



# Mechanical characterization of REBCO CC layer materials at the microscale

**Gianluca Vernassa**  
PhD Candidate at the  
École des Mines de Saint-Étienne



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G. Kermouche, M. **Rusinowicz**, S. **Kalacska**, S. S. **Joao**, J.M. Bergheau and L. Bottura, H. Felice, B. Bordini.



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[10.36227/techrxiv.172962986.60466462/v1](https://doi.org/10.36227/techrxiv.172962986.60466462/v1)





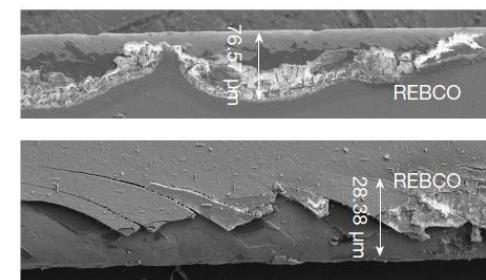
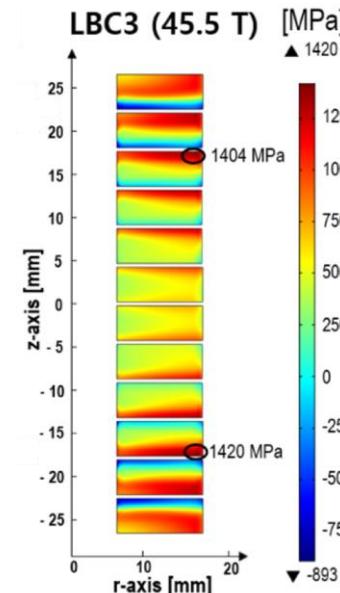
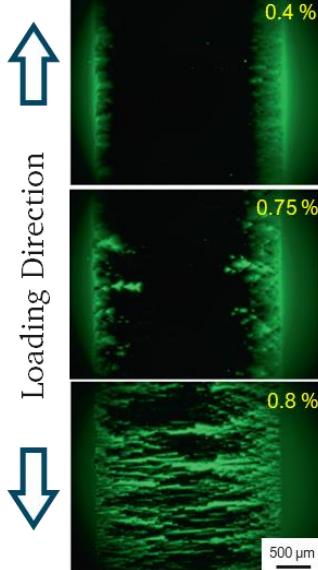
# Outline



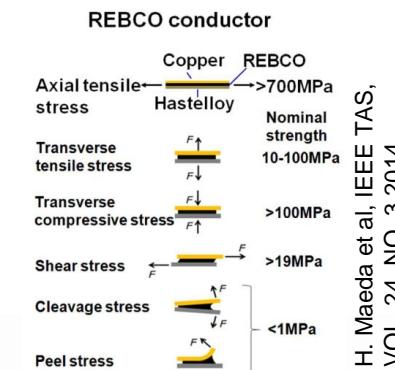
- Background
  - 1. Nanoindentation
  - 2. Micropillar compression
  - 3. Micropillar splitting
- Conclusions & Next steps
- Discussion

# Why material properties ?

- High field → **high stresses**
  - Plastic deformation
  - Delamination



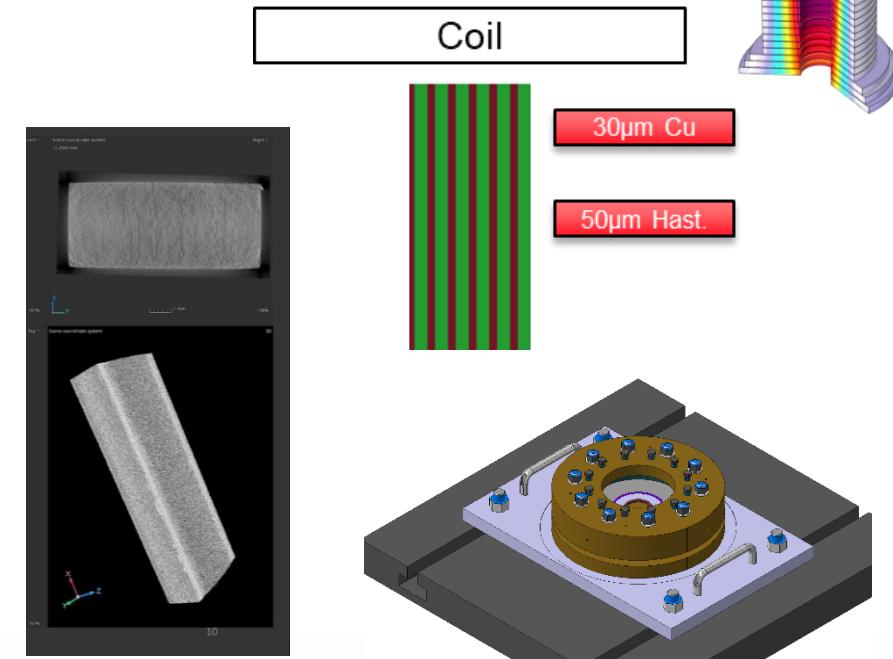
Xinbo Hu et al 2020 Supercond. Sci. Technol. 33 095012



$$p_m = \frac{B^2}{2\mu_0}$$

$$p_m(50 \text{ T}) \sim 1 \text{ GPa}$$

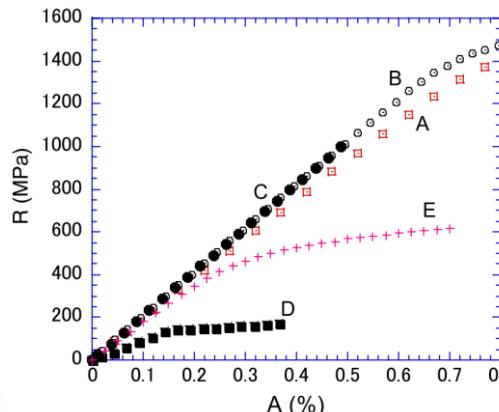
For the 40 T FC Solenoid:  
**extensive material characterization & modeling**



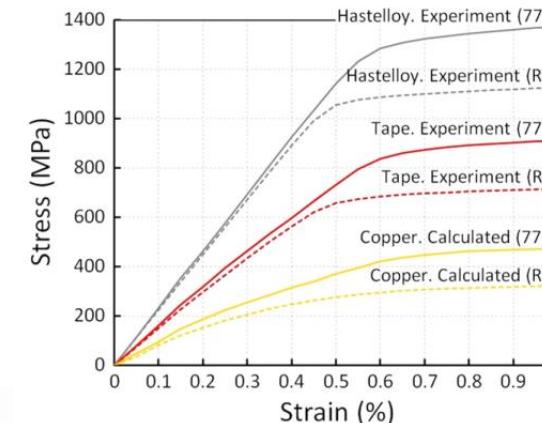
C. Accettura - Magnets R&D for the Muon Collider Study - <https://indico.cern.ch/event/1476966/>

# Characterization: at which scale ?

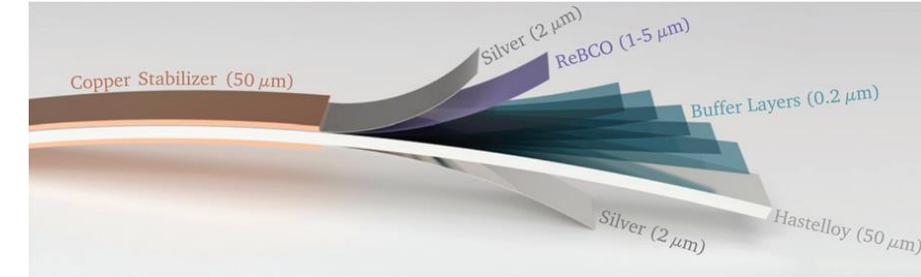
- REBCO CC are made of several thin layers (**0.1 – 100 μm**) of materials which behave mechanically very differently.
- The **limiting factors** for our applications (critical current degradation, delamination, etc.) occur at the **micro** scale.
- For a deeper understanding of the degradation mechanisms, we have to rely on properties measured at a coherent scale.



