

# Vacuum Systems

## Slot 4

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<https://indico.cern.ch/event/1470062/timetable/?view=standard#day-2025-02-17>

# Outline

1. Hydrogen reduction
2. Other materials
3. Qualification of materials

# 1. Hydrogen reduction

# Vacuum firing

- A method to **reduce hydrogen content in stainless steel** (316 series)
- Degassing of the material is performed in an oven at 950°C under vacuum ( $<10^{-5}$  mbar) for 2 h
- The high temperature allows to enhance hydrogen diffusion



Courtesy P. Chiggiato, TE-VSC

## CERN large furnace

Length: 6 m

Diameter: 1 m

Maximum charge weight: 1000 Kg

Ultimate pressure:  $10^{-9}$  mbar

P at the end of the treatment:  
high  $10^{-6}$  mbar range

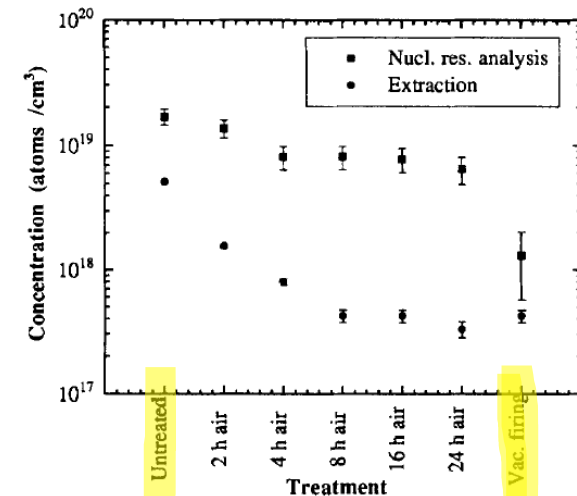
# Impact on structural properties

- Under the heat surface treatment **304 series** stainless steel are recrystallized due to carbide precipitation at the grain boundaries
  - **cannot be used as material for flanges** (leak at the level of the knife)!
  - low carbon and low carbon nitrogen alloys stainless steel are used (316LN)
- The hardness of the material is not modified
- The surface is enriched in Fe due to the Cr evaporation during the heat treatment
- When the material is brought back to atmospheric pressure, it keeps the memory of the treatment since the hydrogen diffusion at room temperature is small
  - **A single treatment** is needed for the full life of the material

**Table 1.** Deduced hydrogen concentration in the samples from the nuclear resonance analysis (NRA) and an extraction method

Treatment	Time(h)	Temperature (°C)	NRA Hydrogen conc. (At/cm <sup>-3</sup> )	Extraction Hydrogen conc. (At/cm <sup>-3</sup> )
Untreated			$1.70(25) \cdot 10^{19}$	$5.17(5) \cdot 10^{18}$
Air baked	2	400	$1.37(22) \cdot 10^{19}$	$1.56(5) \cdot 10^{18}$
Air baked	4	400	$8.2(17) \cdot 10^{18}$	$8.0(5) \cdot 10^{17}$
Air baked	8	400	$8.2(17) \cdot 10^{18}$	$4.2(5) \cdot 10^{17}$
Air baked	16	400	$7.8(17) \cdot 10^{18}$	$4.2(5) \cdot 10^{17}$
Air baked	24	400	$6.5(16) \cdot 10^{18}$	$3.3(5) \cdot 10^{17}$
Vacuum Fired	1	950	$1.3(7) \cdot 10^{18}$	$4.2(5) \cdot 10^{17}$

$c \sim 2 \cdot 10^{19} \text{ H/cm}^3$  reduced to  $10^{18} \text{ H/cm}^3$



**Figure 1.** The average hydrogen concentration in the 0.05–0.7 μm depth range of the virgin, air baked and the vacuum fired samples. The results from the extraction method are also included.

L. Westerberg *et al.*, Vacuum 48 (1997) 771-773

# Subsequent bakeouts following vacuum firing

- As in previous lecture (slide 32), considering the achieved hydrogen surface concentration following the vacuum firing, the hydrogen outgassing rate after n successive bakeout at temperature  $T_{BO}$  and duration  $t_{BO}$  is obtained from the 1<sup>st</sup> Fick Law:

$$q(t) = D \left( \frac{\partial c(x, t)}{\partial x} \right)_{x=0}$$

$$q_{n,F}(t) = \left[ c_F + (c_O - c_F) e^{-\left(\frac{\pi}{L}\right)^2 D(T_F)t_F} \right] \frac{4 D(T_{RT})}{L} e^{-n \left(\frac{\pi}{L}\right)^2 D(T_{BO})t_{BO}}$$

R. Calder, G. Lewin, Br J Appl. Phys, 18, 1967, 1459

- The diffusion terms dominates:

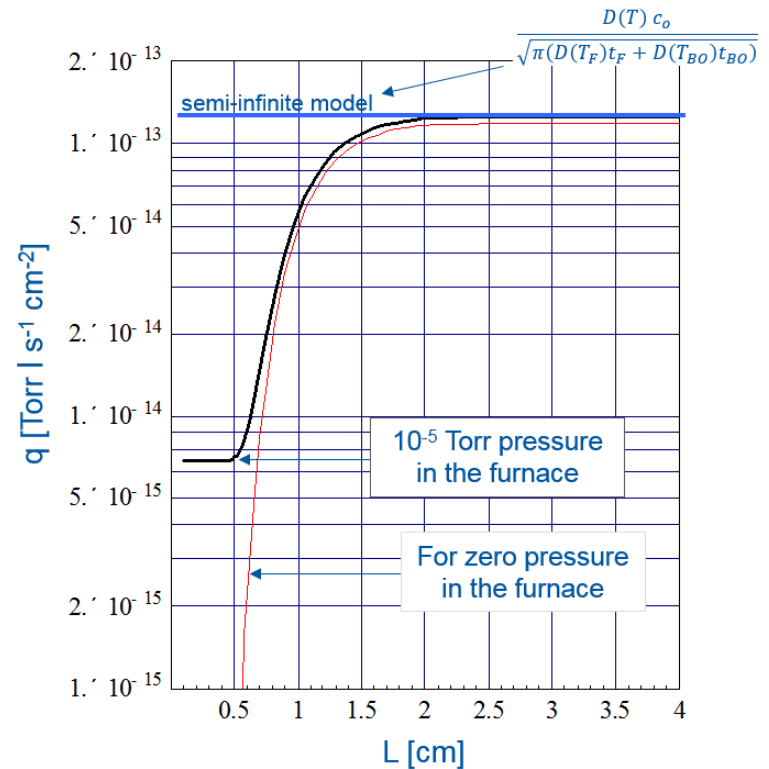
$$D(T) = D_0 e^{-E_{diff}/kT}$$

- For **thin sheets** (tubes), the initial content of the hydrogen is fully removed. The final outgassing is defined by the H<sub>2</sub> pressure in the furnace:

$$q \sim 5 \cdot 10^{-15} \text{ mbar.l/(s.cm}^2\text{)}$$

- For **thick slab** (flanges), the pressure in the furnace as limited influence:

