



September 1 - 6, 2024, Salt Lake City, Utah



Development of a ReBCO non/metal-insulated 40 T solenoid for the Muon Collider



Funded by
the European Union



MuCol

B. Bordini, C. Accettura, A. Bertarelli, L. Bottura, A. Dudarev,
M.A. Hafiz, A. Kolehmainen, T. Mulder, D. Rinaldoni, F. Sanda,
G. Vernassa, A. Verweij, M. Wozniakc



Outline



■ Introduction

- The Muon Collider & its Final Cooling Channel
- The Final Cooling Solenoids and the proposed conceptual design

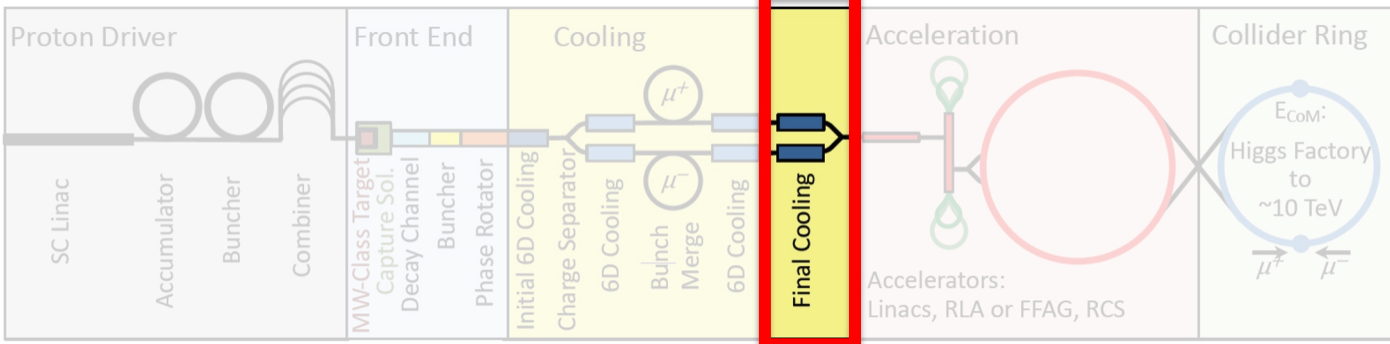
■ Design and studies for the final cooling solenoid

- Advancing on the: engineering Design and; mechanical analysis
- Studying the effects of magnetization and quenches on mechanics
- Protection studies and development of new electrodynamics models

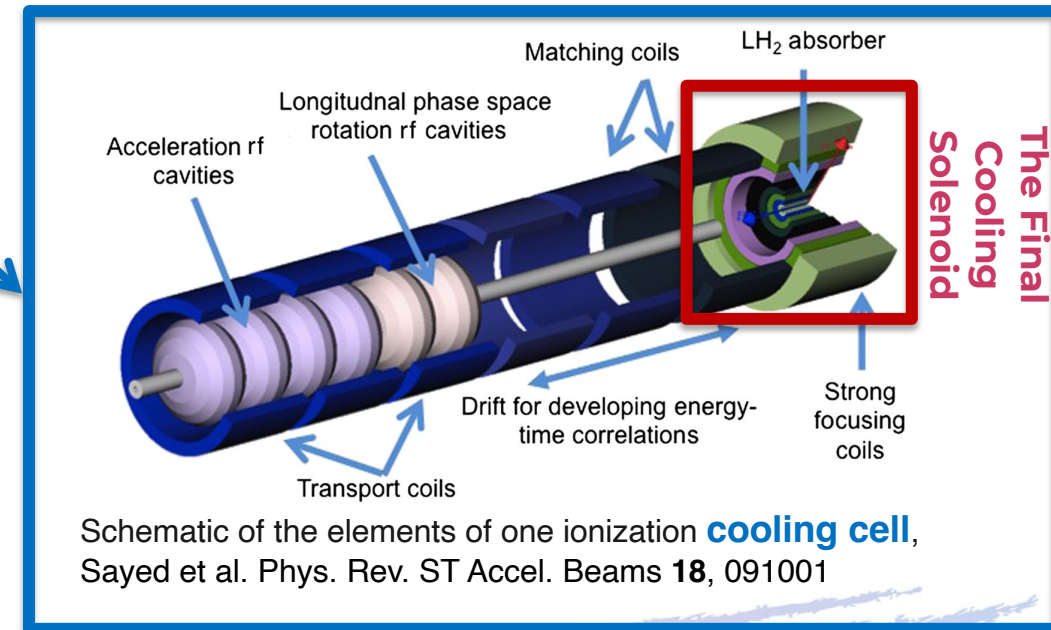
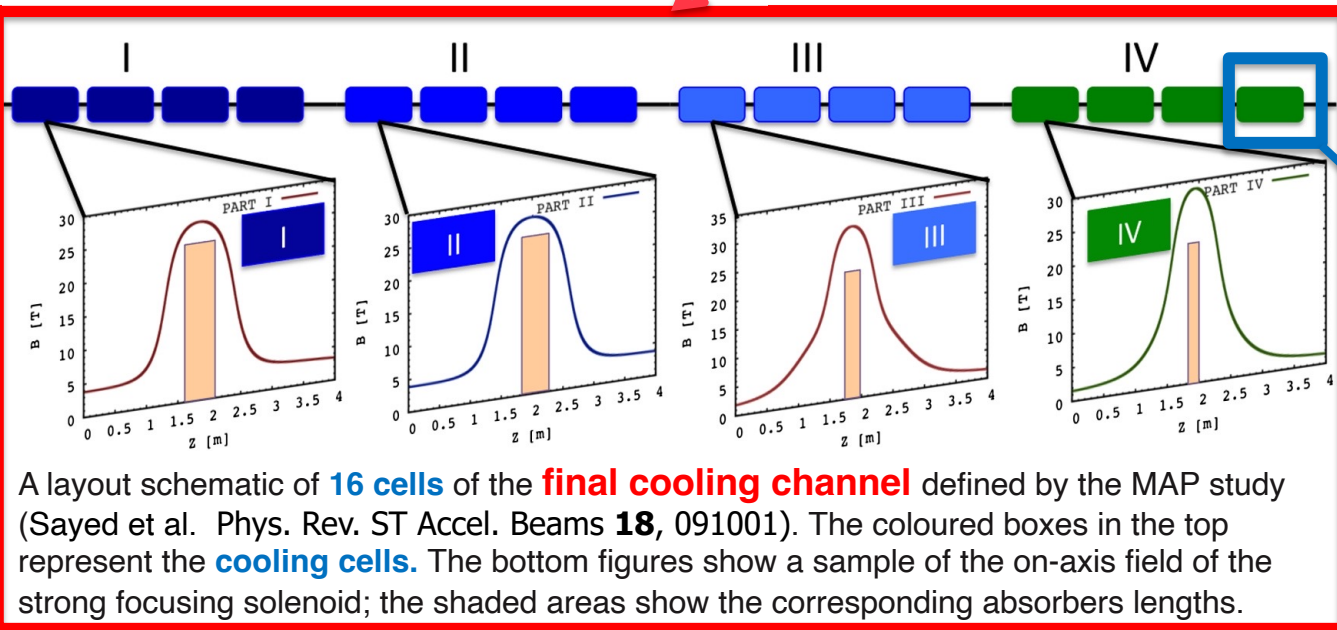
■ Some Experimental Activities

- Technological Studies
- Macro & Micro mechanical characterizations
- Critical current measurements on procured ReBCO tapes

The Muon Collider Final Cooling Channel



- The final cooling solenoids are part of the **final cooling channel**, which is constituted by several **cooling cells**
- **16** were proposed by the MAP study



The Final Cooling (FC) Solenoid

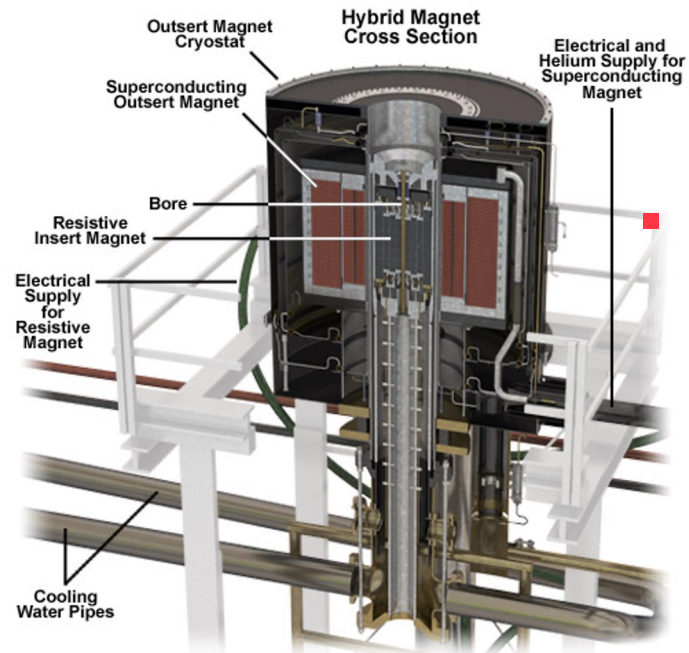
Design proposed by MAP

$R_{\text{out}} = 83 \text{ cm}$

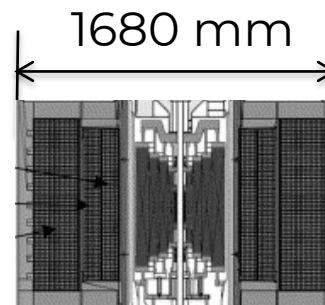
A set of eight **superconducting** coaxial coils providing a peak field of **50 T**

The inner diameter of the smallest coils is **50 mm**.