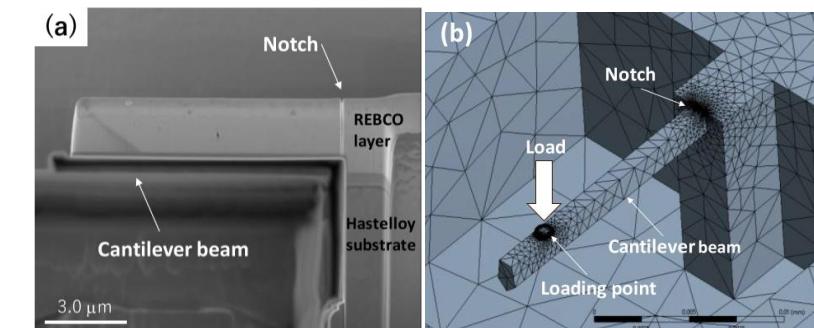
K. Osamura et Al., Supercond.  
Sci. Technol. 22 (2009)



Ilin et Al., Supercond. Sci.  
Technol. 28 (2015)



J. Van Nugteren, 2016



S. Muto et al., IEEE TAS 30, 4, 2020



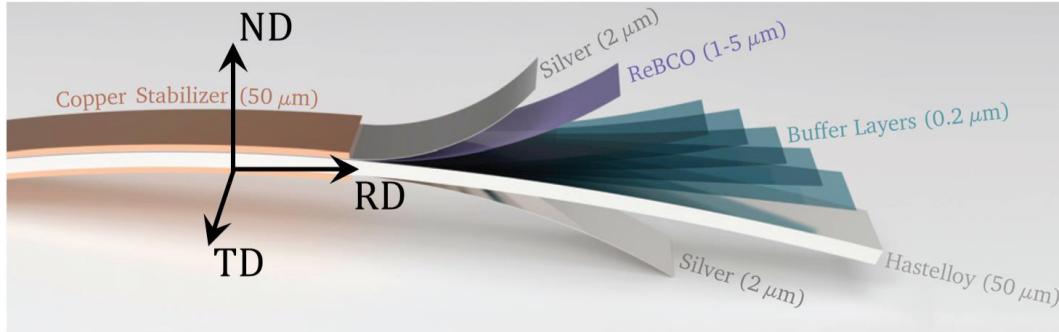
# Methodologies proposed



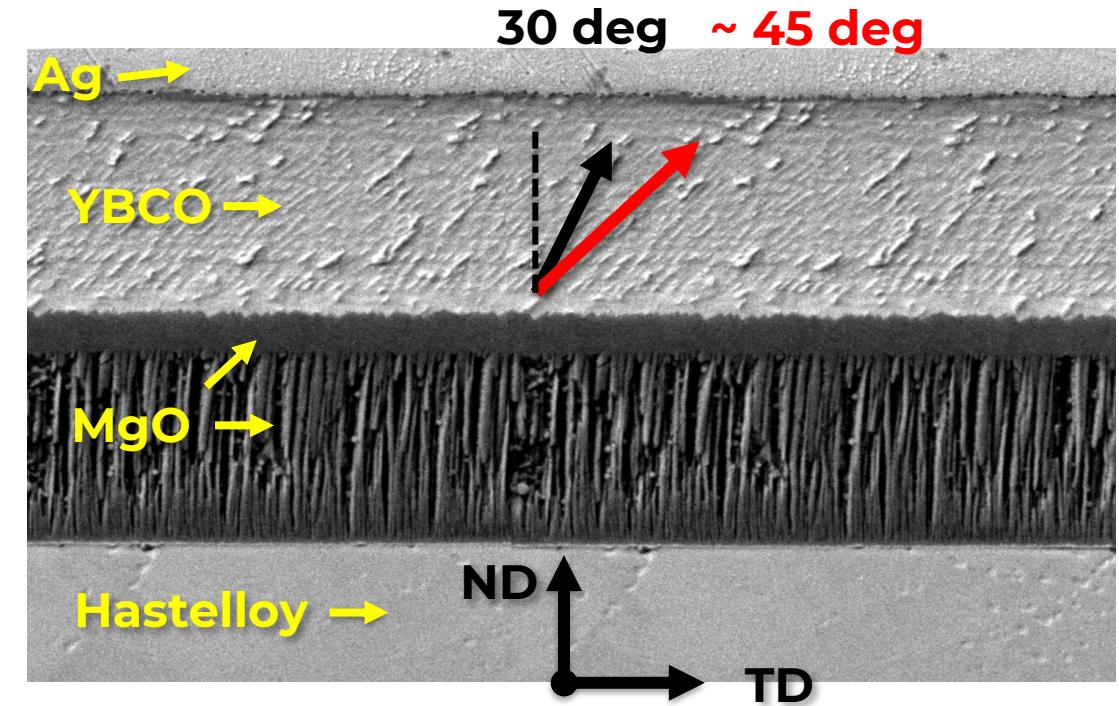
- Background
  - 1. Nanoindentation → Elastic-plastic behavior
  - 2. Micropillar compression → Plastic flow
  - 3. Micropillar splitting → Fracture toughness
- Conclusions & Next steps
- Discussion

# Materials: YBCO tape from THEVA®

- THEVA® TPL4000-series: Inclined Substrate Deposition (30 deg)

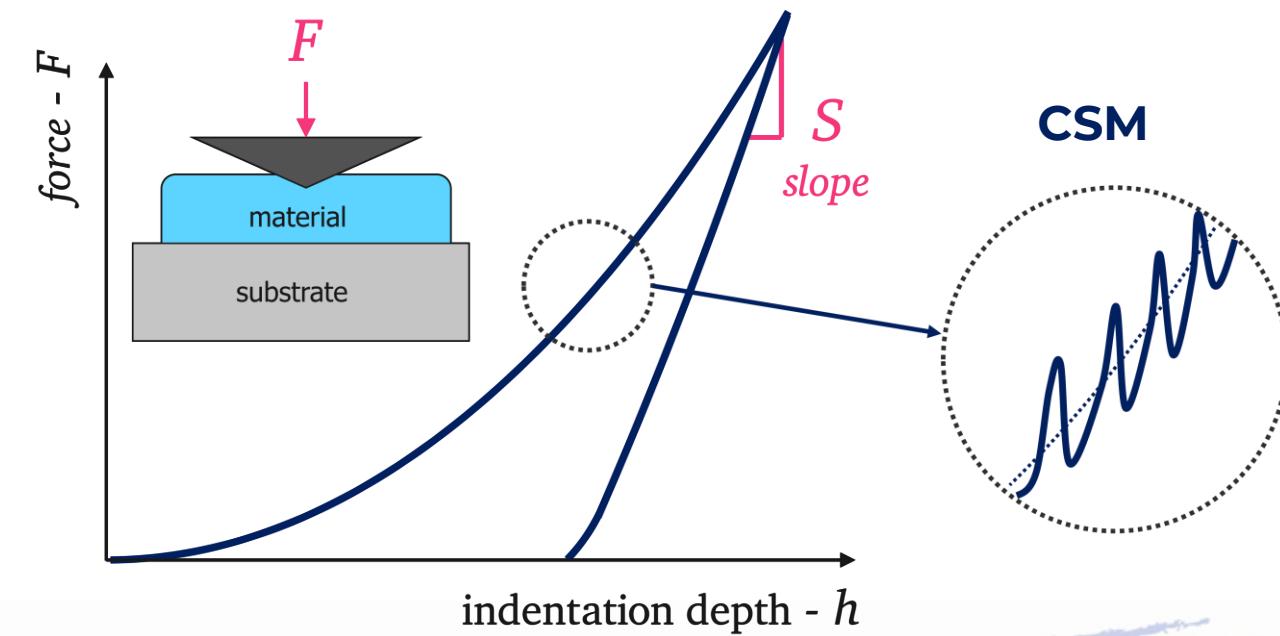
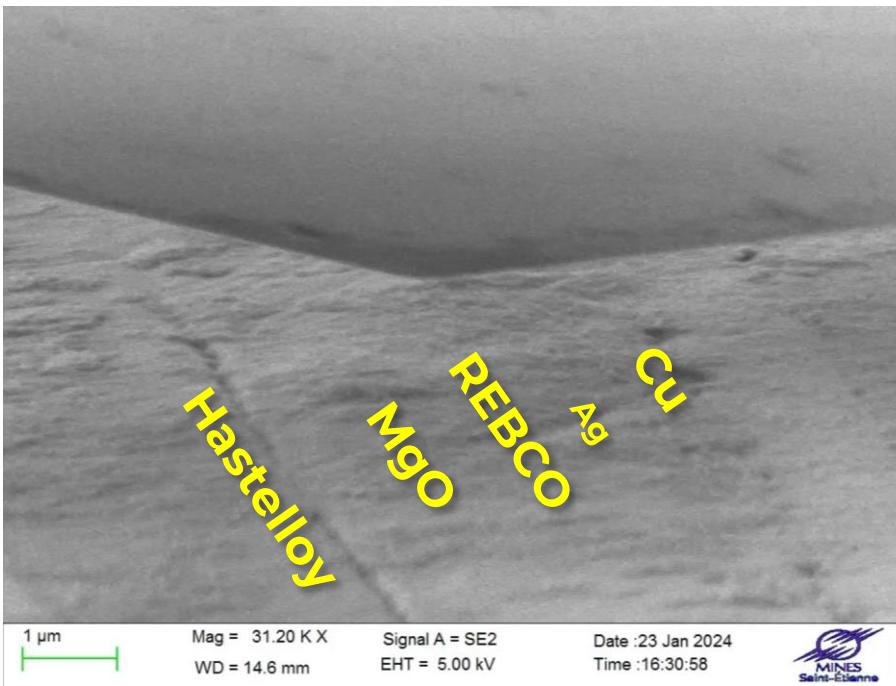


