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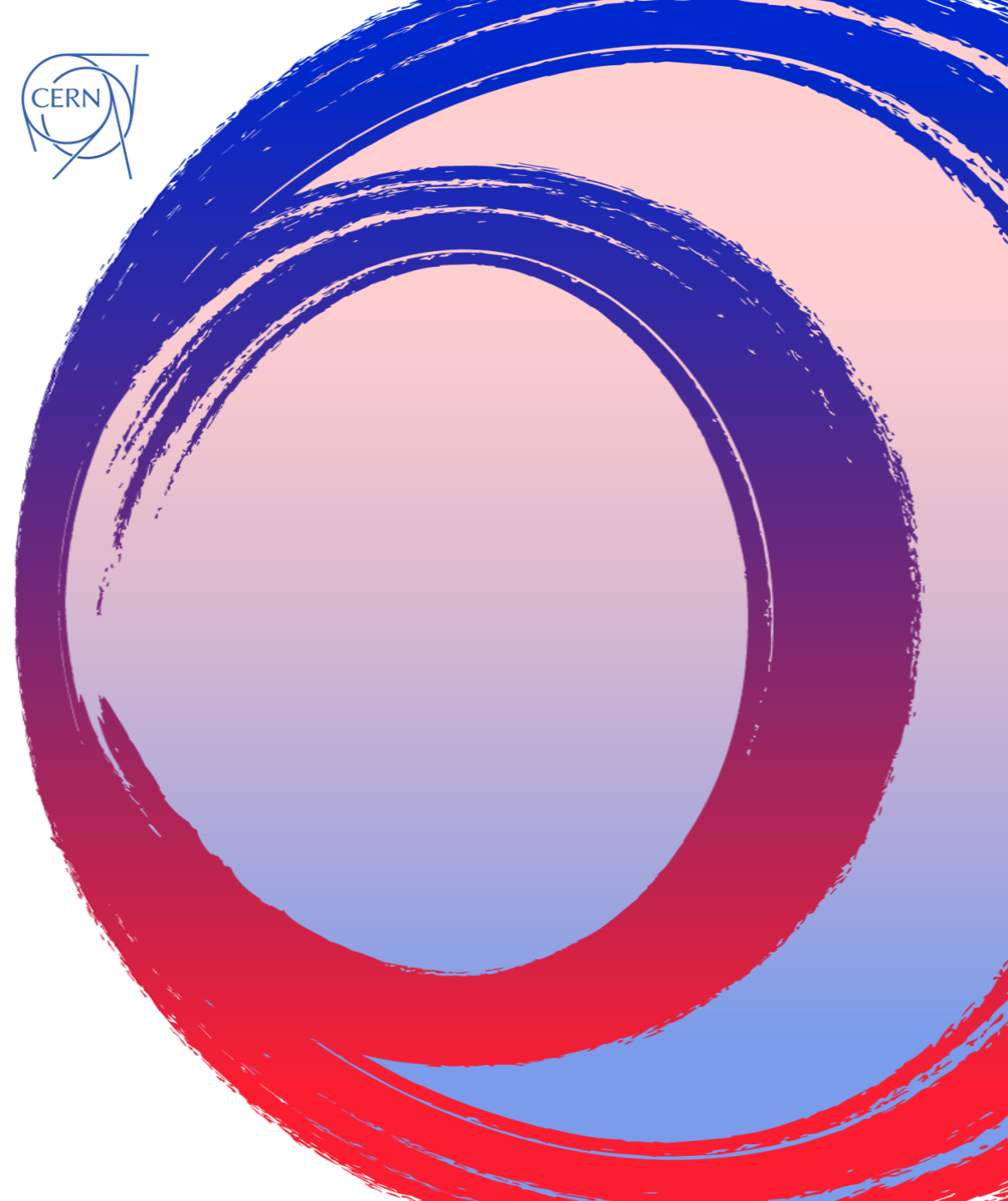


# PERFORMANCE LIMITS OF COMBINED FUNCTION MAGNETS

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S. Farinon<sup>2</sup>, F. Mariani<sup>1</sup>, S. Mariotto<sup>3</sup>, A. Pampaloni<sup>2</sup>, T. Salmi<sup>4</sup>**

<sup>1</sup>Sapienza University of Rome, <sup>2</sup>INFN – Genoa, <sup>3</sup>INFN and University of Milan

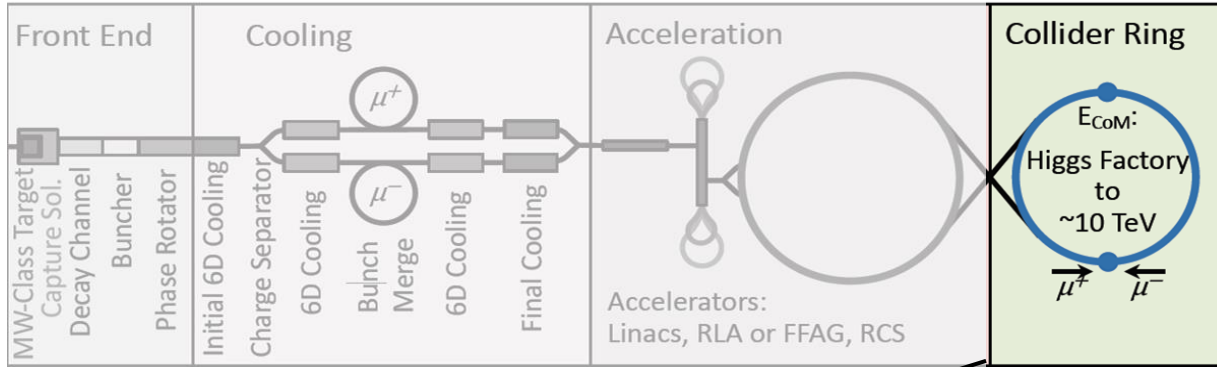
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**9 December 2024**

## Main stages of a muon collider complex



Need for high fields in large apertures

|                                     | 2 cm                        | 3 cm                        | 4 cm                        |
|-------------------------------------|-----------------------------|-----------------------------|-----------------------------|
| Beam aperture (radius)              | 23.5 mm                     | 23.5 mm                     | 23.5 mm                     |
| Outer shielding radius              | 43.5 mm                     | 53.5 mm                     | 63.5 mm                     |
| Inner coil aperture (radius)        | 59 mm                       | 69 mm                       | 79 mm                       |
| Power penetrating tungsten absorber | 19.1 W/m (3.8%)             | 8.2 W/m (1.6%)              | 4.1 W/m (0.8%)              |
| Peak power density in coils         | 6.5 mW/cm <sup>3</sup>      | 2.1 mW/cm <sup>3</sup>      | 0.7 mW/cm <sup>3</sup>      |
| Peak dose in Kapton (5/10 years)    | 56/112 MGy                  | 18/36 MGy                   | 7/14 MGy                    |
| Peak dose in coils (5/10 years)     | 45/90 MGy                   | 15/30 MGy                   | 5/10 MGy                    |
| Peak DPA in coils (5/10 years)      | 8/16 × 10 <sup>-5</sup> DPA | 6/12 × 10 <sup>-5</sup> DPA | 5/10 × 10 <sup>-5</sup> DPA |

Courtesy of Anton Lechner

Assuming 10 TeV machine and coil at 4.5 K

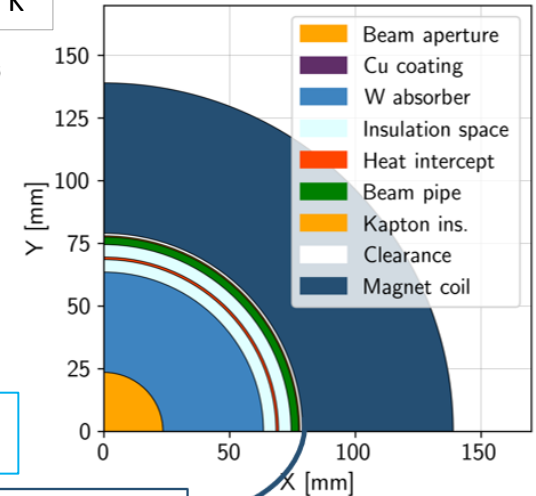
- Beam aperture (5 $\sigma$ ) 23.5 mm radius
- Cu layer beam screen 0.01 mm thick
- Tungsten absorber 40 mm thick
- Insulation space 5 mm thick
- Heat intercept 1 mm thick
- Insulation space 5 mm thick
- Beam pipe 3 mm thick
- Kapton insulation 0.5 mm thick
- Clearance 1 mm thick
- Coil pack\* (60 mm thick)

\*thickness TBD, placeholder

Courtesy of Patricia Borges de Sousa

<https://indico.cern.ch/event/1250075/contributions/5357594/>

## Dipole Radial Build

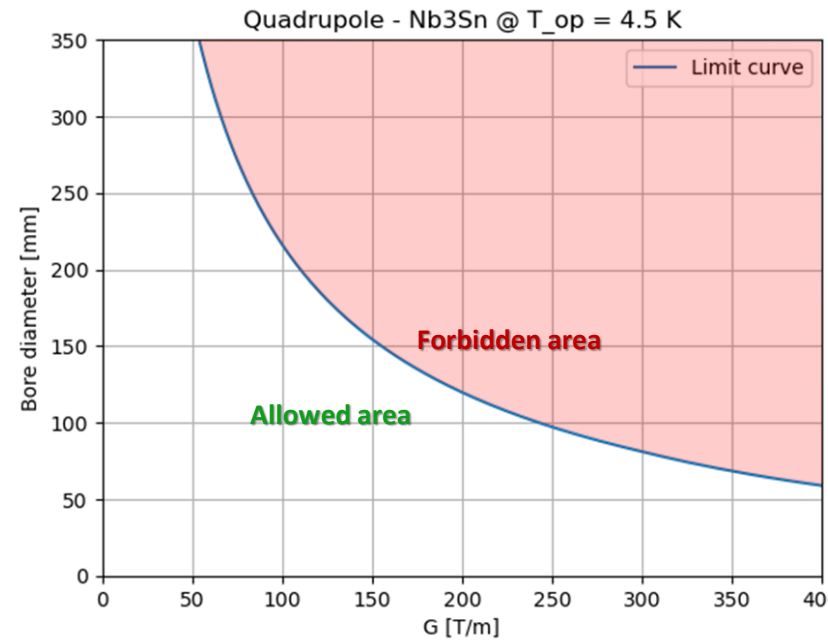
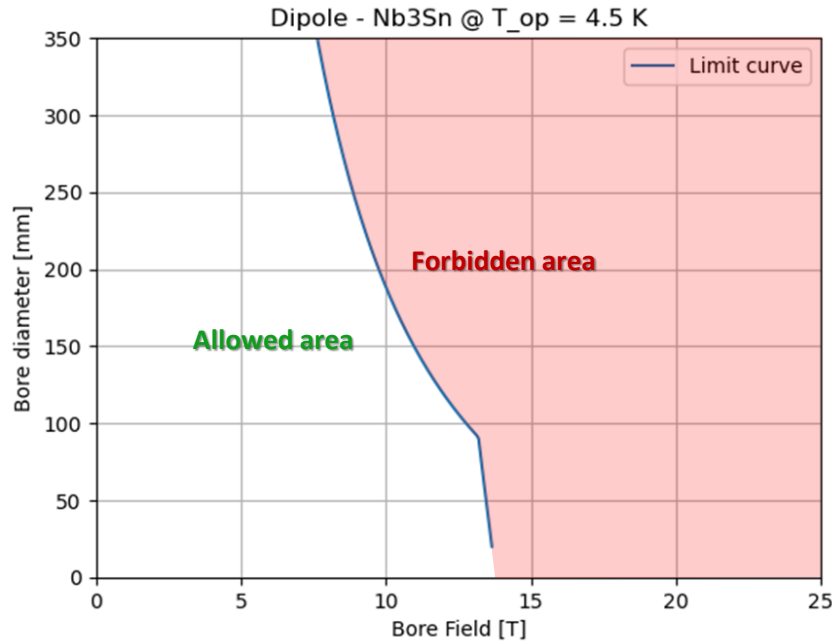