Sayed et al. Phys. Rev. ST Accel. Beams 18, 091001



Cross section of **45 T, 32 mm** NHFML user facility solenoid



In the world, only **two solenoids** (at **NHFML** and **CHFML**) **$B \geq 40 \text{ T}$** in a **free bore aperture** (32 mm) **comparable** with what needed for **FC solenoids**

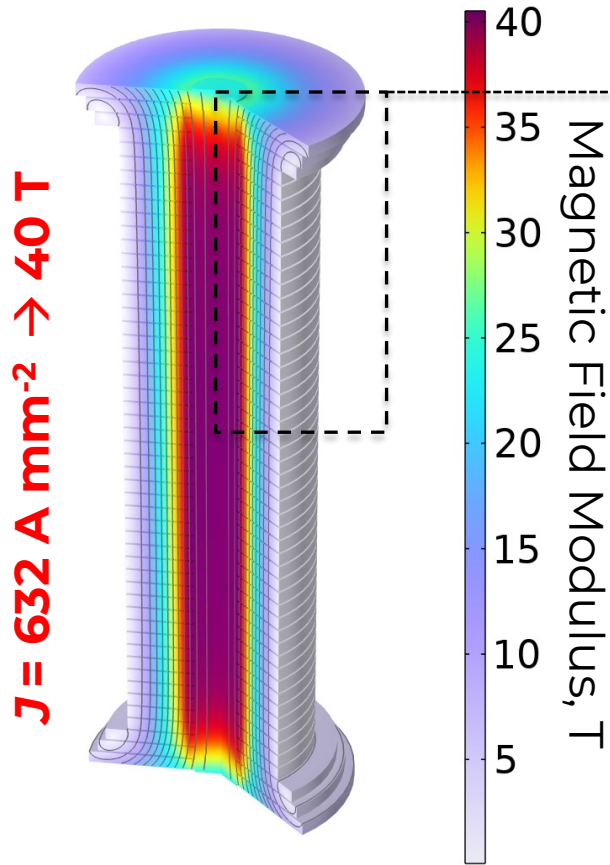
- For both, outermost winding diameter **$\sim 1.7 \text{ m}$**
- Hybrid Magnets: 33.5/29 T** from **resistive** insert, **11.5/11 T** by **superconducting** outsert
- their **large power consumption** (20-30 MW) is **unacceptable** for accelerator magnets

- Main specs** used for the CERN conceptual design
 - $B \geq 40 \text{ T}$** , aperture **$\phi \geq 50 \text{ mm}$** ,
 - field **homogeneity 1 %** over **0.5 m**
 - Energizing time 6 hrs** and **persistence 0.1 Units/s**

40+ T Conceptual design*

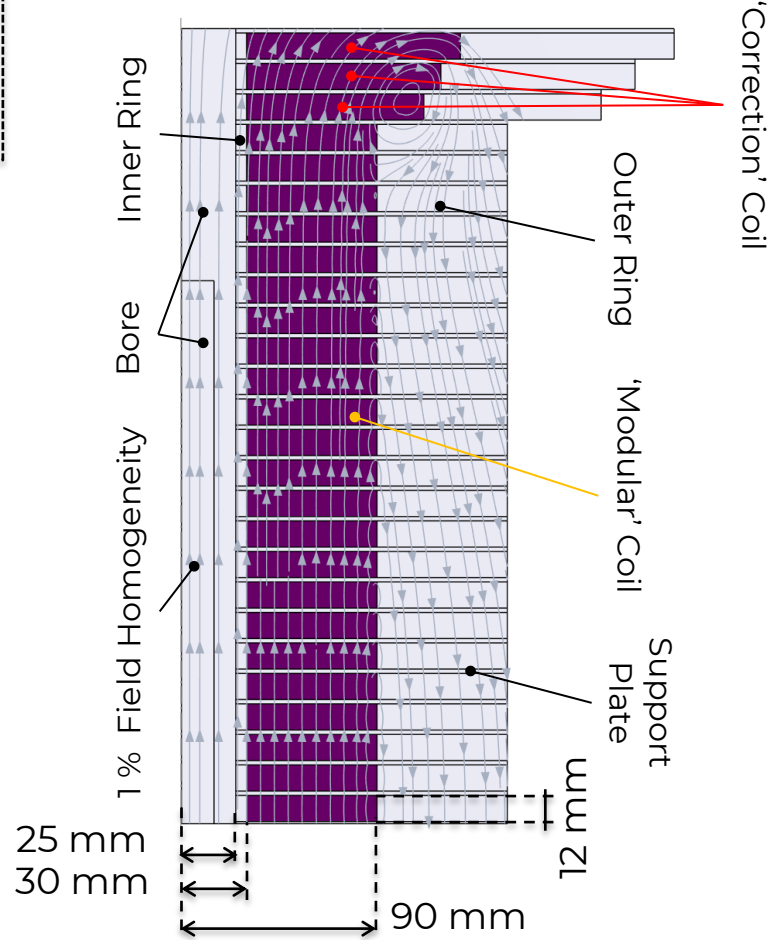
Ultra Compact Full ReBCO Solenoid

73 cm height 40 T solenoid
50 cm 1% field homogeneity



$J = 632 \text{ A mm}^{-2} \rightarrow 40 \text{ T}$

Cross Section of 1/4 Solenoid



1605 mm

Windings of the **Hybrid 45 T, 32 mm** user facility solenoid at **CHMFL**

574 mm

Winding of the **full superconducting** (15 T LTS, 17 T ReBCO) **32 T, 32 mm** user facility solenoid

180 mm

Winding of the **full ReBCO 40 T-50 mm** solenoid proposed for the Final Cooling

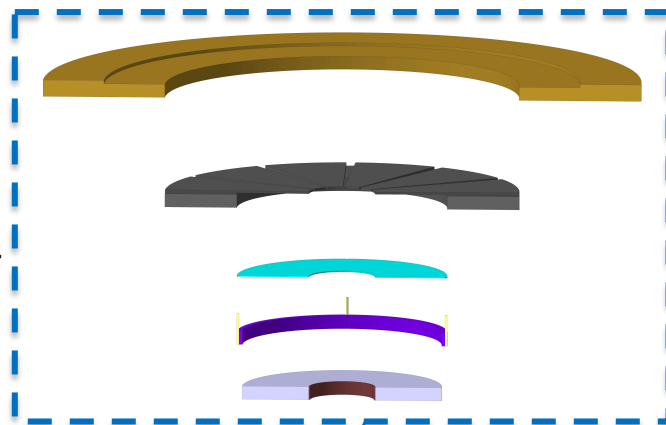
Two ReBCO double pancake coils

*B. Bordini et al., "Conceptual Design of a ReBCO Non/Metal-Insulated Ultra-High Field Solenoid for the Muon Collider," in *IEEE Transactions on Applied Superconductivity*, vol. 34, no. 3, pp. 1-10, May 2024

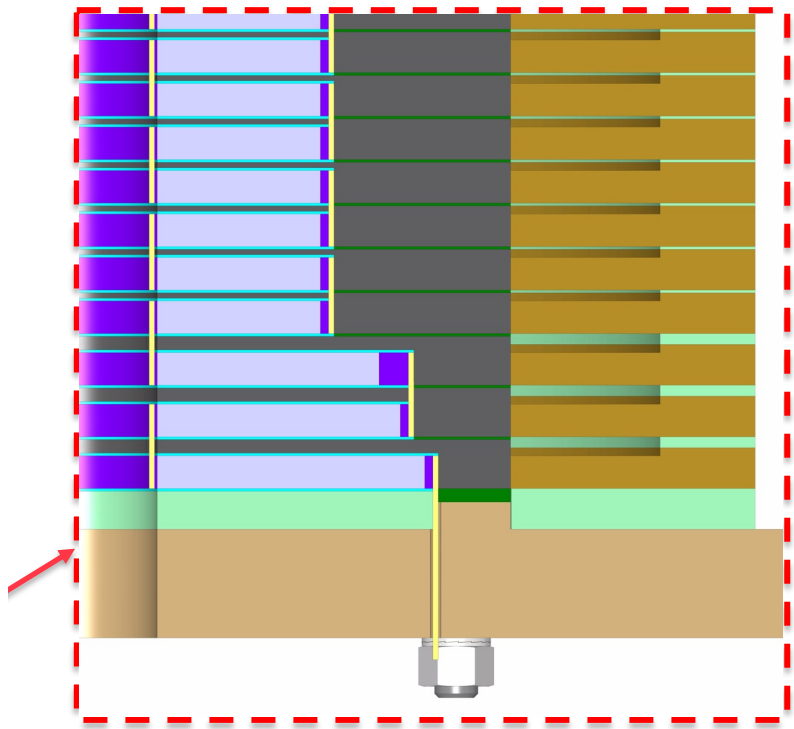
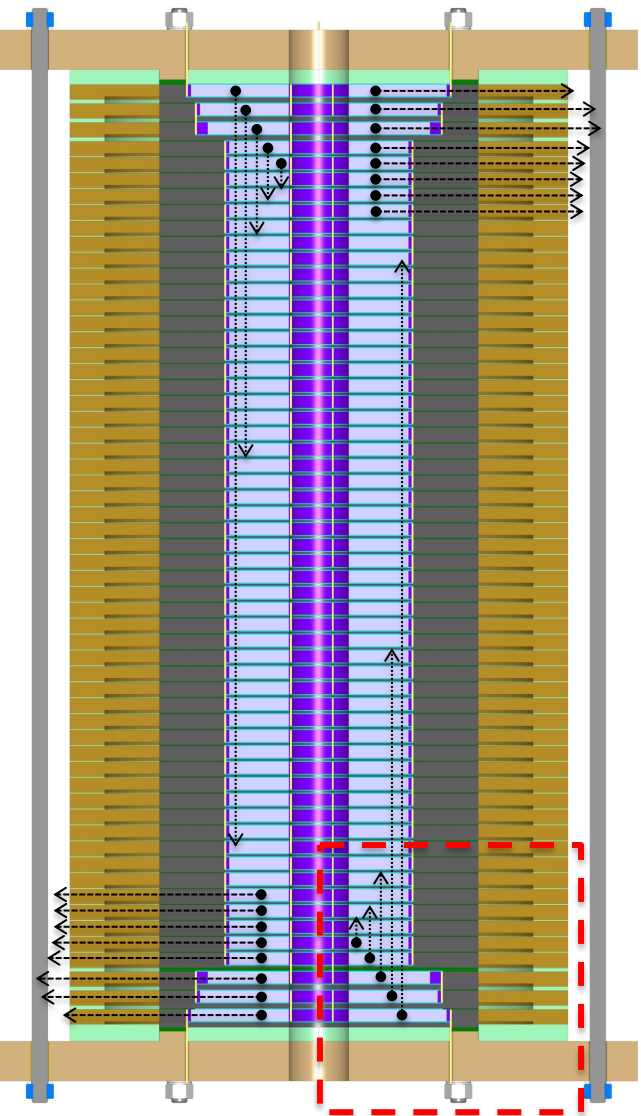
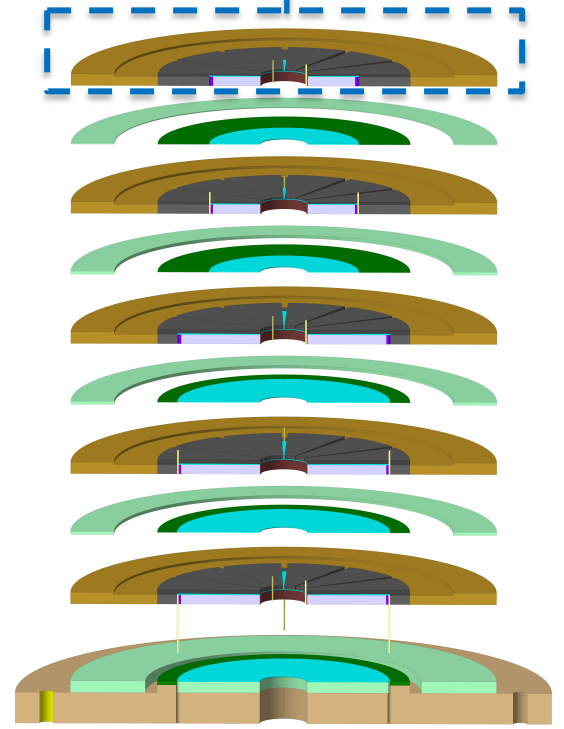
Advancing on the Engineering Design

