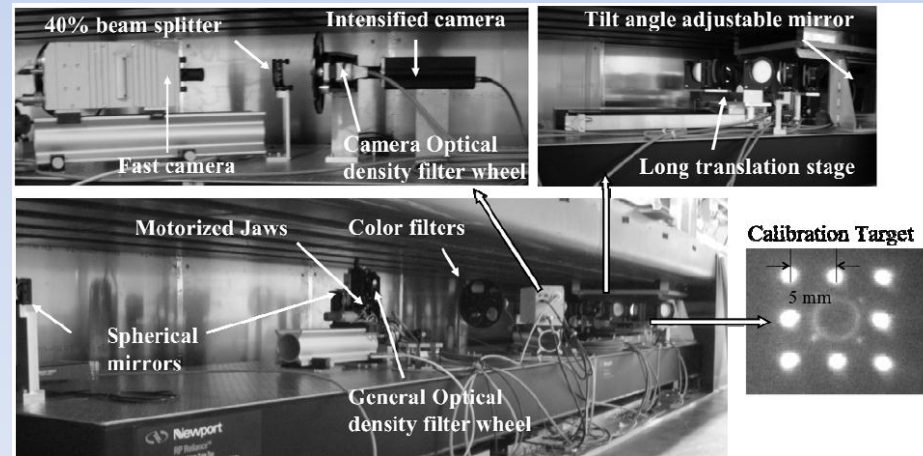
$$\sigma_v = 0.56\text{mm}$$



$$\sigma_v = 1.05\text{mm}$$

Important instrument design:

1. Simulation:
  - Synchrotron radiation source
  - Optical line transport through all lenses, mirrors, filters
  - Camera response
2. Calibration target.
3. Remote control of all devices
4. Filters for variable bunch intensity



→ Why do we need diagnostics

→ What do we need to measure?

- Position
  - Capacitive BPM
- Current
  - Wall current monitor
  - Faraday Cup
- Transverse Profile (emittance, TWISS ( $\alpha\beta\gamma$ ) parameters)
  - Intercepting methods
    - » Scanning wires
    - » Radiative screens
    - » Scintillation screens
    - » Cerenkov targets
  - Non intercepting methods
    - » Synchrotron light
- Longitudinal Profile
  - Streak Camera
  - RF deflector
  - Electro optical techniques
  - RF power measurements and spectroscopy
- Luminosity Detectors
- Beam Loss Detectors

First  
Lecture

Second  
Lecture

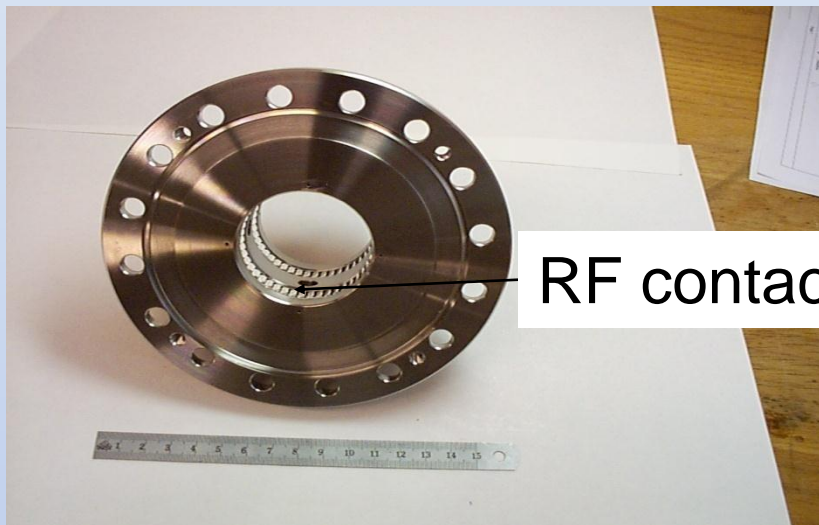
→ Discuss diagnostics developments needed for new machines



