



Fermi National Accelerator Laboratory

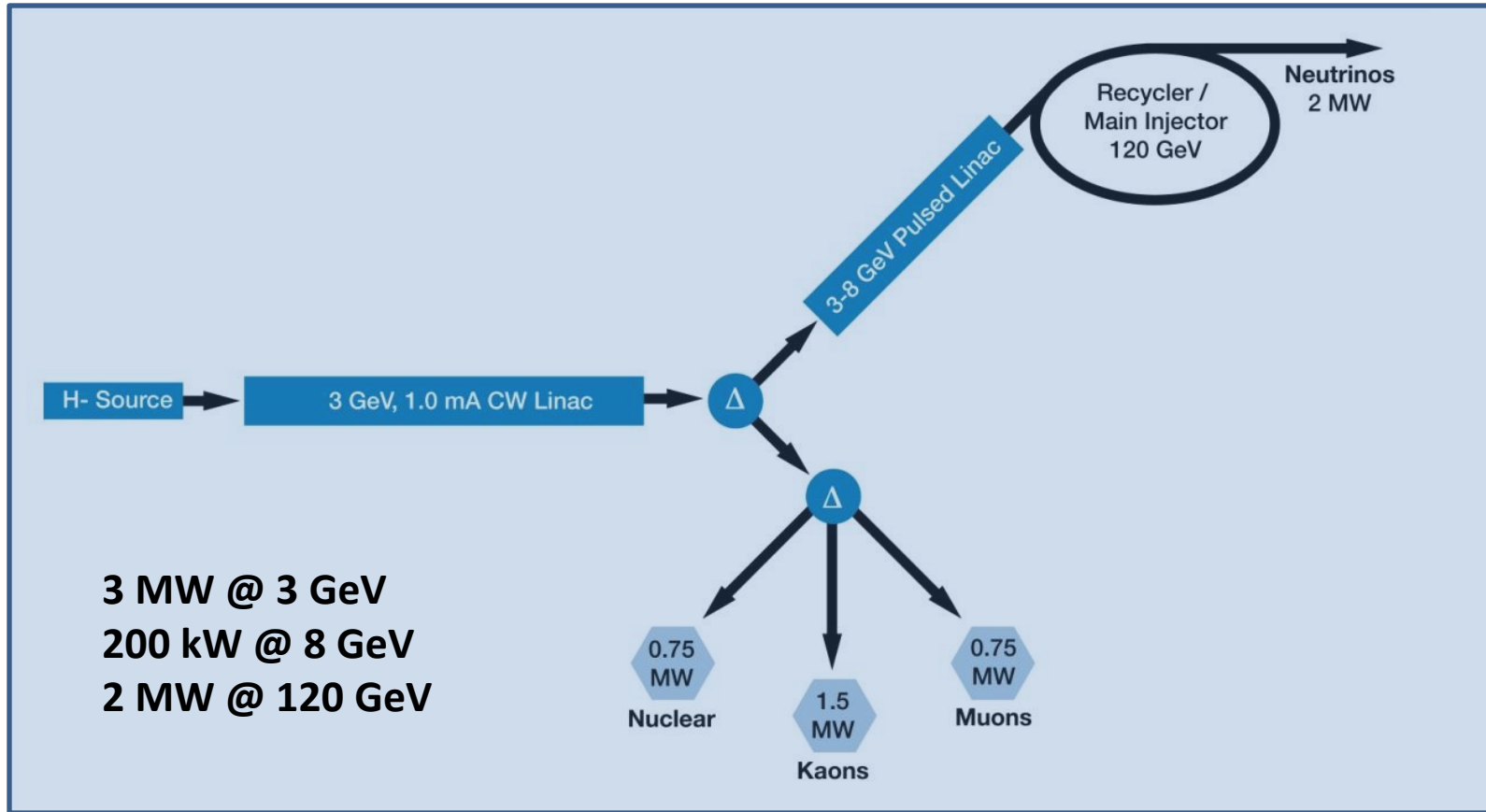
# **A beam splitter for the Project X**

**LHC Crab Cavity Meeting**

**11/15/2011**

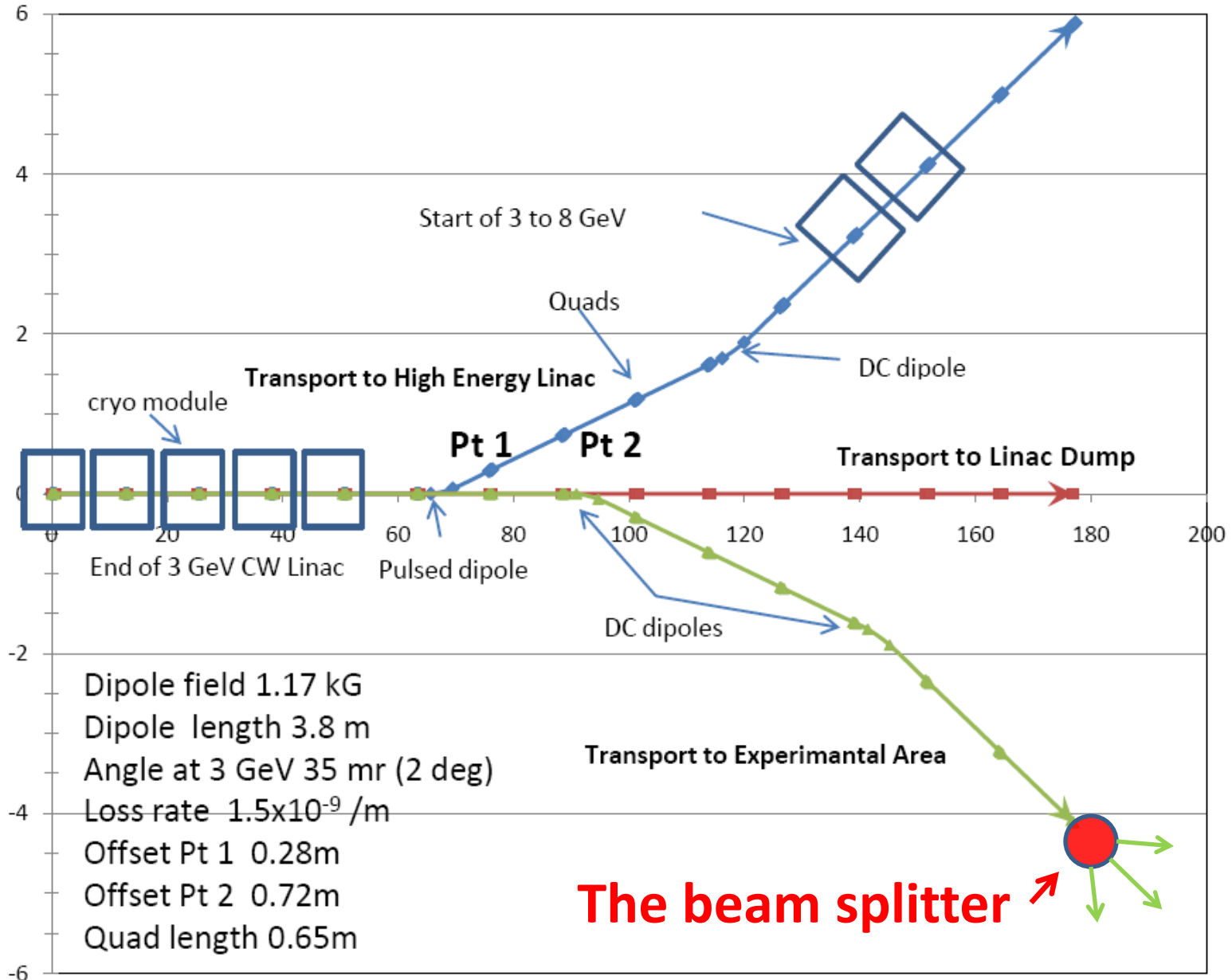
**V. Yakovlev and M. Champion**

# Project X multi-experiment facility:

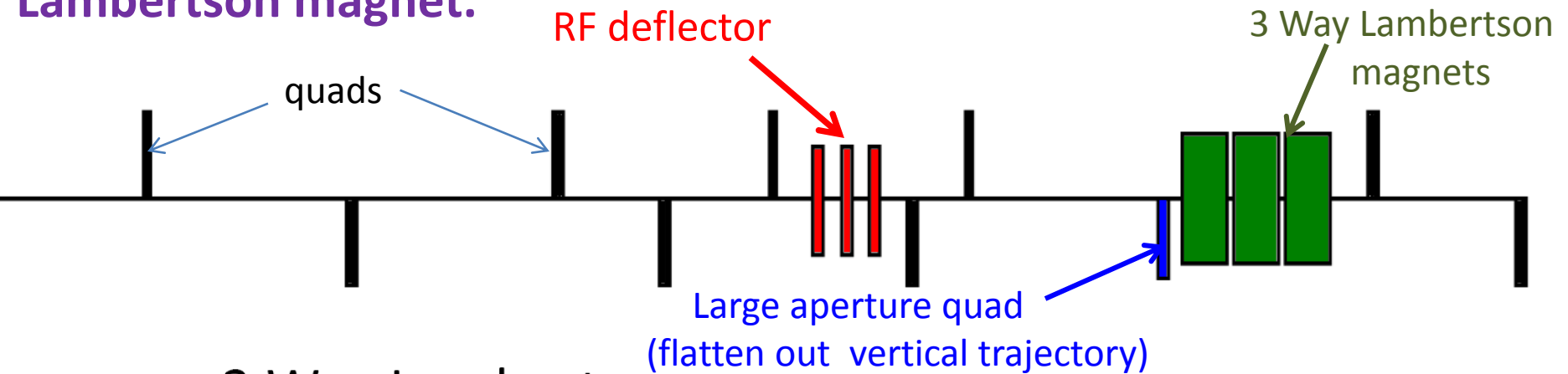


- 3-GeV, 1-mA CW linac provides beam for rare processes program ~3 MW;
- flexible provision for beam requirements supporting multiple users;
- <5% of beam is sent to the Main Injector.

# 3 GeV Switchyard

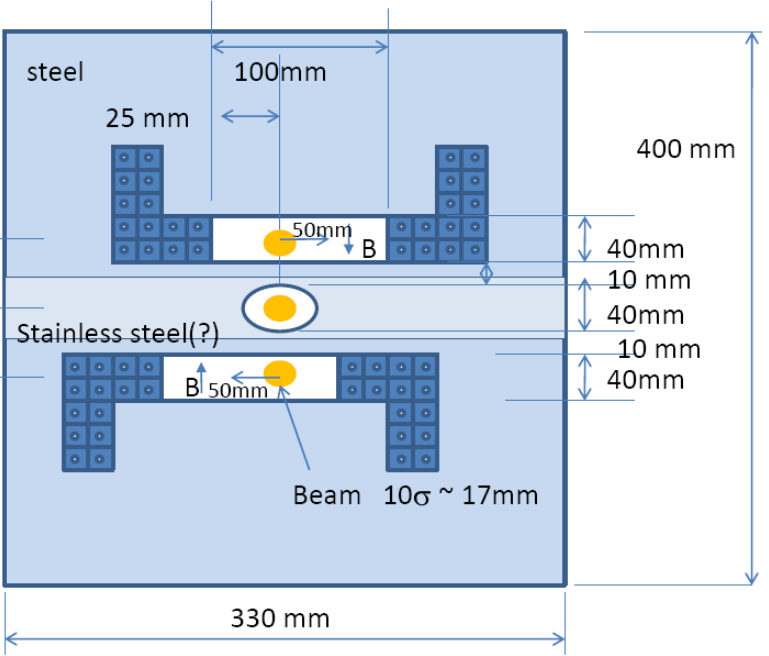


The bunches are separated in vertical direction by RF cavity by 50 mm ( $\sim 25 \sigma_t$ ) and then deflected in horizontal direction by 3 Way Lambertson magnet.

