Transverse Beam Optics IV

Bernhard Holzer, CERN

Errors in Field and Gradient

The " überhaupt nicht ideal world "



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Dispersion:

$$x'' + x(\frac{1}{\rho^2} - k) = \frac{\Delta p}{p} \cdot \frac{1}{\rho}$$

general solution:

$$x(s) = x_h(s) + x_i(s)$$

$$\begin{cases} x_h''(s) + K(s) \cdot x_h(s) = 0\\ x_i''(s) + K(s) \cdot x_i(s) = \frac{1}{\rho} \cdot \frac{\Delta p}{p} \end{cases}$$

Normalise with respect to $\Delta p/p:/$

$$D(s) = \frac{x_i(s)}{\frac{\Delta p}{p}}$$

Dispersion function D(s)

* is that special orbit, an ideal particle would have for $\Delta p/p = 1$

* the orbit of any particle is the sum of the well known x_{B} and the dispersion

* as **D**(s) is just another orbit it will be subject to the focusing properties of the lattice



Matrix formalism:

$$x(s) = x_{\beta}(s) + D(s) \cdot \frac{\Delta p}{p}$$
$$x(s) = C(s) \cdot x_0 + S(s) \cdot x'_0 + D(s) \cdot \frac{\Delta p}{p}$$

$$\begin{pmatrix} \boldsymbol{x} \\ \boldsymbol{x}' \end{pmatrix}_{s} = \begin{pmatrix} \boldsymbol{C} & \boldsymbol{S} \\ \boldsymbol{C}' & \boldsymbol{S}' \end{pmatrix} \begin{pmatrix} \boldsymbol{x} \\ \boldsymbol{x}' \end{pmatrix}_{0} + \frac{\Delta \boldsymbol{p}}{\boldsymbol{p}} \begin{pmatrix} \boldsymbol{D} \\ \boldsymbol{D}' \end{pmatrix}_{0}$$

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Calculate D, D': ... takes a couple of sunny Sunday evenings !

$$D(s) = S(s) \int_{s_0}^{s_1} \frac{1}{\rho} C(\tilde{s}) d\tilde{s} - C(s) \int_{s_0}^{s_1} \frac{1}{\rho} S(\tilde{s}) d\tilde{s}$$

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Dispersion and Beam Size:

Super-position of two Gaussian distributions

In this example from the HERA storage ring (DESY) we see the Twiss parameters and the dispersion near the interaction point. In the periodic region,

$$egin{aligned} x_eta\left(s
ight) &= 1 \dots 2 \,\, ext{mm} \ D\left(s
ight) &= 1 \dots 2 \,\, ext{m} \ \Delta P/P_{m 0} &pprox 1 \cdot 10^{-3} \end{aligned}$$

Remember:

$$x\left(s
ight)=x_{eta}\left(s
ight)+D\left(s
ight)rac{\Delta P}{P_{0}}$$

Beware: the dispersion contributes to the beam size:

$$\sigma_{x} = \sqrt{\sigma_{x_{\beta}}^{2} + \mathsf{std}\left(D \cdot \frac{\Delta P}{P_{0}}\right)^{2}} = \sqrt{\epsilon_{\mathsf{geometric}} \cdot \beta + D^{2} \cdot \frac{\sigma_{P}^{2}}{P_{0}^{2}}}$$

 $\sqrt{\beta}$

D

We need to suppress the dispersion at the IP !

► We need a special insertion section: a *dispersion suppressor*

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Dispersion:

$$Example: Drift \qquad M_{Drift} = \begin{pmatrix} 1 & l \\ 0 & 1 \end{pmatrix}$$
$$M_{Drift} = \begin{pmatrix} 1 & l & 0 \\ 0 & 1 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$D(s) = S(s) \int_{s0}^{s1} \frac{1}{\rho} C(\tilde{s}) d\tilde{s} - C(s) \int_{s0}^{s1} \frac{1}{\rho} S(\tilde{s}) d\tilde{s}$$
$$= 0 = 0$$

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Dispersion:

Example: Drift
$$M_{Drift} = \begin{pmatrix} 1 & l \\ 0 & 1 \end{pmatrix}$$

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 $D(s) = S(s) \int_{s0}^{s1} \frac{1}{\rho} C(\tilde{s}) d\tilde{s} - C(s) \int_{s0}^{s1} \frac{1}{\rho} S(\tilde{s}) d\tilde{s}$
 $\neq 0$
 $\neq 0$
 $\neq 0$

Example: Dispersion in a Sector Dipole Magnet

Remember: Matrix of a magnetic element

$$M_{foc} = \begin{pmatrix} \cos(\sqrt{|K|}l) & \frac{1}{\sqrt{|K|}}\sin(\sqrt{|K|}l) \\ -\sqrt{|K|}\sin(\sqrt{|K|}l) & \cos(\sqrt{|K|}l) \end{pmatrix}$$

in general: $K = k - \frac{1}{\rho^2}$

 \dots but in a dipole, as $k = 0 \dots$ the focusing properties are

$$M_{foc} = \begin{pmatrix} C & S \\ C' & S' \end{pmatrix} = \begin{pmatrix} \cos \frac{l}{\rho} & \rho \sin \frac{l}{\rho} \\ -\frac{1}{\rho} \sin \frac{l}{\rho} & \cos \frac{l}{\rho} \end{pmatrix}$$

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 $\neq 0$

calculate the "D" elements for the marix a Sector Dipole Magnet

$$D(s) = S(s) \int_{s0}^{s1} \frac{1}{\rho} C(\tilde{s}) d\tilde{s} - C(s) \int_{s0}^{s1} \frac{1}{\rho} S(\tilde{s}) d\tilde{s}$$
$$D(s) = (\rho \sin \frac{l}{\rho}) * \frac{1}{\rho} * (\rho \sin \frac{l}{\rho}) - \cos \frac{l}{\rho} * \frac{1}{\rho} * \rho \cdot (-\cos \frac{l}{\rho} + 1) * \rho$$
$$D(s) = \rho \sin^2 \frac{l}{\rho} + \rho \cos \frac{l}{\rho} * (\cos \frac{l}{\rho} - 1)$$

$$\boldsymbol{D}(\boldsymbol{s}) = \rho \cdot (1 - \cos \frac{l}{\rho})$$
, $\boldsymbol{D}'(\boldsymbol{s}) = \sin \frac{l}{\rho}$

