

# BEAM-INDUCED HEATING / BUNCH LENGTH / RF AND LESSONS FOR 2012

Elias Métral (for ICE section & collaborators & equipment groups etc. Many thanks to all!)  
(20 + 10 min talk, 42 slides)

- ◆ **Observations of beam-induced heating in 2011**
- ◆ **News / work since then**
- ◆ **Several possible sources of heating => RF heating discussed only**
  - RF heating: broad-band vs. narrow-band (long. real.) impedance
  - Bunch / beam spectrum
  - Usual solutions to avoid RF heating
  - Heat transfers
  - Synchronous phase shift as a meas. of power loss & impedance
- ◆ **“Hot” topics: VMTSA, TDI and MKI**
- ◆ **Lessons for 2012 (and after)**

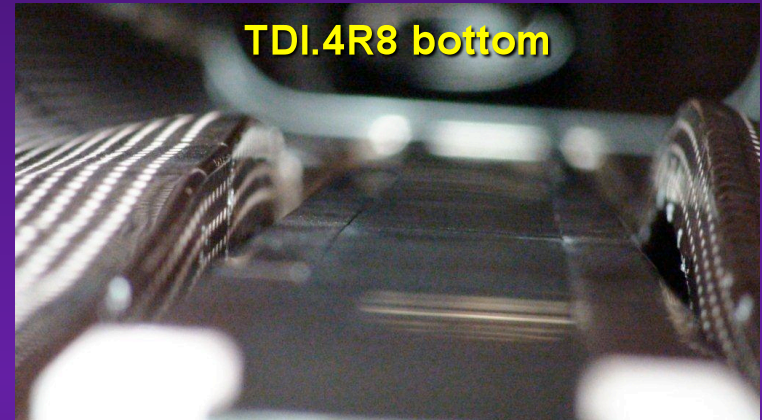
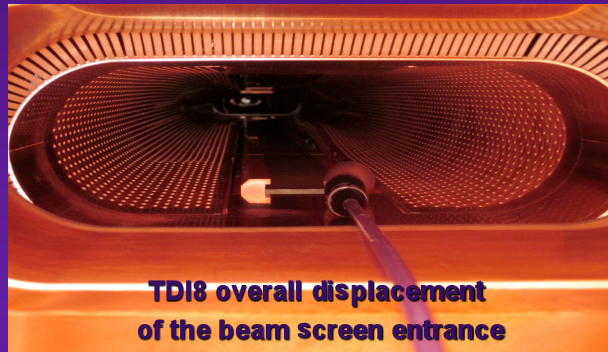
# 2011 run observations: Summary table (BenoitS, Evian11)

|             | observable                                  | Cooling? | Limits operation?  | better if bunch length increased | improves with time? | Is it happening to all similar devices                       |
|-------------|---|----------|--|----------------------------------|---------------------|--|
| TCP_B6L7_B1 | temperature                                 | water    | Yes, dump in Sept 17 <sup>th</sup> interlock increase from 55 to 70 degrees                            | yes                              | no                  | No (1/6)   |
| TCTVB.4R2   | temperature                                 | water    | Yes, dump in October 9 <sup>th</sup> interlock increase from 50 to 70 degrees                          | Yes                              | Not obvious         | No (1/4)   |
| TDI         | Vacuum Temperature (outside tank)           | no       | Not anymore, should be put in parking position   | ?                                | no                  | Yes (2/2)  |
| MKI         | Temperature and Rise time and delay (soon)  | no       | Yes (kick strength), and temp interlock increased from 50 deg to 62 deg. Needed to wait 4h in Oct 2011 | Yes                              | no                  | All are heating but MKI-8D seems to be heating more No (1/8) |
| Beam screen | Heat load computed from regulation response | yes      | No, except in one cell Q6R5  | Yes                              | no                  | No (only one)  |
| ALFA        | Temperature on the roman pots               | no       | Not yet (18deg increase in temperature in 2011, with margin of 40 degrees)                             |                                  | ?                   | Cooling was needed in TOTEM                                  |
| VM TSA      | Vacuum Spring broken after May              | no       | Yes (spring broken and dangling fingers)   |                                  | ?                   | Yes  |
| BSRT Mirror | Jitter in BSRT measurement                  |          | mirror is deforming and RF heating is suspected  |                                  |                     | N/A  |
| BGI         | Vacuum                                      |          | Probably not a heating issue   |                                  | No data             | N/A  |

## News / work since then

- ◆ **VMTSA** => (8 instead of 10) new modules installed in the LHC (shorter RF fingers + ferrite) + bench imped. meas. (see later)
- ◆ **TDI** => New observations: beam screen deformation

*Benoit Salvant et al.*



- ◆ **TCTVB.4R2** => Has been removed during the shutdown. TCTVB.4L2 (i.e. not the most critical one) has been looked at and some RF fingers were found not in contact
- ◆ **TCP.B6L7.B1** => Nothing obvious by visual inspection. Xrays still to be done but might be quite difficult
- ◆ **Q6R5 (beam screen)** => Xrays performed and nothing special
- ◆ **ALFA and MKI and TDI** => More simulations performed

# RF HEATING (1/17)

- ◆ **General formula in the case of  $M$  equi-spaced equi-populated bunches (Furman-Lee-Zotter1986)**

$$P_{loss} = M I_b^2 Z_{loss}$$

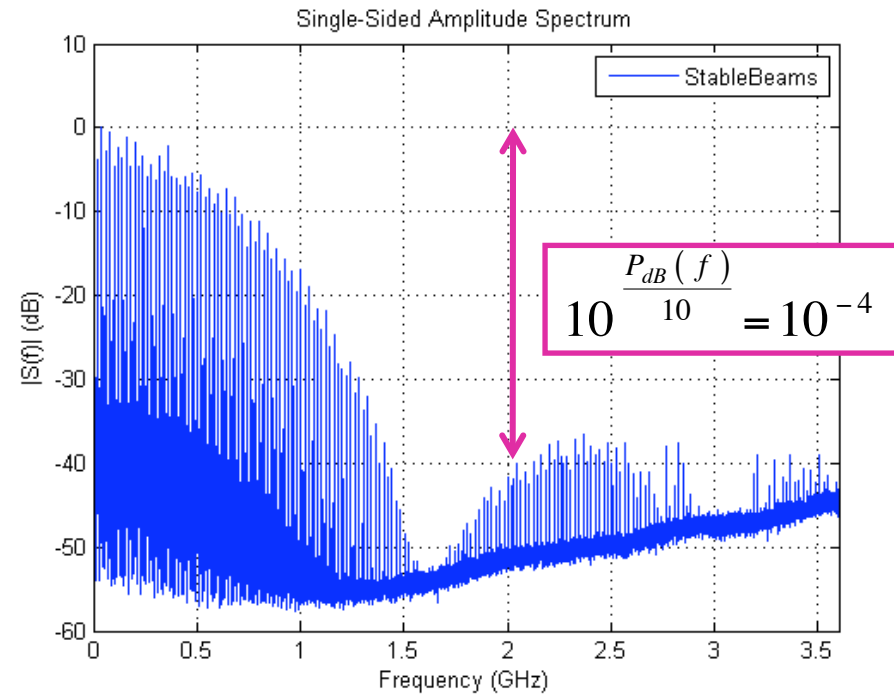
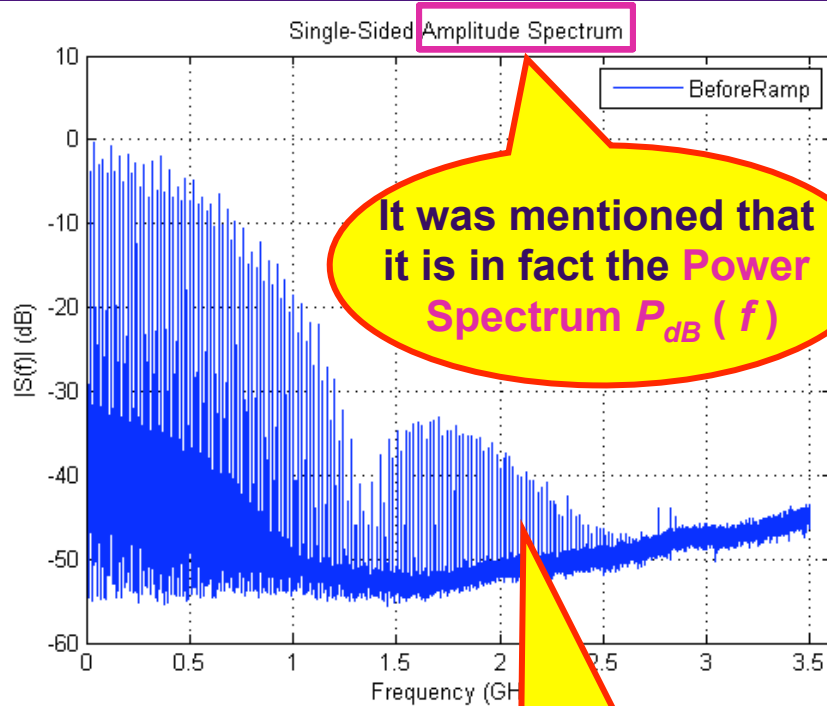
$$Z_{loss} = 2 M \sum_{p=0}^{\infty} \text{Re} [ Z_l ( p M \omega_0 ) ] \times \text{PowerSpectrum} [ p M \omega_0 ]$$

$$I_b = N_b e f_0$$
$$\omega_0 = 2 \pi f_0$$

- **Broad-band impedance  $\Rightarrow$  Sum can be replaced by an integral ( $M$  in front disappears)  $\Rightarrow P_{loss} \propto M$  (i.e. it is  $M$  times the single-bunch case)**
- **(Very) narrow-band impedance  $\Rightarrow$  Only 1 term in the sum  $\Rightarrow P_{loss} \propto M^2$  (i.e. it is **NOT**  $M$  times the single-bunch case)**

# RF HEATING (2/17)

Measurements on B1 by ThemisM and PhilippeB on fill # 2261

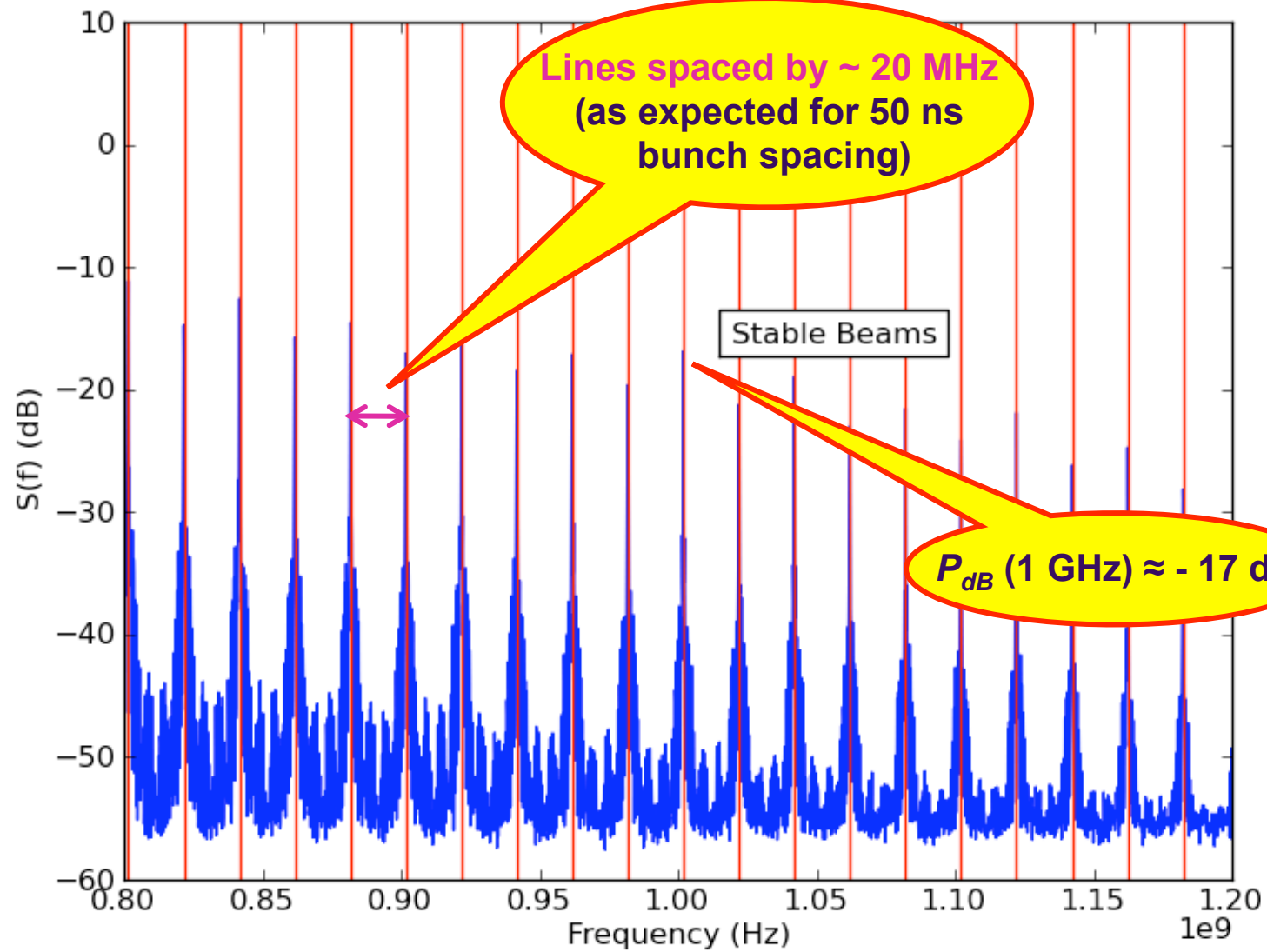


Coupled-bunch lines spaced by  $M f_0 \sim 20$  MHz (for 50 ns bunch spacing) => It would be  $\sim 40$  MHz for 25 ns