Coil aperture 158 mm

4 cm  $W_{abs}$  @  $T < 20$  K ( $P < 5$  W/m)  
 → 158 mm magnet aperture

3 cm  $W_{abs}$  @  $T = 20$  K ( $P < 10$  W/m)  
 → 138 mm magnet aperture

# A-B Plots for Nb<sub>3</sub>Sn



- A-B plots show the **performance limits** as a function of aperture diameter (A) and bore field (B) or gradient (G).
- Starting the design of a magnet **in the forbidden area** means already knowing from analytical approximations that one or more **technological limits** in the construction of superconducting magnets **will be exceeded**.
- Starting the design of a magnet **in the allowed area** but close to the limit curves does not mean that the magnet is easy to manufacture; rather, it indicates that **with progress in R&D**, it could become **feasible**.

The **Limit curve** includes:

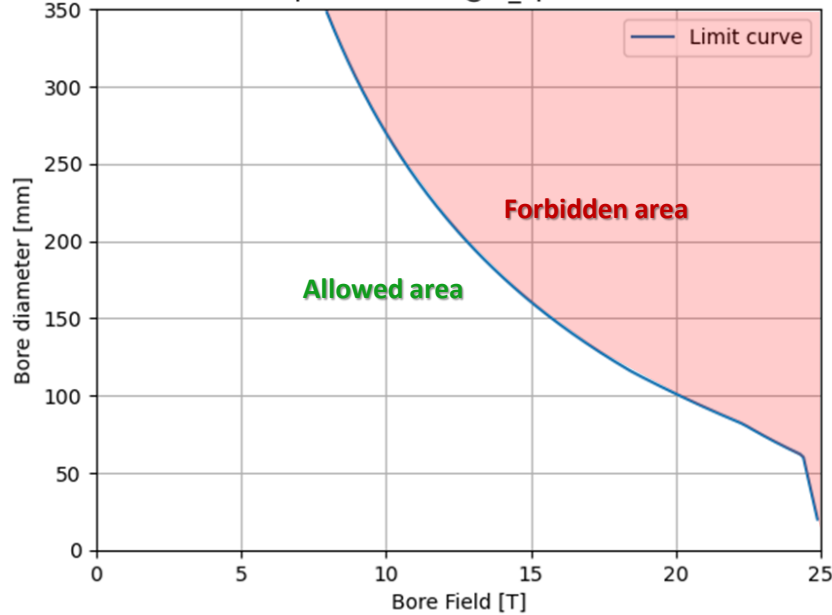
- Cost model: including coils, iron, structures and labour
- Protection: maximum hotspot temperature of 350K
- Margin: FCC cable target performance for the Jc fit
- Maximum midplane stress: 150 MPa

- Budget: 400 kEUR/m for each magnet.
- SC cost: 700 EUR/kg (aspirational, same cost as ITER procurement).
- These plots apply to both ARC and FF.
- Operating temperature: 4.5 K  
→ tungsten shield with a radius of 4 cm.

Nb<sub>3</sub>Sn is not considered for the 10 TeV as it falls short of the required performance. It may be an option for the 3TeV.

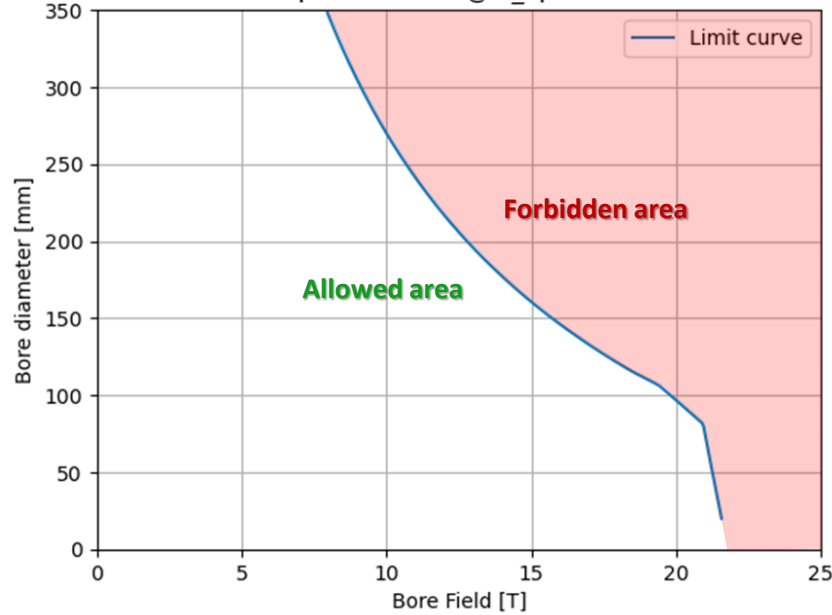
# HTS ARC Dipoles A-B Plots

Dipole - ReBCO @  $T_{op} = 4.5$  K



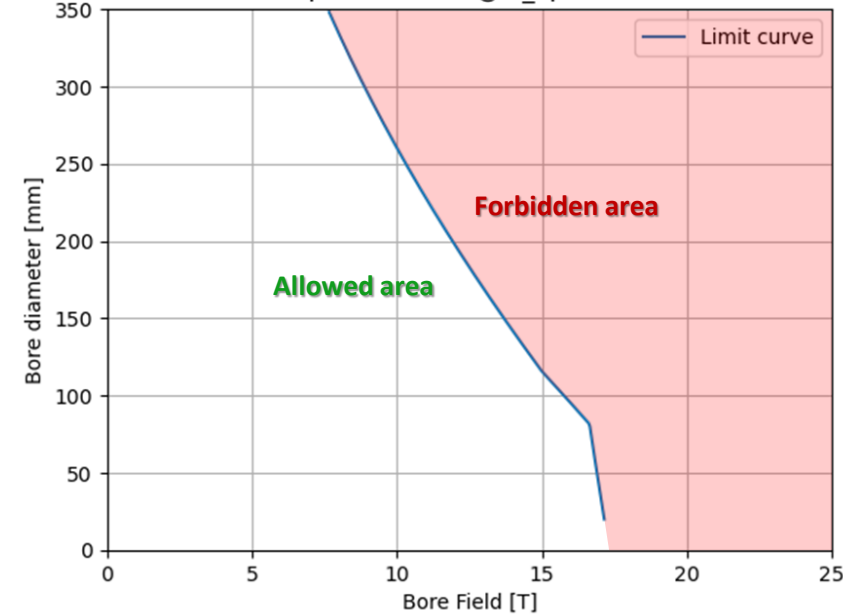
- Operating temperature: 4.5 K  
→ tungsten shield with a radius of 4 cm
- Budget: 400 kEUR/m for each magnet.
- SC cost: 2500 EUR/kg (aspirational value).
- These plots apply to ARC dipoles.

Dipole - ReBCO @  $T_{op} = 10$  K



- Operating temperature: 10 K  
→ tungsten shield with a radius of 4 cm

Dipole - ReBCO @  $T_{op} = 20$  K

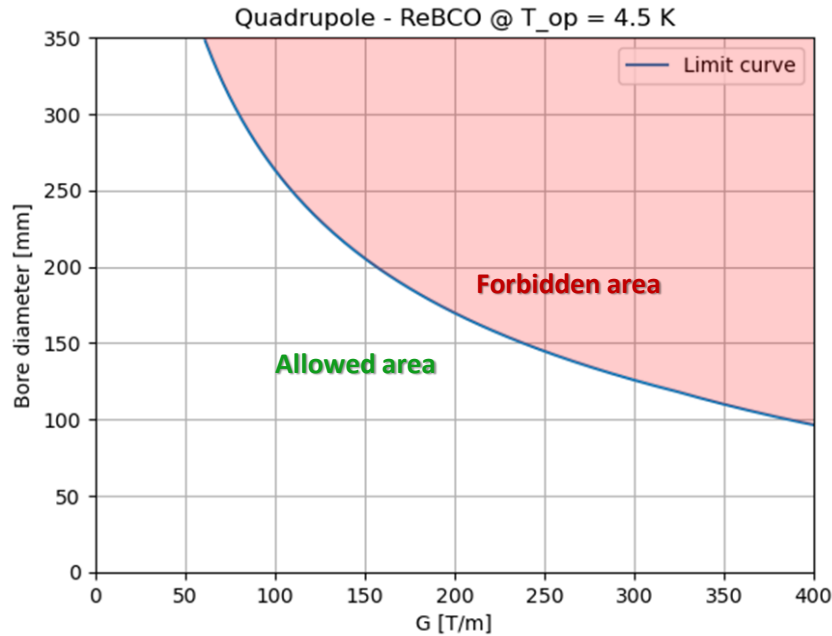


- Operating temperature: 20 K  
→ tungsten shield with a radius of 3 cm

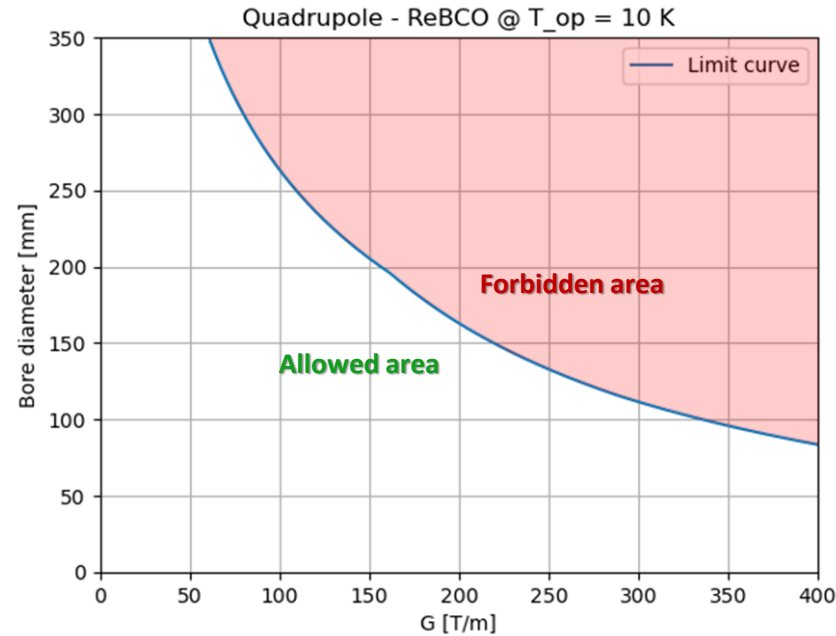
The **Limit curve** includes:

- Cost model: including coils, iron, structures and labour
- Protection: Non-insulated or Metal-insulated cable
- Margin: Fujikura FESC AP Tape for the  $J_c$  fit
- Maximum midplane stress: 400 MPa

ReBCO is considered the baseline for 10 TeV.