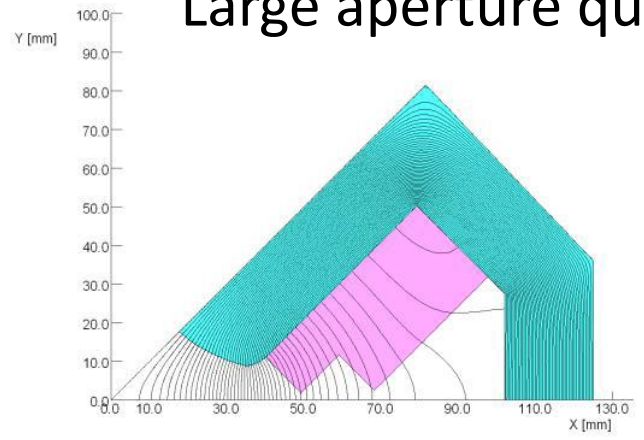


### 3 Way Lambertson

Beam = Hminus  
 K.E. = 3 GeV  
 $\beta\rho = 127.58\text{kG}\cdot\text{m}$   
 $B = 1.2\text{kG}$   
 Length = 2.5 meters  
 $BL = 3\text{ kG}\cdot\text{m}$   
 Angle = 23.5 mr  
 $I \sim 275\text{A}/\text{pole}$   
 Aperture  $\sim 20 \sigma$   
 Need 3 short magnets  
 Or 1 long magnet 7.5m



### Large aperture quad



Example from RCS:  
 5.5T/m (inj)  
 17.5T/m peak (670A)  
 Only need:  $\sim 2\text{ T/m}$  gradient

# Operating scenario at the bunch sequence

## frequency of 162.5 MHz:

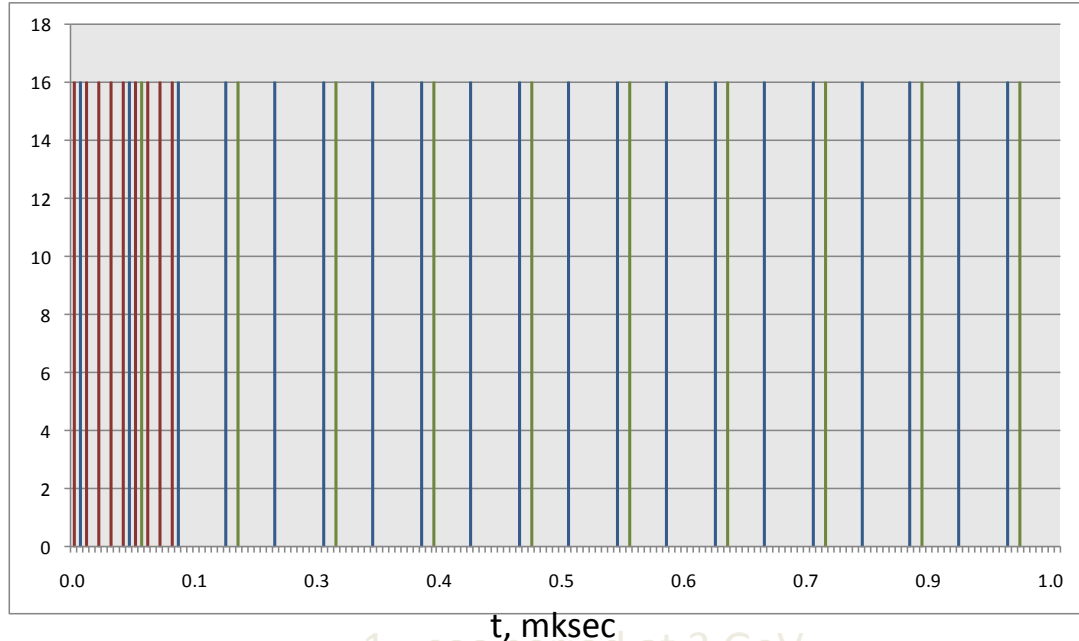
- RF separator directs

Muon pulses (16e7) 81.25 MHz, 100 nsec at 1 MHz 700 kW;

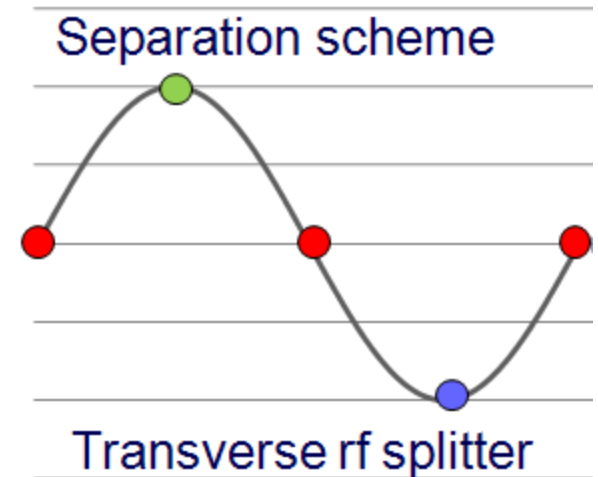
Kaon pulses (16e7) 20.3 MHz 1540 kW

Nuclear pulses (16e7) 10.15 MHz 770 kW

- Deflecting structure should operating at the frequency  $f_0(m \pm 1/4)$ , where  $f_0$  is the bunch sequence frequency ( $f_0=162.5$  MHz).