$$M_{50} = 1782$$

$$M_{25} = 3564$$

# RF HEATING (3/17)



# RF HEATING (4/17)

From theory

$$\tau_b = 4\sigma$$

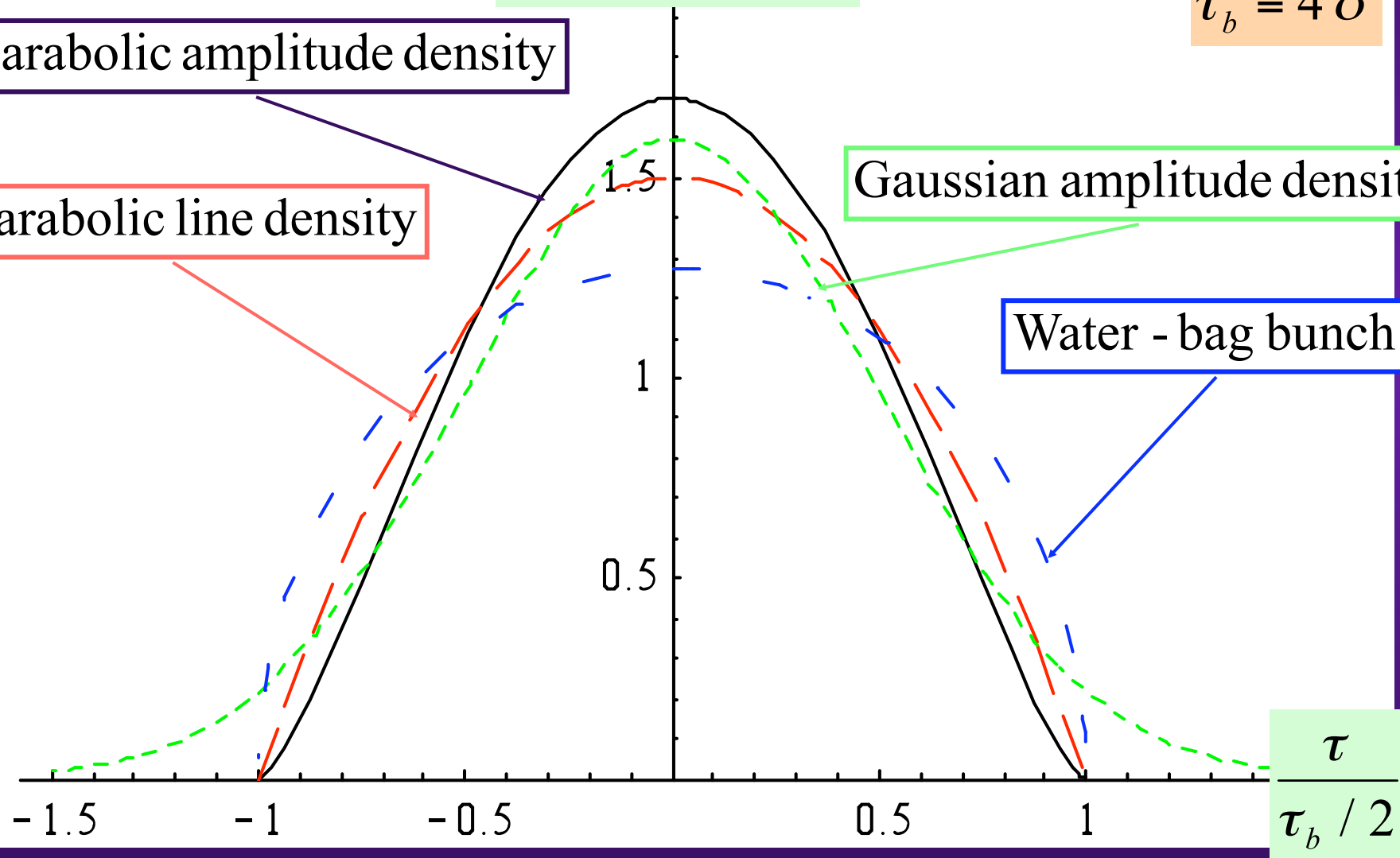
Line density  $\times \tau_b$

Parabolic amplitude density

Parabolic line density

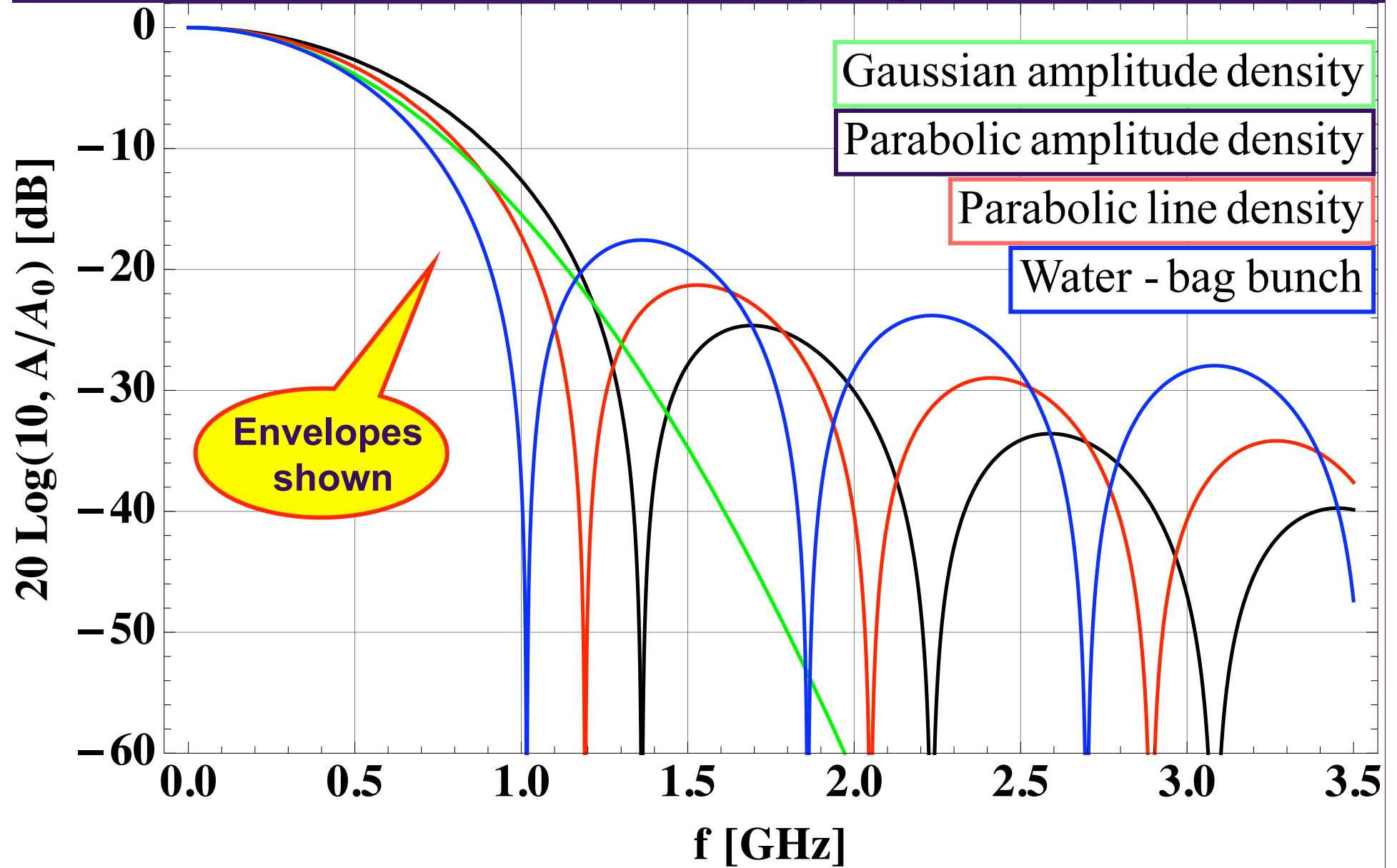
Gaussian amplitude density

Water - bag bunch



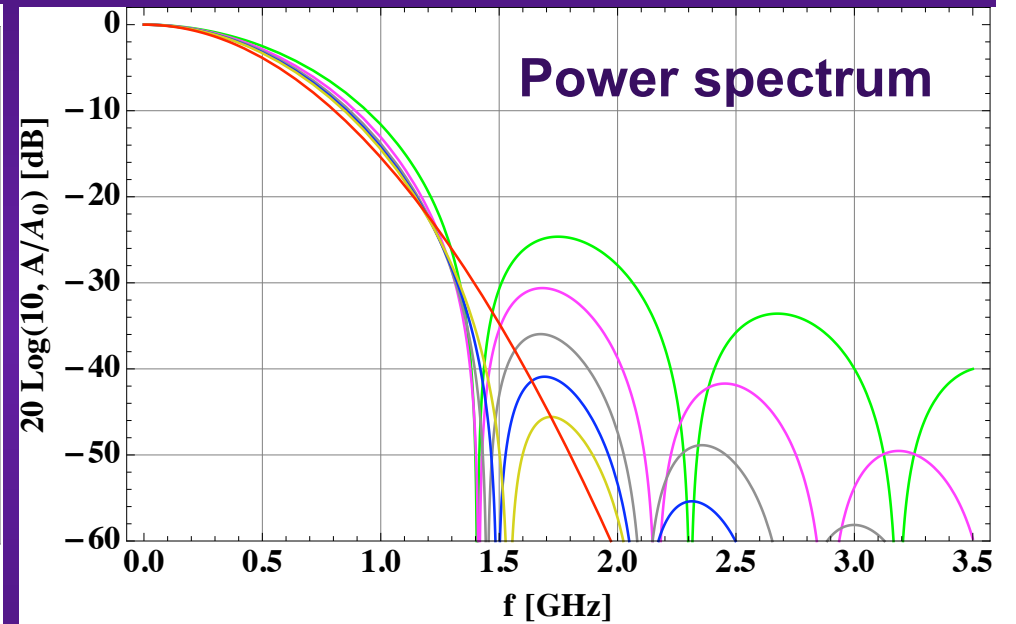
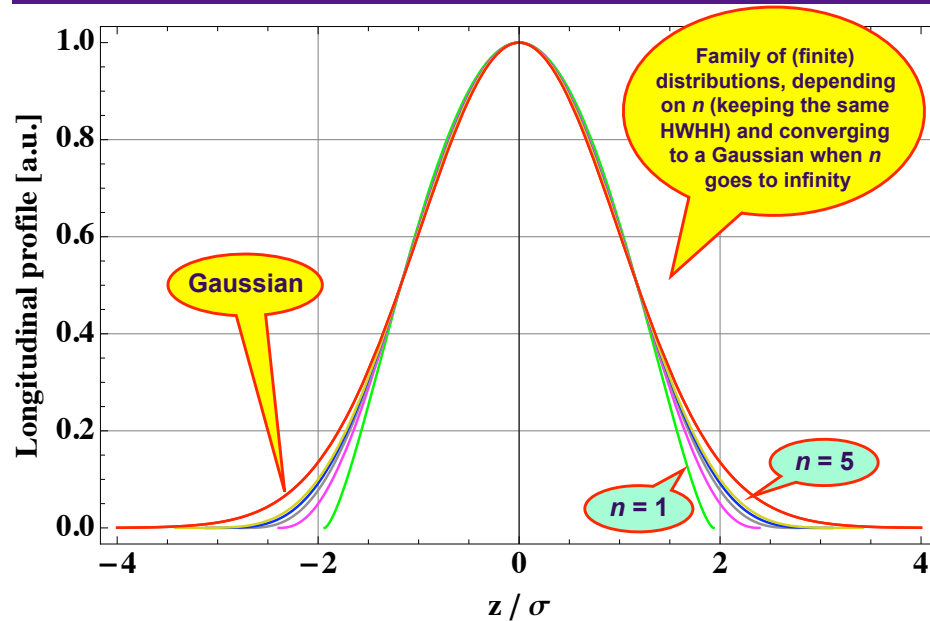
# RF HEATING (5/17)