$$q \sim 10^{-13} \text{ mbar.l/(s.cm}^2\text{)}$$



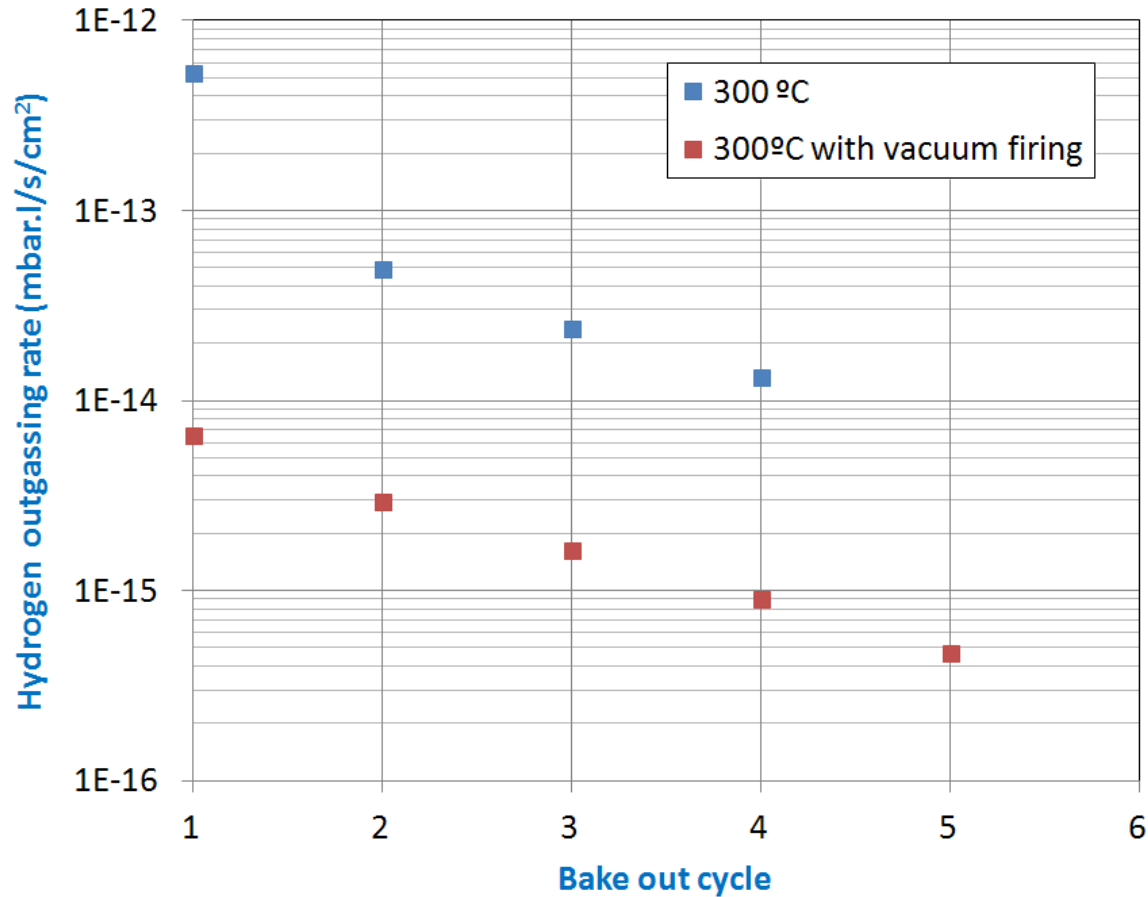
Courtesy P. Chiggiato, TE-VSC

# Stainless steel 316 LN

- 1.5 mm thick sheet held at 300°C for 24 h, rate measured 120 h after the end of bake-out
- As expected from diffusion theory:
  - H<sub>2</sub> outgassing rate of  $6 \cdot 10^{-15}$  mbar.l/(s.cm<sup>2</sup>) and a reduction of ~ 1.8 between each cycle



316 LN stainless steel hydrogen outgassing rate



B. Versolatto, N. Hilleret, CERN Vacuum Technical Note 2002



# Diffusion barrier: air baking

- The hydrogen diffusion is reduced by a **diffusion barrier** created during the air bake-out
- Stainless steel tube:
  - 8 m length, 1.2 m diameter, 2mm thick
- Air fired at 400 deg for 38h
- Then baked at 150 deg for 7 days
- Oxide thickness x 10
- $q = 10^{-15}$  mbar.l/s/cm<sup>2</sup>
- Diffusion energy increased from 0.5 to 0.6 eV
- **Low cost!**

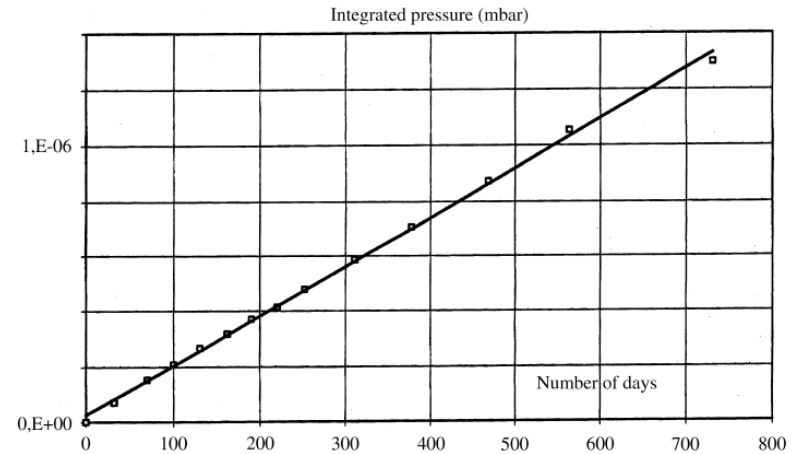
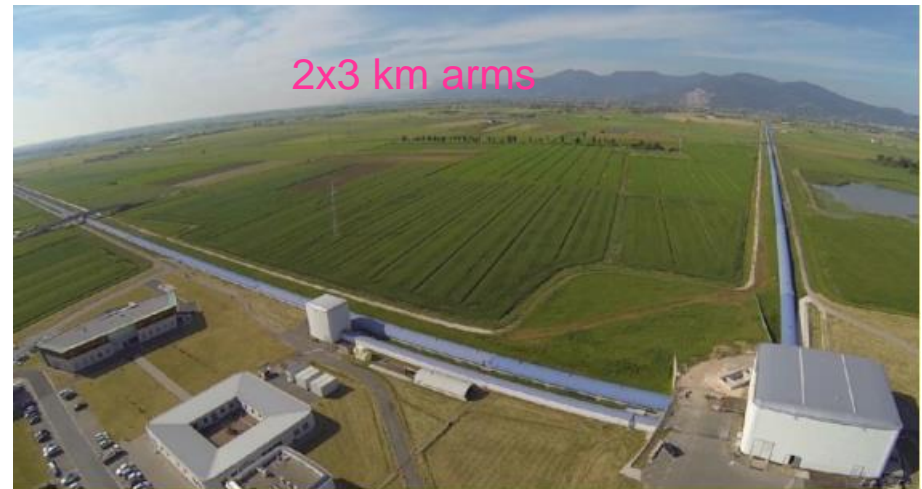


Fig. 1. Hydrogen accumulation over a long period of time in the Orsay corrugated prototype tube for VIRGO.