Dispersion elements in a sector dipole magnet

$$M_{dipole} = \begin{pmatrix} \cos\frac{l}{\rho} & \rho \sin\frac{l}{\rho} & D \\ -\frac{1}{\rho} \sin\frac{l}{\rho} & \cos\frac{l}{\rho} & D' \\ 0 & 0 & 1 \end{pmatrix} \qquad \begin{pmatrix} x \\ x' \\ \frac{\lambda p}{\rho} \end{pmatrix}_{s2} = \begin{pmatrix} \cos\frac{l}{\rho} & \rho \sin\frac{l}{\rho} & \rho * (1 - \cos\frac{l}{\rho}) \\ -\frac{1}{\rho} \sin\frac{l}{\rho} & \cos\frac{l}{\rho} & \sin\frac{l}{\rho} \\ 0 & 0 & 1 \end{pmatrix} * \begin{pmatrix} x \\ x' \\ \frac{\lambda p}{\rho} \end{pmatrix}_{s1}$$

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Dispersion in a Dipole:

Nota bene: even an ideal particle with x = x' = 0 will start to oscillate if it passes a dipole magnet and has a momentum error $\Delta p/p$.

A dispersion trajectory will obey the same focusing forces (i.e. will be transferred by the same matrices) as a normal betatron oscillation.

Dipole magnets are described by a 3 x 3 matrix and carry as element m₁₃ and m₂₃ the dispersion driving expressions.

We get the full trajectory amplitude by multiplying the matrix with the vector

$$\begin{pmatrix} x \\ x' \\ \Delta p/p \end{pmatrix}_{f} = \begin{pmatrix} \cos \frac{l}{\rho} & \rho \sin \frac{l}{\rho} & D \\ -\frac{1}{\rho} \sin \frac{l}{\rho} & \cos \frac{l}{\rho} & D' \\ 0 & 0 & 1 \end{pmatrix}_{i \to f} \begin{pmatrix} x \\ x' \\ \Delta p/p \end{pmatrix}_{i}$$

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27.) Dispersion in a FoDo Cell:

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!! we have now introduced dipole magnets in the FoDo: —> we still neglect the weak focusing contribution $1/p^2$ —> but take into account 1/p for the dispersion effect assume: length of the dipole = l_D

Calculate the matrix of the FoDo half cell in thin lens approximation:in analogy to the derivations of $\hat{\beta}$, $\hat{\beta}$ ** thin lens approximation: $f = \frac{1}{k\ell_Q} >> \ell_Q$ * length of quad negligible $\ell_Q \approx 0, \rightarrow \ell_D = \frac{1}{2}L$ * start at half quadrupole $\frac{1}{\tilde{f}} = \frac{1}{2f}$

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Matrix of the half cell

$$M_{HalfCell} = M_{\underline{QD}} * M_B * M_{\underline{QF}}$$

$$M_{Half Cell} = \begin{pmatrix} 1 & 0 \\ \frac{1}{\tilde{f}} & 1 \end{pmatrix} * \begin{pmatrix} 1 & \ell \\ 0 & 1 \end{pmatrix} * \begin{pmatrix} 1 & 0 \\ \frac{-1}{\tilde{f}} & 1 \end{pmatrix}$$

$$M_{Half \ Cell} = \begin{pmatrix} C & S \\ C' & S' \end{pmatrix} = \begin{pmatrix} 1 - \frac{\ell}{\tilde{f}} & \ell \\ \frac{-\ell}{\tilde{f}^2} & 1 + \frac{\ell}{\tilde{f}} \end{pmatrix}$$

calculate the dispersion terms D, D' from the matrix elements

$$D(s) = S(s)^* \int \frac{1}{\rho(\tilde{s})} C(\tilde{s}) d\tilde{s} - C(s)^* \int \frac{1}{\rho(\tilde{s})} S(\tilde{s}) d\tilde{s}$$

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 $l_{\rm D}$





and we get the complete matrix of the half cell including the dispersion terms D, D'

$$M_{halfCell} = \begin{pmatrix} C & S & D \\ C' & S' & D' \\ 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} 1 - \frac{\ell}{\tilde{f}} & \ell & \frac{\ell^2}{2\rho} \\ \frac{-\ell}{\tilde{f}^2} & 1 + \frac{\ell}{\tilde{f}} & \frac{\ell}{\rho} (1 + \frac{\ell}{2\tilde{f}}) \\ 0 & 0 & 1 \end{pmatrix}$$

boundary conditions for the transfer from the center of the foc. to the center of the defoc. quadrupole



Test-FODD Ring for Zeuthen

typ_southen, southencel2, hfs-0 341/mm2

Optimisation of the FoDo Phase advance --Dispersion --

$$\rightarrow \overset{\vee}{D} = \hat{D}(1 - \frac{\ell}{\tilde{f}}) + \frac{\ell^2}{2\rho}$$
$$\rightarrow 0 = -\frac{\ell}{\tilde{f}^2} * \hat{D} + \frac{\ell}{\rho}(1 + \frac{\ell}{2\tilde{f}})$$

$$D_{max} = \frac{l^2}{r} \cdot \frac{1 + \frac{1}{2}sin\frac{\psi_{cell}}{2}}{sin^2 \frac{\psi_{cell}}{2}} \qquad D_{min} = \frac{l^2}{r} \cdot \frac{1 - \frac{1}{2}sin\frac{\psi_{cell}}{2}}{sin^2 \frac{\psi_{cell}}{2}}$$

where ψ_{cell} denotes the phase advance of the full cell and $1/f = sin(\frac{\psi_{cell}}{2})$