J. Van Nugteren, 2016



# Nanoindentation: Introduction

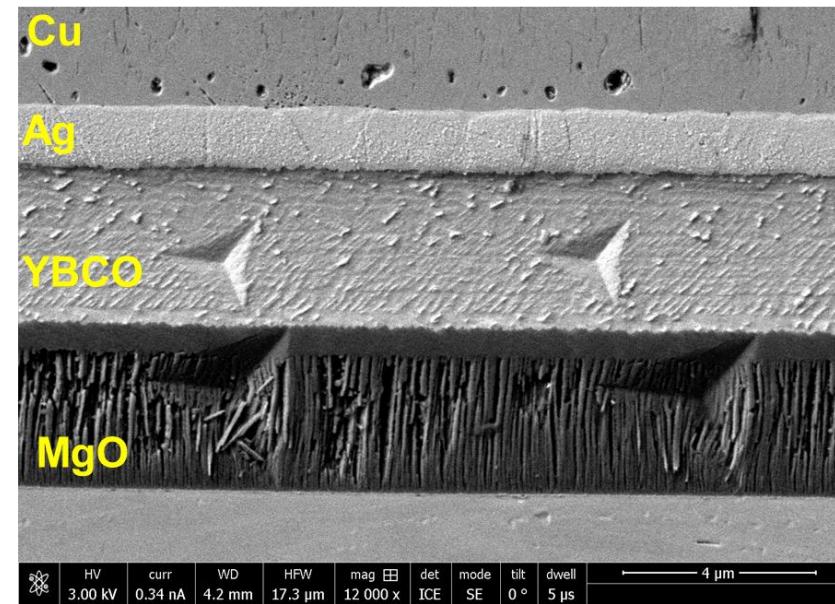
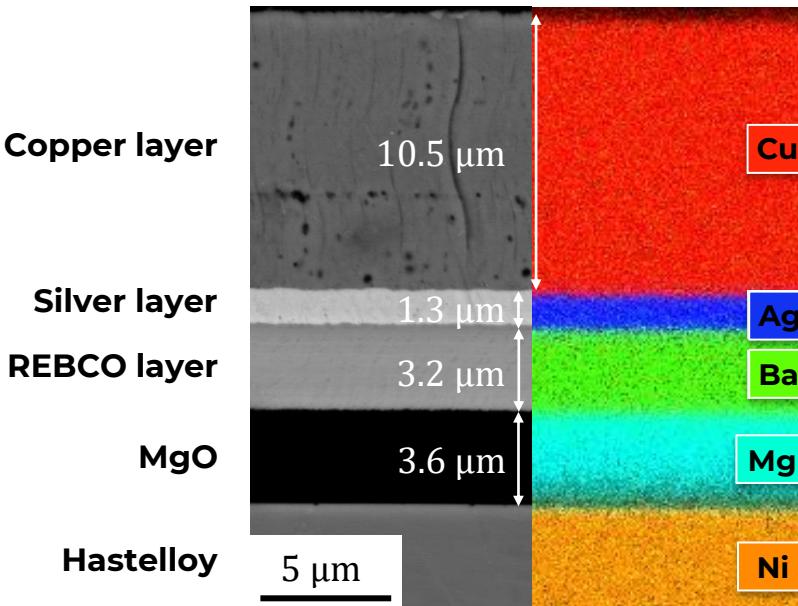
- Applying a controlled load  $F$  to a diamond tip and monitoring the penetration depth  $h$  inside the material.
- We measure the contact stiffness  $S$  and obtain the elastic modulus  $E$  and hardness  $H$  of the material.



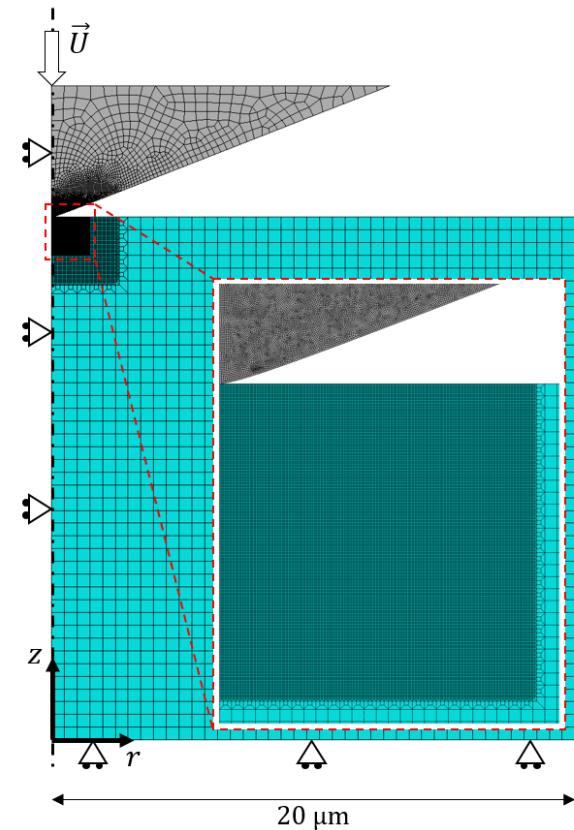
# Nanoindentation: Methodology

For REBCO & MgO:

- 5-10 indents optically targeted.
- Valid penetration depth  $< 150$  nm.

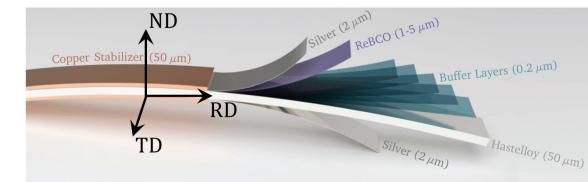
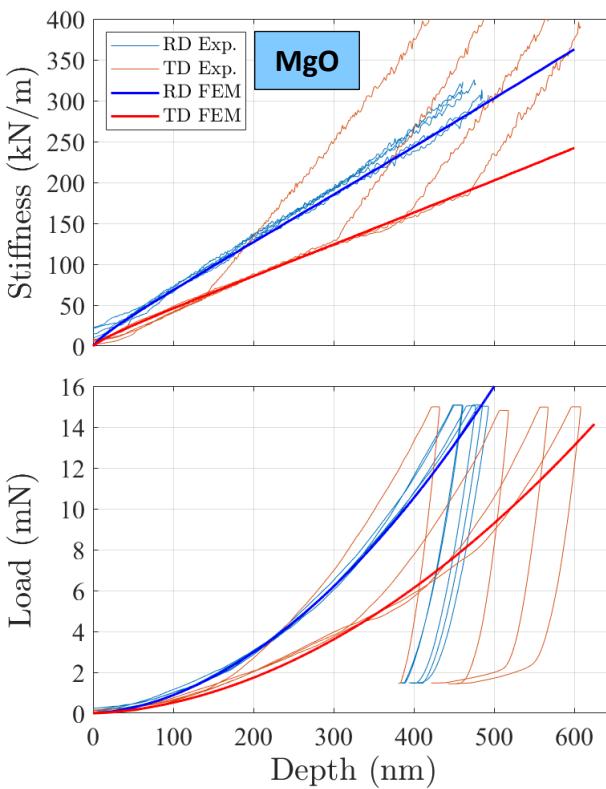
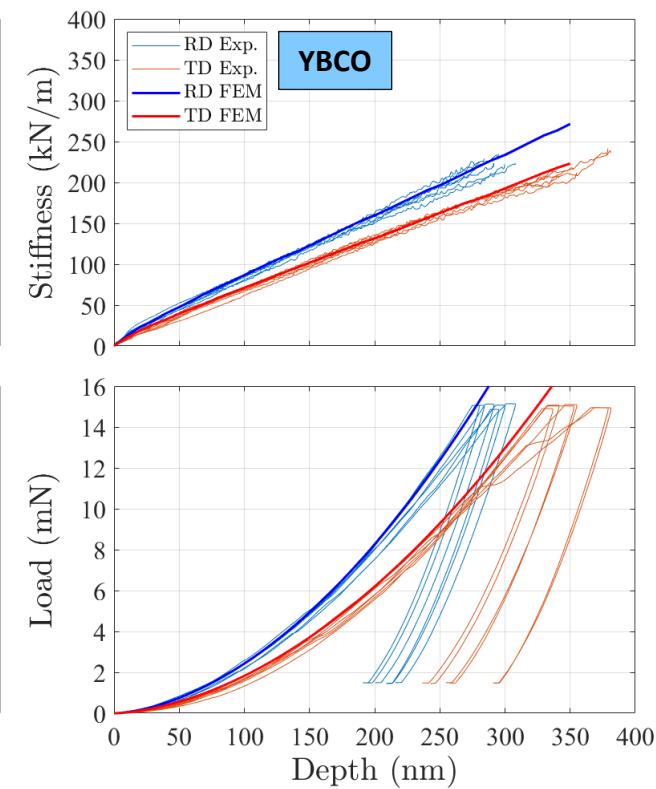
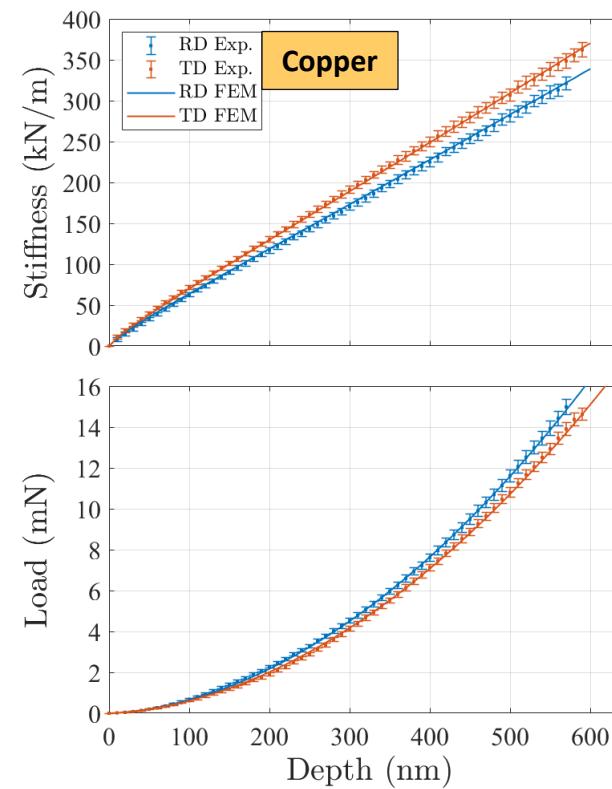
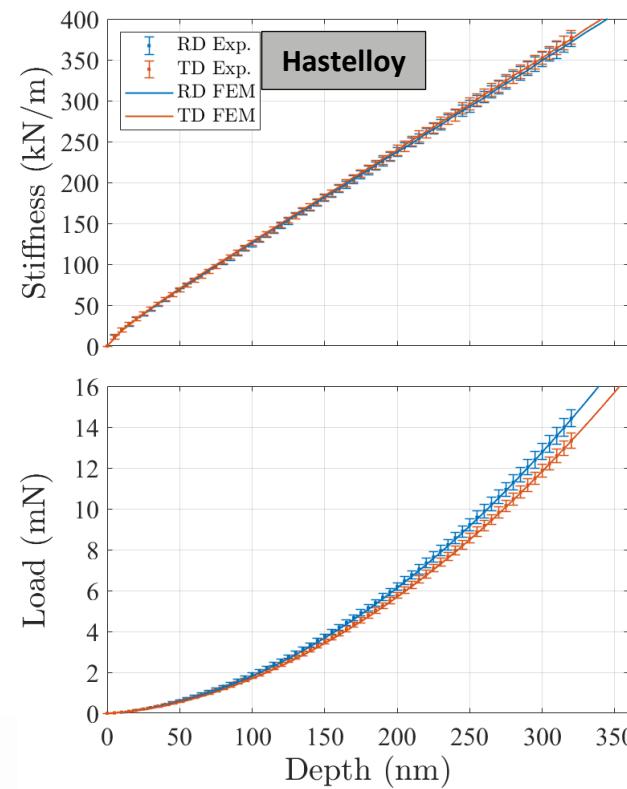