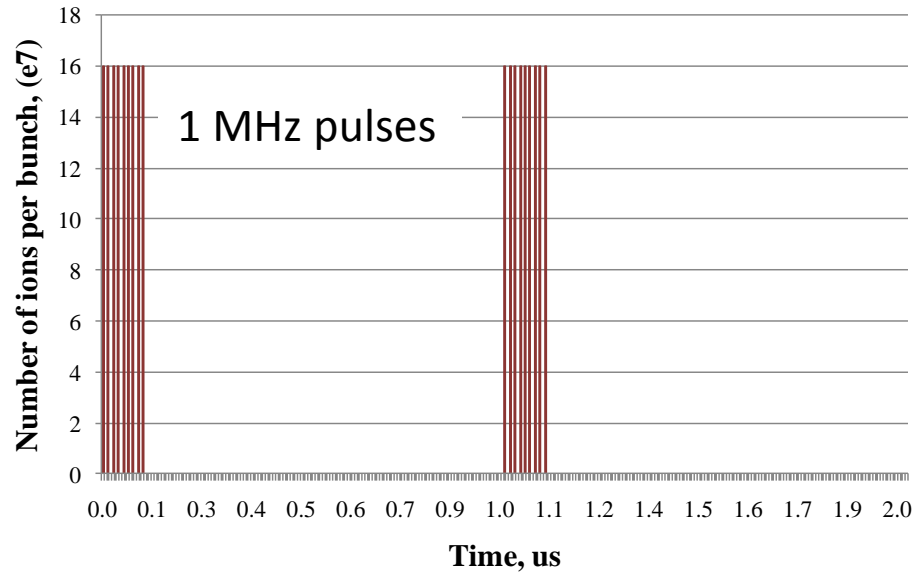


1  $\mu$ sec period at 3 GeV

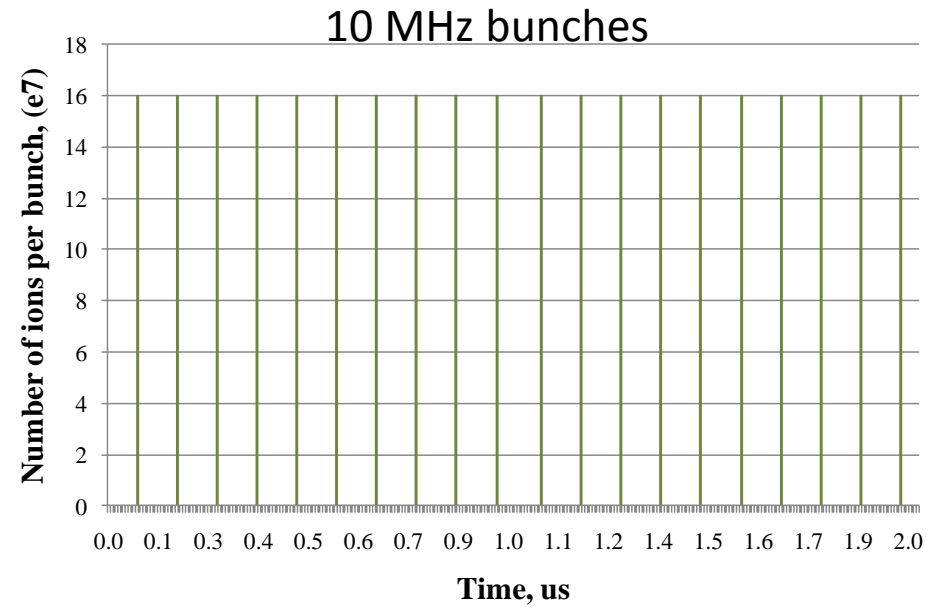


# Beam after splitter

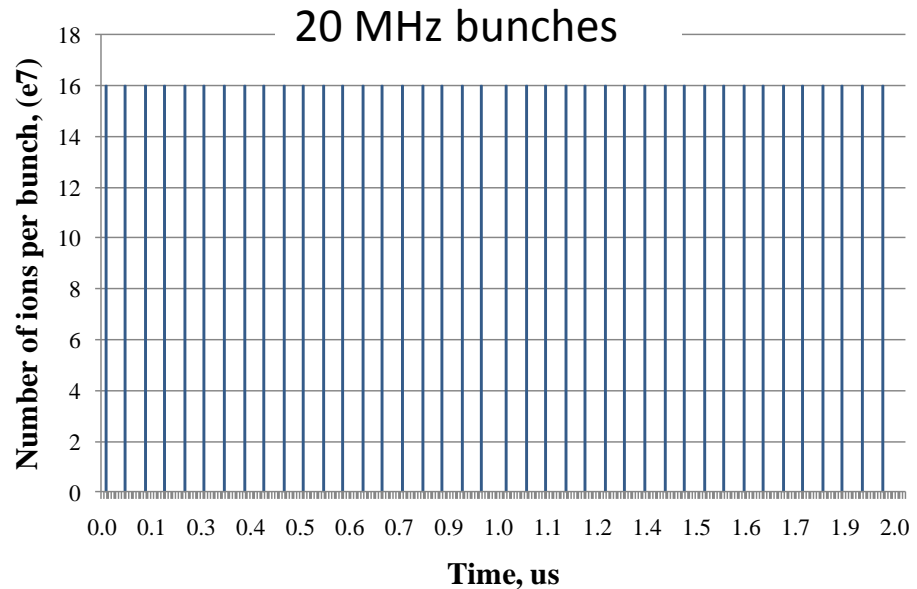
Muon pulses



Nuclear pulses



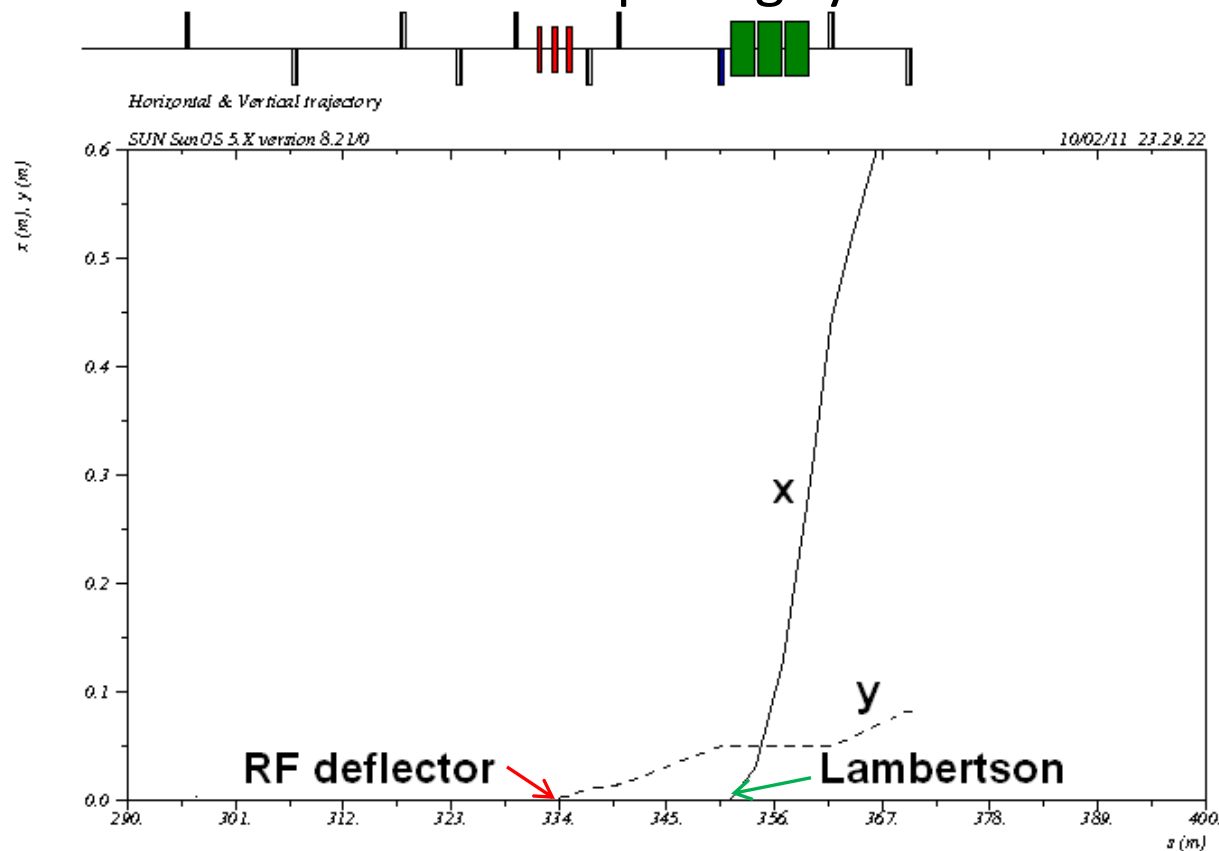
Kaon pulses



# Requirements for RF kick:

Trajectory of the deflected beam in the spitting system:

- Three Lambertson magnets provide about 70 mrad bend to produce 285 mm at end of Lambertson.
- RF Separator requires total vertical kick of +/-2.5 mrad to match into bending aperture of 3-way Lambertson.



RF kick:

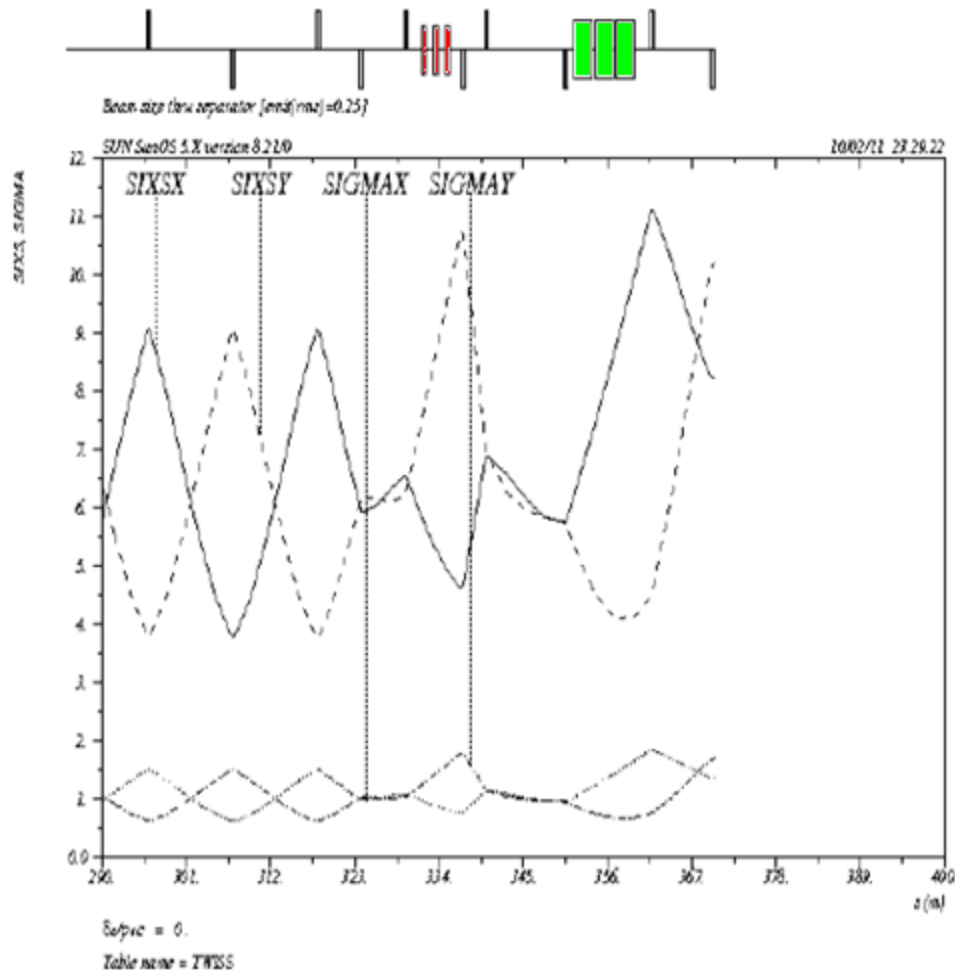
$$\Delta p_{\perp} c = 2.5 \times 10^{-3} p_{\parallel} c = 10 \text{ MeV}$$

D. Johnson

The cavities should be superconducting because of the relatively high voltage requirement and the continuous wave operation.

# Aperture requirements for deflecting RF cavity:

Beam transverse sizes in the beam splitting system.



- Beam sigma < 2 mm for  $\epsilon_t$  (rms) 0.25 mm-mr
- Typical quad apertures ~75mm diameter
- Typical dipole gap ~ 50 mm

RF cavity aperture of 70-80 mm is OK



## Frequency requirements:

- Operating frequency of the deflecting RF structure is limited
  - by the bunch longitudinal size - at high frequency;**
  - by the cavity transverse size - at low frequency.**
- Deflecting structure should operate at the frequency of  $f_0(m \pm 1/4)$ , where  $f_0$  is the bunch sequence frequency, 162.5 MHz.
- The frequencies of **365.625 MHz** ( $m=2, +1/4$ ) or **446.875 MHz** ( $m=3, -1/4$ ) are reasonable possibilities.

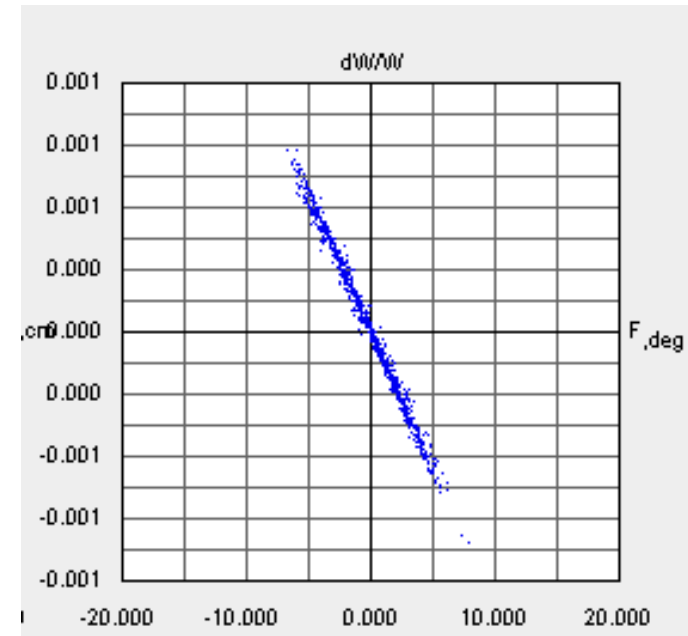
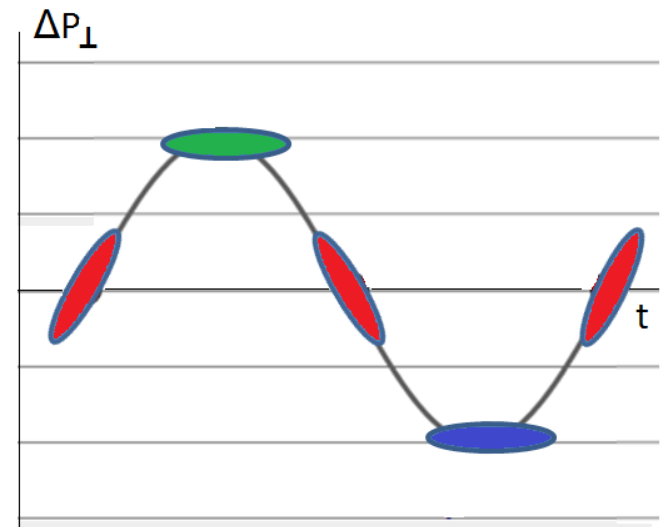
# Transverse emittance dilution caused by the splitting cavity:

➤ The magnitude of the kick spread inside the bunch depends on the bunch length;

▪ For the *non-deflected* bunch  $\theta_{\text{rms}} \sim 2\pi\theta_{\text{RF}} \times (\sigma_z/\lambda)$ , where  $\sigma_z$  is the rms bunch length and  $\lambda$  is the RF wavelength (for 447 MHz  $\lambda = 0.67\text{m}$ ) and  $\theta_{\text{RF}} = 2.5$  mrad is deflecting angle.