F. Sanda, A. Kolehmainen,
C. Accettura, A. Bertarelli

'Explosion' of
the assembly of
one pancake



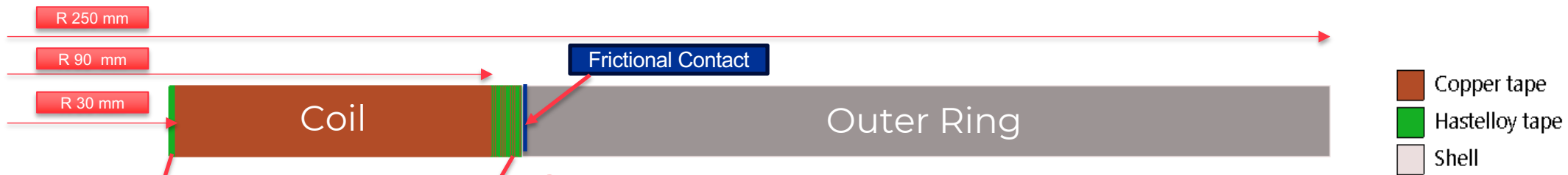
'Explosion' of the assembly
of the first 5 pancakes from
the bottom



Mechanical Analysis

2 D FEM : geometry

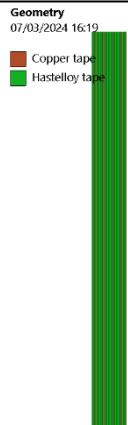
- Mechanical **Simulation** of a **modular coil**: all **750 coil windings** are **represented**
- The **Joint rings** and the **coil** are **wound** with **80 μm thick tapes (50 μm Hastelloy, 30 μm Cu)**



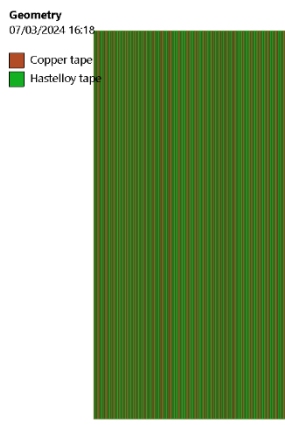
See Accettura et al. Poster 2LPo1B-03

- **3 different loading steps** simulated
 - **I pre-compression** via **shrink fitting**
 - the outer ring cools down to Room Temperature
 - **II cooldown** from RT to **4.2 K**;
 - **III energization** to 40 T
- The model accounts for
 - **Cu yielding**
 - **Thermal contractions** of the different materials

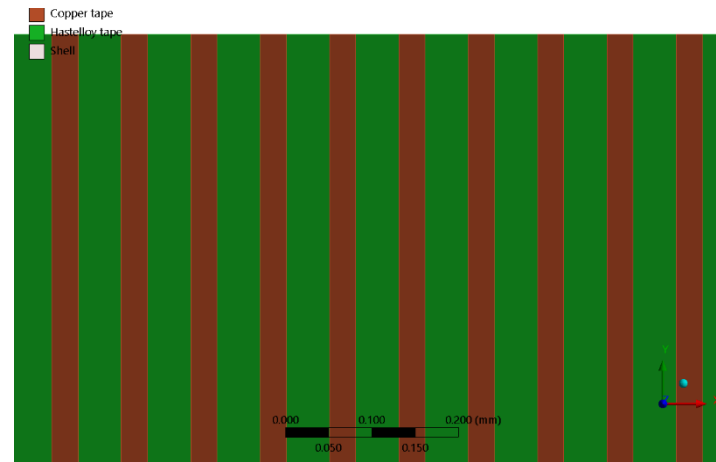
Inner Joint Ring 0.5mm or 1mm



Outer Joint Ring



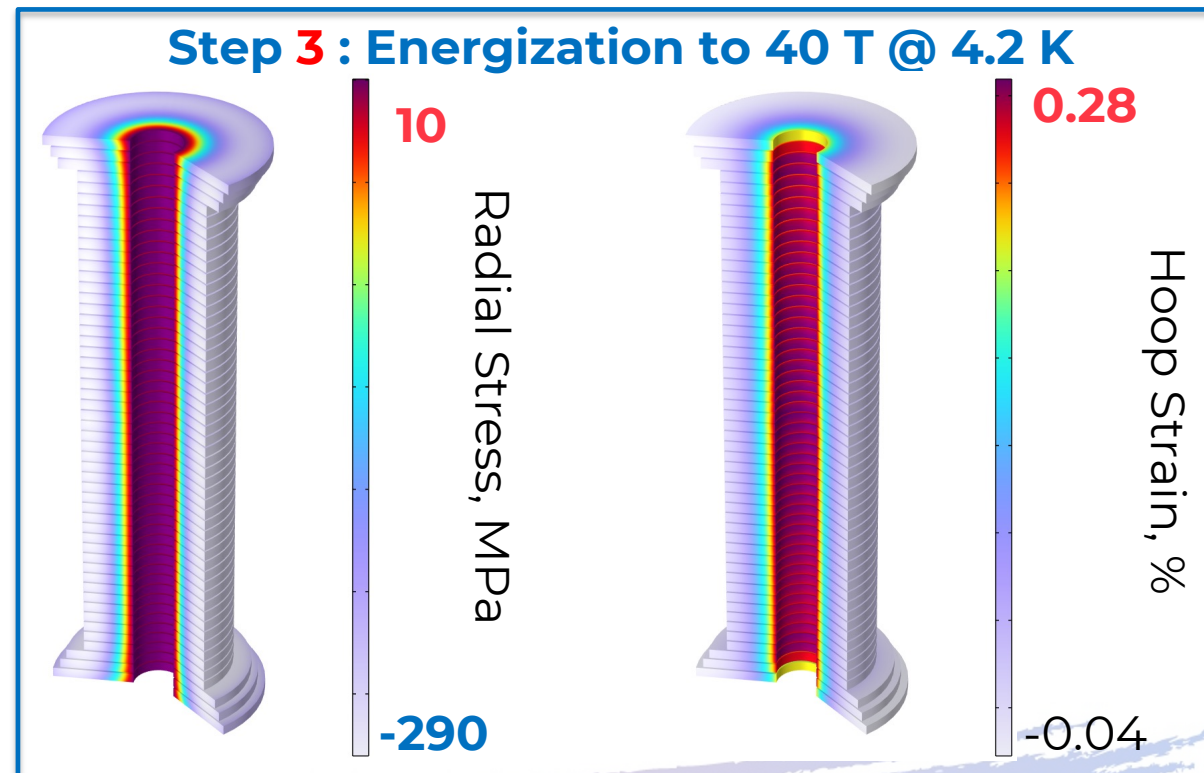
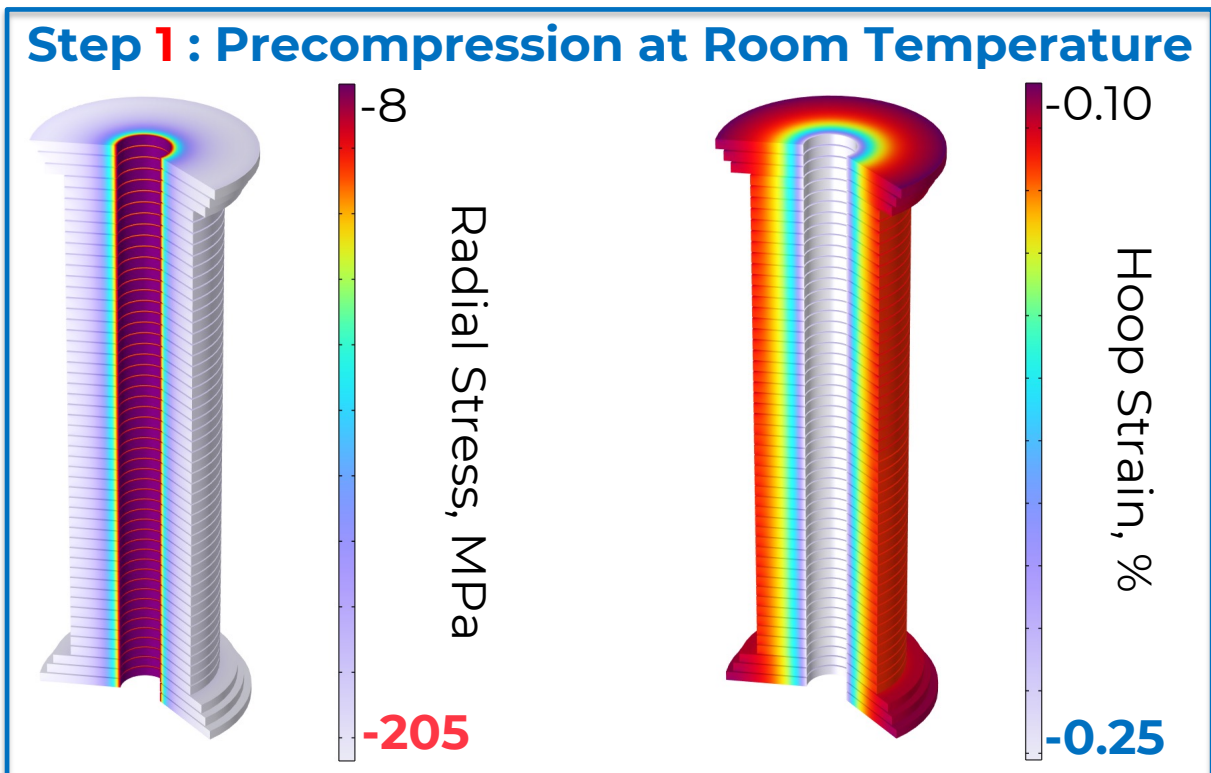
Coil



Mechanical Analysis

2 D FEM: ~200 MPa Pre-compression

Inner Joint ring thickness [mm]	Pre-compression at cold [MPa]	Min/Max <i>Radial</i> stress [MPa]			Min/Max <i>Hoop</i> Strain [%]		
		Step 1	Step 2	Step 3	Step 1	Step 2	Step 3
0.5	170						



Mechanical Analysis

2 D FEM : four Case Studies

Inner Joint ring thickness [mm]	Pre-compression at cold [MPa]	Min/Max <i>Radial</i> stress [MPa]			Min/Max <i>Hoop</i> Strain [%]		
		Step 1	Step 2	Step 3	Step 1	Step 2	Step 3
0.5	170	-205/-8	-190/-5	-290 /10	-0.25 /-0.10	-0.20 /-0.12	-0.04/ 0.28
	250	-318/-12	-258/-8	-367/7	-0.39 /-0.17	-0.31 /-0.16	-0.09/ 0.18
1	170	-205/-14	-190/-10	-288/19	-0.25 /-0.10	-0.2 /-0.12	-0.05/ 0.29
	250	-320/-21	-259/-15	-366/13	-0.39 /-0.17	-0.3 /-0.16	-0.09/ 0.18