Nota bene:

! small dispersion needs strong focusing → *large phase advance*

!! \leftrightarrow *there is an optimum phase for small* β

!!! ...do you remember the stability criterion? $\frac{1}{2}$ trace = cos $\psi \leftrightarrow \psi < 180^{\circ}$

!!!! ... life is not easy

Optimisation of the FoDo Phase advance --Betafunctions --



20

18

16

14

12

10

0

30

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60

90

120

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150

180

 Ψ_{cell}

20

10

 β_{sum}

$$\beta_{max} + \beta_{min} = \frac{\left(1 + \sin\frac{\psi_{cell}}{2}\right)L}{\sin\left(\psi_{cell}\right)} + \frac{\left(1 - \sin\frac{\psi_{cell}}{2}\right)L}{\sin\left(\psi_{cell}\right)}$$

 $\beta_{max} + \beta_{min} = \frac{2L}{sin \ (\psi_{cell})}$

search for the phase advance μ that results in a minimum of the sum of the beta's

 \rightarrow require $\frac{1}{a}$

$$\frac{d}{d\psi_{cell}}\left(\frac{2L}{\sin\left(\psi_{cell}\right)}\right) = 0$$



 $\rightarrow \psi_{cell} = 90^{\circ}$

Example: Dispersion, calculated by an optics code for a real machine

$$x_{D} = D(s) * \frac{\Delta p}{p}$$

* D(s) is created by the dipole magnets ... and afterwards focused by the quadrupole fields



Dispersion is visible

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Printing) Optionen Korrekturen (Offsets Save File Select File Set Op	tics Set Bunch Spezial Orbit View E	(pert	
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HERA Standard Orbit

HERA Dispersion Orbit

dedicated energy change of the stored beam —> closed orbit is moved to a dispersions trajectory

$$x_{p} = D(s) * \frac{\Delta p}{p}$$

Attention: at the Interaction Points we require D=D'=0

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Dispersion

For one magnet element or a sequence the dispersion is part of the (3x3) matrix and the trajectory is calculated including the effect $\Delta p/p \neq 0$

$$\begin{pmatrix} x \\ x' \\ \Delta p/p \end{pmatrix}_{f} = \begin{pmatrix} \cos\frac{l}{\rho} & \rho\sin\frac{l}{\rho} & D \\ -\frac{1}{\rho}\sin\frac{l}{\rho} & \cos\frac{l}{\rho} & D' \\ 0 & 0 & 1 \end{pmatrix}_{f} \cdot \begin{pmatrix} x \\ x' \\ \Delta p/p \end{pmatrix}_{i}$$

Example: Single Dipole magnet or Transfer Line.

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Dispersion

For one magnet element or a sequence the dispersion is part of the (3x3) matrix and the trajectory is calculated including the effect $\Delta p/p \neq 0$

$$\begin{pmatrix} x \\ x' \\ \Delta p/p \end{pmatrix}_{f} = \begin{pmatrix} \cos\frac{l}{\rho} & \rho\sin\frac{l}{\rho} & D \\ -\frac{1}{\rho}\sin\frac{l}{\rho} & \cos\frac{l}{\rho} & D' \\ 0 & 0 & 1 \end{pmatrix}_{f} \cdot \begin{pmatrix} x \\ x' \\ \Delta p/p \end{pmatrix}_{i}$$

Example: Single Dipole magnet or Transfer Line.

For one full turn - or a periodic part of it - we have to require periodicity conditions for the closed orbit as well as for the "periodic" dispersion η , η' .

$$\begin{pmatrix} D \\ D' \\ 1 \end{pmatrix}_{periodic} \equiv \begin{pmatrix} \eta \\ \eta' \\ 1 \end{pmatrix} := \begin{pmatrix} C & S & D \\ C' & S' & D' \\ 0 & 0 & 1 \end{pmatrix}_{turn} \cdot \begin{pmatrix} \eta \\ \eta' \\ 1 \end{pmatrix}$$

The periodic dispersion $D_{periodic} \equiv \eta$ defines the closed orbit for particles with $\Delta p/p \neq 0$. Around this new closed orbit the trajectories perform the good old betatron oscillations.

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28.) Momentum Compaction Factor:

The dispersion function relates the momentum error of a particle to the horizontal orbit coordinate.

inhomogeneous differential equation

$$x'' + K(s) * x = \frac{1}{\rho} \frac{\Delta p}{p}$$

general solution

$$x(s) = x_{\beta}(s) + D(s)\frac{\Delta p}{p}$$



But it does much more: it changes the length of the off - energy - orbit !!

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Momentum Compaction Factor:

particle with a displacement x to the design orbit has different path length dl ...

$$\frac{dl}{ds} = \frac{\rho + x}{\rho}$$
$$\rightarrow dl = \left(1 + \frac{x}{\rho(s)}\right) ds$$



circumference of an off-energy closed orbit

$$l_{\Delta E} = \oint dl = \oint \left(1 + \frac{x_{\Delta E}}{\rho(s)}\right) ds$$

remember:
$$x_{\Delta E}(s) = D(s) \frac{\Delta p}{p_0}$$

$$\delta l = l_{\Delta E} - l_0 = \frac{\Delta p}{p_0} \oint \left(\frac{D(s)}{\rho(s)}\right) ds$$

* The lengthening of the orbit for off-momentum particles is given by the dispersion function and the bending radius.