▪ For the *deflected* bunch  $\theta_{\text{rms}} \sim (\sigma_z/\lambda)^2$  – negligible;

➤ Due to the bunch sheering in transport to the cavity ( $\sim 300\text{m}$ ) the rms bunch length is  $\sim 3.5$  mm, so  $\theta_{\text{rms}} \sim 2\pi(2.5\text{mrad})(3.5\text{mm}/.67\text{m}) \sim 0.082$  mrad.



➤ The initial rms normalized emittance  $\epsilon_{0y}$  is 0.28 mm-mrad.

➤ The new emittance is given by  $\epsilon_y = [\epsilon_{0y}^2 + \epsilon_{0y} \cdot \beta \theta_{rms}^2 \cdot (\gamma\beta)]^{1/2}$ , where  $\beta$  (46m) is the lattice function at the RF cavity, and  $\gamma\beta$  ( $\sim 4$ ) is the relativistic factor.

➤ The increase in the normalized rms emittance is determined by  $\Delta\epsilon_y = \beta \theta_{rms}^2 (\gamma\beta) \sim 1.08$  mm-mrad

This gives an emittance dilution factor of 3 for non-deflected bunches.

- Muon experiments need small emittance. Deflected beam is to be used.
- For other experiments it's OK.
- 447 MHz is OK.
- This problem does not exist for LHC CC, it is specific for PX.

# Amplitude and phase stability requirements:

- Amplitude stability:

$$\frac{\delta \varepsilon_{\perp}}{\varepsilon_{\perp}} = \frac{\delta y}{\sigma_y} = \frac{\delta y}{\Delta y} \cdot \frac{\Delta y}{\sigma_y} = \frac{\delta U_{kick}}{U_{kick}} \cdot \frac{\Delta y}{\sigma_y} \ll 1;$$

or

$$\frac{\delta U_{kick}}{U_{kick}} \ll \frac{\sigma_y}{\Delta y}.$$

If  $\sigma_y = 2 \text{ mm}$ ,  $\Delta y = 50 \text{ mm}$ ,  $\delta U_{kick}/U_{kick} \ll 4\%$ .

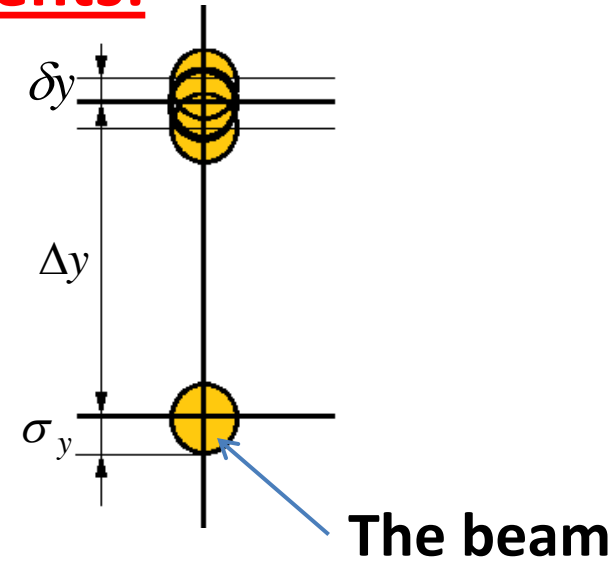
$\delta U_{kick}/U_{kick} \leq 1\%$  is OK.

- Phase stability:

$$\frac{\delta \varepsilon_z}{\varepsilon_z} \approx \frac{\delta \varphi}{\sigma_{\varphi}} \ll 1; \quad \sigma_{\varphi} = \frac{2\pi\sigma_z}{\lambda};$$

If  $\sigma_z = 3.5 \text{ mm}$ ,  $\lambda = 0.67 \text{ m}$ ,  $\Delta\varphi \ll 2^\circ$ .

$\Delta\varphi \leq 0.5^\circ$  is OK.



# Transverse alignment requirements:

- Energy spread is caused by transverse misalignment of the cavity;
  - Energy change because transverse misalignment of the cavity;
  - Input power increase in order to compensate voltage induced by the beam.
  - Excitation of dipole SOM/HOMs .
- 

- Energy spread:

$$\delta E = (2\pi)^2 U_{kick} \Delta y \sigma_z / \lambda^2 \ll \frac{\varepsilon_z}{\sigma_z}; \quad (\text{from Panofsky-Wentzel theorem})$$

$$\Delta y \ll \frac{\varepsilon_z \lambda^2}{(2\pi)^2 U_{kick} \sigma_z^2}.$$

if  $\varepsilon_z = 1 \text{ keV} \times \text{nsec}$  or  $30 \text{ keV} \times \text{cm}$ ,  $\sigma_z = 3.5 \text{ mm}$ ,  $\lambda = 0.67 \text{ m}$ ,  $U_{kick} = 10 \text{ MeV}$ ,  
 $\Delta y \ll 3 \text{ cm}$  – not a problem.  $\Delta y = \underline{\underline{2-3 \text{ mm}}}$  is OK.

- Energy Change:

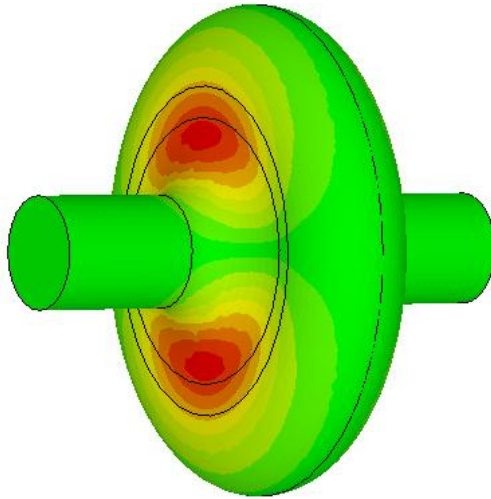
$$\Delta E = 2\pi U_{kick} \Delta y / \lambda = 330 \text{ keV at } E=3 \text{ GeV} - \text{OK}$$

for  $\Delta y \leq 2 \text{ mm}$ .

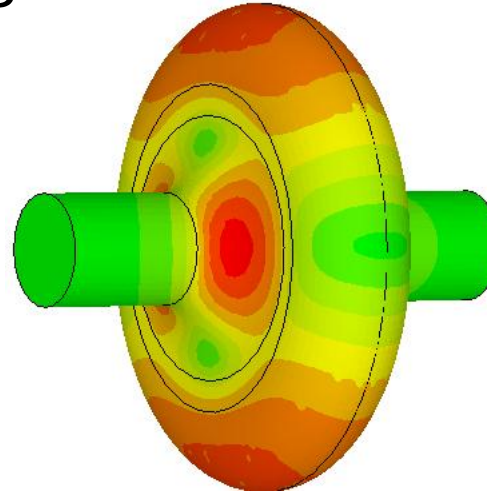
- In contrast to LHC CC, the induced voltage at operating mode is small because the operating frequency does not coincide to harmonics of the bunch sequence frequency – OK.

- Dipole SOM/HOM excitation is not a problem because of a small beam current;  $\Delta y \leq 2 \text{ mm}$  is OK.

# Fermilab KEK-type design of 406 MHz deflecting cavity\*:



Distribution of E field



Distribution of H field

| Parameters        |      | Units            |
|-------------------|------|------------------|
| $R/Q$             | 27   | Ohm              |
| $G$               | 255  | Ohm              |
| $G \times (R/Q)$  | 4845 | Ohm <sup>2</sup> |
| $B_{sp}/V_{kick}$ | 19.2 | mT/MeV           |
| $E_{sp}/V_{kick}$ | 7.8  | MV/m/MeV         |
| Longitudinal size | 440  | mm               |
| Vertical size     | 865  | mm               |
| Horizontal size   | 962  | mm               |
| Aperture          | 220  | mm               |

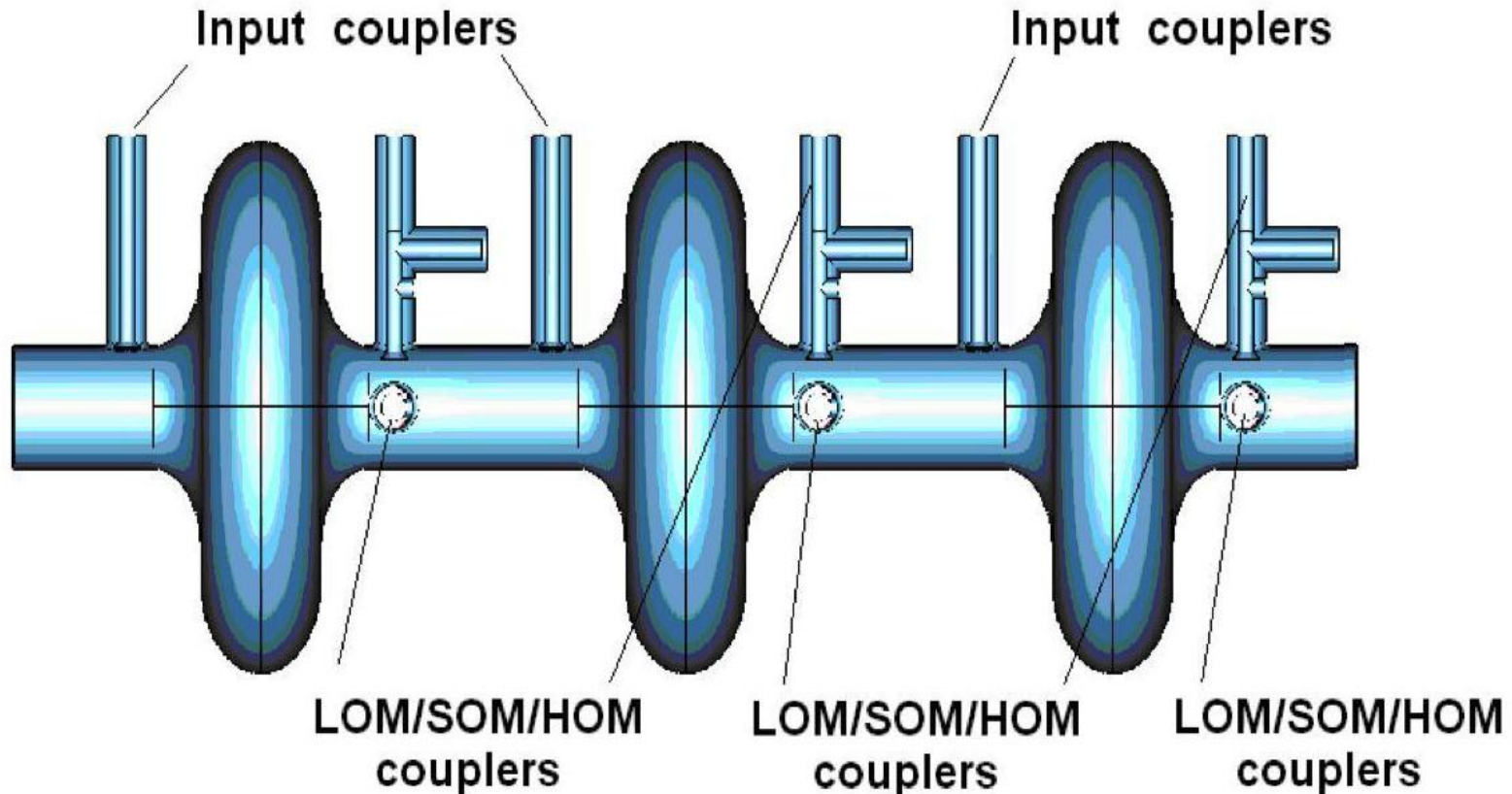
| MONOPOLE |       | DIPOLE1 |       | DIPOLE2 |       |
|----------|-------|---------|-------|---------|-------|
| F,MHz    | R/Q,Ω | F,MHz   | R/Q,Ω | F,MHz   | R/Q,Ω |
| 289.2    | 118   | 406.25  | 27.3  | 427.9   | 25.2  |
| 557.1    | 1.5   | 529.1   | 6.2   | 528.3   | 6.1   |
| 635.7    | 6     | 691.4   | 0.16  | 695.7   | 0.04  |
| 692.6    | 0.001 | 726.7   | 0.03  | 743.6   | 0.14  |
| 730.1    | 16    | 759.5   | 2.8   | 759.4   | 2.5   |
| 825.2    | 0.002 | 797.6   | 0.08  | 797.8   | 0.12  |