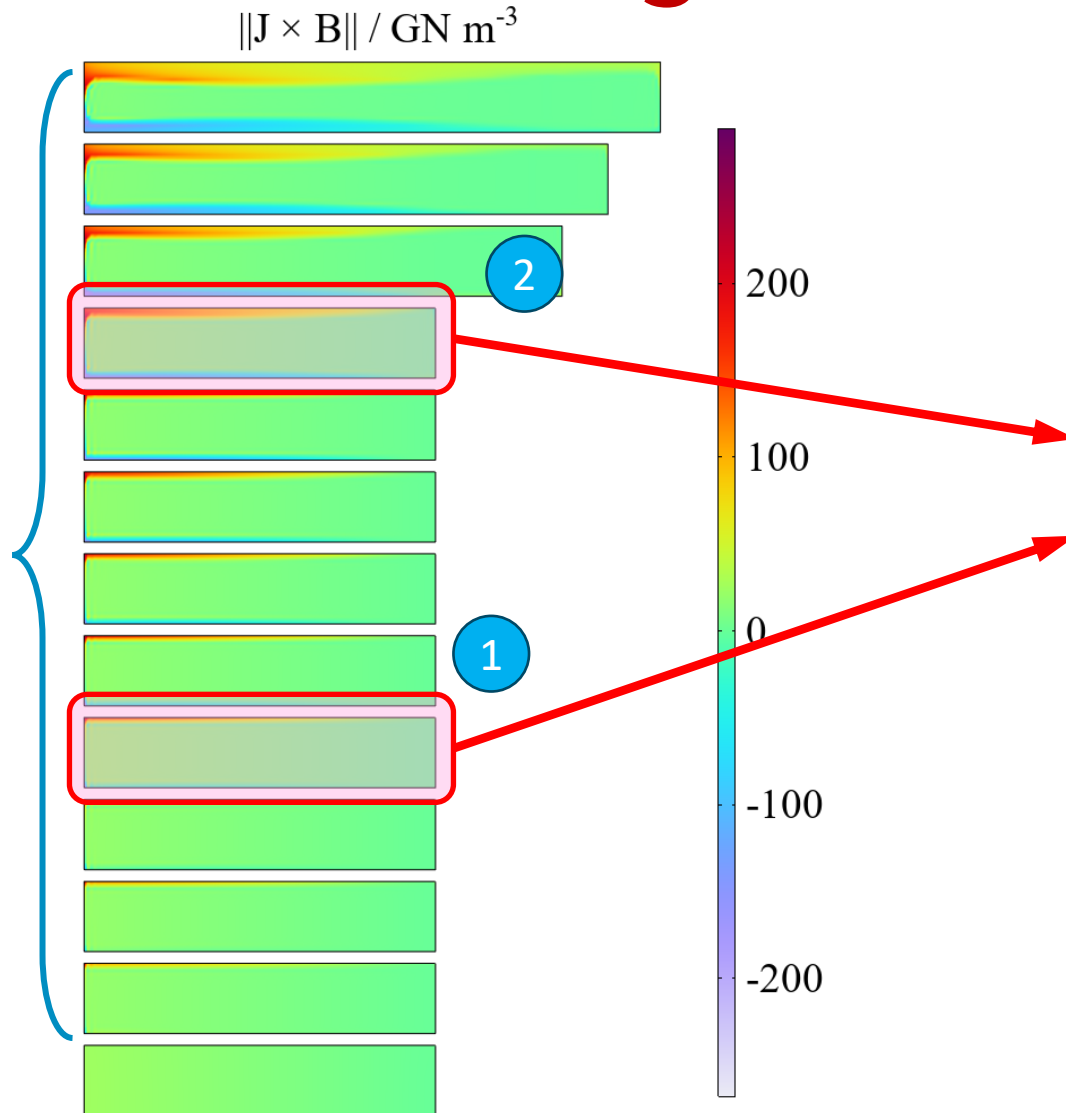
Mechanical **loads** are **under control** (in **stationary** operating **conditions** and **neglecting** the **solenoid heads** where the conductor get **magnetized**)

**See Accetura et al. Poster
2LPo1B-03**

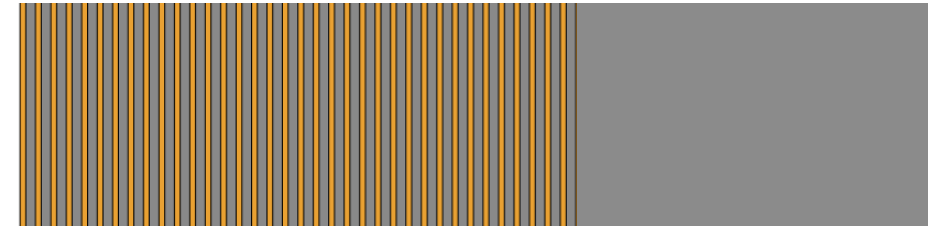
Electro-Mechanical Analysis

2 D FEM – Magnetization in Operation

Coils Electro
dynamics with
T-A Formulation



We study the mechanic,
with a detailed model to the tapes' scale



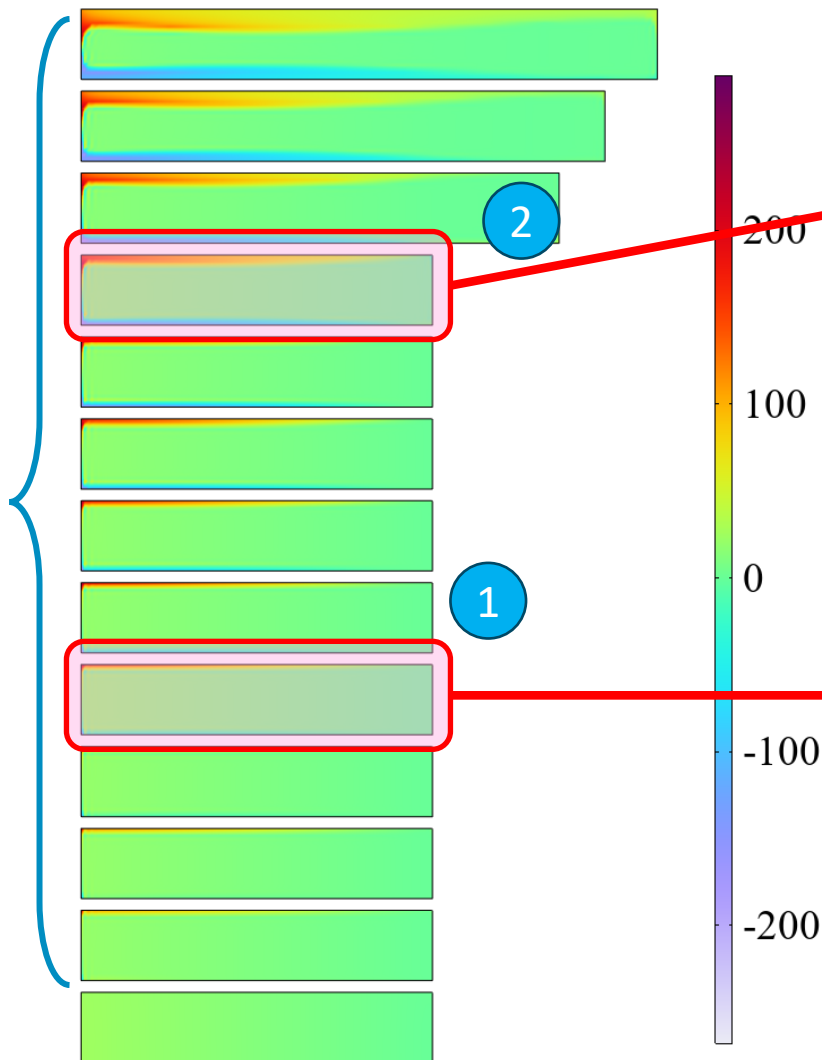
G. Vernassa

Electro-Mechanical Analysis

2 D FEM – Magnetization in Operation

$$\|J \times B\| / \text{GN m}^{-3}$$

Coils Electro
dynamics with
T-A Formulation



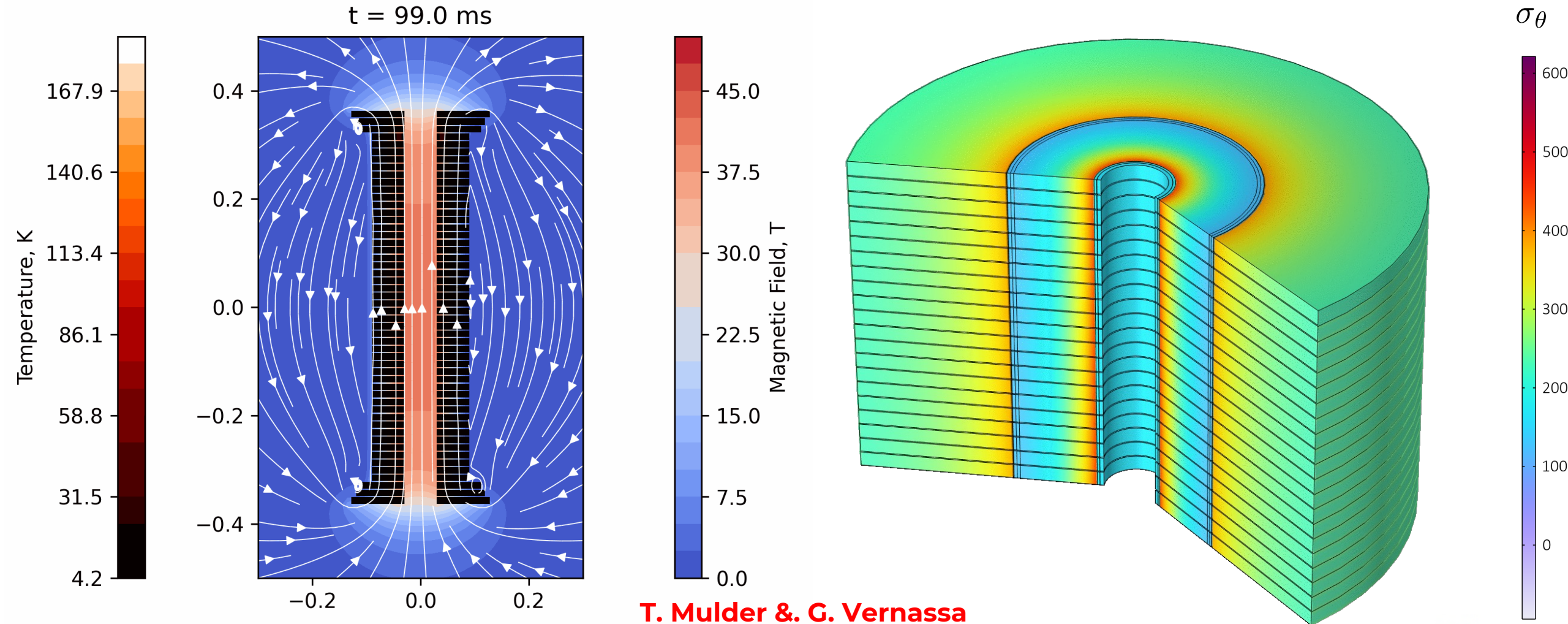
- Significant **Increase** of max **hoop strain ~30%**