$\tau_b = 1.2$  ns



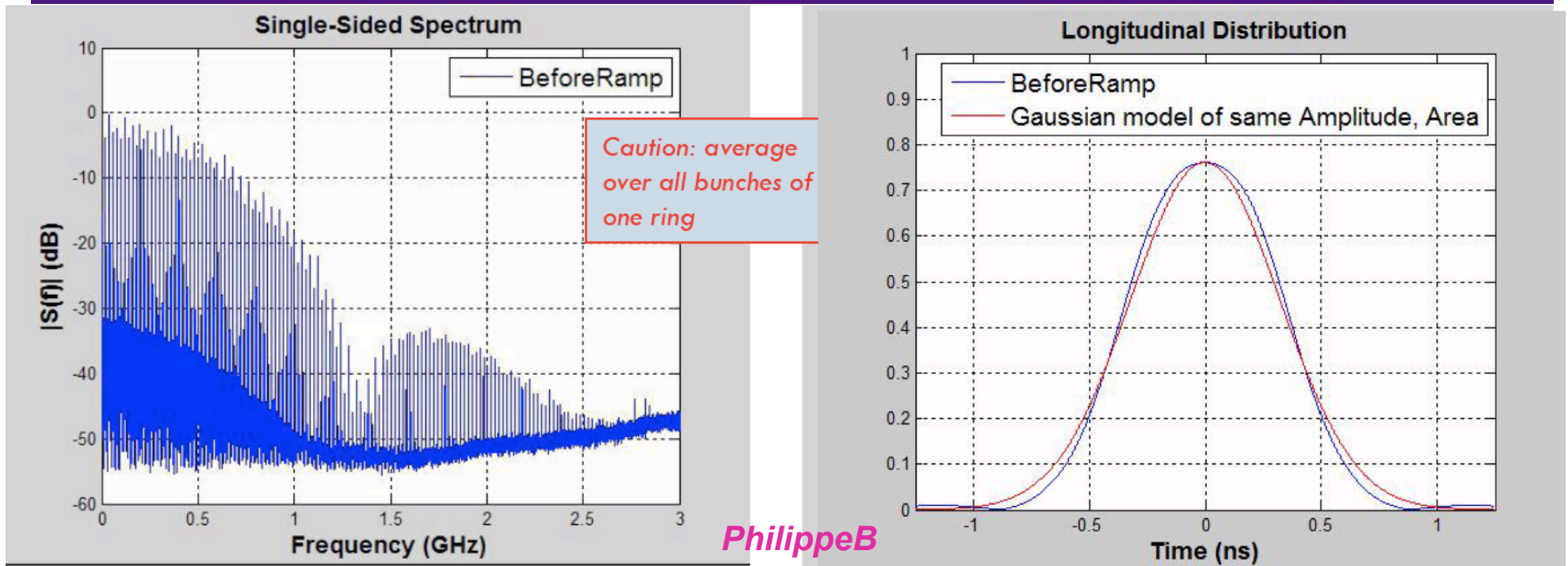


# RF HEATING (6/17)



# RF HEATING (7/17)

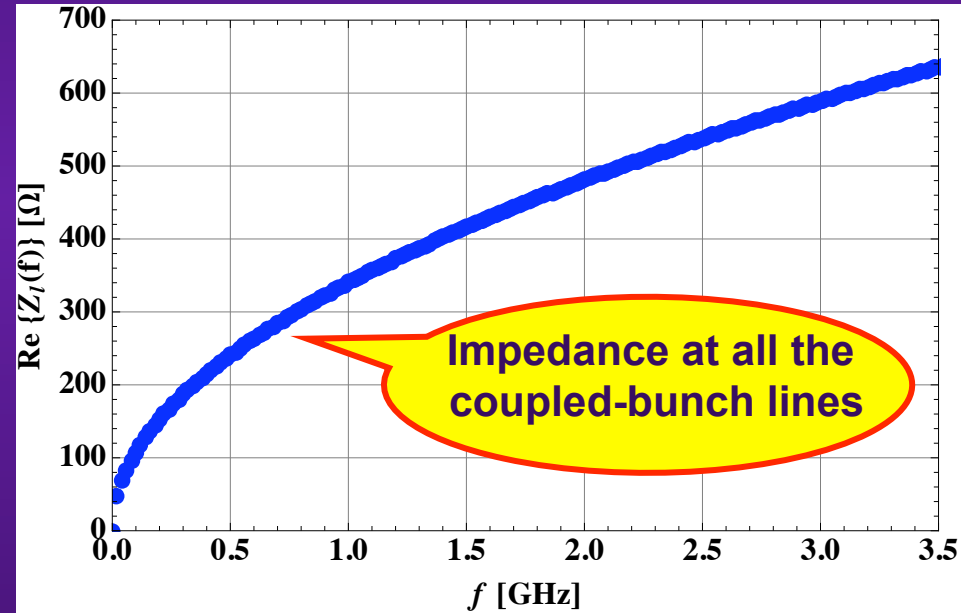
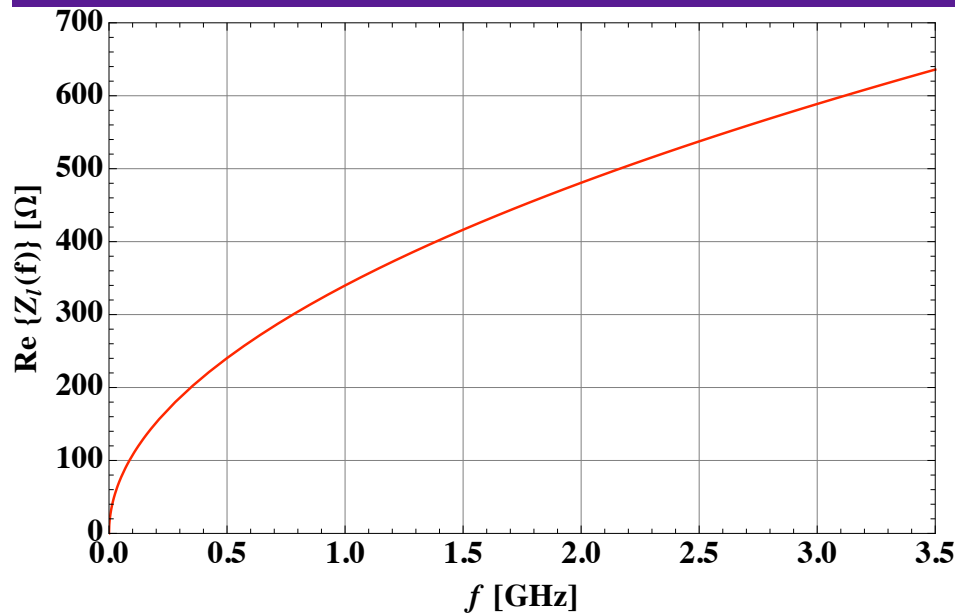
- ◆ By taking the inverse Fourier Transform, ThemisM and PhilippeB found the following distribution



- ◆ Studies also by ThomasB and ElenaS with the PD Schottky => 2 peaks are visible

# RF HEATING (8/17)

- ◆ Consider 1<sup>st</sup> the case of the Resistive-Wall impedance => Application to the case of the LHC beam screen (neglecting the holes, whose contribution has been estimated to be small, and the weld for the moment)



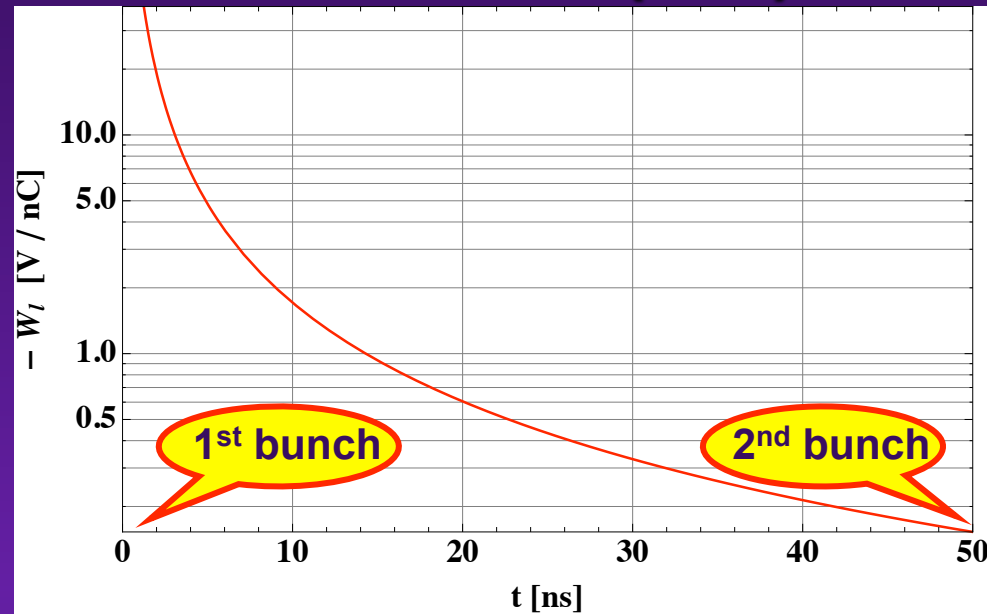
$$Z_l(f) = (1 + j) \frac{L}{2\pi b} \sqrt{\frac{\pi f \rho Z_0}{c}}$$

$$\begin{aligned} \text{LHC circumference} &= L \\ &= 2\pi R = 26658.883 \text{ m} \end{aligned}$$

$$\rho_{Cu}^{20K} = 5.5 \times 10^{-10} \text{ } \Omega\text{m}$$

$$b = \text{beam screen half height} = 36.8 / 2 = 18.4 \text{ mm}$$

# RF HEATING (9/17)



$$f(p M \omega_0) = \text{Re} \left[ Z_l(p M \omega_0) \right] \times \text{PowerSpectrum} \left[ p M \omega_0 \right]$$

$$\sum_{p=0}^{\infty} f(p M \omega_0) \approx \frac{1}{M \omega_0} \int_{x=0}^{\infty} f(x) dx$$

$$Z_{loss} = 2 M \sum_{p=0}^{\infty} f(p M \omega_0)$$

$\Rightarrow$

$$P_{loss} = \frac{2 M I_b^2}{\omega_0} \int_{x=0}^{\infty} f(x) dx$$

## RF HEATING (10/17)

- Assuming a Gaussian bunch

$$P_{loss/m}^{G,RW,1layer} = \frac{1}{2\pi R} \Gamma\left(\frac{3}{4}\right) \frac{M}{b} \left(\frac{N_b e}{2\pi}\right)^2 \sqrt{\frac{c \rho Z_0}{2}} \sigma_t^{-3/2} \approx 85 \text{ mW/m}$$

$$\Gamma\left(\frac{3}{4}\right) = 1.23$$

Euler gamma function

$$M_{50} = 1782$$

$$N_b = 1.4 \times 10^{11} \text{ p/b}$$

$$\sigma_t = 0.30 \text{ ns}$$

- Assuming the real power spectrum it would give the same result within few tens of %
- With the 25 ns beam and 2 times more bunches, it would give a factor 2 more power

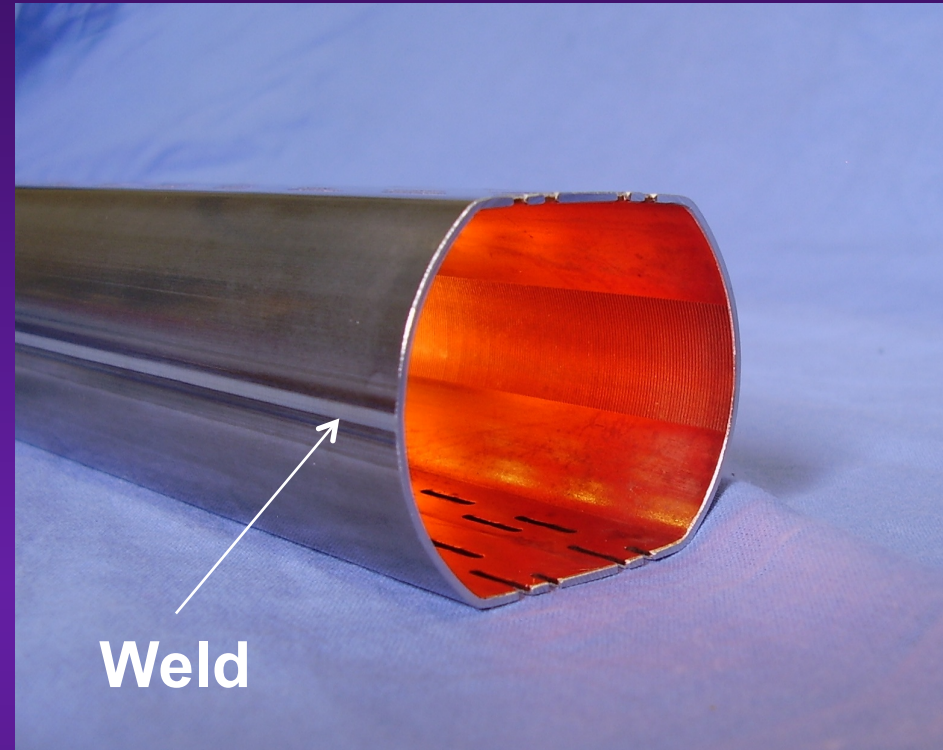
# RF HEATING (11/17)

- ◆ Consider now the longitudinal weld

$$\rho_{Cu}^{20K} = 5.5 \times 10^{-10} \Omega m$$

$$\rho_{SS}^{20K} = 6 \times 10^{-7} \Omega m$$

$$\frac{\Delta_l^{Weld}}{2\pi b} = \frac{2}{2\pi \times 18.4} = \frac{1}{\pi \times 18.4} \approx \frac{1}{60}$$



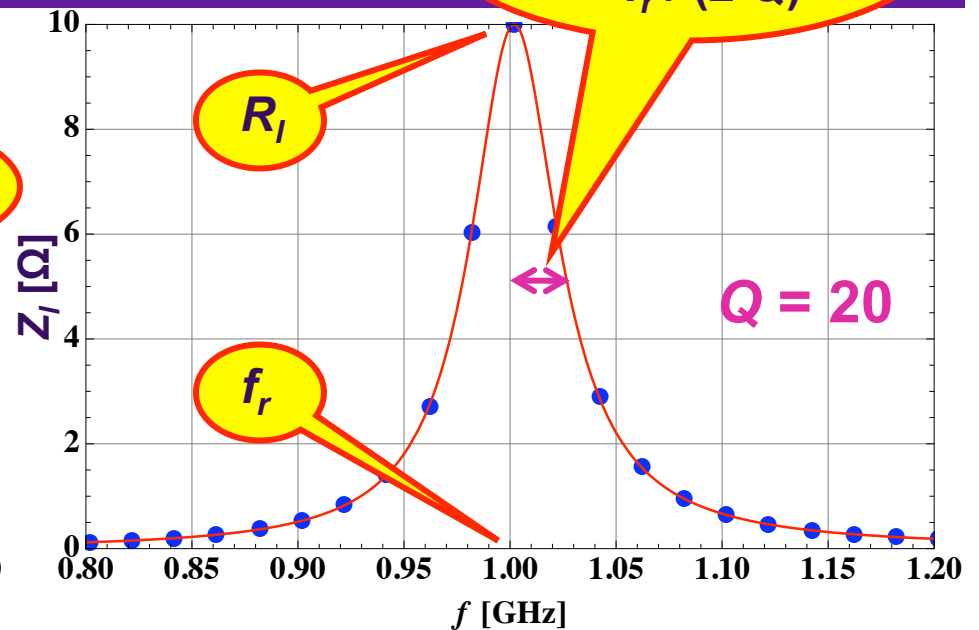
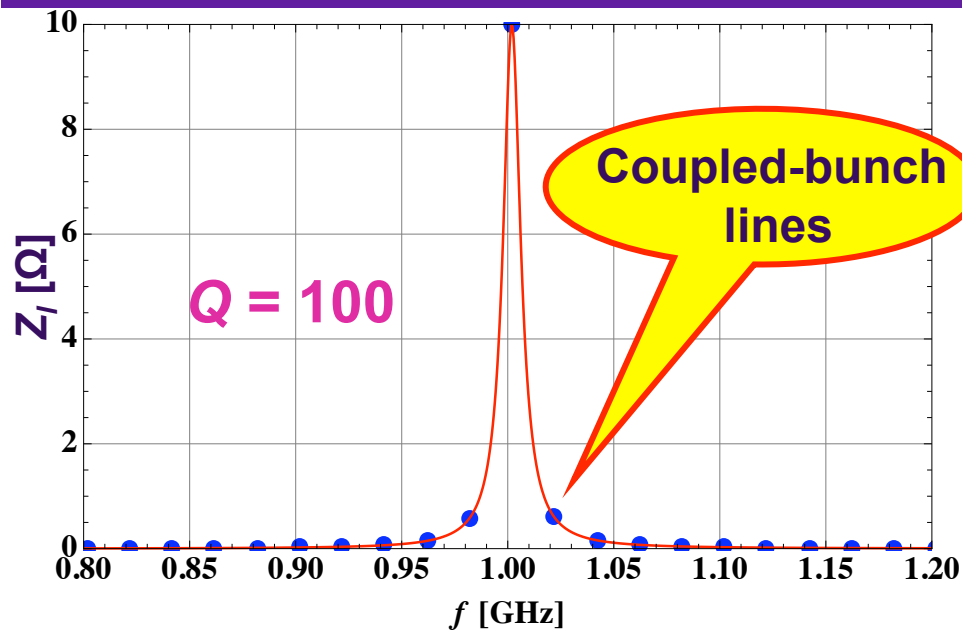
⇒

$$\frac{P_{loss/m}^{Weld}}{P_{loss/m}^{G,RW,1layer}} \approx \sqrt{\frac{\rho_{SS}^{20K}}{\rho_{Cu}^{20K}}} \times \frac{\Delta_l^{Weld}}{2\pi b} \approx 57\%$$