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Momentum Compaction Factor:

Definition:

$$\frac{\delta l}{L_0} = \alpha_p \frac{\Delta p}{p_0}$$

$$\Rightarrow \alpha_{p} = \frac{1}{L_{0}} \oint \left(\frac{D(s)}{\rho(s)} \right) ds$$

For first estimates assume: $\frac{1}{\rho} = const$

$$\int_{dipoles} D(s) \, ds = \sum \left(l_{dipoles} \right)^* \left\langle D \right\rangle_{dipoles}$$

$$\alpha_p = \frac{1}{L_0} \Sigma(l_{dipoles}) < D > \frac{1}{\rho} = \frac{1}{L_0} 2\pi\rho < D > \frac{1}{\rho} \longrightarrow \qquad \alpha_p \approx \frac{2\pi}{L_0} \langle D \rangle \approx \frac{\langle D \rangle}{R}$$

Assume: $v \approx c$

$$\Rightarrow \frac{\delta T}{T_0} = \frac{\delta l}{L_0} = \alpha_p \frac{\Delta p}{p_0}$$

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 α_p combines via the dispersion function the momentum spread with the longitudinal motion of the particle.

Introduction to Transverse Beam Optics **29.)** Errors in Field and Gradient



 $\sqrt{\beta}$

DISPERSION X/Z



Errors in Field and Gradient - life is not so easy -

The derivation of the equation of motion is based on the presumption that

... in our accelerator there are only linear magnetic fields

$$\frac{B(x)}{p/e} = \frac{1}{\rho} + k^* x + \frac{1}{2!}mx^2 + \frac{1}{3!}nx^3 + \dots$$

dipole quadrupole



linear magnet structure of LEAR (CERN)



Multipole expansion of magnetic field:

$$B_{\theta}(r,\theta) = B_{main} \cdot \sum_{n=1}^{\infty} \left(\frac{r}{r_0}\right)^{n-1} \left[b_n \cos(n\theta) + a_n \sin(n\theta)\right]$$

example: mid plane $\longrightarrow \theta = 0$, radius = ref radius r_0

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$$b_n = \frac{B_{multipole}}{B_{main}}$$

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Example: HERA multipole coefficients of sc. dipole magnets



30.) Sources of field errors

1.) power supply errors:

dipole error: remember from lecture N° 1:

$$B = \frac{\mu_0 (n I)}{h}$$

2.) error in dipole strength: the gap

$$B = \frac{\mu_0 n I}{h}$$

Yoke production: laminations, made by stamping out of steel sheet. variations of gap "h" by wear out of die or use of multiple dies

Tolerance:



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Sources of field errors

power supply stability:

16 bit digital electronic for current control and stabilisation



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Dipole Magnet errors: closed orbit distortion

The sum of all dipole magnets in a ring defines a curve that we call closed orbit. perfect situation \leftrightarrow design orbit

normalised effect on the beam:

$$\int \frac{Bdl}{B\rho} = \frac{L_0}{\rho} = \alpha = 2\pi$$

effect of single dipole magnet error:

$$\int \frac{(Bds)}{B\rho} = \int \frac{1}{\rho} ds$$

A dipole error will cause a distortion of the closed orbit, that will "run around" the storage ring, being observable everywhere ... but – if small enough – still will lead to a closed orbit !!

Assume one single dipole error in a linac,

$$\begin{pmatrix} \mathbf{x} \\ \mathbf{x}' \end{pmatrix}_{s} = M_{lattice} * \begin{pmatrix} 0 \\ \Delta \mathbf{x}' \end{pmatrix}_{s0}$$



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Overall amplitude of a single particle trajectory: $x = x_{co}(s) + x_{\beta}(s) + x_{D}(s)$ B. J. Holzer, CERN JUAS 2025, Transverse Beam Dynamics 4

Calculation of Orbit Distortion in a circular machine: dipole kick $1/\rho^*\Delta s$ X_{co}

periodicity condition still has to be fulfilled: we still get (!) a closed orbit

in any case: distorted orbit will be a betatron oscillation.

 $x_{d}(s) = a\sqrt{\beta(s)} * \cos(\psi(s) - \varphi)$ $a = orbit amplitude, \varphi = initial phase$

()

put starting conditions:

$$s=0$$
, $\psi(s)=0$

boundary condition (1):

boundary condition (2):

$$s=0$$
, $\psi(s)=0$

$$x_d(s+L) = x_d(s)$$

$$x'_d(s+L) + \frac{\Delta s}{\rho} = x'_d(s)$$

periodic closed orbit at the place of the distortion, $(s=0, \psi=0)$

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Closed Orbit Distortion

Calculation of Orbit Distortion in a circular machine:



periodicity condition still has to be fulfilled: we still get (!) a closed orbit

in any case: distorted orbit will be a betatron oscillation.

 $x_d(s) = a\sqrt{\beta(s)} * \cos(\psi(s) - \varphi)$ $a = orbit amplitude, \varphi = initial phase$

boundary condition (1): $x_d(s+L) = x_d(s)$ periodic closed orbit

$$a\sqrt{\beta(s+L)} * \cos(\psi(s) + 2\pi Q - \varphi) = a\sqrt{\beta(s)} * \cos(\psi(s) - \varphi)$$

 $\cos(2\pi Q - \varphi) = \cos(-\varphi) = \cos(\varphi)$

 $\varphi = \pi Q$

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Calculation of Orbit Distortion:

angle x':

$$x_d(s) = a\sqrt{\beta(s)} * \cos(\psi(s) - \varphi)$$

$$x'_{d}(s) = -a\sqrt{\beta} * \sin(\psi(s) - \varphi) * \psi'(s) + \frac{\beta'}{2\sqrt{\beta}} a * \cos(\psi(s) - \varphi)$$

remember: $\psi'(s) = \frac{1}{\beta}$ $x'_{d}(s) = \frac{-a}{\sqrt{\beta}} \sin(\psi(s) - \varphi) + \frac{\beta'}{2\sqrt{\beta}} a * \cos(\psi(s) - \varphi)$