$$*R/Q = V_{kick}^2 / (2\omega W)$$

High order modes

\*Design developed for previous variant with 325 MHz bunch sequence frequency

- In order to achieve the kick of 10 MeV one needs **3** cavities.
- The kick per cavity is **3.3** MeV.
- The surface magnetic field is **63** mT, that is OK for this frequency.
- The length of the cavity+power coupler +HOM couplers is about **1** m.
- The total length of the deflecting RF structure is **~3.5** m.
- Transverse size is about **~1** m.

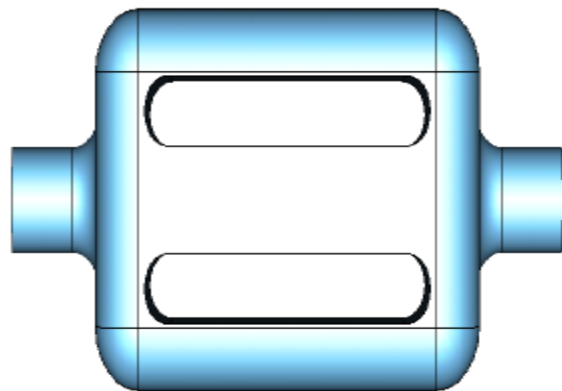
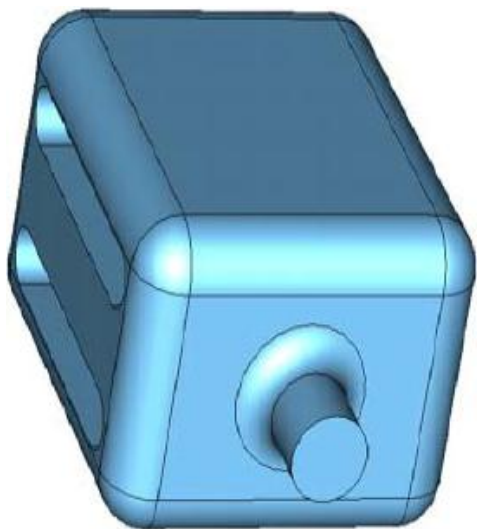


Most probably, LOM/SOM/HOM couplers are not necessary because of small beam current.



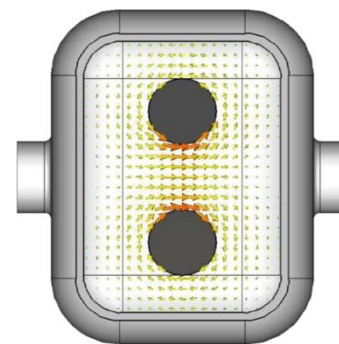
# Alternative deflecting cavity version: TEM rectangular parallel-bar cavity (PBC)

(Jean Delayen, Center for Accelerator Science, Old Dominion University)



- Much lower cryo losses (~3 times);
- Much smaller transverse dimensions;
- Surface fields are about the same as for KEK-type cavity;
- The concept is not tested yet.

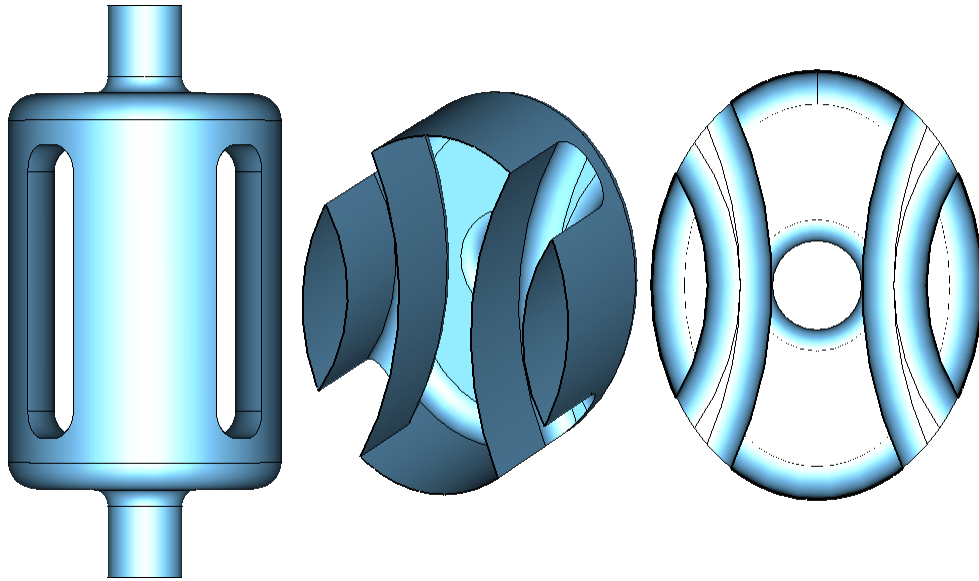
| Parameters        |       | Units            |
|-------------------|-------|------------------|
| $R/Q$             | 206.7 | Ohm              |
| $G$               | 74.1  | Ohm              |
| $G \times (R/Q)$  | 15316 | Ohm <sup>2</sup> |
| $B_{sp}/V_{kick}$ | 21.0  | mT/MeV           |
| $E_{sp}/V_{kick}$ | 5.9   | MV/m/MeV         |
| Longitudinal size | 445   | mm               |
| Vertical size     | 383   | mm               |
| Horizontal size   | 300   | mm               |
| Aperture          | 84    | mm               |



TEM field in the BPC with round bars

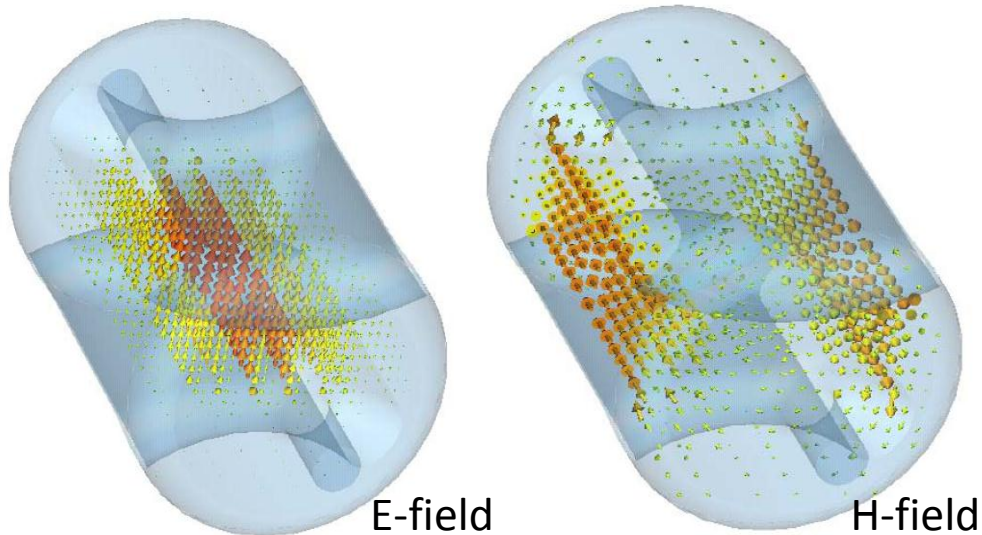
Niowave Inc. submitted Phase I SBIR proposal to DoE

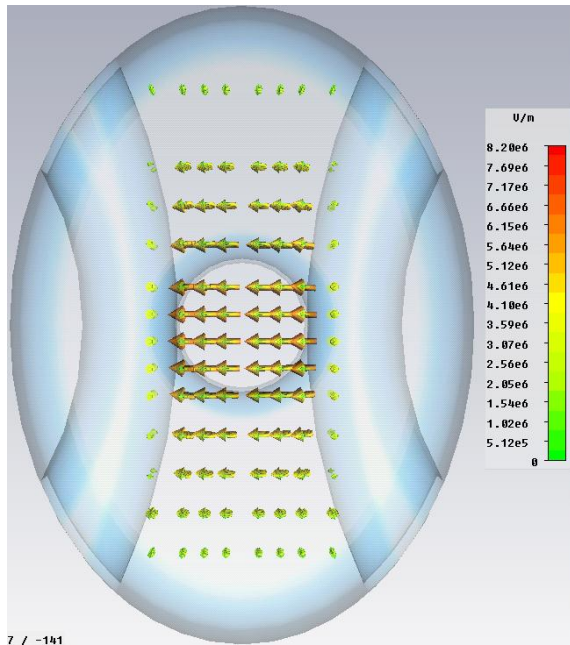
# Parallel - bar ellipsoidal cavity (J. Delayen, ODU)



| Parameters        |       | Units            |
|-------------------|-------|------------------|
| $R/Q$             | 132   | Ohm              |
| $G$               | 108   | Ohm              |
| $G \times (R/Q)$  | 14256 | Ohm <sup>2</sup> |
| $B_{sp}/V_{kick}$ | 16.0  | mT/MeV           |
| $E_{sp}/V_{kick}$ | 7.2   | MV/m/MeV         |
| Longitudinal size | 445   | mm               |
| Vertical size     | 406   | mm               |
| Horizontal size   | 295   | mm               |
| Aperture          | 84    | mm               |

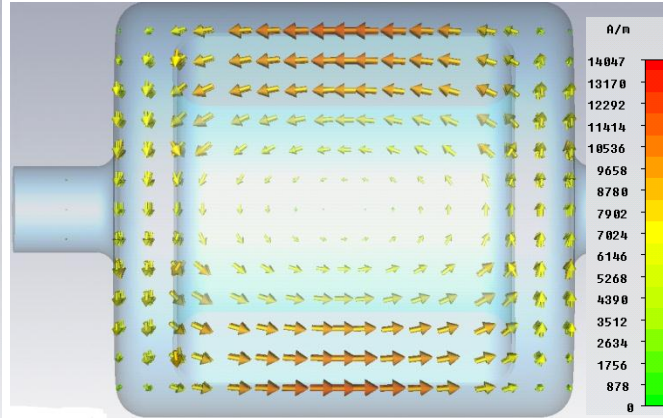
- Parameters are about the same as for rectangular PBC