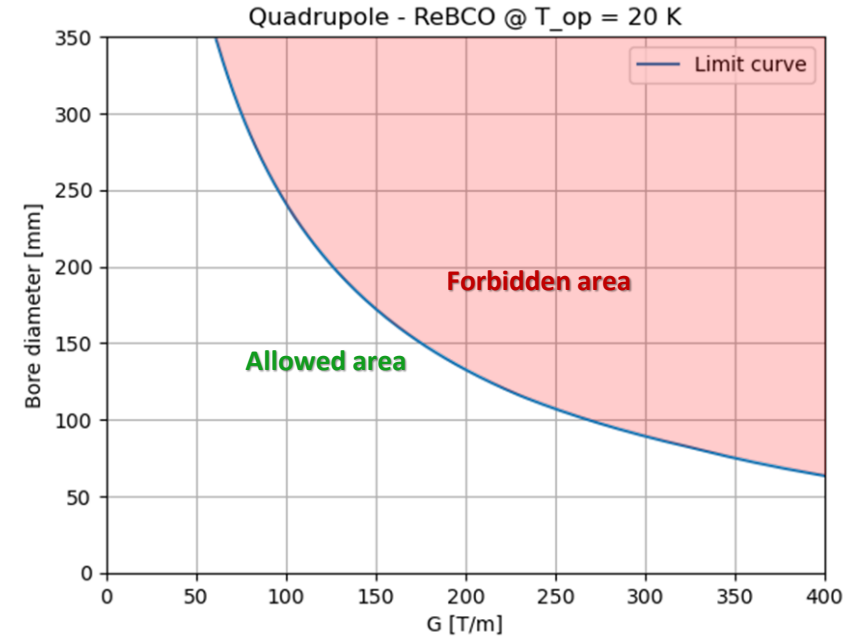
- Operating temperature: 4.5 K  
→ tungsten shield with a radius of 4 cm
- Budget: 400 kEUR/m for each magnet.
- SC cost: 2500 EUR/kg (aspirational value).
- These plots apply to ARC quadrupoles.



- Operating temperature: 10 K  
→ tungsten shield with a radius of 4 cm

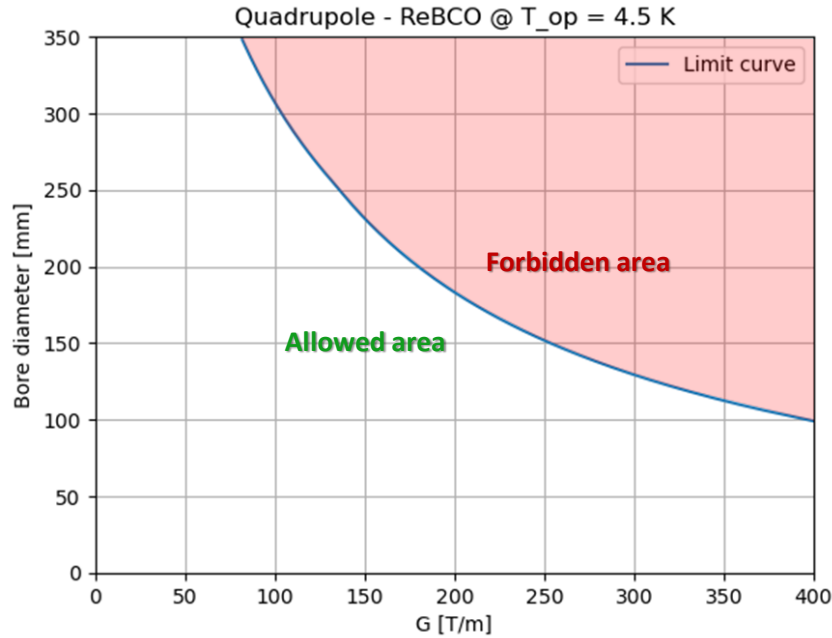
The **Limit curve** includes:

- Cost model: including coils, iron, structures and labour
- Protection: Non-insulated or Metal-insulated cable
- Margin: Fujikura FESC AP Tape for the  $J_c$  fit
- Maximum midplane stress: 400 MPa

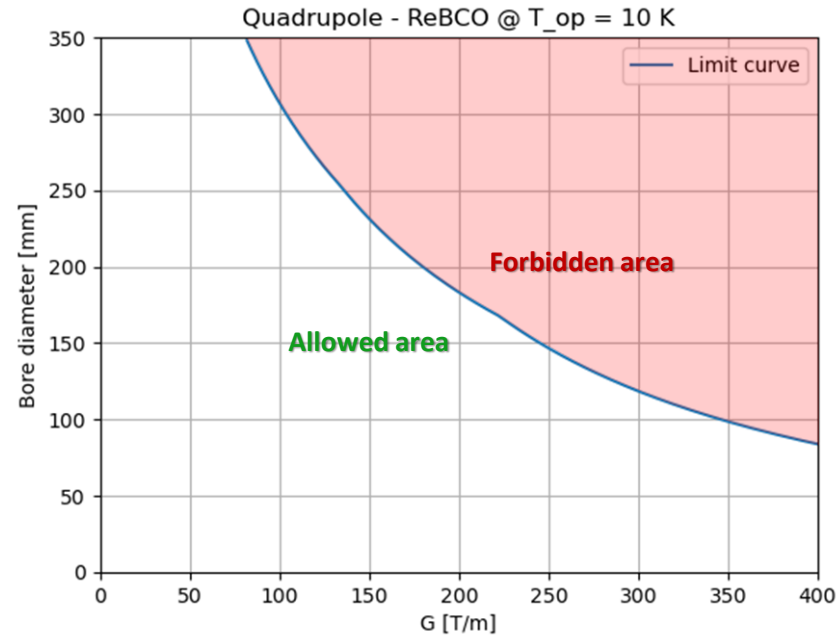


- Operating temperature: 20 K  
→ tungsten shield with a radius of 3 cm

ReBCO is considered the baseline for 10 TeV.



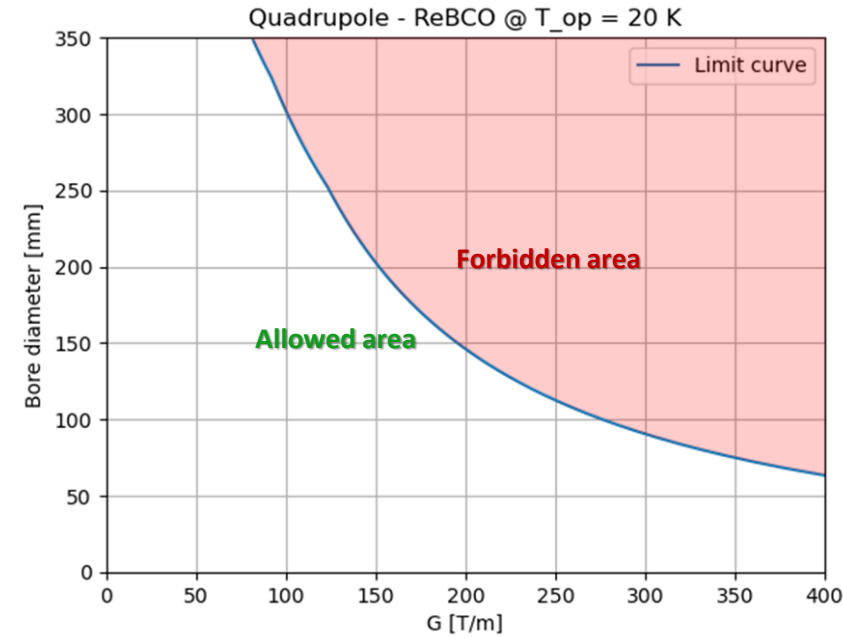
- Operating temperature: 4.5 K  
→ tungsten shield with a radius of 4 cm
- Budget: 800 kEUR/m for each magnet.
- SC cost: 2500 EUR/kg (aspirational value).
- These plots apply to FF quadrupoles.



- Operating temperature: 10 K  
→ tungsten shield with a radius of 4 cm

The **Limit curve** includes:

- Cost model: including coils, iron, structures and labour
- Protection: Non-insulated or Metal-insulated cable
- Margin: Fujikura FESC AP Tape for the Jc fit
- Maximum midplane stress: 400 MPa

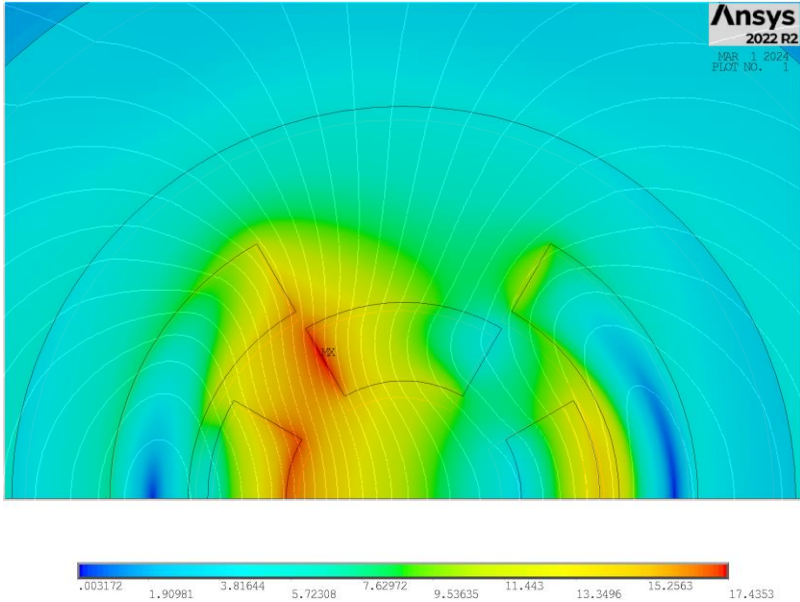


- Operating temperature: 20 K  
→ tungsten shield with a radius of 3 cm

ReBCO is considered the baseline for 10 TeV.