boundary condition (2): $x'_d(s+L) + \frac{\Delta s}{\rho} = x'_d(s)$

at the place of the distortion, s = 0, $\psi = 0$

$$\frac{-a}{\sqrt{\beta(s+L)}}\sin(2\pi Q-\varphi) + \frac{\beta'(s+L)}{2\sqrt{\beta(s+L)}}a *\cos(2\pi Q-\varphi) + \frac{\Delta s}{\rho} = \\ = \frac{-a}{\sqrt{\beta(s)}}\sin(-\varphi) + \frac{\beta'(s)}{2\sqrt{\beta(s)}}a *\cos(-\varphi)$$

periodicity: $\beta(s) = \beta(s+L), \quad \varphi = \pi Q$

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$$\frac{-a}{\sqrt{\beta}}\sin(\pi Q) + \frac{\beta'}{2\sqrt{\beta}}a \cos(\pi Q) + \frac{\Delta s}{\rho} = \frac{-a}{\sqrt{\beta}}\sin(-\pi Q) + \frac{\beta'}{2\sqrt{\beta}}a \cos(-\pi Q)$$

remember: $\sin(-x) = -\sin(x)$, $\cos(-x) = \cos(x)$

$$\frac{-a}{\sqrt{\beta}}\sin(\pi Q) + \frac{\beta'}{2\sqrt{\beta}}a \cos(\pi Q) + \frac{\Delta s}{\rho} = \frac{a}{\sqrt{\beta}}\sin(\pi Q) + \frac{\beta'}{2\sqrt{\beta}}a \cos(\pi Q)$$



put into orbit equation:

$$x_d(s) = a\sqrt{\beta(s)} * \cos(\psi(s) - \pi Q) = \frac{\delta_1 * \sqrt{\beta(s)\beta_1}}{2\sin(\pi Q)} * \cos(\psi(s) - \pi Q)$$

where $\delta = \Delta s$ denotes the orbit kick

$$x_{co}(s) = \frac{\sqrt{\beta(s)} * \int \frac{1}{\rho_{s1}} \sqrt{\beta_{s1}} * \cos(|\psi_{s1} - \psi_s| - \pi Q) ds}{2\sin \pi Q}$$

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Nota bene:

* orbit distortion is visible at any position "s" in the ring, ... even if the dipole error is located at one single point "s1".

* the β function describes the sensitivity of the beam to external fields

* the β function acts as amplification factor for the orbit amplitude at the given observation point

* in any case we (clearly ...) will obtain a cosine-like orbit travelling around the ring ... but being closed !!! after one turn.

* there is a resonance denominator

$$x_{co}(s) = \frac{\sqrt{\beta(s)} * \int \frac{1}{\rho_{s1}} \sqrt{\beta_{s1}} * \cos(|\psi_{s1} - \psi_s| - \pi Q) ds}{2\sin\pi Q}$$



Example: ,, bad orbit", i.e. closed orbit that contains large oscillation amplitudes

 \rightarrow eats up available magnet aperture

 $x(s) = x_{\beta}(s) + x_D(s) + x_{co}(s)$

—> particle trajectories pass nonlinear field regions
—> detector components suffer from beam halo particles & light



30.) Finally: Resonances

closed orbit distortion:

$$\kappa_{co}(s) = \frac{\sqrt{\beta(s)} * \int \frac{1}{\rho_{s1}} \sqrt{\beta_{s1}} * \cos(|\psi_{s1} - \psi_s| - \pi Q) ds}{2\sin \pi Q}$$

remember from lecture 1:

 $\mu = phase advance per revolution$ in general measured and expressed in units of 2π ... and called "Tune" Q

 $Q = \frac{\mu}{2\pi}$

... and it depends on the focusing strength of the lattice cells.

Tune: number of oscillations per turn

31.292 32.297

Relevant for beam stability: non integer part

HERA revolution frequency: 47.3 kHz $0.292 * 47.3 \ kHz = 13.81 \ kHz$

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permanent tune measurement ... and control





Integer tunes lead to a resonant increase of the closed orbit amplitude in presence of the smallest dipole field error.

Qualitatively spoken:



Tune & Resonances

The particles – oscillating under the influence of the external magnetic fields – can be excited to infinite high amplitudes in case of resonant tunes—> particle loss within a short number of turns.

—> avoid large magnet errors —> avoid forbidden tune values in both planes

$$m * Q_x + n * Q_y = p$$
 $n,m,p = integer numbers$



31.) Quadrupole Errors:



go back to Lecture I, page 1 single particle trajectory

Solution of equation of motion

$$\boldsymbol{x} = \boldsymbol{x}_0 * \cos(\sqrt{k*l}) + \boldsymbol{x}_0' * \frac{1}{\sqrt{k}} \sin(\sqrt{k*l})$$

$$\begin{pmatrix} \mathbf{x} \\ \mathbf{x}' \end{pmatrix}_2 = \mathbf{M}_{\mathbf{Q}F} * \begin{pmatrix} \mathbf{x} \\ \mathbf{x}' \end{pmatrix}_1 \qquad \qquad M_{\mathbf{Q}F} = \begin{pmatrix} \cos(\sqrt{k} * l) & \frac{1}{\sqrt{k}} \sin(\sqrt{k} * l) \\ -\sqrt{k} \sin(\sqrt{k} * l) & \cos(\sqrt{k} * l) \end{pmatrix}$$

Definition: phase advance of the particle oscillation per revolution in units of 2π is called tune $Q = \frac{\Delta \psi_{turn}}{2\pi} = \frac{\mu}{2\pi}$