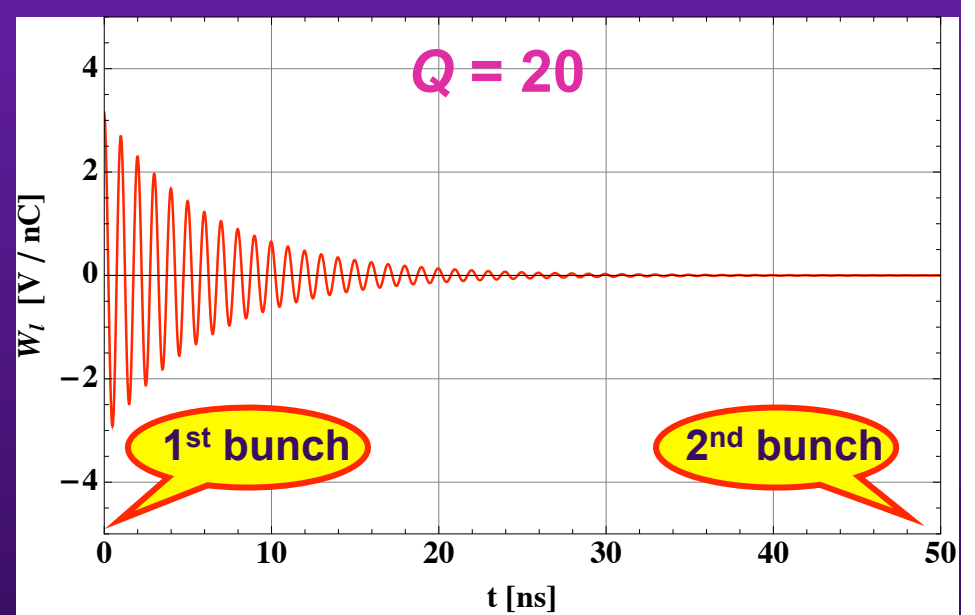
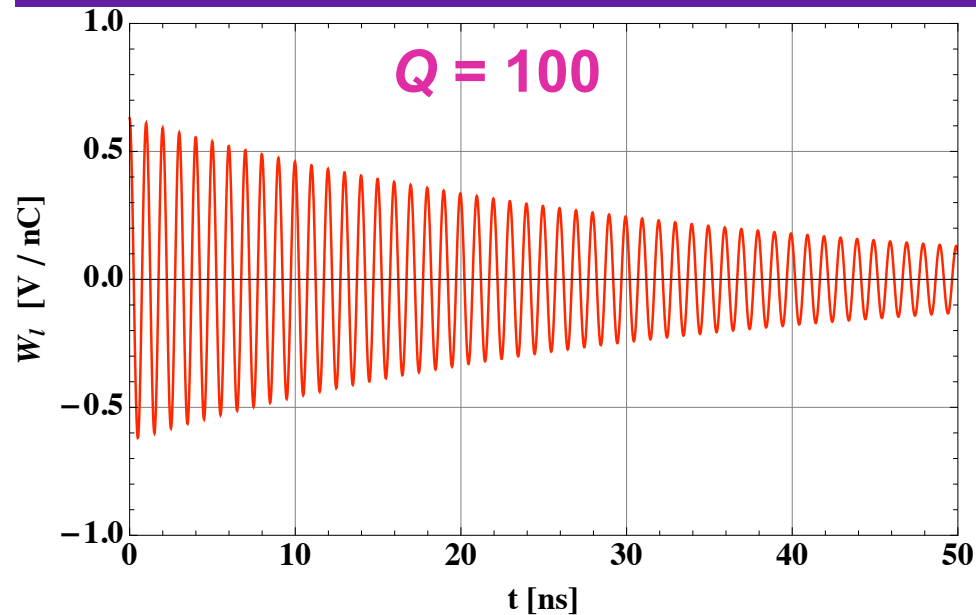
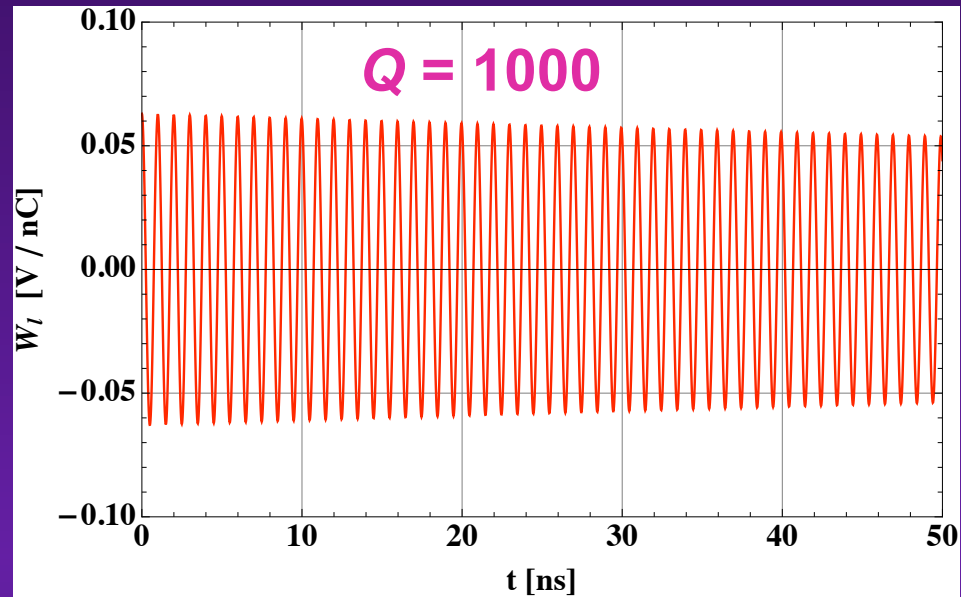
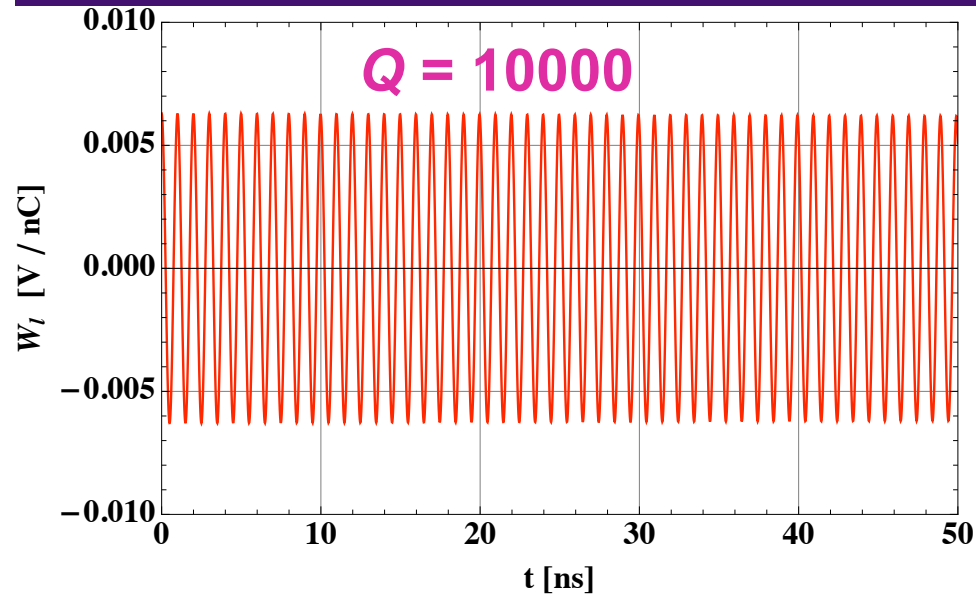
# RF HEATING (12/17)

◆ Consider now the case of a narrow resonance (trapped mode due to the geometry) => 3 parameters:

- Resonance frequency => Assumed to be here  $f_r = 1$  GHz
- Shunt impedance => Assumed to be here  $R_l = 10 \Omega$
- Quality factor  $Q$  => Scanned below



# RF HEATING (13/17)





## RF HEATING (14/17)

- Power loss formula for the case of a (sharp) resonance (i.e. with only 1 line)

$$P_{loss} = (M I_b)^2 \times R_l \times 10^{\frac{P_{dB}(f_r)}{10}}$$

Total beam current

$P_{dB}(f_r)$  is the power in dB read from a power spectrum (computed or measured) at the frequency  $f_r$

- ✧ A.N.:  $M = 1380$ ,  $N_b = 1.45E11$  p/b  $\Rightarrow M \times I_b = I_{total} \approx 0.36$  A,  
 $R_l = 10$  Ohm and  $f_r = 1$  GHz  $\Rightarrow P_{dB}(1 \text{ GHz}) \approx -17$  dB (see slide 6)  
 $\Rightarrow P_{loss} \approx 26$  mW

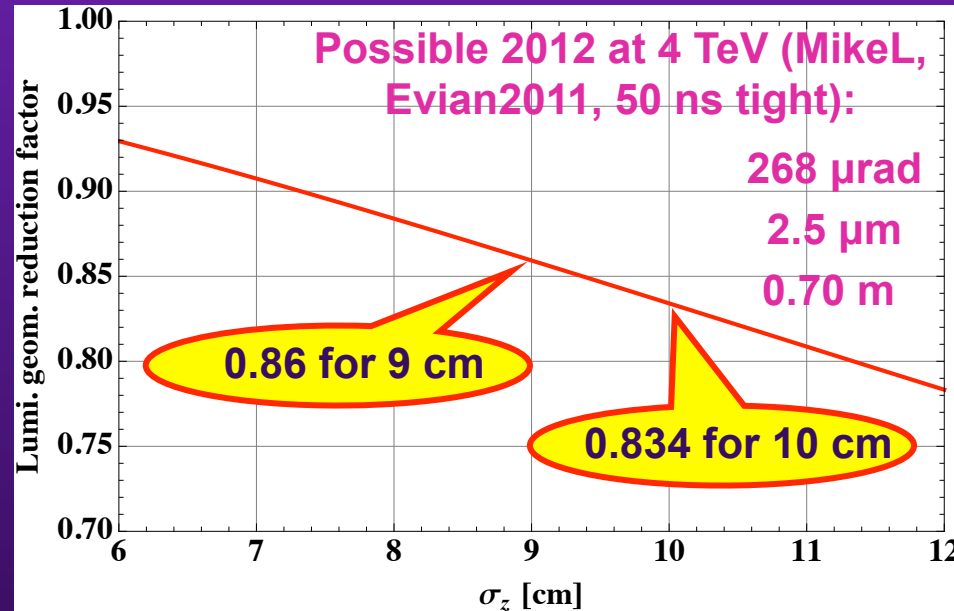
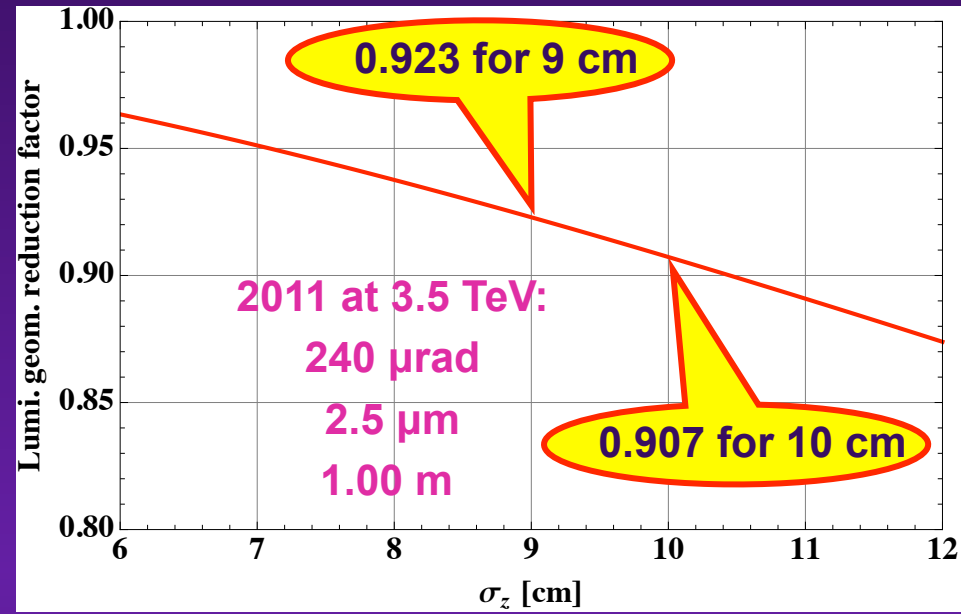
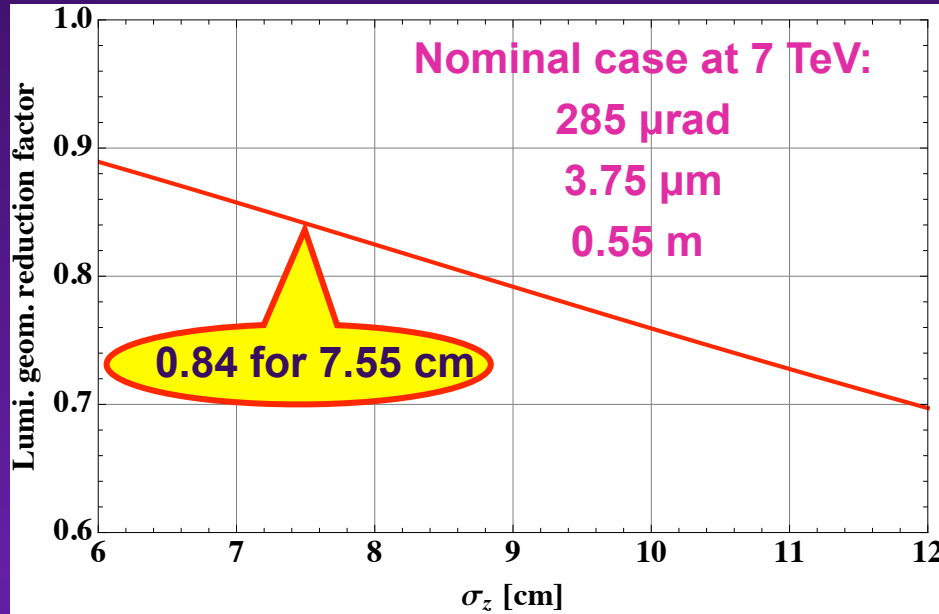
- Note that in the case of a Gaussian bunch, the power loss is

$$P_{loss}^{Gaussian} = (M I_b)^2 \times R_l \times e^{-(2\pi f_r \sigma_\tau)^2}$$

