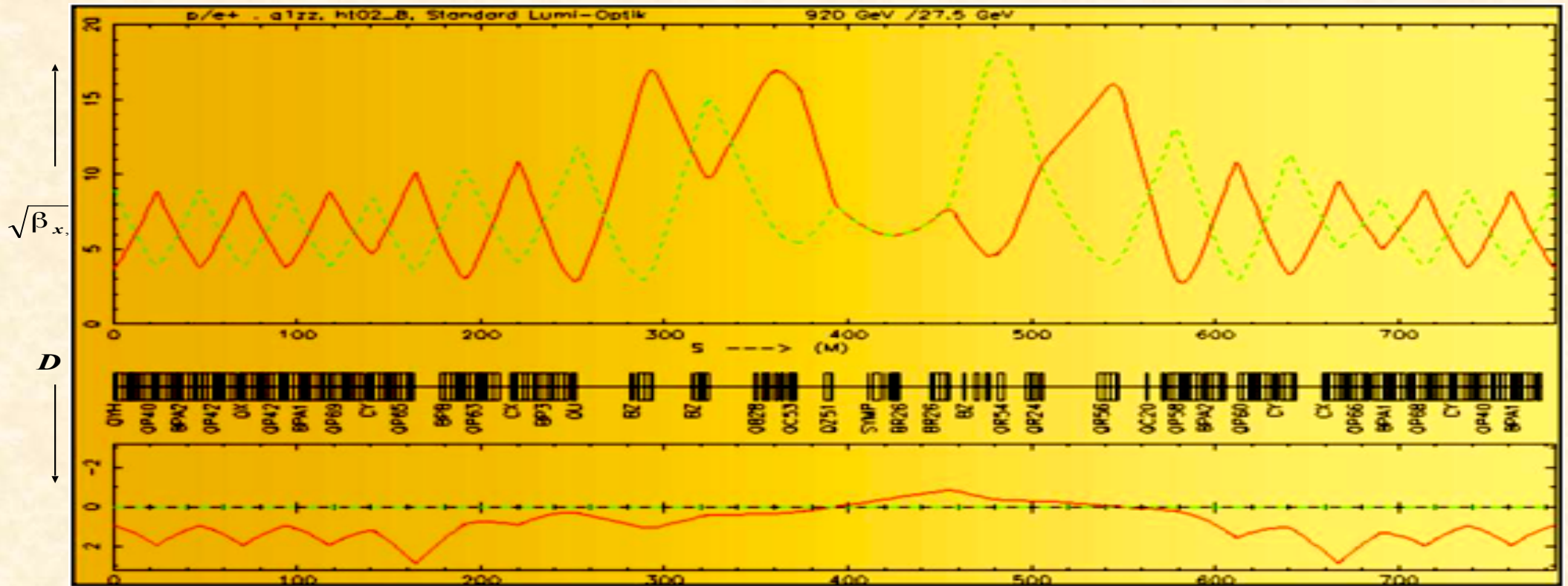


# Transverse Beam Dynamics III

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CERN

## The „not so ideal“ World Lattice Design in Particle Accelerators



**1952: Courant, Livingston, Snyder:**

***Theory of strong focusing in particle beams***

# Recapitulation: ...the story with the matrices !!!

## Equation of Motion:

$$\mathbf{x}'' + \mathbf{K} \mathbf{x} = 0 \quad K = \frac{1}{\rho^2} - k$$

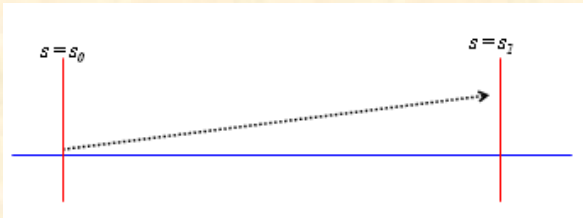
$$K = k$$

... hor. plane:

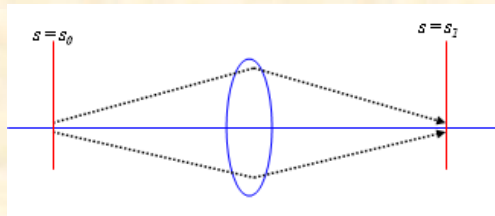
... vert. Plane:

## Solution of Trajectory Equations

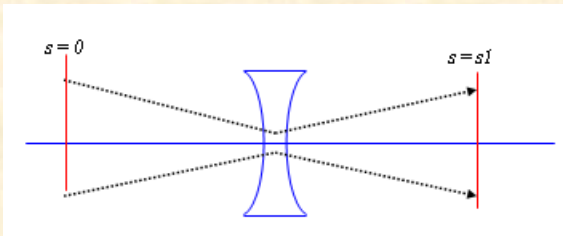
$$\begin{pmatrix} \mathbf{x} \\ \mathbf{x}' \end{pmatrix}_{s_1} = \mathbf{M} * \begin{pmatrix} \mathbf{x} \\ \mathbf{x}' \end{pmatrix}_{s_0}$$



$$\mathbf{M}_{drift} = \begin{pmatrix} 1 & l \\ 0 & 1 \end{pmatrix}$$



$$\mathbf{M}_{foc} = \begin{pmatrix} \cos(\sqrt{|K|}l) & \frac{1}{\sqrt{|K|}} \sin(\sqrt{|K|}l) \\ -\sqrt{|K|} \sin(\sqrt{|K|}l) & \cos(\sqrt{|K|}l) \end{pmatrix}$$



$$\mathbf{M}_{defoc} = \begin{pmatrix} \cosh(\sqrt{|K|}l) & \frac{1}{\sqrt{|K|}} \sinh(\sqrt{|K|}l) \\ \sqrt{|K|} \sinh(\sqrt{|K|}l) & \cosh(\sqrt{|K|}l) \end{pmatrix}$$

$$\mathbf{M}_{total} = \mathbf{M}_{QF} * \mathbf{M}_D * \mathbf{M}_B * \mathbf{M}_D * \mathbf{M}_{QD} * \mathbf{M}_D * \dots$$

**Recapitulation:** ...and for the complete particle ensemble  
the betas and epsilons !!!

general solution of Hill equation

$$\left\{ \begin{array}{l} (1) \quad x(s) = \sqrt{\varepsilon} * \sqrt{\beta(s)} * \cos(\psi(s) + \phi) \\ (2) \quad x'(s) = -\frac{\sqrt{\varepsilon}}{\sqrt{\beta(s)}} * \{ \alpha(s) * \cos(\psi(s) + \phi) + \sin(\psi(s) + \phi) \} \end{array} \right.$$

from (1) we get

$$\cos(\psi(s) + \phi) = \frac{x(s)}{\sqrt{\varepsilon} * \sqrt{\beta(s)}}$$

Insert into (2) and solve for  $\varepsilon$

$$\alpha(s) = \frac{-1}{2} \beta'(s)$$

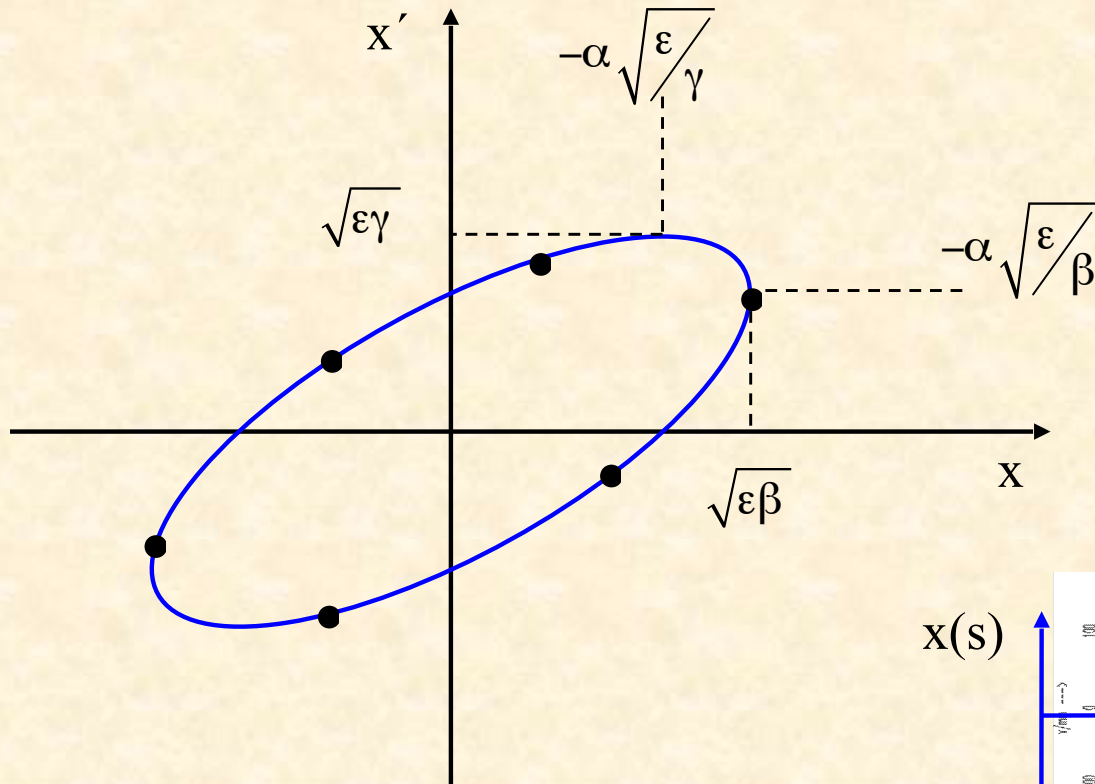
$$\gamma(s) = \frac{1 + \alpha(s)^2}{\beta(s)}$$

$$\varepsilon = \gamma(s) * x^2(s) + 2\alpha(s)x(s)x'(s) + \beta(s)x'(s)^2$$

- \*  $\varepsilon$  is a **constant** of the motion ... it is independent of „s“
- \* parametric representation of an **ellipse** in the  $x x'$  space
- \* shape and orientation of ellipse are given by  $\alpha, \beta, \gamma$

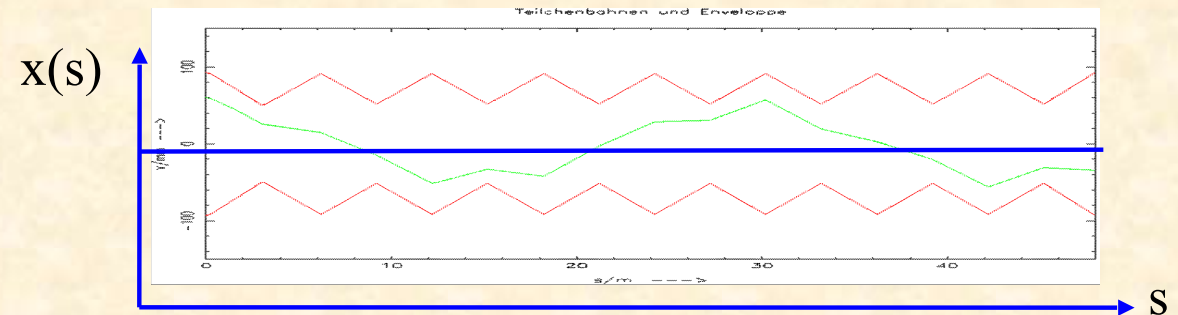
# Beam Emittance and Phase Space Ellipse

$$\varepsilon = \gamma(s) x^2(s) + 2\alpha(s)x(s)x'(s) + \beta(s) x'^2(s)$$



**Liouville: in reasonable storage rings area in phase space is constant.**

$$A = \pi * \varepsilon = \text{const}$$

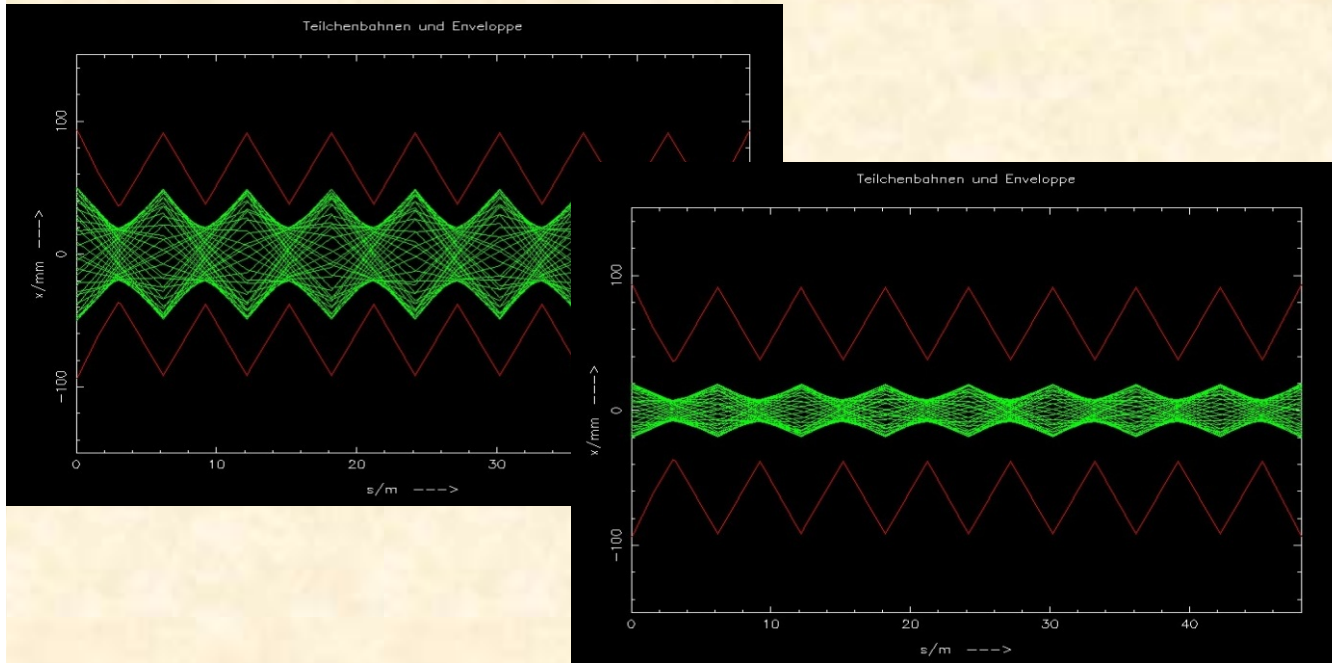


$\varepsilon$  beam emittance = **woozilycity** of the particle ensemble, **intrinsic beam parameter**, cannot be changed by the foc. properties.