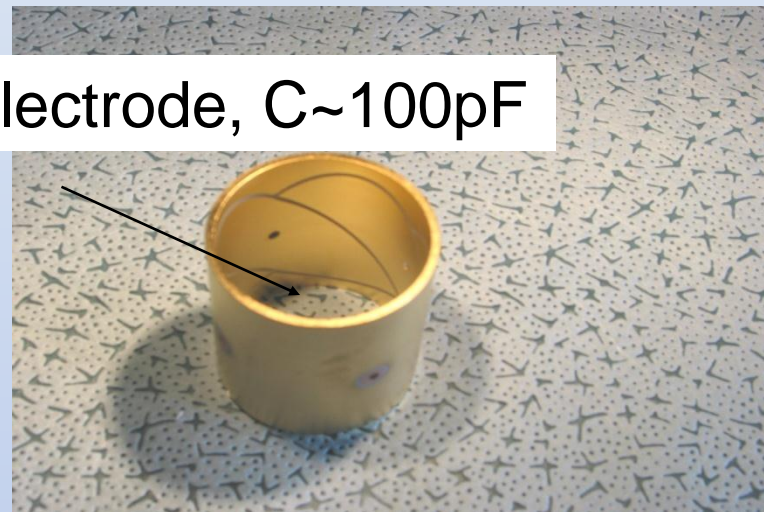


# Measure current as a function of x- position

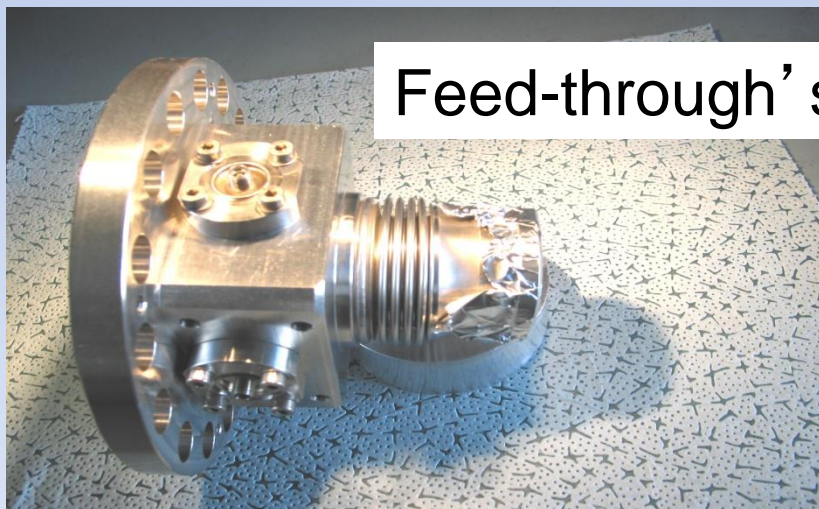
# Electrostatic Pick-up (BPE) – CTF3



RF contacts

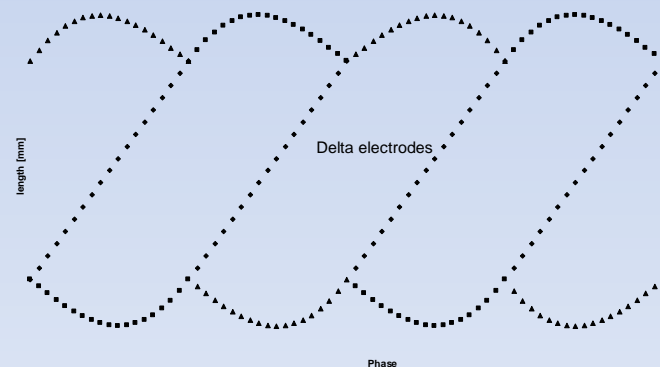


Electrode, C~100pF



Feed-through's

$$\hat{V}(t) = \frac{1}{v} \times \frac{l_{\text{eff}}}{C_{\text{Elec}}} i(t)$$



Developed by L. Sørby, CERN



# Electrostatic PU



## PICK-UP SEMI AUTOMATED CALIBRATION BENCH -- GRAPHS RESULTS

Author's name

Pick-Up name

Front end name

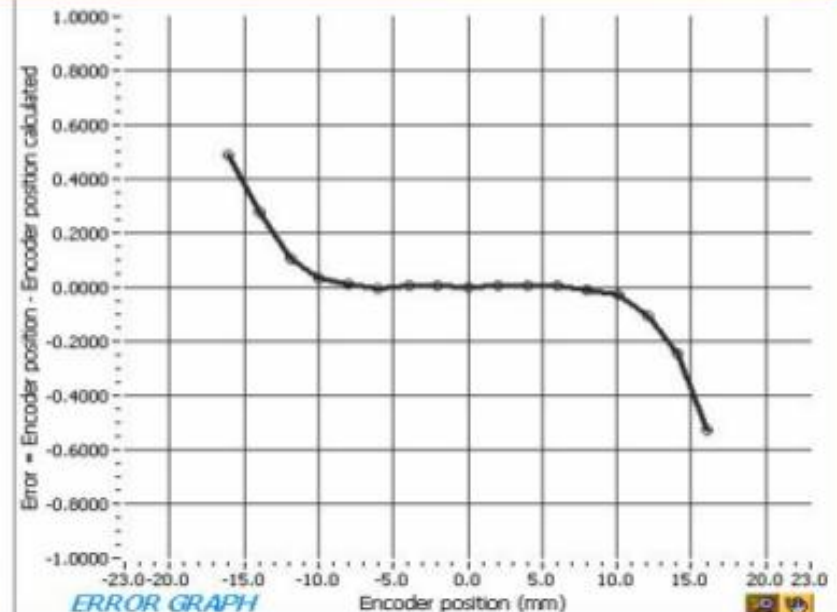
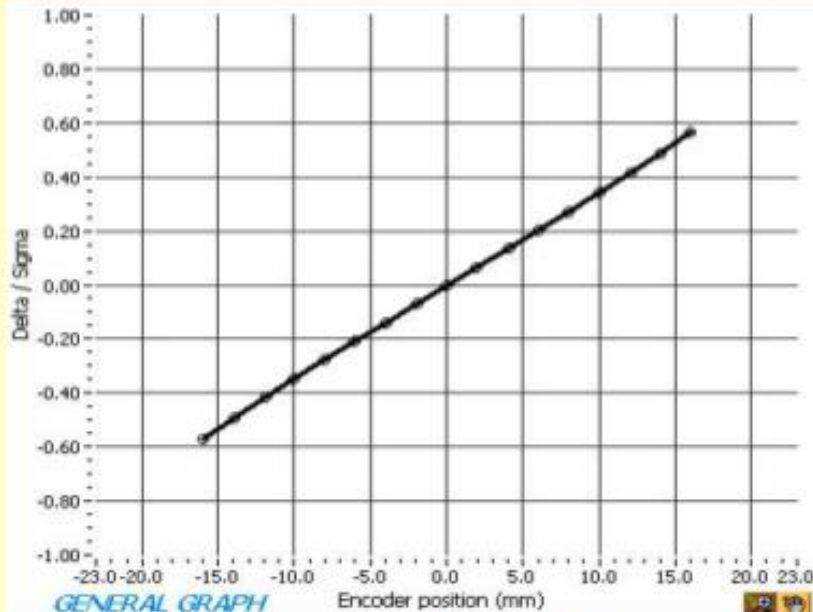
Comments

Date

Pick-Up number

Pick-Up diameter (mm)

Front end number



### General

Step size:

Number of points:

Offset (mm):

Mechanical zero (mm):

Scanned:  Vertically

### Curve fitting

Polynomial order:

Max Error D/S:

Max Error S (V):

FE installed? (coef.):

Impedance (Ohms):

