



The SPL Short Cryo-module: Status Report *(outcome of the conceptual review)*

V.Parma,
CERN, TE-MS
*On behalf of the
Cryomodule development team*

1st Open Collaboration Meeting on Superconducting Linacs for High Power Proton Beams
(SLHiPP-1), CERN, 4th November 2011



The cryomodule development team

System/Activity	Responsible/members	Lab
Cryo-module coordination	V.Parma	CERN
Cryo-module conceptual design	R.Bonomi, D.Caparros, O.Capatina, P.Coelho, V.Parma, Th.Renaglia, A.Vande Craen, L.R.Williams	CERN
Cryo-module detailed design & Integration & Cryostat assembly tooling	Ph.Dambre, P.Duthil, P.Duchesne, S.Rousselot, D.Reynet	CNRS/IPNO-Orsay
Cavities/He vessel/tuner	O.Brunner, O.Capatina, Th.Renaglia, F.Pillon, N.Valverde, W.Weingarten/S.Chel, G.Devanz	CERN/CEA-Saclay
RF Coupler	E.Montesinos/S.Chel, G.Devanz	CERN/CEA Saclay
Vacuum systems	S.Calatroni (now G.Vandoni)	CERN
Cryogenics	U.Wagner	CERN
Survey and alignment	P.Bestman	CERN
SPL Machine architecture	F.Gerigk	CERN



Goals of the conceptual review

Reviewers: R.Garoby, CERN BE-HDO (Chair); C.Hauviller, CERN EN-HDO; L.Tavian, CERN TE-CRG; P.Bosland, CEA-Saclay; H.Saugnac, IPNO-Orsay.

Charge to the Review Committee:

In general, comments and feedback are encouraged on any subject that you find relevant.

More specifically, the Review Committee is asked to comment upon the design adequacy and make recommendations on the following points:

- 1) - Cavity helium tank concept and interfaces to cryo-module;
- 2) - Supporting system concept for the cavities in the cryo-module;
- 3) - Vacuum vessel concept and choice of the associated assembly tooling; possibility of extending the concepts to a full size 8-cavity cryo-module;
- 4) - Cryostat thermal design concept;
- 5) - Cryogenic scheme, control and diagnostic devices.



Agenda of the review

Agenda:

- 8:45-8:50 Welcome (R.Garoby), 5';
- 8:50-9:20 The Short Cryomodule: requirements (V.Parma), 30';
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<https://indico.cern.ch/conferenceDisplay.py?confId=154284>



Report from the review committee

21/11/2011

Report of the Review Committee of the SPL Cryo-module Conceptual Design

November 4, 2011 - CERN

Committee Members

P. Bosland (CEA-Saclay), R. Garoby (CERN) [Chair], C. Hauviller (CERN), H. Saugeat (IPN-Corvax), L. Taviani (CERN).

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- Supporting system concept for the cavities in the cryo-module;
- Vacuum vessel concept and choice of the associated assembly tooling; possibility of extending the concepts to a full size S-cavity cryo-module;
- Cryostat thermal design concept;
- Cryogenic scheme, control and diagnostic devices.

Report Content

1. Preamble
2. General observations
3. Responses to the charge

Annex 1: Agenda
Annex 2: Participants



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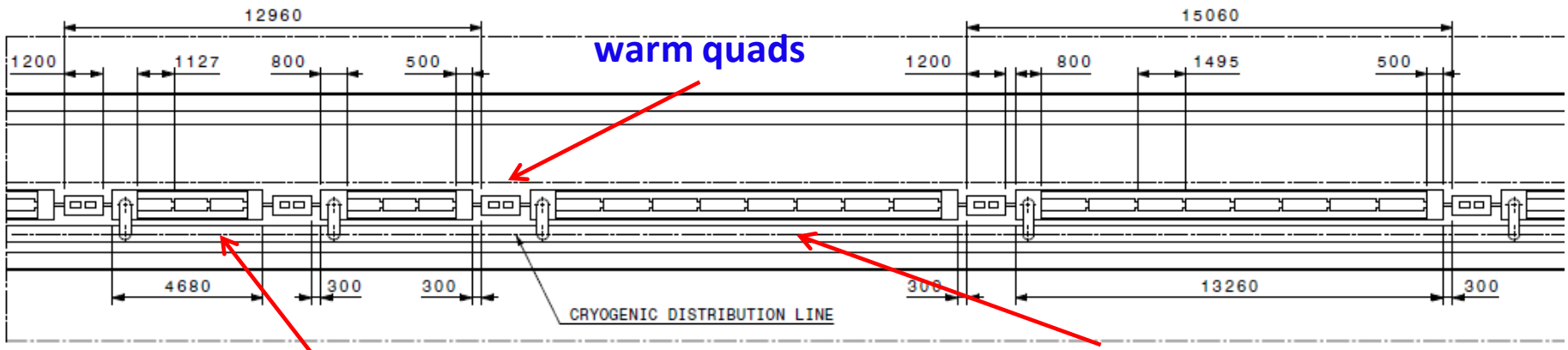
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A possible SPL architecture

«segmented» with warm quads and a cryo distribution line:



$\beta = 0.65$ cryomodule (3 cavities)

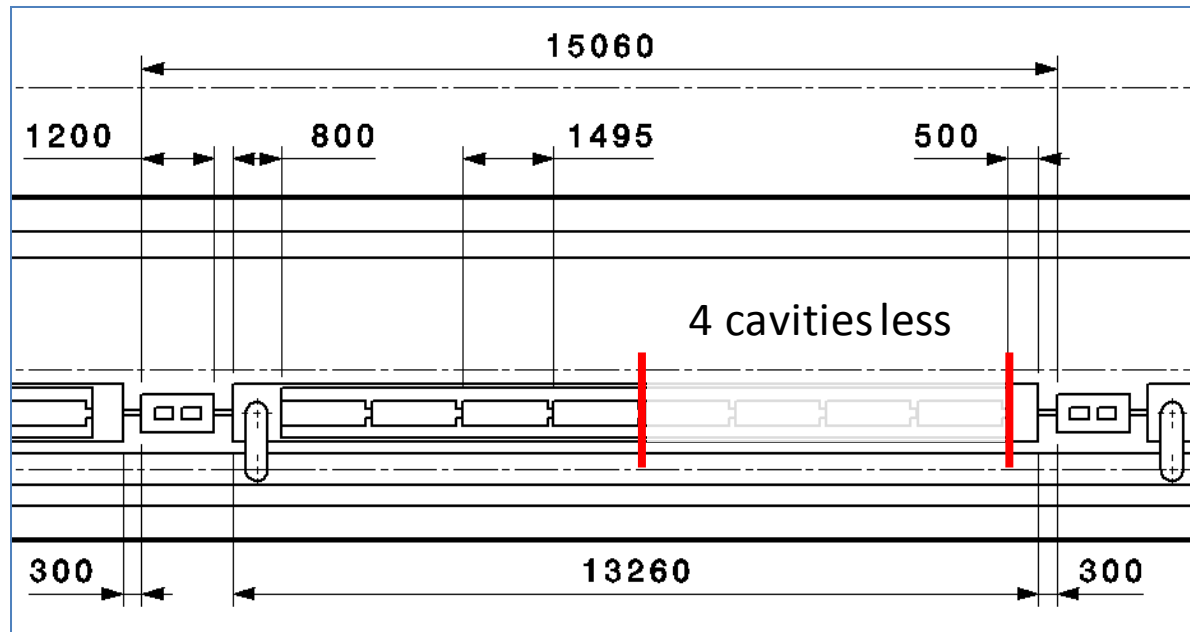
$\beta = 1$ cryomodule (8 cavities)

Short Cryomodule designed possibly

to be compatible with a full-length

8 cavity cryomodule:

- Mechanical design
- Cryogenics (Heat loads, T and p profiles)





Short Cryo-module: Goal & Motivation

Goal:

- Design and construct a $\frac{1}{2}$ -length cryo-module for testing of a string of 4 $\beta=1$ cavities

1st Motivation:

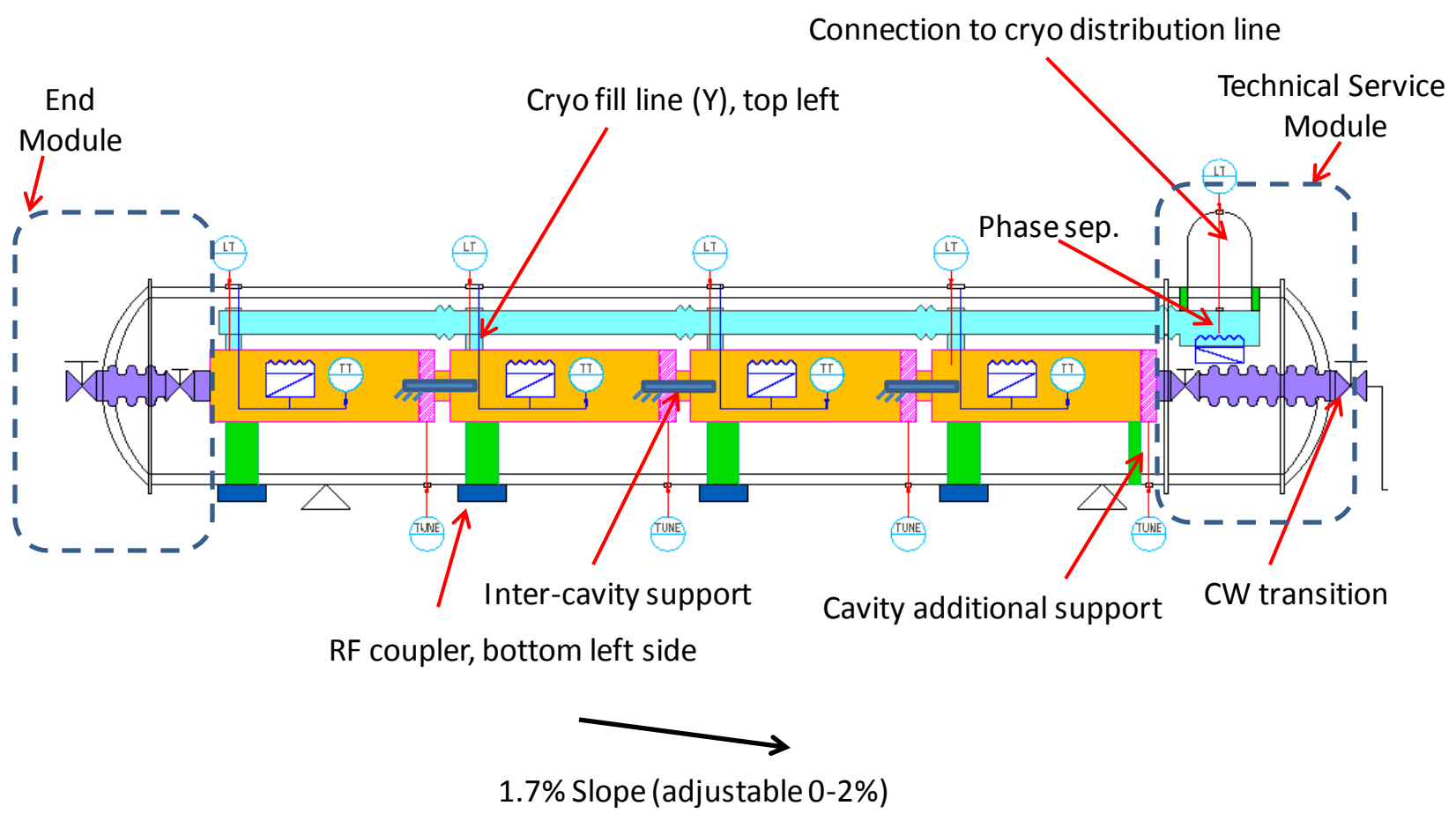
- Test-bench for RF testing on a multi-cavity assembly driven by a single or multiple RF source(s)
- Enable testing of critical components like RF couplers, tuners, HOM couplers in their real operating environment

Cryo-module-related goals:

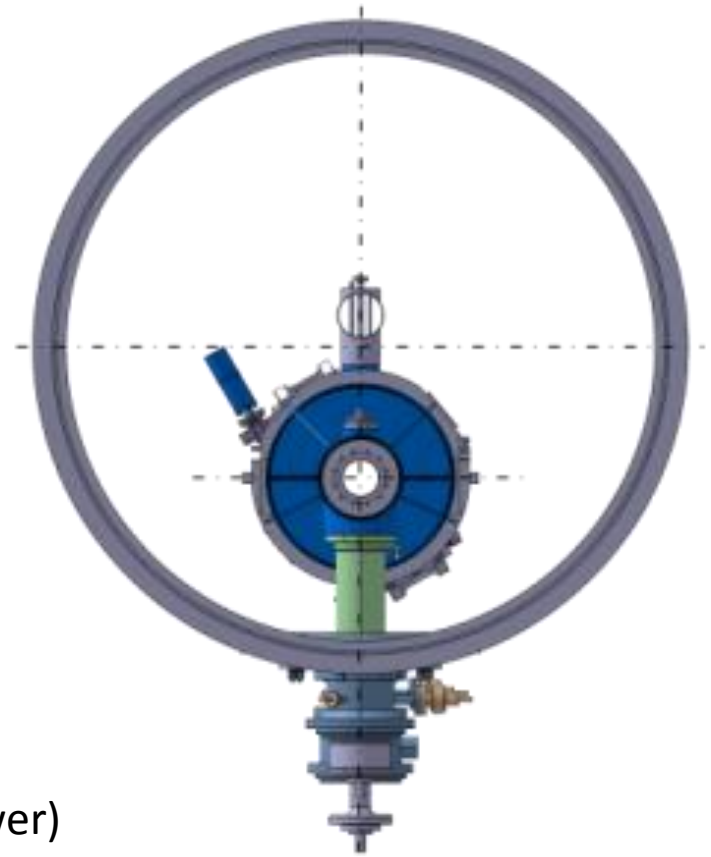
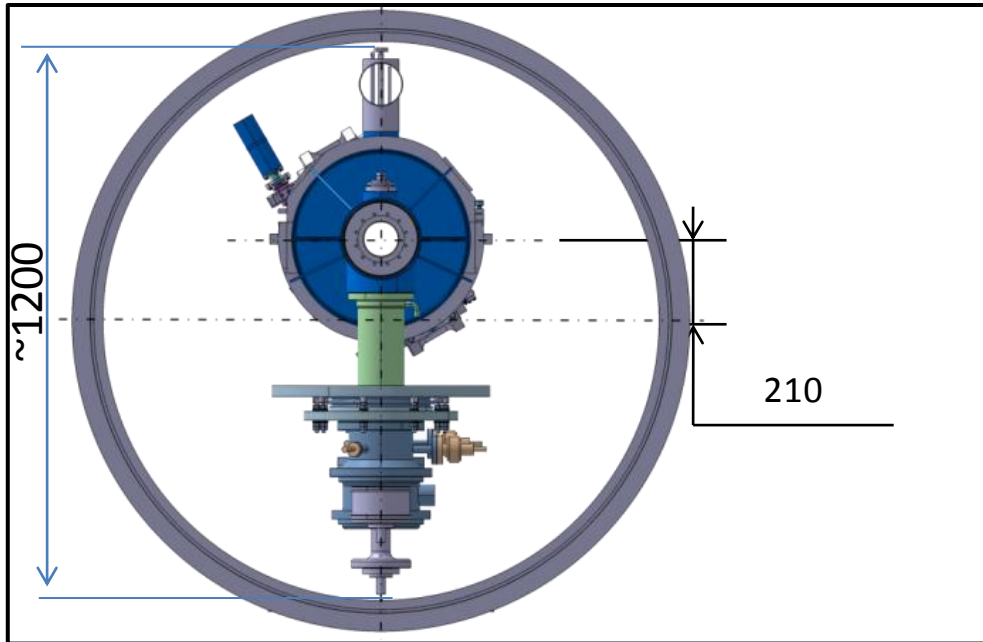
- Validation of design & construction issues
- Learning of the critical assembly phases (from clean-room to cryostat assembly)
- Learning and validation through operational experience:
 - Cool-down/warm-up transients and thermal mechanics
 - Alignment/position stability of cavities
 - Cryogenic operation (He filling, level control, RF coupler support tube cooling ...)