**Scientifiquely speaking: area covered in transverse  $x, x'$  phase space ... and it is constant !!!**



# Emittance of the Particle Ensemble:



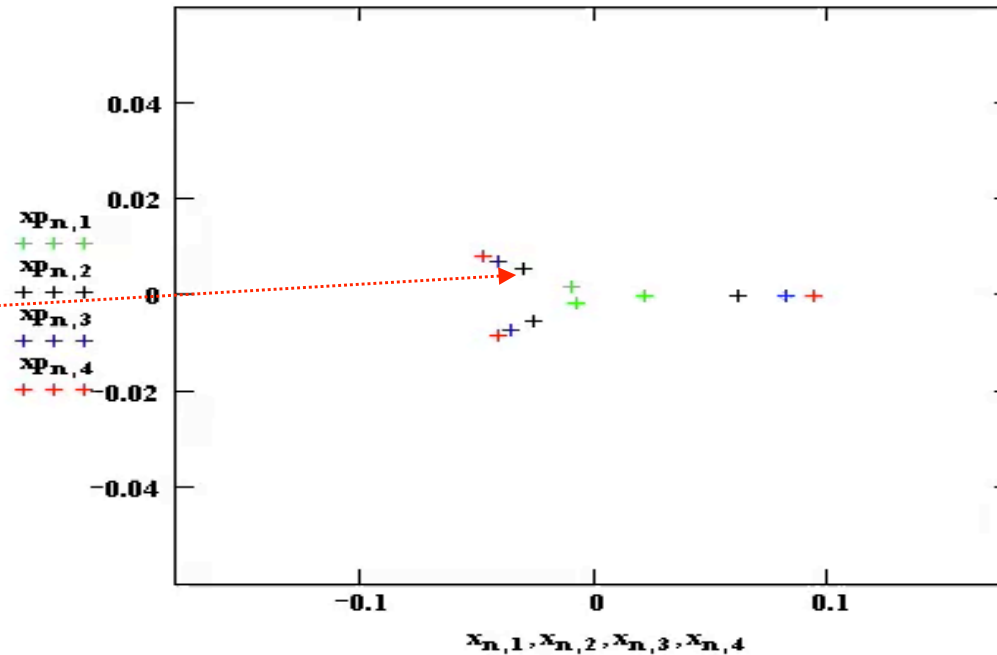
## Example: LHC

*beam parameters in the arc*

$$\beta(x) \approx 180 \text{ m}$$

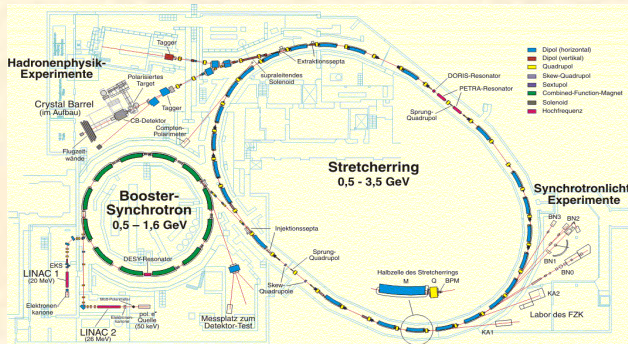
$$\varepsilon \approx 5 \cdot 10^{-10} \text{ rad} \cdot \text{m} \quad (\Leftrightarrow 1\sigma)$$

$$\sigma = \sqrt{\varepsilon\beta} \approx 0.3 \text{ mm}$$



# Periodic Lattices

*transfer matrix for particle trajectories as a function of the lattice parameters*



$$\begin{pmatrix} x \\ x' \end{pmatrix}_{s1} = M * \begin{pmatrix} x \\ x' \end{pmatrix}_{s0}$$

$$M = \begin{pmatrix} \sqrt{\frac{\beta_s}{\beta_0}} (\cos\psi_s + \alpha_0 \sin\psi_s) & \sqrt{\beta_s \beta_0} \sin\psi_s \\ \frac{(\alpha_0 - \alpha_s) \cos\psi_s - (1 + \alpha_0 \alpha_s) \sin\psi_s}{\sqrt{\beta_s \beta_0}} & \sqrt{\frac{\beta_0}{\beta_s}} (\cos\psi_s - \alpha_s \sin\psi_s) \end{pmatrix}$$

*„This rather formidable looking matrix simplifies considerably if we consider one complete turn ...“*

## One Turn Matrix

$$M(s) = \begin{pmatrix} \cos\psi_{turn} + \alpha_s \sin\psi_{turn} & \beta_s \sin\psi_{turn} \\ -\gamma_s \sin\psi_{turn} & \cos\psi_{turn} - \alpha_s \sin\psi_{turn} \end{pmatrix}$$

$$\psi_{turn} = \int_s^{s+L} \frac{ds}{\beta(s)} \quad \psi_{turn} = \text{phase advance per period}$$

*Stability in a periodic structure requires  $\Leftrightarrow |\text{Trace}(M)| < 2$*

# Transformation of $\alpha$ , $\beta$ , $\gamma$

consider two positions in the storage ring:  $s_0$ ,  $s$

$$\begin{pmatrix} x \\ x' \end{pmatrix}_s = M \cdot \begin{pmatrix} x \\ x' \end{pmatrix}_{s_0}$$

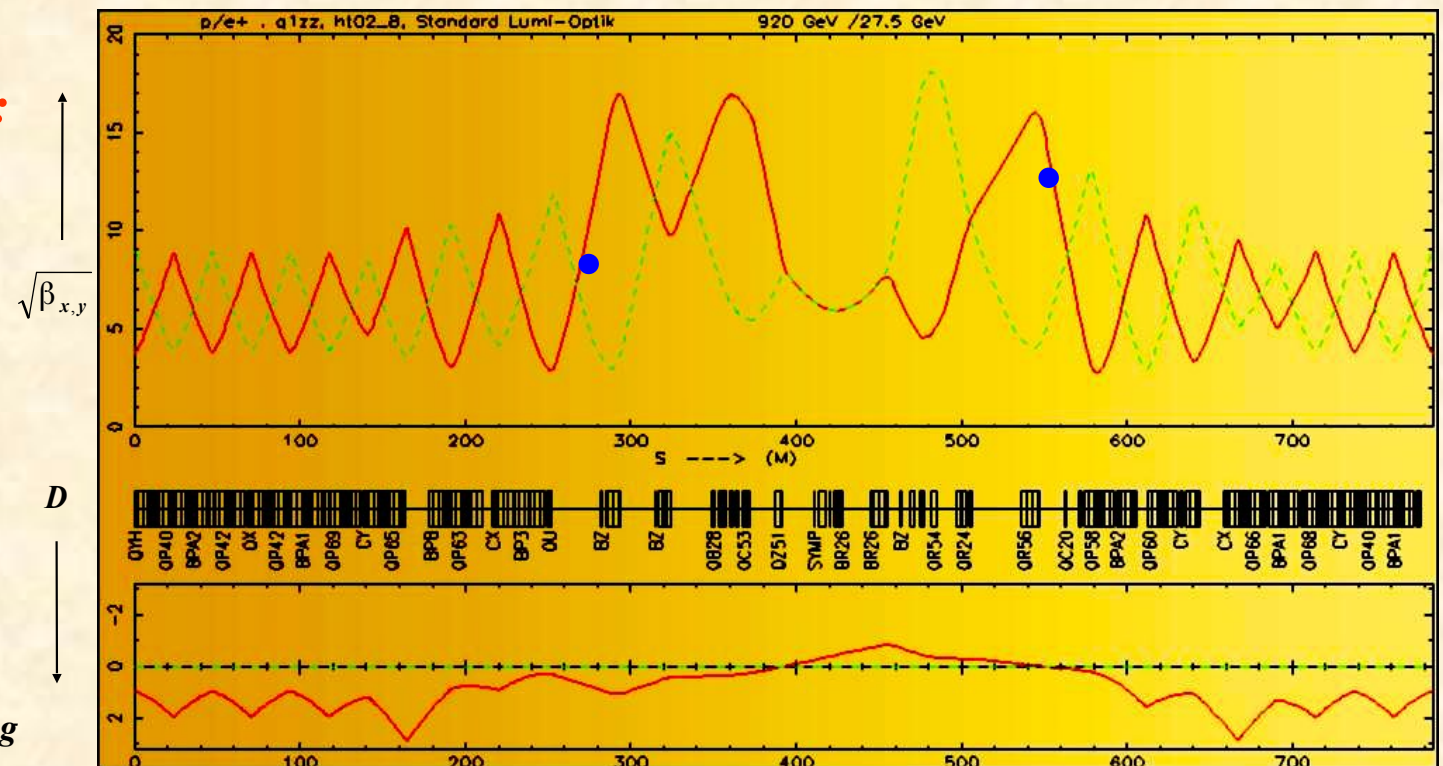
where ...  $M = M_{QF} \cdot M_{QD} \cdot M_B \cdot M_{Drift} \cdot M_{QF} \cdot \dots$

$$M = \begin{pmatrix} C & S \\ C' & S' \end{pmatrix} \longleftrightarrow M_{foc} = \begin{pmatrix} \cos(\sqrt{|K|}l) & \frac{1}{\sqrt{|K|}} \sin(\sqrt{|K|}l) \\ -\sqrt{|K|} \sin(\sqrt{|K|}l) & \cos(\sqrt{|K|}l) \end{pmatrix}$$

since  $\varepsilon = \text{const}$  (Liouville):

$$\varepsilon = \beta x'^2 + 2\alpha x x' + \gamma x^2$$

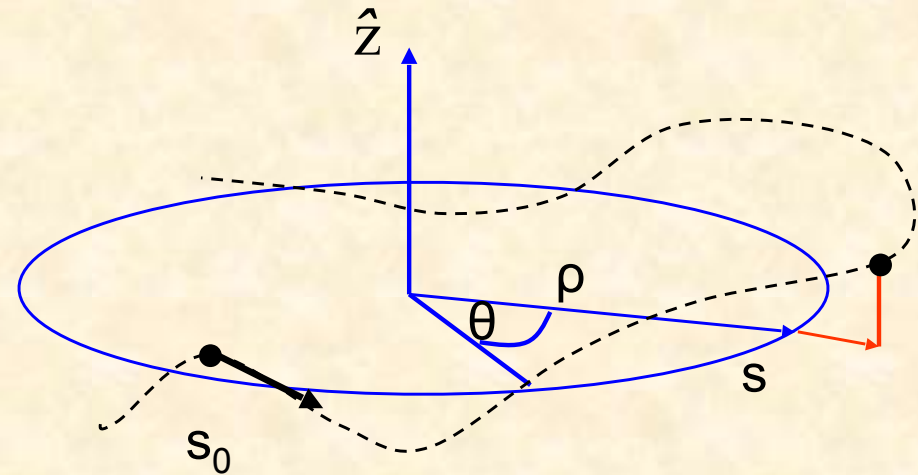
$$\varepsilon = \beta_0 x_0'^2 + 2\alpha_0 x_0 x_0' + \gamma_0 x_0^2$$



Beta function in a storage ring

express  $x_0, x'_0$  as a function of  $x, x'$ .

$$\begin{pmatrix} x \\ x' \end{pmatrix}_s = M \cdot \begin{pmatrix} x \\ x' \end{pmatrix}_{s_0}$$



... remember  $W = CS' - SC' = 1$

$$\begin{pmatrix} x \\ x' \end{pmatrix}_0 = M^{-1} \cdot \begin{pmatrix} x \\ x' \end{pmatrix}_s$$

$$M^{-1} = \frac{1}{\det(M)} \begin{pmatrix} m_{22} & -m_{12} \\ -m_{21} & m_{11} \end{pmatrix} = \begin{pmatrix} S' & -S \\ -C' & C \end{pmatrix}$$

$\det(M) = 1$



$$\begin{aligned} x_0 &= S'x - Sx' \\ x'_0 &= -C'x + Cx' \end{aligned}$$

inserting into  $\varepsilon$

$$\varepsilon = \beta x'^2 + 2\alpha xx' + \gamma x^2$$

$$\varepsilon = \beta_0 (Cx' - C'x)^2 + 2\alpha_0 (S'x - Sx')(Cx' - C'x) + \gamma_0 (S'x - Sx')^2$$

sort via  $x, x'$  and compare the coefficients to get ....



$$\beta(s) = C^2 \beta_0 - 2SC \alpha_0 + S^2 \gamma_0$$

$$\alpha(s) = -CC' \beta_0 + (SC' + S'C) \alpha_0 - SS' \gamma_0$$

$$\gamma(s) = C'^2 \beta_0 - 2S'C' \alpha_0 + S'^2 \gamma_0$$

*in matrix notation:*

$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_s = \begin{pmatrix} C^2 & -2SC & S^2 \\ -CC' & SC' + CS' & -SS' \\ C'^2 & -2S'C' & S'^2 \end{pmatrix} \cdot \begin{pmatrix} \beta_0 \\ \alpha_0 \\ \gamma_0 \end{pmatrix}$$



- 1.) *this expression is important*
- 2.) *given the twiss parameters  $\alpha$ ,  $\beta$ ,  $\gamma$  at any point in the lattice we can transform them and calculate their values at any other point in the ring.*
- 3.) *the transfer matrix is given by the focusing properties of the lattice elements, the elements of  $M$  are just those that we used to calculate single particle trajectories.*
- 4.) *go back to point 1.)*

## Résumé:

*equation of motion:*

$$\mathbf{x}''(s) + \mathbf{K}(s) \mathbf{x}(s) = 0, \quad K = \frac{1}{\rho^2} - k$$

*general solution of Hill's equation:*

$$x(s) = \sqrt{\varepsilon} \sqrt{\beta(s)} \cdot \cos(\psi(s) + \phi)$$

*phase advance & tune:*

$$\psi_{12}(s) = \int_{s_1}^{s_2} \frac{1}{\beta(s)} ds, \quad Q(s) = \frac{1}{2\pi} \oint \frac{1}{\beta(s)} ds$$

*emittance:*

$$\varepsilon = \gamma(s) \mathbf{x}^2(s) + 2\alpha(s) \mathbf{x}(s) \mathbf{x}'(s) + \beta(s) \mathbf{x}'^2(s)$$

*transfer matrix from  $s_1 \longrightarrow s_2$ :*

$$M = \begin{pmatrix} \sqrt{\frac{\beta_s}{\beta_0}} (\cos \psi_s + \alpha_0 \sin \psi_s) & \sqrt{\beta_s \beta_0} \sin \psi_s \\ \frac{(\alpha_0 - \alpha_s) \cos \psi_s - (1 + \alpha_0 \alpha_s) \sin \psi_s}{\sqrt{\beta_s \beta_0}} & \sqrt{\frac{\beta_0}{\beta_s}} (\cos \psi_s - \alpha_s \sin \psi_s) \end{pmatrix}$$

*matrix for 1 turn:*

$$M(s) = \begin{pmatrix} \cos \psi_{turn} + \alpha_s \sin \psi_{turn} & \beta_s \sin \psi_{turn} \\ -\gamma_s \sin \psi_{turn} & \cos \psi_{turn} - \alpha_s \sin \psi_{turn} \end{pmatrix}$$

*stability criterion:*

$$|\text{Trace}(M)| < 2$$

# Transfer Matrix $M$

Transformation of particle coordinates:

$$\begin{pmatrix} x \\ x' \end{pmatrix}_s = M \begin{pmatrix} x \\ x' \end{pmatrix}_0$$

1.) using matrix notation in magnet parameters:

$$M_{total} = M_{QF} * M_D * M_B * M_D * M_{QD} * M_D * \dots$$

$$M_{foc} = \begin{pmatrix} \cos(\sqrt{|K|}l) & \frac{1}{\sqrt{|K|}} \sin(\sqrt{|K|}l) \\ -\sqrt{|K|} \sin(\sqrt{|K|}l) & \cos(\sqrt{|K|}l) \end{pmatrix}$$

2.) using matrix notation in Twiss form:

$$M = \begin{pmatrix} \sqrt{\frac{\beta_s}{\beta_0}} (\cos\psi_s + \alpha_0 \sin\psi_s) & \sqrt{\beta_s \beta_0} \sin\psi_s \\ \frac{(\alpha_0 - \alpha_s) \cos\psi_s - (1 + \alpha_0 \alpha_s) \sin\psi_s}{\sqrt{\beta_s \beta_0}} & \sqrt{\frac{\beta_0}{\beta_s}} (\cos\psi_s - \alpha_s \sin\psi_s) \end{pmatrix}$$

3.) Transformation of Twiss parameters:

$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_s = \begin{pmatrix} C^2 & -2SC & S^2 \\ -CC' & SC' + CS' & -SS' \\ C'^2 & -2S'C' & S'^2 \end{pmatrix} \cdot \begin{pmatrix} \beta_0 \\ \alpha_0 \\ \gamma_0 \end{pmatrix}$$

# III. Lattice Design in Particle Accelerators

„... how to build a storage ring“

High energy accelerators → **circular machines**

somewhere in the lattice we need a number of **dipole magnets**,  
that are bending the design orbit to a **closed ring**