### Polynomial Coefficients

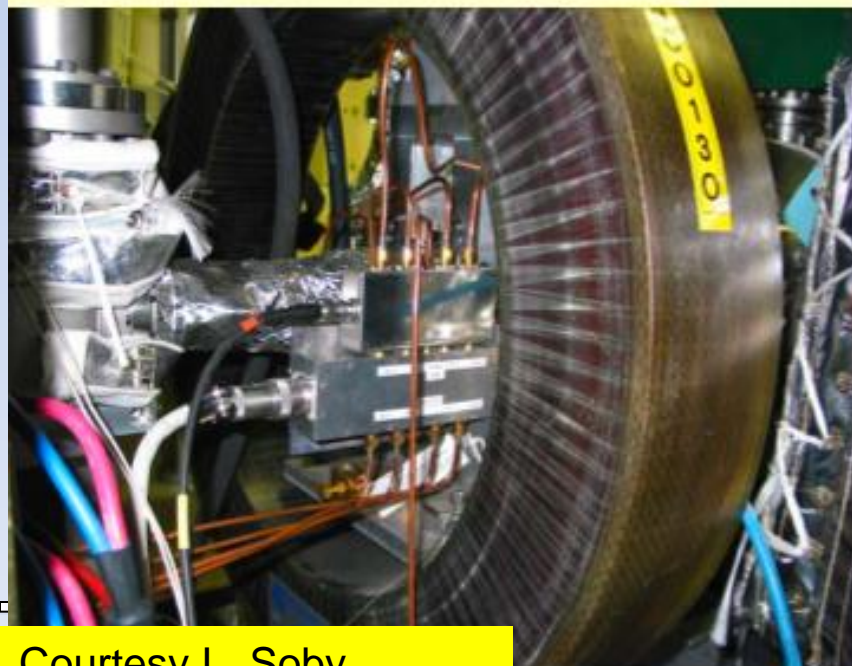
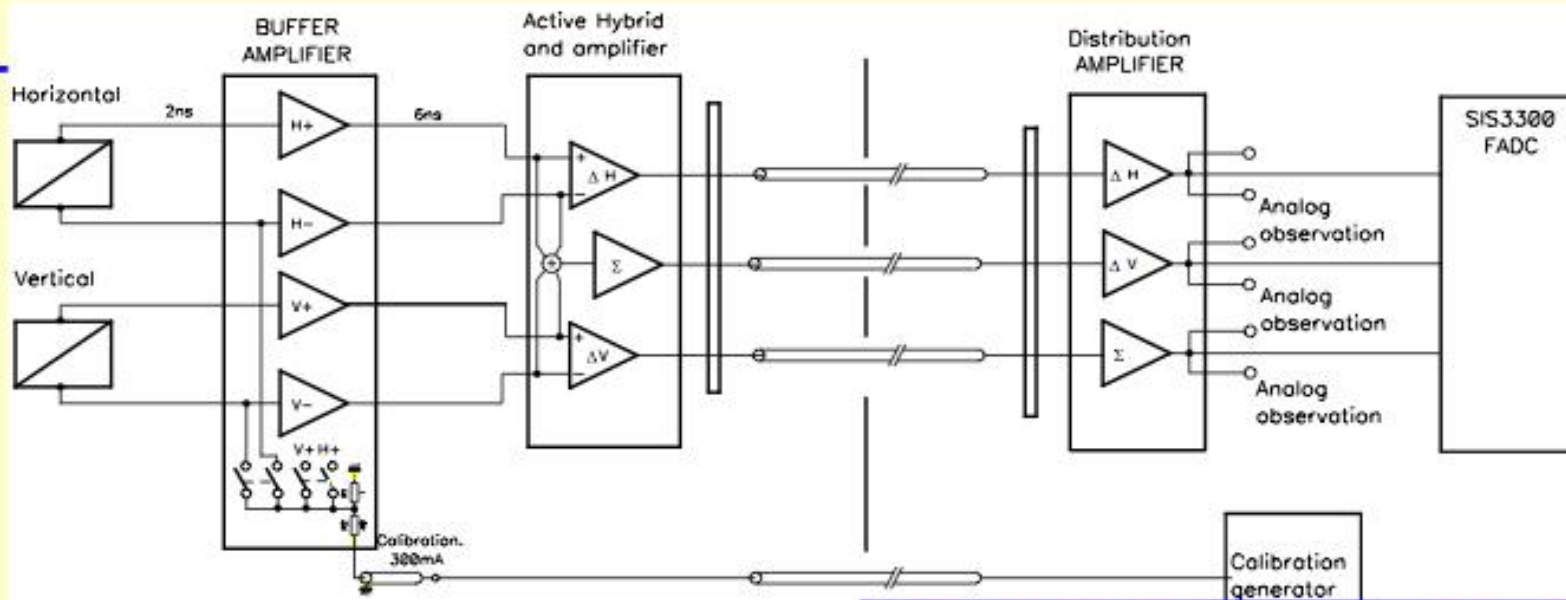
b0: 1.027E-1  
b1: 2.920E+1

### Equation of fitted curve Delta / Sigma

Delta / Sigma = +102.661E-3 + 29.200E+0 Pos



# Electrostatic PU



Transverse sensitivity	$\Delta = \Sigma$ @ ~10mm
Resolution	10um / 20um
Relative precision ( $\pm 10$ mm)	0.2%
Longitudinal coupling impedance	0.17 / 1.7 ohm
Resolution	12mA / 1.2mA
Absolute precision (I)	~ 1%
Low frequency cut off	1kHz
High frequency cut off	200MHz
Calibration	Yes
ID / Length	46mm / 130mm
Number of feedthroughs	4
Flange types	DN40CF / DN100CF
Max. bake-out temperature	130 °C

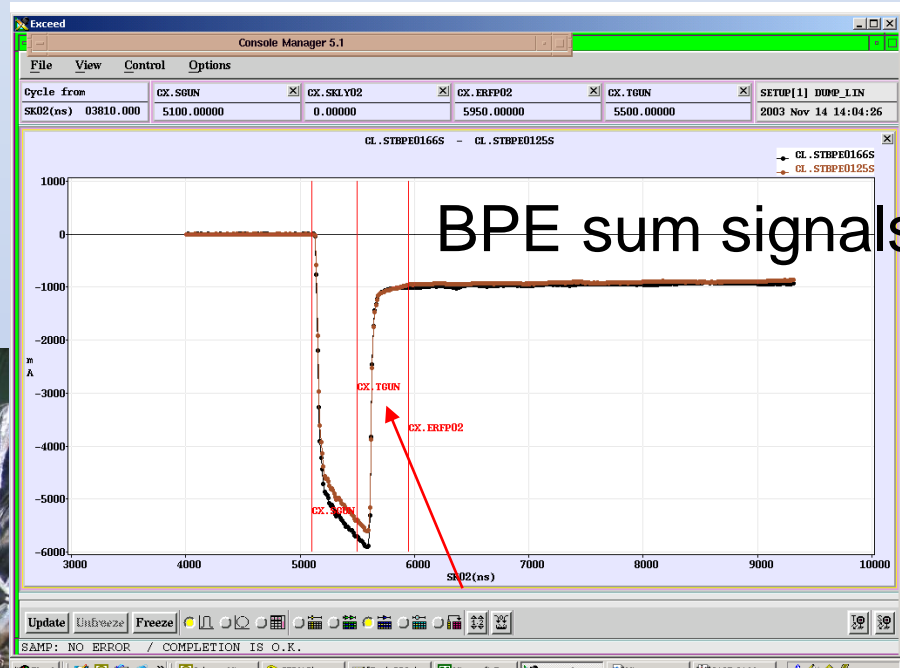
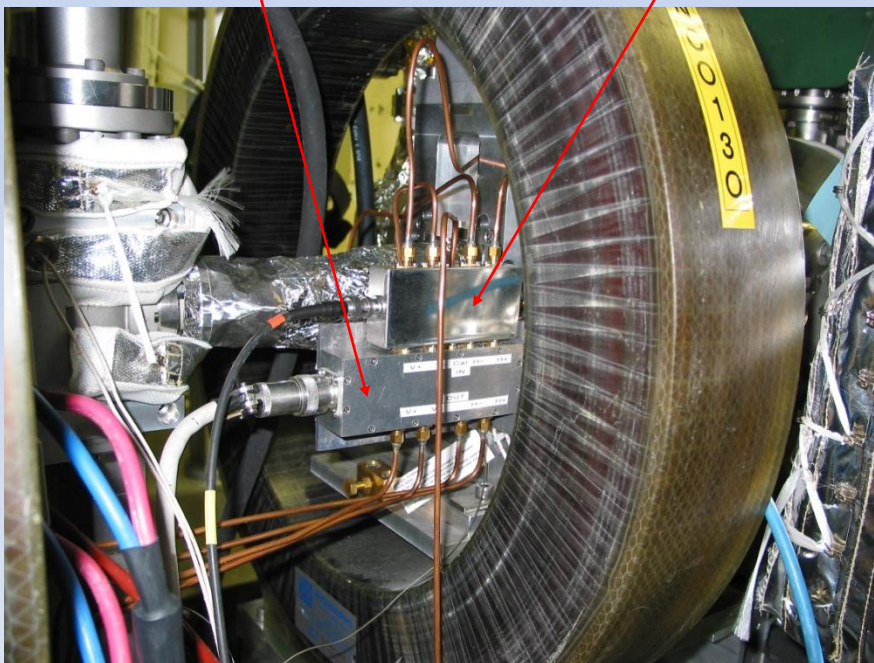
# Electrostatic PU (BPE)