+ Coupled Mechanical  
FE Model

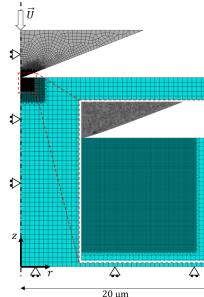


# Nanoindentation: Results on THEVA® at Room Temperature

	Hastelloy	Copper	YBCO	MgO
	$E$ (GPa)	$E$ (GPa)	$E$ (GPa)	$E$ (GPa)
RD	197	84	155	95
TD	195	90	120	60

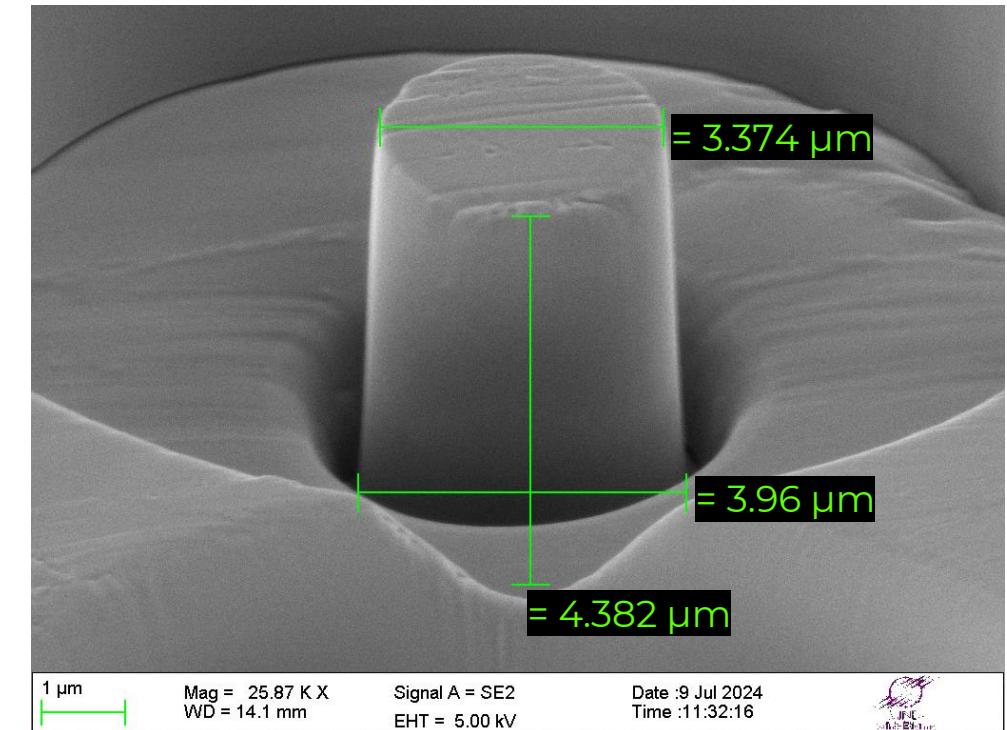
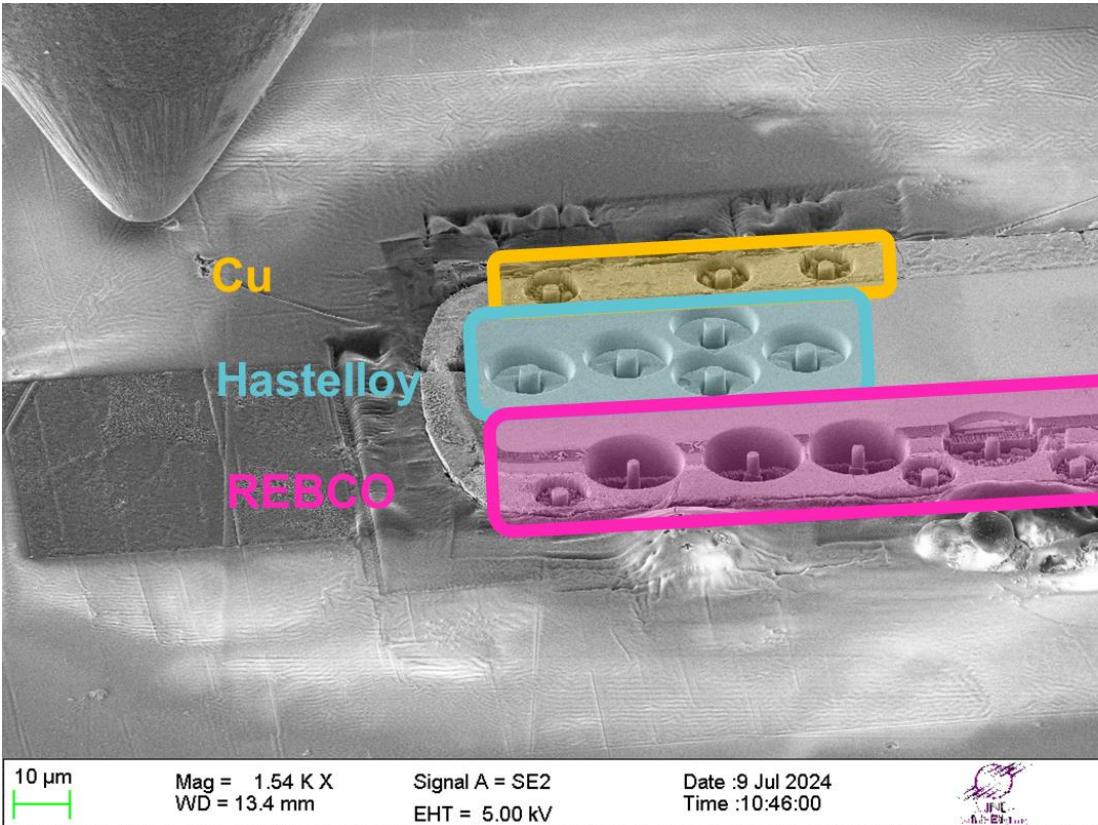