Short cryomodule: layout schematic



Cryostat assembly constraint



Constraints:

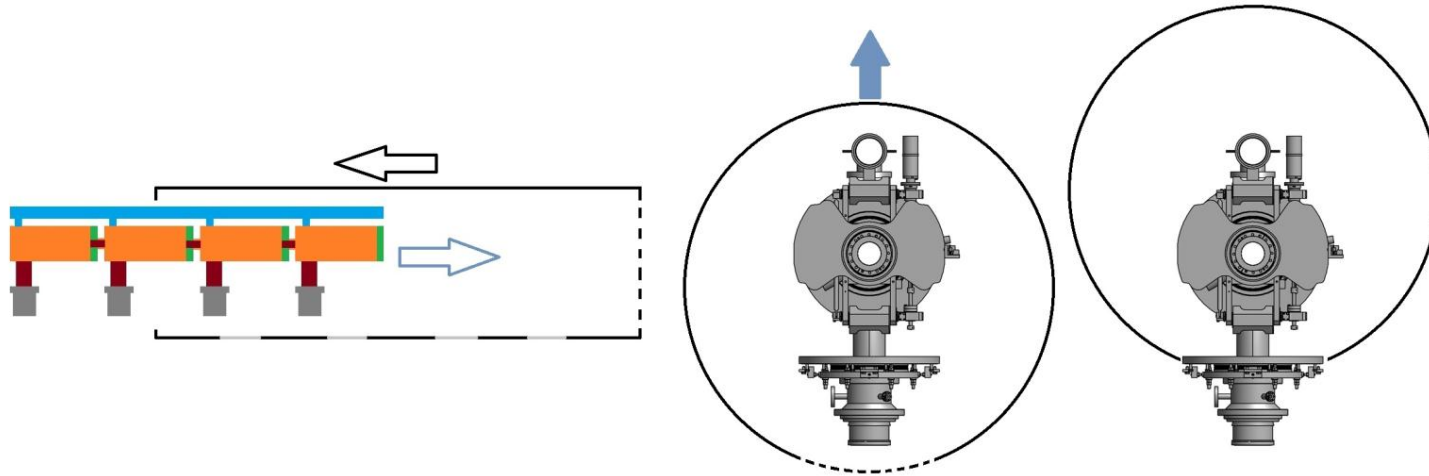
- RF coupler in 1 part (single window for high power)
- Cavity and RF coupler are assembled in clean-room class 10
- Train of cavities assembled in clean room class 10

Consequences:

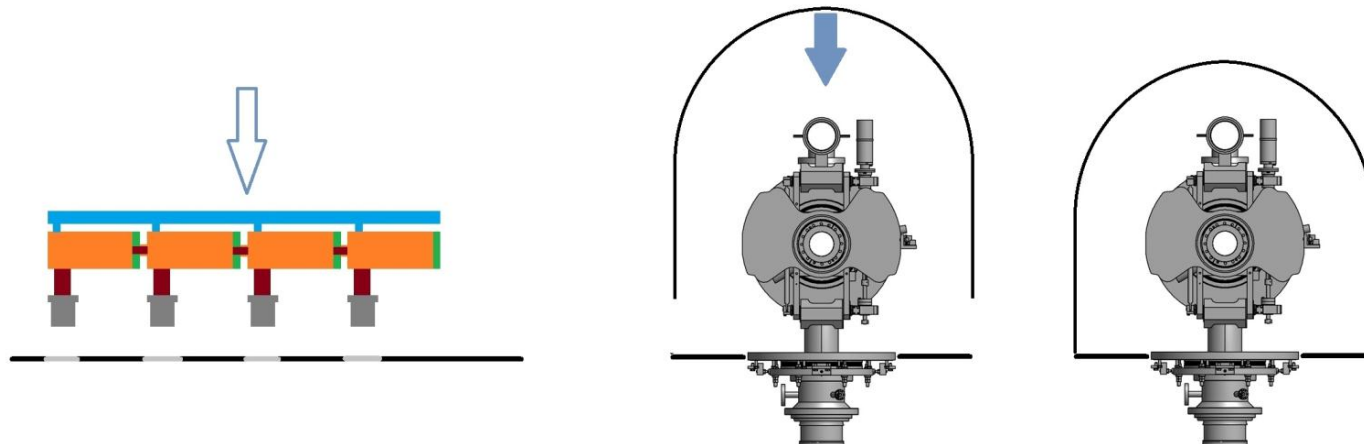
- No cryostat component allowed in a class 10 clean room
- An LHC-type cryostat **leads to a large diameter** (i.e. tunnel space, HL from RT,...)

Vacuum vessel conceptual alternatives

Cylindrical vessel type (LHC like)



2-part vessel type



see talk of Patxi



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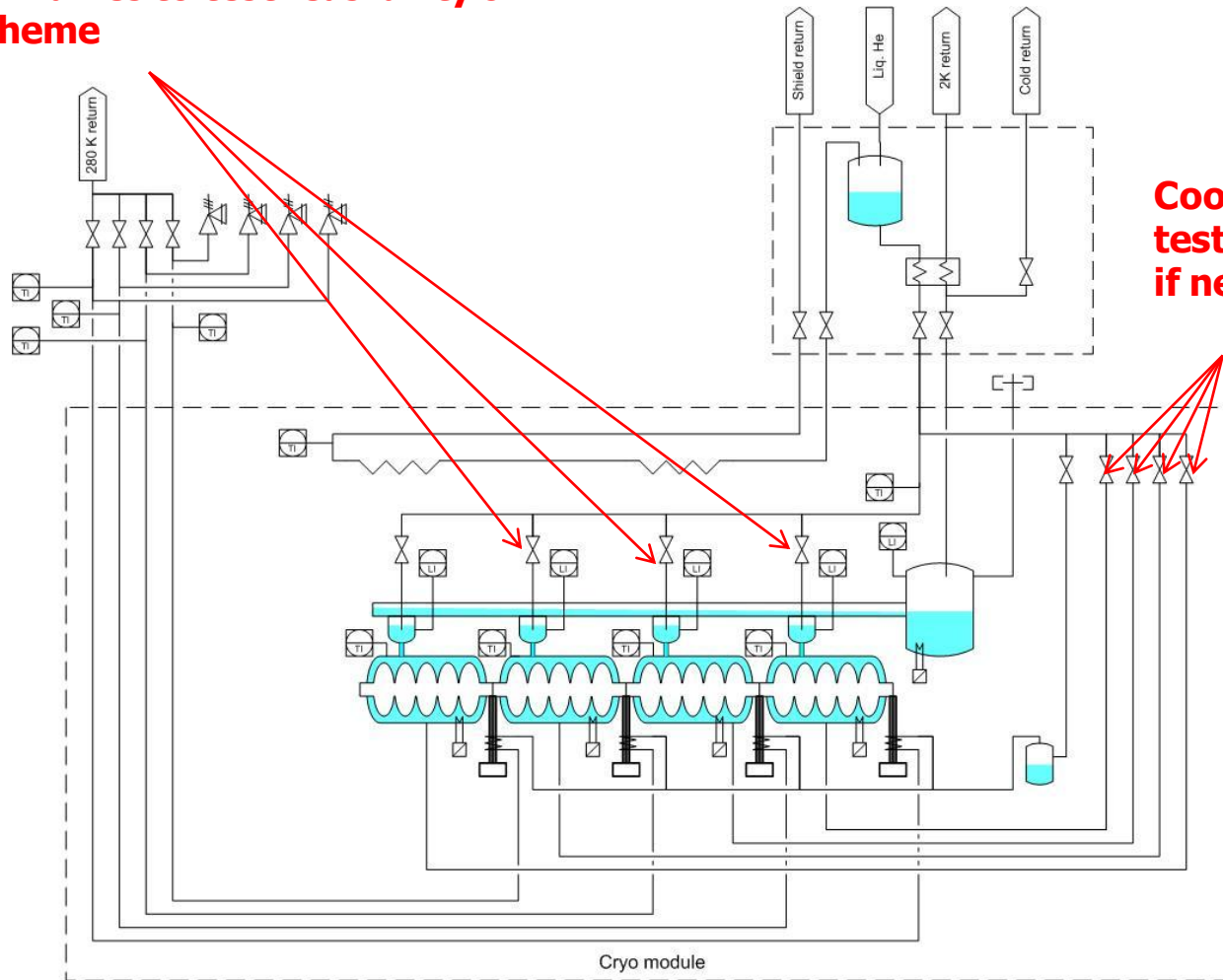
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Additional valves to test feasibility of 2 K supply scheme



**Cool down valves;
tests should show
if necessary**

Definition basis

Heat loads for SPL high- β module

	Heat load [W]	Temperature level [K]	Nominal pressure [bar]	Nominal mass flow [g/s]
Thermal shield	240	50 - 75	16 - 18	1.8
Coupler cooling	(1120)	5-280	1.1	0.78
2.0 K static load	5.0	2.0	0.031	0.25
2.0 K total load	200	2.0	0.031	10

**Static load estimated to 2.5 % of total load.
Even half or double the static load has no influence on design.**

Assessment of static load is of minor importance at this state.

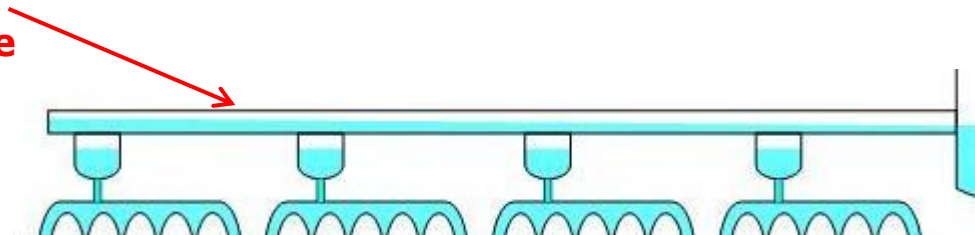
Definition basis

- **Short module cryostat as integration test for full-size high- β module**
- **Piping and valve dimensioning as for full-size high- β module**
 - Where reasonable!
- **General remark:**
 - The design has "reasonable margins".
 - Principally we want to test cavities not piping limits.

Line X: 2-phase pipe

- **Design basis:**
 - Vapour flow speed < 7 m/s to avoid drag of liquid
 - Low pressure loss for isothermal cavities
- **Value: 80 mm Di**
 - **15 m** line; 10 g/s; $\Delta p = 0.07$ mbar; $\Delta T(\Delta p) = 0.08$ mK; vapour speed = 2.7 m/s

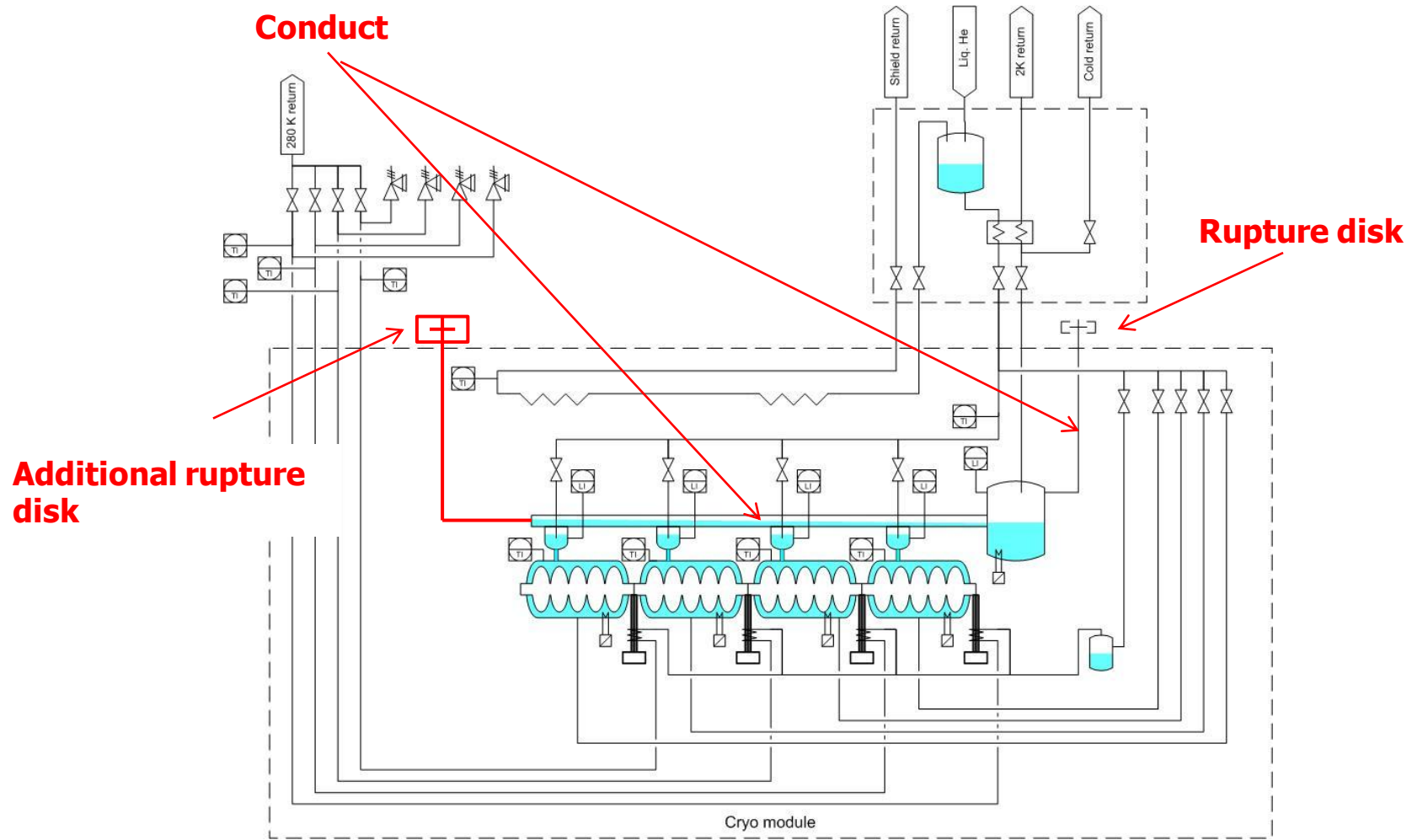
Line "X":
2-phase pipe



Updated table

SPL Pressure/Temperature Table											
Line	Description	Pipe Size (ID min. value) [mm]	Normal operating pressure [MPa]	Normal operating temperature [T]	Cool-down / warm-up pressure [MPa]	Cool-down / warm-up temperature [K]	T range [K]	Maximum operating pressure [MPa]	Design pressure [MPa]	Test pressure [MPa]	Comment
L	Cavity helium enclosure	cavity OD + 10	0.0031	2	0.13 @ 293K 0.2 @ 2K	293-2	2-293	0.15 @ 293K 0.2 @ 2K	TBD	TBD	
X	Bi-phase pipe	80	0.0031	2	0.13 @ 293K 0.2 @ 2K	293-2	2-293	0.15 @ 293K 0.2 @ 2K	TBD	TBD	
Y	Cavity top connection	80			0.13 @ 293K 0.2 @ 2K	293-2	2-293	0.15 @ 293K 0.2 @ 2K	TBD	TBD	
XB	Pumping line	80	0.0031	2	0.13 @ 293K 0.2 @ 2K	293-2	2-293	0.15 @ 293K 0.2 @ 2K	TBD	TBD	
E	Thermal shield supply	15	1.8	~50	2	293-50	50-293	2	2		Heat intercept
E'	Thermal shield return	15	1.8	~50	2	293-50	50-293				Return only
W	Cryostat vacuum vessel	1000 (TBD)	vacuum	293	vacuum	293	237-293	O.P. 0.1	I.P. 0.15	N.A.	
C1	Cavity filling	6	0.1	4.5	0.1	293-4.5	4.5-293				Liquid supply
C2	Coupler cooling	6	0.1	4.5-293	0.1	293-4.5	4.5-293				Gaseous supply
C3	Cavity top supply	10	0.1	2	0.1	293-4.5	2-293				2 phase supply

Minimum values



Recommandations

3.3 Cryostat thermal design concept / Cryogenic scheme, control and diagnostic devices

Observation

- Incomplete cryogenic risk analysis for the final sizing of safety relief system on the He circuits and on the vacuum vessels.