$$F_{\text{Low}} = \frac{1}{2 \times p \times R_L \times C_{\text{Elec}}}$$

CTF3 bunch spacing 3 GHz  $\gg$   $F_{\text{low}}$

**Buffer amplifier,  $R_L=1\text{M}\Omega$**

**HT bias**



**Electrodes charging up due to beam halo!**

Courtesy L. Soby

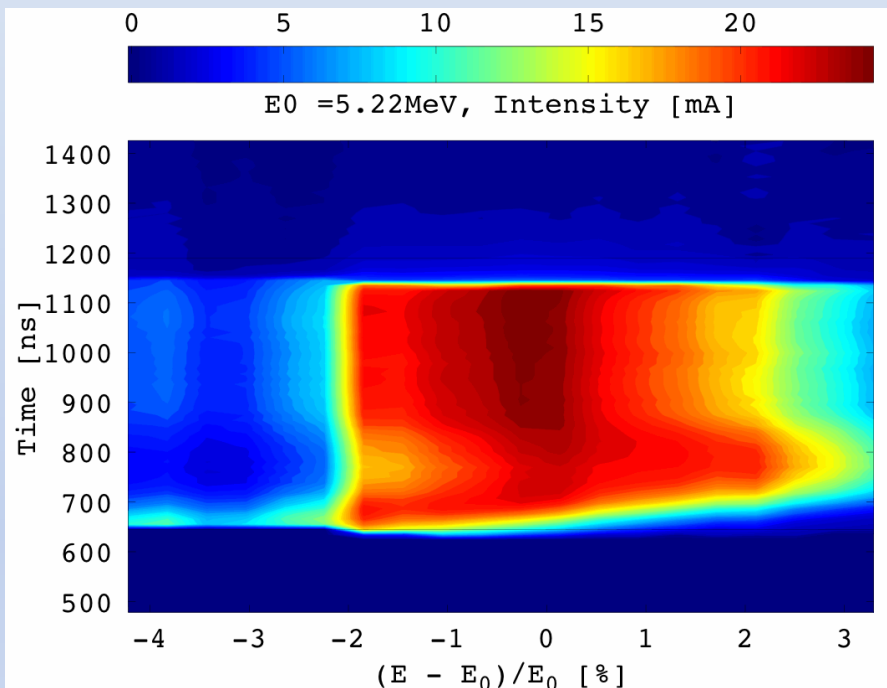
# Comparison of different BPM types

Pickup	Transformer	Button	Matched Stripline	RF Cavity
<b>Spectrum</b>				
<b>Monopole Mode Suppression</b>	Modal (hybrid) / electronics	Modal (hybrid) / electronics	Modal (hybrid) / electronics	Modal (coupler), frequency,
<b>Typical RMS Noise, 10pC, *20mm pipe*</b>	>50 $\mu$ m	>100 $\mu$ m	~60 $\mu$ m	<1 $\mu$ m
<b>Typical Electronics Frequency</b>	0.1...200MHz	300...800MHz	300...800MHz	1-12GHz
<b>Pictures</b>				

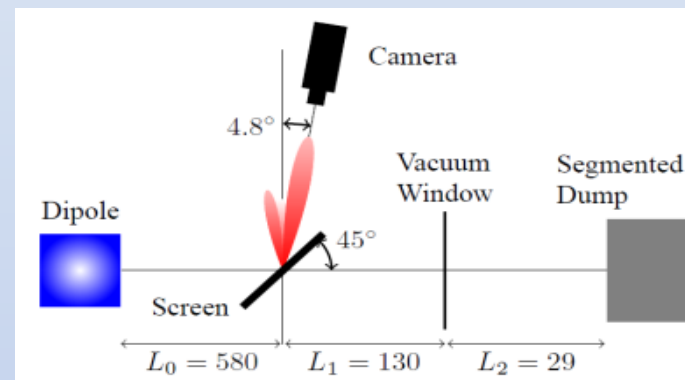
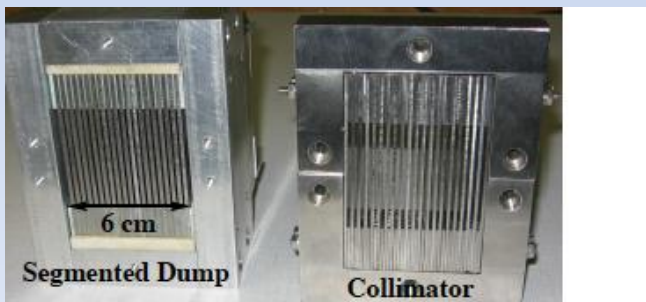
H. H. Braun (CAS RF 2010)



# Current Measurement- Segmented Dump –Electron Beam

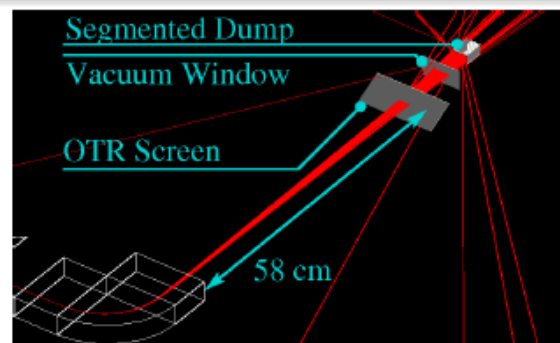


Measure profile in a dispersive region → energy spectrum



## PHIN Spectrometer

- Segmented dump at 78 cm
- OTR screen at 58 cm



Daniel Egger

# Beam Intensity - Toroids

$$\oint \mathbf{B} \cdot d\mathbf{l} = \mu_0 I_{enc}$$

Ampere's Law

If  $r_0$  is thicker than the toroid

$$B = \langle B_n \rangle = \frac{\mu_0 I_b}{2\pi r_0}$$

$$e = \frac{d\Phi}{dt}, \text{ where } \Phi = \oint \mathbf{B} \cdot d\mathbf{a}$$