## RF HEATING (15/17)

- ◆ **Usual solutions to avoid RF heating => Depending on the situation**
  - Increase the distance between the beam and the equipment
  - Coating with good conductor
  - Close large volumes (could lead to resonances at low frequency) and smooth transition => Beam screens, RF fingers etc.
  - Put ferrite (close to maximum of magnetic field of the mode):
    - Adding a material with losses the Q factor is decreased (by few tens, say 50), while the R / Q is conserved (depends only on the geometry)
    - =>  $R_2 = (R_1 / Q_1) \times Q_2$  is decreased by 50
    - => Power loss is decreased accordingly if Q still sufficiently high or less if other coupled-bunch lines are involved
    - The ferrite should absorb the remaining (much smaller) power
    - Note that the resonance frequency should also slightly decrease
  - Bunch length increase, but then lumi. geom. red. factor + possible losses from the bucket (to be studied in detail)

# RF HEATING (16/17)



$$F = 1 / \sqrt{1 + \left( \frac{\theta_c \sigma_z}{2\sigma^*} \right)^2}$$

# RF HEATING (17/17)

## ◆ Heat transfers

- Convection: **none in vacuum**
- Radiation: **usually temperature already quite high**
- Conduction: **if good contacts + good thermal conductivity**
- Active cooling => **LHC strategy: All the near beam elements in the LHC are water cooled (Ralph Assmann)**

## ◆ Synchronous phase shift as a meas. of power loss & impedance

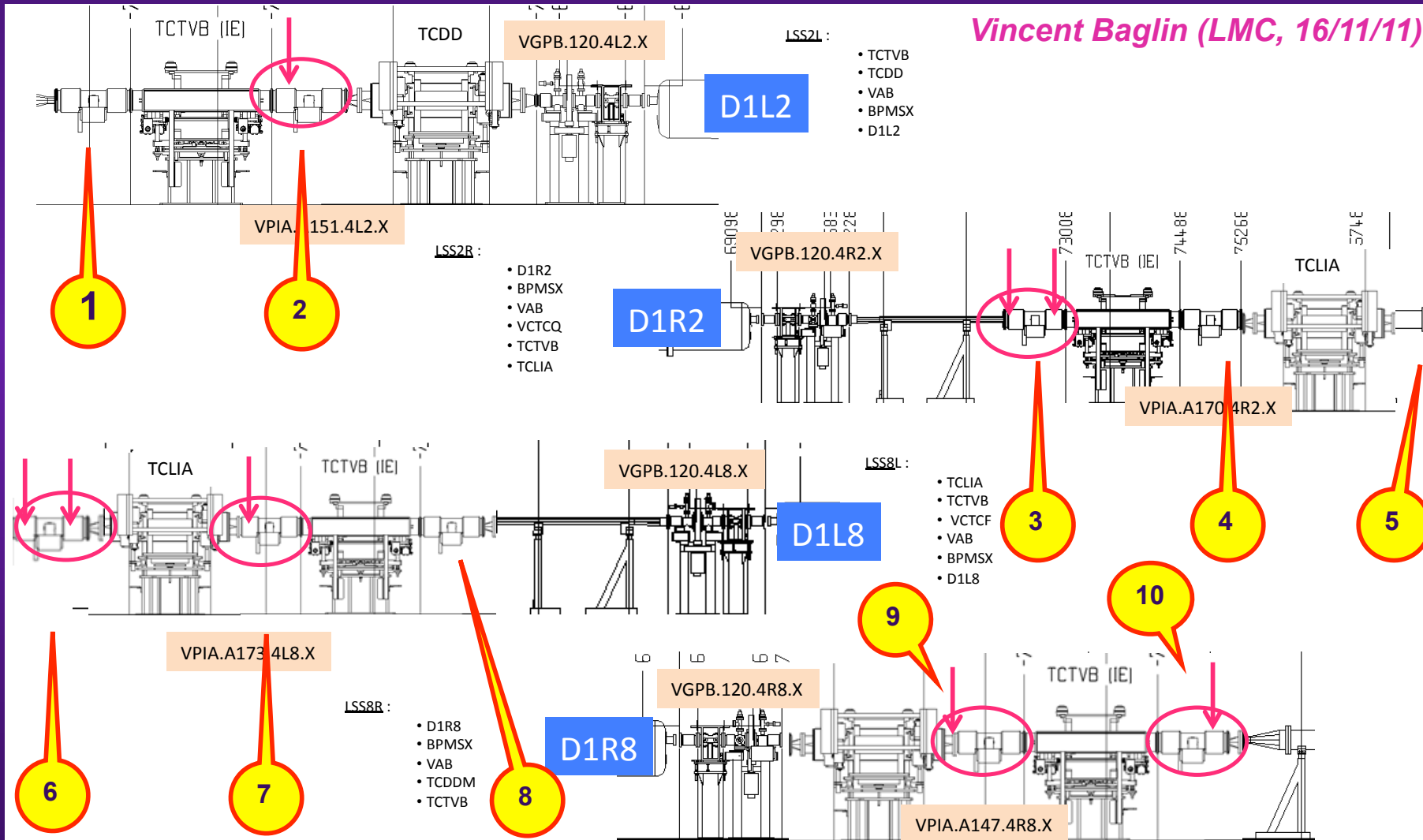
- Bunch power gain with no imped.:  $\Delta P_{bunch,1} = e \hat{V}_{RF} \sin \phi_{s1} f_0 N_b$
- Delta bunch power due to impedance:

$$\Delta P_{bunch,1 \rightarrow 2} = \Delta P_{bunch,2} - \Delta P_{bunch,1} = e \hat{V}_{RF} f_0 N_b \left( \sin \phi_{s2} - \sin \phi_{s1} \right)$$
$$\approx e \hat{V}_{RF} f_0 N_b \cos \phi_{s1} \Delta \phi_s \quad \text{with} \quad \Delta \phi_s = \phi_{s2} - \phi_{s1}$$

- **Scaling with # of bunches  $M$  => Depends on the impedance!**

# VMTSA (1/5)

- ◆ 10 modules (each of 2 bellows) in total in 2011. 8 bellows were found with defaults (see arrows below). 2 modules removed for 2012



## VMTSA (2/5)

# Typical default, DCUM 3259.3524

Left side

Vincent Baglin (LMC, 16/11/11)

Side view (xray from corridor to QRL)

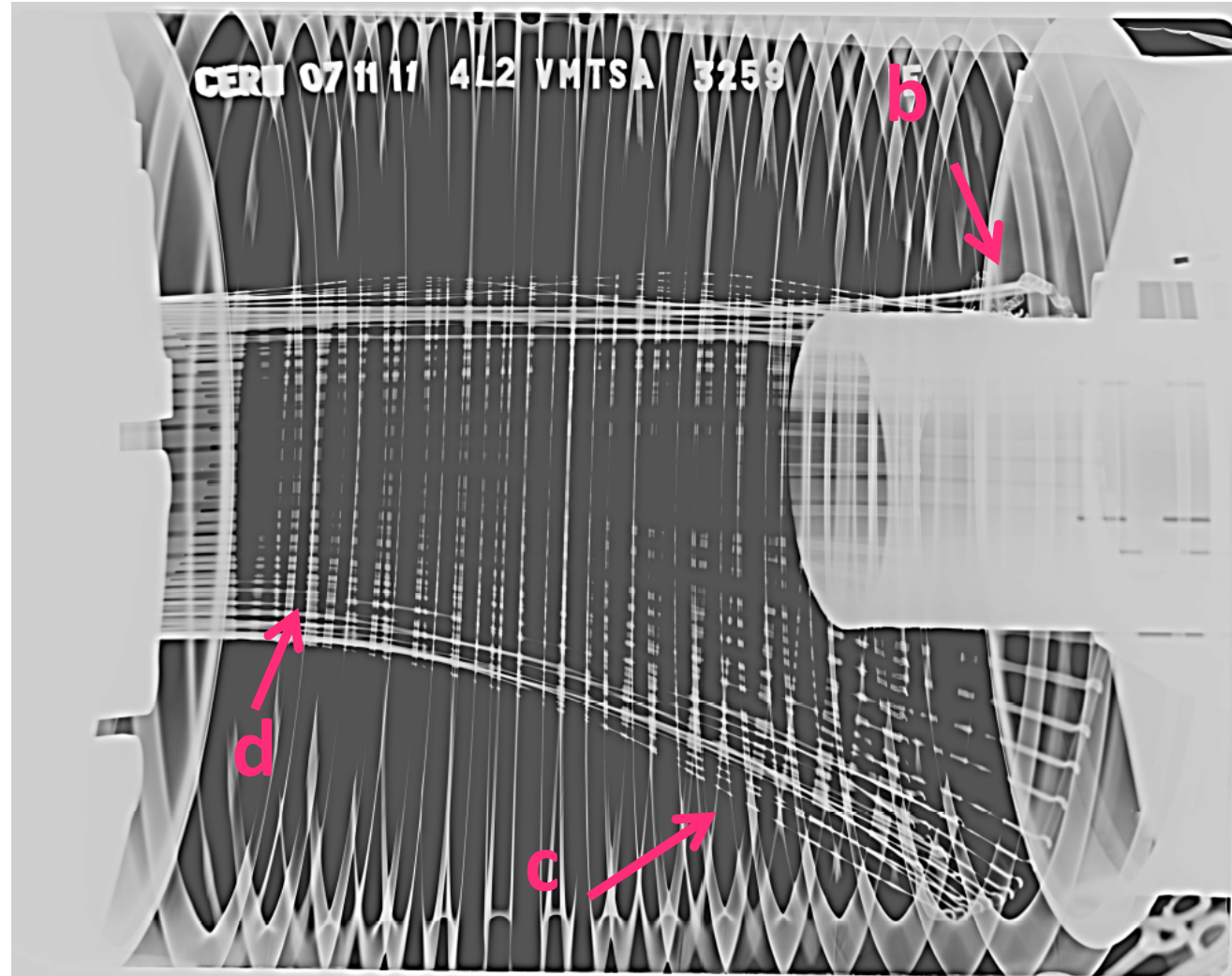
b) Metallic noise due to loose spring when hitting vacuum chamber

c) RF fingers falling due to broken spring

d) aperture reduced ?

Non Conform

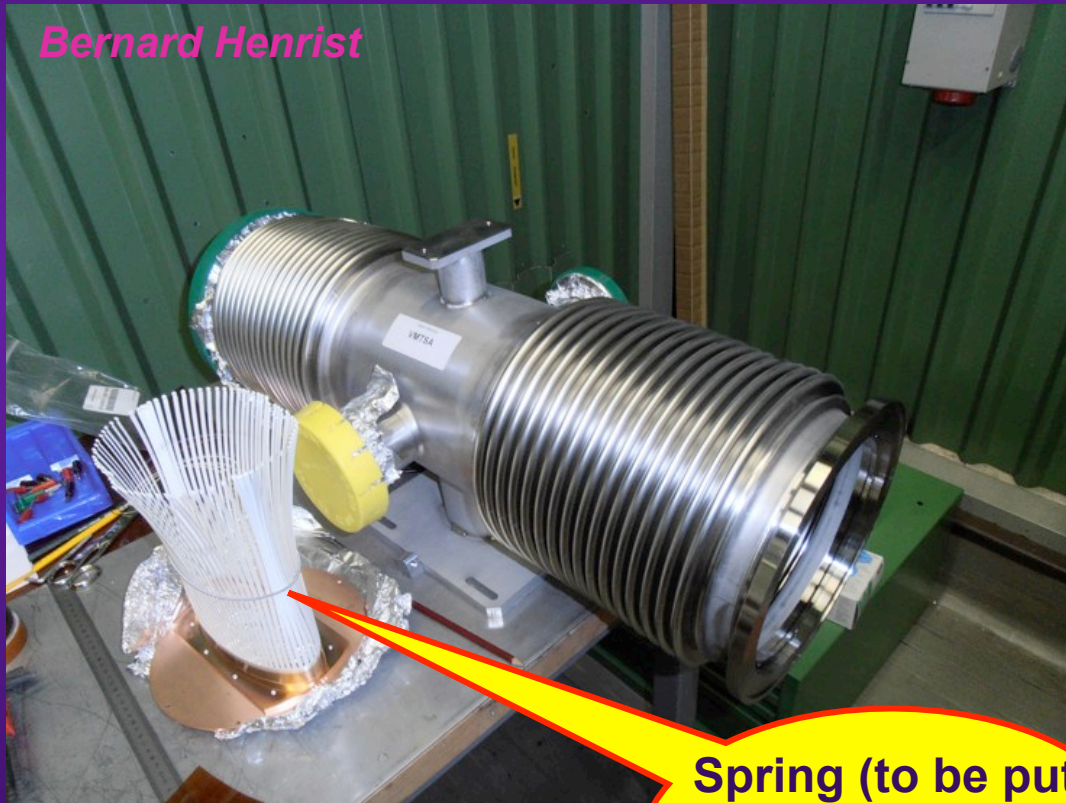
Spring was broken  
between May and  
November 2011