**Geometry of the ring:**

**centrifugal force = Lorentz force**



**Example: heavy ion storage ring TSR**  
**8 dipole magnets of equal bending strength**

$$e * v * B = \frac{mv^2}{\rho}$$
$$\rightarrow e * B = \frac{mv}{\rho} = p / \rho$$

$$\rightarrow B * \rho = p / e$$

$p$  = momentum of the particle,  
 $\rho$  = curvature radius

$B\rho$  = beam rigidity



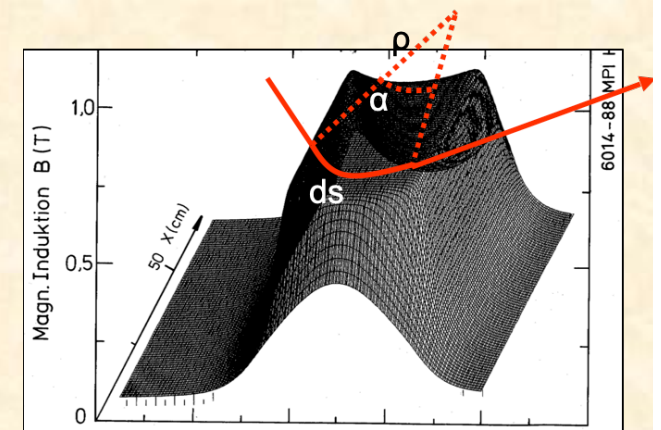
# 19.) Lattice Design:

$$B \rho = p / q$$

*Circular Orbit: dipole magnets to define the geometry and the particle momentum ( ... energy)*

$$\alpha = \frac{ds}{\rho} \approx \frac{dl}{\rho} = \frac{Bdl}{B\rho}$$

*The integrated B-field of the dipoles determines the particle momentum  
The number of dipoles is determined by the momentum of the beam ... or vice versa.  
—> tutorial exercise*



field map of a storage ring dipole magnet



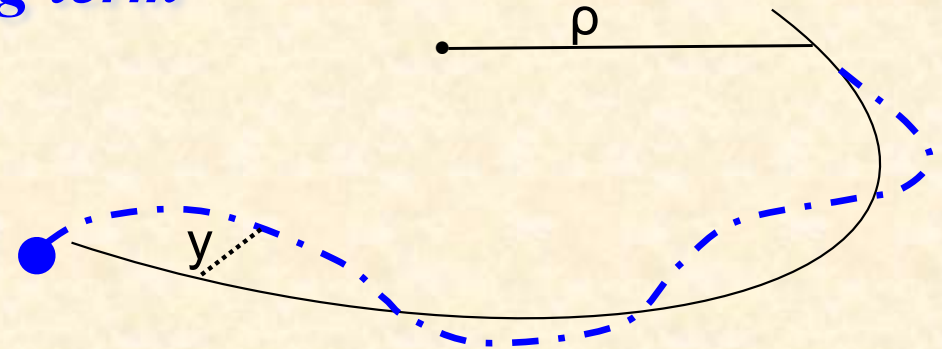
$$\int Bdl = 2\pi \frac{p}{q}$$

## 20.) Focusing forces ... weak focusing term

$$x'' + K * x = 0$$

$$K = \frac{1}{\rho^2} - k \quad \text{hor. plane}$$

$$K = k \quad \text{vert. plane}$$



|                   |                                  |   |
|-------------------|----------------------------------|---|
| dipole magnet     | $\frac{1}{\rho} = \frac{B}{p/q}$ | } |
| quadrupole magnet | $k = \frac{g}{p/q}$              |   |

**Example: LHC Ring:**

**Bending radius:  $\rho = 2.8 \text{ km}$**

**Quadrupole Gradient:  $g = 220 \text{ T/m}$**

$$k = 9.4 * 10^{-3} / \text{m}^2$$

$$1/\rho^2 = 1.3 * 10^{-7} / \text{m}^2$$

**For estimates in large accelerators the weak focusing term  $1/\rho^2$  can in general be neglected**

**Solution for a focusing magnet**

$$x(s) = x_0 * \cos(\sqrt{K} * s) + \frac{x'_0}{\sqrt{K}} * \sin(\sqrt{K} * s)$$

$$x'(s) = -x_0 \sqrt{K} * \sin(\sqrt{K} * s) + x'_0 * \cos(\sqrt{K} * s)$$

*The Twiss parameters  $\alpha$ ,  $\beta$ ,  $\gamma$  can be transformed through the lattice via the matrix elements defined above.*

$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_s = \begin{pmatrix} C^2 & -2SC & S^2 \\ -CC' & SC' + S'C & -SS' \\ C'^2 & -2S'C' & S'^2 \end{pmatrix} * \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_0$$

**Question:** „ What does that mean ????? “

## Most simple example: *drift space*

$$M = \begin{pmatrix} C & S \\ C' & S' \end{pmatrix} = \begin{pmatrix} 1 & l \\ 0 & 1 \end{pmatrix}$$

*particle coordinates*

$$\begin{pmatrix} x \\ x' \end{pmatrix}_l = \begin{pmatrix} 1 & l \\ 0 & 1 \end{pmatrix} * \begin{pmatrix} x \\ x' \end{pmatrix}_0$$

→

$$\begin{aligned} x(l) &= x_0 + l * x_0' \\ x'(l) &= x_0' \end{aligned}$$

*transformation of twiss parameters:*

$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_l = \begin{pmatrix} 1 & -2l & l^2 \\ 0 & 1 & -l \\ 0 & 0 & 1 \end{pmatrix} * \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_0$$

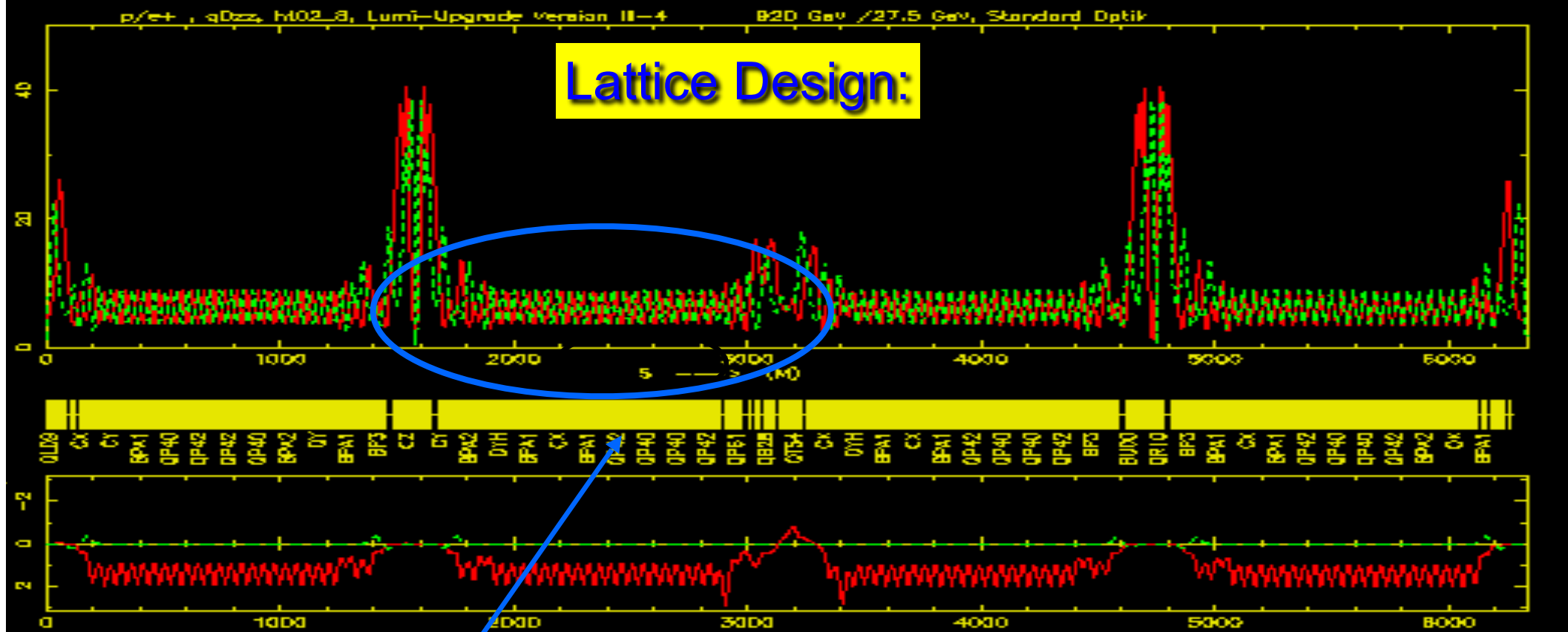
$$\beta(s) = \beta_0 - 2l * \alpha_0 + l^2 * \gamma_0$$

*Stability ...?*

$$\text{trace}(M) = 1 + 1 = 2$$

→ *A periodic solution doesn't exist in a lattice built exclusively out of drift spaces.*





**Arc:** regular (periodic) magnet structure:

bending magnets to define the energy of the ring  
 main focusing & tune control, chromaticity correction,  
 multipoles for higher order corrections

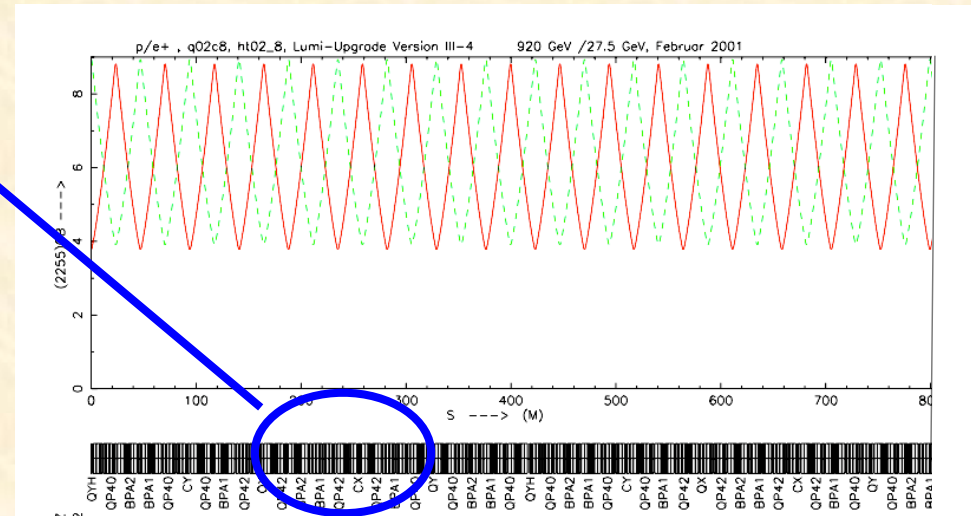
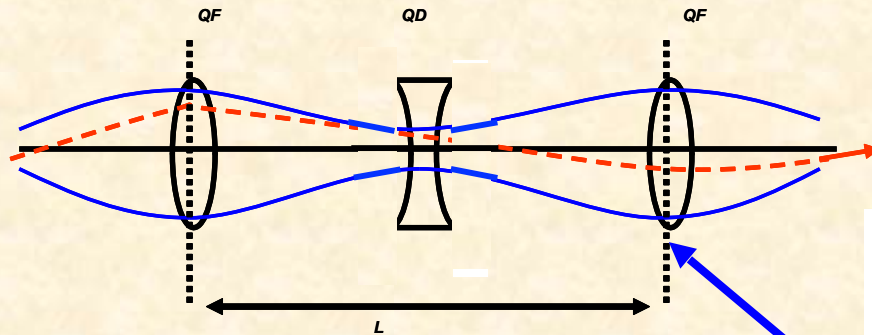
**Straight sections:** drift spaces for injection, dispersion suppressors,  
 low beta insertions, RF cavities, etc....

... and the high energy experiments if they cannot be avoided

# 21.) The FoDo-Lattice

A magnet structure consisting of focusing and defocusing quadrupole lenses in alternating order with *nothing* in between.

(*Nothing* = elements that can be neglected on first sight: drift, bending magnets, RF structures ... *and especially experiments...*)

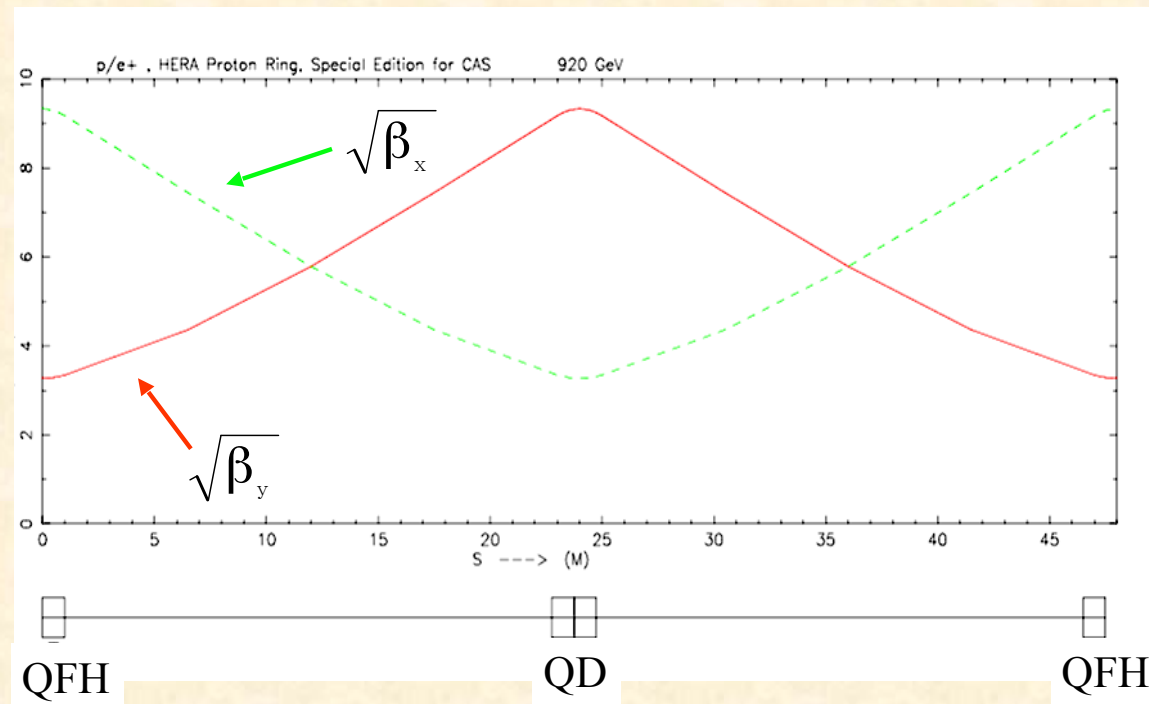


Starting point for the calculation: in the middle of a focusing quadrupole

Phase advance per cell  $\mu = 45^\circ$ ,

—> calculate the optics parameters for a *periodic* solution

# Periodic Solution of a FoDo Cell



Output of the optics program:

| Nr | Type   | Length<br>m | Strength<br>1/m <sup>2</sup> | $\beta_x$<br>m | $\alpha_x$ | $\varphi_x$<br>1/2 $\pi$ | $\beta_y$<br>m | $\alpha_y$ | $\varphi_y$<br>1/2 $\pi$ |
|----|--------|-------------|------------------------------|----------------|------------|--------------------------|----------------|------------|--------------------------|
| 0  | Marker | 0,000       | 0,000                        | 11,611         | 0,000      | 0,000                    | 5,295          | 0,000      | 0,000                    |
| 1  | QFH    | 0,250       | -0,541                       | 11,228         | 1,514      | 0,004                    | 5,488          | -0,781     | 0,007                    |
| 2  | QD     | 3,251       | 0,541                        | 5,488          | -0,781     | 0,070                    | 11,228         | 1,514      | 0,066                    |
| 3  | QFH    | 6,002       | -0,541                       | 11,611         | 0,000      | 0,125                    | 5,295          | 0,000      | 0,125                    |
| 4  | Marker | 6,002       | 0,000                        | 11,611         | 0,000      | 0,125                    | 5,295          | 0,000      | 0,125                    |

Qx= 0,125    Qy= 0,125

$$0.125 * 2\pi = 45^\circ$$

# Can we understand what the optics code is doing ?

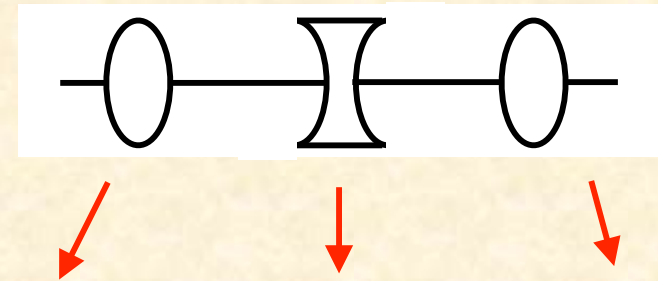
*matrices*

$$M_{QF} = \begin{pmatrix} \cos(\sqrt{K} * l_q) & \frac{1}{\sqrt{K}} \sin(\sqrt{K} * l_q) \\ -\sqrt{K} \sin(\sqrt{K} * l_q) & \cos(\sqrt{K} * l_q) \end{pmatrix}, \quad M_{Drift} = \begin{pmatrix} 1 & l \\ 0 & 1_d \end{pmatrix}$$

*strength and length of the FoDo elements*

$$K = +/- 0.54102 \text{ m}^{-2}$$
$$l_q = 0.5 \text{ m}$$
$$l_d = 2.5 \text{ m}$$

The matrix for the *complete cell* is obtained by multiplication of the element matrices



$$M_{FoDo} = M_{QFH} \cdot M_{ld} \cdot M_{QD} \cdot M_{ld} \cdot M_{QFH}$$

Putting the numbers in and *multiplying out* ...

$$M_{FoDo} = \begin{pmatrix} 0.707 & 8.206 \\ -0.061 & 0.707 \end{pmatrix}$$



The transfer matrix for 1 period gives us all the information that we need !