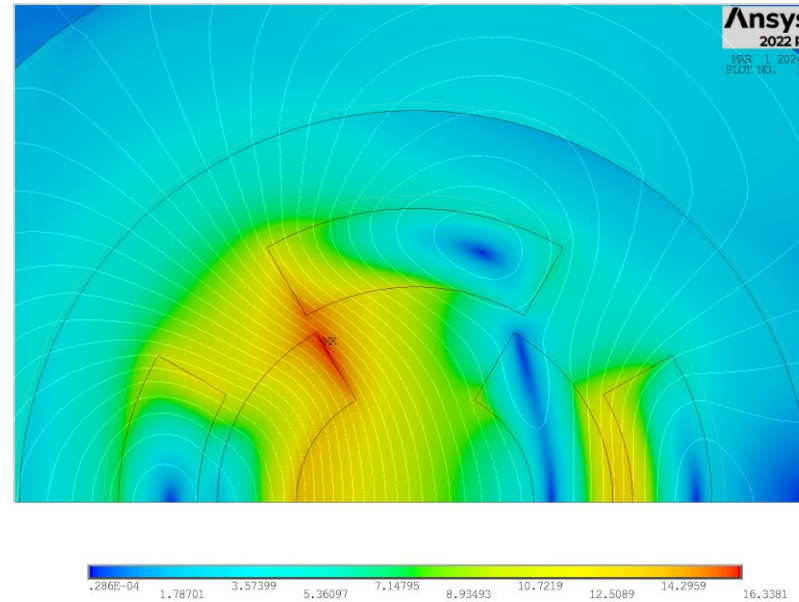


# COMBINED: NESTED CONFIGURATION



### Quad into dipole:

(ReBCO @20 K)  
 $J = 3.5 \cdot 10^8 \text{ A/m}^2$   
 $B \sim 11.7 \text{ T}$   
 $G \sim 143.3 \text{ T/m}$



### Dipole into quad:

(ReBCO @20 K)  
 $J = 3.5 \cdot 10^8 \text{ A/m}^2$   
 $B \sim 12.4 \text{ T}$   
 $G \sim 90.4 \text{ T/m}$



### Arc:

- Combined function magnets: B1, **B1+B2** and **B1+B3**
- $B \approx 8 \dots 16 \text{ T}$ ;  $G \approx 320 \text{ T/m}$ ;  $G' \approx 7100 \text{ T/m}^2$
- Aperture  $\approx 160 \text{ mm}$

### Final focus:

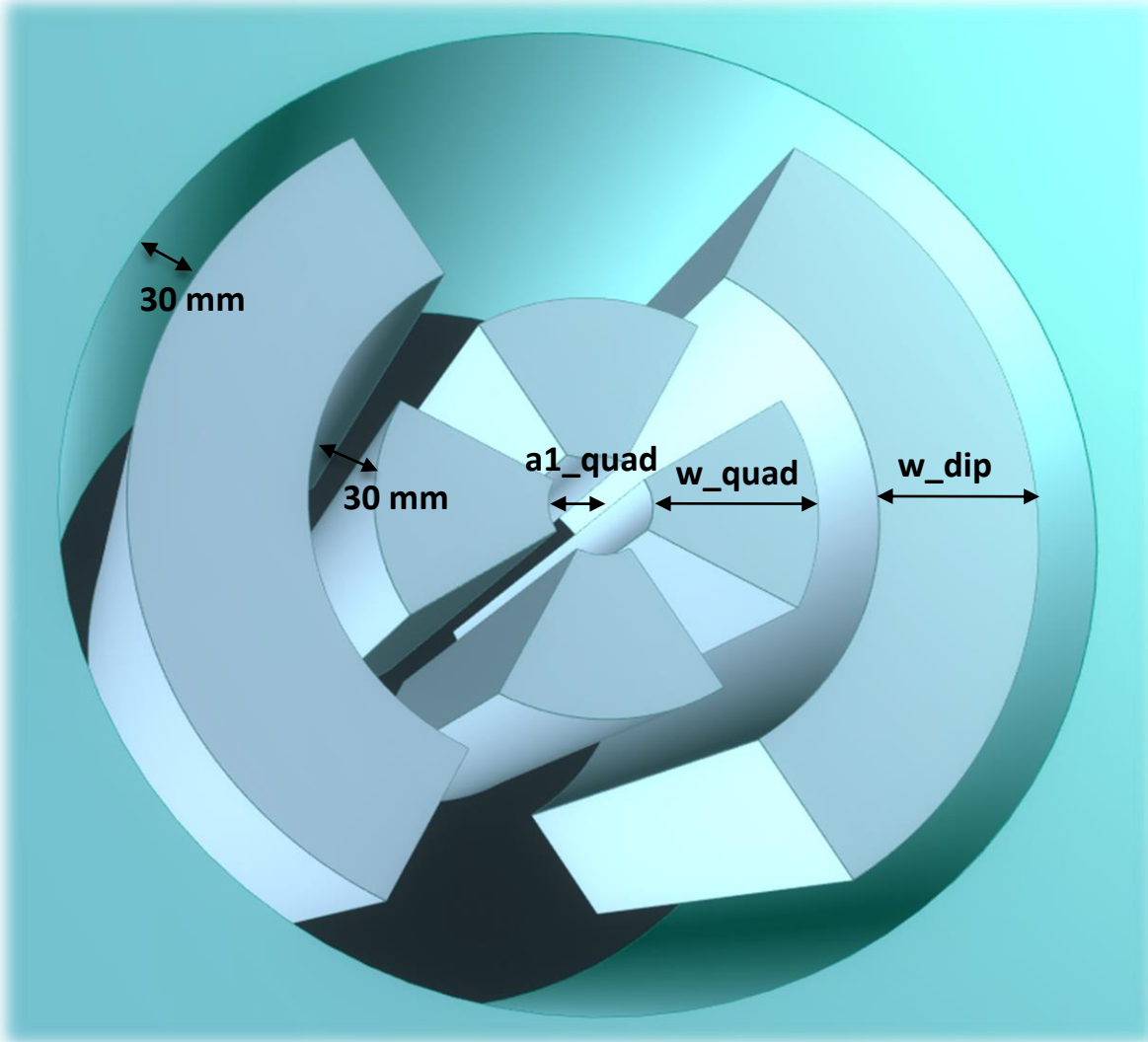
- Combined function magnets: B1, B2, **B1+B2**, **B1+B3**
- $B \approx 4 \dots 16 \text{ T}$ ;  $G \approx 100 \dots 300 \text{ T/m}$ ;  $G' \approx 12000 \text{ T/m}^2$
- Aperture  $\approx 120 \dots 300 \text{ mm}$

The quadrupole into dipole configuration is the most efficient one, in accordance with US-MAP. Additionally, for combined function magnets in the muon collider, quadrupoles are generally required to be stronger than dipoles.

|                           | Dipole             | Dipole/Quadrupole  | Quadrupole/Dipole  |
|---------------------------|--------------------|--------------------|--------------------|
| Superconductor            | Nb <sub>3</sub> Sn | Nb <sub>3</sub> Sn | Nb <sub>3</sub> Sn |
| Cable                     | 40x1mm             | 40x1mm             | 40x1mm/30x1mm      |
| $B_{coil,max}$ , T        | 15.1               | 16.6/16.2          | 16.2/16.1          |
| $B_{max}/G_{max}$ , T/T/m | 14.4               | 9.9/70.1           | 10.3/89.8          |
| $B_{op}/G_{op}$ , T/T/m   | 10                 | 8/71               | 8/81               |
| Margin                    | -40%               | ~24%/~20%          | ~28%/~20%          |

*Most efficient configuration*

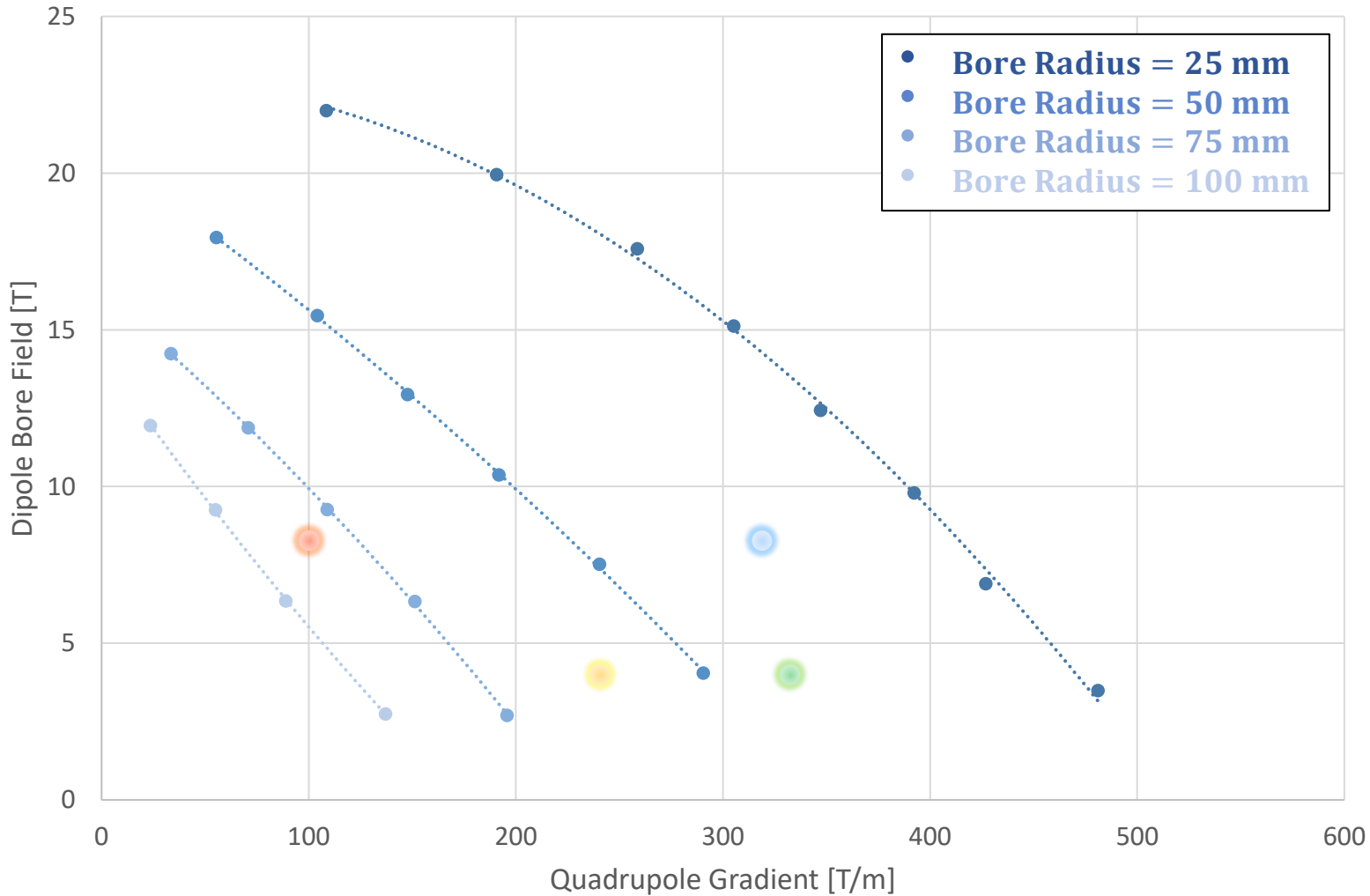
Fermilab



- A **Python-ANSYS interface** was developed to run FEM configurations capable of providing the electromagnetic performance of various designs.
- Loops were implemented by varying the temperature,  $a1\_quad$  and  $w\_quad$ . For each fixed value, the maximum  $w\_dip$  was calculated using a **cost model**, and an optimization code for electromagnetic performance was executed. This code aimed to maximize the current density while staying within **stress and margin limits**.
- As anticipated, the performance limits for combined function magnets are significantly more stringent compared to those for dipoles and quadrupoles individually. **Extending the curves along the axes reveals the boundaries defined by the A-B and A-G plots.**



# FINAL B-G PLOT AT T = 4.5 K



From v0.7:

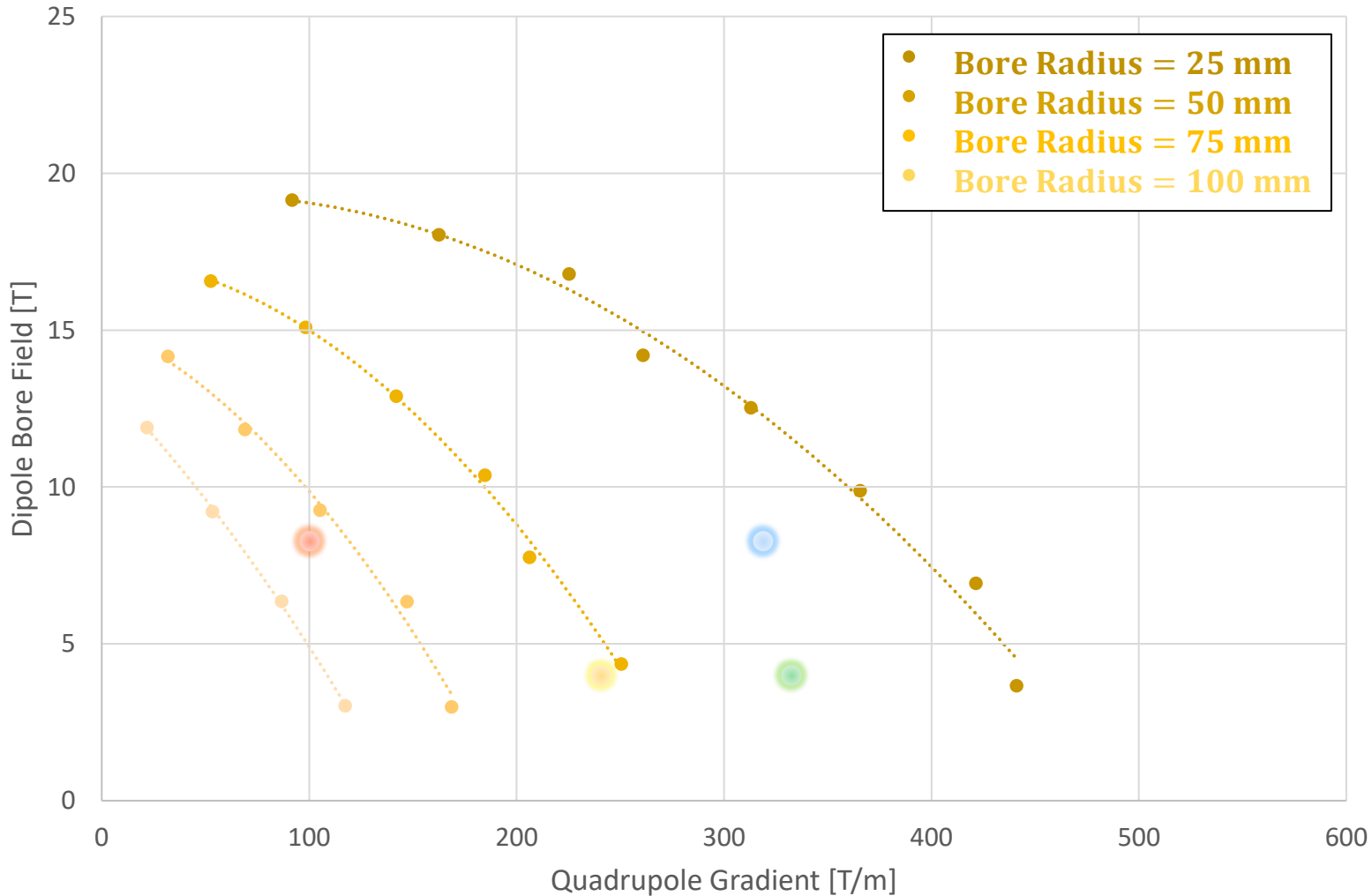
- 8 T, 100 T/m, 140 mm of radius
- 8 T, 320 T/m, 50 mm of radius
- 4 T, 240 T/m, 70 mm of radius
- 4 T, 330 T/m, 50 mm of radius

*Courtesy of Kyriacos Skoufaris*  
<https://indico.cern.ch/event/1351046/>

Maximum budget = 400 kEUR/m  
 Labour = 20 kEUR/m  
 Iron and Structures = 60 kEUR/m  
 ↓  
 Budget for the SC = 320 kEUR/m

The radial build might change: a solution needs to be studied to address the issue of the quadrupole moving inward.

# FINAL B-G PLOT AT T = 10 K



From v0.7:

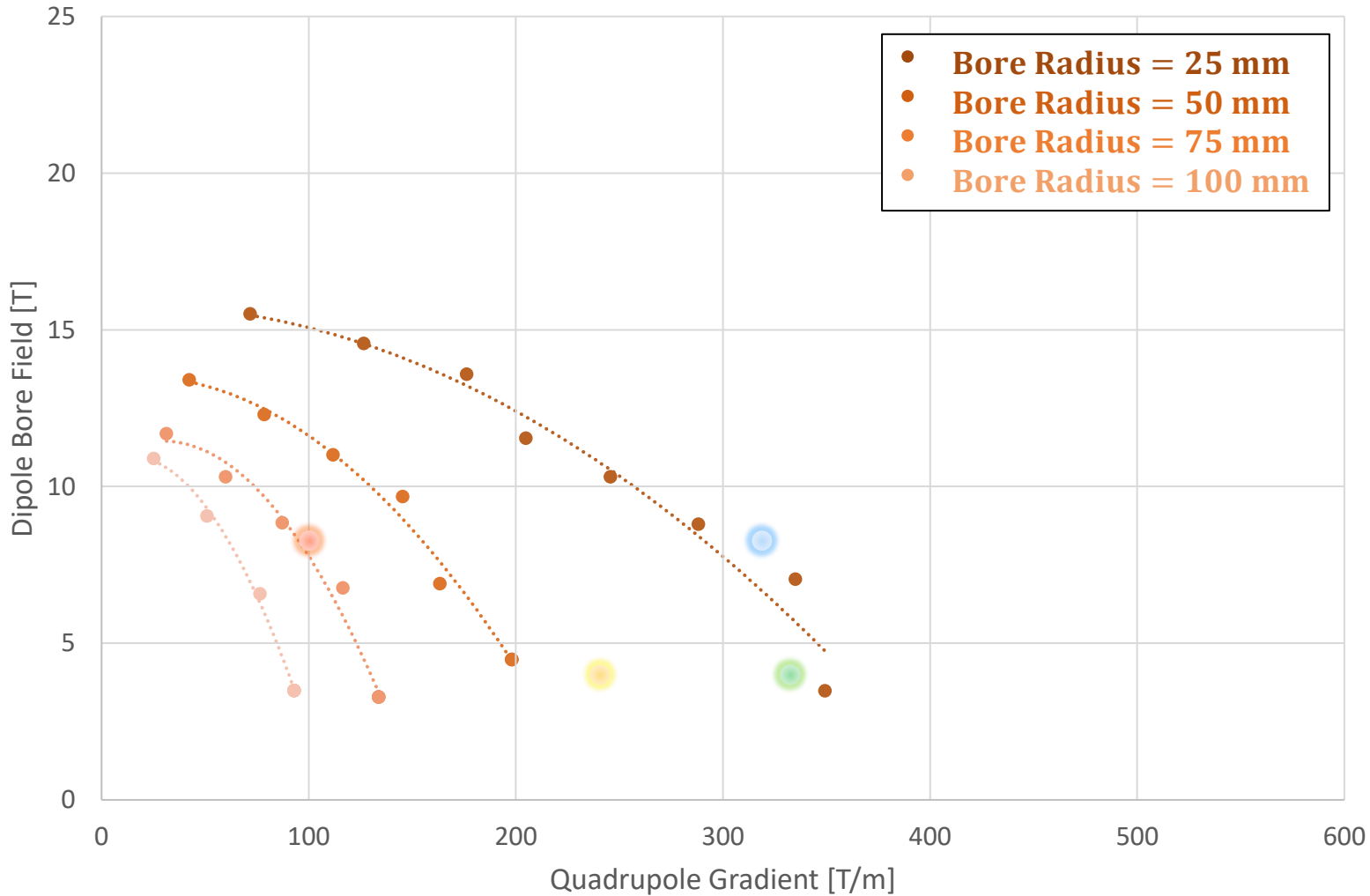
- 8 T, 100 T/m, 140 mm of radius
- 8 T, 320 T/m, 50 mm of radius
- 4 T, 240 T/m, 70 mm of radius
- 4 T, 330 T/m, 50 mm of radius

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Maximum budget = 400 kEUR/m  
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 ↓  
 Budget for the SC = 320 kEUR/m

The radial build might change: a solution needs to be studied to address the issue of the quadrupole moving inward.

# FINAL B-G PLOT AT T = 20 K



From v0.7:

- 8 T, 100 T/m, 140 mm of radius
- 8 T, 320 T/m, 50 mm of radius
- 4 T, 240 T/m, 70 mm of radius
- 4 T, 330 T/m, 50 mm of radius