$$e = \frac{\mu_0 A}{2\pi r_0} \frac{di_b}{dt}$$

Faraday's law of induction

Lenz's law

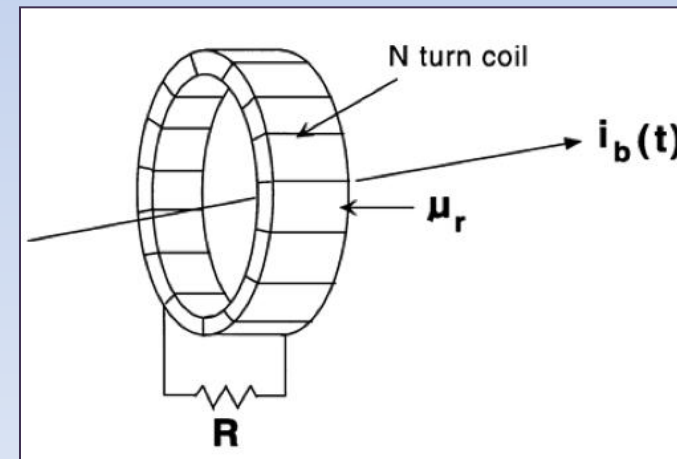
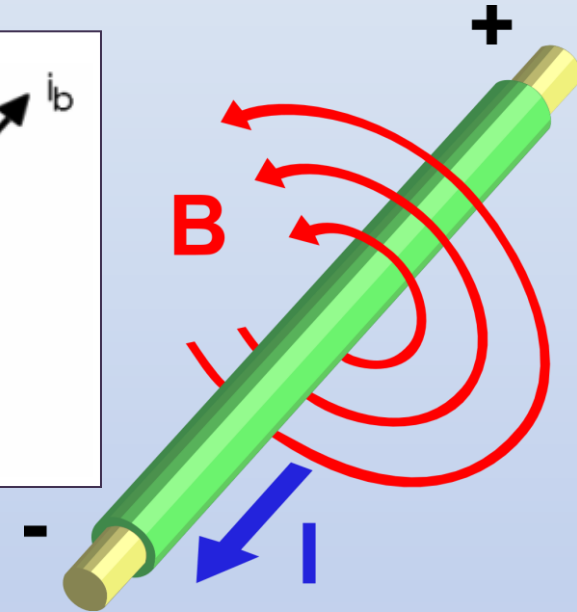
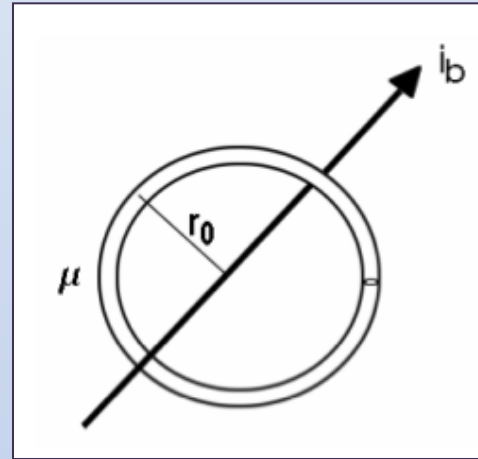
Coil is wound around the core

This coil senses the induced emf, and acts to oppose the magnetic field induced by the beam

Add a resistor in series →

$$V_r = I_r R = (I_b / N) R$$

What about the bandwidth of this signal?





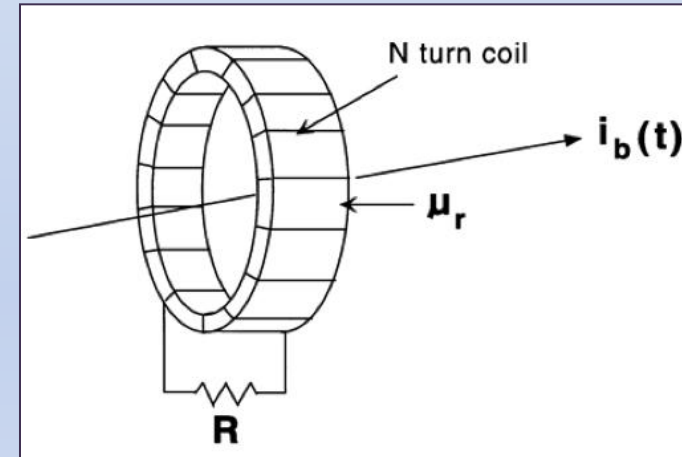
# Beam Intensity - Toroids

$$e = \frac{\oint f}{\oint t}, \text{ where } f = \oint B \cdot da$$

$$e = \frac{mA}{2\pi r_0} \frac{\oint i_b}{\oint t}$$

Faraday's law of induction

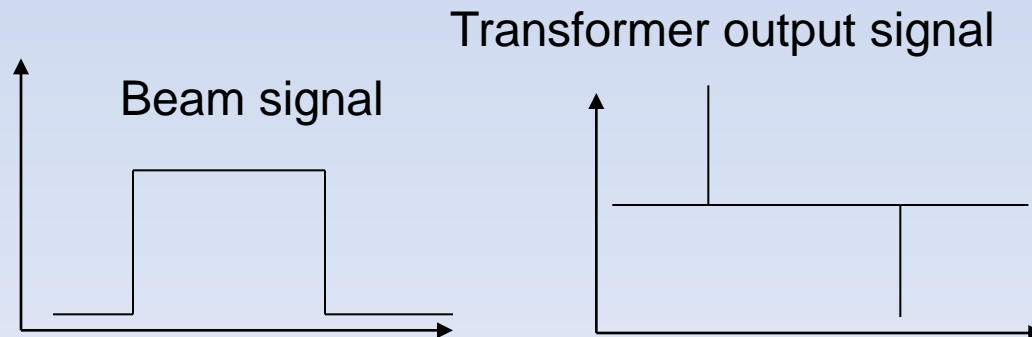
Lenz's law



Coil is wound around the core  
 This coil senses the induced emf, and acts to  
 oppose the magnetic field induced by the beam  
 Add a resistor in series →

$$V_r = I_r R = (I_b / N) R$$

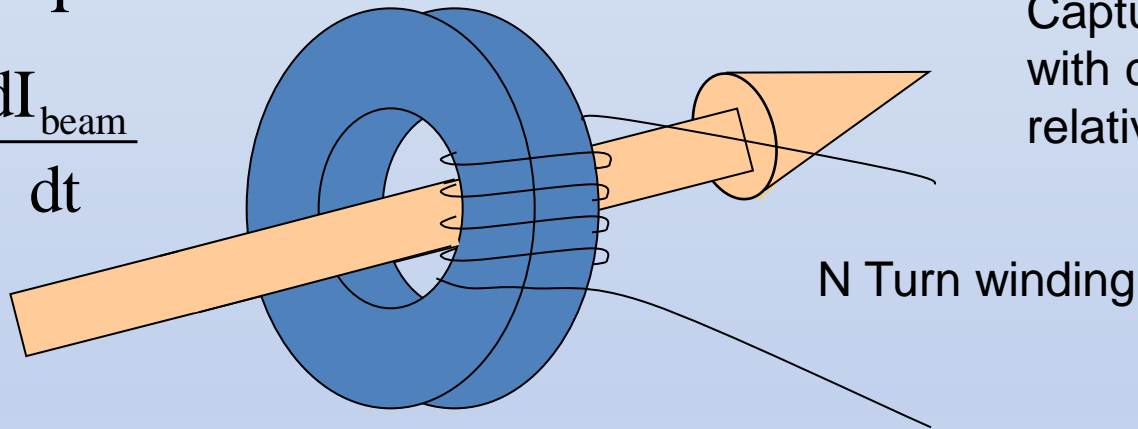
What about the bandwidth of this signal?