- to be considered striated tapes as in magnet heads

- **Increase** of max hoop strain **negligible ~1%**

G. Vernassa

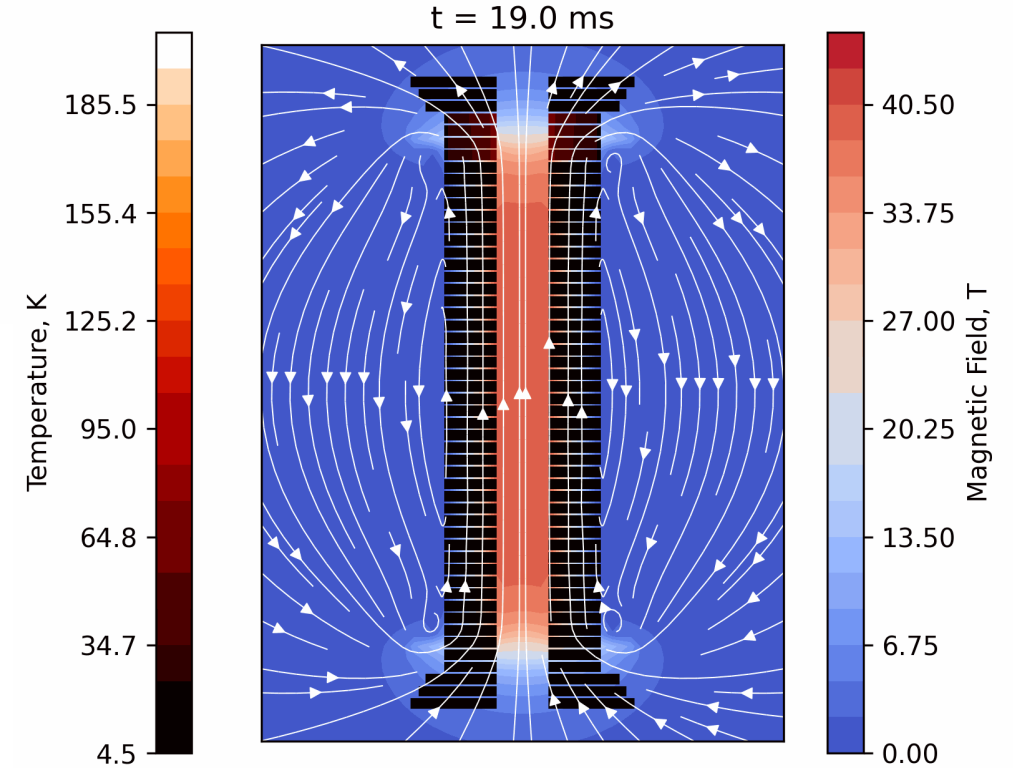
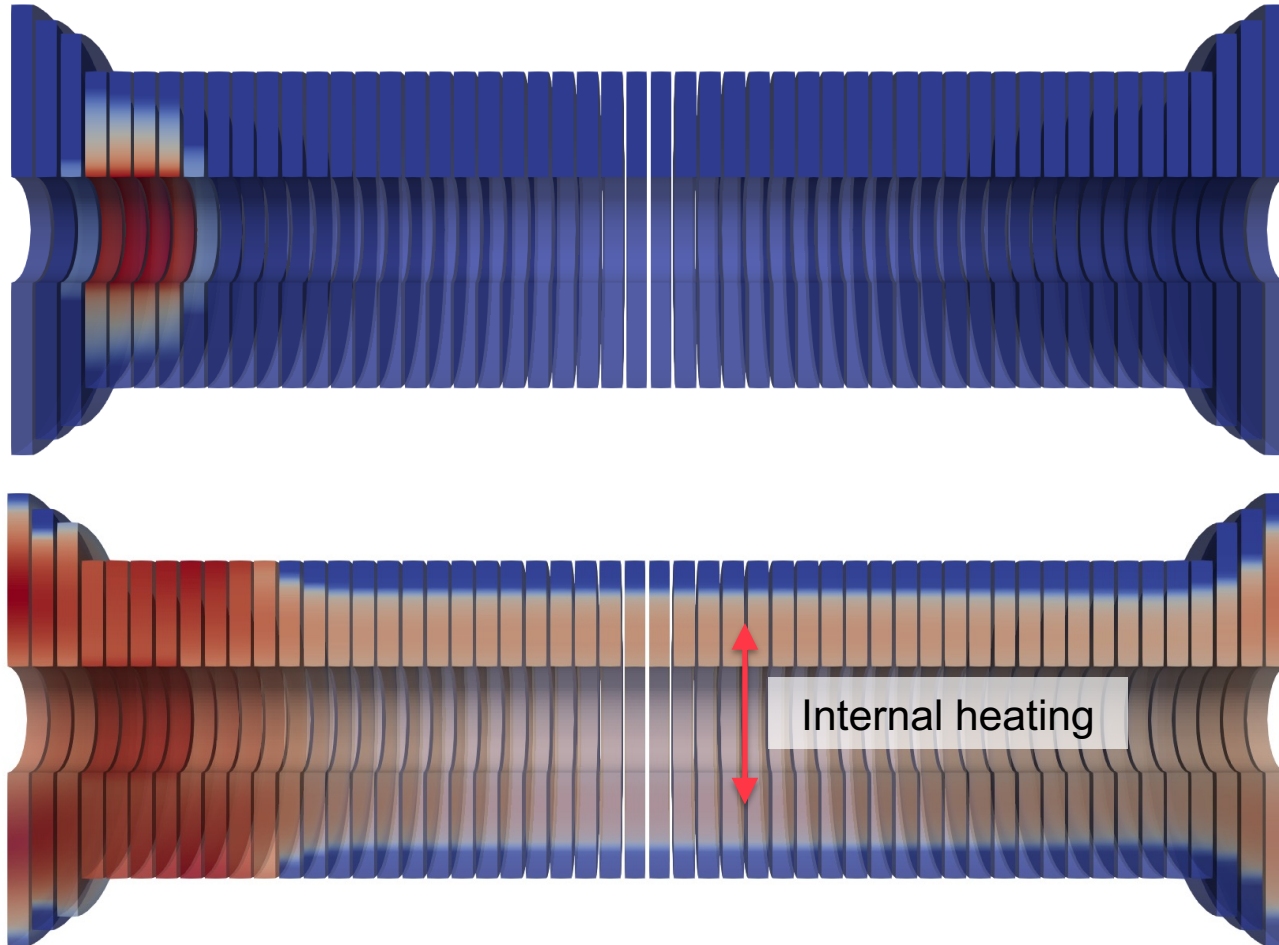
Integrated Mechanical-Electrodynamic simulations



T. Mulder & G. Vernassa

Protection Studies

See Mulder et al. Presentation
3J-ML-Or2A-04



- ✓ Magnet's turn-to-turn resistance used as internal quench heater.
- ✓ Good distribution of dissipated stored energy and a resulting peak temperature of below 200 K.
- ✓ No large induced currents, mechanically favorable solution.

3D electrodynamic models

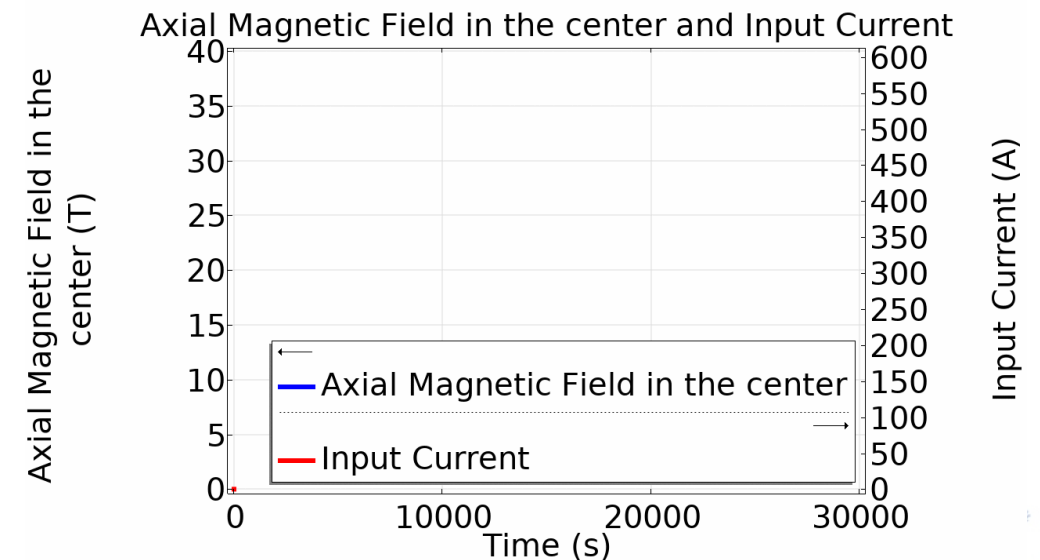
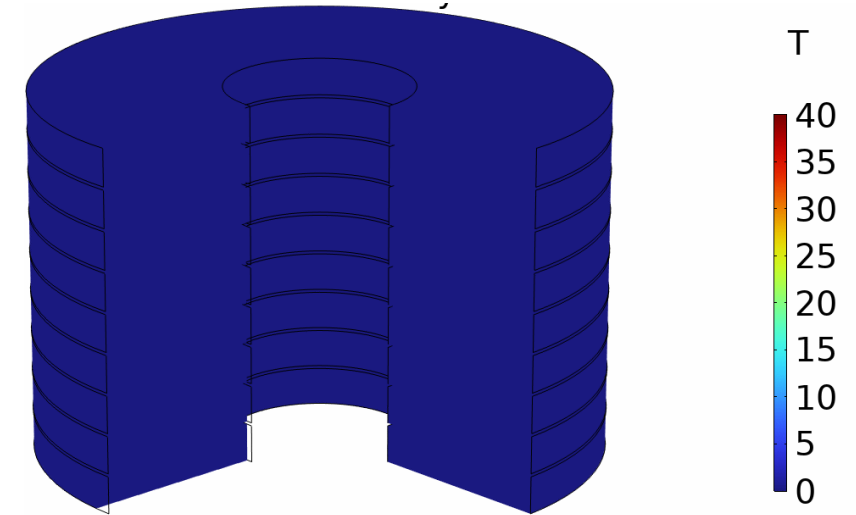
40 T Solenoid - Energization

Assumptions:

- **Infinite** number of identical **3D** pancakes
- Coil winding thickness **6 cm**
- **Conductor** made of **two tapes** (total thickness 160 μm)
- **750 layers** of conductor
- Tape width **12 mm**
- contact resistance, **10 $\mu\Omega \text{ cm}^2$**
- **2 mm** of air between coils

Only 1 hour computational time in a 2 k\$ PC !!!