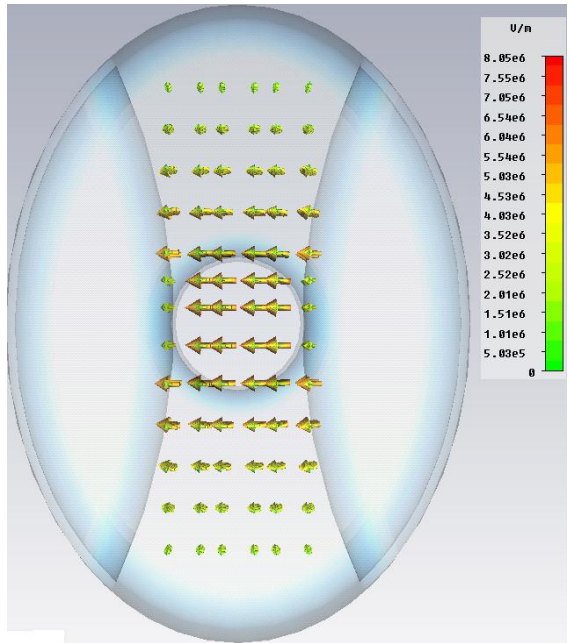
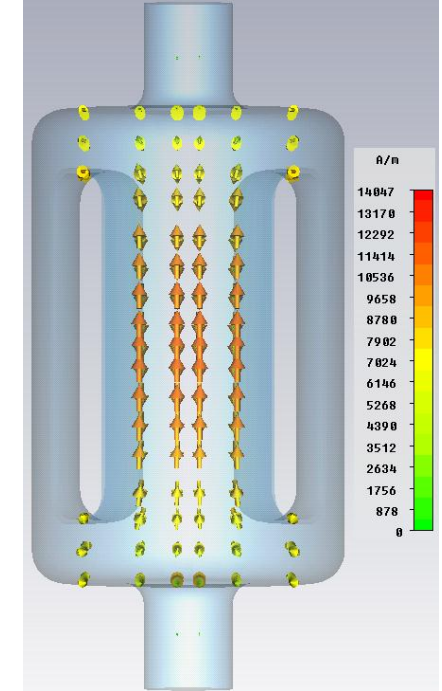


E-Field

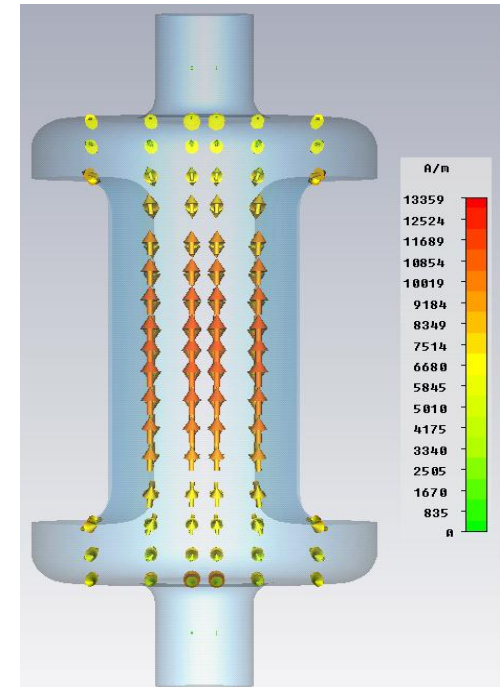
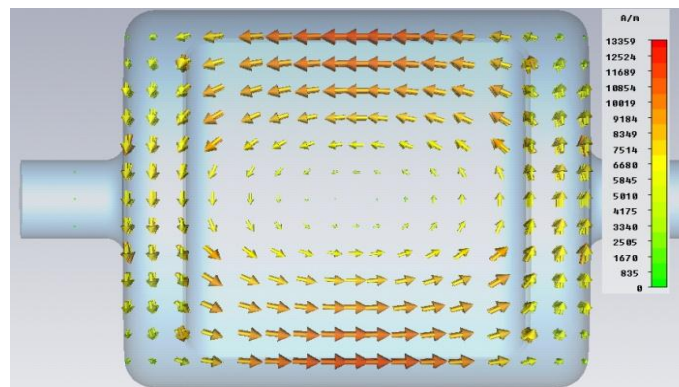
# ORIGINAL ODU VARIANT