## VMTSA (3/5)

- ◆ Why? Is it an impedance problem? => Bench impedance measurements with 1 wire (and simulations ongoing)

*Bernard Henrist*

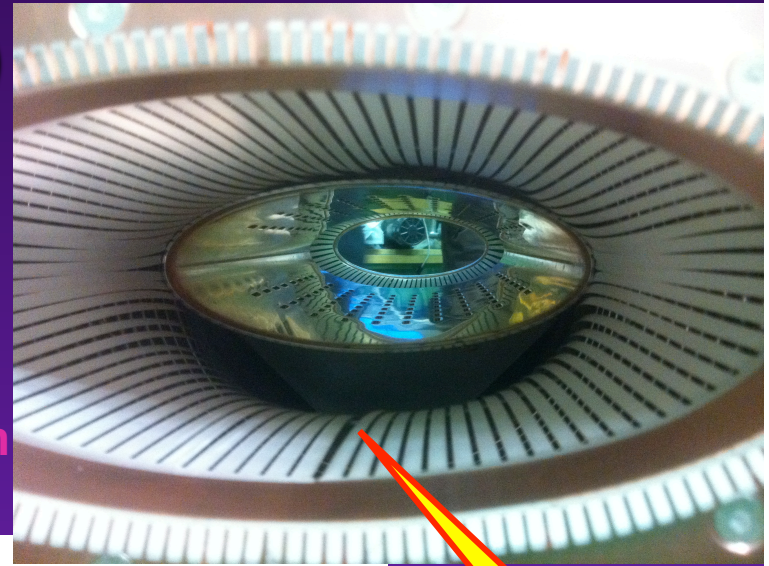
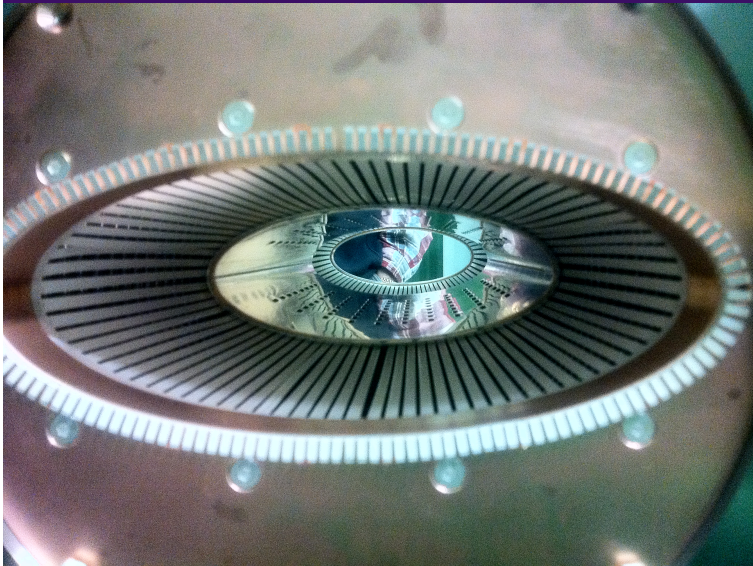


**Spring (to be put  
at the extremity of  
the RF fingers)**



# VMTSA (4/5)

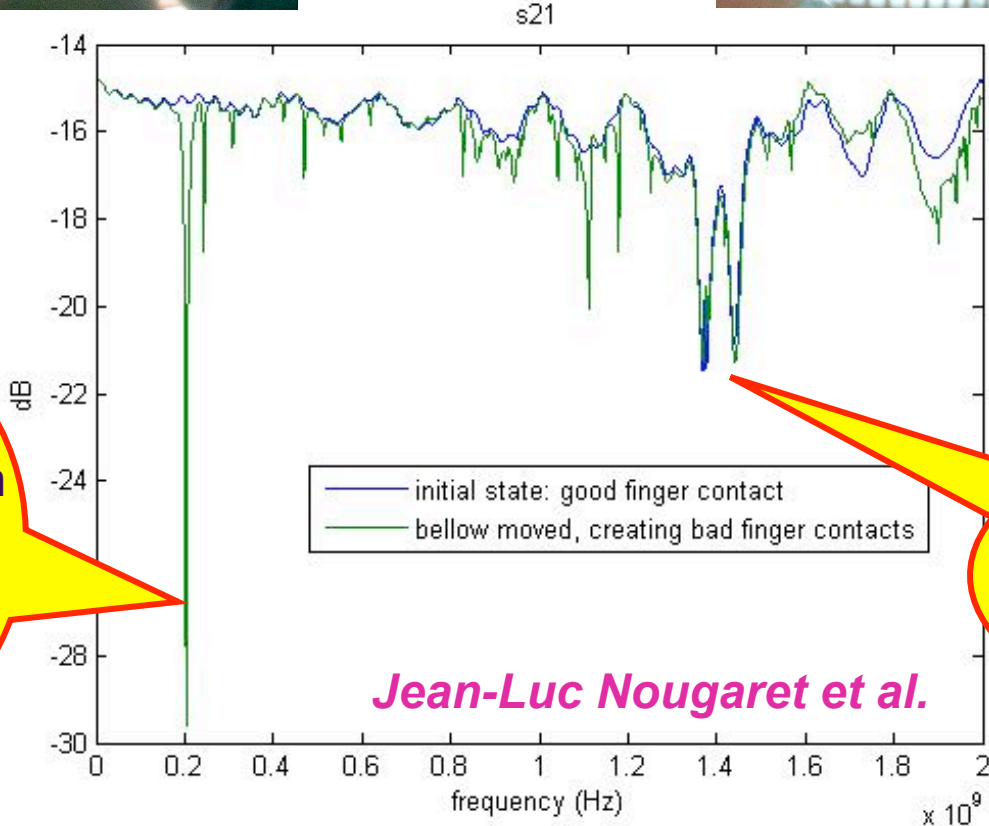
→  
Spring jumped back by moving laterally the bellow by few mm



Spring

Disappear with good contact at the end plates

Huge resonance at ~ 200 MHz when the spring jumped back! => ~ -15 dB in  $S_{21}$



Jean-Luc Nougaret et al.



## VMTSA (5/5)

- ◆ Longitudinal impedance can be deduced from  $S_{21}$

$$Z_l = -2 Z_{ch} \ln\left(\frac{S_{21}}{S_{REF}}\right)$$

$$S_{REF} = e^{-j\omega \frac{L}{c}}$$

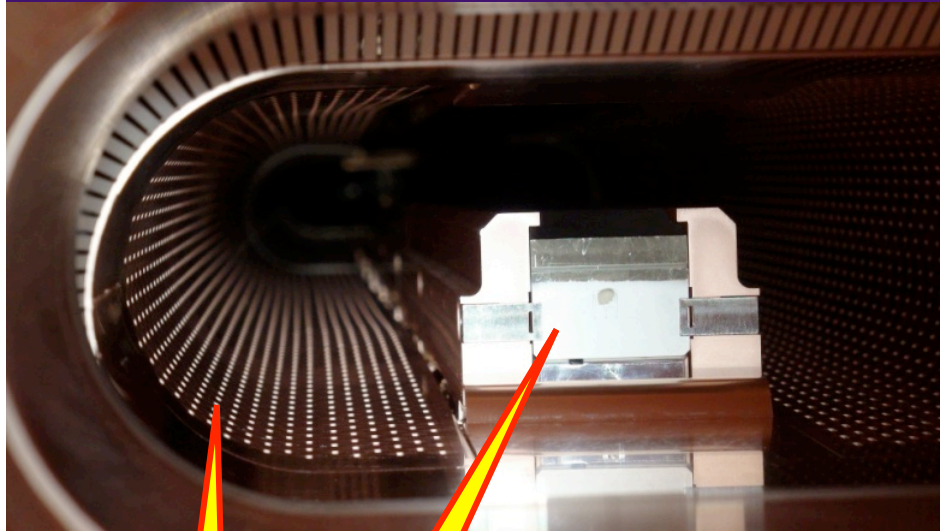
=> Numerical application for the real part of the impedance

- $Z_{ch}$  was measured and found to be  $\sim 270 \Omega$
- We use  $S_{REF} = 1$

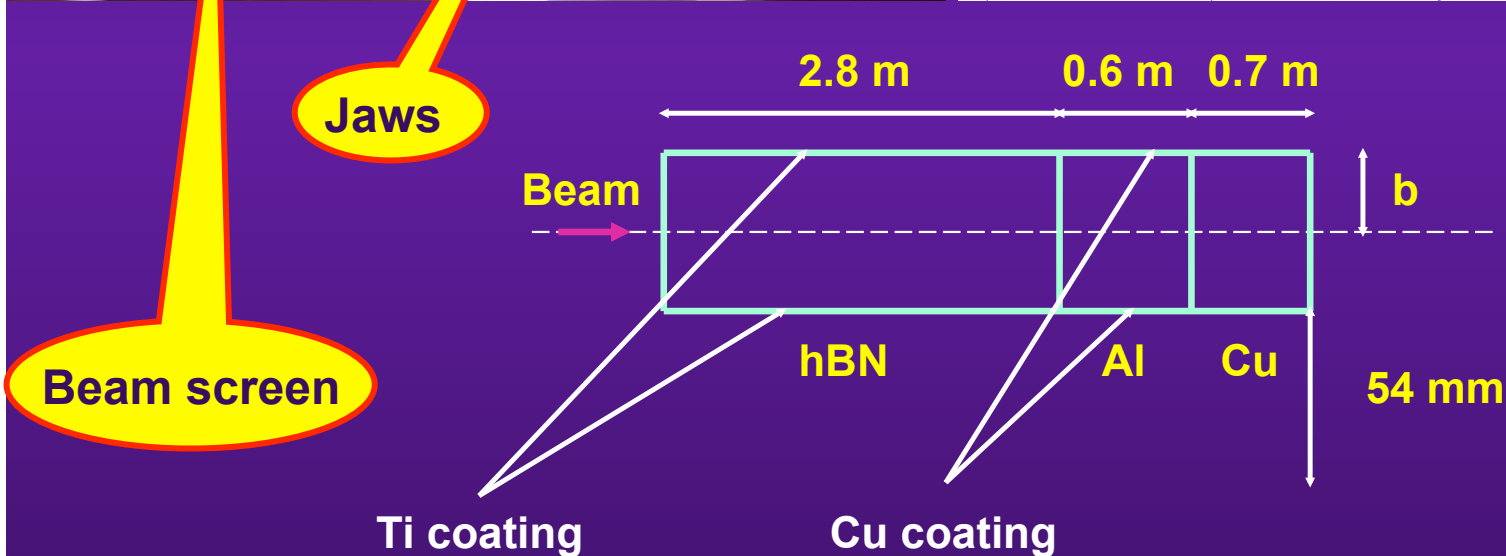
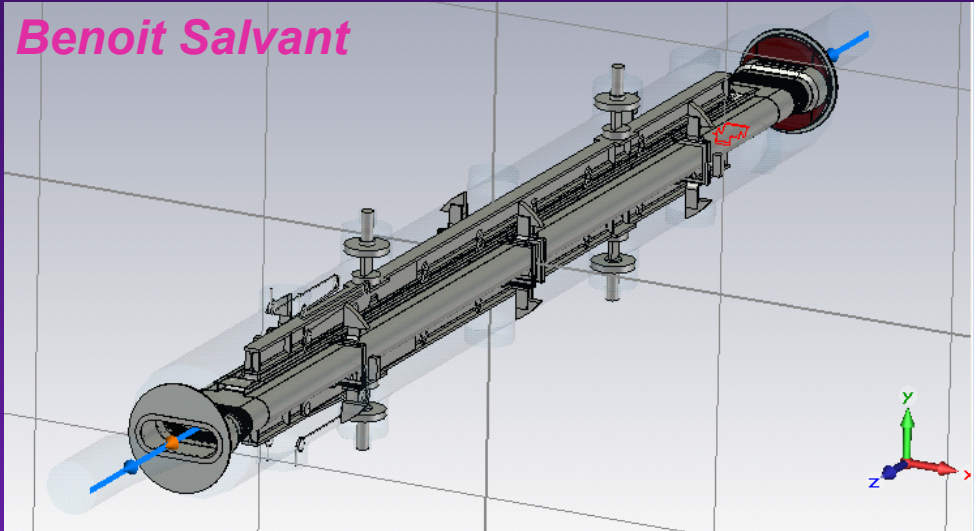
$$\Rightarrow Z_l = -2 Z_{ch} \ln\left(\frac{S_{21}}{S_{REF}}\right) = -2 Z_{ch} \ln\left(10^{\frac{S_{21}[\text{dB}]}{20}}\right) \approx 2 \times 270 \times \ln\left(10^{\frac{15}{20}}\right) \approx 930 \Omega$$

- ◆ **Power loss:**  $P_{loss} \sim 0.36^2 \times 930 \times 0.7 \sim 85 \text{ W}$  for 1 beam and  $\sim 4 \times 85 = 340 \text{ W}$  for 2 beams (worst case)
- ◆ **Conclusion: No impedance problem foreseen when the RF contacts are OK => 1<sup>st</sup> recommendation:** Improve the RF contacts

# TDI (1/13)



Benoit Salvant



=> **2 contributions:** resistive-wall (from the jaws) and trapped modes

## TDI (2/13)

### ◆ Observations during the 2011 run

- Vacuum pressure increase after ~ 1-2 h in stable beam, maximum reached and then decrease:
  - Started on May 1<sup>st</sup>, 2011 for TDI.4R8
  - Started on August 6<sup>th</sup>, 2011 for TDI.4L2
- Heating at both extremities (meas. after installation of thermocouples) on TDI.8R => Delta from 8 to 17 deg
- Since fill # 2219 (16/10) the TDI ½ gap was increased from 22 mm to 55 mm (parking position) in stable beam
  - Pressure => Remains in the few 1E-8 mbar range
  - BUT, temperature increase remains
- Higher impedance than expected from simulations and from previous measurements in 2010 => See NicolasM's talk at Evian11
- Unstable positions meas., unexpected aperture restriction in P2...