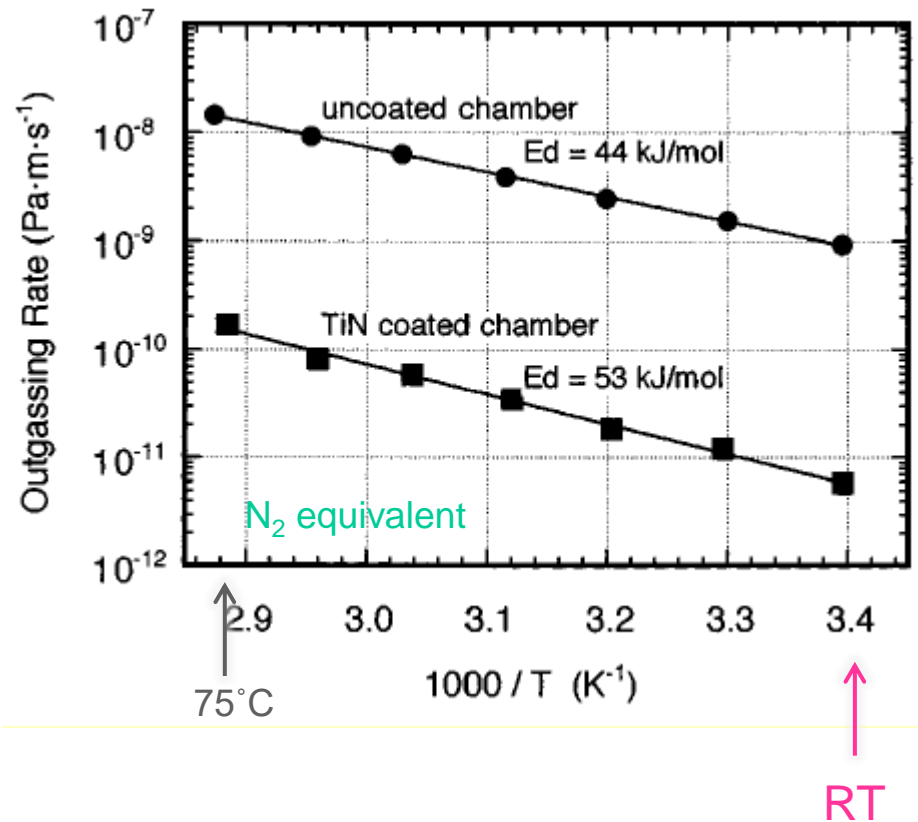
Outgassing performance of an industrial prototype tube for the Virgo antenna, P. Marin *et al.* , Vacuum 49 (1998) 309



VIRGO Gravitational Waves detector at Pisa, Italy

# Diffusion barrier: TiN coating

- The hydrogen diffusion is reduced by a diffusion barrier created by a coating e.g. TiN
- At least 1  $\mu\text{m}$  film thickness
- The film **reduce** the hydrogen **permeation**
- Extrapolation from coupons measurements predicts  $10^{-14} \text{ Pa}\cdot\text{m s}^{-1}$  ( $10^{-17} \text{ mbar}\cdot\text{l/s/cm}^2$ )
- 3D objects: **difficulties** to realise a uniform coating without pinholes which compromised the observed performance on a tube or vacuum chamber
- Reduction of 2 orders of magnitude of the hydrogen outgassing rate:
  - Uncoated chamber:  $10^{-12} \text{ mbar}\cdot\text{l/s/cm}^2$
  - TiN coated chamber:  $7 \cdot 10^{-15} \text{ mbar}\cdot\text{l/s/cm}^2$



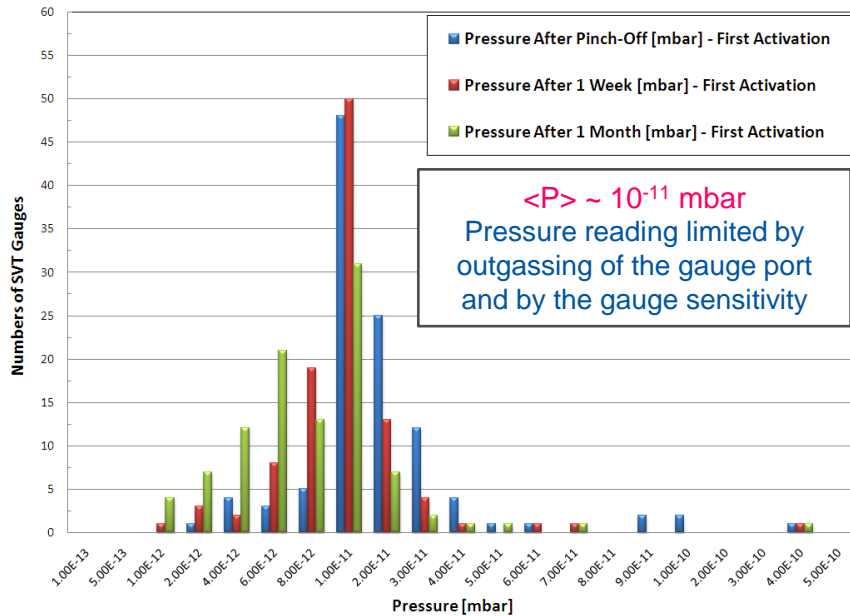
TiN thin film on stainless steel for extremely high vacuum material, K. Saito *et al.*, J. Vac. Sci. Technol. A 13(3) May/June 1995, 556

**Today: no application in accelerator yet** (some attempts for SNS ring, P. He et al., PAC 2003)

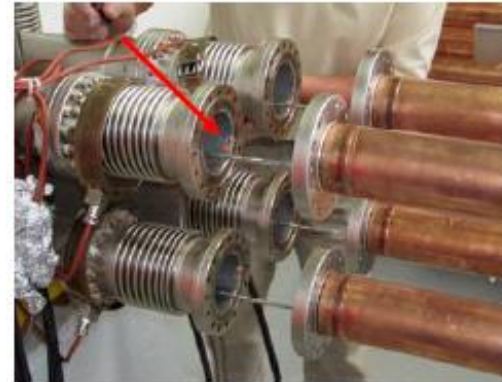
# Dissolving hydrogen: NEG (TiZrV) coating

- Ti-Zr-V is coated by **magnetron sputtering** using Kr gas
  - ~ 1  $\mu\text{m}$  thick
  - Owing to the **high solubility** and **diffusivity** of hydrogen once activated to 180-200°C, the coating provides at room temperature extremely:
    - Low outgassing rate:  $<10^{-17}$  Torr. $\cdot$ l/cm<sup>2</sup> that means  $< 300$  CH<sub>4</sub>/cm<sup>2</sup>
    - Large pumping speed: 0.3-2.2 l/s/cm<sup>2</sup> for H<sub>2</sub> and 5-9 l/s/cm<sup>2</sup> for CO
- ~ 2 000 & 15 000 l /s per m of LHC vacuum chamber for H<sub>2</sub> and CO resp. !

Pressure distribution in the LHC RT vacuum sectors



G. Bregliozzi *et al.* EPAC'08, Genoa 2008

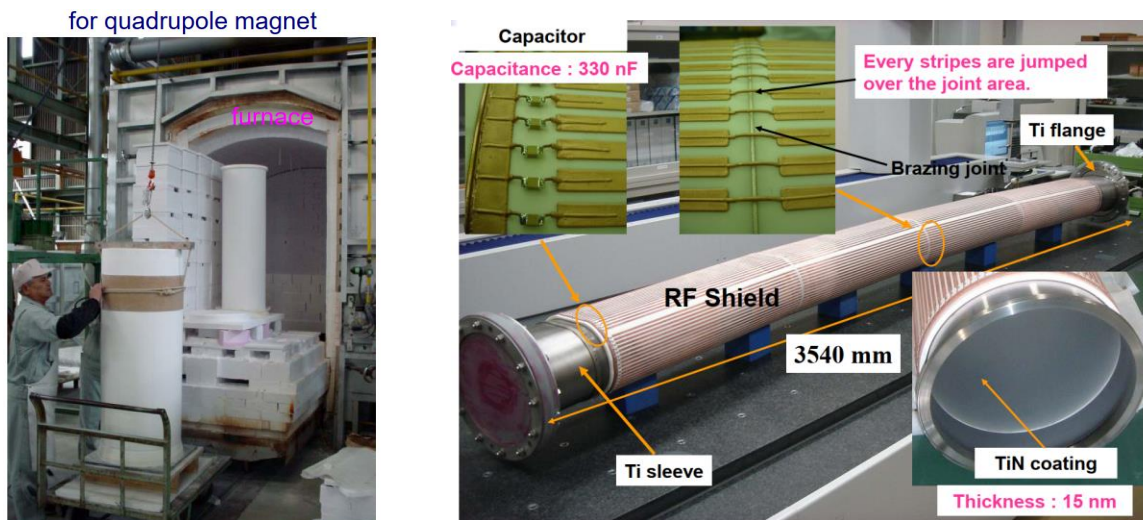


C. Benvenuti *et al.* Vacuum 60 (2001) 57-65  
 P. Costa Pinto, P. Chiggiato / Thin Solid Films 515 (2006) 382-388

## 2. Other materials

# Outgassing of ceramics

- Ceramics are used as **insulators** for feedthrough, as RF windows for their **transparency to EM fields** or to **minimise Foucault's currents** induced in the vacuum chambers of fast ramping magnets (kickers) or fast cycling accelerators.
- Outgassing rates are function of the porosity