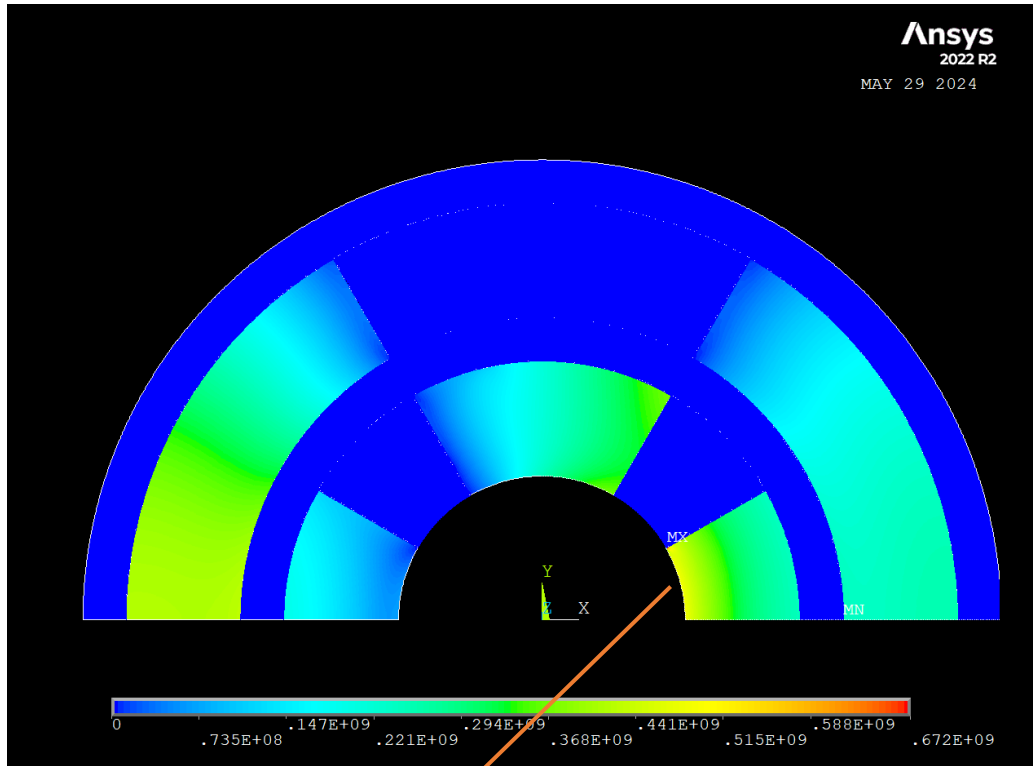
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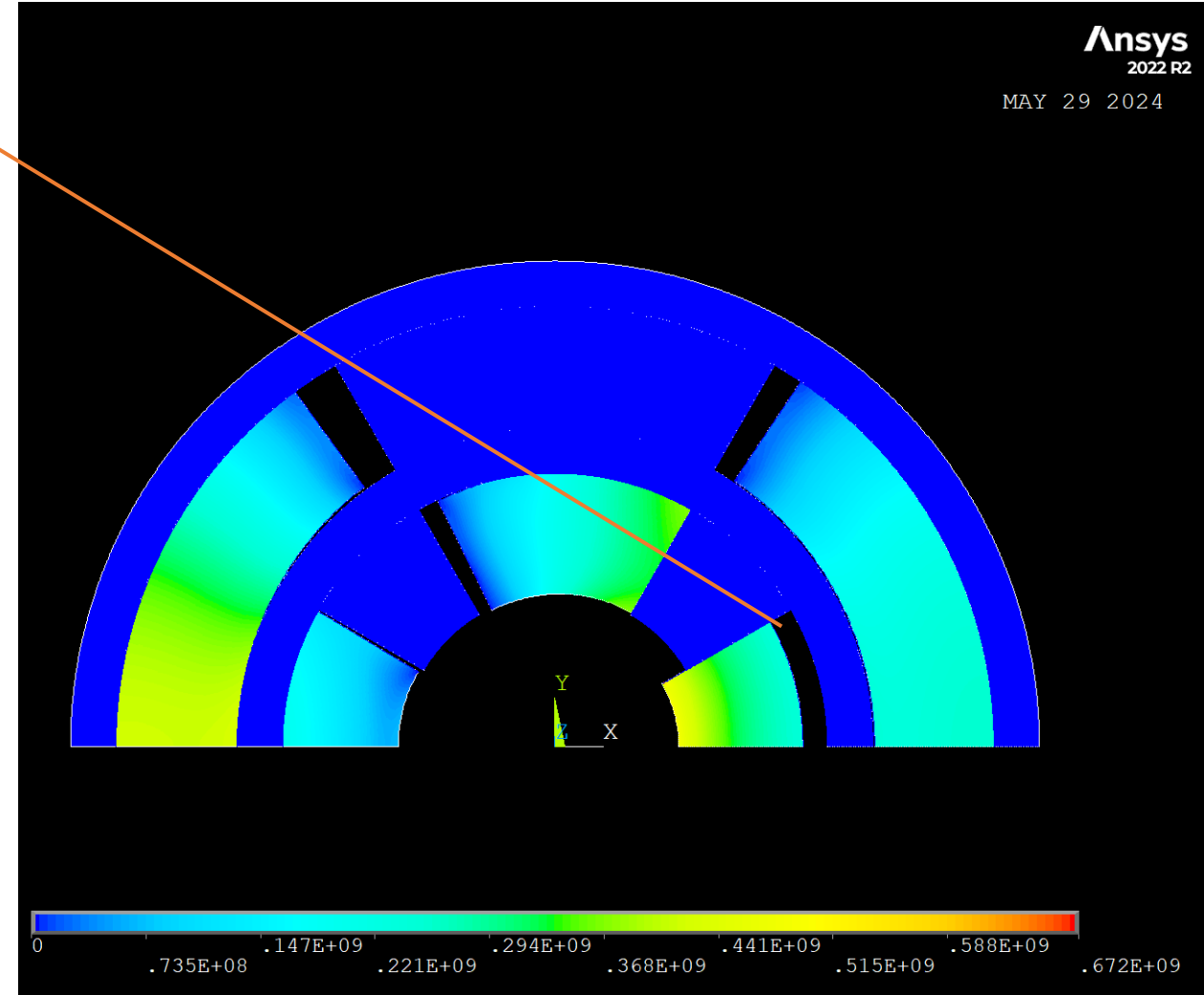
The radial build might change: a solution needs to be studied to address the issue of the quadrupole moving inward.

# STRESS ISSUE

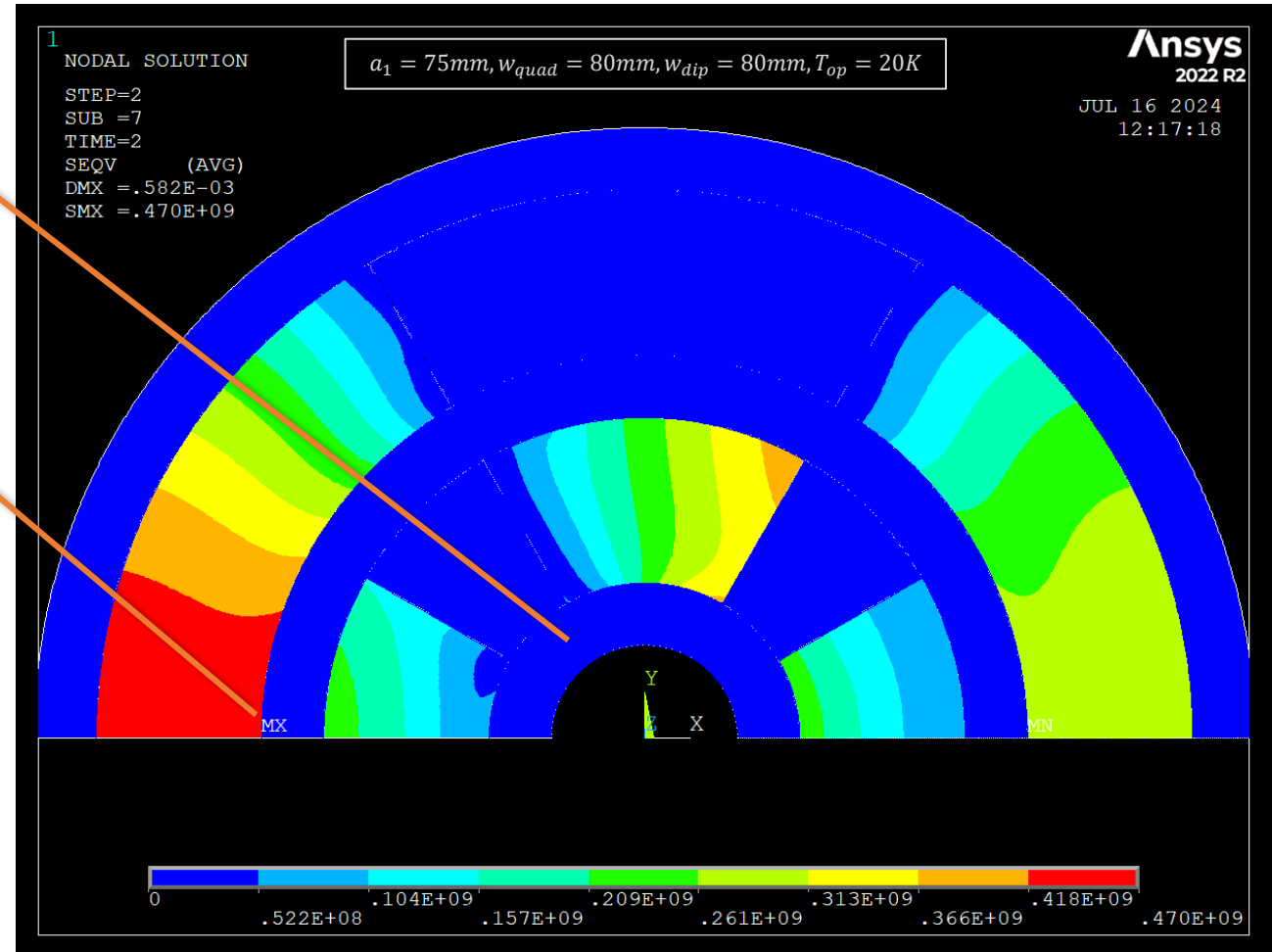
- Zoom-in on the displacements shows that this sector of the quadrupole moves inward



The Von Mises peak stress is on the inner part of the coil



- To address the issue, we insert an **infinitely rigid internal structure** to enable the study of stress behavior in the coils.
- Now the **peak stress**, in the same configuration discussed so far, is on the dipole in compression on the midplane (by changing the parameters, the maximum could be shifted).
- Now that we have a stress distribution in the coils, we can run the code and add a column with the peak stress to the data.
- With all information we will try to create B-G plots for the combined.





- As the **A-B plots** for dipoles and the **A-G plots** for quadrupoles were presented, the performance of combined function superconducting magnets was analyzed in various configurations, leading to the development of **B-G plots**.
- In the **cost model**, the same limitations discussed for the arc magnets were assumed.
- The study will continue to address the **issue of stress** (one of the quadrupole coils moves into the aperture), in collaboration with the cryogenic and energy deposition groups, and to develop a potential **quench protection system**, while further exploring innovative approaches such as non-insulated and metal-insulated coils.
- **The presented B-G plots should be considered as the best representation of the EM performance of combined function magnets.** Consequently, target designs can be identified in collaboration with beam optics.



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# THANK YOU FOR YOUR ATTENTION