## TDI (3/13)

### ◆ => Inspection was requested

- Check the hBN metallization + shielding foil (large imp. meas.)
- Identify possible aperture restrictions for B1 between TDI and TCTVB left of point 2 evidenced by the aperture measurements conducted in preparation of the 2011 ion run

### ◆ Conclusions of the visual inspection

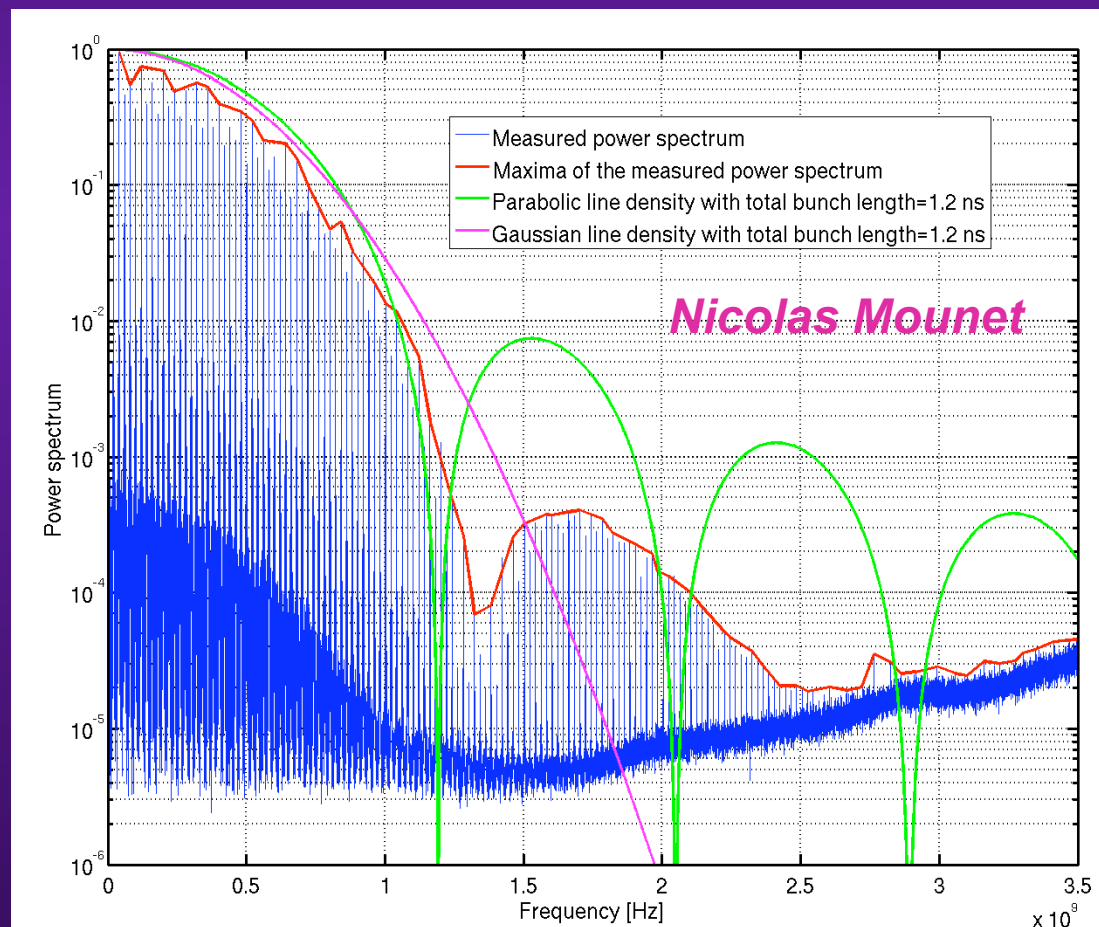
- Ti coating seems to be OK
- But, deformation of the beam screen in P8 mainly and to a smaller extent in P2 also
- Soft copper used for the beam screen instead of copper coated stainless steel

## TDI (4/13)

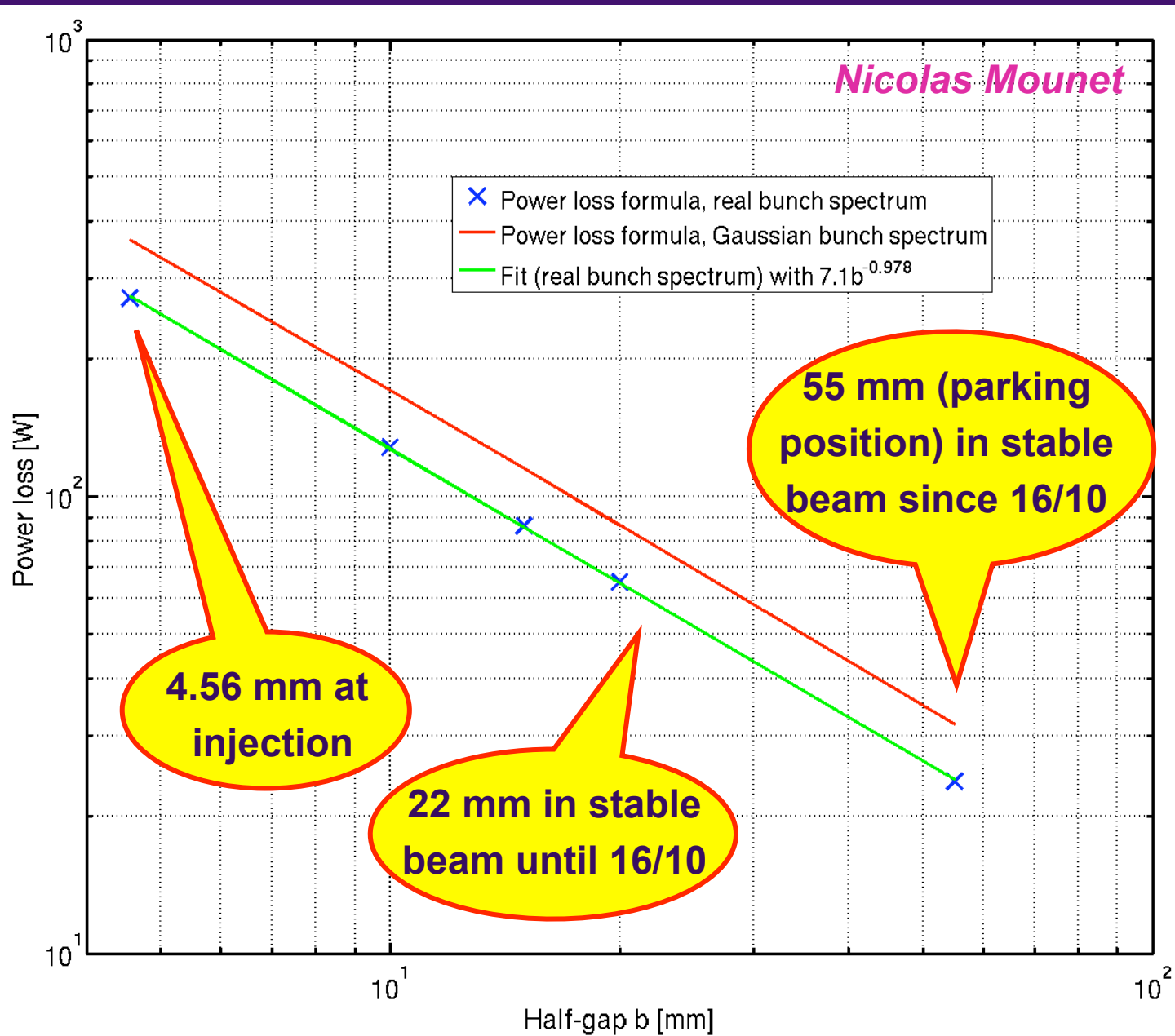
- ◆ **What is the role of the impedance? => Reminder on past predictions**
  - Power loss due to resistive-wall (jaws) ~ 200 W
  - Water cooling present on the Al frame holding the blocks – but clamped, not brazed. Capacity 20 kW => How much cooling at block surfaces?
  - Trapped modes and beam screen => Work done in the past to minimize them (simulations and measurements done with some limitations) => Not expected to be a big problem
  - No cooling of the beam screen
  - Nominal TDI operation: Should be IN only for injection (~ 20 min for nominal case) and then fully retracted (~ 55 mm half gap) => No impedance issue foreseen in the fully retracted position

## TDI (5/13)

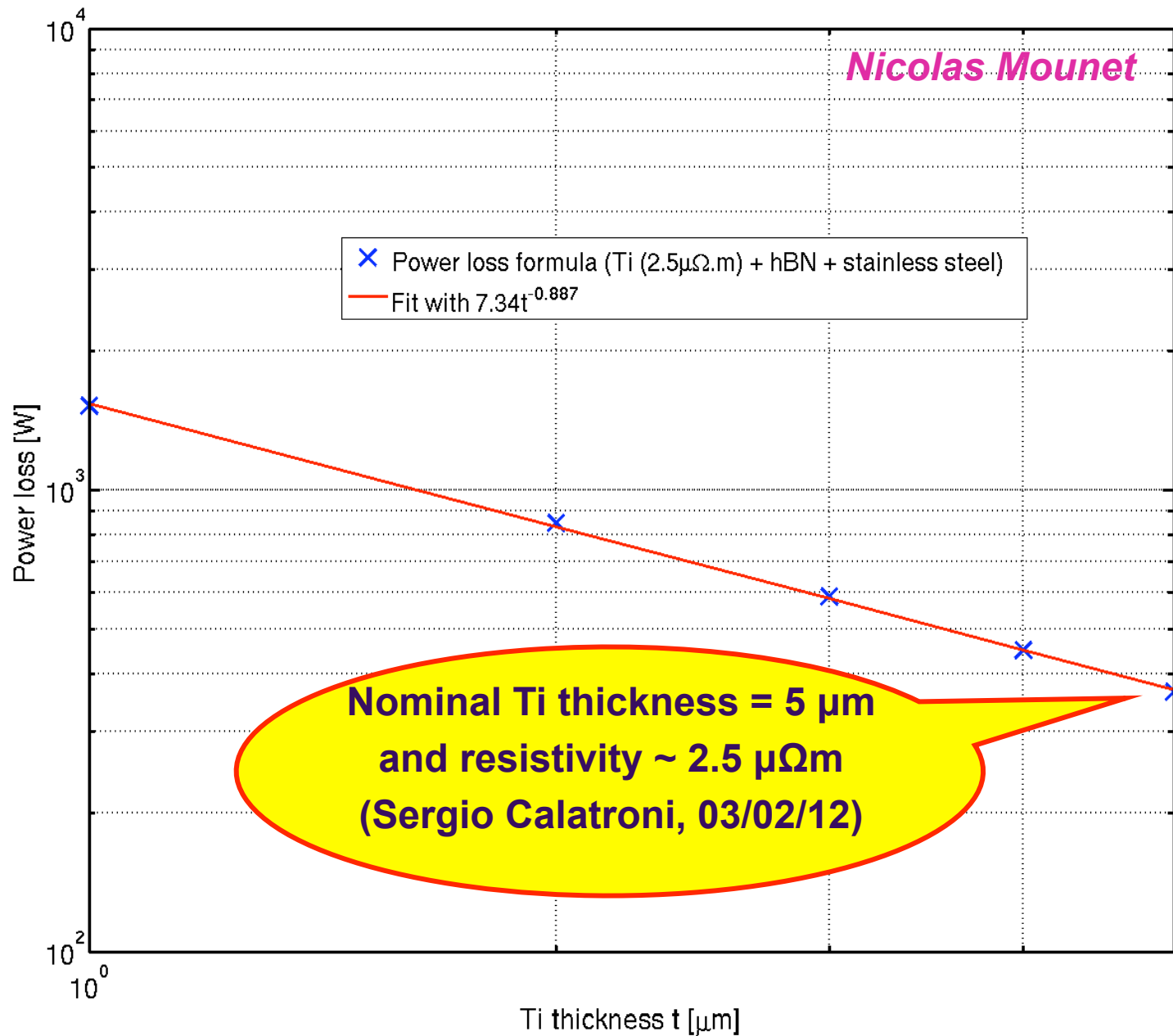
- ◆ Power loss from resistive-wall has been re-estimated for 1380 bunches,  $1.45E11$  p/b, 1.2 ns 4-sigma bunch length, half gap 4.56 mm
  - It is mainly in the Ti coating of the hBN block
  - hBN has a very good thermal conductivity => All the block heated