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Quadrupole Error in the Lattice

optics perturbation described by thin lens quadrupole

$$M(s) = \begin{pmatrix} \cos\psi_{turn} + \alpha_s \sin\psi_{turn} & \beta_s \sin\psi_{turn} \\ -\gamma_s \sin\psi_s & \cos\psi_{turn} - \alpha_s \sin\psi_{turn} \end{pmatrix}$$

$$M_{dist} = M_{\Delta k} \cdot M_0 = \begin{pmatrix} 1 & 0 \\ -\Delta k ds & 1 \end{pmatrix} \cdot \begin{pmatrix} \cos\psi_{turn} + \alpha \sin\psi_{turn} & \beta \sin\psi_{turn} \\ -\gamma \sin\psi_{turn} & \cos\psi_{turn} - \alpha \sin\psi_{turn} \end{pmatrix}$$

$$ideal \ storage$$

 $M_{dist} = \begin{pmatrix} cos\psi_0 + \alpha \cdot sin\psi_0 & \beta \cdot sin\psi_0 \\ -\Delta kds \cdot (cos\psi_0 + \alpha sin\psi_0) - \gamma \cdot sin\psi_0 & -\Delta kds \cdot \beta sin\psi_0 + cos\psi_0 - \alpha sin\psi_0 \end{pmatrix}$

rule for getting the tune

$$Trace(M) = 2cos\psi = 2cos\psi_0 - \Delta k ds\beta \sin\psi_0$$

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Quadrupole error —> Tune Shift $\psi = \psi_0 + \Delta \psi \longrightarrow cos\psi = cos(\psi_0 + \Delta \psi) = cos\psi_0 - \frac{\Delta k \ ds \ \beta \sin \psi_0}{2}$

remember the old fashioned trigonometric stuff and assume that the error is small !!!

$$\cos\psi_{0} \cdot \cos\Delta\psi) - \sin\psi_{0} \cdot \sin\Delta\psi) = \cos\psi_{0} - \frac{\Delta k ds\beta \sin\psi_{0}}{2}$$
$$\approx 1 \qquad \approx \Delta\psi$$
$$\Delta\psi = \frac{k ds\beta}{2}$$

and referring to Q instead of ψ :

$$\psi = 2\pi Q$$

$$\Delta Q = \int_{s_0}^{s_0+l} \frac{\Delta k(s)\beta(s)ds}{4\pi}$$

- *the tune shift is proportional to the β-function at the quadrupole*
- *field quality, power supply tolerances etc are much tighter at places where β is large*
- *!!!* mini beta quads: $\beta \approx 1900$ m arc quads: $\beta \approx 80$ m
- *!!!!* β is a measure for the sensitivity of the beam

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Example: deliberate change of quadrupole strength in a synchrotron:

$$\Delta \boldsymbol{Q} \approx \int_{s_0}^{s_0+l} \frac{\Delta \boldsymbol{K}(s)\,\beta(s)}{4\pi} ds \approx \frac{\Delta \boldsymbol{K}(s)^* \boldsymbol{l}_{quad}^* \beta}{4\pi}$$



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tupenshift as an function gradient change 41

Clearly there is another problem: *a focussing error at any location in the machine* ... will shift the tune ... and distort the optics ... at any place in the ring



Example GA quadrupole: burned quadrupole coil

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Quadrupole error —> Beta Beat

$$\Delta\beta(s_0) = -\frac{\beta_0}{2\sin 2\pi Q} \int_{s_1}^{s_1+l} \beta(s_1) \Delta k \cos(2(\psi_{s_1} - \psi_{s_0}) - 2\pi Q) ds$$



Example LHC:

Many small quadrupole errors (gradient tolerances) add up

Tolerance limit: $\frac{\Delta\beta}{\beta} < 20\%$

Quadrupole error —> Beta Beat

A series of quadrupole errors Δk_i cause distortion of the β -function at s,

$$\frac{\Delta\beta}{\beta}(s) = \frac{1}{2\sin 2\pi Q} \sum_{i} \beta_i \Delta k_i \cos\left(2\pi Q - 2(\mu_i - \mu_s)\right) \tag{132}$$



32.) Chromaticity: A Quadrupole Error for $\Delta p/p \neq 0$

Influence of external fields on the beam: prop. to magn. field & prop. zu 1/p

Chromaticity: Q' (... sometimes aka ... " ξ ")

$$k = \frac{g}{p/e} \qquad p = p_0 + \Delta p$$

in case of a momentum spread:

$$k = \frac{eg}{p_0 + \Delta p} \approx \frac{e}{p_0} \left(1 - \frac{\Delta p}{p_0}\right) g = k_0 + \Delta k$$

$$\Delta k = -\frac{\Delta p}{p_0} k_0$$

... which acts like a quadrupole error in the machine and leads to a tune spread:

$$\Delta Q = -\frac{1}{4\pi} \frac{\Delta p}{p_0} k_0 \beta(s) ds$$

definition of chromaticity:

$$\Delta Q = Q' \quad \frac{\Delta p}{p} ; \qquad Q' = -\frac{1}{4\pi} \oint k(s)\beta(s)ds$$

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Where is the Problem ?

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... what is wrong about Chromaticity:

Problem: chromaticity is generated by the lattice itself !!

Q' is a number indicating the size of the tune spot in the working diagram,
Q' is always created if the beam is focussed
—> it is determined by the focusing strength k of all quadrupoles

$$Q' = -\frac{1}{4\pi} \oint k(s)\beta(s)ds$$

k = quadrupole strength $\beta = beta function indicates the beam size ... and even more the sensitivity of the beam to external fields$

Example: LHC

Q' = 250 $\Delta p/p = +/- 0.2 * 10^{-3}$ $\Delta Q = 0.256 \dots 0.36$ →Some particles get very close to resonances and are lost

in other words: the tune is not a point it is a pancake

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Betatron Tune: Qx, Qy

Effect of Chromaticity

Tune signal for a nearly uncompensated cromaticity $(Q' \approx 20)$

Ideal situation: cromaticity well corrected, $(Q' \approx 1)$

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Once more: Tune and Resonances

 $m^{*}Q_{x}+n^{*}Q_{y}+l^{*}Q_{s} = integer$

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HERA e Tune diagram up to 3rd order

... and up to 7th order

Homework for the operateurs: find a nice place for the tune where against all probability the beam will survive

Correction of Q':

Need: additional quadrupole strength for each momentum deviation $\Delta p/p$

Sextupoles, through a non-linear magnetic field, correct the effect of energy spread and focuses particles at a single location.