Comment

- Lack of a unique database for designers (heat loads, pressure, temperature,...).
- Is a phase separator for the coupler supply really needed? Consequence of feeding the couplers directly with 2.2 K, 1.3 bar subcooled liquid?
- The process and instrumentation diagram shows 2 Joule-Thomson valves in series (one in the cryo-module and the second in the SM18 cryogenic infrastructure) which could create hydraulic impedance issue.

Recommendations

- Make available and maintain a complete and up-to date set of parameters.
- Make an exhaustive cryogenic risk analysis prior to deciding upon the size of the safety relief systems.
- Specify cool-down and warm-up requirements and constraints.
- Check deformations (screens, shields,...) during cool-down and warm-up.
- Check compatibility with SM18 cryogenic infrastructure.
- Assess the unbalance of the subcooling heat exchanger.
- Develop a thermo-hydraulic model to analyze the robustness of the 2 K He level controls (RF transients).
- Finalize the list of additional instrumentation for prototype validation and include it on the P&I diagram.
- Study alternative for instrumentation feedthroughs without cold ceramic insulators.
- Elaborate a procedure for cooling down the cold magnetic shield, taking into account the cavity cool down and the impact on the '100K effect'.



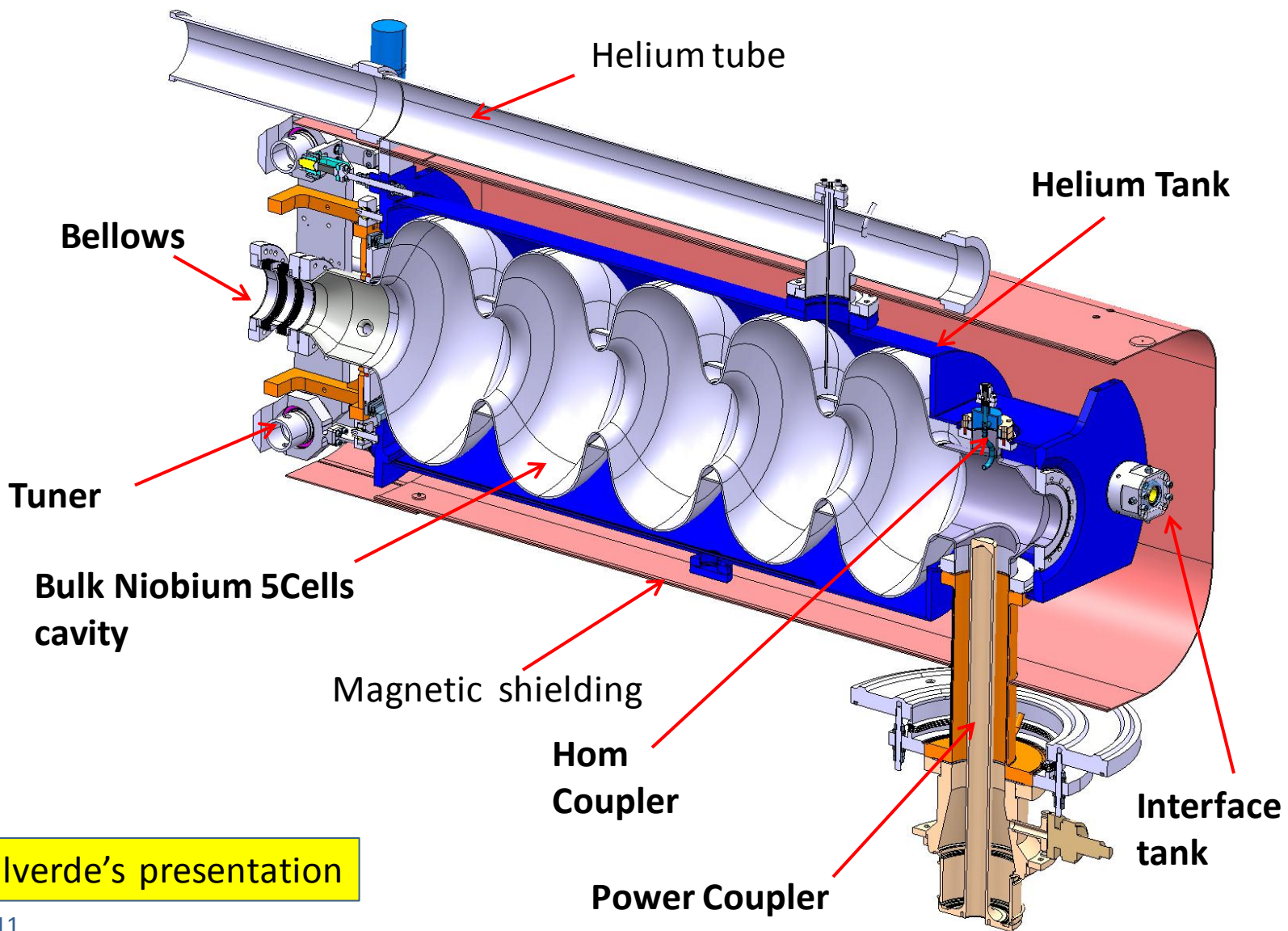
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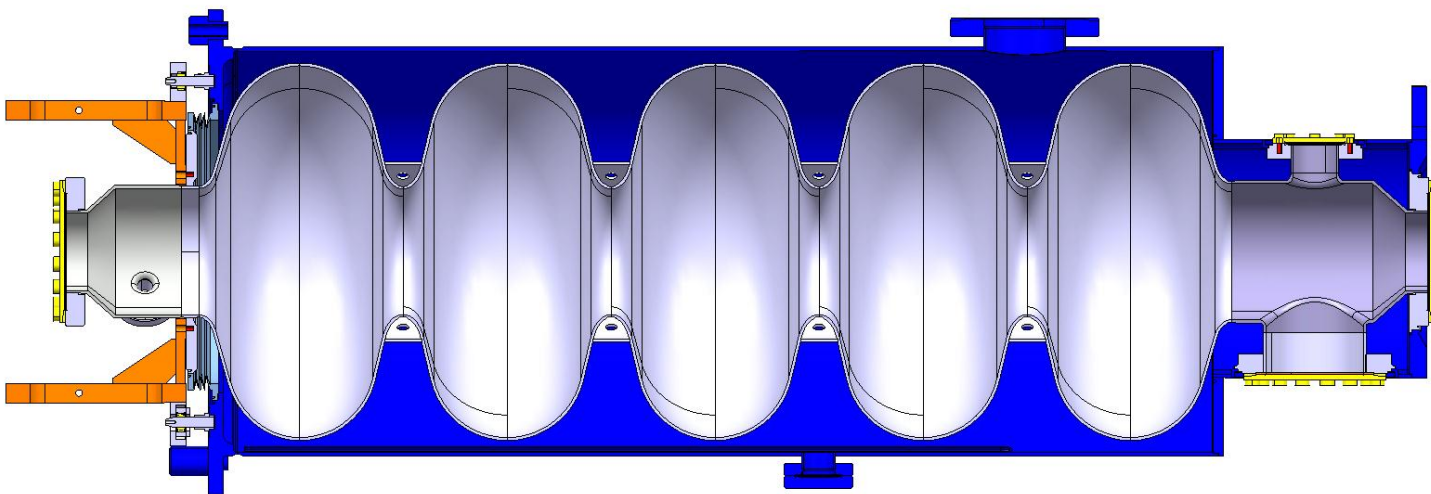
INTRODUCTION- CAVITY SPL

SPL cryo-module conceptual design review



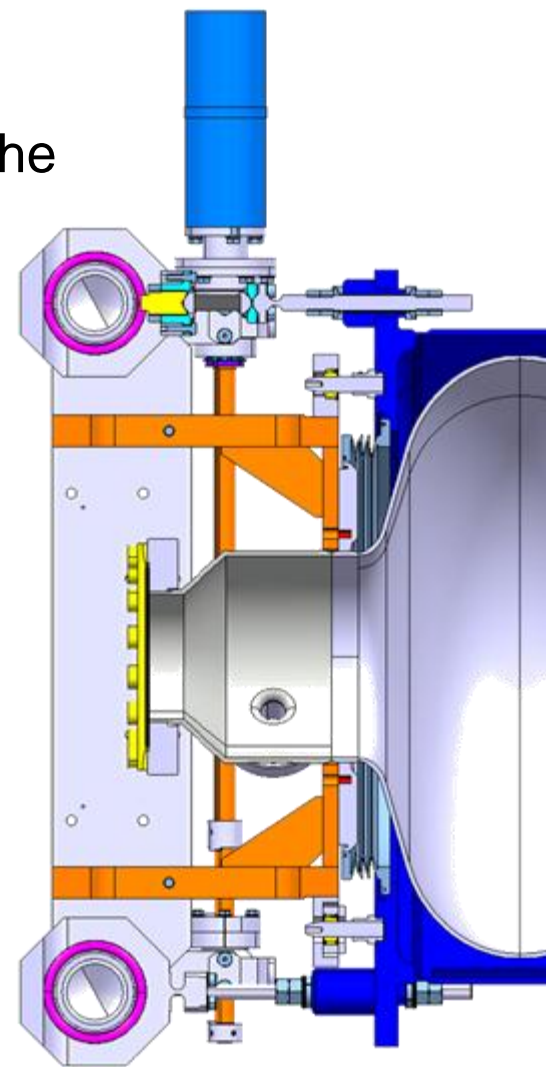
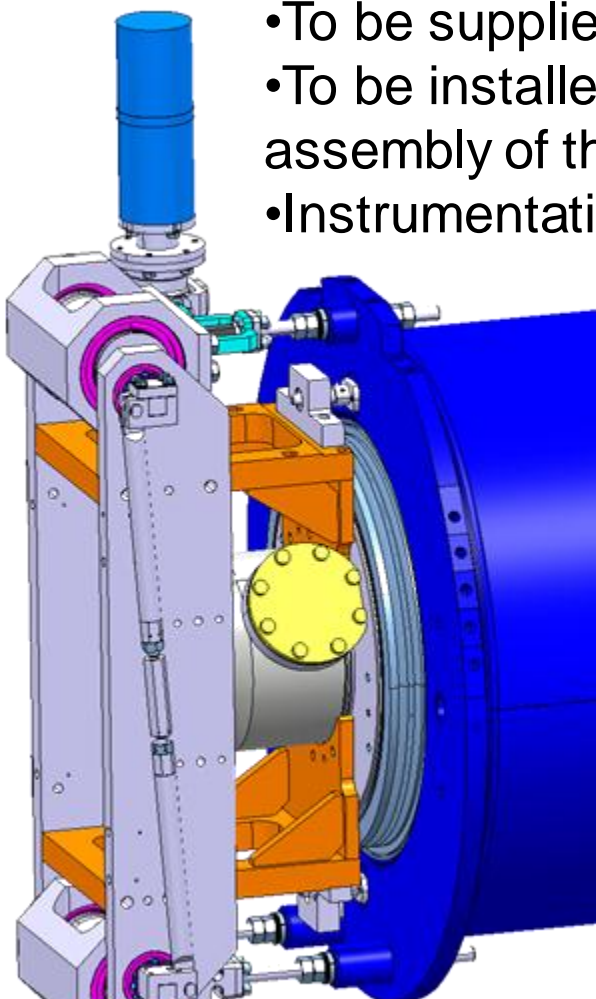
N.Valverde's presentation

- Designed by CERN (SS material)
- To be manufactured by CEA
- Assembly cavity-tank by CERN



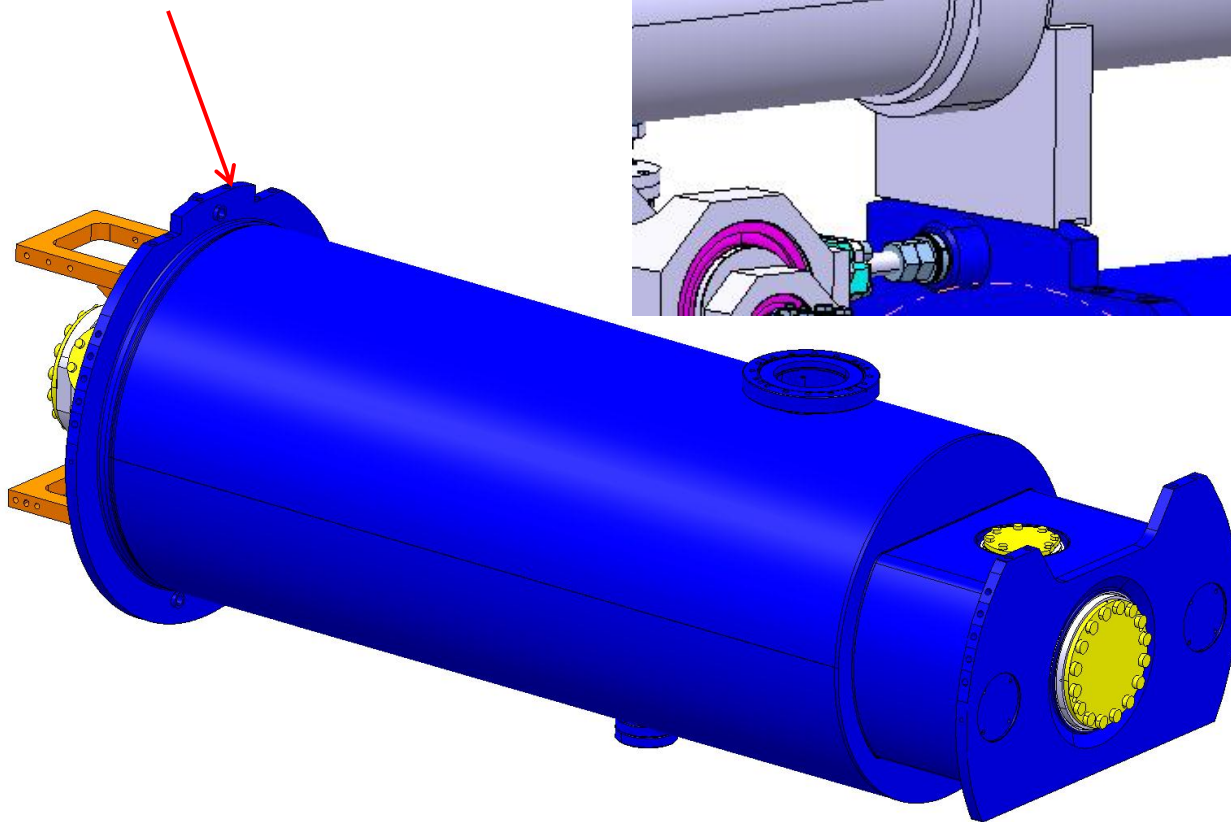
TUNER

- To be supplied by CEA
- To be installed by CERN during the assembly of the cryo-module
- Instrumentation / control cables