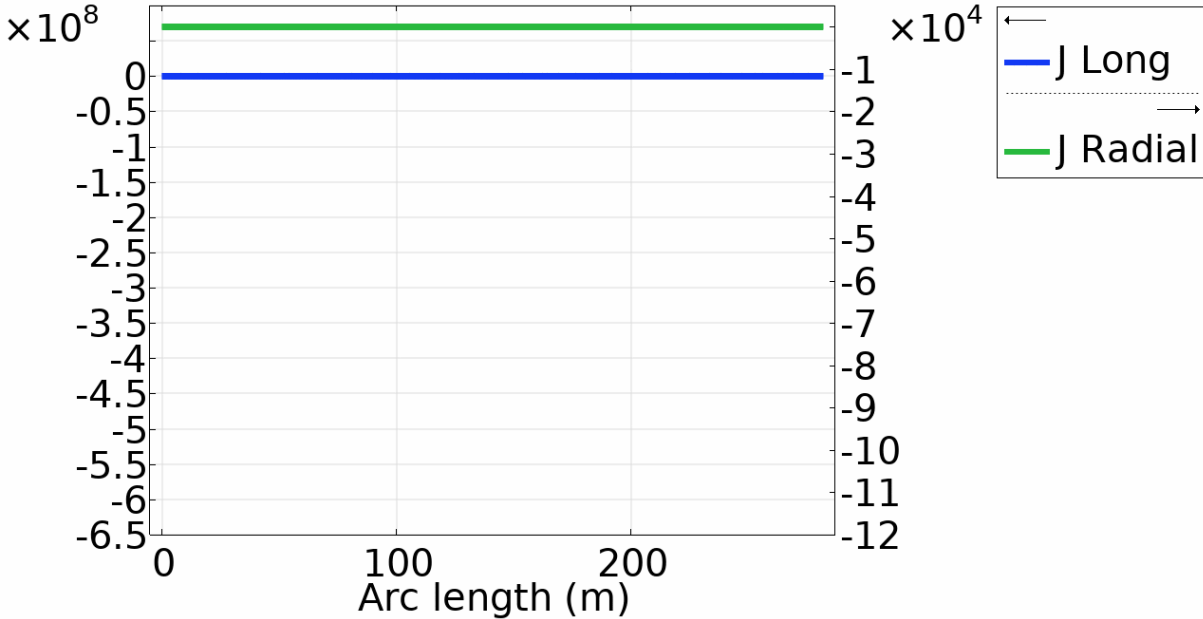
D. Rinaldoni



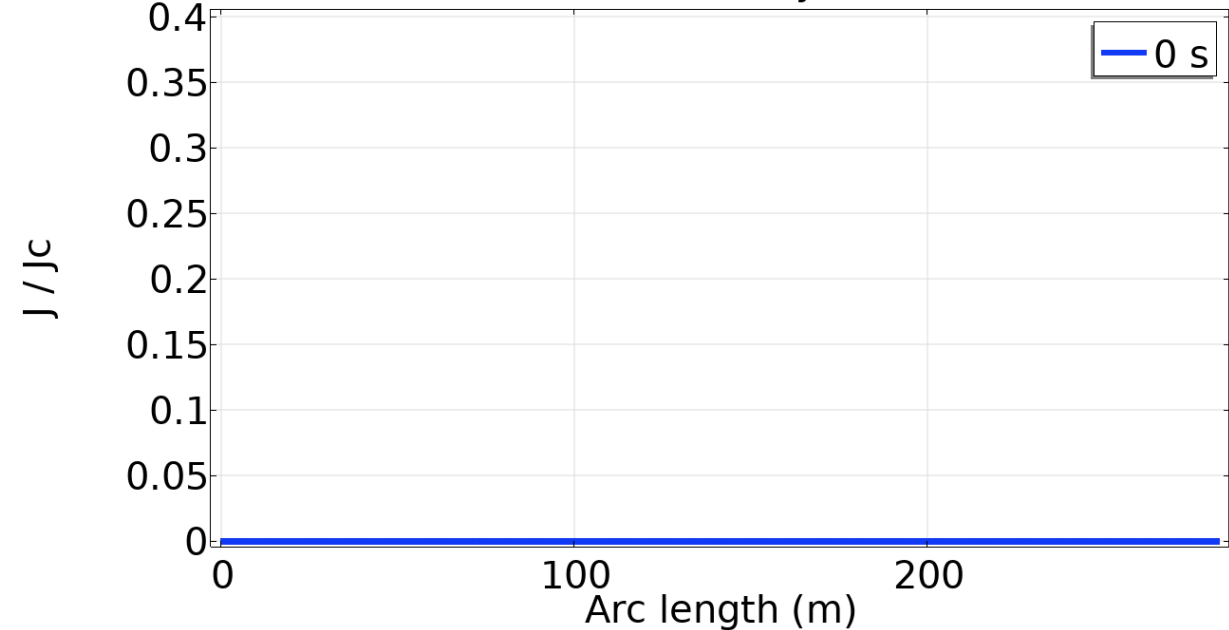
3D electrodynamic models

40 T Solenoid – Current Distribution

Time = 0 s Longitudinal Current in the Tape over time (A/m^2)



Ratio between Current Density and Critical Current.

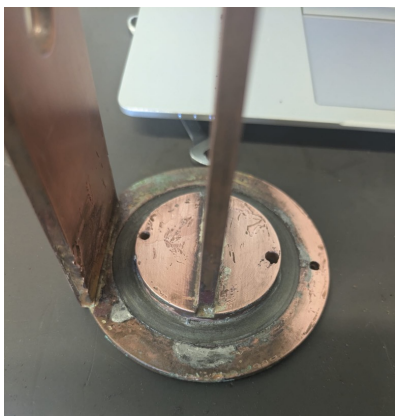


D. Rinaldoni

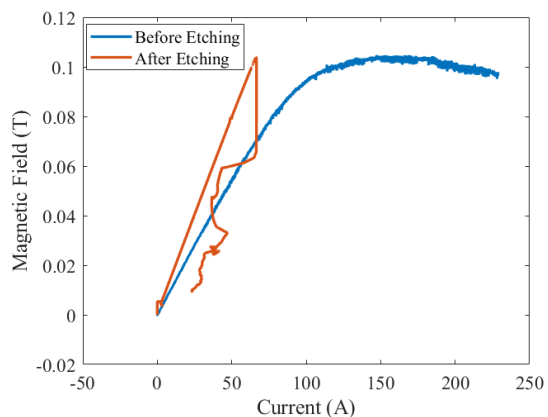
- **Large Current margin:** the current density along the superconductor is less than **40 %** of the **critical current**

Technological Studies

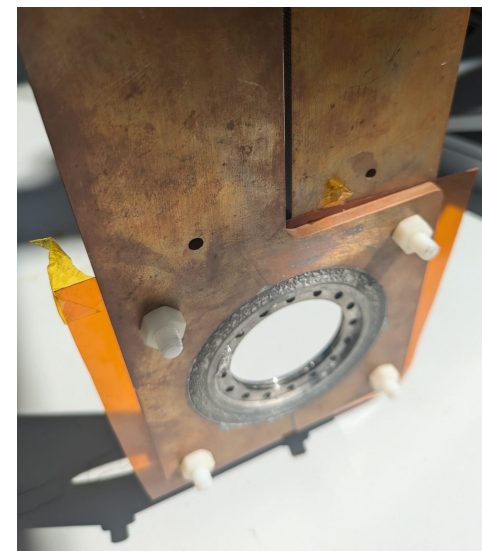
Fully soldered pancake



Energization Current	τ_c (s)	
	Before Etching	After Etching
5 A	4.9	0.042
10 A	4.7	0.041
20 A	4.8	0.030
50 A	4.6	0.052