# The ideal transformer

$$L = \frac{N^2 m_r m_0 A}{l}$$

$$U = L \frac{dI_{\text{beam}}}{dt}$$

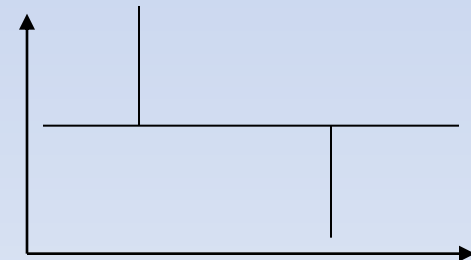
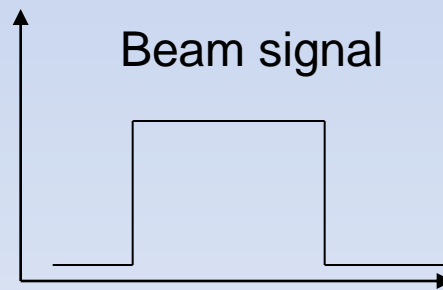


Fields are very low

Capture magnetic field lines with cores of high relative permeability

Inductance L of the winding

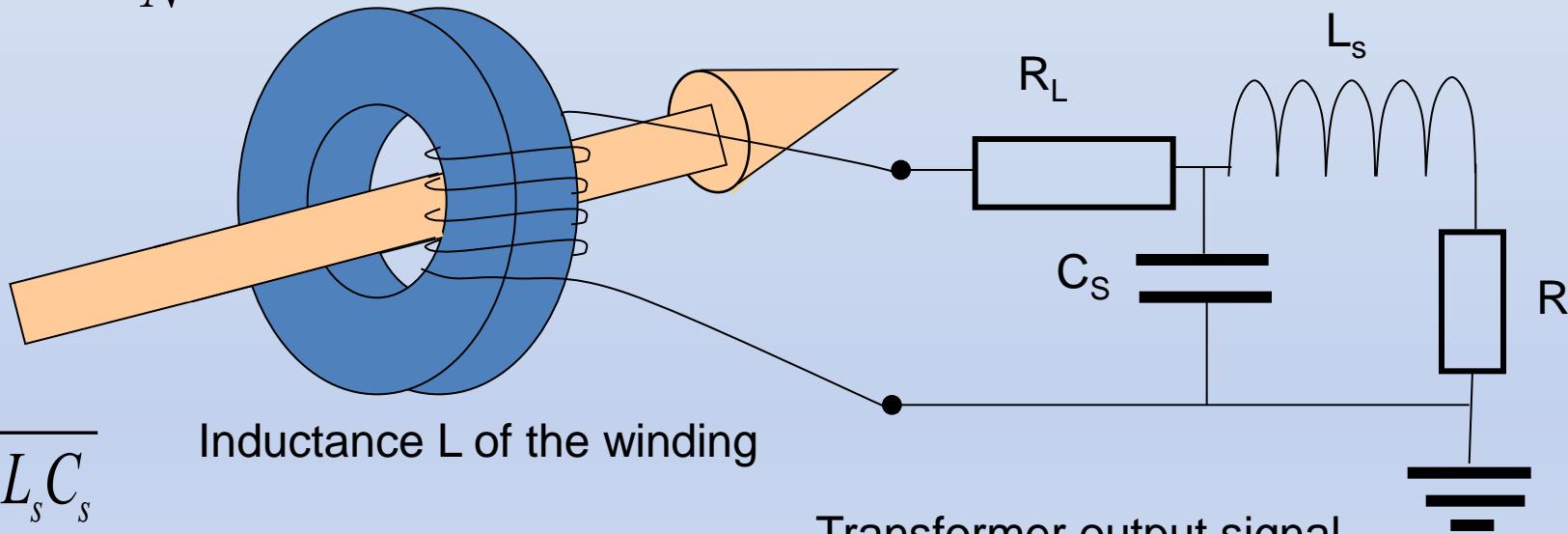
Transformer output signal



# The AC transformer

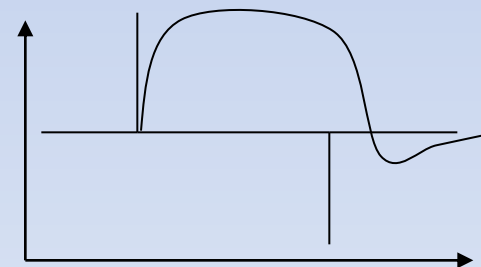
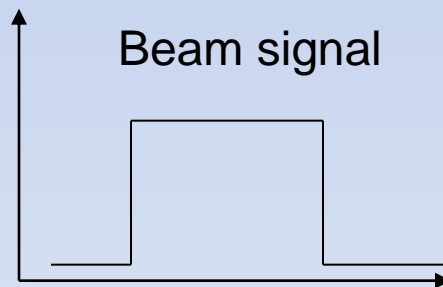
$$U(t) = I_{beam}(t) \frac{R}{N} e^{-\frac{t}{t_{droop}}}$$

Winding of N turns and Inductance L



$$t_{rise} = \sqrt{L_s C_s}$$

$$t_{droop} = \frac{L}{R + R_L}$$



# Beam Profile Monitoring using Screens

- Screen Types

- Luminescence Screens

- destructive (thick) but work during setting-up with low intensities

- Optical Transition Radiation (OTR) screens

- much less destructive (thin) but require higher intensity

Sensitivities measured with protons with previous screen holder, normalised for  $7 \text{ px}/\sigma$

Type	Material	Activator	Sensitivity
<b>Luminesc.</b>	CsI	Tl	$6 \cdot 10^5$
“	$\text{Al}_2\text{O}_3$	0.5%Cr	$3 \cdot 10^7$
“	Glass	Ce	$3 \cdot 10^9$
“	Quartz	none	$6 \cdot 10^9$
<b>OTR [bwd]</b>	Al		$2 \cdot 10^{10}$
“	Ti		$2 \cdot 10^{11}$
“	C		$2 \cdot 10^{12}$
<b>Luminesc. GSI</b>	P43: $\text{Gd}_2\text{O}_2 \text{ S}$	Tb	$2 \cdot 10^7$