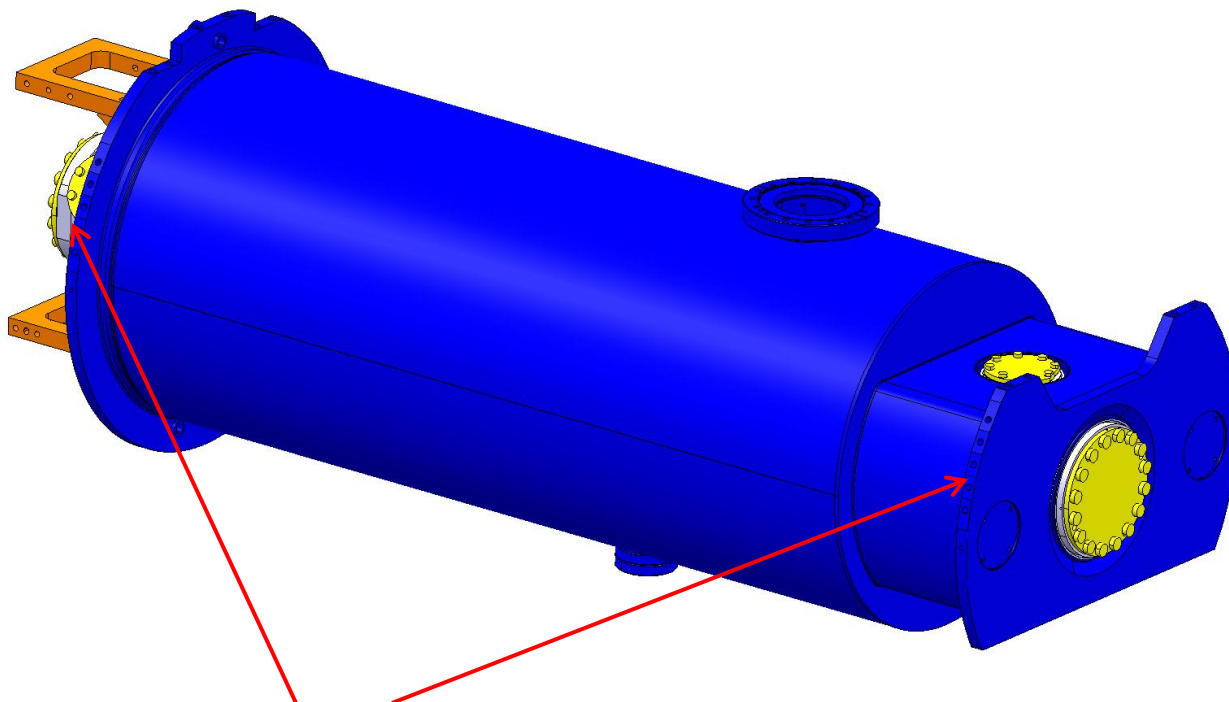


N.Valverde's presentation

Support for helium tube



N.Valverde's presentation

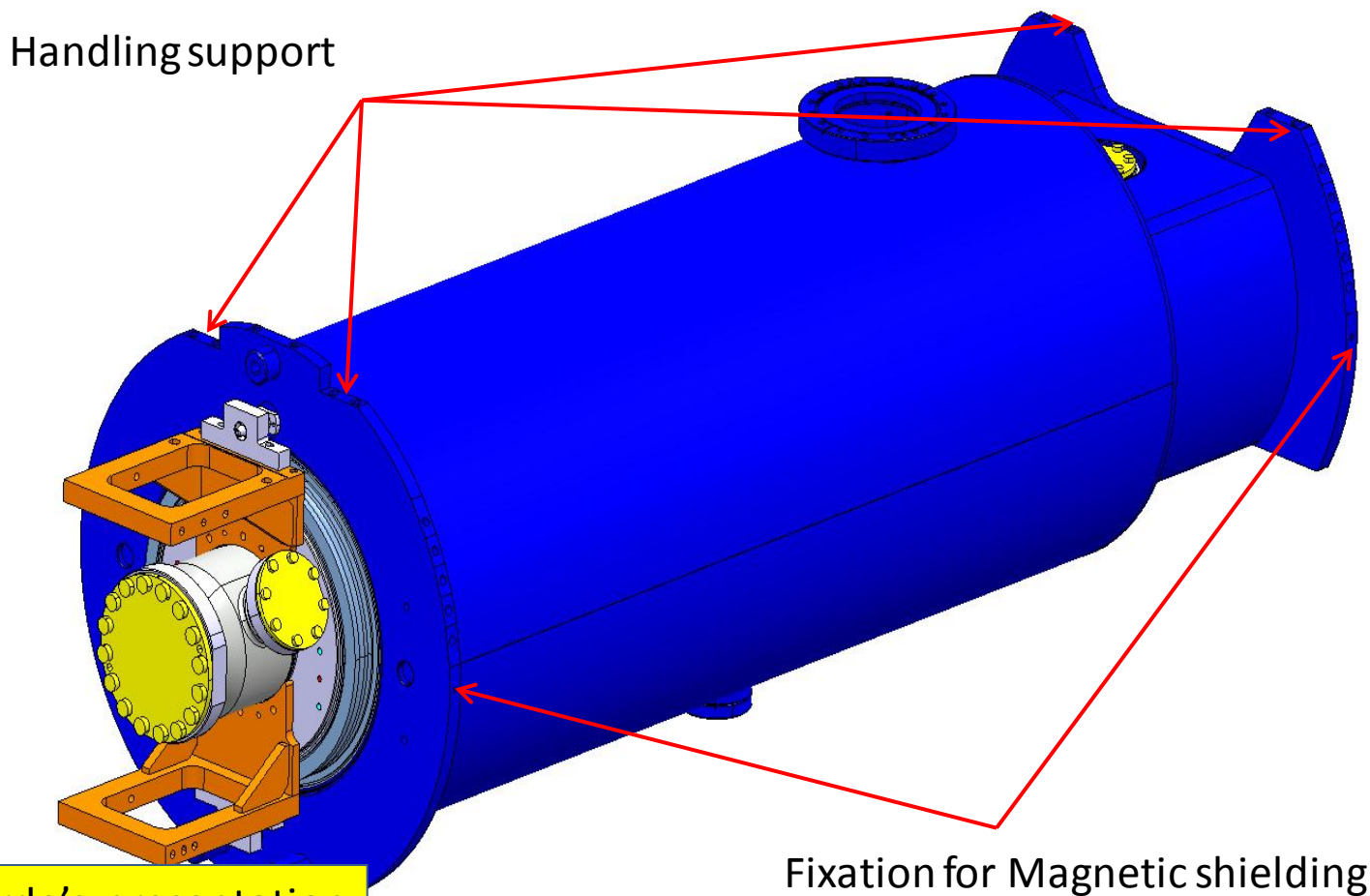


Interface for alignment supports

The alignment system supports are designed by the cryo-module team compatible with all adjacent equipment (magnetic shielding etc.)

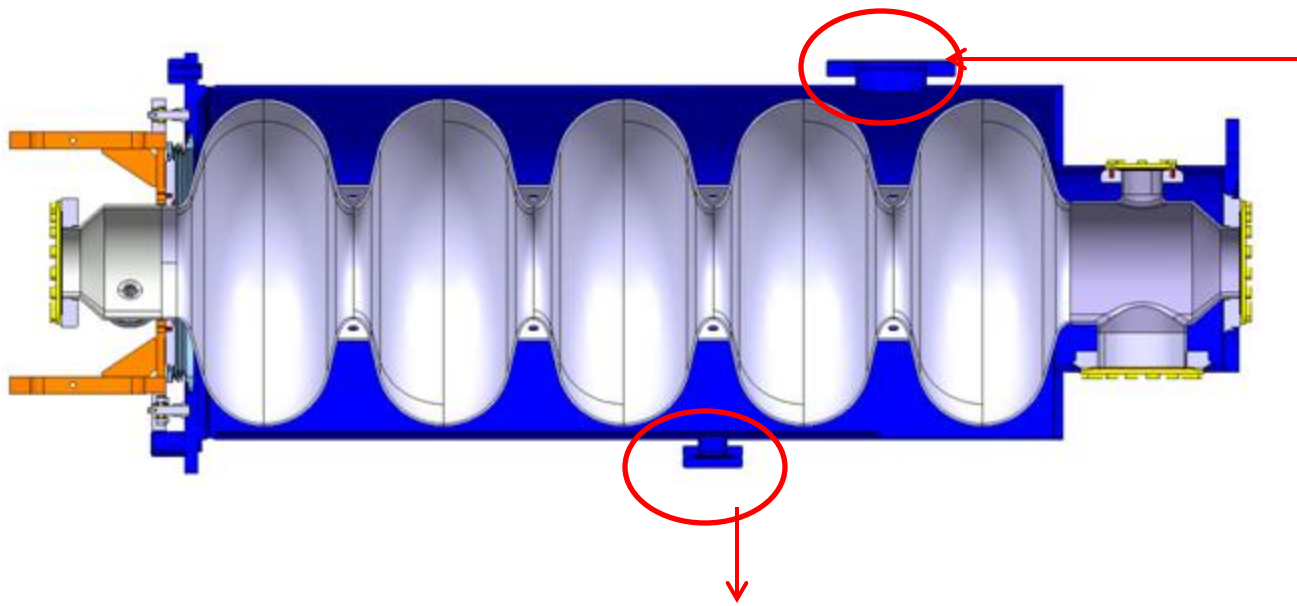
N.Valverde's presentation

HELIUM TANK



N.Valverde's presentation

HELIUM TANK- Interface Cryo



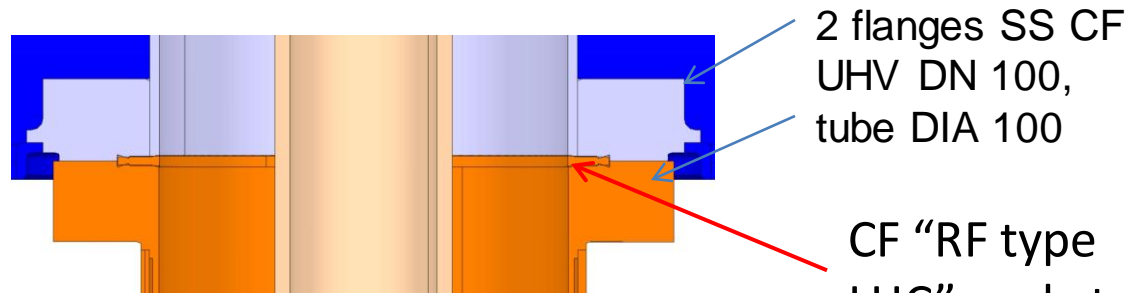
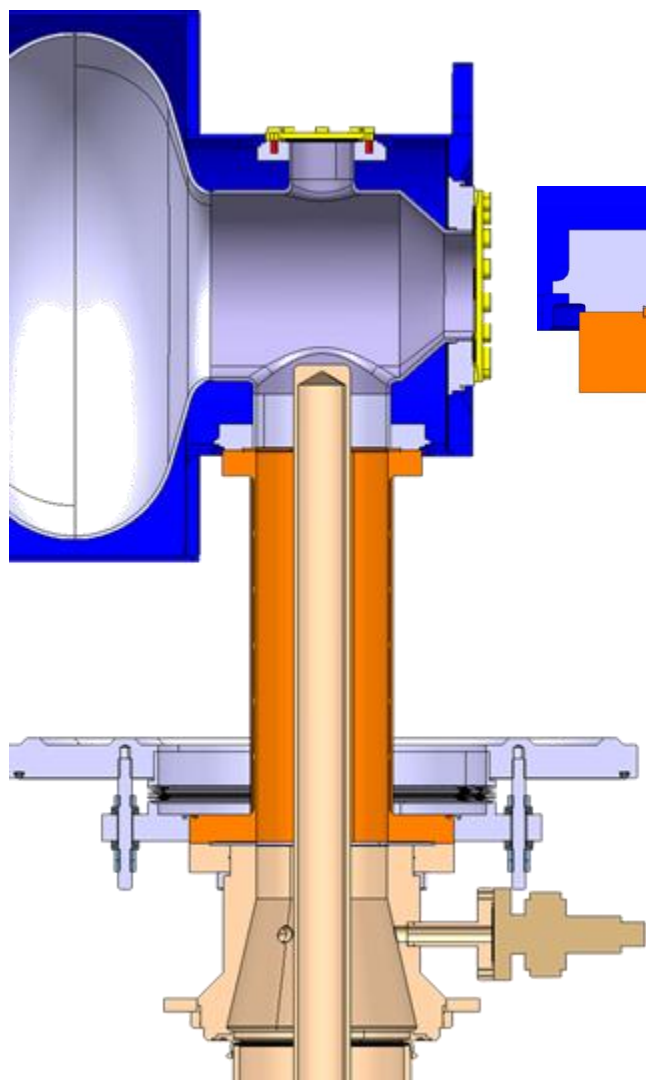
SS CF UHV DN100, tube dia 80 mm -It has been designed to extract the heat in a nominal performance (pulsed).

SS CF UHV DN 40, tube dia 27 mm. In principle not needed in a first phase. Will be closed with a flange.

Needs to be defined by cryo if instrumentation (ex. heaters...) or other equipments (ex. helium supply pipe...) need to be installed before assembly of the helium tank.