J-Parc Vacuum chambers, M. Kinsho, Nov. 2005

- Alumina ( $\text{Al}_2\text{O}_3$ ) is sintered at high temperature ( $1600^\circ\text{C}$ ) and chemically stable
- TiN coated alumina chamber has  $q = 1 \cdot 10^{-11} \text{ mbar}\cdot\text{l/s/cm}^2$  after 50 h pumping

Y. Saito et al. Vacuum 86 (2012) 817-821

- Macor and nitrides ceramics requires in-situ bakeout at  $200^\circ\text{C}$  to reach  $\sim 10^{-11} \text{ mbar}\cdot\text{l/s/cm}^2$  at RT

K. Battes et al. J. Vac. Sci. Technol. B39, 034202 (2021)

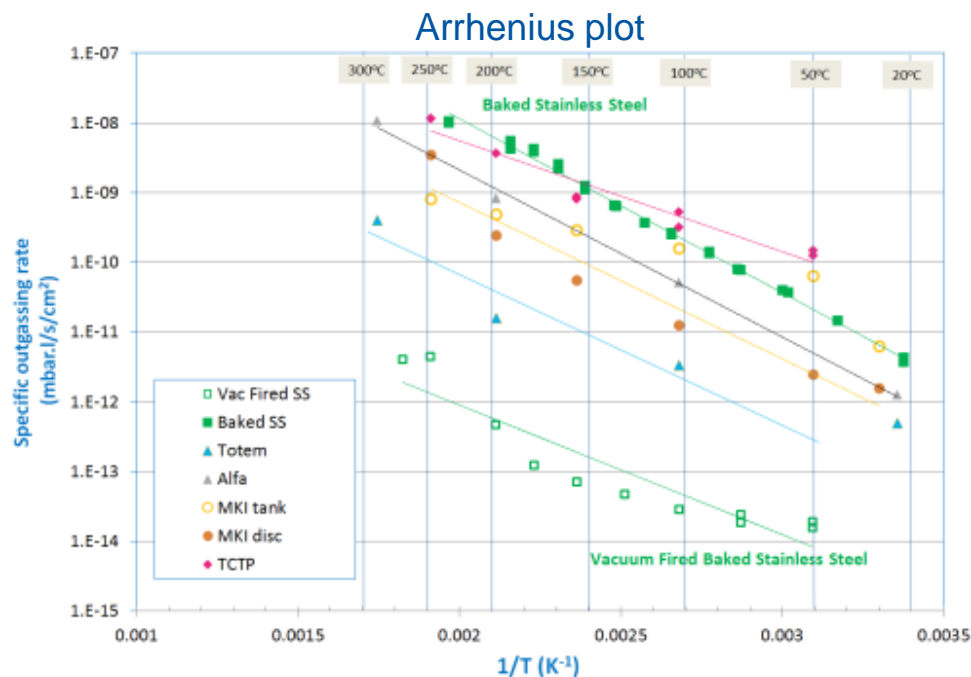


# Outgassing of ferrites

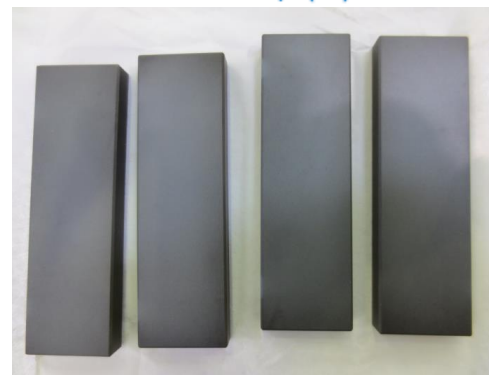
- Ferrites inserted in devices (XRP, TCSP, TCTP, MKI, TDI ...) have low outgassing rate  $10^{-11}$  mbar.l/s/cm<sup>2</sup> (after bakeout)
- TT2-111R, CMD5005 and CMD10
- Treated at 400°C – 1000°C

- But can heat up during operation => **increase** of outgassing rate

°C	50	100	150	200
$\frac{q}{q_{RT}}$	5	40	150	600



LHC Roman Pots ferrite

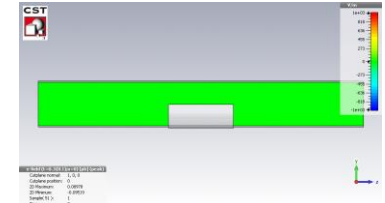


# Example TDI during RUN1 and 2

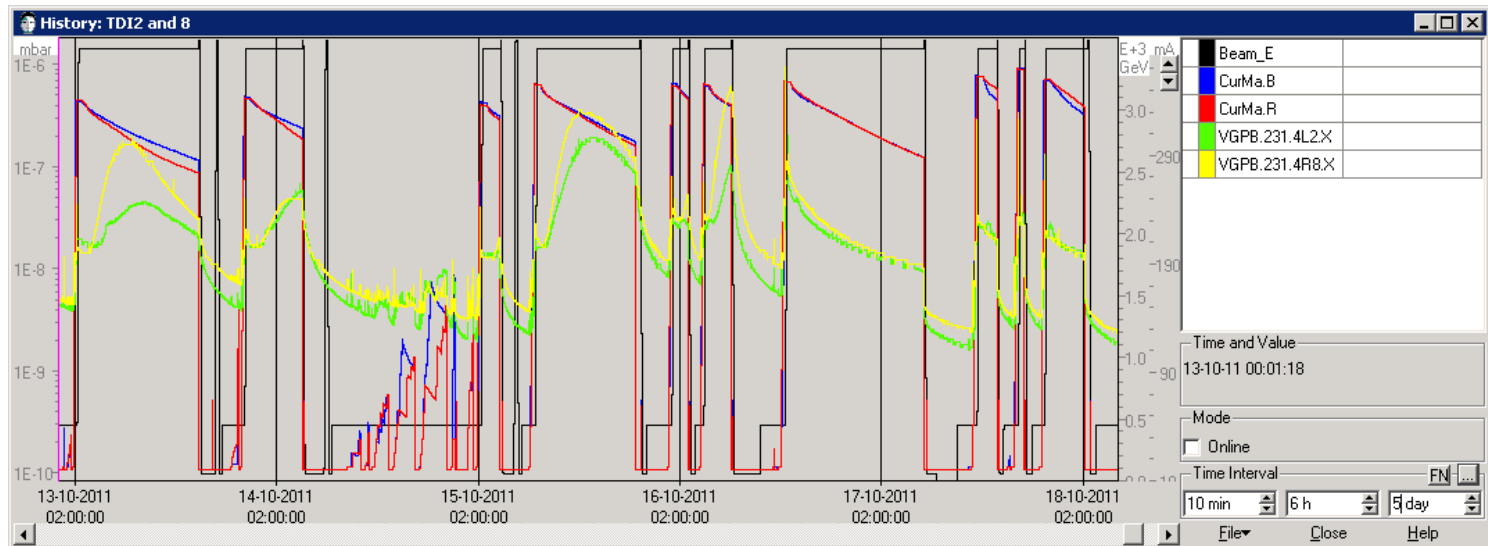
- A Target Dump for Injection device to protect downstream elements
- Circulating beams increase the temperature of the BN jaws by impedance effects
- Any beampipe component generates EM **wakefields** and may behave like a resonator or a damper

Beam induced heating

$$Q = Q_0 e^{-\frac{E}{kT}}$$



X. Buffat, CAS, 2022



B. Salvant et al. EM simulations of the impedance of the LHC TDI. Proc. of IPAC 2012, New Orleans, USA  
B. Salvant et al. Update on beam induced RF heating in the LHC. Proc. of IPAC 2013, Shanghai, China

# Outgassing of additive manufactured materials

- Recent technique, only few applications yet
- Additive manufactured stainless steel tube outgassing are as low as conventional ones.