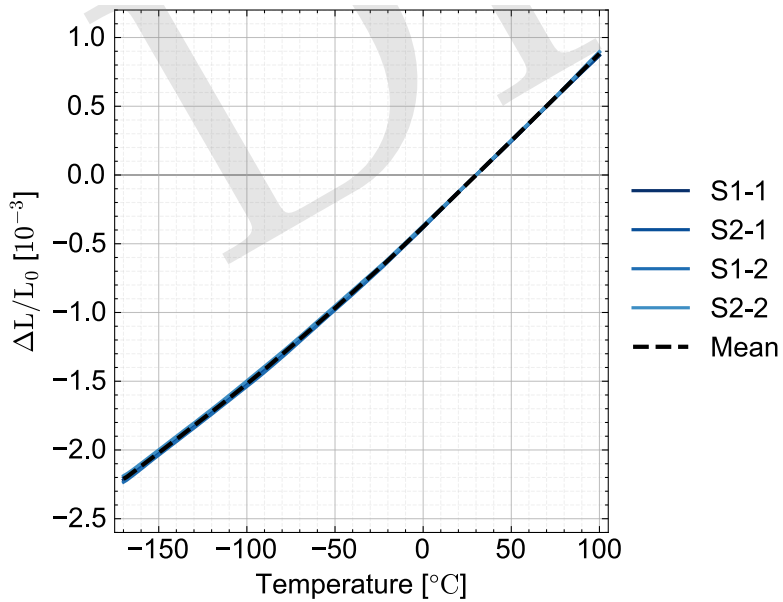


Single pancake

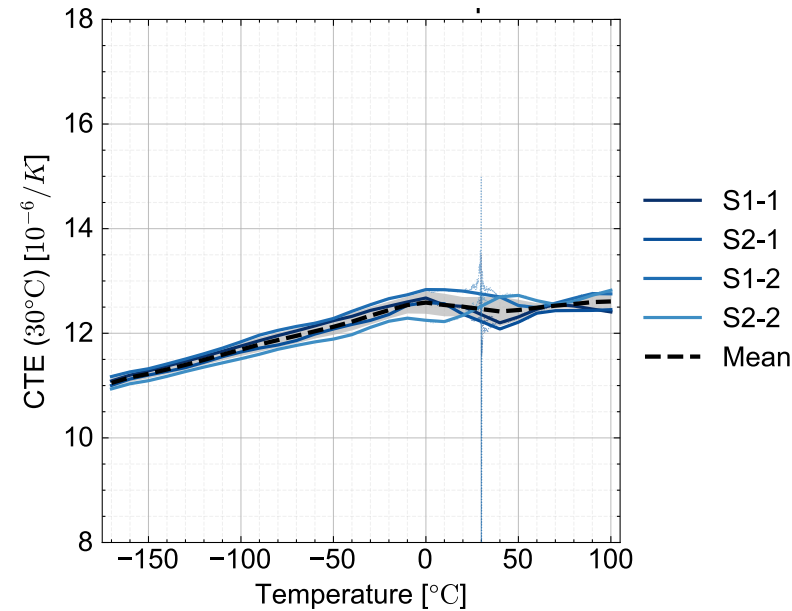


Double pancake configuration to be tested in the coming days

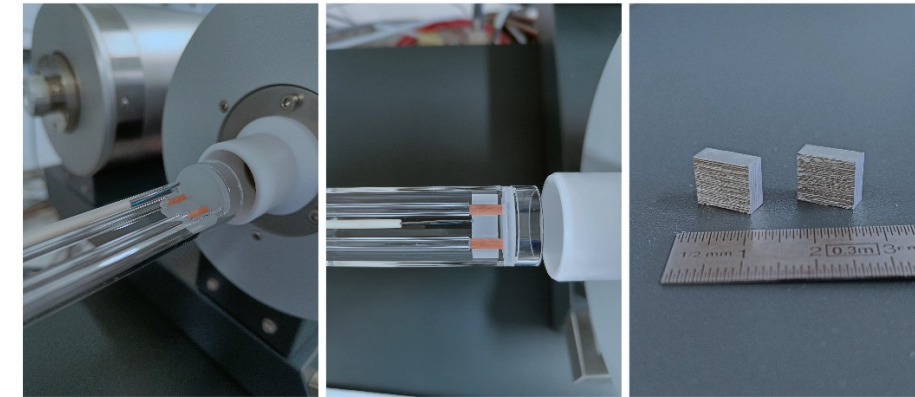
Stack Samples



(a) Relative change in length



(b) Coefficient of thermal expansion

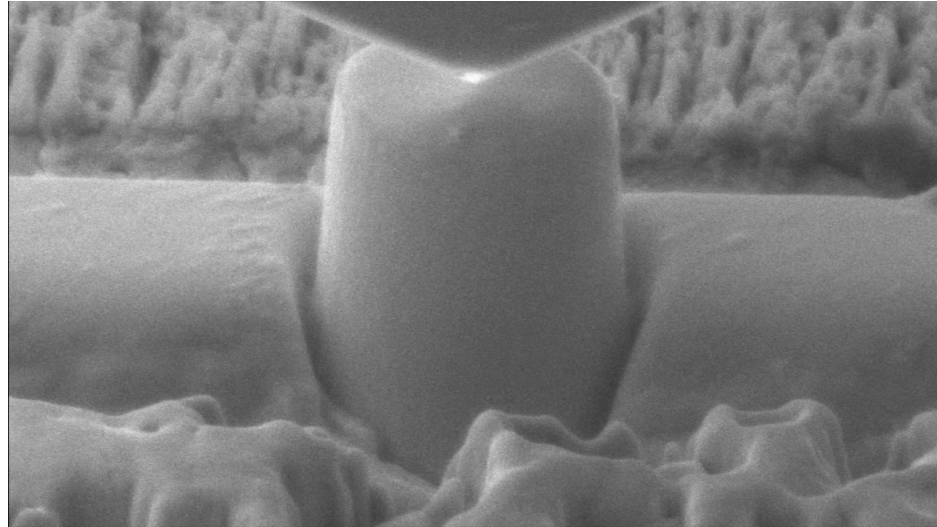


Sample holder including two samples of the Fujikura FESC-SCH04 tape

Thermal expansion measured for two samples of the Fujikura FESC-SCH04 tape

Courtesy of Stefan Hoell & Oscar Sacristian de Frutos, CERN

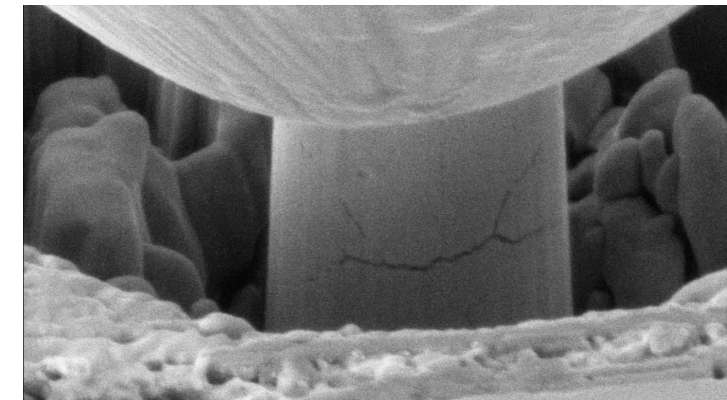
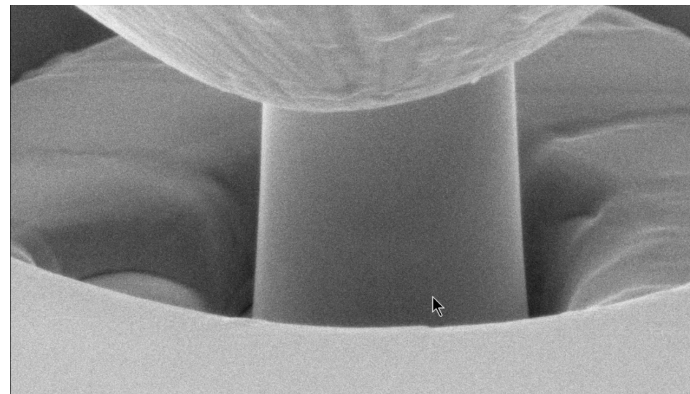
Micropillars Splitting at 300 K



***See Vernassa et al. Poster 2MPo2C-08**

Hastelloy	Copper
σ^y / GPa	σ^y / GPa
???*	???*

Micropillar compression on Hastelloy and Copper

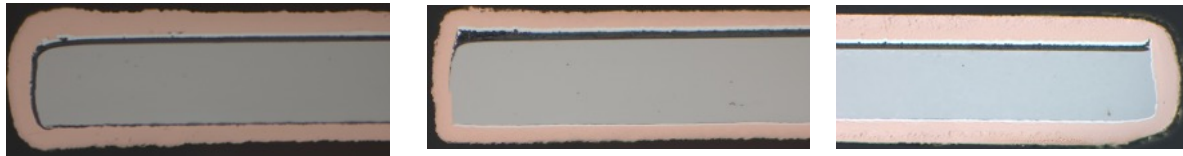


REBCO
$K_c / \text{MPa m}^{0.5}$
???*

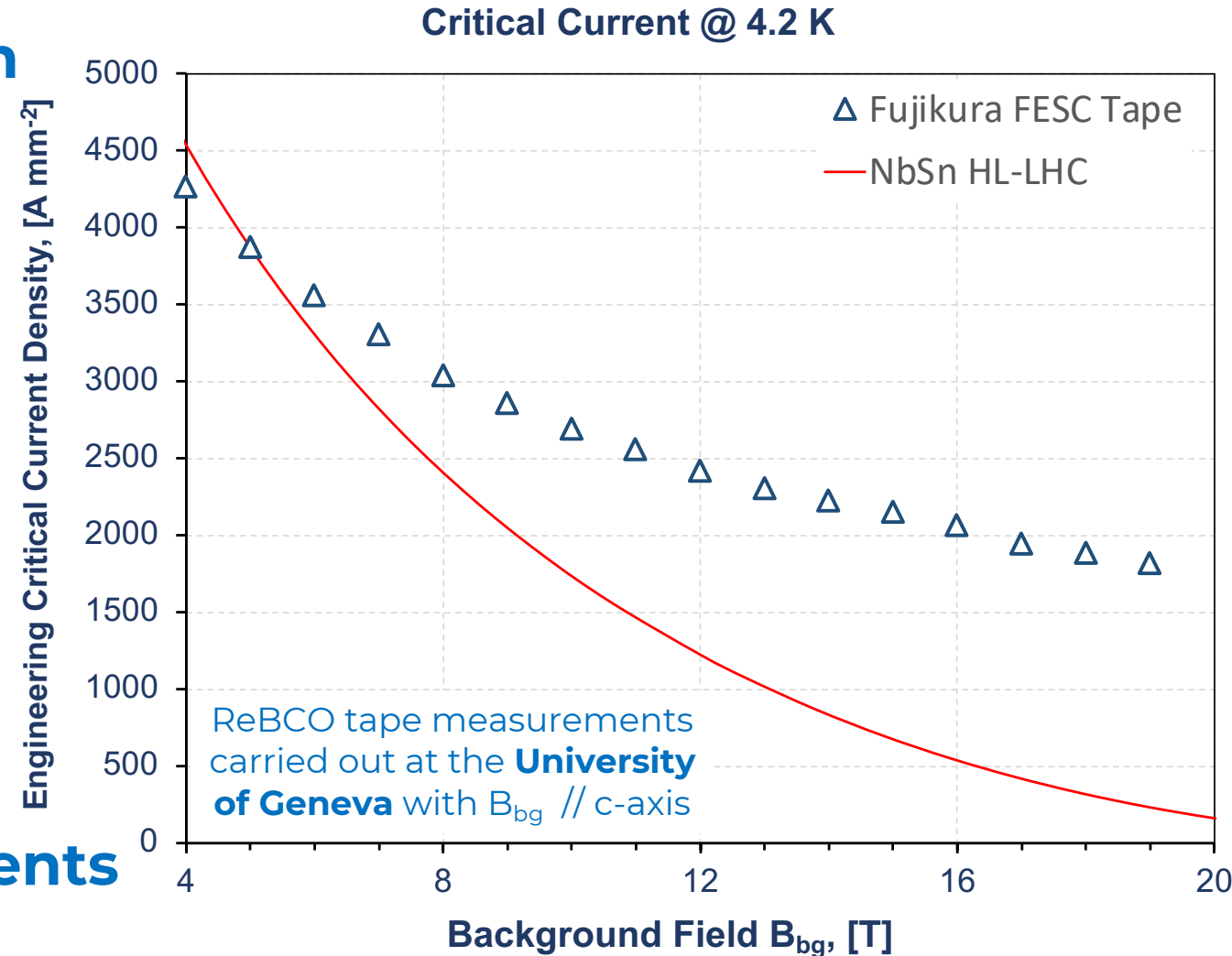
ReBCO Tape Procurement & Electrical Characterization