1.) is the motion stable?  
 $trace < 2$

$$trace(M_{FoDo}) = 1.415 \rightarrow \text{😊}$$

$$M(s) = \begin{pmatrix} \cos\psi_{cell} + \alpha_s \sin\psi_{cell} & \beta_s \sin\psi_{cell} \\ -\gamma_s \sin\psi_{cell} & \cos\psi_{cell} - \alpha_s \sin\psi_{cell} \end{pmatrix}$$

2.) phase advance per cell

$$\cos(\Psi_{cell}) = \frac{1}{2} Trace(M) = 0.707$$

$$\rightarrow \Psi_{cell} = \cos^{-1} \left\{ \frac{1}{2} Trace(M) \right\} = \underline{\underline{45^\circ}}$$

3.) hor  $\beta$ -function

$$\beta = \frac{m_{12}}{\sin\psi_{cell}} = \underline{\underline{11.611 \text{ m}}}$$

4.) hor  $\alpha$ -function

$$\alpha = \frac{m_{11} - \cos\psi_{cell}}{\sin\psi_{cell}} = \underline{\underline{0}}$$

## *We can determine the Twiss parameters !!*

- ... by calculating the matrix of a given periodic structure*
- ... using the magnet parameters and the product matrix of the structure*
- ... and compare with the (periodic) matrix in Twiss form.*

*The prize to pay ... is hidden in these crazy functions like cos / sinh / cosh etc ...*

*Can we do a bit easier ?*

*We can ... in thin lens approximation !*

*Matrix of a focusing quadrupole magnet:*

$$M_{QF} = \begin{pmatrix} \cos(\sqrt{K} * l) & \frac{1}{\sqrt{K}} \sin(\sqrt{K} * l) \\ -\sqrt{K} \sin(\sqrt{K} * l) & \cos(\sqrt{K} * l) \end{pmatrix}$$

*If the focal length  $f$  is much larger than the length of the quadrupole magnet,*

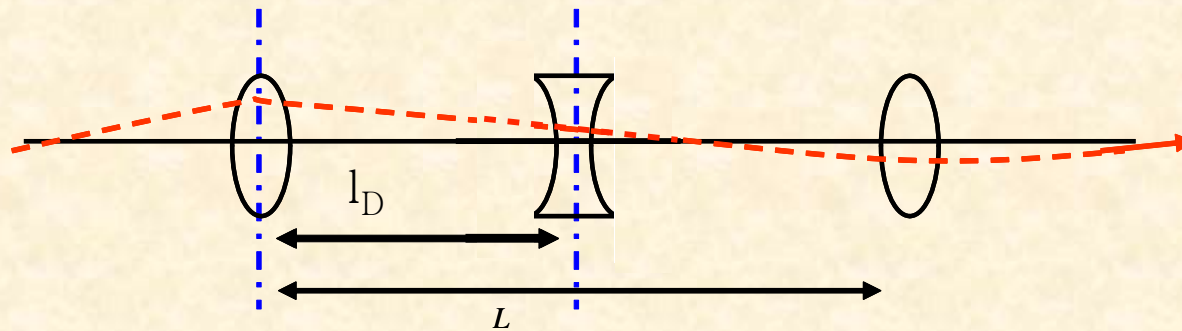
$$f = \frac{1}{kl_q} \gg l_q$$

*the transfer matrix can be approximated using*  $kl_q = \text{const}, l_q \rightarrow 0$

$$M_{QF} = \begin{pmatrix} 1 & 0 \\ \frac{-1}{f} & 1 \end{pmatrix}, \quad M_{QD} = \begin{pmatrix} 1 & 0 \\ \frac{1}{f} & 1 \end{pmatrix}$$

*=> we keep the focusing strength  $k \cdot l_q$  constant, but make the length zero.*

## 22.) FoDo in thin lens approximation



$$l_D = L/2$$

$$\tilde{f} = 2f$$

Calculate the matrix for a half cell, starting in the middle of a foc. quadrupole:

$$M_{halfCell} = M_{QD/2} * M_{ID} * M_{QF/2}$$

$$M_{halfCell} = \begin{pmatrix} 1 & 0 \\ 1/\tilde{f} & 1 \end{pmatrix} * \begin{pmatrix} 1 & l_D \\ 0 & 1 \end{pmatrix} * \begin{pmatrix} 1 & 0 \\ -1/\tilde{f} & 1 \end{pmatrix}$$

*note:* denotes the focusing strength of half a quadrupole, so

$$\tilde{f} = 2f$$

$$M_{halfCell} = \begin{pmatrix} 1 - l_D/\tilde{f} & l_D \\ -l_D/\tilde{f}^2 & 1 + l_D/\tilde{f} \end{pmatrix}$$

for the second half cell set  $f \rightarrow -f$



## *FoDo in thin lens approximation*

*Matrix for the complete FoDo cell*

$$M = \begin{pmatrix} 1 + \frac{l_D}{\tilde{f}} & l_D \\ -\frac{l_D}{\tilde{f}^2} & 1 - \frac{l_D}{\tilde{f}} \end{pmatrix} * \begin{pmatrix} 1 - \frac{l_D}{\tilde{f}} & l_D \\ -\frac{l_D}{\tilde{f}^2} & 1 + \frac{l_D}{\tilde{f}} \end{pmatrix}$$

$$M = \begin{pmatrix} 1 - \frac{2l_D^2}{\tilde{f}^2} & 2l_D \left(1 + \frac{l_D}{\tilde{f}}\right) \\ 2\left(\frac{l_D^2}{\tilde{f}^3} - \frac{l_D}{\tilde{f}^2}\right) & 1 - 2\frac{l_D^2}{\tilde{f}^2} \end{pmatrix}$$

*Now we know, that the phase advance is related to the transfer matrix by*

$$\cos(\Psi_{cell}) = \frac{1}{2} \text{trace}(M) = \frac{1}{2} \cdot \left(2 - \frac{4l_D^2}{\tilde{f}^2}\right) = 1 - \frac{2l_D^2}{\tilde{f}^2} \quad (i)$$

*After some beer and with a little bit of trigonometric gymnastics*

$$\cos(x) = \cos^2(x/2) - \sin^2(x/2) = 1 - 2 \cdot \sin^2(x/2) \quad (ii)$$

*we can calculate the phase advance as a function of the FoDo parameter ...  
by comparing (i) and (ii)*

$$\cos(\Psi_{cell}) = 1 - 2 \cdot \sin^2(\Psi_{cell}/2) = 1 - \frac{2l_d^2}{\tilde{f}^2} \rightarrow \sin(\Psi_{cell}/2) = l_d/\tilde{f} = \frac{L_{cell}}{2\tilde{f}}$$

*phase advance of a FoDo cell:  
(in thin lens approx)*

$$\sin(\Psi_{cell}/2) = \frac{L_{cell}}{4f}$$

*Example:  
45-degree Cell*

$$\begin{aligned} L_{Cell} &= l_{QF} + l_D + l_{QD} + l_D \\ &= 0.5m + 2.5m + 0.5m + 2.5m = 6m \end{aligned}$$

$$1/f = k \cdot l_Q = 0.5m \cdot 0.541 m^{-2} = 0.27 m^{-1} \rightarrow f = 3.7 m$$

$$\sin(\Psi_{cell}/2) = \frac{L_{cell}}{4f} = 0.405$$

$$\rightarrow \psi_{cell} = 47.8^\circ$$

$$\rightarrow \beta = 11.4 m$$

*Remember:*

*Exact calculation yields:*

$$\rightarrow \psi_{cell} = 45^\circ$$

$$\rightarrow \beta = 11.6 m$$

# Stability in a FoDo structure



SPS Lattice

$$M_{\text{FoDo}} = \begin{pmatrix} 1 - \frac{2l_D^2}{\tilde{f}^2} & 2l_D \left(1 + \frac{l_D}{\tilde{f}}\right) \\ 2\left(\frac{l_D^2}{\tilde{f}^3} - \frac{l_D}{\tilde{f}^2}\right) & 1 - 2\frac{l_D^2}{\tilde{f}^2} \end{pmatrix}$$

Stability requires:

$$|\text{Trace}(M)| < 2 \quad |\text{Trace}(M)| = \left| 2 - \frac{4l_D^2}{\tilde{f}^2} \right| < 2$$

$$\rightarrow f > \frac{L_{\text{cell}}}{4}$$

**For stability the focal length has to be larger than a quarter of the FoDo cell length ... don't focus too strong !**

Example:

45-degree Cell

$$\begin{aligned} L_{\text{Cell}} &= l_{QF} + l_D + l_{QD} + l_D \\ &= 0.5\text{m} + 2.5\text{m} + 0.5\text{m} + 2.5\text{m} = 6\text{m} \end{aligned}$$

$$\rightarrow L_{\text{cell}}/4 = 1.5 \text{ m}$$

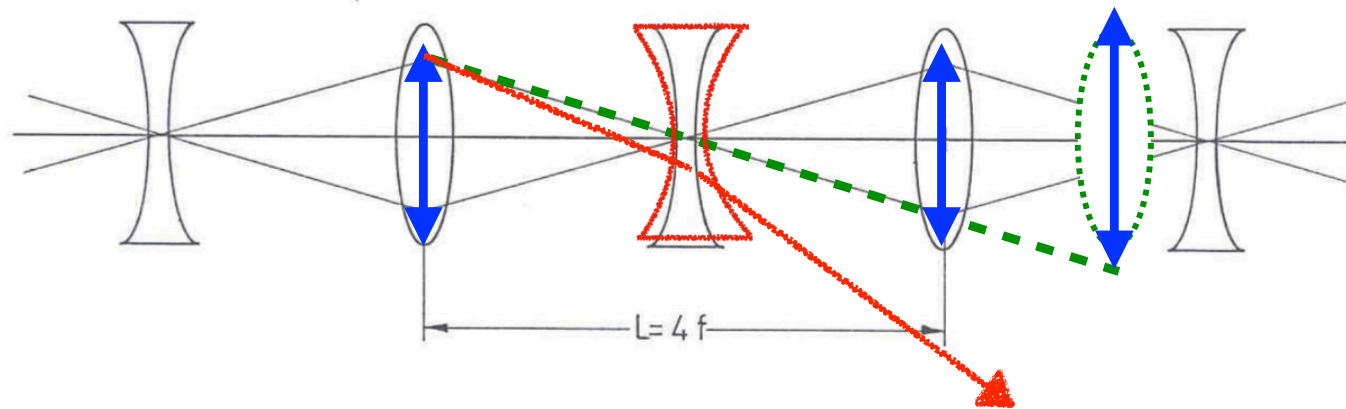
$$1/f = k \cdot l_Q = 0.5\text{m} \cdot 0.541 \text{ m}^{-2} = 0.27 \text{ m}^{-1} \quad \rightarrow f = 3.7 \text{ m}$$

**o.k.**

# The FODO cell

Stability condition  $4f \geq L$ , has a simple interpretation: **—> do not focus too strong !!**

- ▶ It is well known from optics that an object at a distance  $a = 2f$  from a focusing lens has its image at  $b = 2f$



- ▶ The defocusing lenses have no effect if a point-like object is located exactly on the axis at distance  $2f$  from a focusing lens, because they are traversed on the axis
- ▶ If however the lens system is moved further apart ( $L > 4f$ ), this is no more true and the divergence of the light or particle beam is increased by every defocusing lens

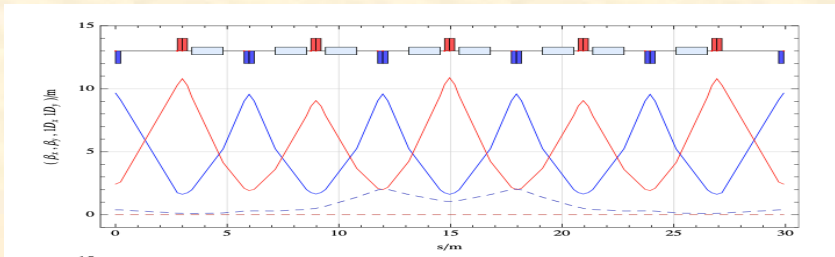


## 23.) Lattice Types: Arc structure

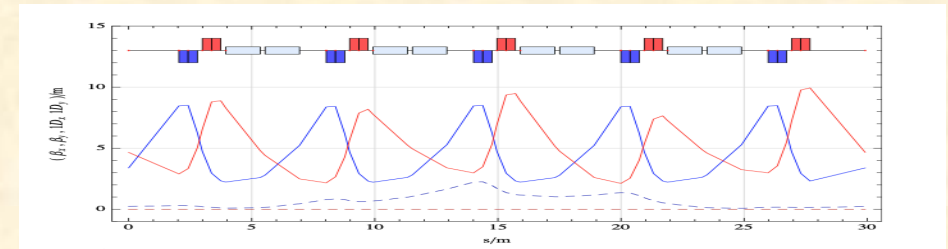
*Magnet structures can be optimised to obtain certain properties of the beam optics*