Table 1: Outgassing Rates at 100h (T=20°C)

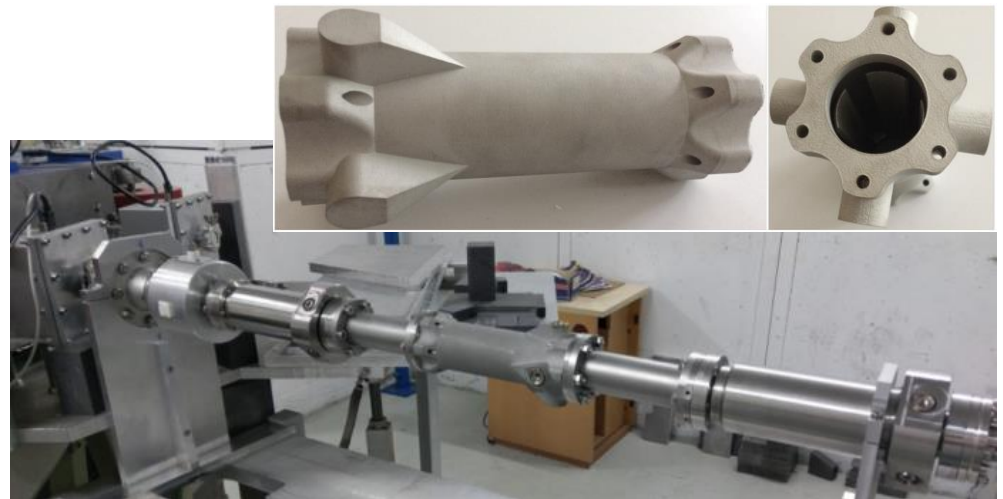
Treatment	Tube	Outgassing rate (mbar.l/s.cm <sup>2</sup> )
Unbaked	Conventional	6.0x10 <sup>-12</sup>
	Unlathed AM	5.6x10 <sup>-12</sup>
	Lathed AM	7x10 <sup>-12</sup>
Baked at 200 °C	Unlathed AM	3.6x10 <sup>-13</sup>
	Lathed AM	3.4x10 <sup>-13</sup>



G. Sattonnay et al. Proc. of IPAC 2019, Melbourne, Australia

- Construction of an AM BPM
- Test on a photo-injector show results as good as conventional BPMs

→ AM BPM became THOM-X baseline



N. Delerue et al. Proc. of IPAC 2019, Melbourne, Australia

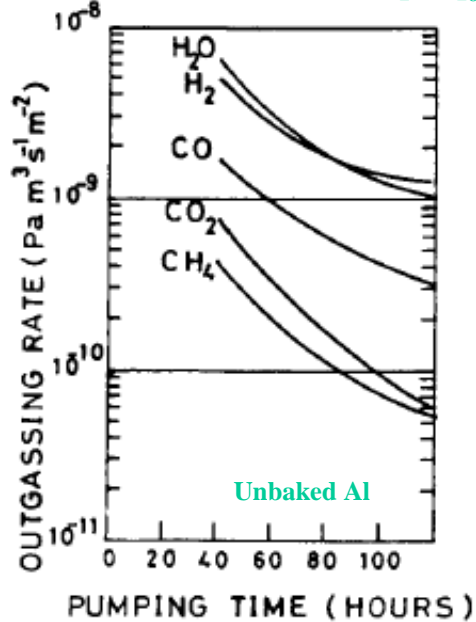


# Outgassing of polymers & elastomers

- Plastic materials are **highly porous** and contains much more water than metallic surfaces
- Their outgassing rate is limited by a **diffusion process** with  $a = 1/2$

$$q(t) = q_0 t^{-a}$$

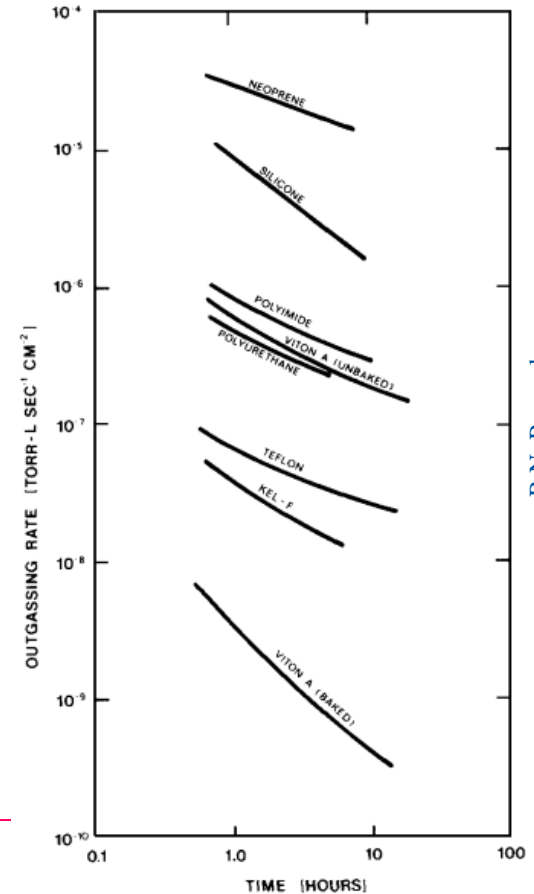
Metallic surfaces  $q \sim q_0/t$



A.G. Mathewson *et al.*  
J.Vac.Sci. 7(1), Jan/Fev 1989, 77-82

$\times 10^2 - 10^5$   
➔

Plastic surfaces  $q \sim q_0/\sqrt{t}$



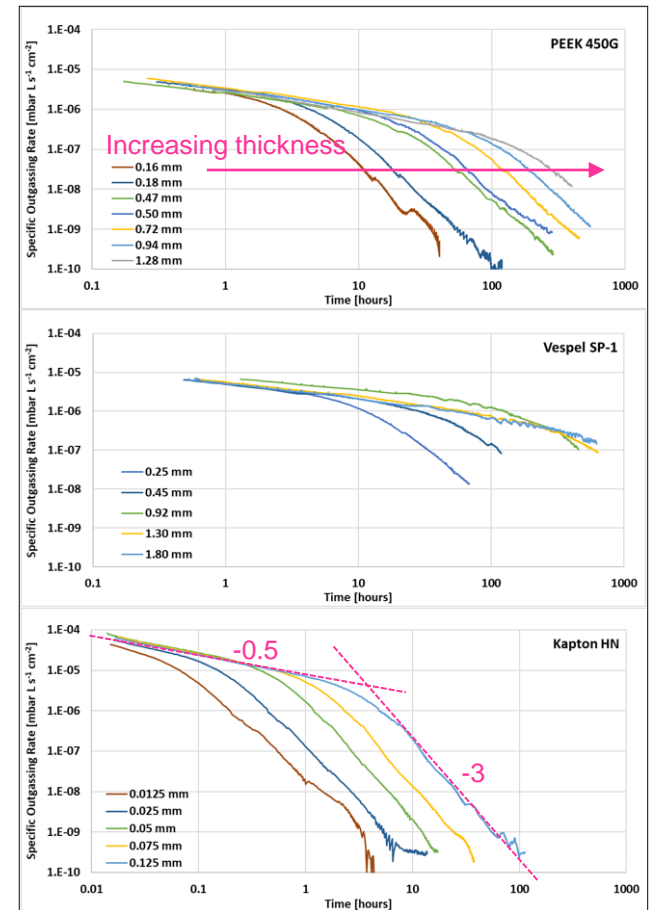
R.N. Peacock  
J.Vac.Sci. 17(1), Jan/Fev 1980, 330-336