J. Van Nugteren, 2016



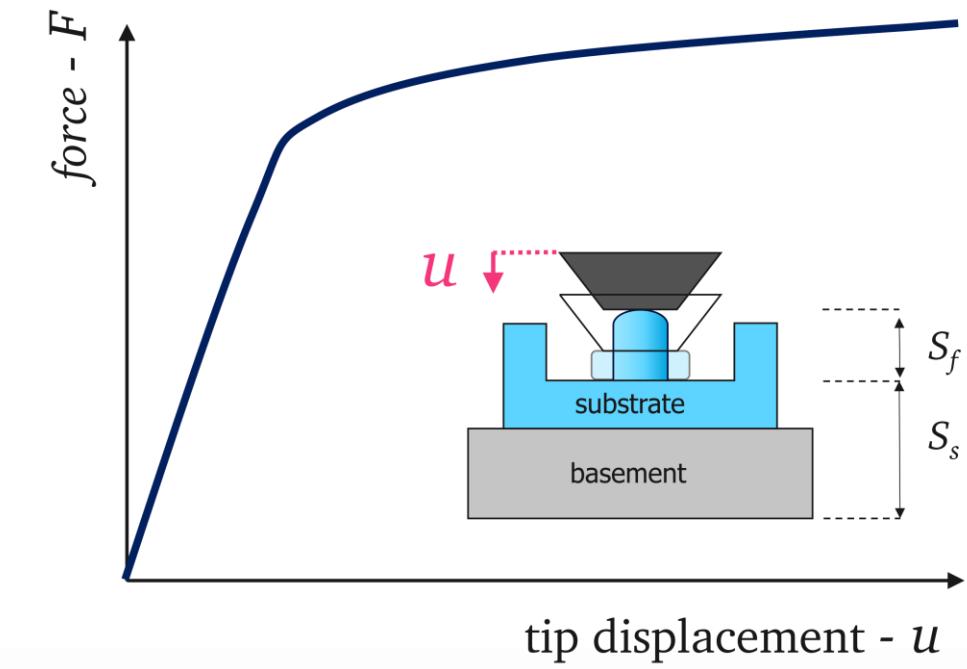
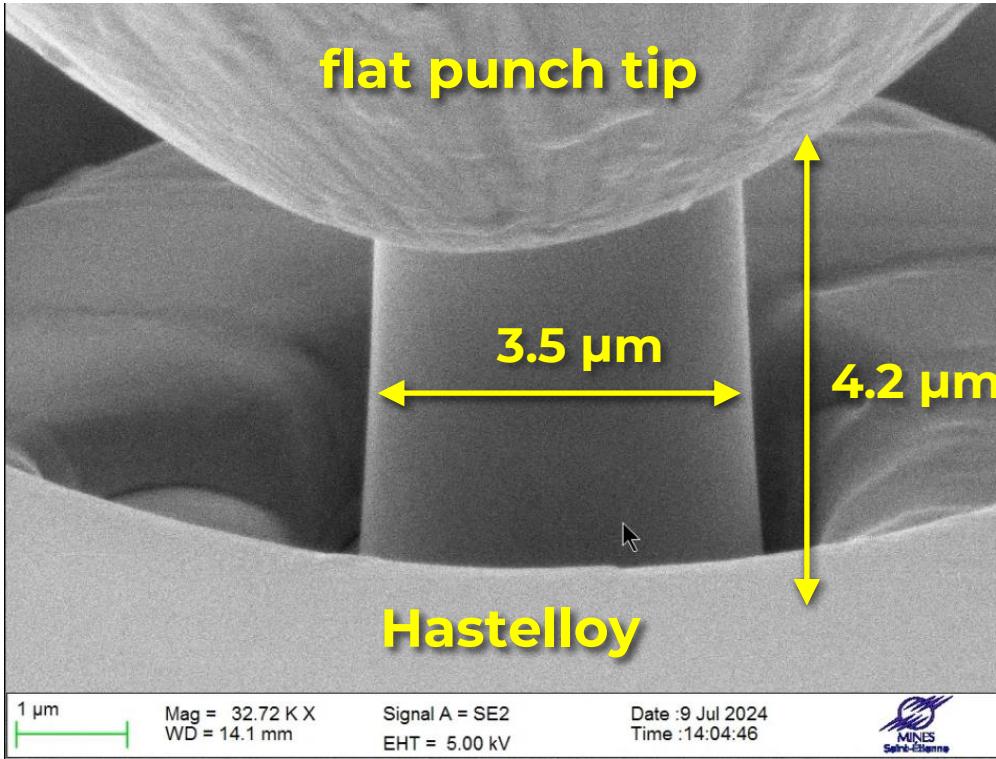
# Micropillars: Drilling

- FIB milling of micropillars

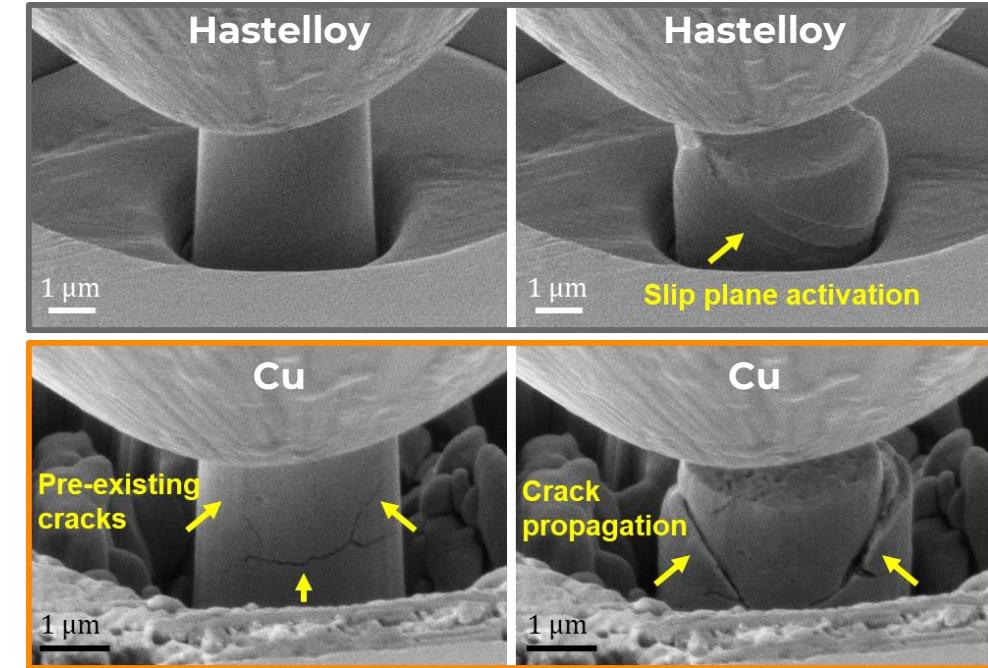
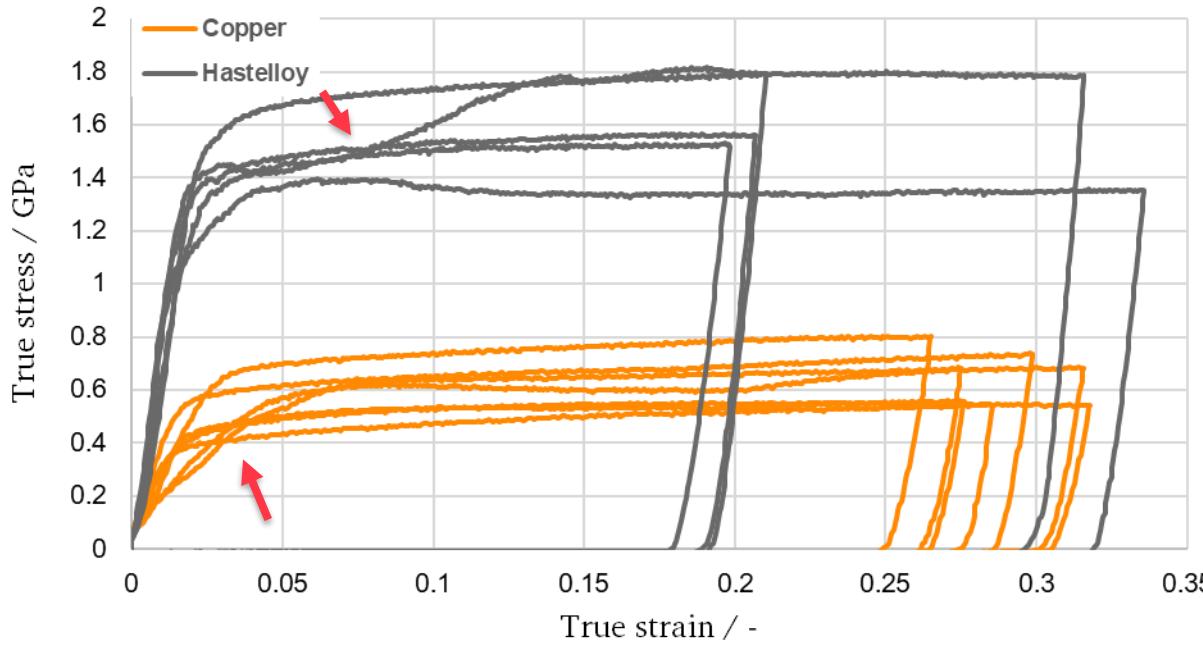


# Micropillar compression: Introduction

- Applying a displacement  $u$  to a flat punch tip measuring the load response  $F$ .