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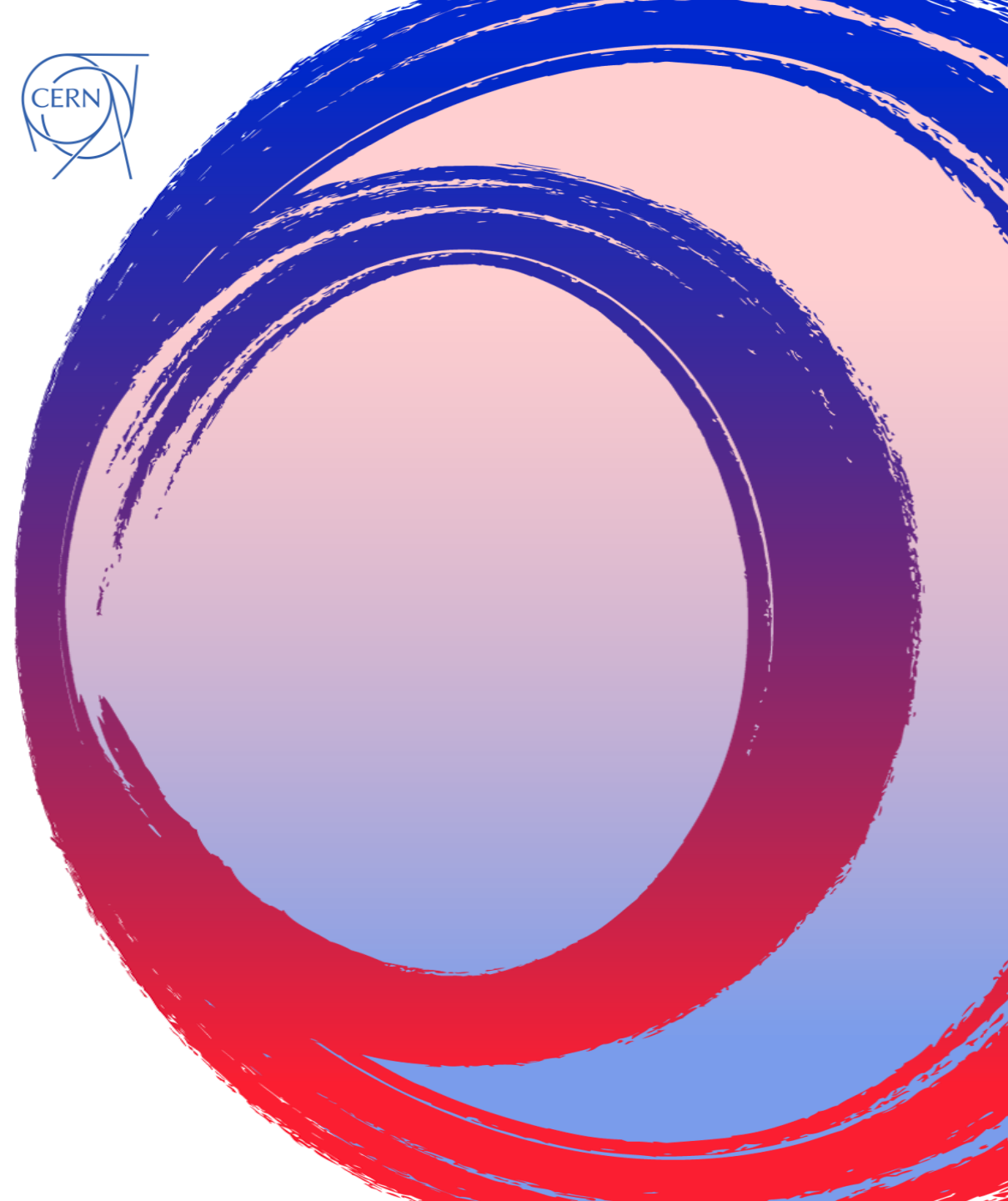
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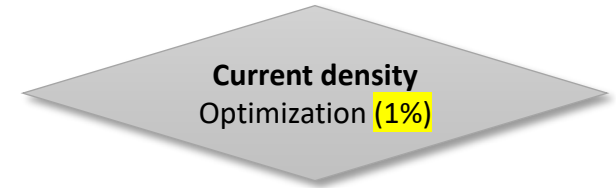
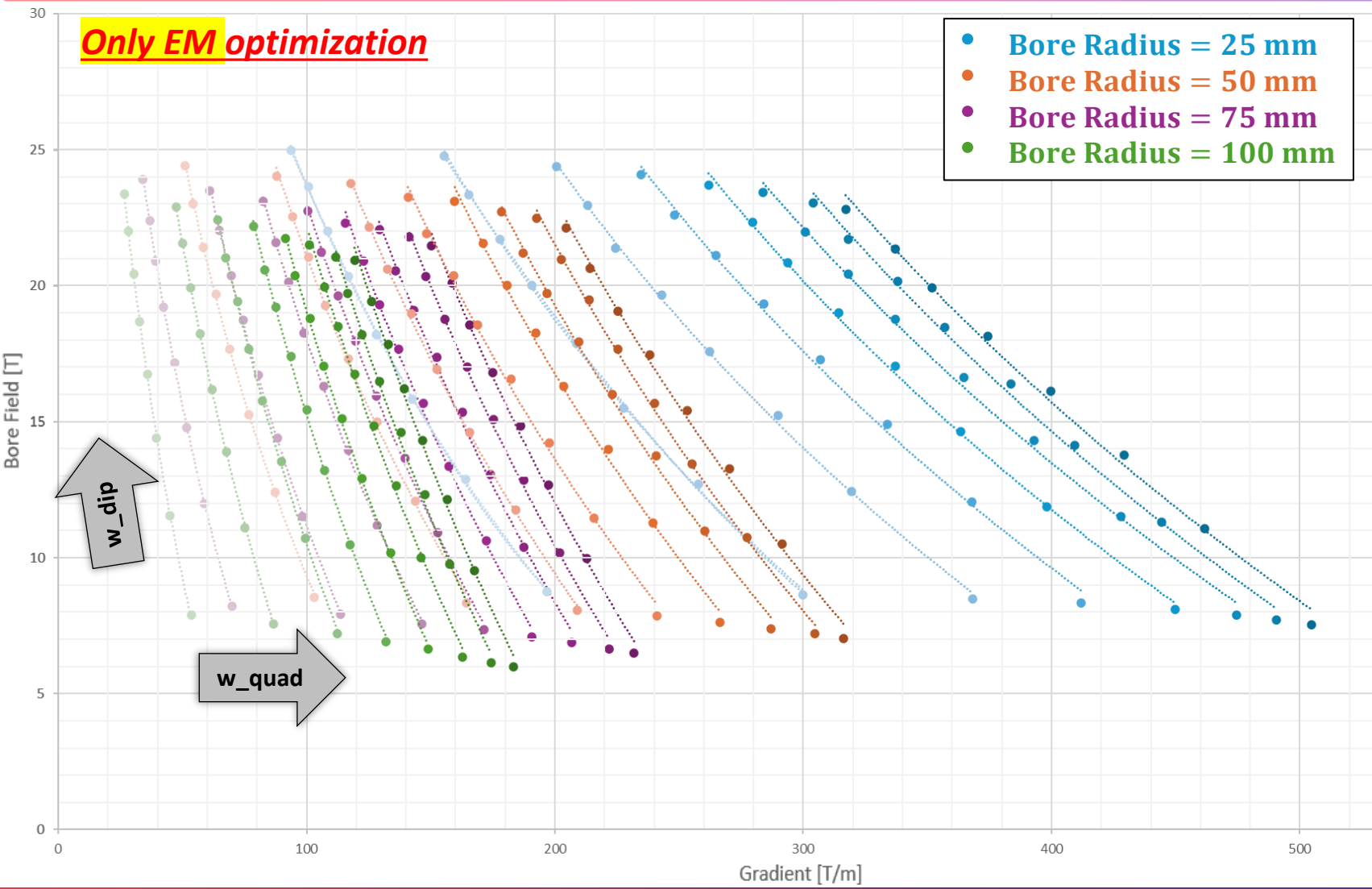
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# BACKUP SLIDES



# EM. B-G PLOT AT 4.5K



Optimize  $J_{quad}$  and  $J_{dip}$  to be close to the critical current density:

```

while not ( 0.99 < f < 1.01 ):
    ....
    → ANSYS input (a1, w_quad, J_quad, w_dip, J_dip)
    Run ANSYS
    ANSYS output →
    f = J_c (B_peak) / J
    if f > 1: J = J * 1.01
    else: J = J * 0.99
    ....
    
```

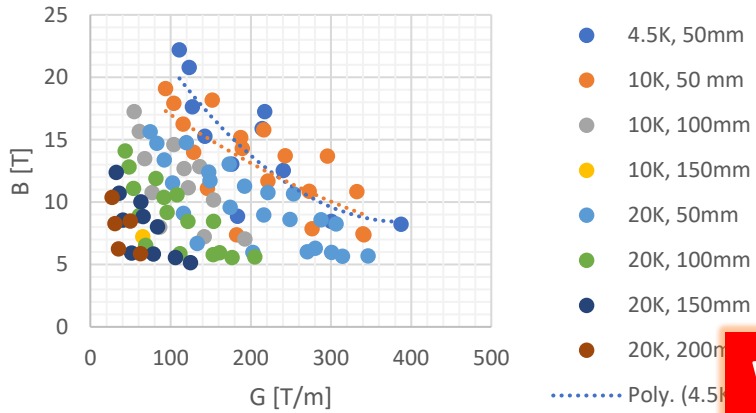
the optimization acts on  $J_{quad}$  and  $J_{dip}$  with corrections of 1%, and the cycle closes when either  $J_{quad}$  or  $J_{dip}$  is within 1% of  $J_c$



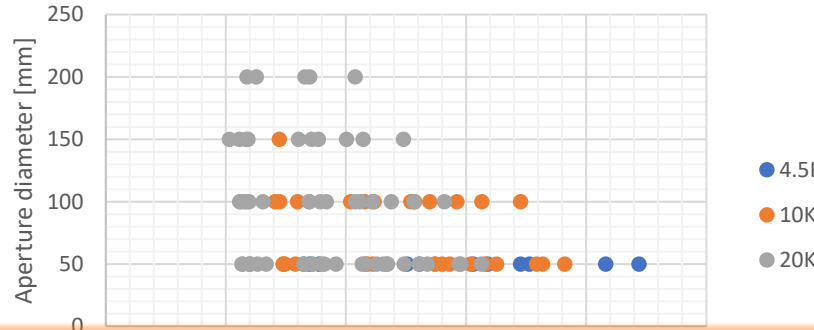
This optimization requires more computational effort, but the result is more understandable graphs.

Manually excluding the points that exceed the cost (400 kEUR/m) and the stress (400 MPa) limits