*The most important ones:*

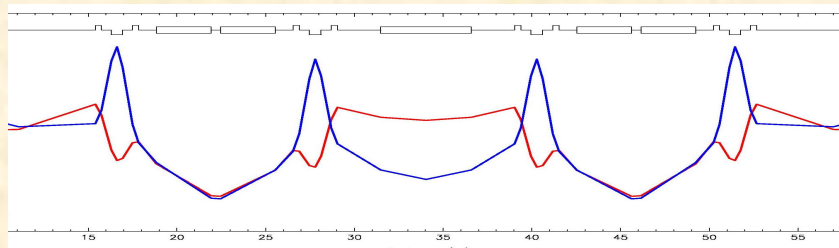
### *FoDo*



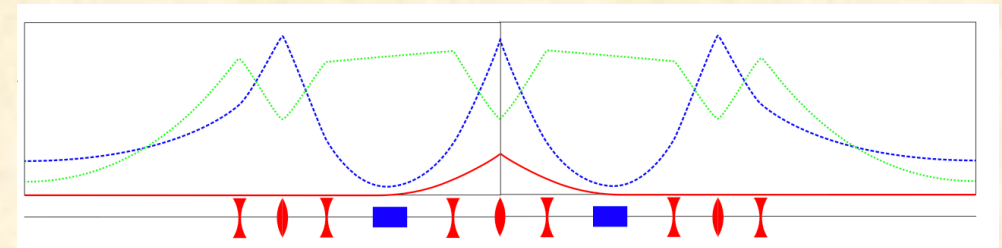
### *Doublets*



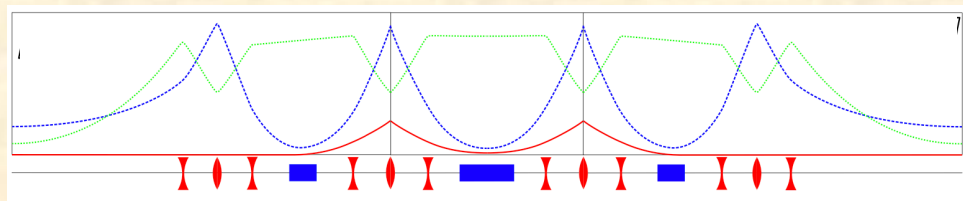
### *Triplet*



### *Double Bend Achromat*



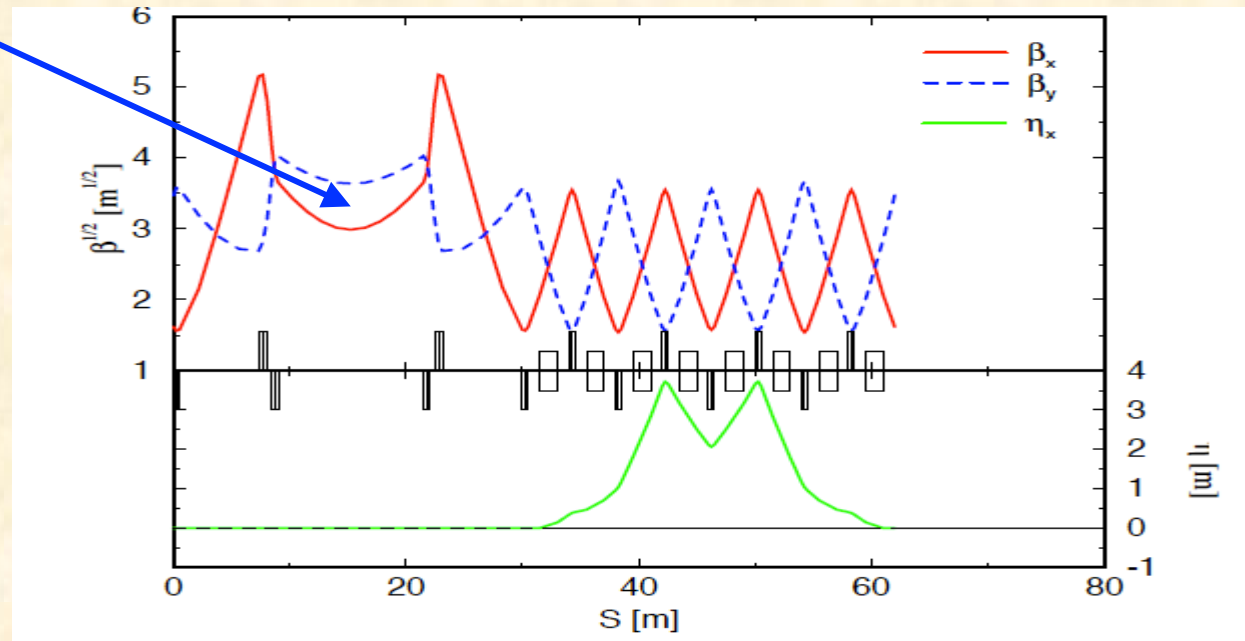
### *Triple Bend Achromat*



# Lattice Types: Insertions

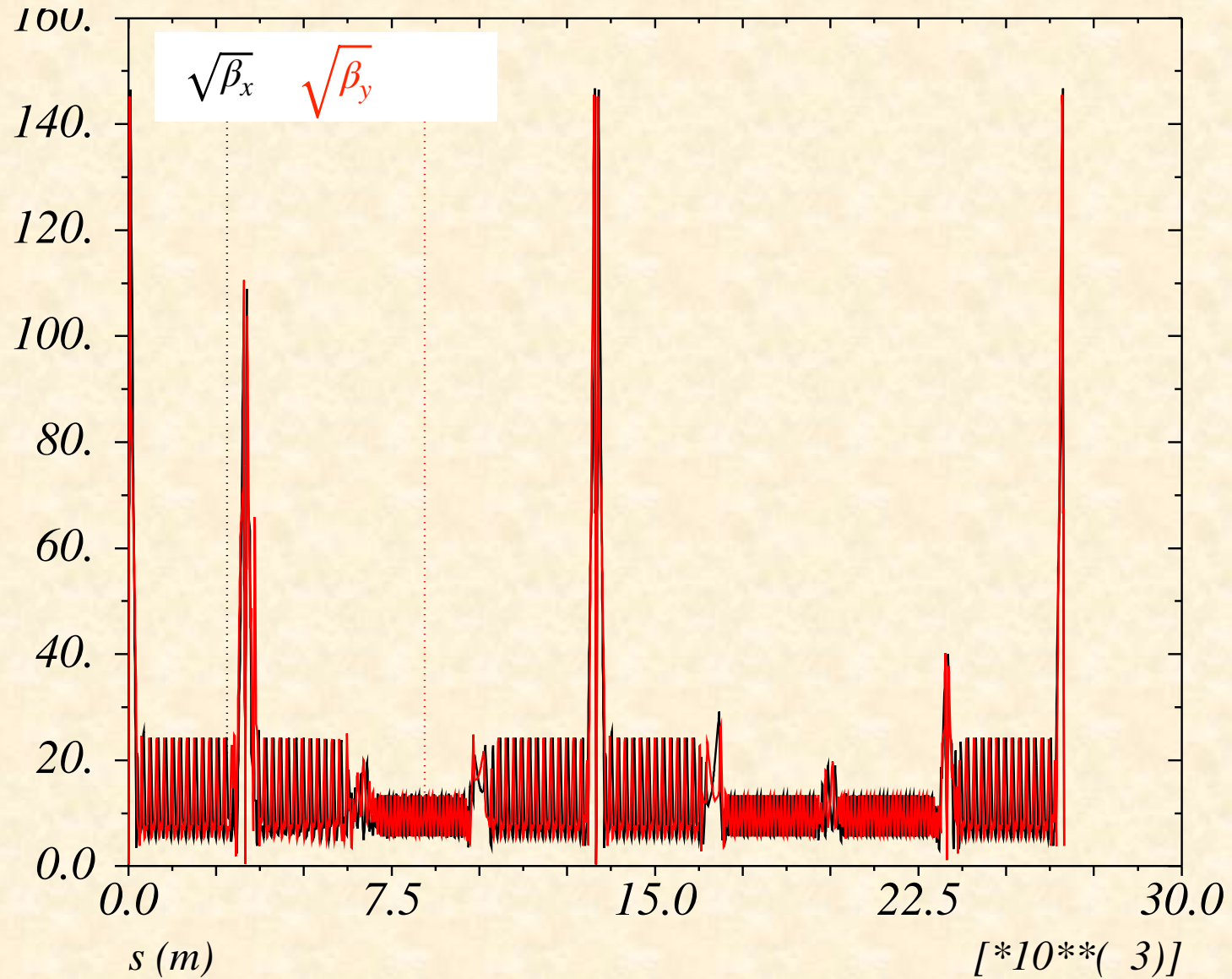
*Magnet structures - lattices - can be optimised to obtain certain properties of the beam optics*

## *Long symmetric Insertion*



*... a symmetric insertion that is optimised for small beta functions at the waist is called “Low-Beta-Insertion” or even “Mini-Beta-Insertion”*

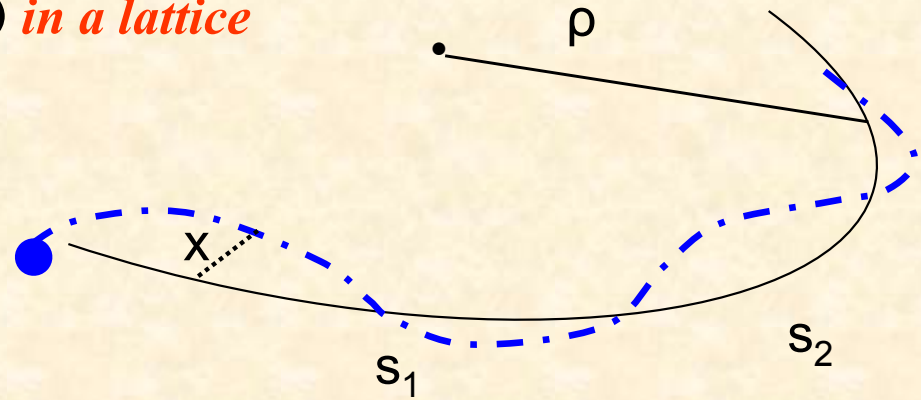
# Back to the FoDo



# Optics parameters of a FoDo:

Transformation of the coordinate vector  $(x, x')$  in a lattice

$$\begin{pmatrix} x(s) \\ x'(s) \end{pmatrix} = M_{s_1, s_2} \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix}$$



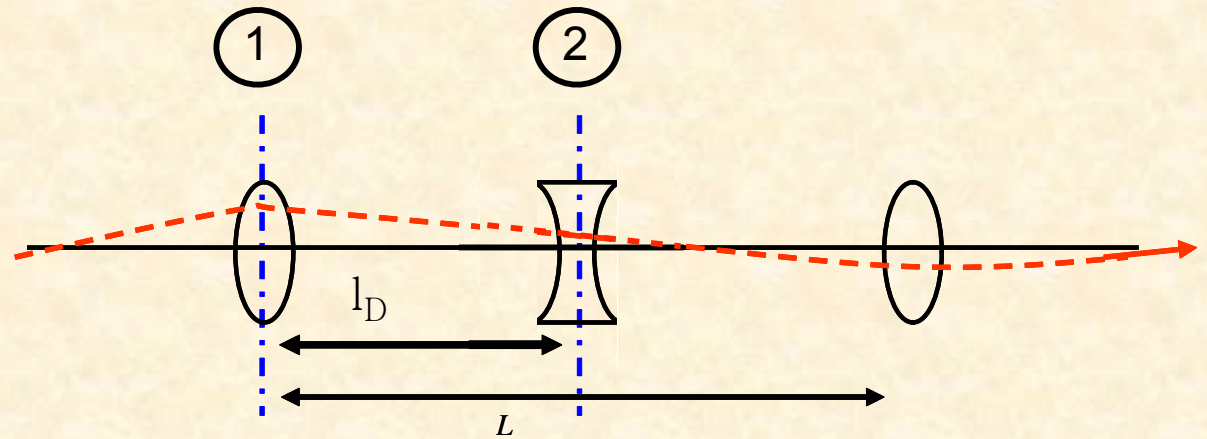
Transformation of the coordinate vector  $(x, x')$  expressed as a function of the Optics parameters

$$M_{1 \rightarrow 2} = \begin{pmatrix} \sqrt{\frac{\beta_2}{\beta_1}} (\cos \psi_{12} + \alpha_1 \sin \psi_{12}) & \sqrt{\beta_1 \beta_2} \sin \psi_{12} \\ \frac{(\alpha_1 - \alpha_2) \cos \psi_{12} - (1 + \alpha_1 \alpha_2) \sin \psi_{12}}{\sqrt{\beta_1 \beta_2}} & \sqrt{\frac{\beta_1}{\beta_2}} (\cos \psi_{12} - \alpha_2 \sin \psi_{12}) \end{pmatrix}$$



## Transfer Matrix for half a FoDo cell:

$$M_{\text{halfcell}} = \begin{pmatrix} 1 - l_D/\tilde{f} & l_D \\ -l_D/\tilde{f}^2 & 1 + l_D/\tilde{f} \end{pmatrix}$$



Compare to the twiss parameter form of  $M$

$$M_{1 \rightarrow 2} = \begin{pmatrix} \sqrt{\frac{\beta_2}{\beta_1}} (\cos\psi_{12} + \alpha_1 \sin\psi_{12}) & \sqrt{\beta_1\beta_2} \sin\psi_{12} \\ \frac{(\alpha_1 - \alpha_2) \cos\psi_{12} - (1 + \alpha_1\alpha_2) \sin\psi_{12}}{\sqrt{\beta_1\beta_2}} & \sqrt{\frac{\beta_1}{\beta_2}} (\cos\psi_{12} - \alpha_2 \sin\psi_{12}) \end{pmatrix}$$

In the *middle of a foc (defoc) quadrupole of the FoDo we always have  $\alpha = 0$ , and the half cell will lead us from  $\beta_{\max}$  to  $\beta_{\min}$*

$$\beta_1 = \beta_{\max} \quad \beta_2 = \beta_{\min}$$

$$M = \begin{pmatrix} \sqrt{\frac{\beta_{\min}}{\beta_{\max}}} \cos \frac{\psi_{\text{cell}}}{2} & \sqrt{\beta_{\min}\beta_{\max}} \sin \frac{\psi_{\text{cell}}}{2} \\ \frac{-1}{\sqrt{\beta_{\min}\beta_{\max}}} \sin \frac{\psi_{\text{cell}}}{2} & \sqrt{\frac{\beta_{\max}}{\beta_{\min}}} \cos \frac{\psi_{\text{cell}}}{2} \end{pmatrix}$$

*Solving for  $\beta_{max}$  and  $\beta_{min}$  and remembering that ....*

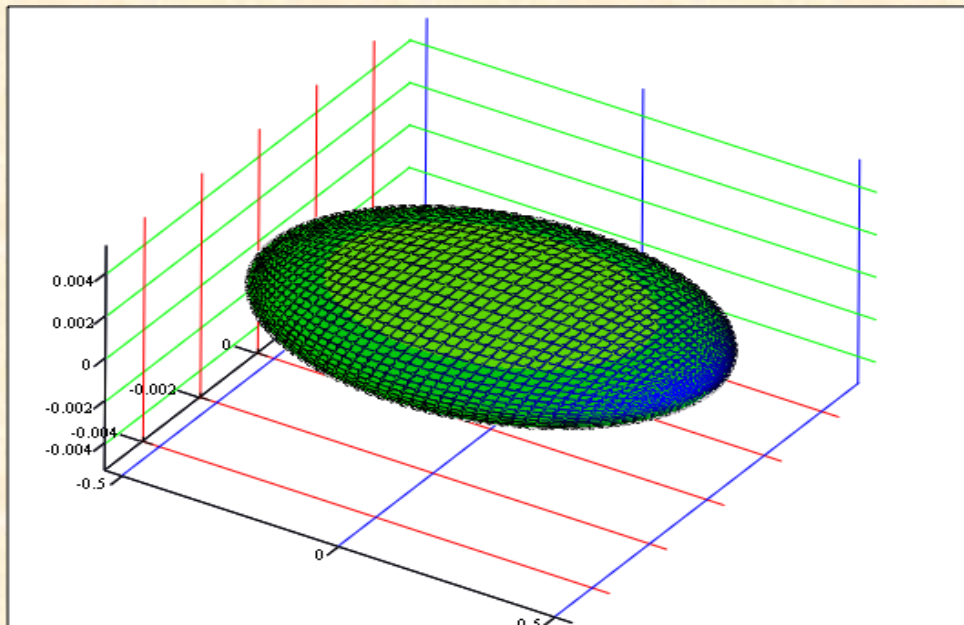
$$\sin \frac{\psi_{cell}}{2} = \frac{l_d}{\tilde{f}} = \frac{L}{4f}$$

$$\frac{m_{22}}{m_{11}} = \frac{\beta_{max}}{\beta_{min}} = \frac{1 + l_d/\tilde{f}}{1 - l_d/\tilde{f}} = \frac{1 + \sin \frac{\psi_{cell}}{2}}{1 - \sin \frac{\psi_{cell}}{2}}$$

$$\frac{m_{12}}{m_{21}} = \beta_{max} \cdot \beta_{min} = \tilde{f}^2 = \frac{l_d^2}{\sin^2 \frac{\psi_{cell}}{2}}$$

$$\beta_{max} = \frac{(1 + \sin \frac{\psi_{cell}}{2}) L}{\sin(\psi_{cell})} !$$

$$\beta_{min} = \frac{(1 - \sin \frac{\psi_{cell}}{2}) L}{\sin(\psi_{cell})} !$$



**The maximum and minimum values of the  $\beta$ -function are solely determined by the phase advance and the length of the cell.**

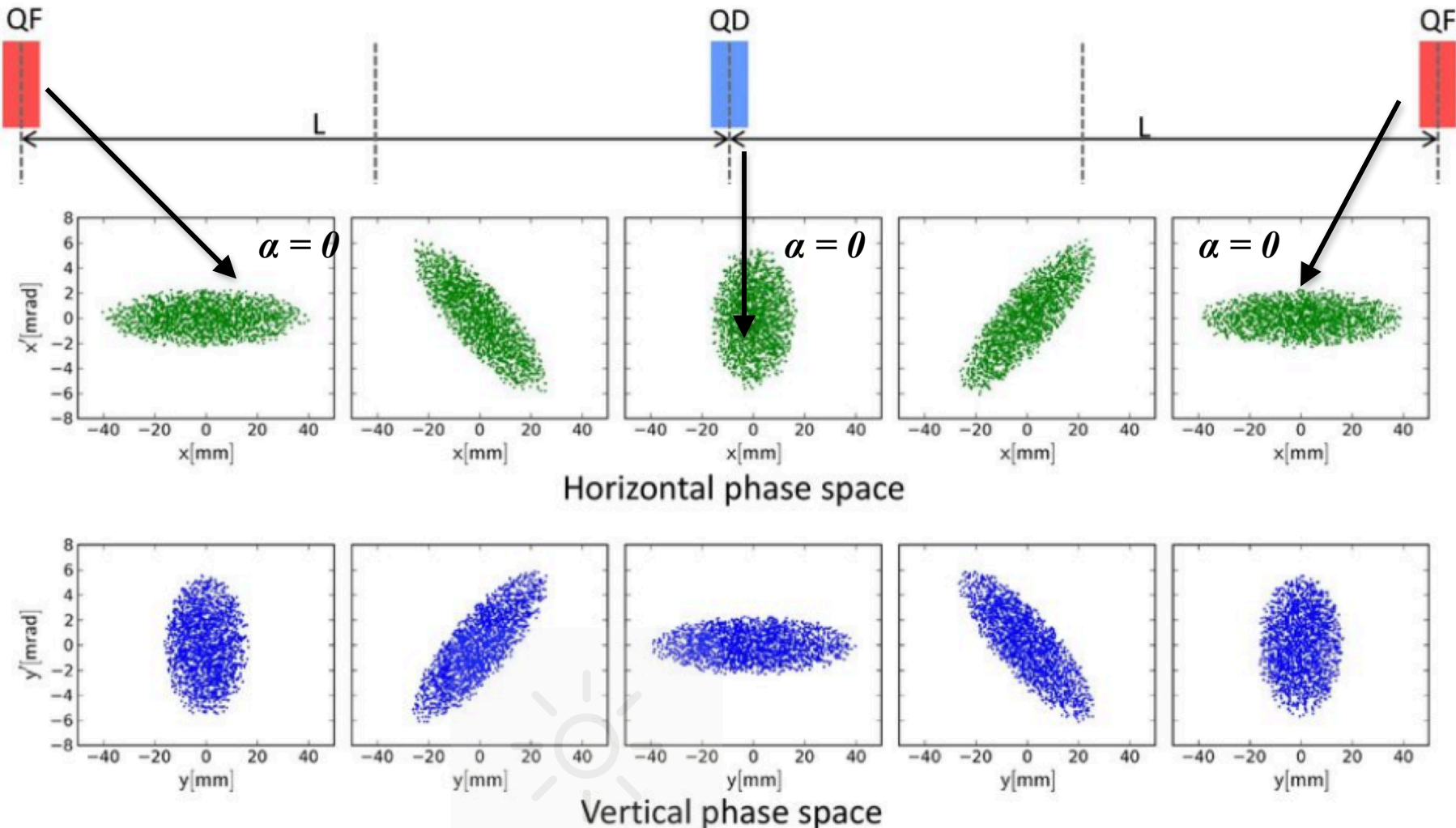
**Longer cells lead to larger  $\beta$**