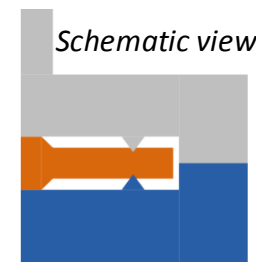
N.Valverde's presentation

Designed and provided by
CERN (BE/RF)



2 flanges SS CF
UHV DN 100,
tube DIA 100

CF "RF type
LHC" gasket



Requirements to fulfill:

- RF Electric continuity
- Support for the cavity → (The cavity + tank is not designed for cantilever supporting)

N.Valverde's presentation

5. Conclusion

BUDGET OF TOLERANCE			
Step	Sub-step	Tolerances (3σ)	Total envelopes
Cryo-module assembly	Cavity and He vessel assembly	$\pm 0.1 \text{ mm (TBD)}$	Positioning of the cavity w.r.t. beam axis $\pm 0.5 \text{ mm}$
	Supporting system assembly	$\pm 0.2 \text{ mm (TBD)}$	
	Vacuum vessel construction	$\pm 0.2 \text{ mm (TBD)}$	

Loads: Self weight and weight of components

Cavity (measured by ends only)
Helium vessel

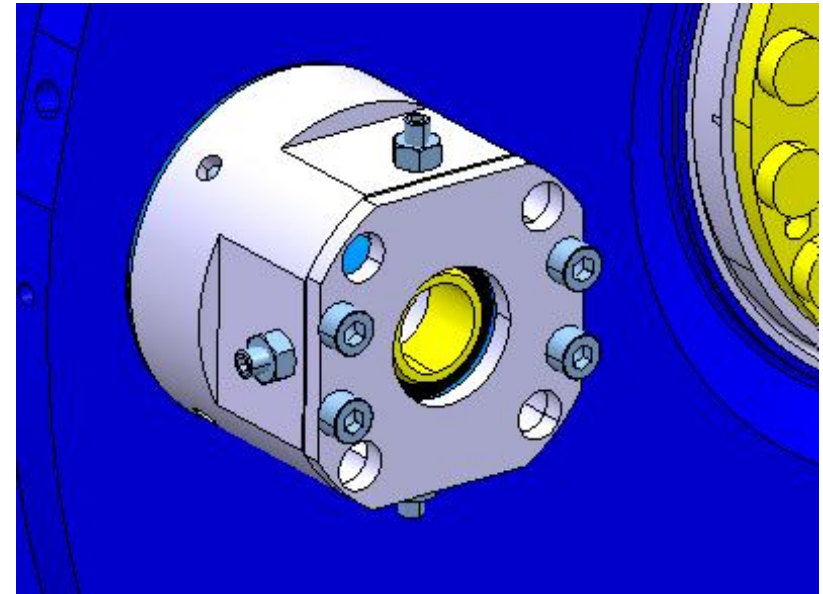
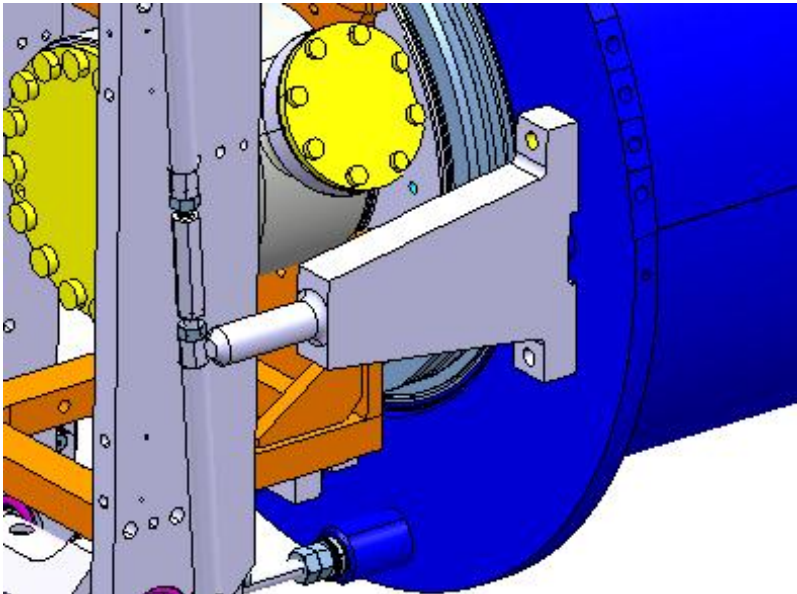
Helium vessel, inter-cavity support, string of cavities

Vacuum vessel, interfaces.

Models above are obsolete or conceptual

Proposed design

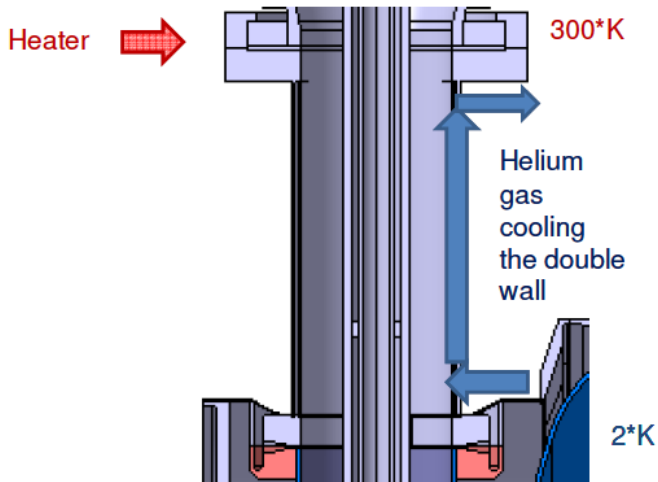
- Proposed solution



2. Power coupler as support

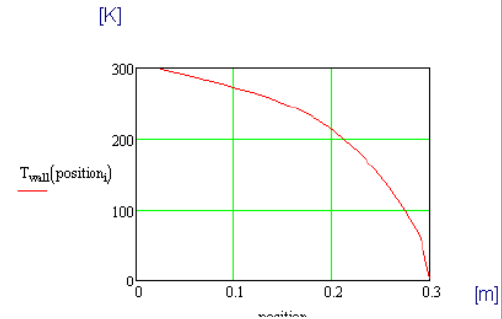
Active cooling of PC double walled tube

- Cooling gas at 4.5 K input
- Lower part at 2 K and upper part at 300 K
- Heater at upper part to insure 30 °C of flange temperature
- 1000 kW pulsed (100 kW average), 704.4 MHz, 50 Ω
- H=300 mm; D=100 mm; eint=1.5 mm; eext=2 mm
- Copper on stainless steel; Copper RRR = 30 (Sergio Calatroni)

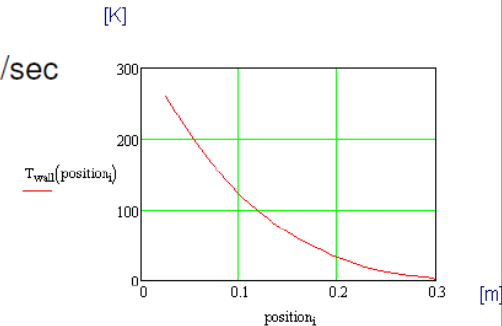


Why cooling the wall?

- No cooling temperature profile
=> Gives 21W to 2K



- Cooling with 42 mgam/sec temperature profile
=> Gives 0.1W to 2K



Courtesy of Ofelia Capatina

The active cooling of the double walled tube was not conceived to cope with its support function. However, due to the cavity alignment requirements, the thermal profile of the double tube and its reproducibility become a fundamental issue.

Further work on this subject is being carried out by Rossana Bonomi (TE/MS).

Power coupler mock-up

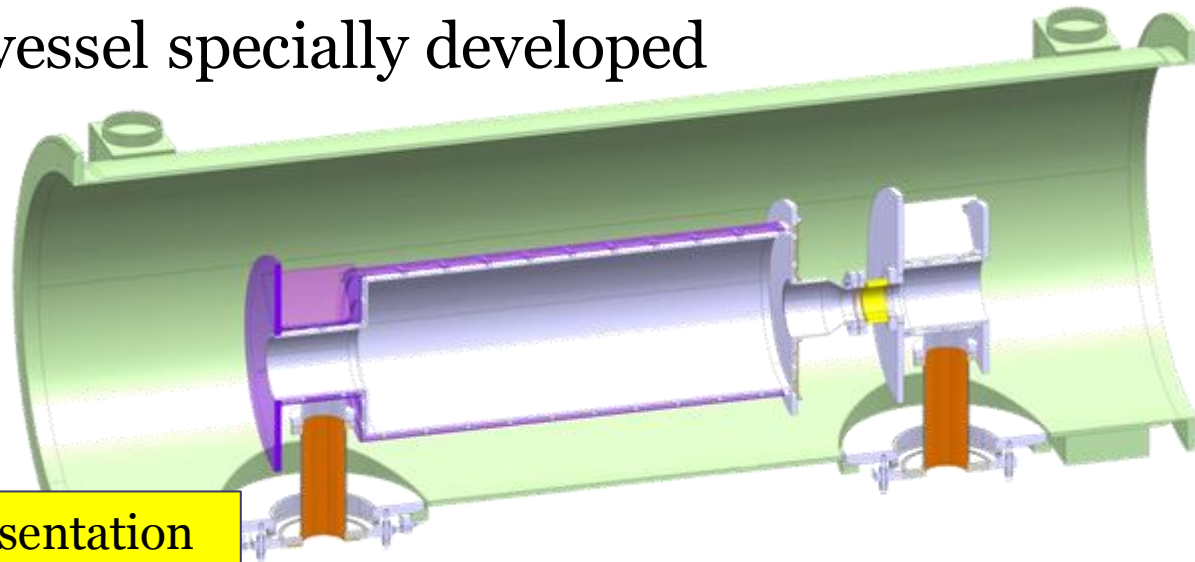
- Tube : same inertia as double walled tube
- Real flanges
- Force at end of beam (torque on flange)



Supporting scheme mock-up

Still in development

- Cooled with liquid nitrogen
- Same mechanical behaviour as real cavity/ Helium Tank
- Real surrounding components
 - Double walled tube
 - Inter-cavity support
- Vacuum vessel specially developed



Recommendations

3. Response to the Charge

3.1 Cavity helium tank concept and interfaces to cryo-module / Supporting system concept for the cavities in the cryo-module

Observation

A new and innovative concept is being proposed which makes use of the large main RF couplers to support all the equipment inside the cryo-module tank. Clear benefits are expected in terms of static heat loss.

Comment

- Delicate design issues:
 - o Transfer of loads through vacuum flanges. Since no data was presented about leak and mechanical robustness at the level of coupler support flange on vacuum vessel, the Committee considers that the design is at initial stage.
 - o Complex inter-tank support with numerous constraints.
- The boundary conditions should be clearly expressed to help understand the relevance of the mechanical analysis.
- The foreseen mock-ups are very important for validating crucial concepts (alignment at cold, inter-cavity connection, ...).

Recommendations

- The solutions imagined for the transfer of loads through vacuum flanges deserve extensive testing.
- Demonstrate that the tank rigidity is sufficient for the slow and fast tuning systems to work properly.
- Demonstrate that no plastic deformation of the cavity will occur during thermal cycling because of the difference in the thermal

contraction coefficients between the stainless steel of the helium tank and the niobium of the cavity.

- The welded bellows between cavities may be a source of dust contamination. Elaborate a cleaning procedure of these bellows in order to limit the risk of cavity performance degradation.
- More mechanical analyses are required to bridge the gap between the ones using simplified models (e.g. for the inter-tank) and the ones with detailed models (e.g. couplers).
- Need for analysis of loads under thermal transients.
- Need for analysis of the mechanical eigenmodes.



Agenda of the review

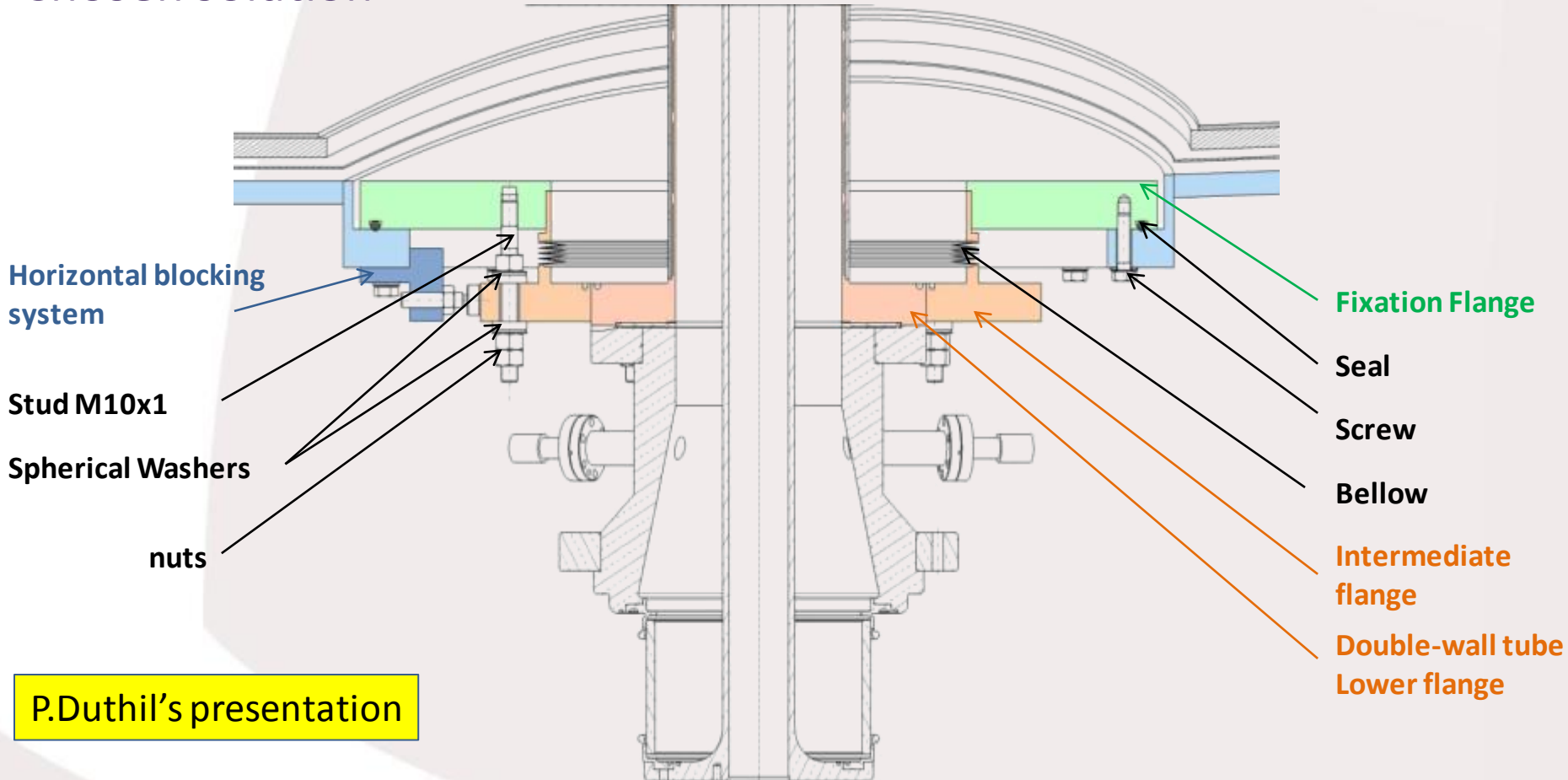
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- 14:45-16:00 Reviewers' closed session, 1h 15';
- 16:00-16:30 Recommendations from reviewers and Conclusions
- 16:30 Adjourn