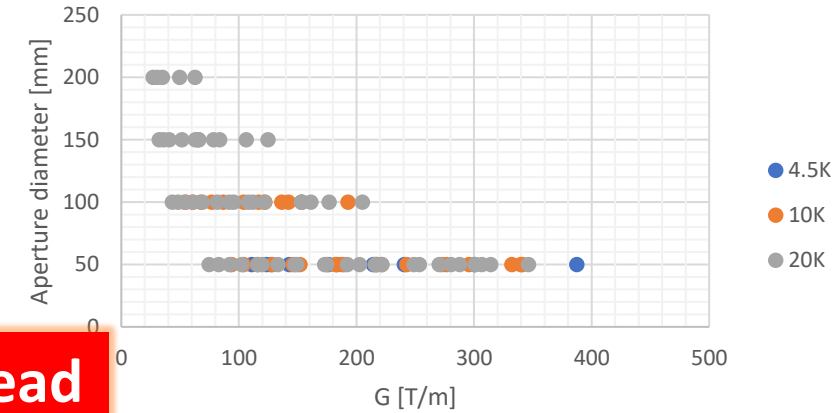
B vs G – Cost and Stress limits



A vs B – Cost and Stress limits

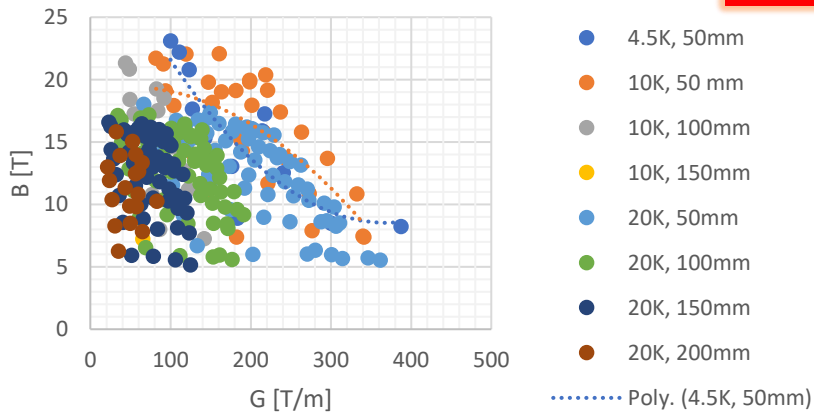


A vs G – Cost and Stress limits

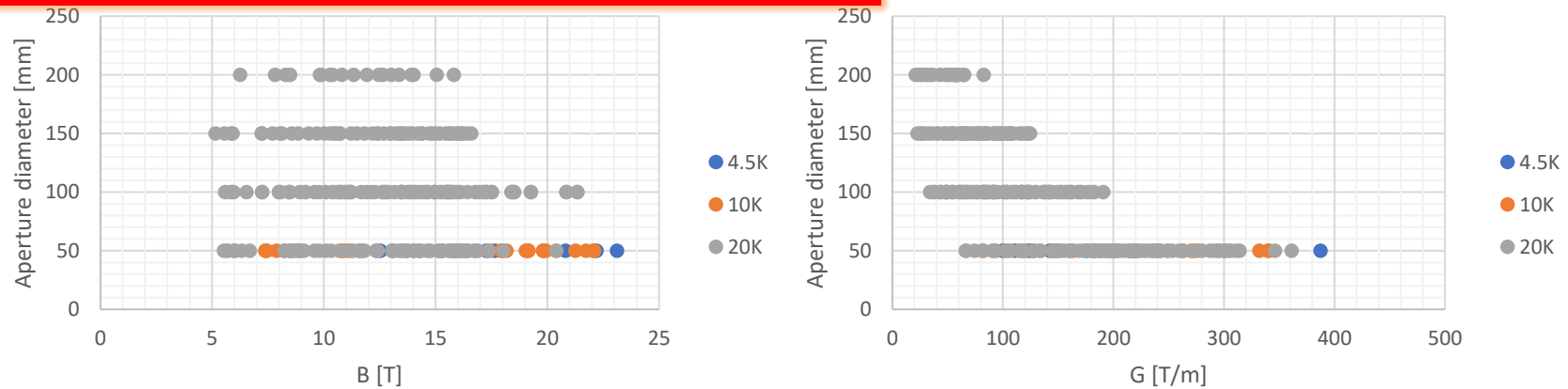


**We should optimize the stress instead of excluding the points manually**

B vs G – only Stress limit



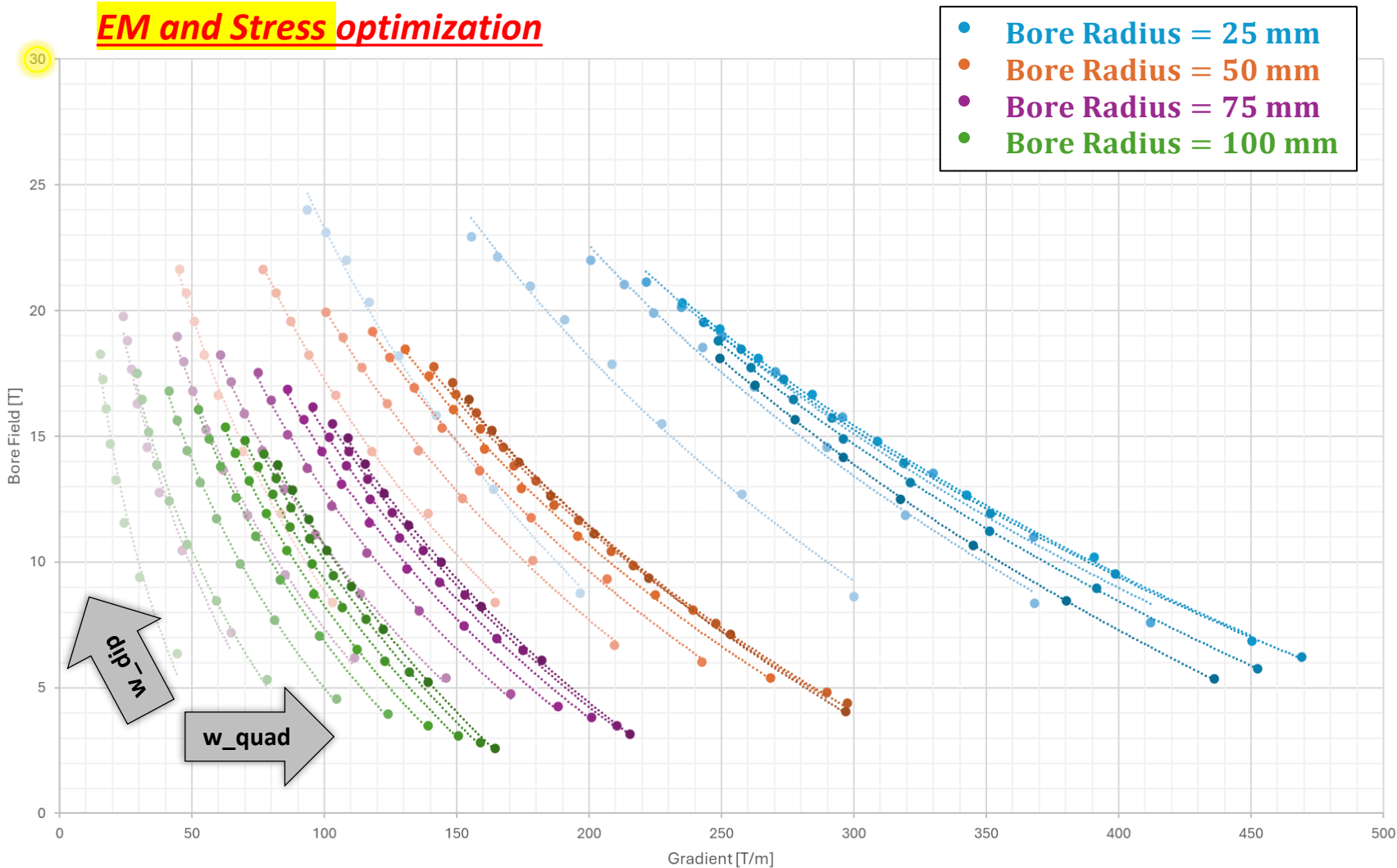
A vs G – only Stress limit





# EM. AND STRESS B-G PLOT AT 4.5K

## EM and Stress optimization



Optimize (decrease)  $J_{quad}$  and  $J_{dip}$  to not exceed the maximum stress (400 MPa)

```

.....
while not ( 0.99 < f < 1.01 ):
.....
  read the J from 1% optimization
  → ANSYS input (a1, w_quad, J_quad, w_dip, J_dip)
  Run ANSYS
  ANSYS output →
  if stress > 400:
    f = 400/stress
    J = J * √f
  .....
.....
  
```

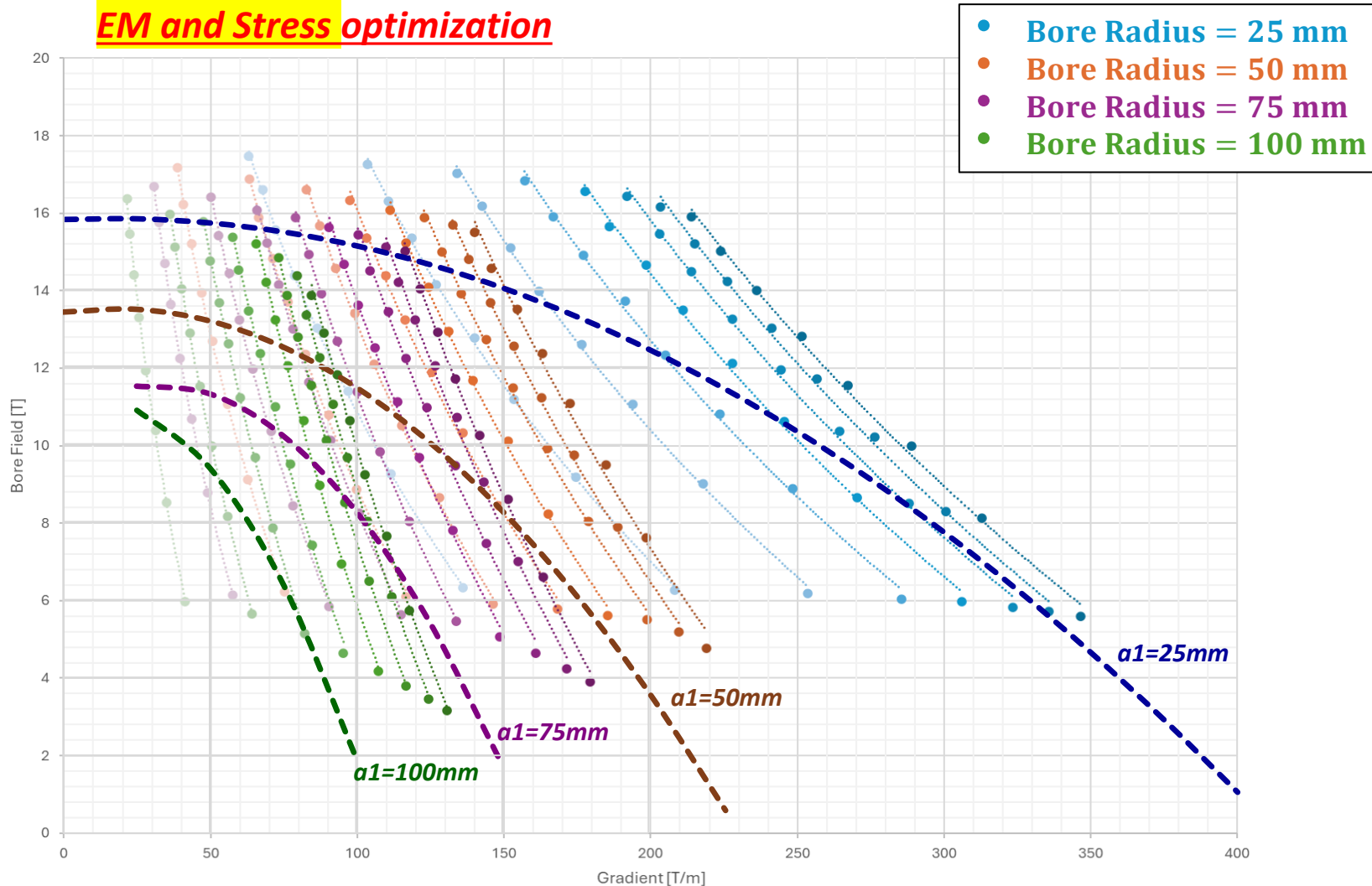
the optimization acts on  $J_{quad}$  and  $J_{dip}$  with quadratic dependence of J on stress, and the cycle closes when the stress is below 400 MPa on both the dipole and the quadrupole.



**Limitations on cost are still missing**

# FINAL B-G PLOT AT 20K

## EM and Stress optimization



Optimize (decrease)  $J_{quad}$  and  $J_{dip}$  to not exceed the maximum stress (400 MPa)

```

.....
while not ( 0.99 < f < 1.01 ):
.....
  read the J from 1% optimization
  → ANSYS input (a1, w_quad, J_quad, w_dip, J_dip)
  Run ANSYS
  ANSYS output →
  if stress > 400:
    f = 400/stress
    J = J * √f
  .....
.....

```

the optimization acts on  $J_{quad}$  and  $J_{dip}$  with quadratic dependence of J on stress, and the cycle closes when the stress is below 400 MPa on both the dipole and the quadrupole.



**Limitations on cost are still missing**