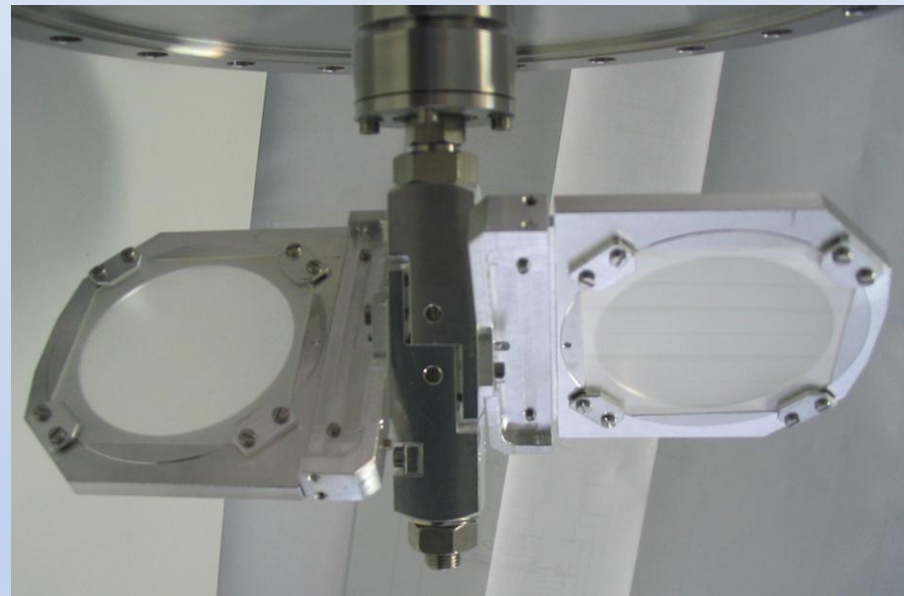


# Beam Profile Monitoring using Screens

- Usual configuration

- Combine several screens in one housing e.g.

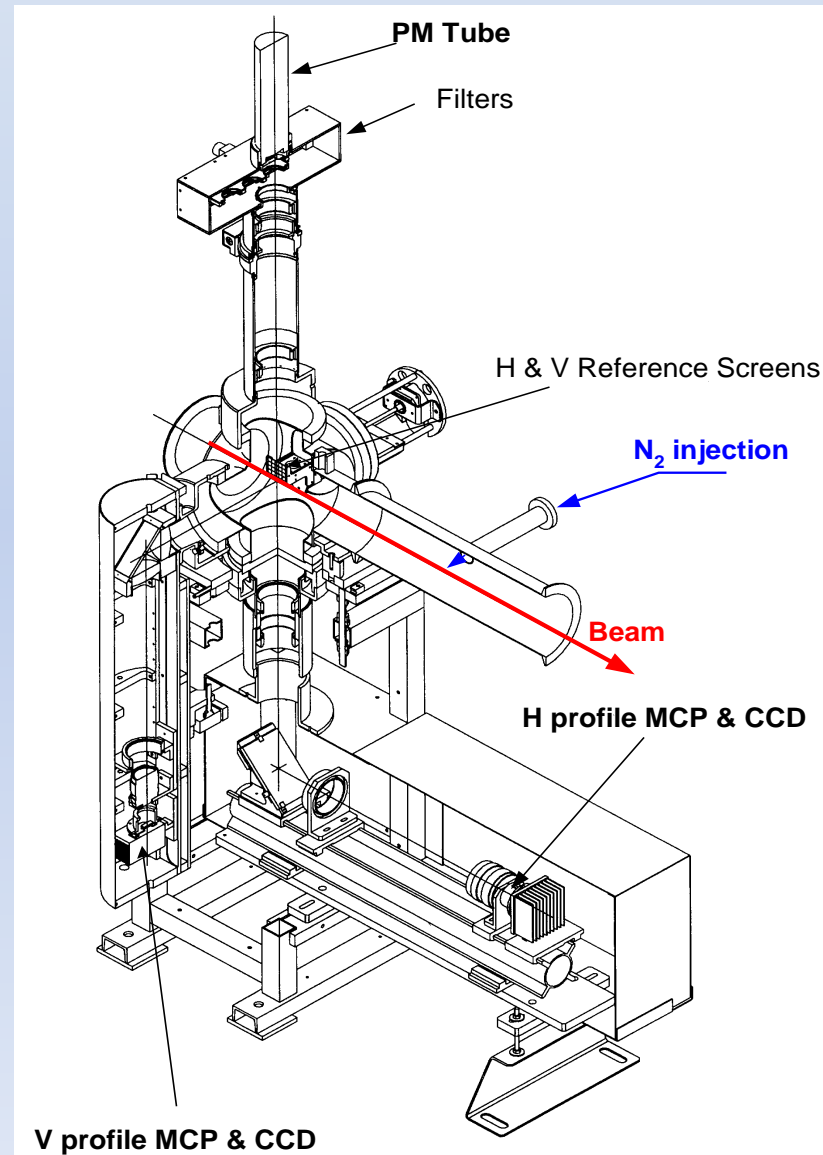
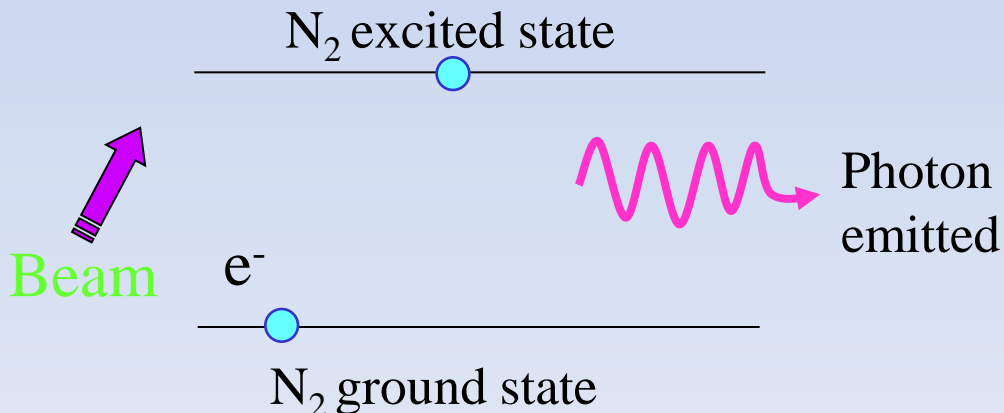
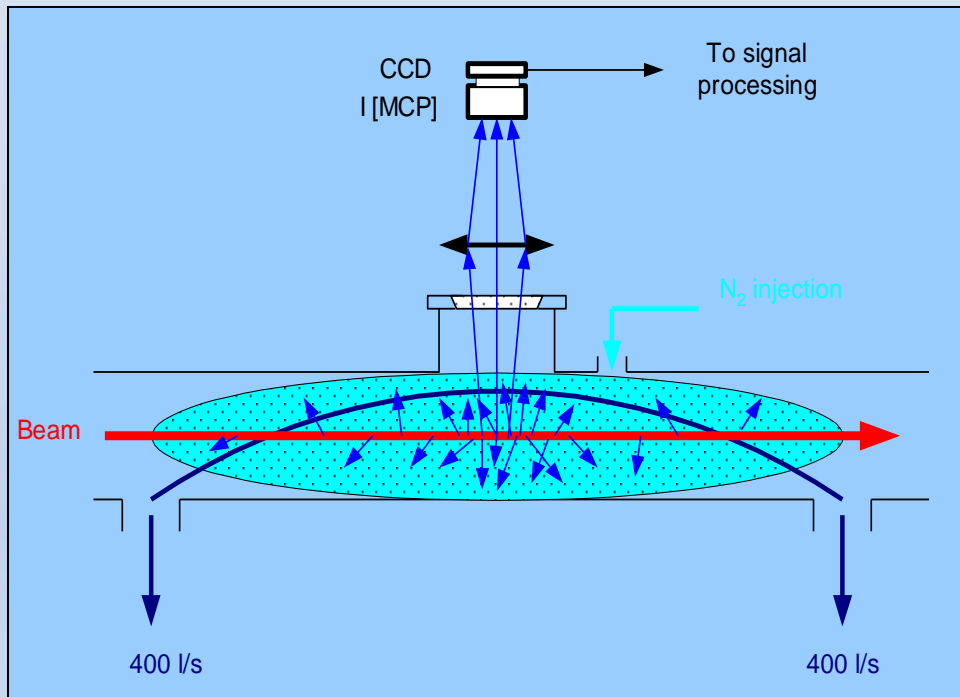
- $\text{Al}_2\text{O}_3$  luminescent screen for setting-up with low intensity
- Thin ( $\sim 10\mu\text{m}$ ) Ti OTR screen for high intensity measurements
- Carbon OTR screen for very high intensity operation