**Good Vacuum Design :**

**Use ONLY metallic surfaces and reduce to ZERO the amount of plastics**

# Outgassing of thin polymers

- The **thicker** the material, the more moisture is embedded
- $q$  decreases from  $10^{-5}$  after 1h to  $10^{-10}$ - $10^{-7}$  after 100h
- Compared to Vespel® & Kapton®, PEEK has:
  - larger diffusion coefficient hence faster  $q$  reduction
  - lower moisture content hence lower  $q$
- Diffusion process in  $1/\sqrt{t}$  then  $1/t^3$  after extended time (>100 h)
- Polymers thicker than ~ 1 mm requires **more than 2 weeks** of pumping to reduce  $q$  significantly
- A **bake-out** to 200°C strongly reduce outgassing in the  $10^{-11}$  –  $10^{-10}$  mbar.l/s/cm<sup>2</sup> range
- **Venting** with N<sub>2</sub> or dry air preserve the bake-out benefit



S. Sammartano et al. CERN-ACC-Note-2020-0039

# Outgassing of gauges filaments

- During operation, filaments are heated to  $\sim 2\,000^\circ\text{C}$  consequently desorbing gas and provoke also Electron Stimulated Desorption (ESD)



$$Q = 2 \cdot 10^{-9} \text{ mbar}\cdot\ell/\text{s} \text{ for W filament}$$

$$= 1 \cdot 10^{-10} \text{ mbar}\cdot\ell/\text{s} \text{ for thoriated W filament}$$



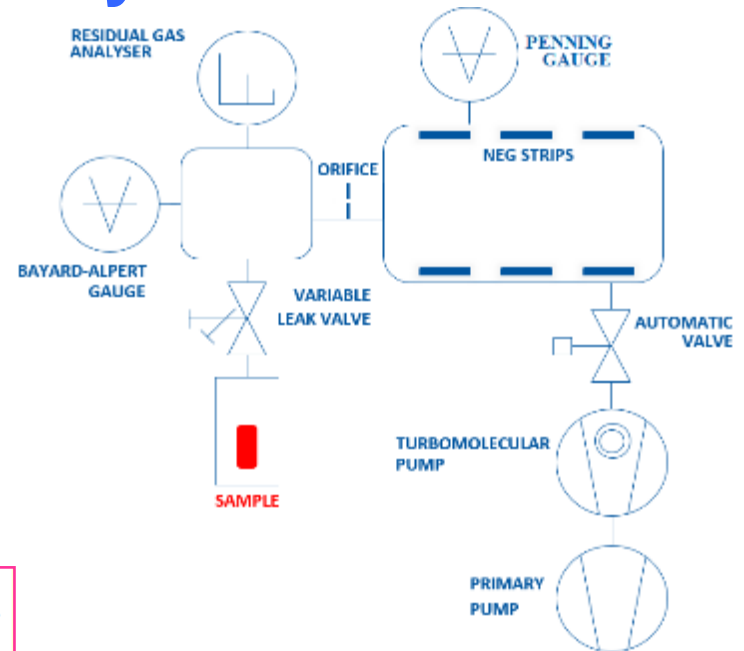
RGA	Ion source	Filament	Q (mbar.ℓ/s)
Faraday/SEM	Vac. fired grid	W	$2 \cdot 10^{-9}$
Faraday/Channeltron	Vac. fired grid	W	$4 \cdot 10^{-9}$
	grid	W	$4 \cdot 10^{-8}$
	Vac. fired open source	Y	$8 \cdot 10^{-9}$
	Open source	Y/W	$2 \cdot 10^{-8}$
			$5 \cdot 10^{-7}$

S. Meunier, CERN, 2019

# 3. Qualification of materials

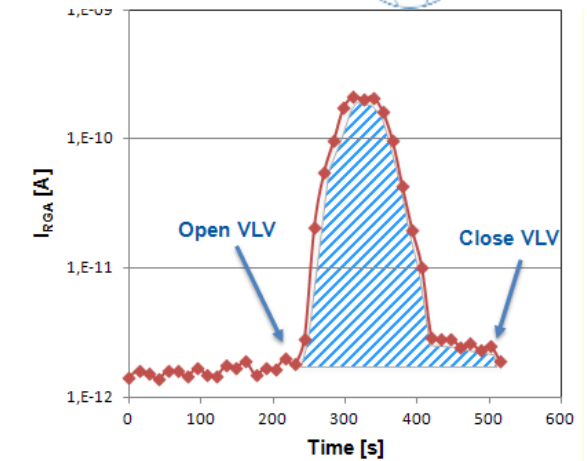
# Outgassing measurement by Accumulation

- A sample is placed in an evacuated vessel and the leak valve closed
- **Desorbed gas accumulates** into the sample chamber
- After some accumulation time  $t_{acc}$ , the leak valve is opened and the mass spectra recorded
- The leak valve is closed again and the procedure repeated every 1 to 72 h



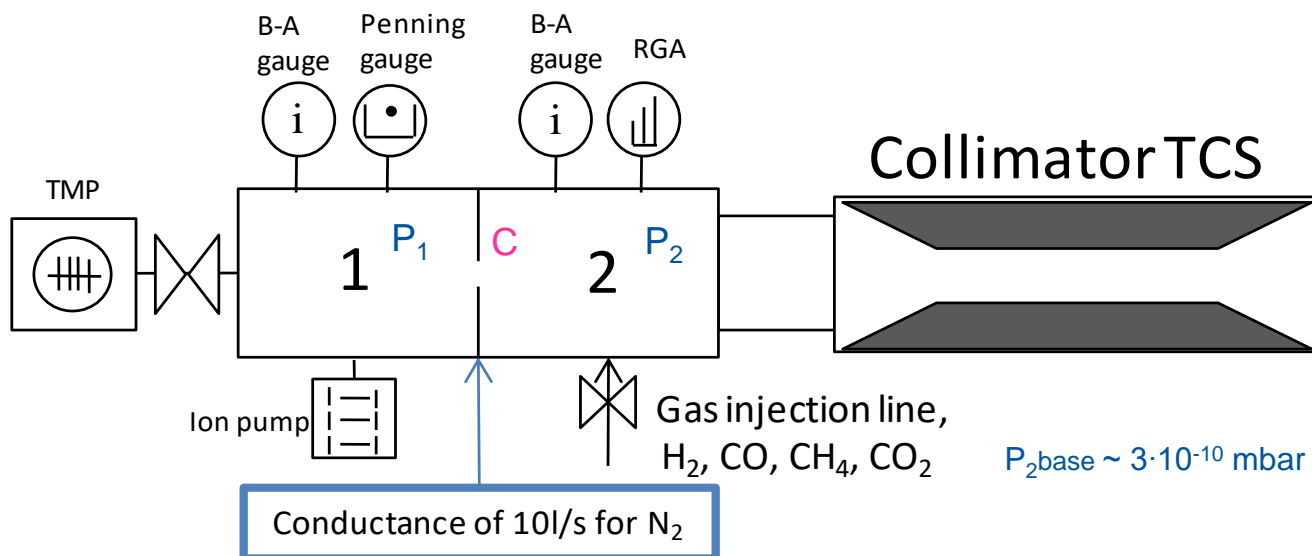
$$Q(\Delta t_{ac}) = \frac{S_i \int_0^{\Delta t} \alpha_i I_{RGA}(t) dt}{\Delta t_{ac}}$$

- With:
  - $S_i$  the pumping speed for gas,  $i$
  - $\alpha$  the RGA calibration factor for gas,  $i$
  - $I_{RGA}$  the current recorded during the leak valve opening
  - $\Delta t$  the RGA recording duration
  - $\Delta t_{ac}$  the accumulation time
- Sensitive measurement but gas re-adsorption may matters