*typical shape of a proton bunch in a FoDo Cell*

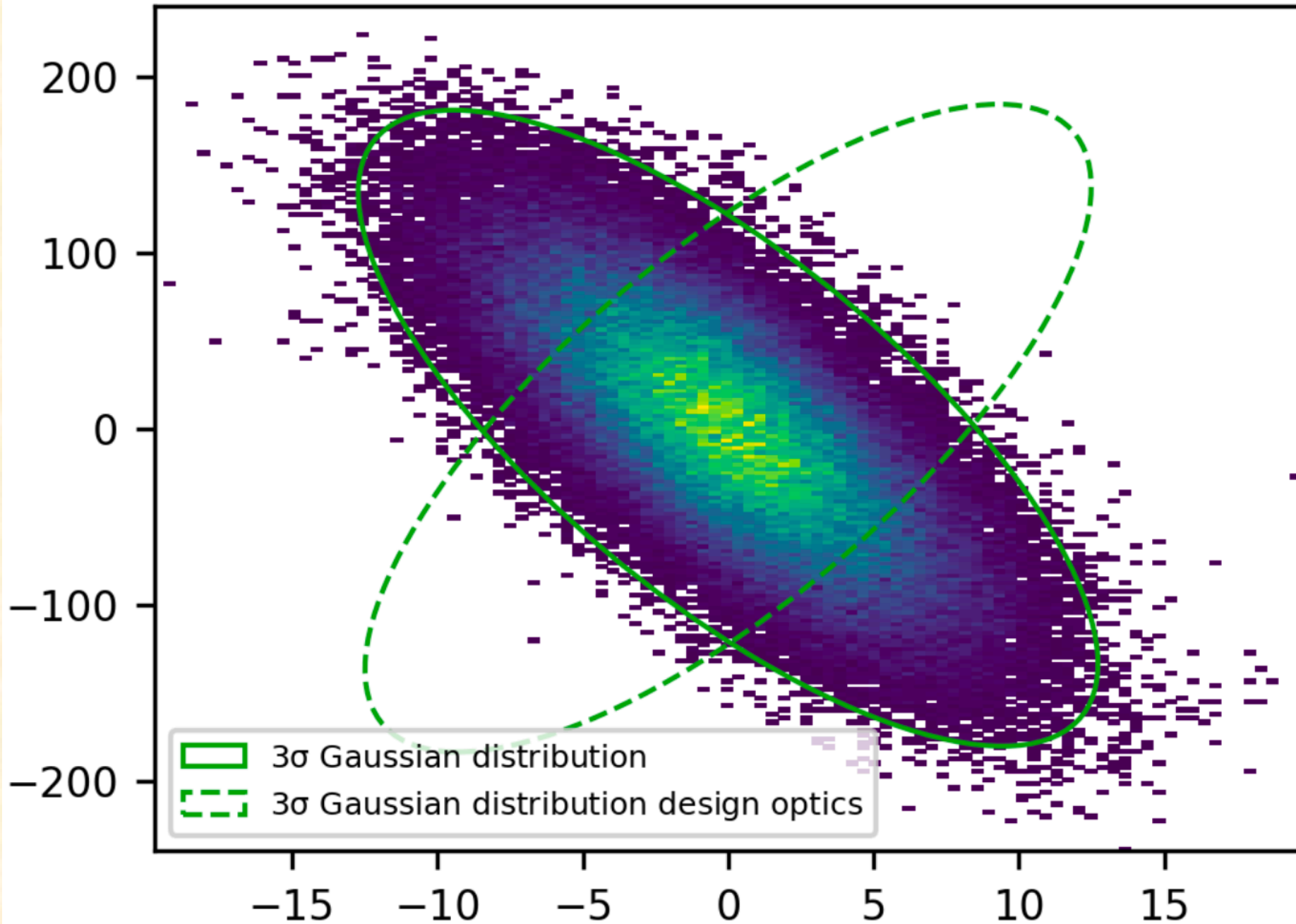
# Phase Space Ellipse in a FoDo

The Twiss family  $\alpha, \beta, \gamma$  determines shape & orientation of the ellipse

Phase space evolution in a FODO cell



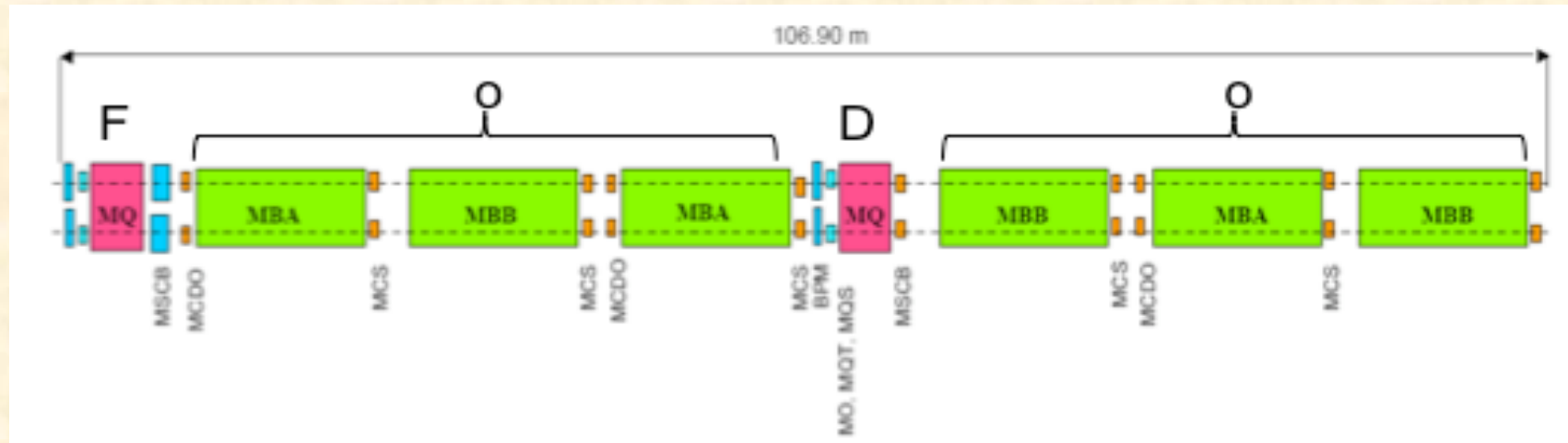
# *Phase Space Ellipse of a real beam in a FoDo*





*and now in reality ...*

*LHC: Arc structure based on 90° FoDo in both planes*



*equipped with additional corrector coils*

- MB: main dipole*
- MQ: main quadrupole*
- MQT: Trim quadrupole*
- MQS: Skew trim quadrupole*
- MO: Lattice octupole (Landau damping)*
- MSCB: Skew sextupole*
- Orbit corrector dipoles*
- MCS: Spool piece sextupole*
- MCDO: Spool piece 8 / 10 pole*
- BPM: Beam position monitor + diagnostics*

## ***One Word about non-periodic Lattices:***

- ▶ In the previous sections the Twiss parameters  $\alpha$ ,  $\beta$ ,  $\gamma$ , and  $\mu$  have been derived for a periodic, circular accelerator. The condition of periodicity was essential for the definition of the beta function (Hill's equation)
- ▶ Often, however, a particle beam moves only **once** along a **beam transfer line**, but one is nonetheless interested in quantities like beam envelopes and beam divergence
- ▶ In a circular accelerator  $\alpha$ ,  $\beta$ , and  $\gamma$  are completely determined by the magnet optics and the condition of periodicity (beam properties are not involved - only the beam emittance is chosen to match the beam size)
- ▶ In a transfer line,  $\alpha$ ,  $\beta$ , and  $\gamma$  are no longer uniquely determined by the transfer matrix, but they also depend on initial conditions which have to be specified in an adequate way

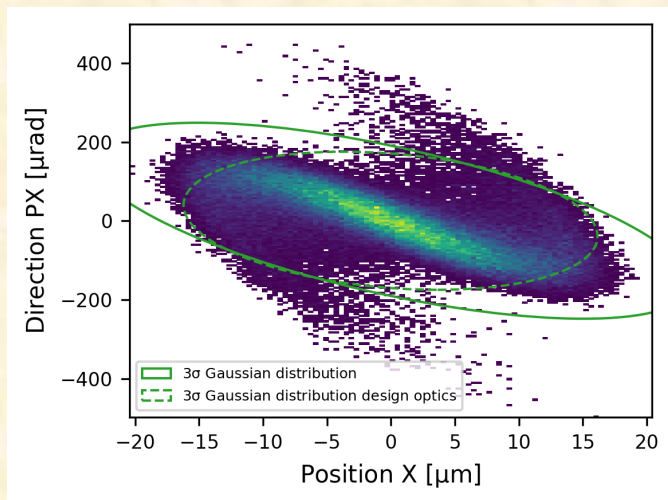
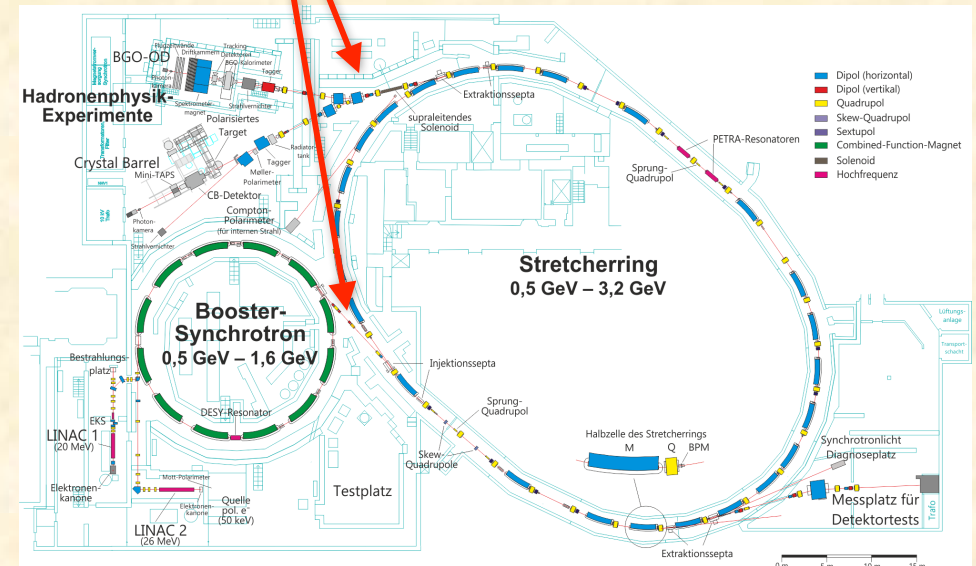
# Transferring the Twiss family:

Rule for a non-periodic situation

$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_s = \begin{pmatrix} C^2 & -2SC & S^2 \\ -CC' & SC' + CS' & -SS' \\ C'^2 & -2S'C' & S'^2 \end{pmatrix} \cdot \begin{pmatrix} \beta_0 \\ \alpha_0 \\ \gamma_0 \end{pmatrix}$$

However we have to **determine (!)** the initial Twisses

*ELSA storage ring: start with the (uniquely) defined periodic Twiss.*



*LHeC: energy recovery linac after the collision  
—> fit ... and guess:  $\beta, \alpha, \varepsilon$*



# *Introduction to Transverse Beam Dynamics*

*III.) The „not so ideal world“*

*Acceleration and Momentum Spread*



# Remember:

## Beam Emittance and Phase Space Ellipse:

equation of motion:  $x'' + K x = 0$

general solution of Hills equation:  $x(s) = \sqrt{\varepsilon} \sqrt{\beta(s)} \cos(\psi(s) + \varphi)$

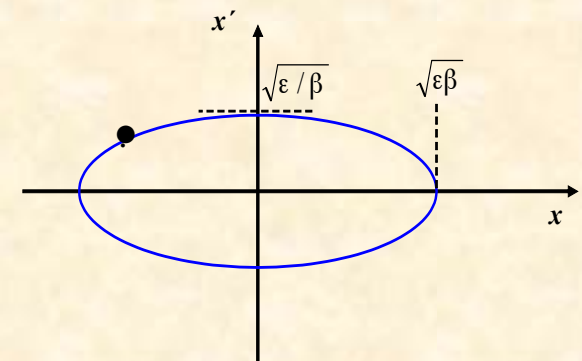
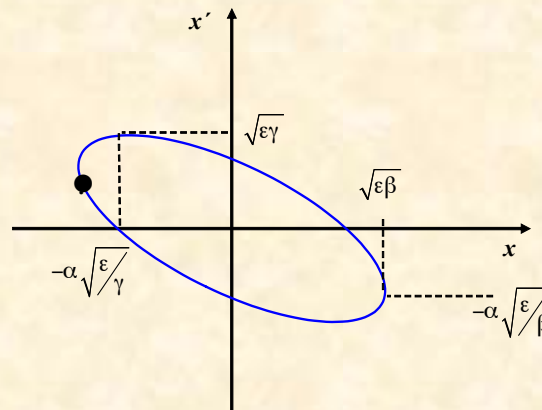
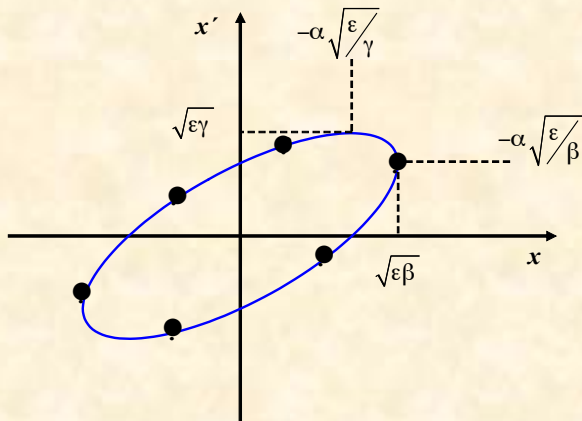
beam size:  $\sigma = \sqrt{\varepsilon\beta} \approx \text{"mm"}$

$$\varepsilon = \gamma(s) x^2(s) + 2\alpha(s)x(s)x'(s) + \beta(s) x'^2(s)$$

$$\alpha(s) = -\frac{1}{2} \beta'(s)$$

$$\gamma(s) = \frac{1 + \alpha(s)^2}{\beta(s)}$$

- \*  $\varepsilon$  is a **constant of the motion** ... it is independent of „s“
- \* parametric representation of an **ellipse in the  $x x'$  space**
- \* shape and orientation of ellipse are given by  $\alpha, \beta, \gamma$

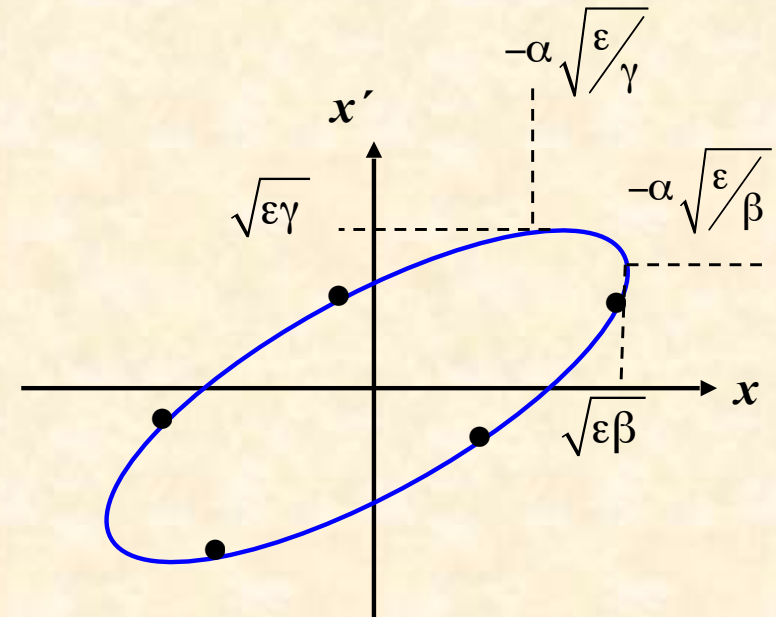


## 24.) Liouville during Acceleration

$$\varepsilon = \gamma(s) x^2(s) + 2\alpha(s)x(s)x'(s) + \beta(s) x'^2(s)$$

*Beam Emittance* corresponds to the area covered in the  $x, x'$  Phase Space Ellipse