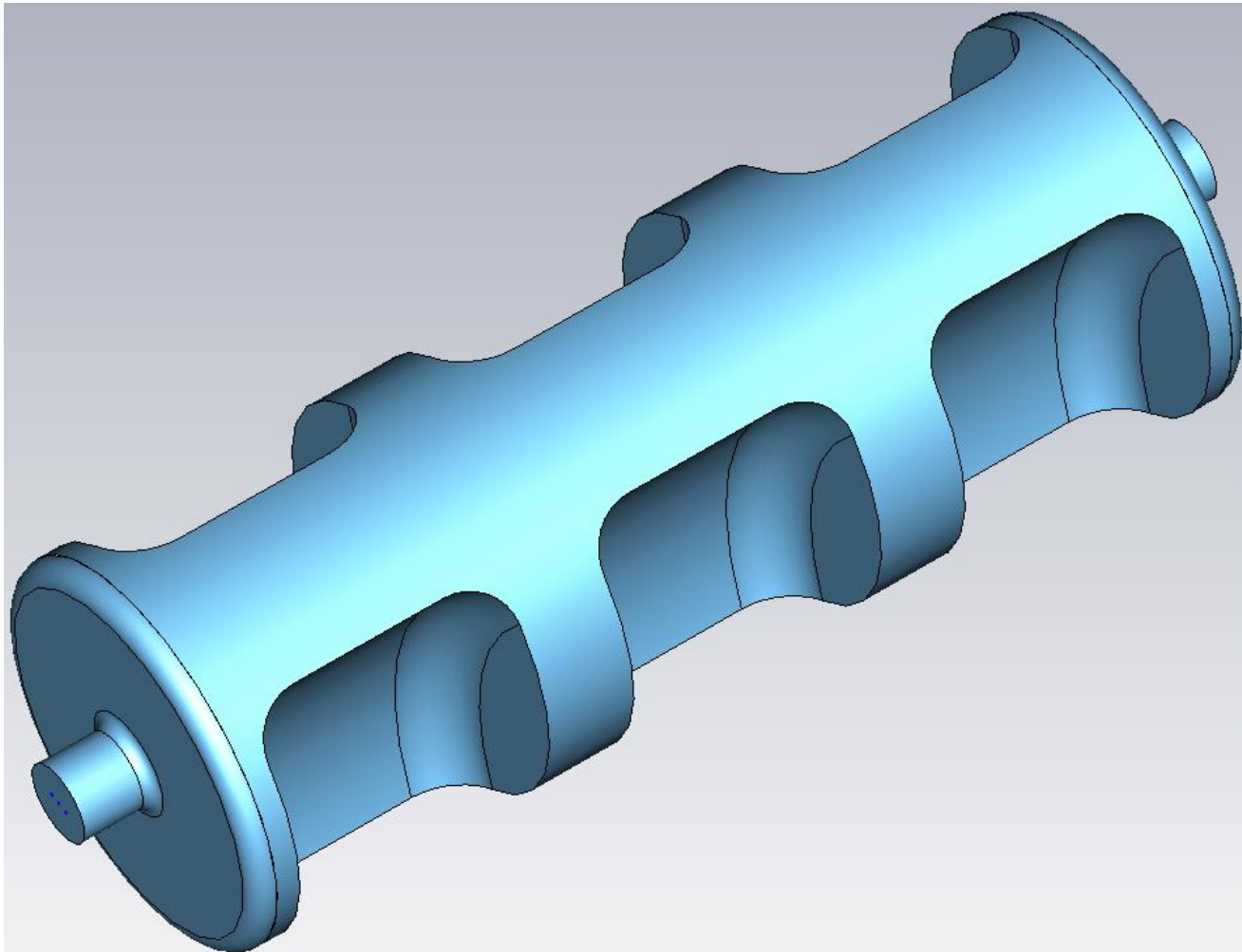


H-Field



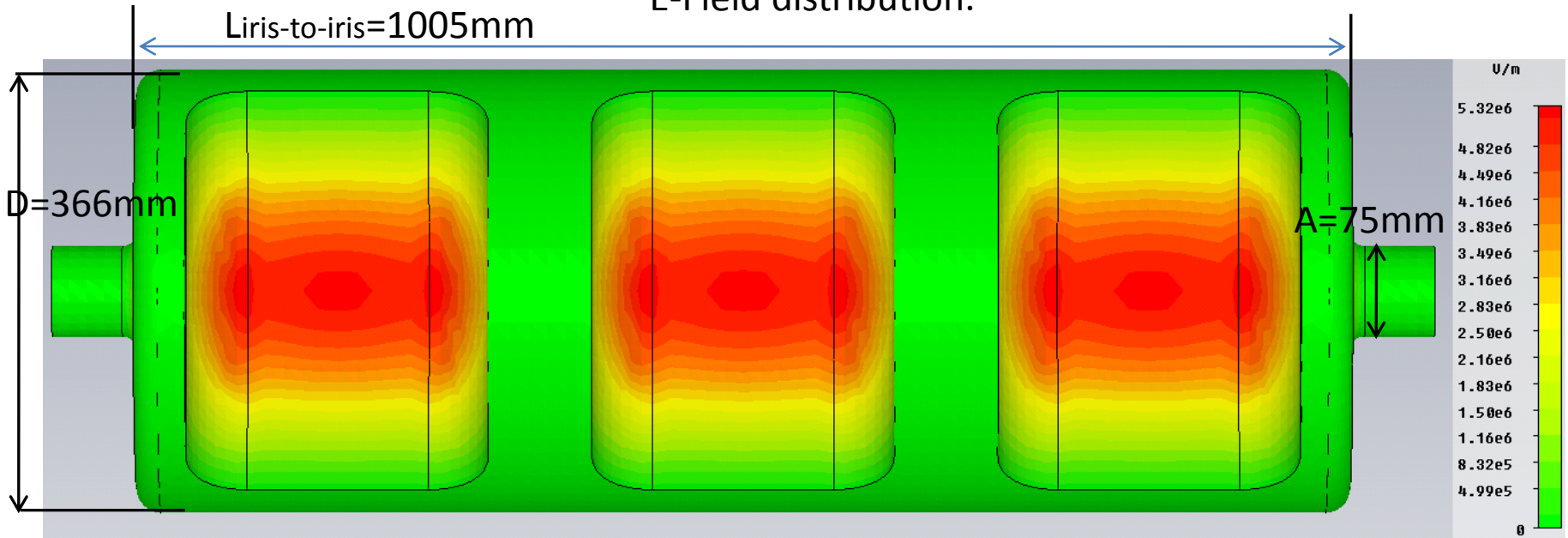
# VARIANT WITHOUT BARS



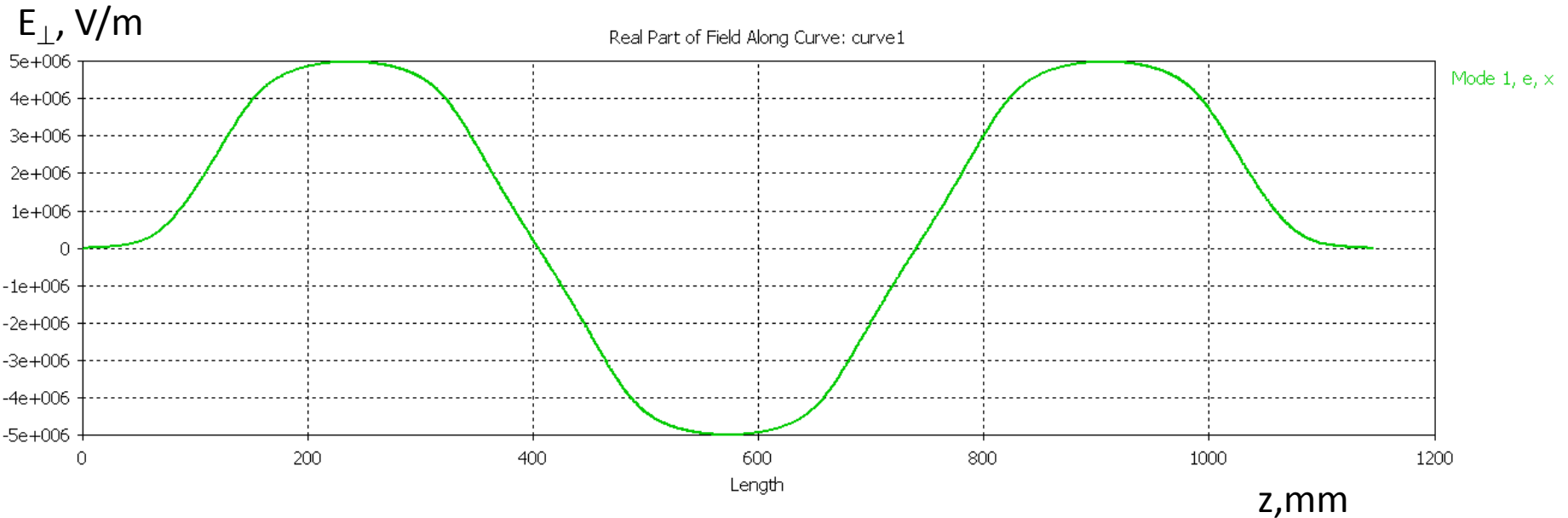


Further development of the ODU TE cavity: FNAL  
Squashed  $TE_{113}$  deflecting cavity for Project X.

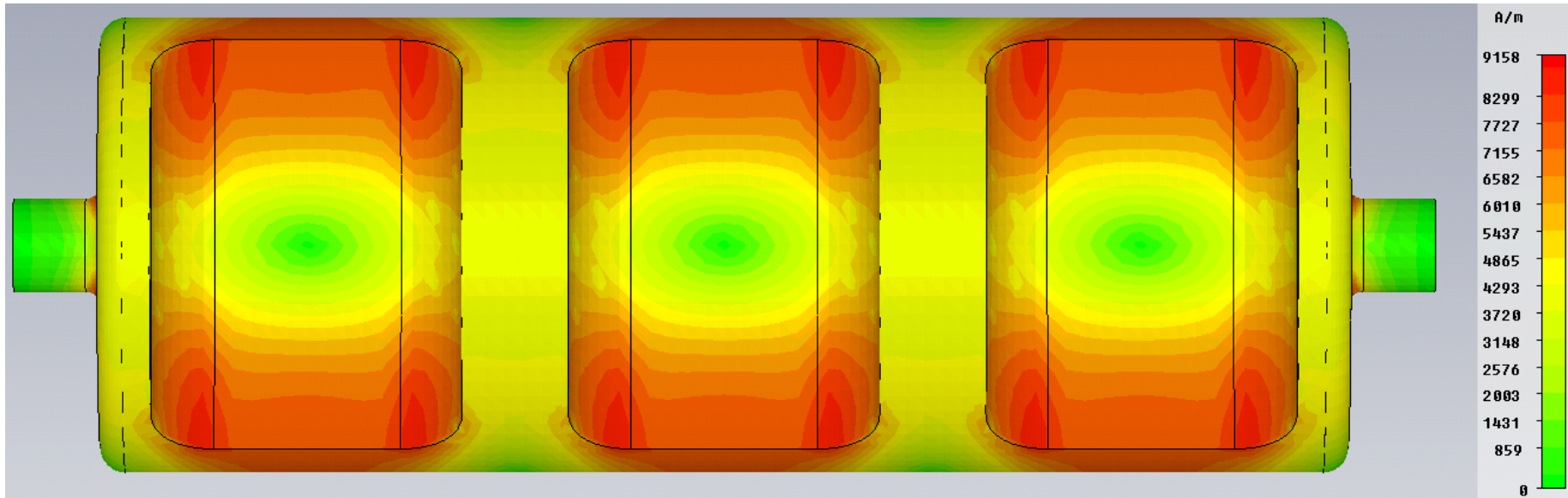
# E-Field distribution.



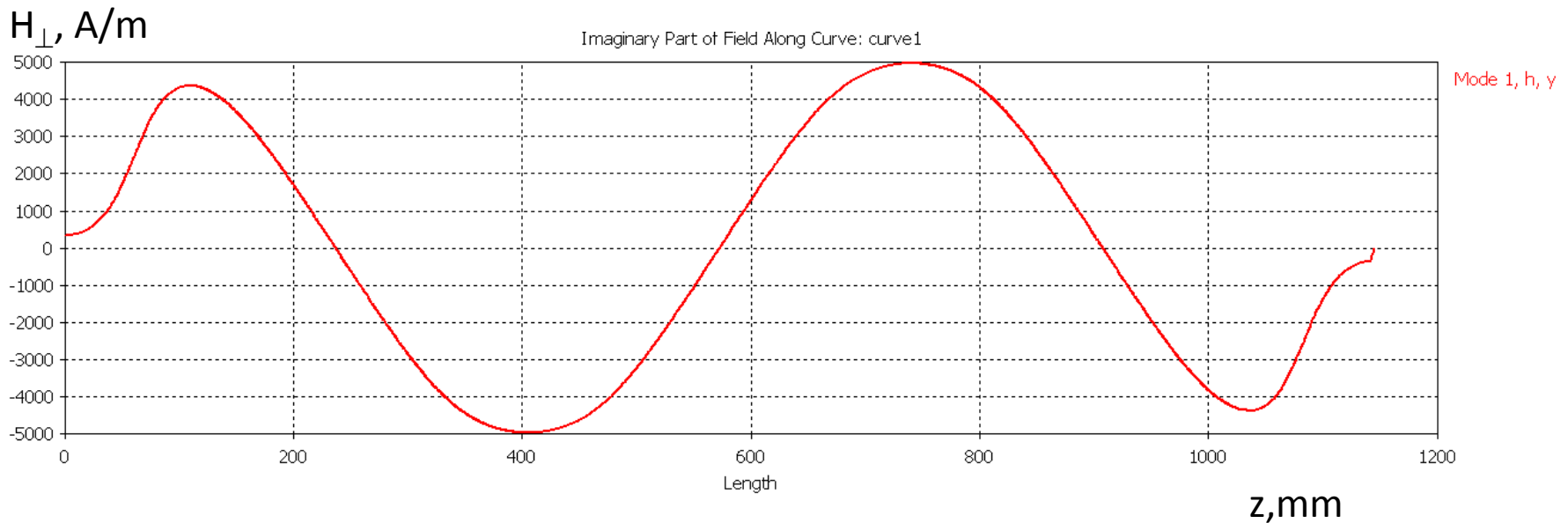
Transverse electric field  $E_{\perp}$  distribution along the axis. Stored energy is 1 J.



# H-Field distribution.



Transverse magnetic field  $H_{\perp}$  distribution along the axis. Stored energy is 1 J.



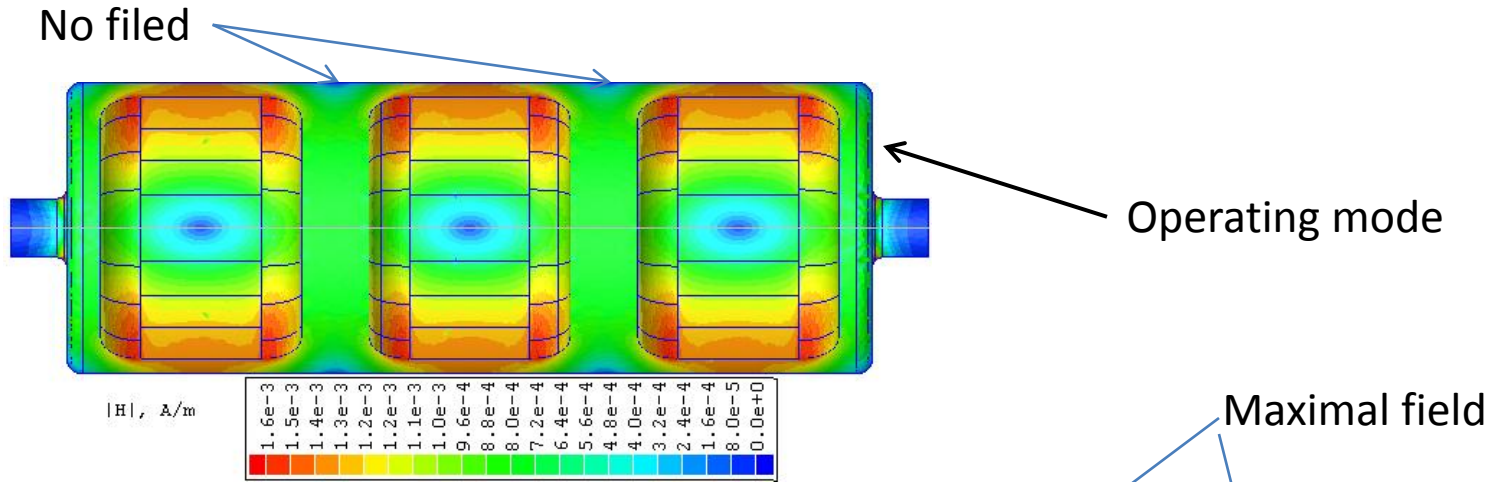
|                          |                   |
|--------------------------|-------------------|
| F , MHz                  | 447               |
| Mode                     | TE <sub>113</sub> |
| R/Q* , Ω                 | 500               |
| G, Ω                     | 117               |
| Vkick, MeV               | 10                |
| Epeak, MV/m              | 34                |
| Bpeak, mT                | 74                |
| Cavity Diameter, mm      | 366               |
| Aperture, mm             | 75                |
| Cavity Length, mm        | 1005              |
| Electric Field Kick, MeV | 15.87             |
| Magnetic Field Kick, MeV | -5.87             |