# Micropillar compression: Hastelloy & Copper



Hastelloy		Copper	
$\sigma^y / \text{GPa}$	$* \varepsilon^y / \%$	$\sigma^y / \text{GPa}$	$* \varepsilon^y / \%$
1.2 – 1.6	0.61 – 0.82	0.4 – 0.6	0.42 – 0.66

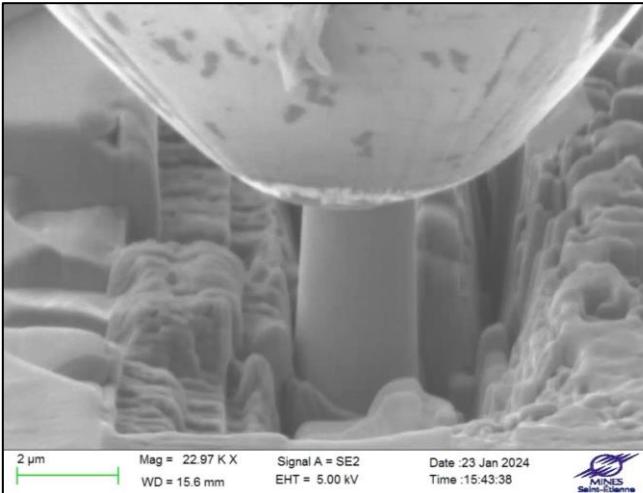
\* using elastic moduli from nanoindentation measurements

Scattering between curves:

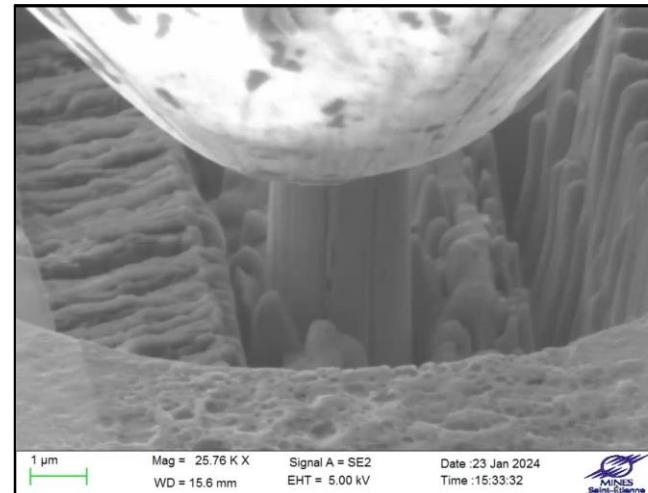
- Hastelloy: single/multiple slip plane activation
- Copper: pre-existing cracks

# Micropillar compression: the anisotropy of RE(Y)-BCO

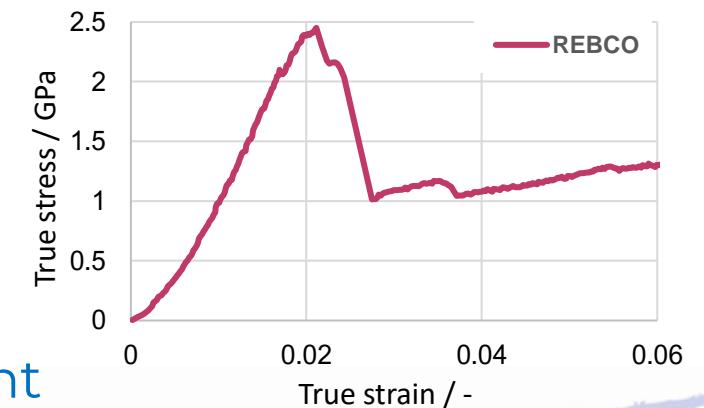
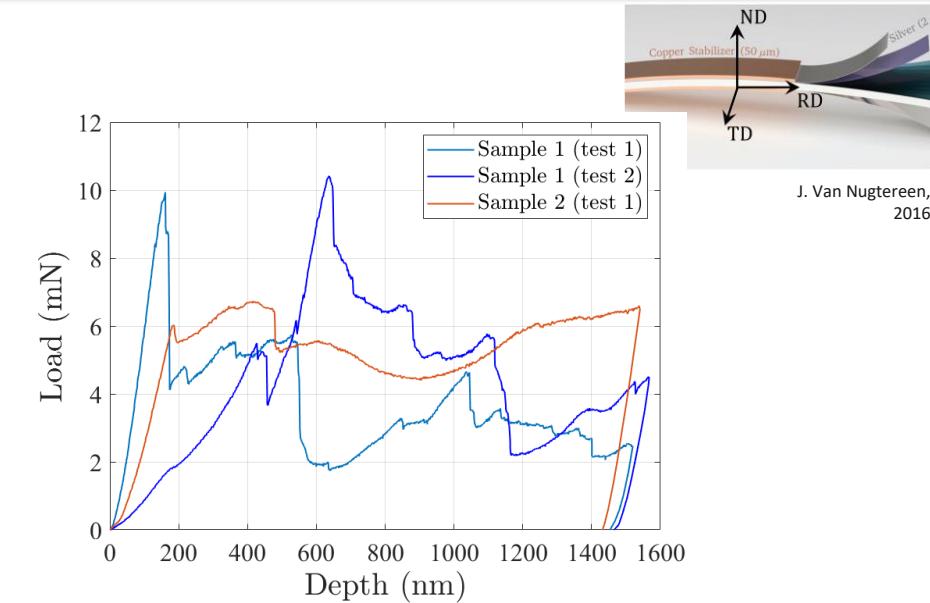
Sample 1 – TD



Sample 2 – RD

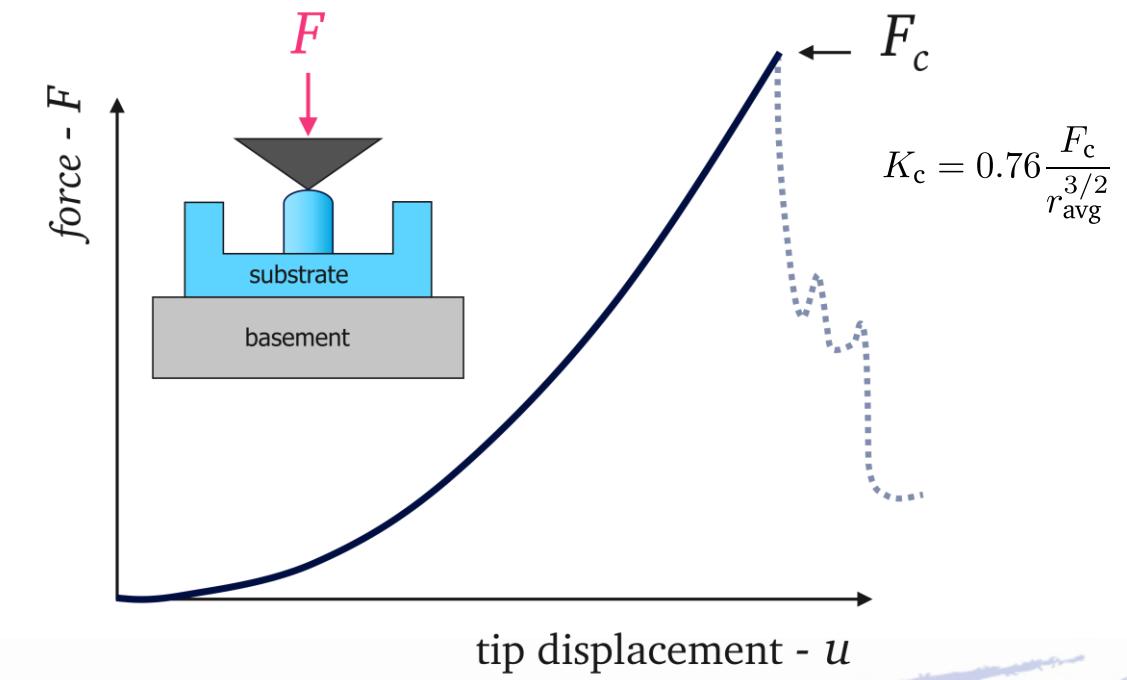
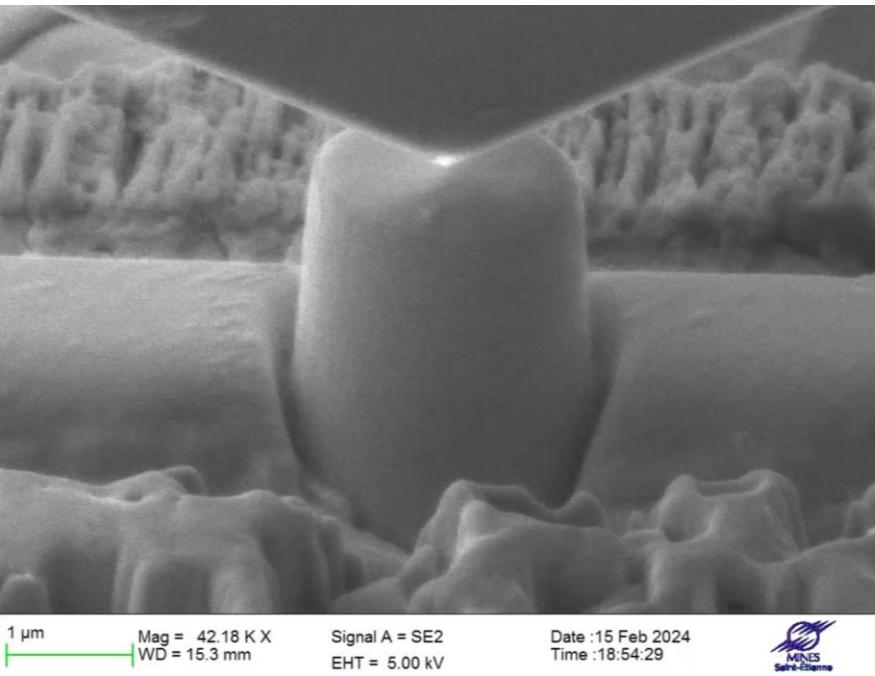


- Sample 1 exhibits brittle failure, as it occurs before any plastic deformation.
- Buckling / plastic failure depending on orientation.
- At the moment it is a non-conclusive measurements.
- Further investigation will be done on tapes of different manufacturers.