▪ **Procured** more than **10 km** of **4 mm** tape from 3 different companies

- Fujikura
- SST
- Faraday

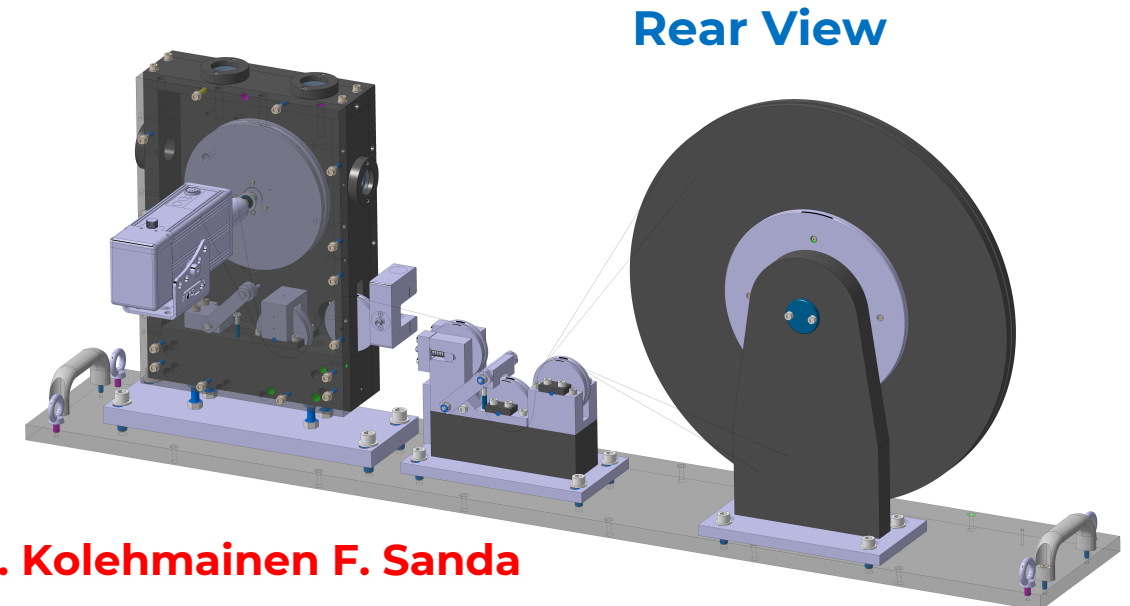
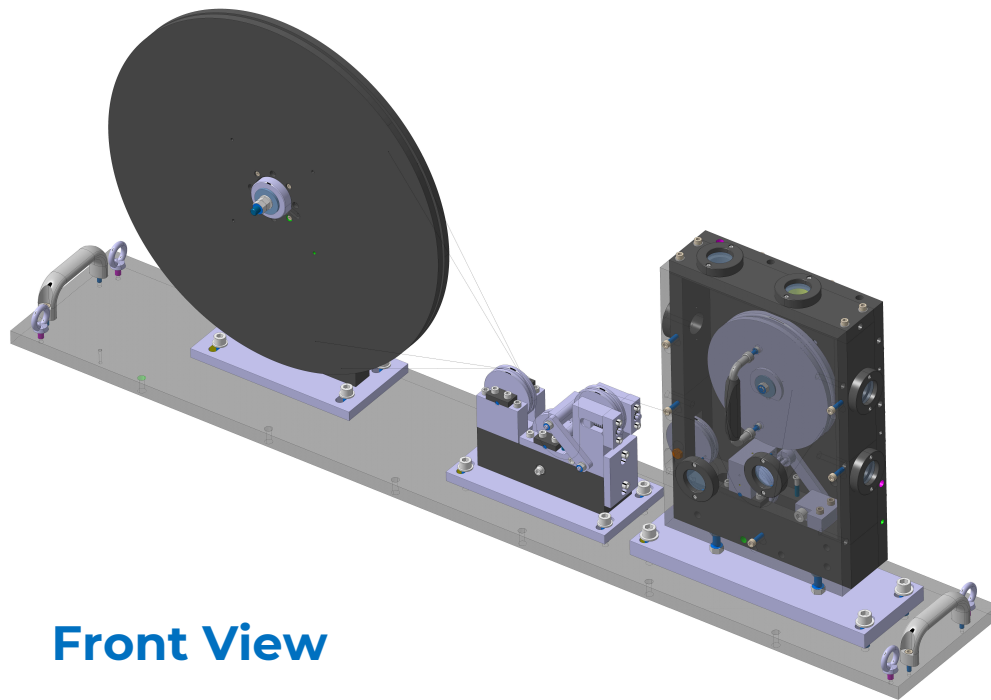


▪ Started **critical current measurements**

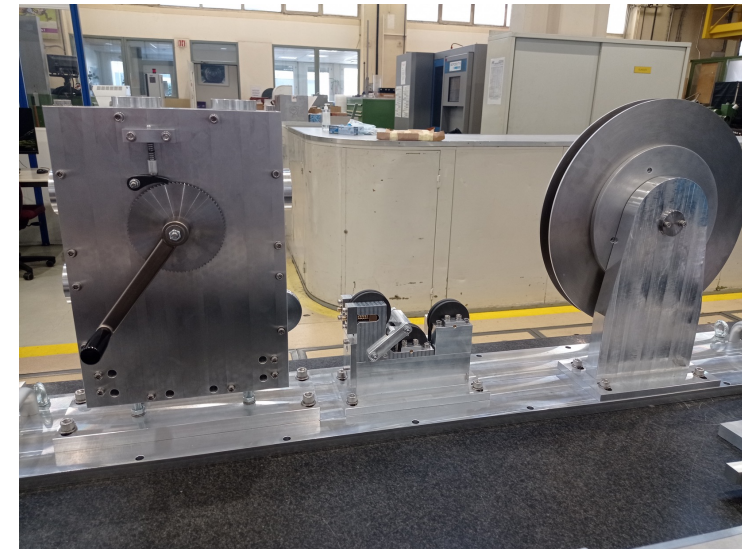
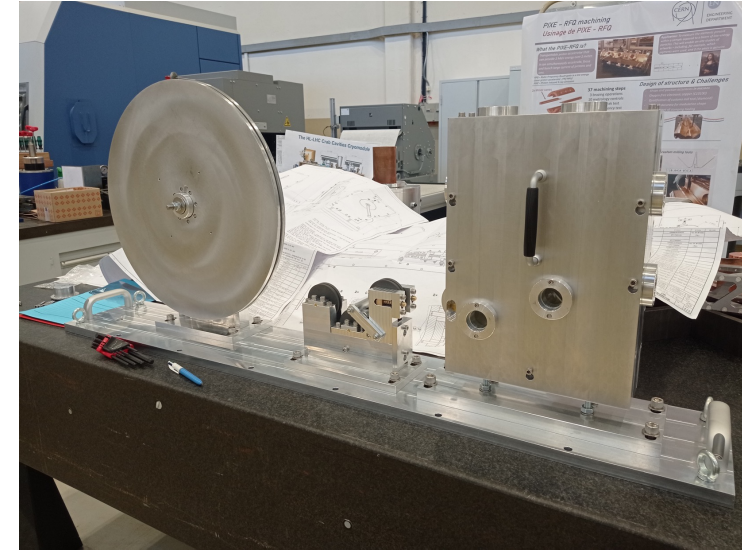
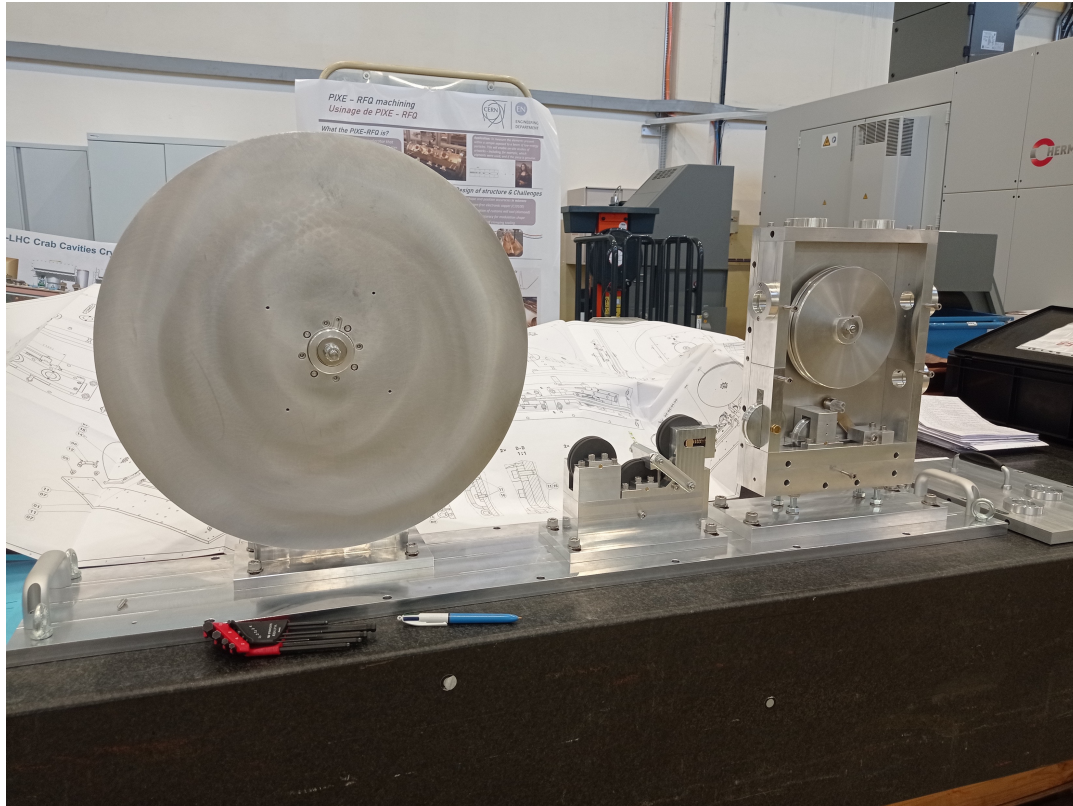


- **Designed** and **procured** the **components** of a **winding machine** allowing hot winding of soldered pancakes; **assembly** is expected starting **this week**

Ready to start manufacturing and testing pancakes in 'series' !!!



A. Dudarev , A. Kolehmainen F. Sanda



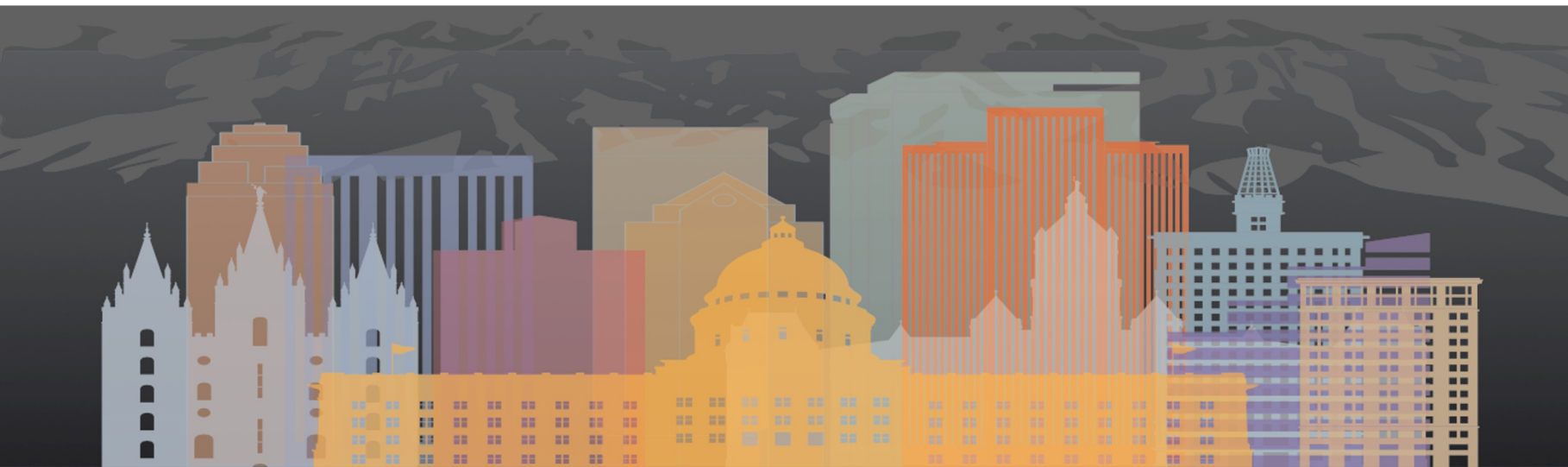
Y. S. Farys , Patrick Louis Bouvier, A. Dallochio, M. Garlasche

Conclusions & Next Steps

- Many activities on going, mostly focusing on the main **identified criticalities**:
 - The **electro-mechanical** design → **stresses** on the **conductor** are very large
 - The **electrodynamics** and **protection** of the magnet → **complex transients** to control
- The project is **challenging** but **no show-stoppers** appeared **so far** and we are a **growing team** strongly **motivated**
- With the arrival of the winding machine, **experimental activities** and the **manufacturing & testing** of **pancakes** will significantly **increase**



Thank You For the Attention



A
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C

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SALT
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SEPTEMBER 1 - 6



SALT PALACE CONVENTION CENTER