$$*R/Q = V_{kick}^2 / 2\omega W$$

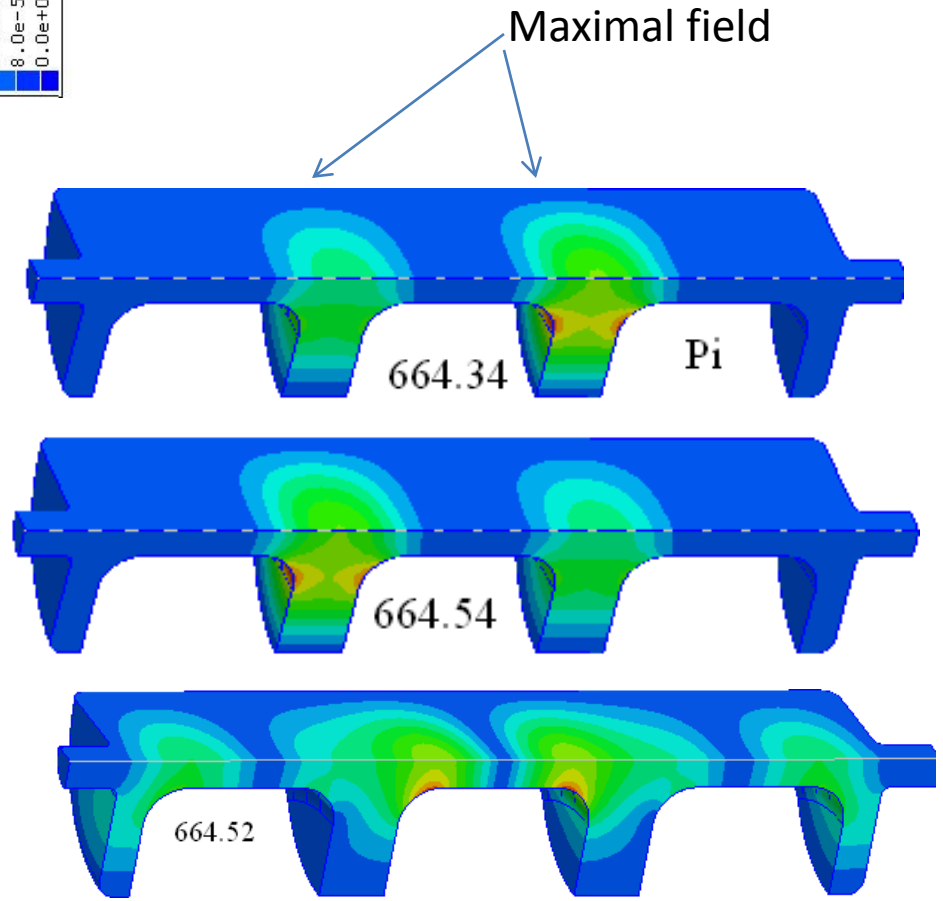
Main parameters of the TE<sub>113</sub> squashed-wall cavity

# HOMs:

Dipole and monopole modes  $F < 1$  GHz



| F, MHz        | $V_{kick}^2/2\omega W$ | $V_{acc}^2/2\omega W$ |
|---------------|------------------------|-----------------------|
| 376.59        | 1.5                    |                       |
| 419.74        | 7.6                    |                       |
| <b>447.30</b> | <b>500</b>             |                       |
| 664.34        |                        | 128.9                 |
| 664.54        |                        | 121.3                 |
| 664.52        | 41.7                   |                       |
| 677.85        |                        | 82.5                  |
| 678.28        |                        | 82.5                  |
| 705.28        | 72.1                   |                       |
| 719.70        | 25.7                   |                       |
| 922.79        | 6.2                    |                       |
| 937.63        | 5.8                    |                       |
| 982.18        | 0.0                    |                       |





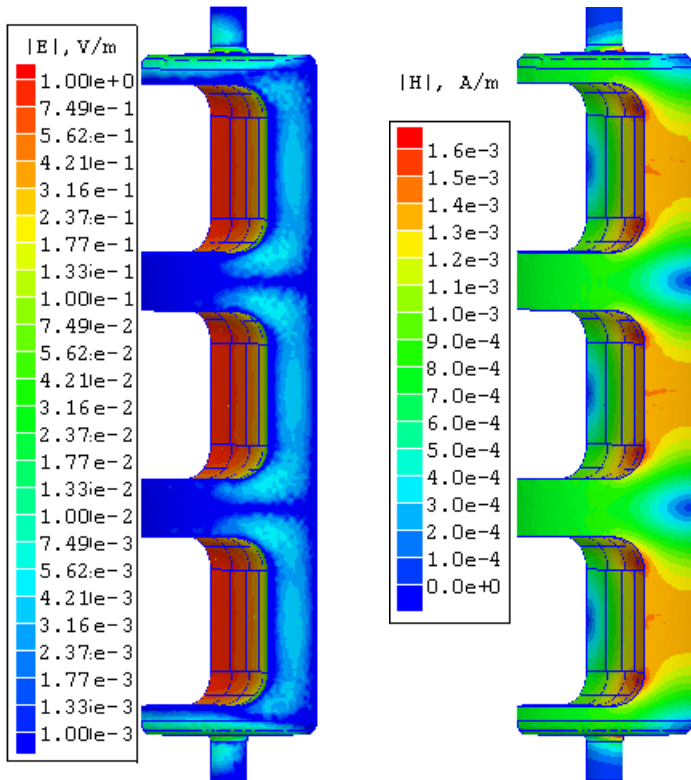
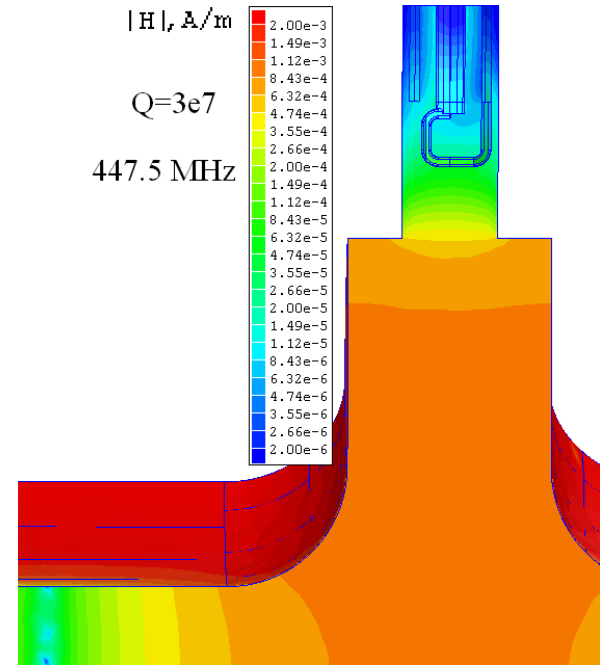
# Power losses on a coupler loop.

447 MHz deflector cavity. Coupler losses at  $V_{kick}=10$  MV.

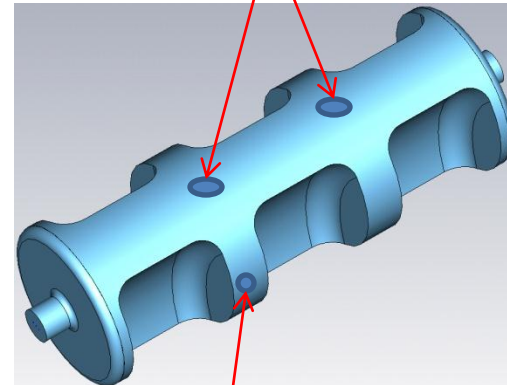
| F, MHz       | $L^*$ , mm | $Q_{ext}$                 | $R_s, \Omega$             | $P_{cav}$ , W | $P_{loop}$ , W |
|--------------|------------|---------------------------|---------------------------|---------------|----------------|
| 447.3        | 193        | $7.6e5$                   | $1E-08$                   | 8.77          | 107.60         |
| 447.3        | 203        | $4.8e6$                   | $1E-08$                   | 8.77          | 17.24          |
| <b>447.3</b> | <b>213</b> | <b><math>3.1e7</math></b> | <b><math>1E-08</math></b> | <b>8.77</b>   | <b>2.62</b>    |

2K

Bandwidth: 15 Hz; Input power in this case is 3.25 kW



HOM damper



Main coupler

$L^*$  is the distance of the loop to the beam axis

- The splitting RF cavity is ~300 m far of the CW linac;
- A separate cryo system is preferable\*;
- Operating temperature ~3.5 K\* (He pressure fluctuations ~0.2 mbar);
- Input power requirements are determined mainly by amplitude of microphonics  $\delta f$ :  $P_{inp} \approx U_{kick}^2 / [(R/Q)_{\perp} \cdot (f/2 \delta f)]$ .  
For squashed-wall cavity for  $\delta f = 15$  Hz  $P_{inp} = 3.25$  kW.
- Microphonics amplitude is determined by
  - Expected He pressure fluctuations ;
  - Cavity mechanical properties, namely,  $df/dP$
- Means necessary to fight microphonics:
  - Minimizing of the He pressure fluctuation;
  - Minimizing of  $df/dP$ ;
  - Minimizing the acoustic energy transmitted to the cavity by external vibration sources;
  - Active piezo control;
  - Cavity over-coupling.

\* A. Klebaner

- A modification of the ODU cavity – a squashed-wall  $TE_{113}$  one - for the beam splitting system of the Project X is simple and compact .
- One such a cavity provides all the necessary kick of 10 MeV.
- The cavity has the length of 1 m and diameter of 0.37 m instead of 4.5 meter-long, 1 m in transverse size 3-cavity KEK-type RF system.
- The new cavity sizes are close to FNAL 650 MHz cavity. Thus, all the same surface processing and test facilities may be used.
- This cavity may be used for 1 GeV extraction, which is also considered for ADS experiments.

# CONCLUSION:

❖ Beam splitting cavity for PX should have the following requirements:

- RF kick – 10 MeV CW;
- Frequency - 447 MHz (or 366 MHz).

❖ Beam splitting cavity for PX has the following features/issues:

- Small beam loading (operating frequency is not harmonic of the bunch sequence frequency);
- Most probably, no problem with HOMs (small beam current);
- No size limitations.

But:

- Microphonics;
- Emittance dilution for non-deflected bunches.

❖ Our baseline:

- 3-gap squashed-wall cavity (version of ODU parallel – bar cavity) .

## Synergy with the LHC crab cavity CM:

|  | Project X                                    | LHC CC |       |
|--|--|--------|-------|
| The kick, MeV  | 10   | 5      |       |
| Frequency, MHz   | 447  | 400    | close |
| Transverse size  | about the same                               |        |       |
| Longitudinal size  | about the same                               |        |       |
|  | (taking into account HOM dampers for LHC CC) |        |       |
| Operating temperature  | about the same                               |        |       |
| HOM issues and dampers   | no   | yes    |       |
| Microphonics issues  | yes  | no     |       |
| Emittance dilution   | yes  | no     |       |
| Environment limitations  | no   | yes    |       |
| (including the second beam pipe)   |  |        |       |
| CMs for PX deflecting cavity and LHC CC may contain many common elements |  |        |       |