VACUUM VESSEL / COUPLER INTERFACE

Coupler compensation interface with the vacuum vessel

Chosen solution



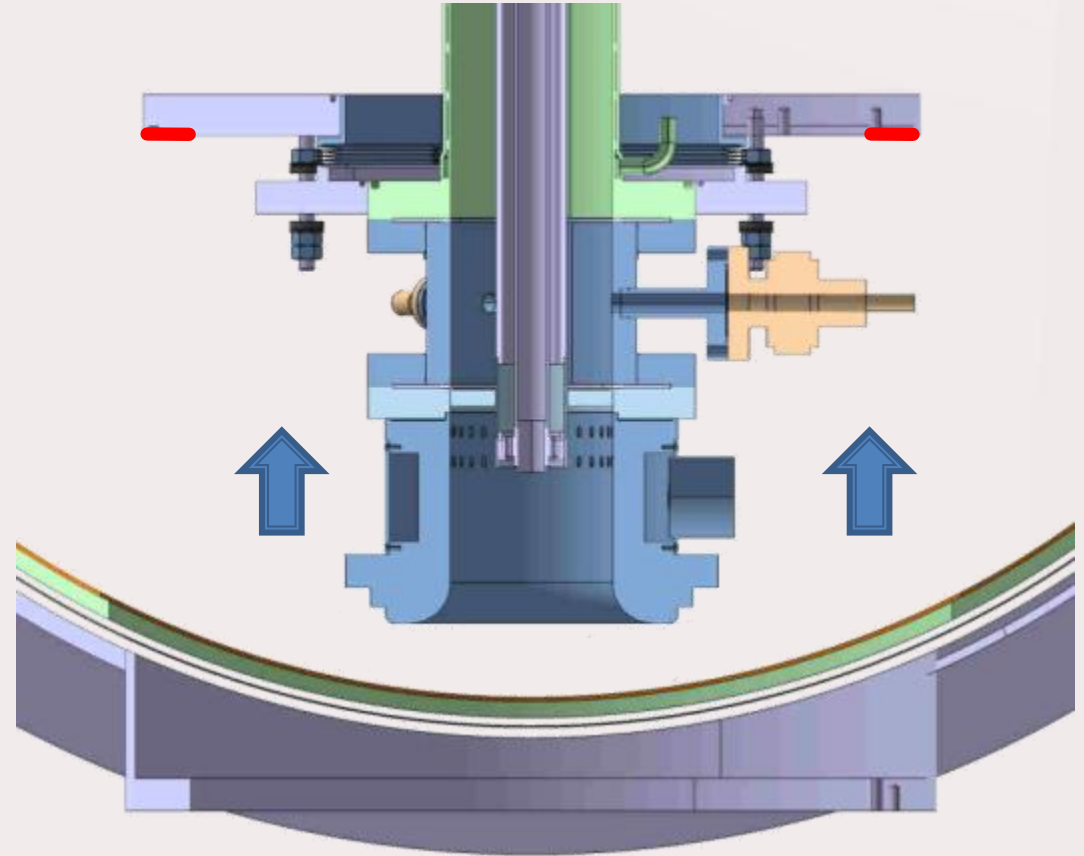
P.Duthil's presentation

The detailed study of this interface has been done.
It will soon be constructed and tested on a mock-up by CERN.

Coupler compensation interface with the vacuum vessel

Assembly procedure

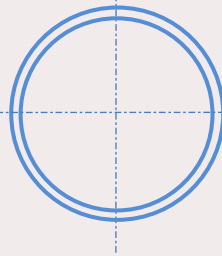
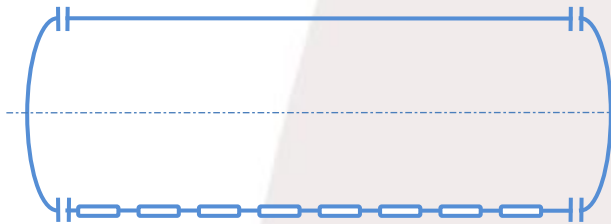
- Vacuum vessel lift of



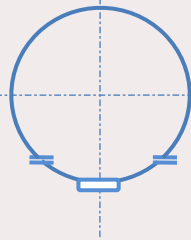
P.Duthil's presentation

- **Contact of the 4 coupler sealing flanges to the 4 bearings of the vacuum vessel**
 - **And fixing**
- ⇒ defaults located at the level of the 4 bearing plans are compensated by the flexibility of the bellows.

Different concepts



Cylindrical vacuum vessel (LHC type)

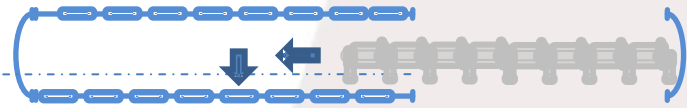


Vacuum vessel with longitudinal aperture

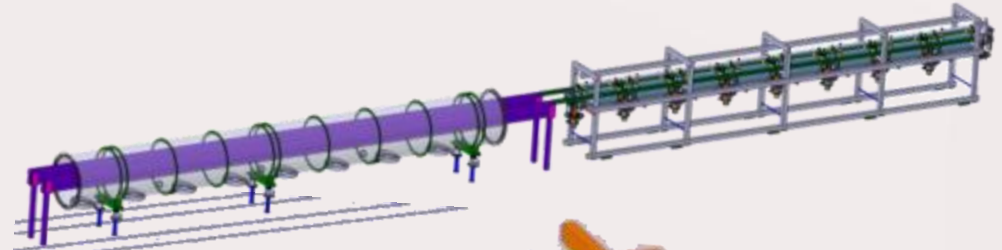
- Bottom cover
- Top cover

CONCEPTUAL CRYOSTATING TOOLING

➤ Horizontal cryostating Tooling Studies



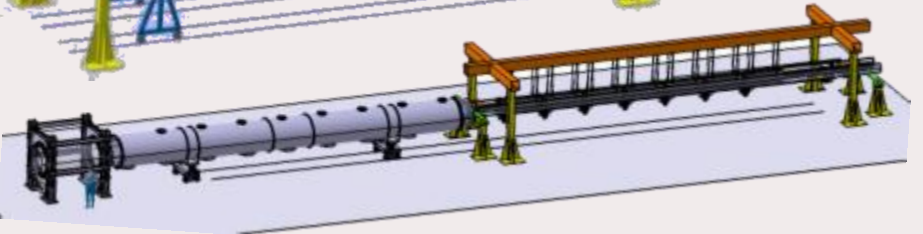
Mobile Frame tooling



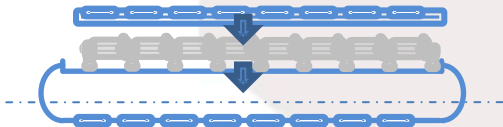
Mobile Trolley Tooling



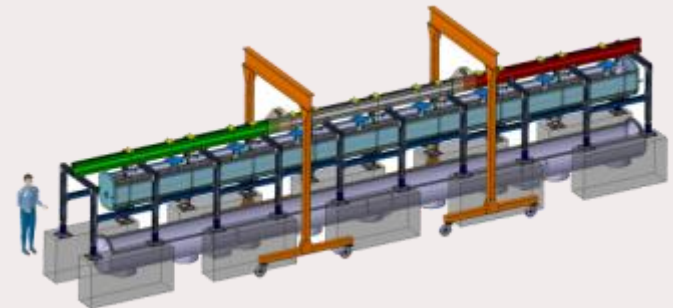
Cantilever Tooling

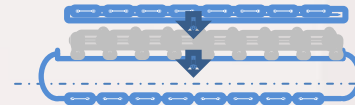


➤ Vertical Cryostating Tooling Study

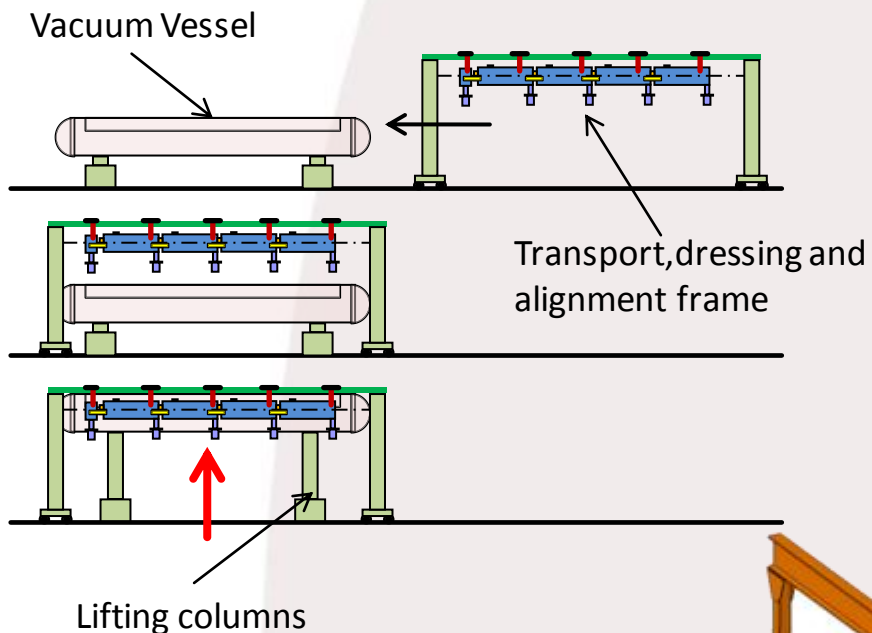


Vertical Cryostating Tooling

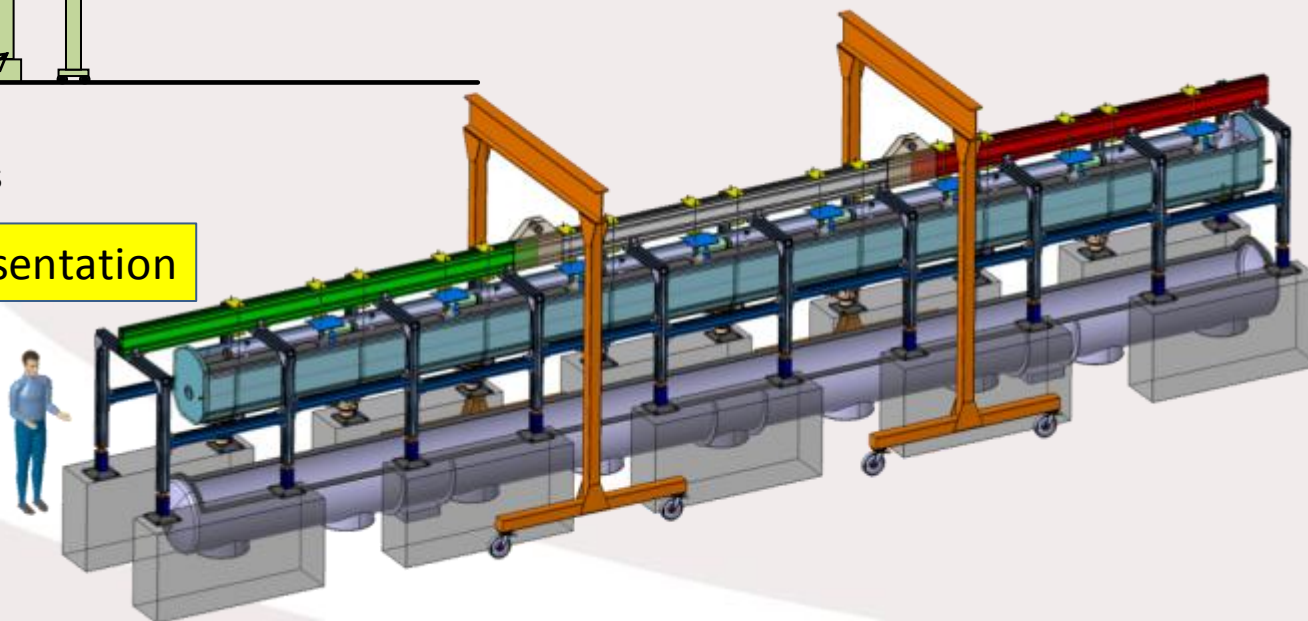




Vertical cryostating tooling



P.Duthil's presentation



➤ Vertical Translation of the Vacuum Vessel

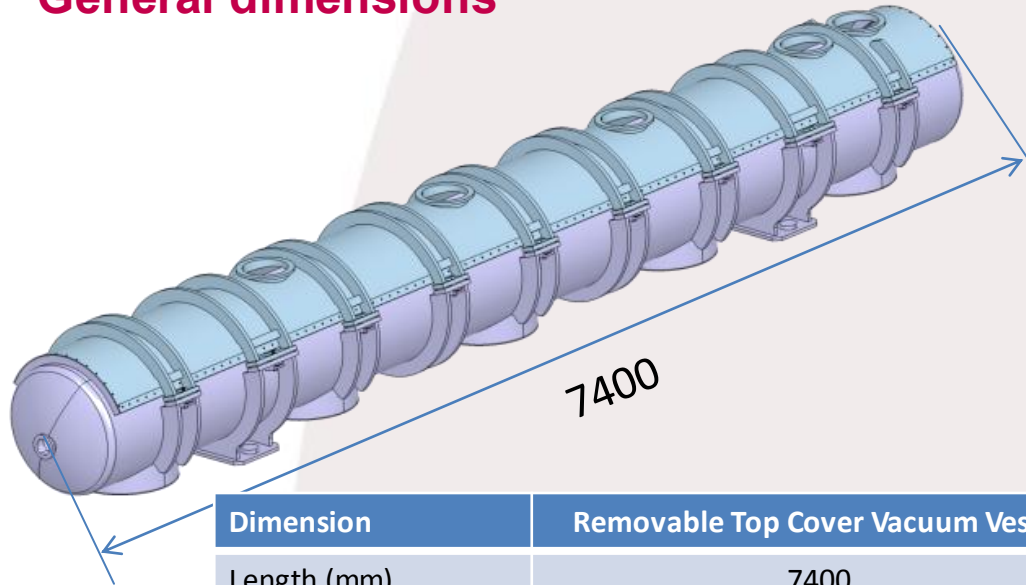


No Loss of alignment

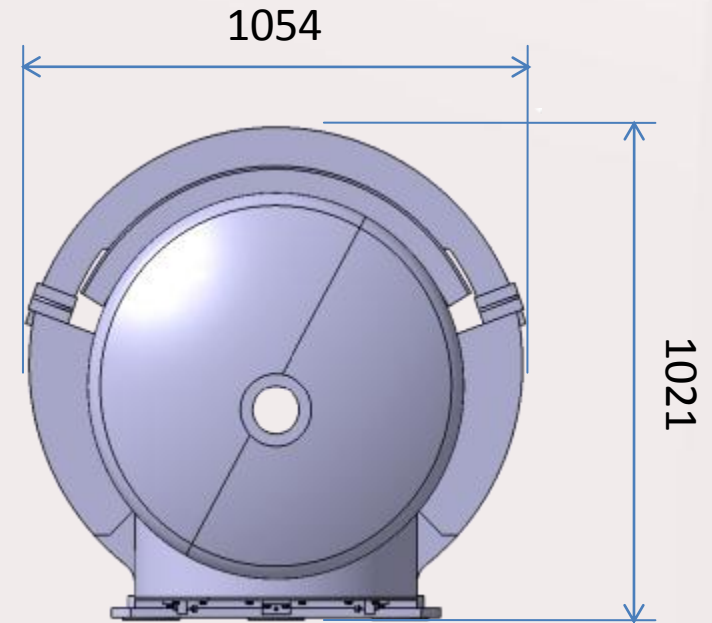
➤ Top Opened Vacuum Vessel

REMOVABLE TOP COVER VACUUM VESSEL

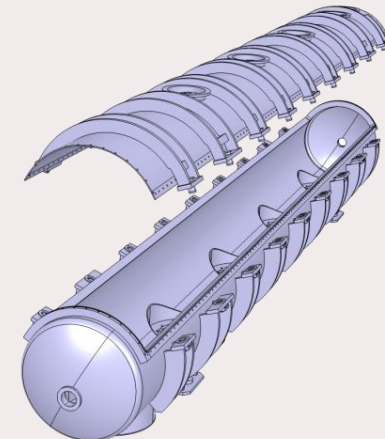
General dimensions



Dimension	Removable Top Cover Vacuum Vessel
Length (mm)	7400
Height (mm)	950
Thickness (mm)	10 (tube) and 6 (Top Cover)
Material	Steel and Stainless steel for flanges
Weight (ton)	2.4
Diameter (mm)	800/900
Number of openings	2 + 5 + 5 (2 beam flanges+ 5 coupler bearings ports + 5 access ports)
Number of Supports	2