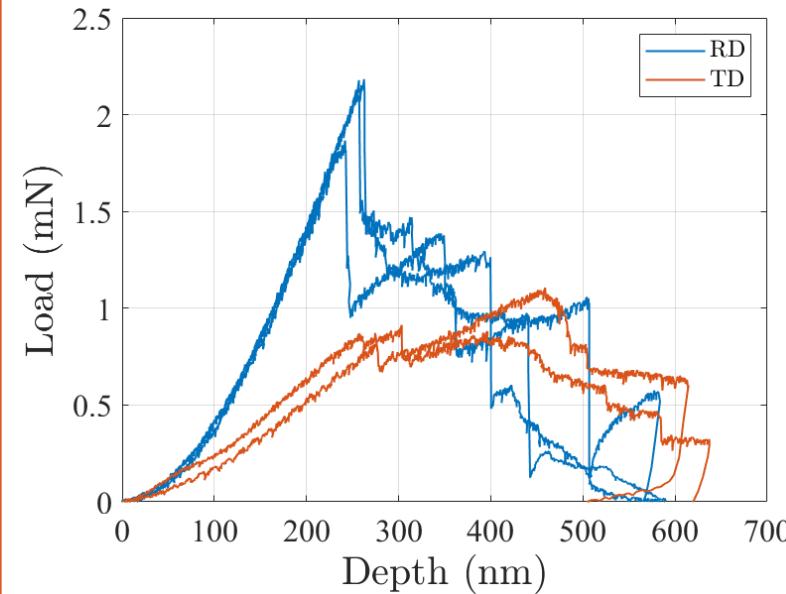
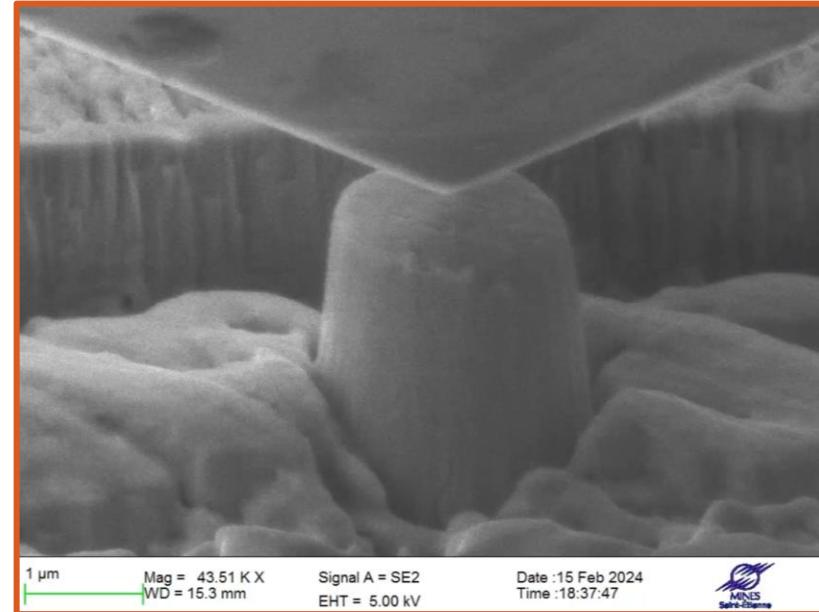
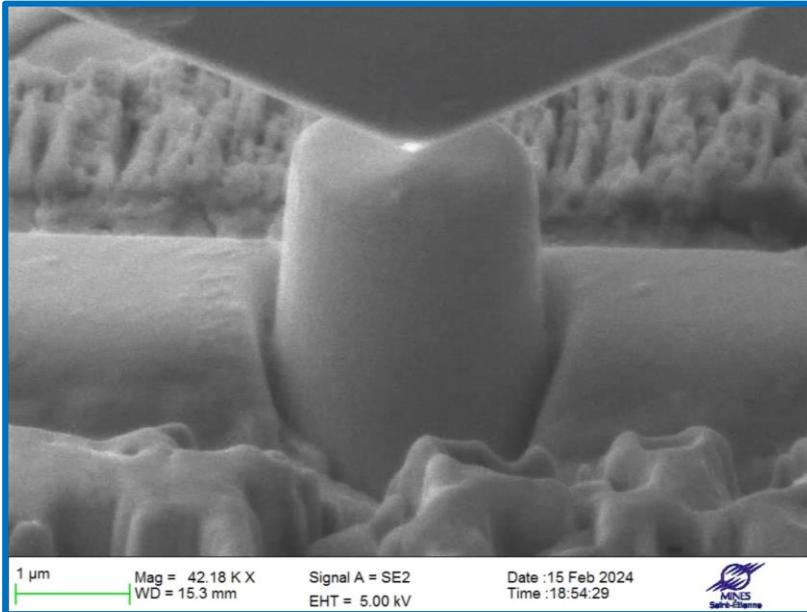


# Micropillar splitting: Introduction

- Driving a sharp tip into a pillar until a fracture occurs. From the critical load  $F_c$ , we determine the fracture toughness  $K_c$ .



# Micropillar splitting: RE(Y)-BCO



- Evident anisotropic behavior.
- Microstructural analyses needed for deeper understanding.
- Values of  $K_c$  are low with respect to traditional metals [ref.1]  $K_c \sim 20 - 110 \text{ MPa}\cdot\sqrt{\text{m}}$ , and ceramics,  $K_c \sim 5 - 10 \text{ MPa}\cdot\sqrt{\text{m}}$ .
- However, they agree with those found in literature [ref.2]

REBCO			
	$E$ (GPa)	$\sigma_y$ (GPa)	$K_c$ (MPa $\sqrt{\text{m}}$ )
RD	155	4.00	$1.34 \pm 0.12$
TD	120	2.80	$0.56 \pm 0.02$

[ref.1]: MatWeb, online, accessible at <https://www.matweb.com/index.aspx>

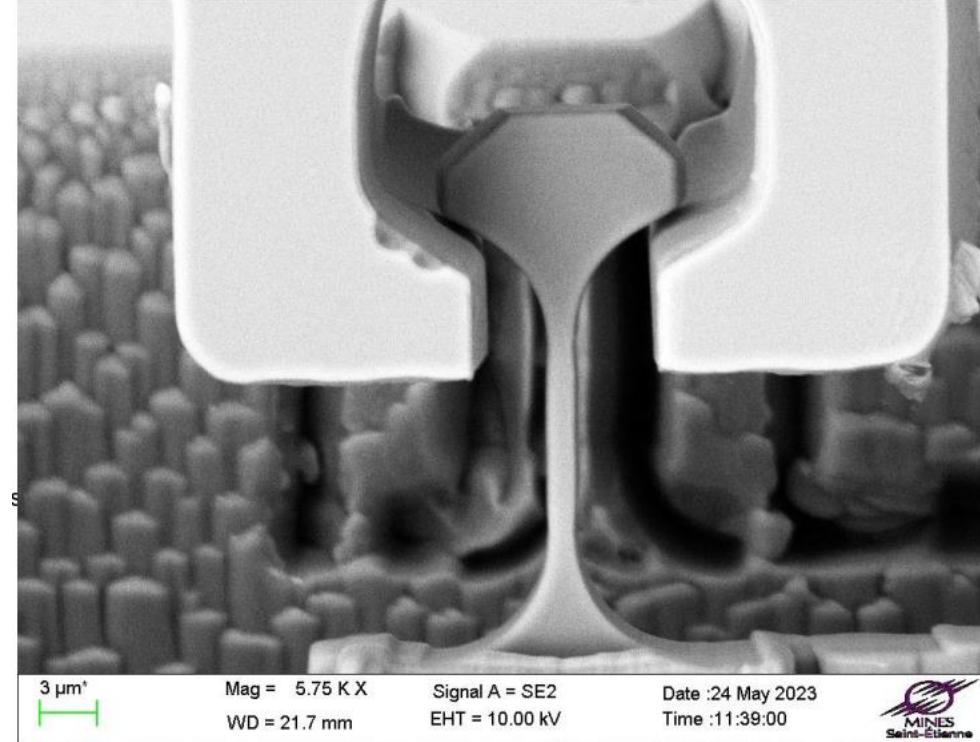
[ref.2]: S. Muto et al., IEEE TAS 30, 4, 2020

# Conclusions

- Nanoindentation measured reliably the **elastic properties** (of most) of the REBCO tape layer materials.
- Micropillar compression has highlighted the high **yield strength** of Hastelloy and Copper.
- Micropillar compression has shown the low **fracture toughness** of YBCO.