Courtesy I. Wevers, TE-VSC

# Outgassing measurement: throughput method



J. Kamiya *et al.*, *Vacuum* 85 (2011) 1178-1181

- The component is connected to a pumping system via a conductance,  $C$
- Background is determined by a dry run
- The outgassing rate is

$$Q_{\text{N}_2\text{eq}} = C (P_2 - P_1)$$

In  $\text{N}_2$  equivalent no RGA is needed!

$$Q_i = S_{\text{eff}} P_{2,i} = C_i (P_{2,i} - P_{1,i})$$

$$S_{\text{eff}} = \frac{C_i (P_{2,i} - P_{1,i})}{P_{2,i}} = C_i \left(1 - \frac{P_1}{P_2}\right)$$



$$Q_i = C_i \alpha_i I_i \left(1 - \frac{P_1}{P_2}\right)$$

$\alpha$  the RGA calibration factor for gas,  $i$   
 $I_i$  the RGA current for gas  $i$   
 $C_i$  the conductance for gas  $i$



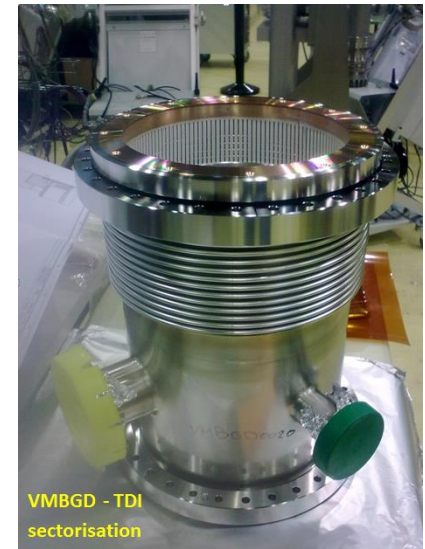
# Vacuum Acceptance Test Laboratory



LHC vacuum laboratory during LS1 (2013-2014)



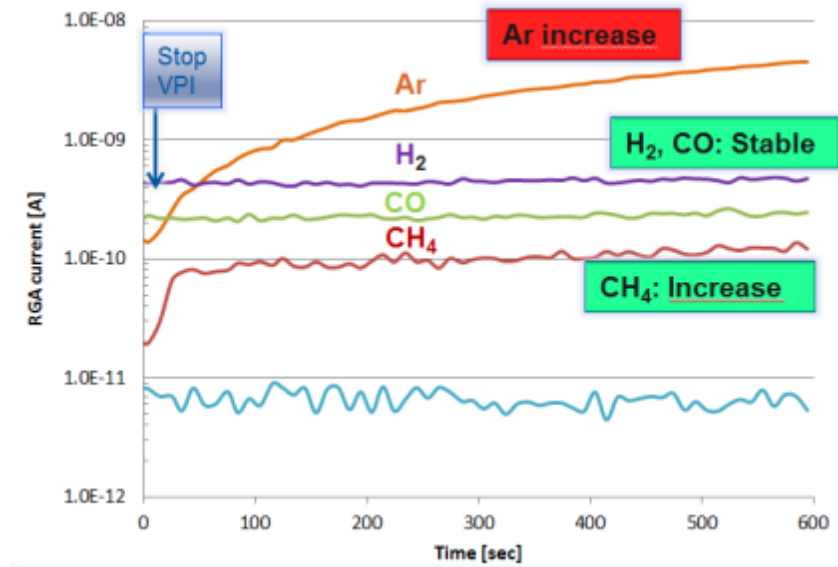
# Example of tested parts



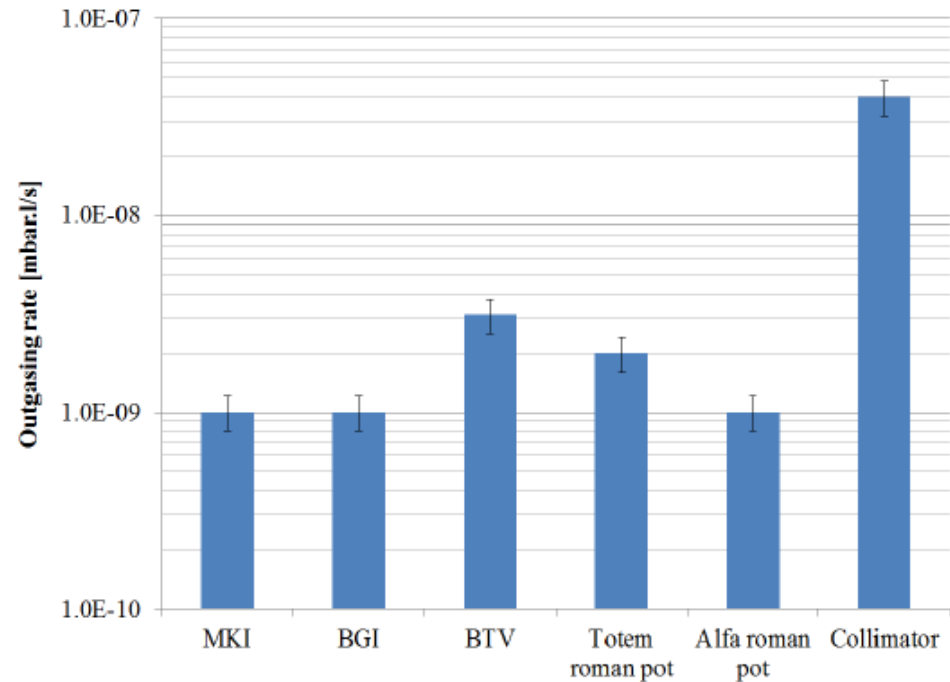


# Vacuum Acceptance Tests

- Prior to LS1 installation ~1200 LSS's equipments have been baked and validated at the surface :
  - functional test
  - pump down
  - leak detection
  - residual gas composition
  - total outgassing rate



Identification of virtual leaks by accumulation test whilst pumping with NEG system