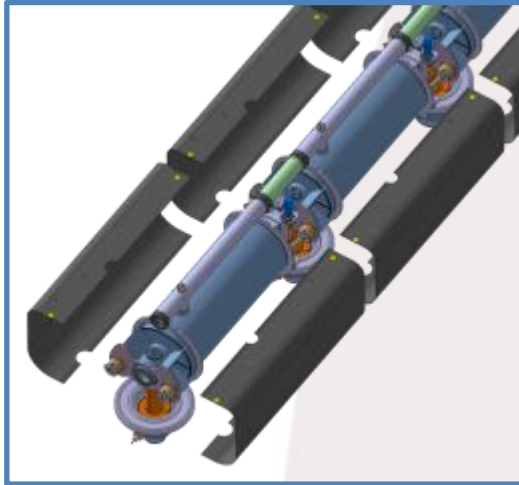


Smaller diameter
⇒ Easier maintenance access

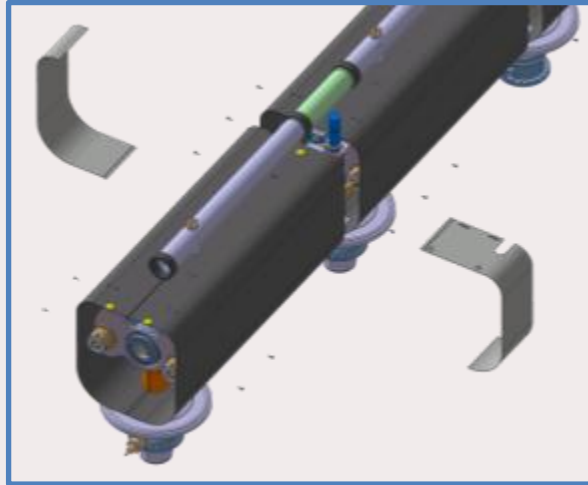


Cold magnetic shield

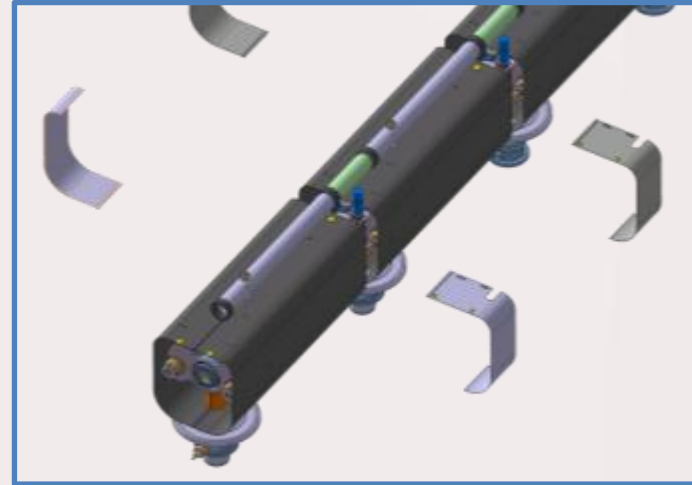
One shield for the string of cavities



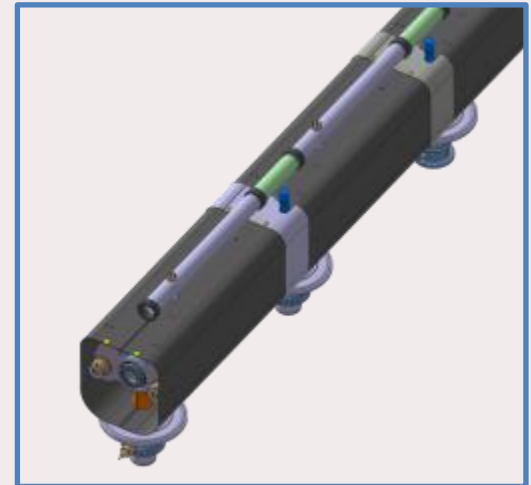
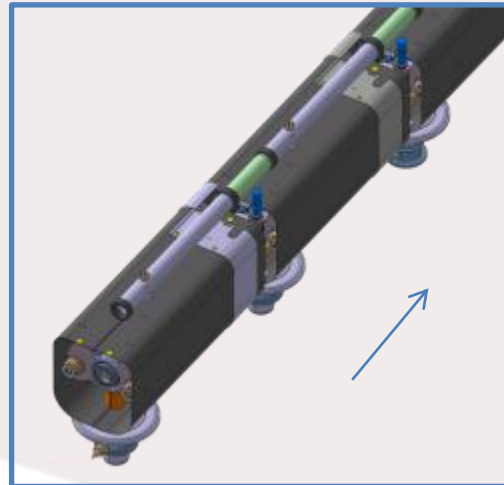
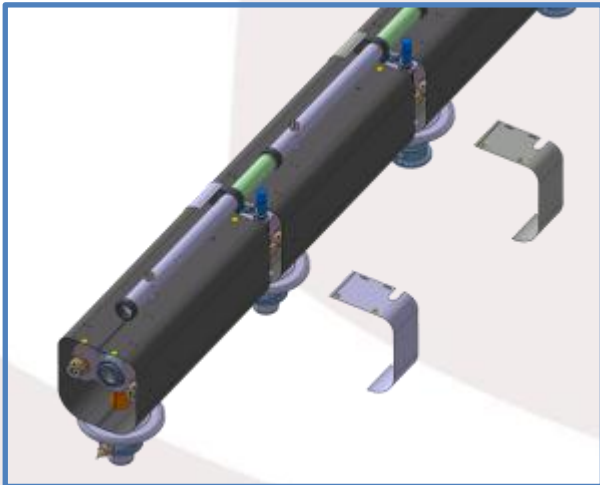
1- Positioning of the half screens



2- Fixation with screws on the tank interface

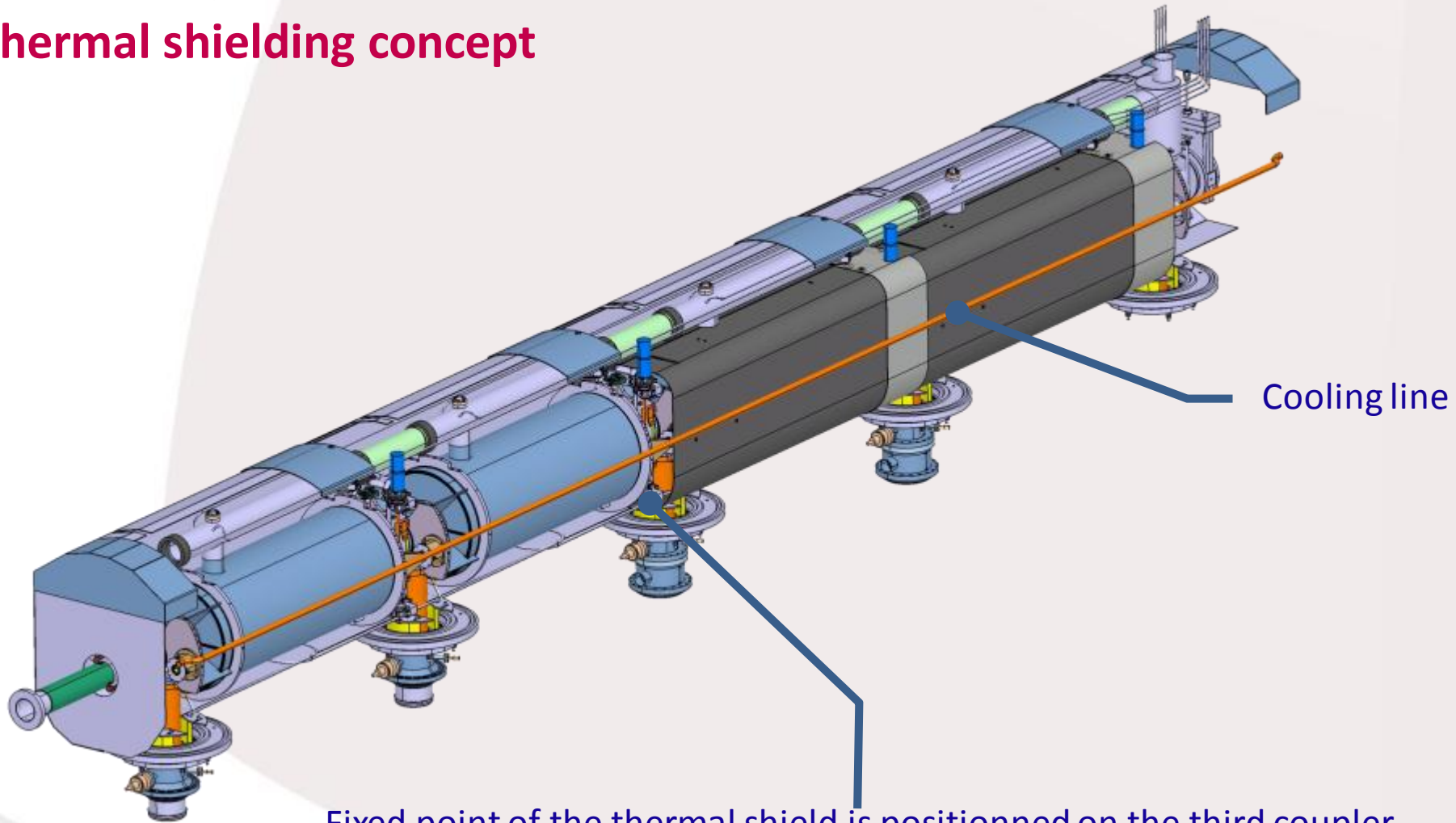


3- Positioning of the half sleeves



4,5 & 6- Positioning of the half sleeves

Thermal shielding concept



Fixed point of the thermal shield is positionned on the third coupler
→ 25mm of max thermal displacement (at extremities)

Recommendations

3.2 Vacuum vessel concept and choice of the associated assembly tooling / Possibility of extending the concepts to a full size 8-cavity cryo-module

Observation

- The design team is explicitly giving priority to the quality of positioning when preferring a removable top cover vacuum vessel.

Comment

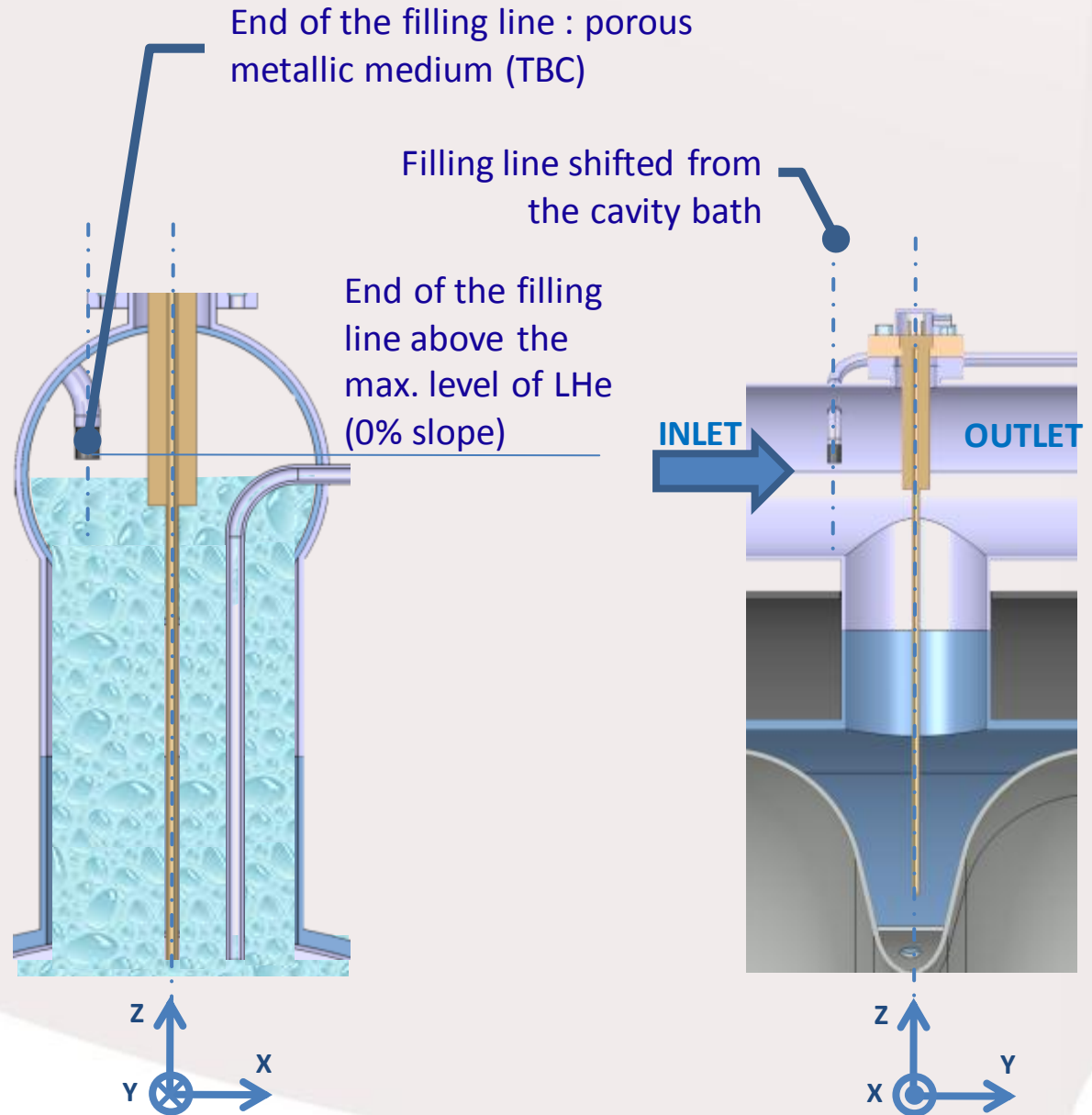
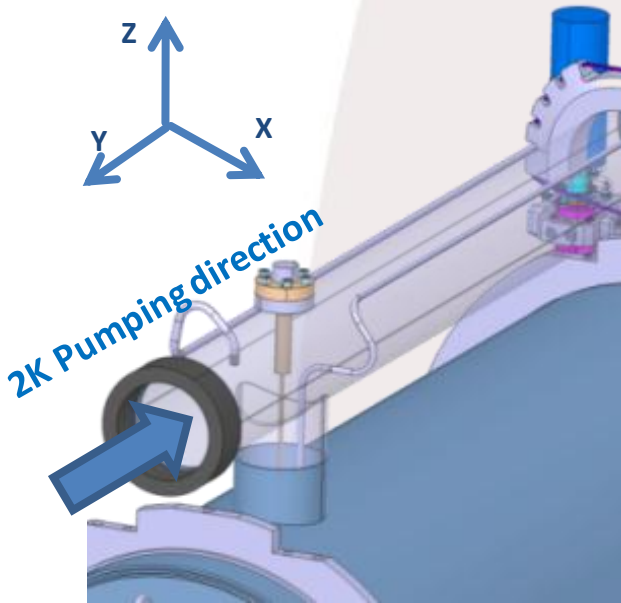
- The removable top cover solution is an interesting choice, simplifying the integration of the helium vessel inside the vacuum vessel
- The vessel flanges are critical because of their dimensions and flexibility. Extrapolation to 13 meters is a challenge. Cost impact has not been shown.