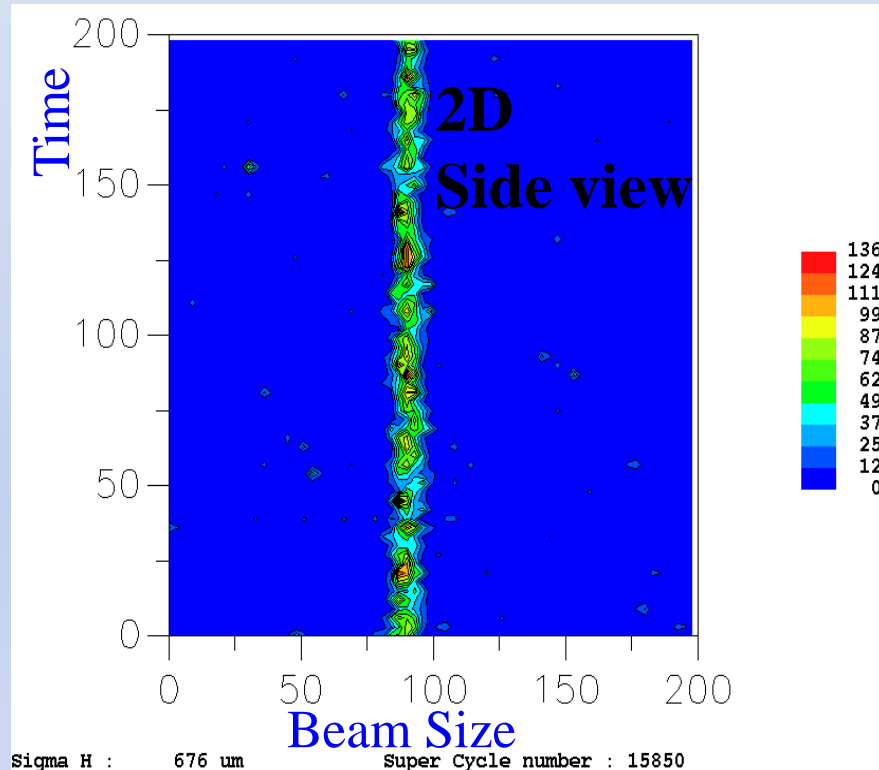
- Advantages compared to SEM grids

- allows analogue camera or CCD acquisition
- gives two dimensional information
- high resolution:  $\sim 400 \times 300 = 120'000$  pixels for a standard CCD
- more economical
  - Simpler mechanics & readout electronics
- Time resolution depends on choice of image capture device
  - From CCD in video mode at 50Hz to Streak camera in the GHz range

# Luminescence Profile Monitor

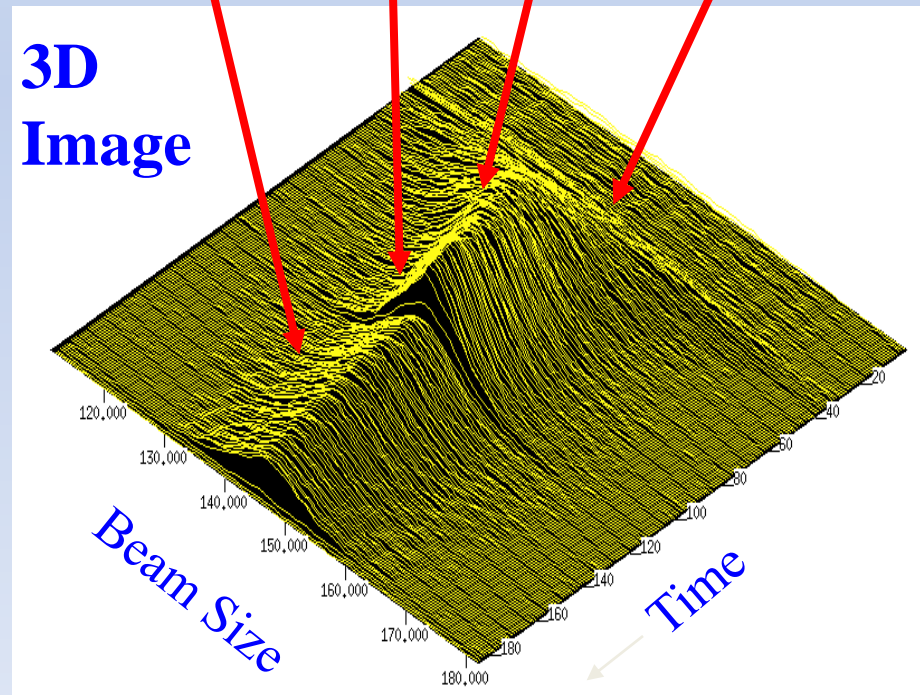


# Luminescence Profile Monitor



Beam size shrinks as beam is accelerated

Fast extraction  
Slow extraction  
Injection



## CERN-SPS Measurements

- Profile Collected every 20ms
- Local Pressure at  $\sim 5 \times 10^{-7}$  Torr