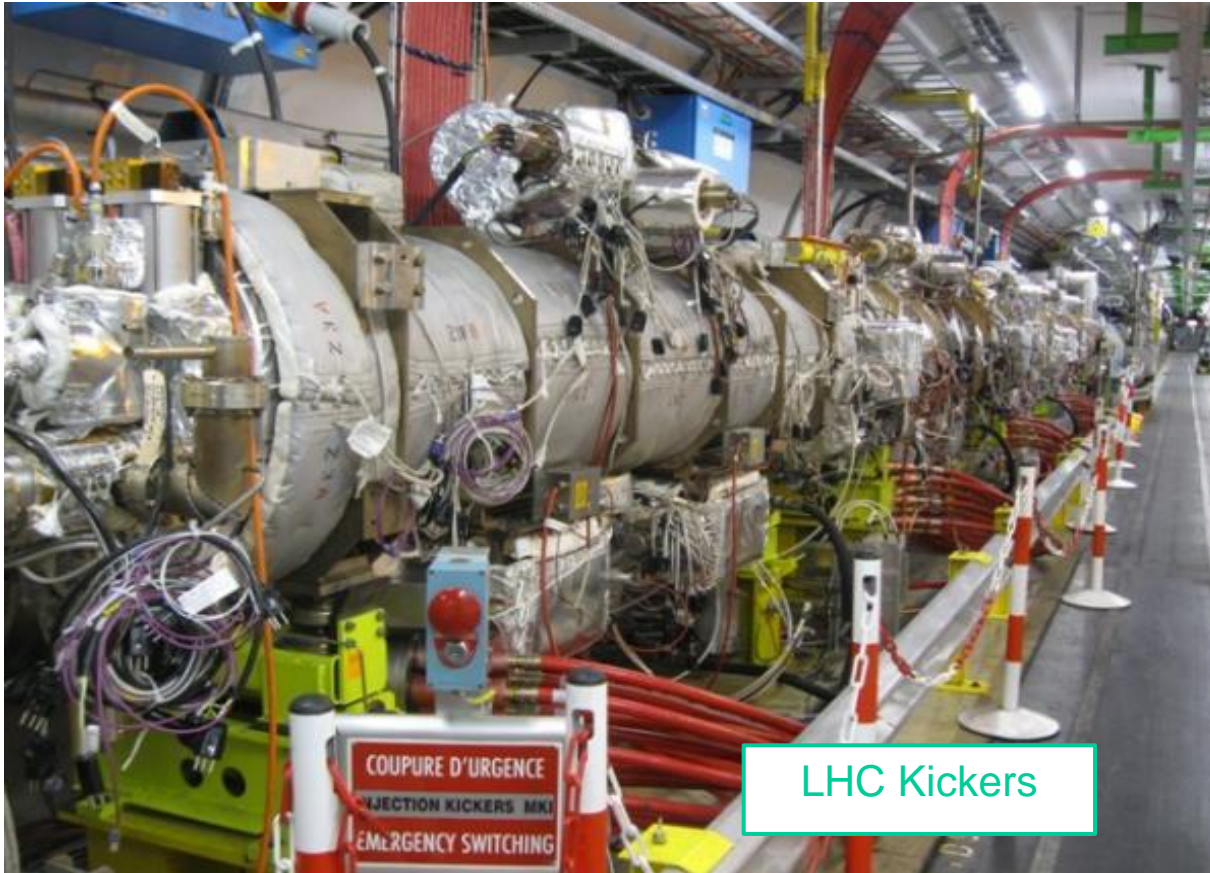


Outgassing rate of some LHC components

G. Cattenoz *et al.* , Proceeding of IPAC'14, Dresden, Germany

# Magnet Kicker for Injection (MKI)

- Total outgassing rate of this chain of 4 MKIs is  $\sim 5 \cdot 10^{-9}$  mbar.l/s  
→ that corresponds to the outgassing of 2 VITON seals after 1 year of pumping



# Cleaning Methods

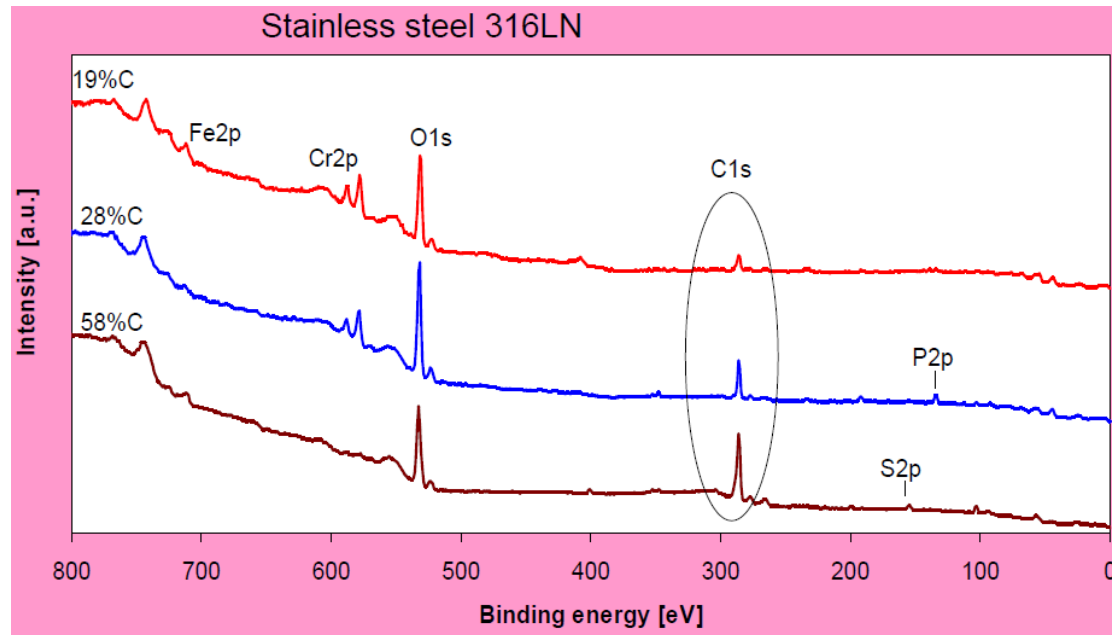
- **Chemical cleaning** is used to remove gross contamination such as grease, oil, fingerprints.
- It can be needed to attack the surface with acids to etch the **oxide layer**
- **Passivation** can be helpful to produce a “stable” oxide layer on the surface
- Example of CERN LHC beam screens :
  - Degreasing with an alkaline detergent at 50°C in an ultrasonic bath
  - Running tap water rinse
  - Cold demineralised water rinse by immersion
  - Rinse with alcohol
  - Dry with ambient air



L. Ferreira, CERN TE-VSC

# Surface analysis methods

- **Surface analysis** is used to evaluate the cleanliness of a material, identify species, monitor a process etc.
- Auger electron Spectroscopy
- X-ray Photoelectron Spectroscopy

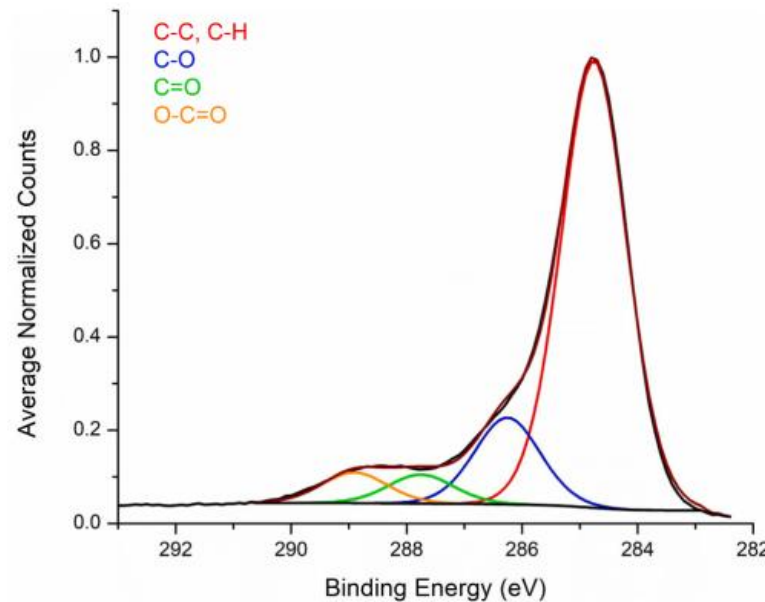


The assessment of metal surface cleanliness by XPS, C. Scheuerlein and M. Taborelli, Appl. Surf. Sci 252 (2006) 4279



# Example of adventitious carbon

- Adventitious carbon = a thin layer of carbonaceous material that deposits on air-exposed surfaces
- XPS analysis of adventitious carbon around C1s at 284.8 eV
- Adventitious carbon layer is aliphatic (hydrocarbons C, H, having an open chain structure) in nature and not graphitic, with functional groups of C, O
- Presence of CO and CO<sub>2</sub> molecules bounded on the very near surface (nm)



LH Grey et al., Appl. Surf. Sci 635 (2024) 159319

# Slot 4 summary

- **Vacuum firing** is used to reduce by 2 orders of magnitude the hydrogen outgassing of baked material.
- Other material than metals have their outgassing rate spread over several orders or magnitude with **plastics at the high extreme** ( $\times 10^5$  metallic surface)
- **Vacuum instruments** outgas!
- Components must be **characterised in the laboratory** with appropriate tools to guarantee a good performance in an accelerator

**Thank you for your attention !!!**



# Some References

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