*Liouville: Area in phase space is constant.*



**But so sorry ...  $\varepsilon \neq \text{const} !$**

*Classical Mechanics:*

*phase space = diagram of the two canonical variables  
position & momentum*

$x$   $p_x$

$$p_j = \frac{\partial L}{\partial \dot{q}_j} ; L = T - V = \text{kin. Energy} - \text{pot. Energy}$$

According to Hamiltonian mechanics:  
phase space diagram relates the variables  $q$  and  $p$

**Liouville's Theorem:**

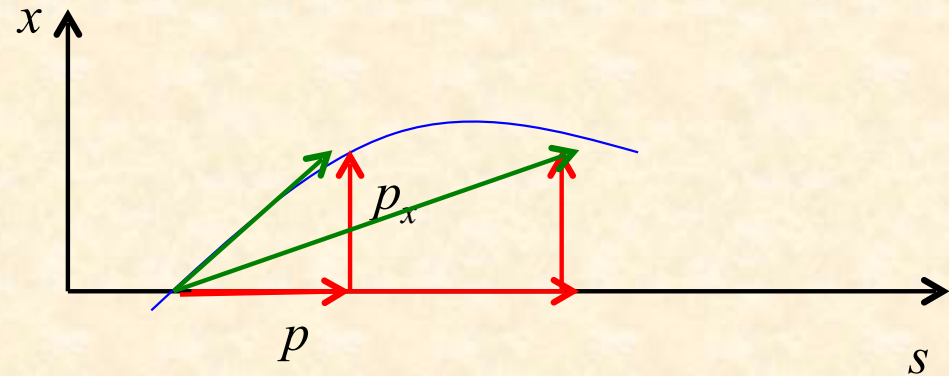
$$\int p dq = \text{const}$$

$$\int p_x dx = \text{const}$$

$$\gamma = \frac{1}{\sqrt{1 - \frac{v^2}{c^2}}} \quad ; \quad \beta_x = \frac{\dot{x}}{c}$$

for convenience (i.e. *because we are lazy bones*) we use in accelerator theory:

$$x' = \frac{dx}{ds} = \frac{dx}{dt} \cdot \frac{dt}{ds} = \frac{\beta_x}{\beta} = \frac{p_x}{p}$$



$$\underbrace{\int x' dx}_{\varepsilon} = \frac{p_x dx}{p} \propto \frac{\text{const}}{m_0 c \gamma \beta}$$

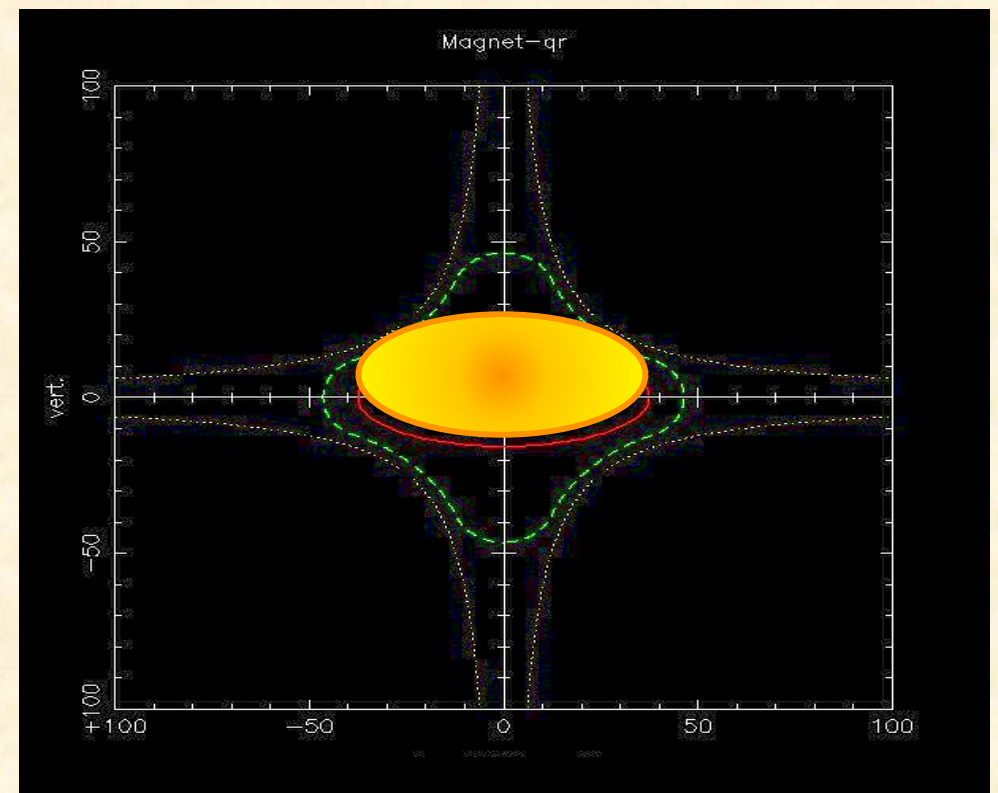
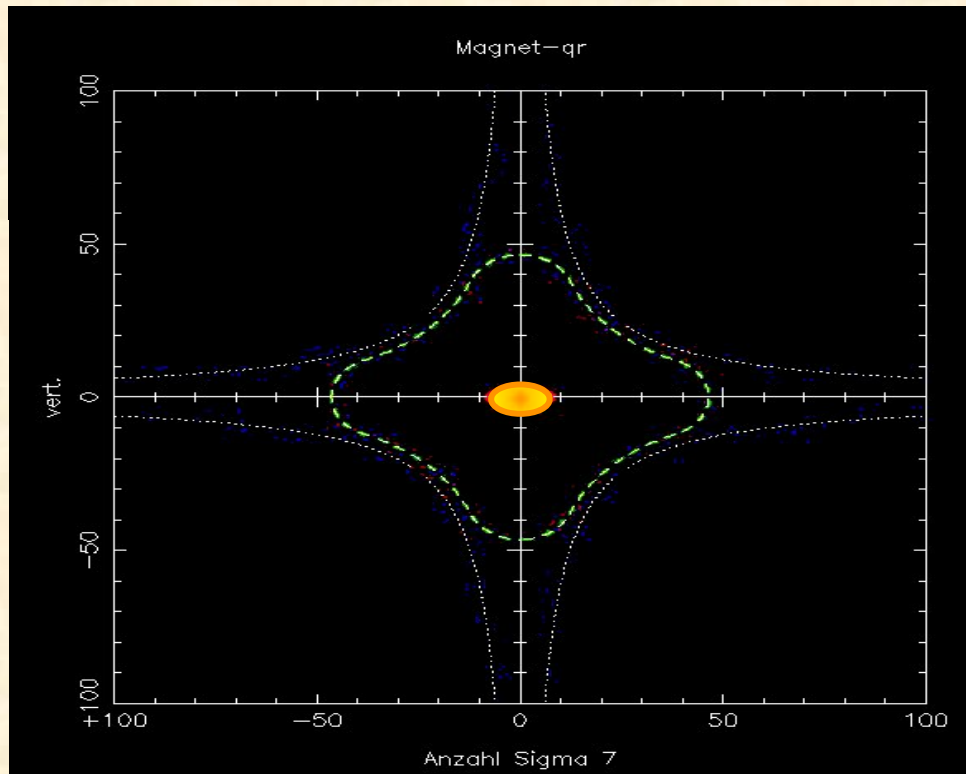
$$\Rightarrow \varepsilon = \int x' dx \propto \frac{1}{\beta \gamma}$$

*the beam emittance  
shrinks during  
acceleration  $\varepsilon \sim 1/\gamma$*

## Example: HERA proton ring

injection energy: 40 GeV      $\gamma = 43$   
flat top energy: 920 GeV      $\gamma = 980$

emittance  $\varepsilon$  (40GeV) =  $1.2 * 10^{-7}$  m rad  
 $\varepsilon$  (920GeV) =  $5.1 * 10^{-9}$  m rad



... at injection, E = 40 GeV

... and at E = 920



## Nota bene:

1.) A proton machine ... or an electron linac ... needs the highest aperture at injection energy !!!

as soon as we start to accelerate the **beam size shrinks as  $\gamma^{-1/2}$**  in both planes.

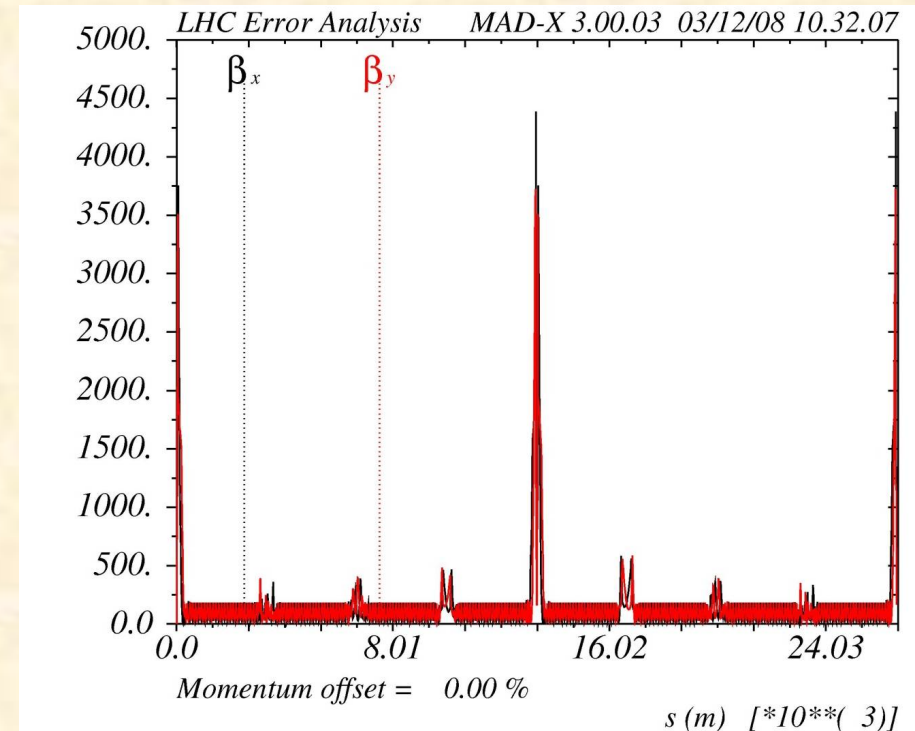
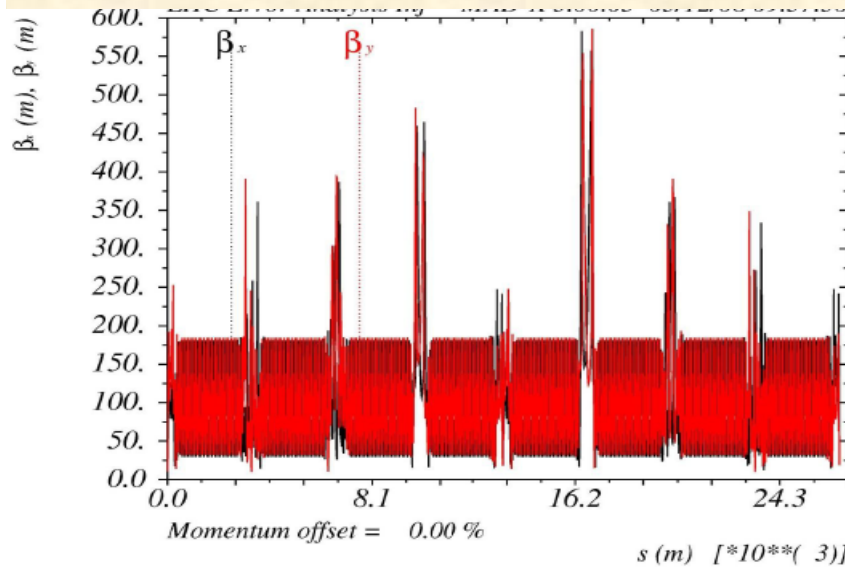
$$\sigma = \sqrt{\epsilon\beta}$$

2.) At lowest energy the machine will have the major aperture problems,

—> here we have to **minimise  $\hat{\beta}$**

3.) we need **different beam optics** adopted to the energy:

**A Mini Beta concept will only be adequate at flat top where the beam emittance is small !!**



LHC injection optics at 450 GeV

LHC mini beta optics at 7000 GeV

# *Liouville during Acceleration*

***Protons***

*... shrink during acceleration*

***ATTENTION !!!***

***Electron beams*** *in a storage ring are determined by light emission and behave completely different.*

*... they grow.*

The „ not so ideal world “

## 25.) The „ $\Delta p / p \neq 0$ “ Problem

*ideal accelerator: all particles will see the same accelerating voltage.*

$$\rightarrow \Delta p / p = 0$$

*„nearly ideal“ accelerator: Cockroft Walton or van de Graaf*

$$\Delta p / p \approx 10^{-5}$$



Vivitron, Straßbourg, inner structure of the acc. section



MP Tandem van de Graaf Accelerator  
at MPI for Nucl. Phys. Heidelberg 47

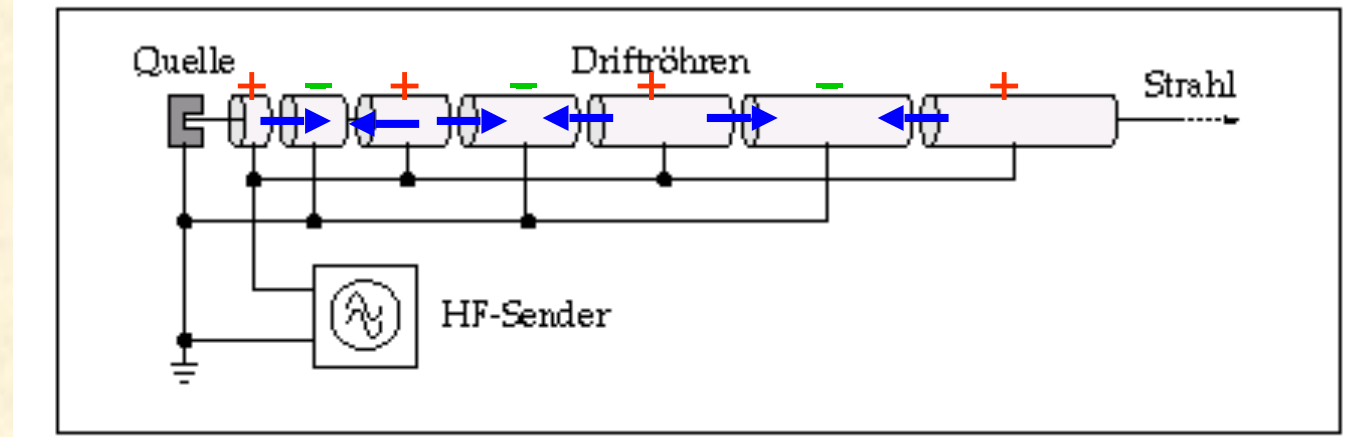


# Linear Accelerator

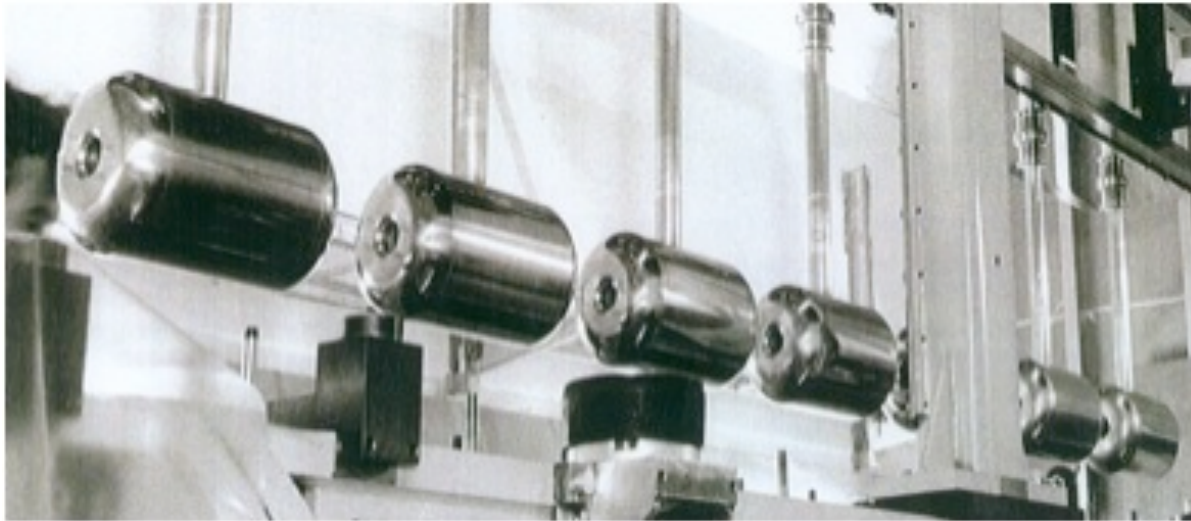
1928, Wideroe: schematic Layout:

Energy Gain per „Gap“:

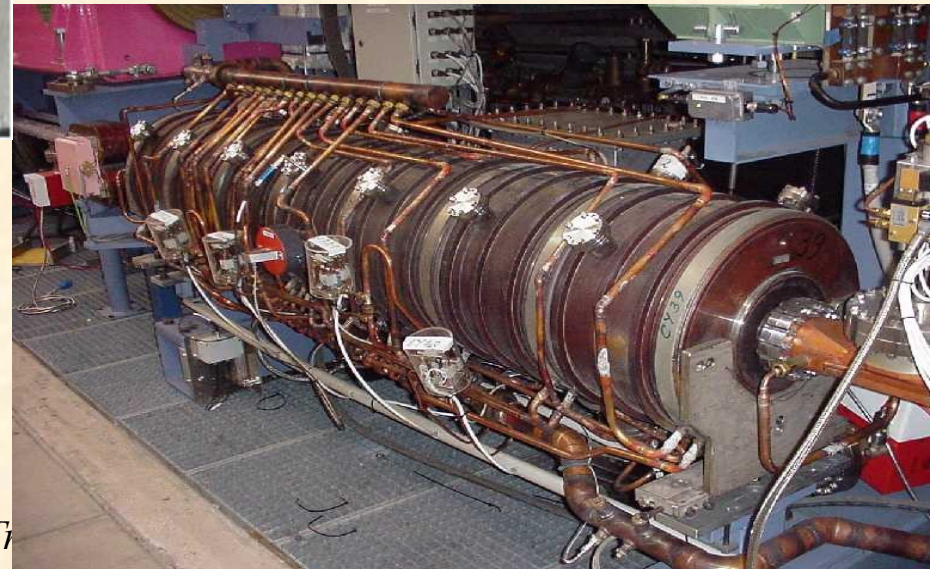
$$W = q U_0 \sin \omega_{RF} t$$



drift tube structure at a proton linac



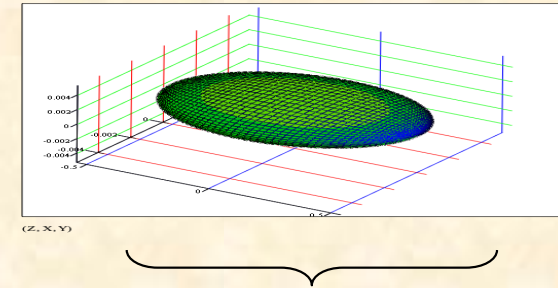
500 MHz cavities in an electron storage ring



\* **RF Acceleration:** multiple application of the same acceleration voltage; brilliant idea to gain higher energies

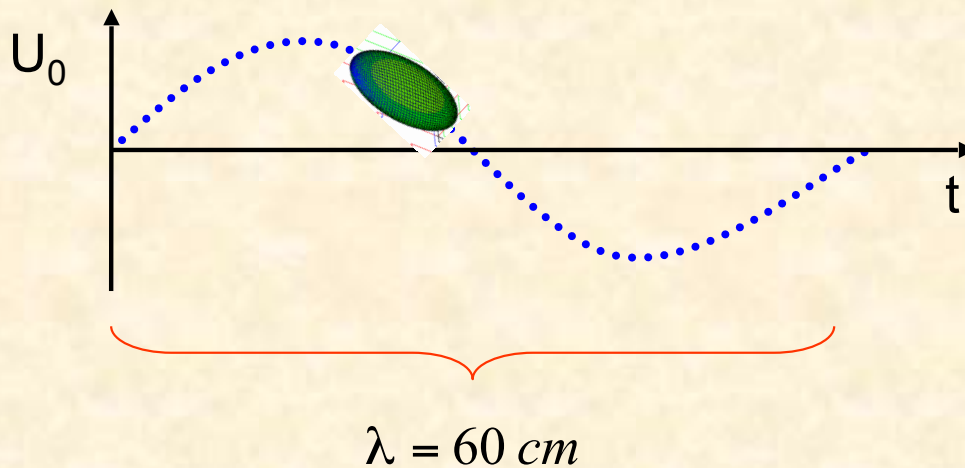
# Problem: panta rhei !!!

(Heraklit: 540-480 v. Chr.)



**Bunch length of Electrons  $\approx 1\text{cm}$**

**Example: HERA RF:**



$$\left. \begin{aligned} \nu &= 500 \text{ MHz} \\ c &= \lambda \nu \end{aligned} \right\} \lambda = 60 \text{ cm}$$

$$\sin(90^\circ) = 1$$

$$\sin(84^\circ) = 0.994$$

$$\frac{\Delta U}{U} = 6.0 \cdot 10^{-3}$$

**typical momentum spread of an electron bunch:**

$$\frac{\Delta p}{p} \approx 1.0 \cdot 10^{-3}$$



# *Dispersive and Chromatic Effects: $\Delta p/p \neq 0$*

*Are there any Problems ???*

*Sure there are !!!*

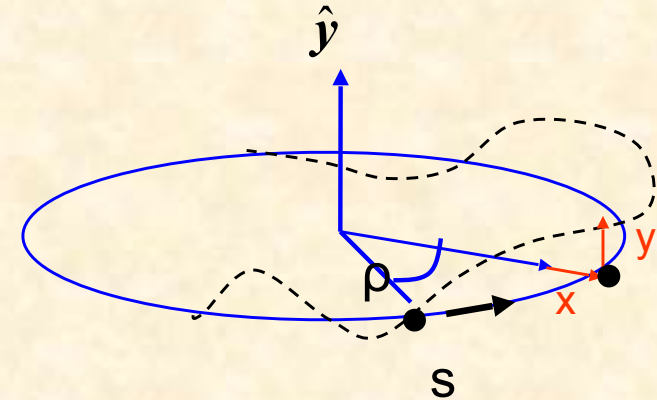
*font colours chosen for  
pedagogical reasons*

## 26.) Dispersion: trajectories for $\Delta p / p \neq 0$

**Question:** do you remember last session, page 12 ? ... sure you do

**Force acting on the particle**

$$F = m \frac{d^2}{dt^2}(x + \rho) - \frac{mv^2}{x + \rho} = - eB_y v$$



**remember:**  $x \approx mm$  ,  $\rho \approx m$  ...  $\rightarrow$  develop for small  $x$

$$m \frac{d^2 x}{dt^2} - \frac{mv^2}{\rho} \left(1 - \frac{x}{\rho}\right) = - eB_y v$$

**consider only linear fields, and change independent variable:  $t \rightarrow s$**   $B_y = B_0 + x \frac{\partial B_y}{\partial x}$

$$x'' - \frac{1}{\rho} \left(1 - \frac{x}{\rho}\right) = - \frac{eB_0}{mv} + \frac{exg}{mv}$$

$$p = p_0 + \Delta p$$

**... but now take a small momentum error into account !!!**

# Dispersion:

develop for small momentum error  $\Delta p \ll p_0 \Rightarrow \frac{1}{p_0 + \Delta p} \approx \frac{1}{p_0} - \frac{\Delta p}{p_0^2}$

$$x'' - \cancel{\frac{1}{\rho}} + \frac{x}{\rho^2} \approx \underbrace{-\frac{eB_0}{p_0}}_{-\frac{1}{\rho}} + \frac{\Delta p}{p_0^2} eB_0 + \underbrace{\frac{exg}{p_0}}_{k * x} - \underbrace{xeg \frac{\Delta p}{p_0^2}}_{\approx 0}$$

$$x'' + \frac{x}{\rho^2} \approx \frac{\Delta p}{p_0} \frac{1}{\rho} + x \cdot k$$

$$x'' + x \left( \frac{1}{\rho^2} - k \right) = \frac{\Delta p}{p_0} \frac{1}{\rho}$$

**Momentum spread** of the beam adds a term on the r.h.s. of the equation of motion.  
 —> **inhomogeneous differential equation.**

## Dispersion: trajectories for $\Delta p / p \neq 0$

### Dispersion

What if particles in a bunch have different momenta?

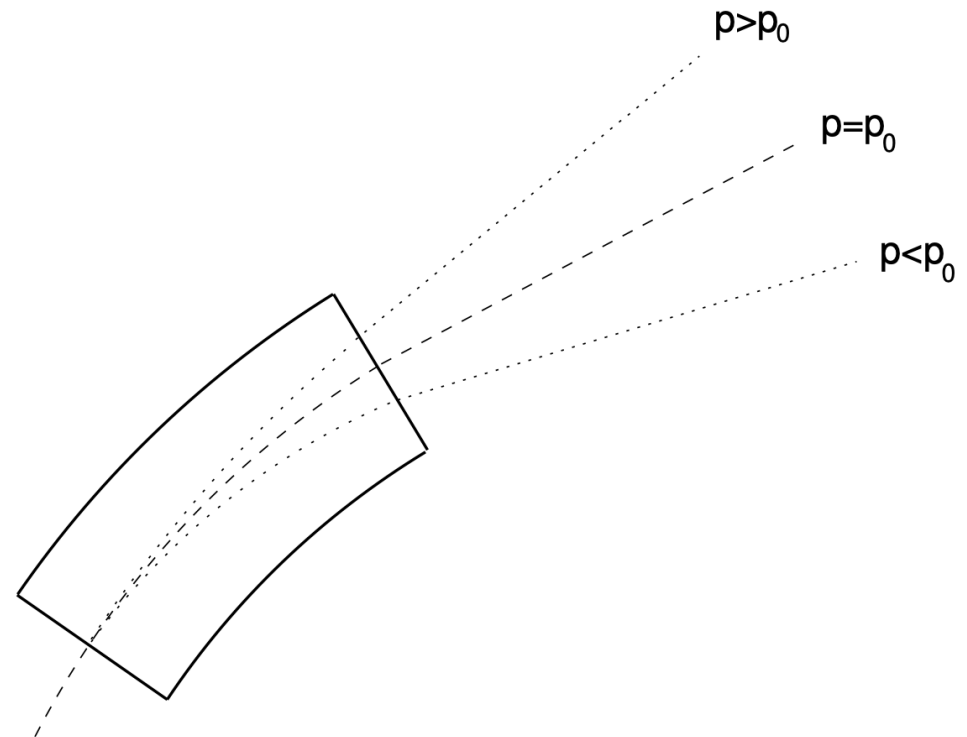
Remember beam rigidity:

$$B\rho = \frac{P}{q} \quad (100)$$

Orbit:

$$x(s) = D(s) \frac{\Delta P}{P_0} \quad (101)$$

where  $D(s)$  is the dispersion function, an intrinsic property of dipole magnets.



# Dispersion:

$$x'' + x\left(\frac{1}{\rho^2} - k\right) = \frac{\Delta p}{p} \cdot \frac{1}{\rho}$$

*general solution:*

$$x(s) = x_h(s) + x_i(s)$$

$$\begin{cases} x_h''(s) + K(s) \cdot x_h(s) = 0 \\ x_i''(s) + K(s) \cdot x_i(s) = \frac{1}{\rho} \cdot \frac{\Delta p}{p} \end{cases}$$

*Normalise with respect to  $\Delta p/p$ :*

$$D(s) = \frac{x_i(s)}{\frac{\Delta p}{p}}$$

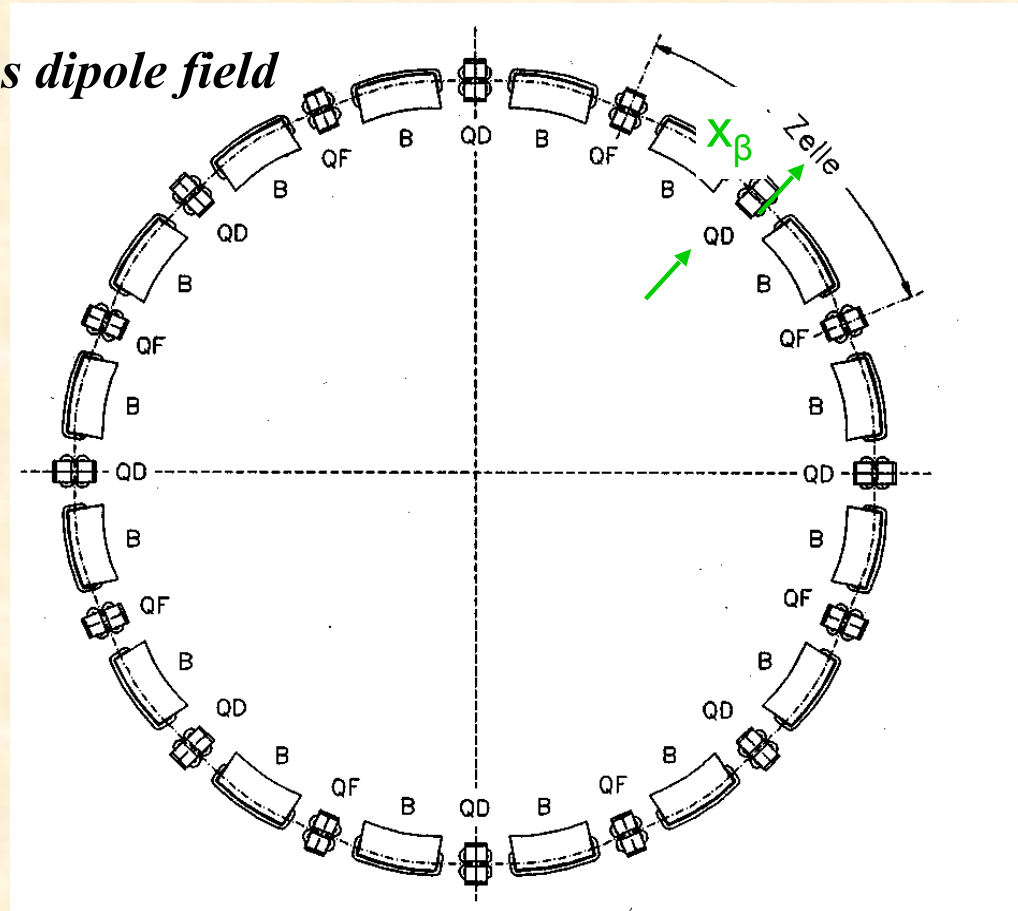
## Dispersion function $D(s)$

- \* is that **special orbit**, an **ideal particle** would have for  $\Delta p/p = 1$
- \* the **orbit of any particle** is the **sum** of the well known  $x_\beta$  and the **dispersion**
- \* as  **$D(s)$**  is just **another orbit** it will be subject to the focusing properties of the lattice



## Dispersion

Example: homogeneous dipole field



for  $\Delta p/p > 0$

$$D(s) \cdot \frac{\Delta p}{p}$$

## Matrix formalism:

$$x(s) = x_\beta(s) + D(s) \cdot \frac{\Delta p}{p}$$

$$x(s) = C(s) \cdot x_0 + S(s) \cdot x'_0 + D(s) \cdot \frac{\Delta p}{p}$$

$$\begin{pmatrix} x \\ x' \end{pmatrix}_s = \begin{pmatrix} C & S \\ C' & S' \end{pmatrix} \begin{pmatrix} x \\ x' \end{pmatrix}_0 + \frac{\Delta p}{p} \begin{pmatrix} D \\ D' \end{pmatrix}_0$$

## *Resume':*

*beam emittance*

$$\varepsilon \propto \frac{1}{\beta\gamma}$$

*beta function in a drift*

$$\beta(s) = \beta_0 - 2\alpha_0 s + \gamma_0 s^2$$

*... and for  $\alpha = 0$*

$$\beta(s) = \beta_0 + \frac{s^2}{\beta_0}$$

*particle trajectory for  $\Delta p/p \neq 0$   
inhomogeneous equation*

$$\mathbf{x}'' + \mathbf{x} \left( \frac{1}{\rho^2} - k \right) = \frac{\Delta \mathbf{p}}{p_0} \frac{1}{\rho}$$

*... and its solution*

$$x(s) = x_\beta(s) + D(s) \cdot \frac{\Delta p}{p}$$