REBCO			
	$E$ (GPa)	$\sigma_y$ (GPa)	$K_c$ (MPa $\sqrt{m}$ )
RD	155	4.00	$1.34 \pm 0.12$
TD	120	2.80	$0.56 \pm 0.02$

## Next steps



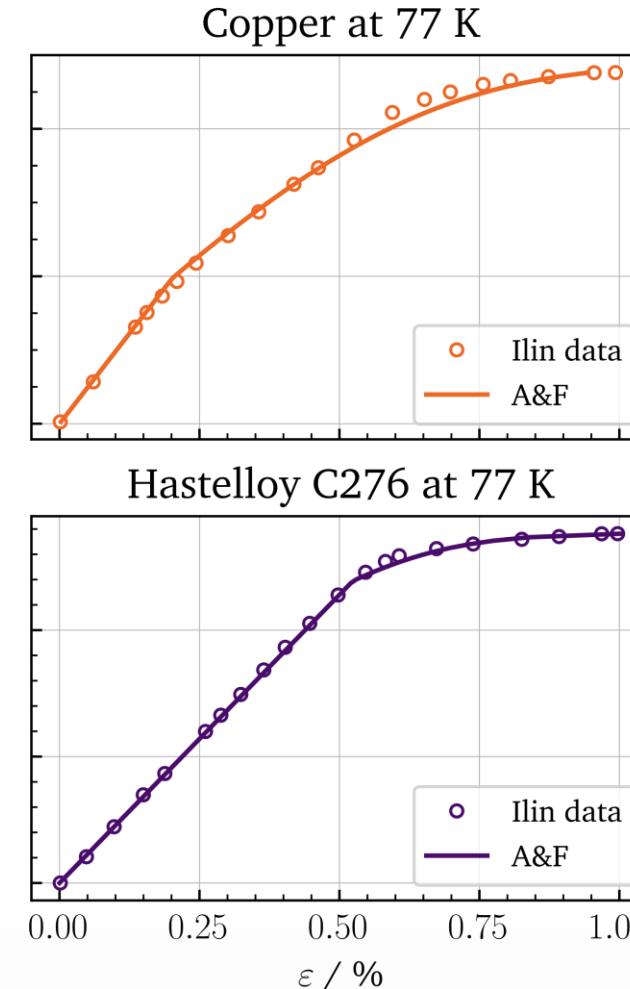
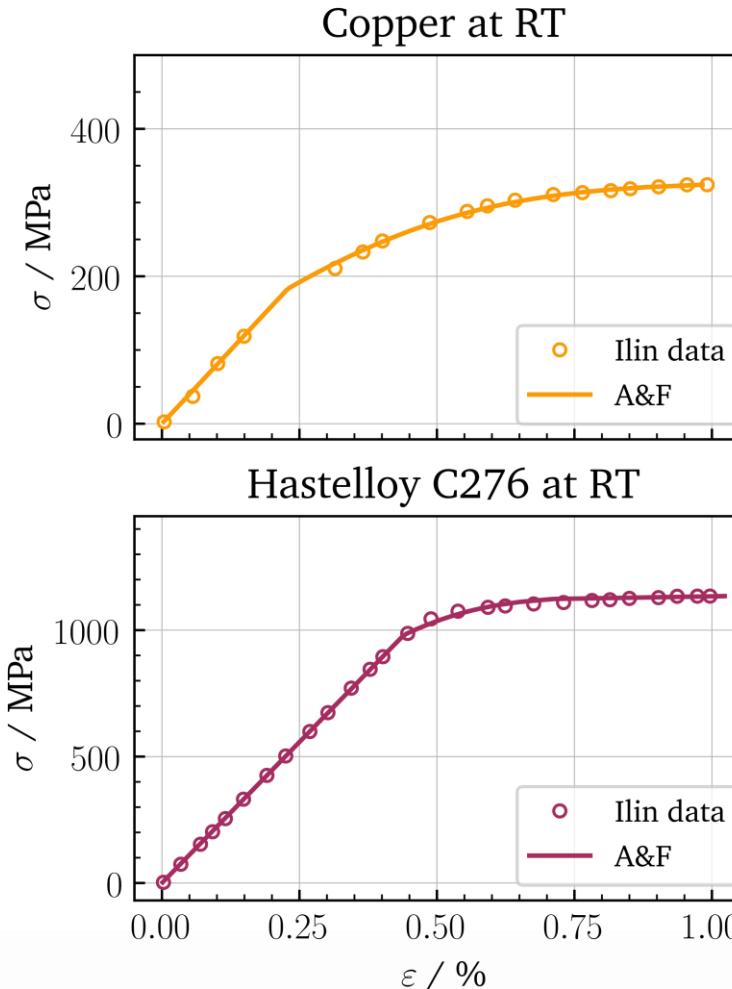
Credit S Kalácska - Mines Saint-Etienne

- We are thinking of trying to characterize the mechanical delamination strength (MDS) at the microscale.



# Thank you !

# Discussion: Properties from Ilin



$$f(\bar{\sigma}, R) = |\sigma| - \sigma^y - R$$

$$R = \frac{H}{\gamma} [1 - \exp(-\gamma p)]$$

$$p = \sqrt{\frac{2}{3}\varepsilon^p : \varepsilon^p}$$

## Copper

	$E_{Cu} / \text{GPa}$	$\sigma^y_{Cu} / \text{MPa}$	$H_{Cu} / \text{GPa}$	$\gamma_{Cu}$
RT		80	183	91
77 K		98	197	648

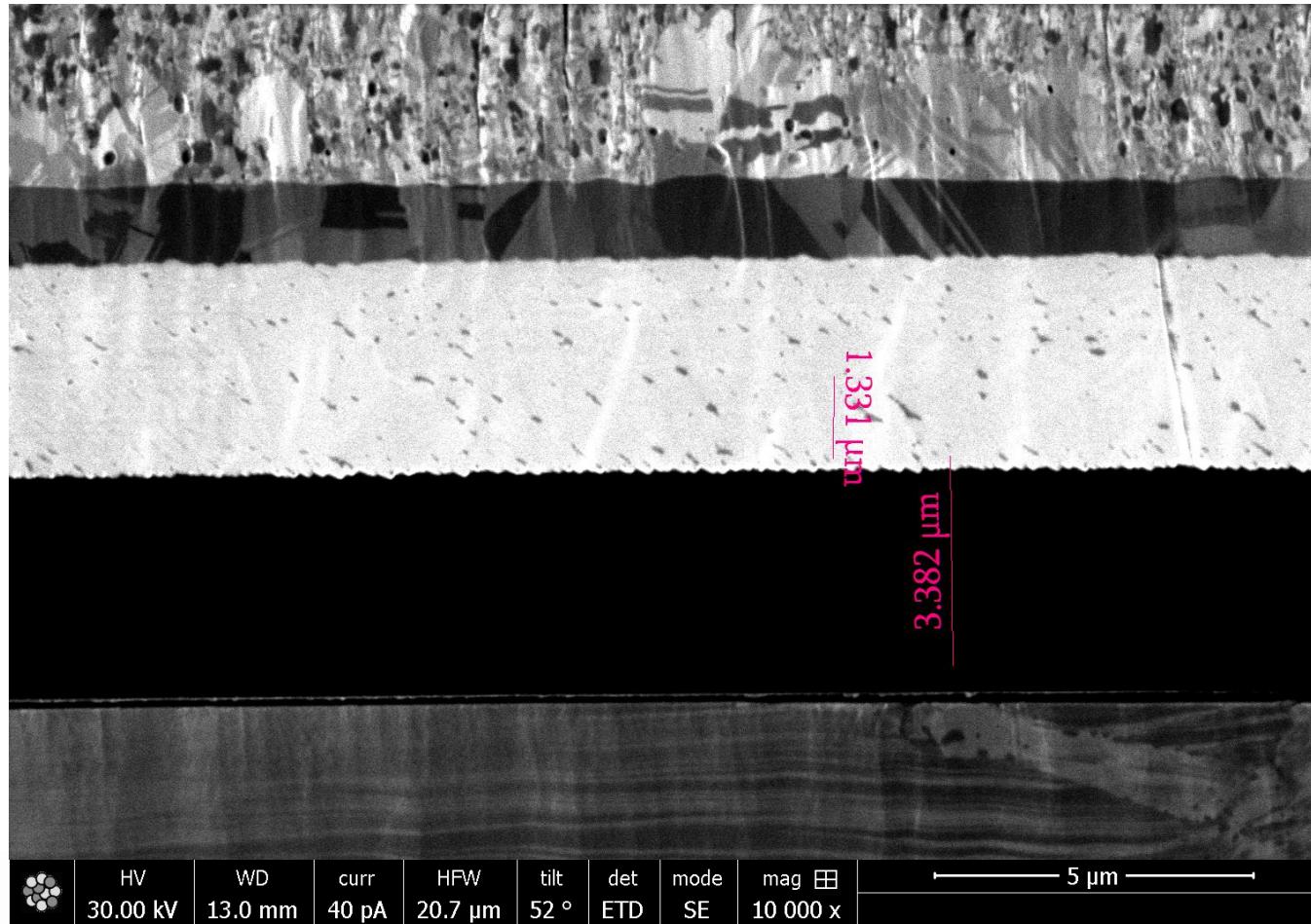
## Hastelloy C276

	$E_{C276} / \text{GPa}$	$\sigma^y_{C276} / \text{MPa}$	$H_{C276} / \text{GPa}$	$\gamma_{C276}$
RT		223	981	191
77 K		228	1194	190

tb,chaboche,mat\_cu,1  
tbdata,1,  $\sigma^y$ , H,  $\gamma$

# Grain sizes

- X-ray Photoelectric Spectroscopy images (XPS) showing the microstructures



# Plastic deformation of a polycrystal

The first slip occurs in crystals with crystallographic slip planes oriented at  $\alpha = \pi/4$  to the direction of external stress.

Fig. 1.17. Deformation of a polycrystal.