Recommendations

- Concerning vessel flanges: special treatment of the corners should be considered (large radii), machining should better be done after welding, X-rings joint could help.
- Study means to rigidify the cover in the axial direction.
- Proceed with transient FEM analysis.
- Start discussions with manufacturers on the Vacuum Vessel fabrication aspects.
- Prepare back-up solutions for the prototype vacuum vessel in case of tightness problems.
- Study the feasibility of a fully welded top-cover option as an alternative for series production.

TECHNICAL ASPECTS

Filling line



Phase separators

Coupler Phase separator

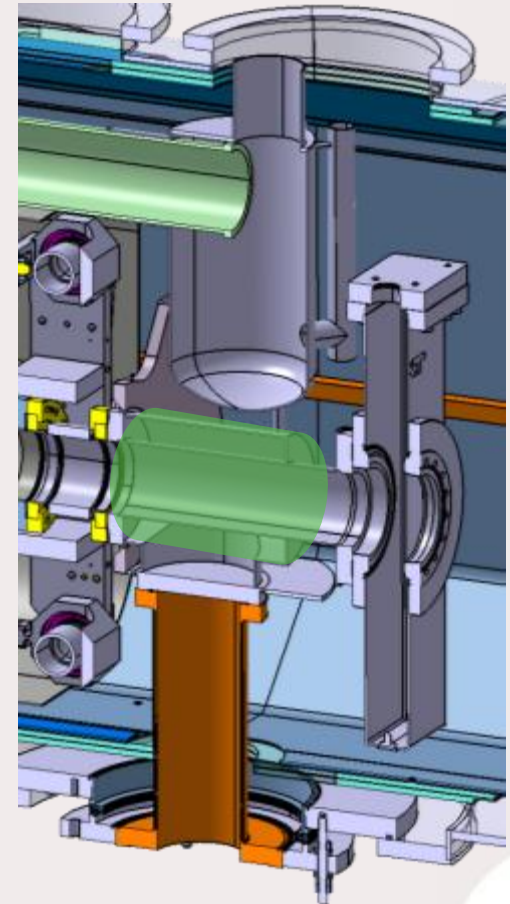
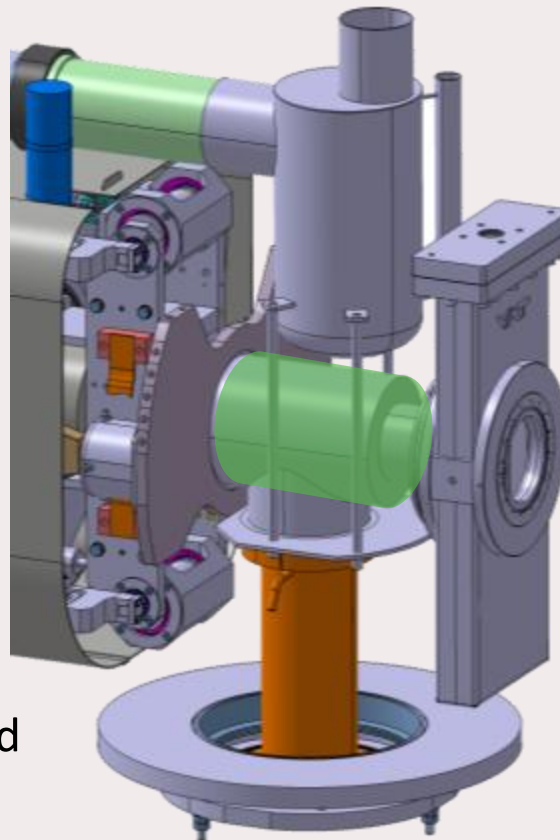
Volume: 1L; $T^\circ=4,5K$.

Positioned around the beam pipe

On the complementary support bi-tube.

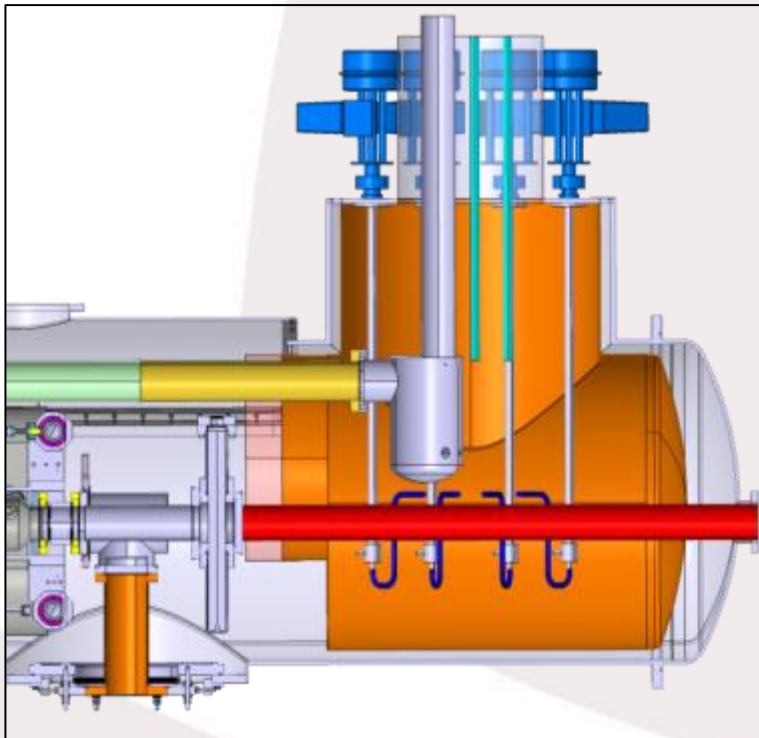
$T^\circ=4,5K > 2K$ will not affect the alignment ($\Delta L/L \ll 1$ for the double-walled tube)

NB: The double-walled tube will partially provide heat loss to generate helium vapor for the couplers cooling (0.1W).
(10W are required; heaters would be required for regulation - TBC)



Technical Service Module

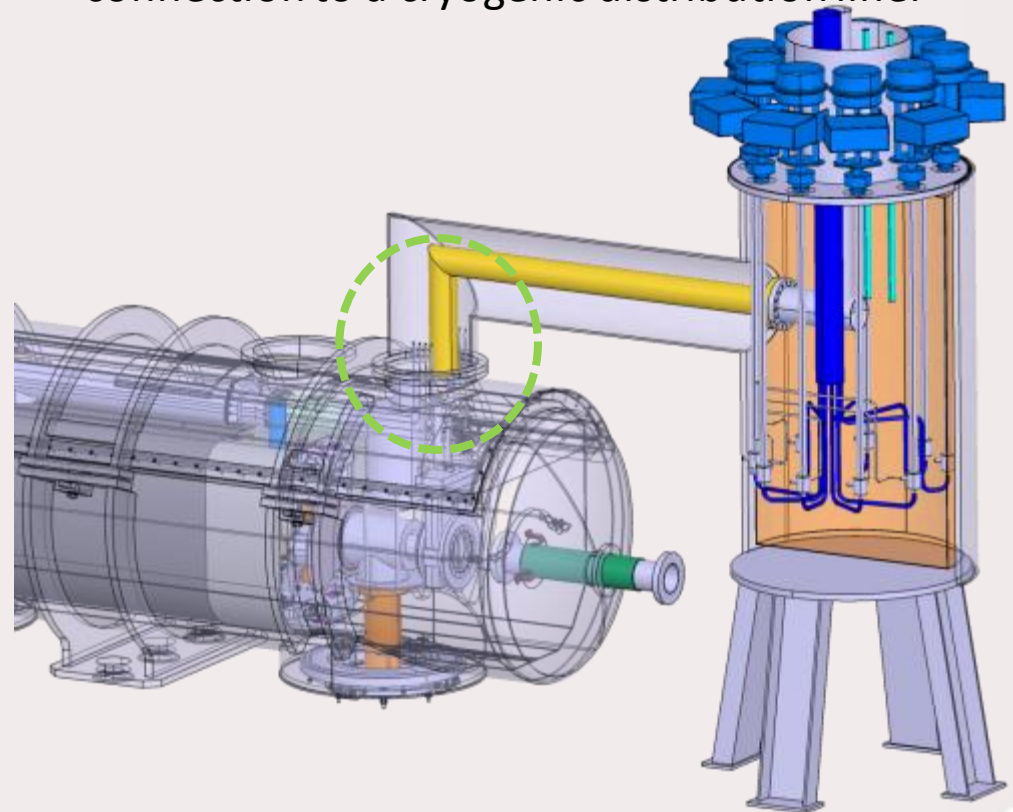
Technical Service Module
Including the cryogenic valves



Proposed solution:

cryogenic valves are placed in a separated cold box

Connection via a jumper to simulate the connection to a cryogenic distribution line.





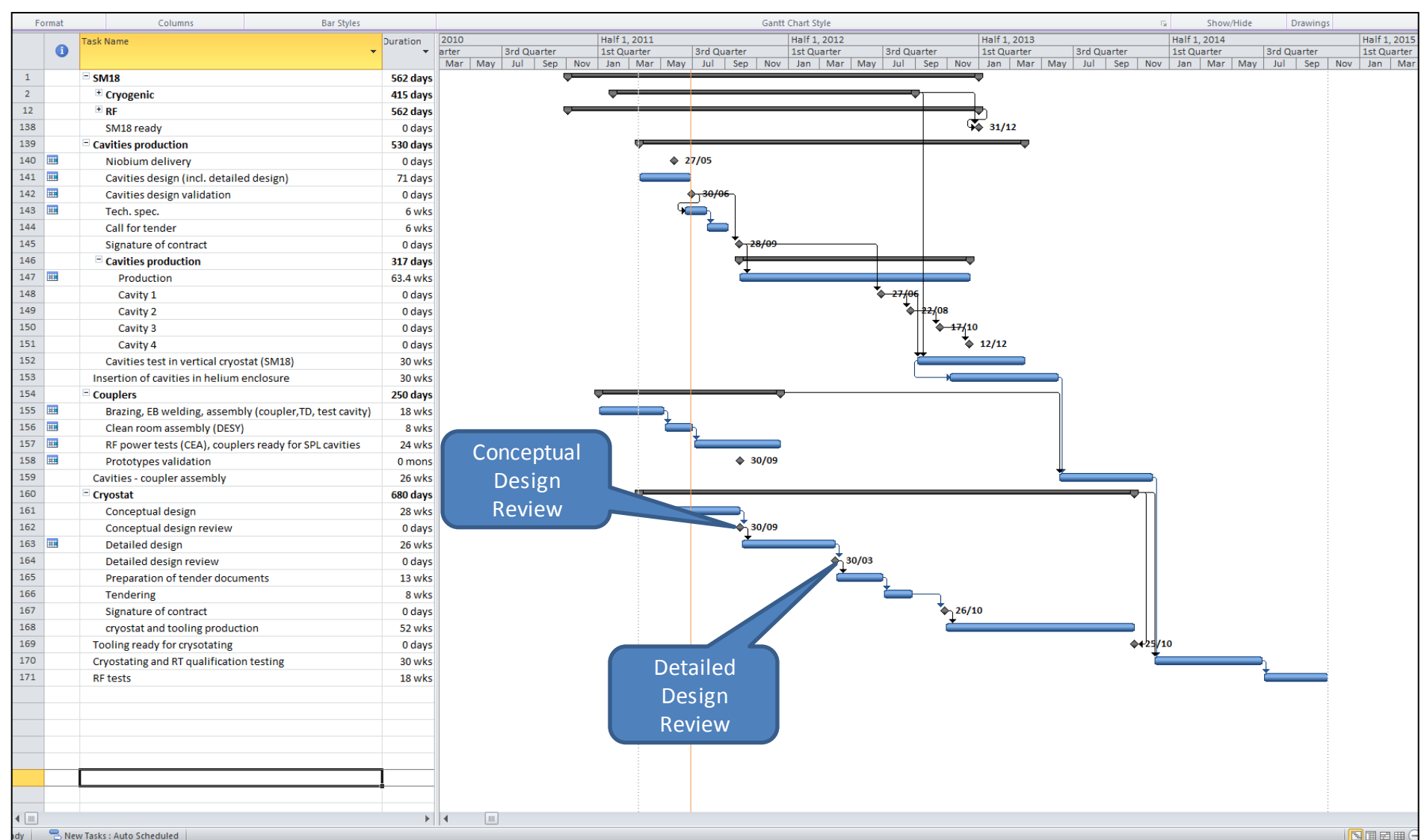
Conclusions from the review

- The review committee **did not identify show stoppers** in the concepts presented, **nor did it recommend major design changes**
- The committee **recognized the value of the original and innovative proposed concepts** (in particular supporting system and cryomodule vessel with top opening);
- and **recommended to pursue the work with additional design effort** (mechanical, both static and dynamic analysis, thermo-mechanics during transients...) and **underlined the importance of the mock-ups for testing**
- The committee suggested a number of changes:
 - Instrumentation (T gauges, heaters) moved to insulation vacuum
 - Vapour generation for coupler tube cooling via active heater (not by static heat load)
 - Introduce the possibility of welding vessel top cover in case of need (back-up for leak tightness)
 - ...
- Additional design effort is recommended (but is part of the detailed design phase!):
 - Cryogenic risk analysis
 - Define cool down and warm up requirements and constraints, and elaborate a procedure for cooling down the cold magnetic shield
 - Check compatibility with SM18 cryogenic infrastructure.
 - Develop a thermo-hydraulic model to analyze the robustness of the 2 K He level controls (RF transients).
 - Finalize the list of additional instrumentation for prototype validation and include it on the P&I diagram.
 - Study alternative for instrumentation feedthroughs without cold ceramic insulators.
 - ...
- **Improve project management & communication**: set-up a complete and up-to-date data-base listing the design parameters.

→ a project oriented working group with regular meetings (typically 1 per month) is probably the most appropriate answer



Schedule





*« nobody will ever blame you for not being on schedule or for overspending.
But you will be judged (and possibly blamed) on the results of your work »*

(CERN anonymous)



Thank you for your patience