- ► Located in dispersive regions.
- ► Usually in arcs.
- ► Sextupole families.

Now is when the party starts

- Sextupoles introduce non-linear fields.
- ▶ ...i.e. they induce non-linear motion.
- resonances, tune shifts, chaotic motion.

Correction of Q':

Need: additional quadrupole strength for each momentum deviation $\Delta p/p$

1.) sort the particles acording to their momentum

... using the dispersion function

2.) apply a magnetic field that rises quadratically with x (sextupole field)

$$B_{x} = \tilde{g}xz$$

$$B_{z} = \frac{1}{2}\tilde{g}(x^{2} - z^{2})$$

$$\frac{\partial B_{x}}{\partial z} = \frac{\partial B_{z}}{\partial x} = \tilde{g}x$$
linear rising "gradient":

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Correction of Q':

Sextupole Magnets:

 k_1 quadrupole strength being off-centre in a sextupole

$$k_1 = \frac{\tilde{g}}{p/e} \cdot x = k_2 \cdot x = k_2 \cdot D \cdot \frac{\Delta p}{p}$$

corrected chromaticity

counter acting effect in the two planes

$$Q'_{x} = \frac{1}{4\pi} \cdot \left\{ -\oint \beta_{x}(s) \cdot |k_{q}(s)| \, ds + |k_{2}^{F}| \cdot l_{sext} \cdot \beta_{x}(s) \cdot D_{x_{sext}} - |k_{2}^{D}| \cdot l_{sext} \cdot \beta_{x}(s) \cdot D_{x_{sext}} \right\}$$
$$Q'_{y} = \frac{1}{4\pi} \cdot \left\{ -\oint \beta_{y}(s) \cdot |k_{q}(s)| \, ds - |k_{2}^{F}| \cdot l_{sext} \cdot \beta_{y}(s) \cdot D_{x_{sext}} + |k_{2}^{D}| \cdot l_{sext} \cdot \beta_{y}(s) \cdot D_{x_{sext}} \right\}$$

"natural" chromaticity

sextupole correction of chromaticity

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Resume':

quadrupole error: tune shift

$$\Delta Q \approx \int_{s0}^{s0+l} \frac{\Delta k(s)\,\beta(s)}{4\pi} ds \approx \frac{\Delta k(s)^* l_{quad}^* \overline{\beta}}{4\pi}$$

beta beat
$$\Delta\beta(s_0) = \frac{\beta_0}{2\sin 2s}$$

$$\Delta\beta(s_0) = \frac{\beta_0}{2\sin 2\pi Q} \int_{s_1}^{s_{1+l}} \beta(s_1) \Delta k \cos(2(\psi_{s_1} - \psi_{s_0}) - 2\pi Q) ds$$

chromaticity
$$\Delta Q = Q' * \frac{\Delta p}{p}$$

$$Q' = -\frac{1}{4\pi} \oint k(s)\beta(s)ds$$

in a FoDo
$$Q'_{cell} = -\frac{1}{\pi} \tan \frac{\mu}{2}$$

corrected chromaticty

$$Q'_{x} = \frac{-1}{4\pi} * \oint k_{1}(s)\beta(s) \, ds + \frac{1}{4\pi} \sum_{F \, sext} k_{2}^{F} l_{sext} \, D_{x}^{F} \beta_{x}^{F} - \frac{1}{4\pi} \sum_{D \, sext} k_{2}^{D} l_{sext} \, D_{x}^{D} \beta_{x}^{D}$$

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Appendix 1: Quadrupole Errors and Beta Function

a quadrupole error will not only influence the oscillation frequency ... "tune" ... but also the amplitude ... "beta function"

$$M_{turn} = B * A$$
 $A = \begin{pmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{pmatrix}$

$$B = \begin{pmatrix} b_{11} & b_{12} \\ b_{21} & b_{22} \end{pmatrix}$$

distorted matrix
$$M_{dist} = \begin{pmatrix} m_{11}^* & m_{12}^* \\ m_{21}^* & m_{22}^* \end{pmatrix} = B \begin{pmatrix} 1 & 0 \\ -\Delta k ds & 1 \end{pmatrix} A$$

$$M_{dist} = B \begin{pmatrix} a_{11} & a_{12} \\ -\Delta k ds a_{11} + a_{12} & -\Delta k ds a_{12} + a_{22} \end{pmatrix}$$

$$M_{dist} = \begin{pmatrix} \sim & b_{11}a_{12} + b_{12}(-\Delta k ds a_{12} + a_{22}) \\ \sim & \sim \end{pmatrix}$$

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the beta function is usually obtained via the matrix element "m12", which is in Twiss form for the undistorted case

$$m_{12} = \beta_0 \sin 2\pi Q$$

and including the error:

$$m_{12}^{*} = b_{11}a_{12} + b_{12}a_{22} - b_{12}a_{12}\Delta kds$$

$$m_{12} = \beta_{0}\sin 2\pi Q$$
(1) $m_{12}^{*} = \beta_{0}\sin 2\pi Q - a_{12}b_{12}\Delta kds$

As M^* is still a matrix for one complete turn we still can express the element m_{12} in twiss form: (2) $m_{12}^* = (\beta_0 + d\beta)^* \sin 2\pi (Q + dQ)$

Equalising (1) and (2) and assuming a small error

$$\beta_0 \sin 2\pi Q - a_{12} b_{12} \Delta k ds = (\beta_0 + d\beta)^* \sin 2\pi (Q + dQ)$$

 $\beta_0 \sin 2\pi Q - a_{12} b_{12} \Delta k ds = (\beta_0 + d\beta) * \sin 2\pi Q \cos 2\pi dQ + \cos 2\pi Q \sin 2\pi dQ$ $\approx 1 \qquad \approx 2\pi dQ$

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$$\beta_0 \sin 2\pi Q - a_{12} b_{12} \Delta k ds = \beta_0 \sin 2\pi Q + \beta_0 2\pi dQ \cos 2\pi Q + d\beta_0 \sin 2\pi Q + d\beta_0 2\pi dQ \cos 2\pi Q$$

ignoring second order terms

$$-a_{12}b_{12}\Delta kds = \beta_0 2\pi dQ \cos 2\pi Q + d\beta_0 \sin 2\pi Q$$

remember: tune shift dQ due to quadrupole error: (index "1" refers to location of the error)

$$dQ = \frac{\Delta k \beta_1 ds}{4\pi}$$

$$-a_{12}b_{12}\Delta kds = \frac{\beta_0\Delta k\beta_1ds}{2}\cos 2\pi Q + d\beta_0\sin 2\pi Q$$

solve for db

$$d\beta_{0} = \frac{-1}{2\sin 2\pi Q} \{ 2a_{12}b_{12} + \beta_{0}\beta_{1}\cos 2\pi Q \} \Delta k ds$$

express the matrix elements a_{12} , b_{12} in Twiss form

$$M = \begin{pmatrix} \sqrt{\frac{\beta_s}{\beta_0}} \left(\cos\psi_s + \alpha_0 \sin\psi_s \right) & \sqrt{\beta_s \beta_0} \sin\psi_s \\ \frac{(\alpha_0 - \alpha_s) \cos\psi_s - (1 + \alpha_0 \alpha_s) \sin\psi_s}{\sqrt{\beta_s \beta_0}} & \sqrt{\frac{\beta_0}{\beta s}} \left(\cos\psi_s - \alpha_s \sin\psi_s \right) \end{pmatrix}$$

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$$d\beta_0 = \frac{-1}{2\sin 2\pi Q} \{ 2a_{12}b_{12} + \beta_0\beta_1\cos 2\pi Q \} \Delta k ds$$

$$a_{12} = \sqrt{\beta_0 \beta_1} \sin \Delta \psi_{0 \to 1}$$
$$b_{12} = \sqrt{\beta_0 \beta_1} \sin(2\pi Q - \Delta \psi_{0 \to 1})$$

$$d\beta_0 = \frac{-\beta_0\beta_1}{2\sin 2\pi Q} \left\{ 2\sin \Delta \psi_{01} \sin(2\pi Q - \Delta \psi_{01}) + \cos 2\pi Q \right\} \Delta k dk$$

... after some TLC transformations ..= $\cos(2\Delta\psi_{01} - 2\pi Q)$

$$\Delta\beta(s_0) = \frac{-\beta_0}{2\sin 2\pi Q} \int_{s_1}^{s_1+l} \beta(s_1) \Delta k \cos(2(\psi_{s_1} - \psi_{s_0}) - 2\pi Q) ds$$

Nota bene: ! the beta beat is proportional to the strength of the error Δk

!! and to the β *function at the place of the error*,

!!! and to the β function at the observation point, (... remember orbit distortion !!!)

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Appendix 2: Dispersion Solution of the inhomogenious equation of motion

Ansatz:

$$D(s) = S(s) \int_{s_0}^{s_1} \frac{1}{\rho} C(\tilde{s}) d\tilde{s} - C(s) \int_{s_0}^{s_1} \frac{1}{\rho} S(\tilde{s}) d\tilde{s}$$

$$D'(s) = S'^* \int \frac{1}{\rho} C \, dt + S \frac{1}{\rho} C - C'^* \int \frac{1}{\rho} S \, dt - C \frac{1}{\rho} S \, dt$$
$$D'(s) = S'^* \int \frac{C}{\rho} \, dt - C'^* \int \frac{S}{\rho} \, dt$$

$$D''(s) = S'' * \int \frac{C}{\rho} d\widetilde{s} + S' \frac{C}{\rho} - C'' * \int \frac{S}{\rho} d\widetilde{s} - C' \frac{S}{\rho}$$
$$= S'' * \int \frac{C}{\rho} d\widetilde{s} - C'' * \int \frac{S}{\rho} d\widetilde{s} + \frac{1}{\rho} (CS' - SC')$$
$$= \det M = 1$$

remember: for Cs) and S(s) to be independent solutions the Wronski determinant has to meet the condition 5, Transverse Beam Dynamics 4

 $W = \begin{vmatrix} C & S \\ C' & S' \end{vmatrix} \neq 0$ 60

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and as it is independent of the variable "s"

$$\frac{dW}{ds} = \frac{d}{ds}(CS' - SC') = CS'' - SC'' = -K(CS - SC) = 0$$

we get for the initial $C_0 = 1, \quad C'_0 = 0$ conditions that we had chosen ... $S_0 = 0, \quad S'_0 = 1$

$$W = \begin{vmatrix} C & S \\ C' & S' \end{vmatrix} = 1$$

$$D'' = S'' * \int \frac{C}{\rho} d\widetilde{s} - C'' * \int \frac{S}{\rho} d\widetilde{s} + \frac{1}{\rho}$$

remember: S & C are solutions of the homog. equation of motion: $\begin{aligned} S'' + K * S &= 0 \\ C'' + K * C &= 0 \end{aligned}$

$$D'' = -K * S * \int \frac{C}{\rho} d\tilde{s} + K * C * \int \frac{S}{\rho} d\tilde{s} + \frac{1}{\rho}$$

$$D'' = -K * \left\{ S \int \frac{C}{\rho} d\tilde{s} + C \int \frac{S}{\rho} d\tilde{s} \right\} + \frac{1}{\rho}$$

$$= D(s)$$

$$D'' = -K * D + \frac{1}{\rho} \qquad \dots or \qquad D'' + K * D = \frac{1}{\rho}$$

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