# TDI (6/13)



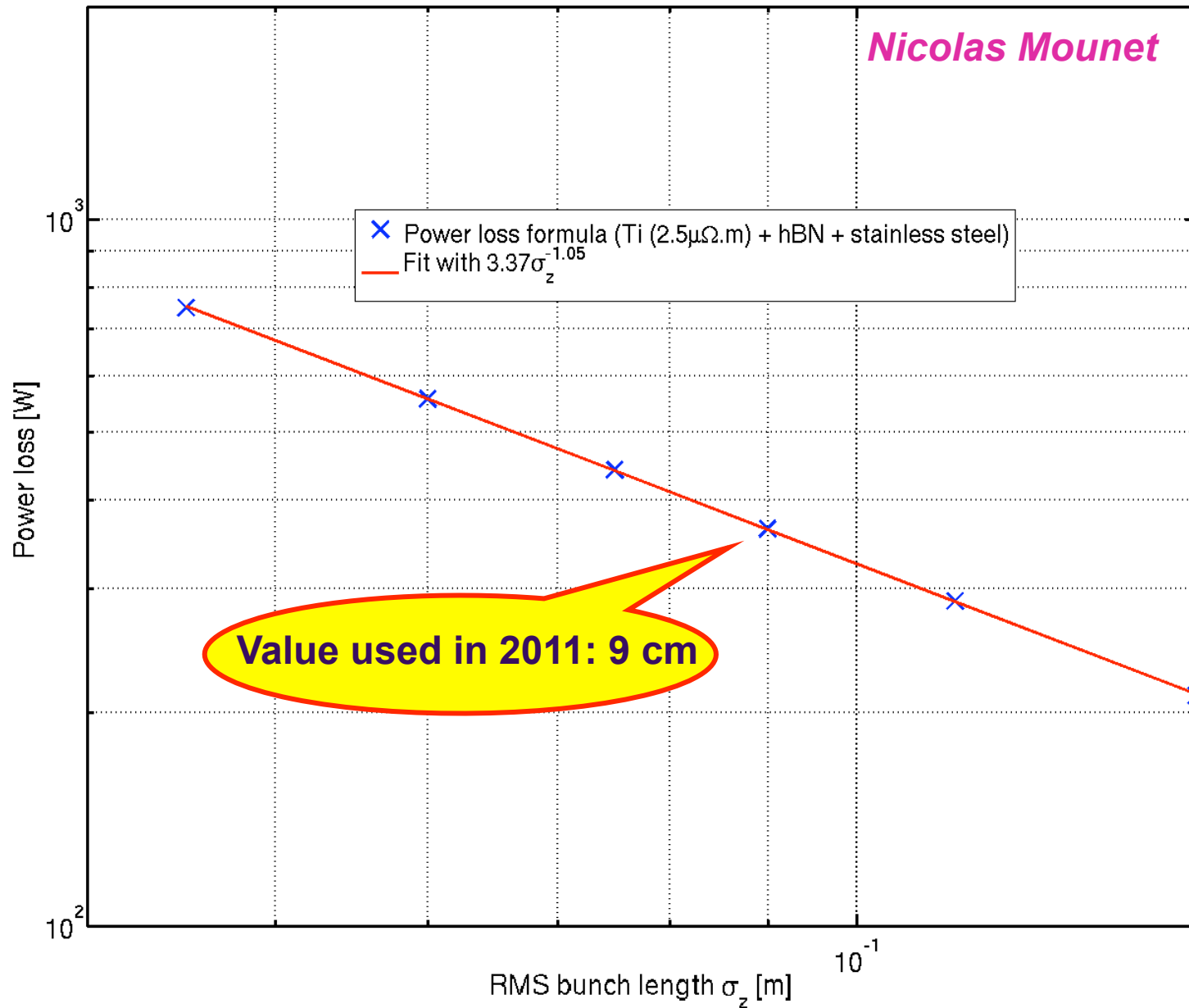
# TDI (7/13)





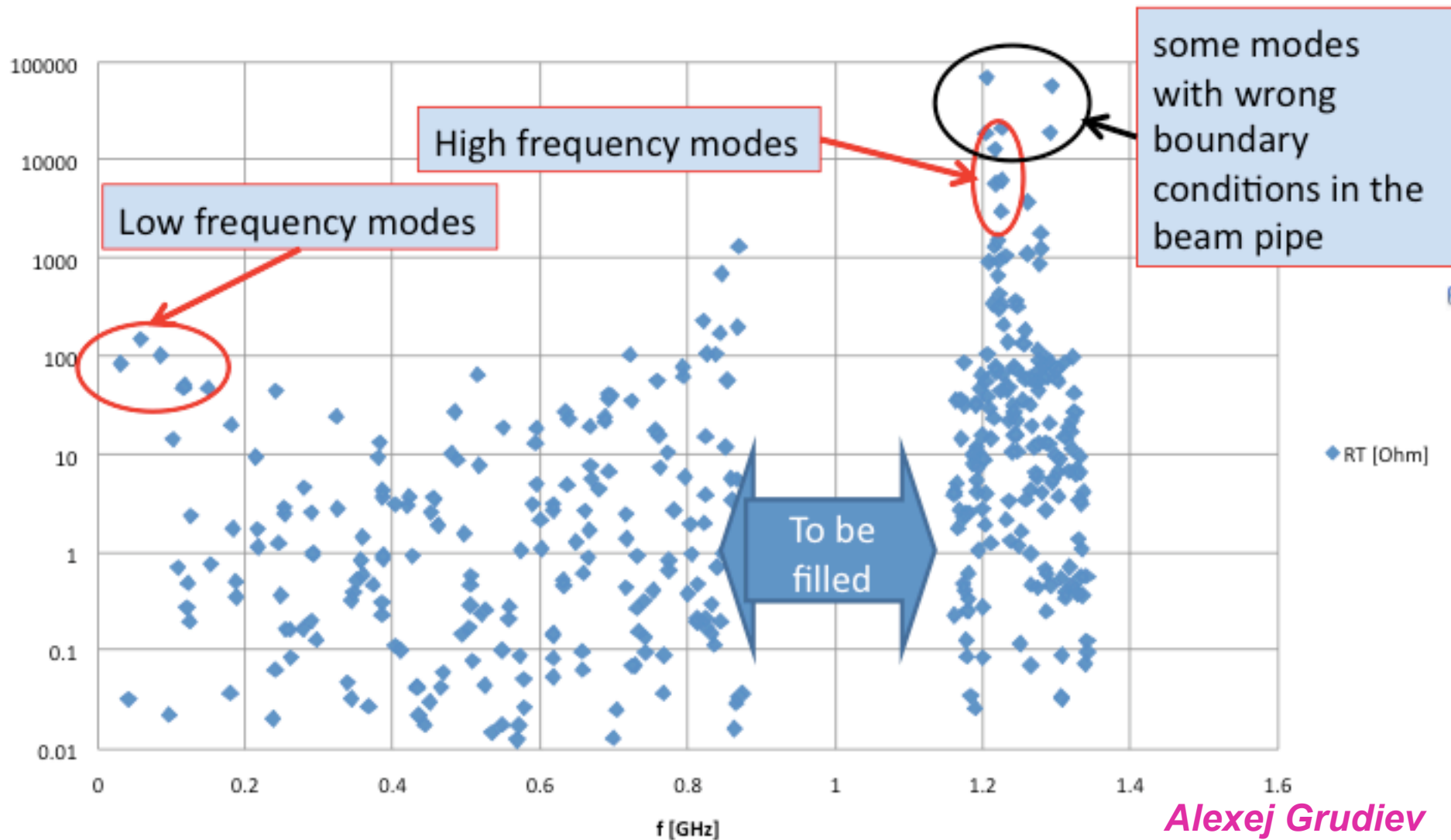
# TDI (8/13)

Nicolas Mounet



# TDI (9/13)

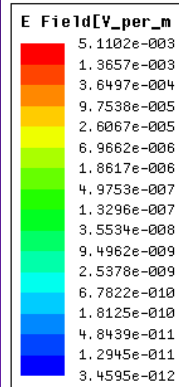
- ◆ Power loss from trapped modes estimated with the 3D model (done in fall 2011) for a half gap of 8 mm (still work in progress)



# TDI (10/13)

Low frequency mode at 31 MHz

Electric field distribution in horizontal and vertical planes (log scale)



All volume filled with EM fields  
Inside and outside of beam screen

$f = 31 \text{ MHz}; Q = 164; RT = 80 \text{ Ohm}$   
power loss distribution:  
50 % -> SS vacuum tank  
21 % -> Cu beam screen  
2 x 1.5 % -> to 2 flexible contacts

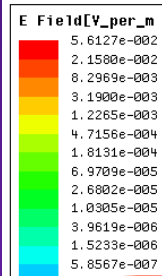
$P_{loss} \sim 0.36^2 \times 150 \times 1$   
 $\sim 19.4 \text{ W}$  for 1 beam and  $\sim 4$   
 $\times 19.4 \sim 78 \text{ W}$  for 2 beams  
(worst)

Other low frequency modes have similar field distribution:  
 $f = 59 \text{ MHz}; Q = 195; RT = 150 \text{ Ohm}$   
 $f = 86 \text{ MHz}; Q = 207; RT = 100 \text{ Ohm}$

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# TDI (11/13)

High frequency mode at 1227 MHz (preliminary)  
Electric field distribution in horizontal planes (log scale)

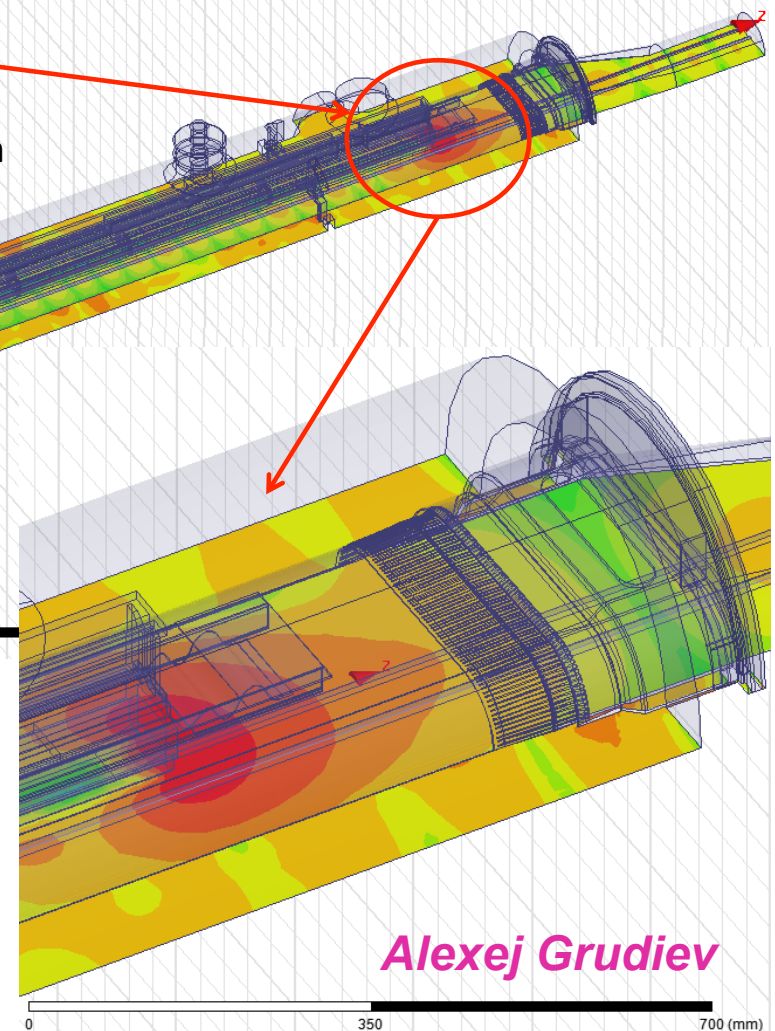


Localized field distribution

$f = 1227 \text{ MHz}; Q = 917; RT = 21000 \text{ Ohm}$

$P_{loss} \sim 0.36^2 \times 21000 \times 10^{-2.8} \sim 4.3 \text{ W}$  for 1 beam  
and  $\sim 4 \times 4.3 = 17.2 \text{ W}$  for 2 beams (worst)

Other high frequency mode:  
 $f = 1218 \text{ MHz}; Q = 970; RT = 13000 \text{ Ohm}$

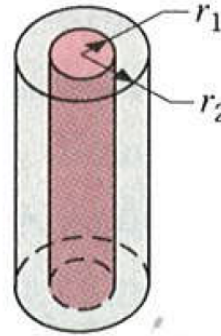


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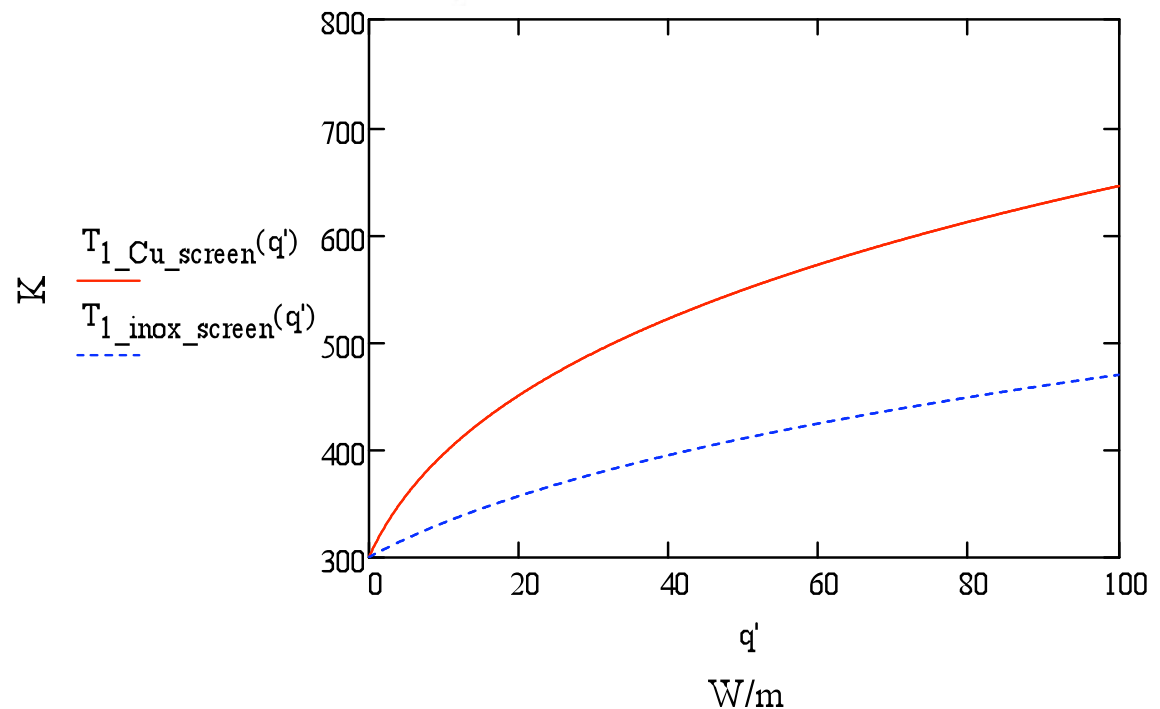
# TDI (12/13)

## ◆ Beam screen temperature estimation

- Radiation between diffuse gray surfaces in an enclosure
- Steady state heat exchange between two infinitely long concentric cylinders
- Vacuum tank at room temperature ( $T_2$ )
- Beam screen (inner cylinder) temperature ( $T_1$ ) calculated for a given heat input per unit length ( $q'$ )



$$q_{12} = \frac{\sigma A_1 (T_1^4 - T_2^4)}{\frac{1}{\epsilon_1} + \frac{1 - \epsilon_2}{\epsilon_2} \left( \frac{r_1}{r_2} \right)}$$

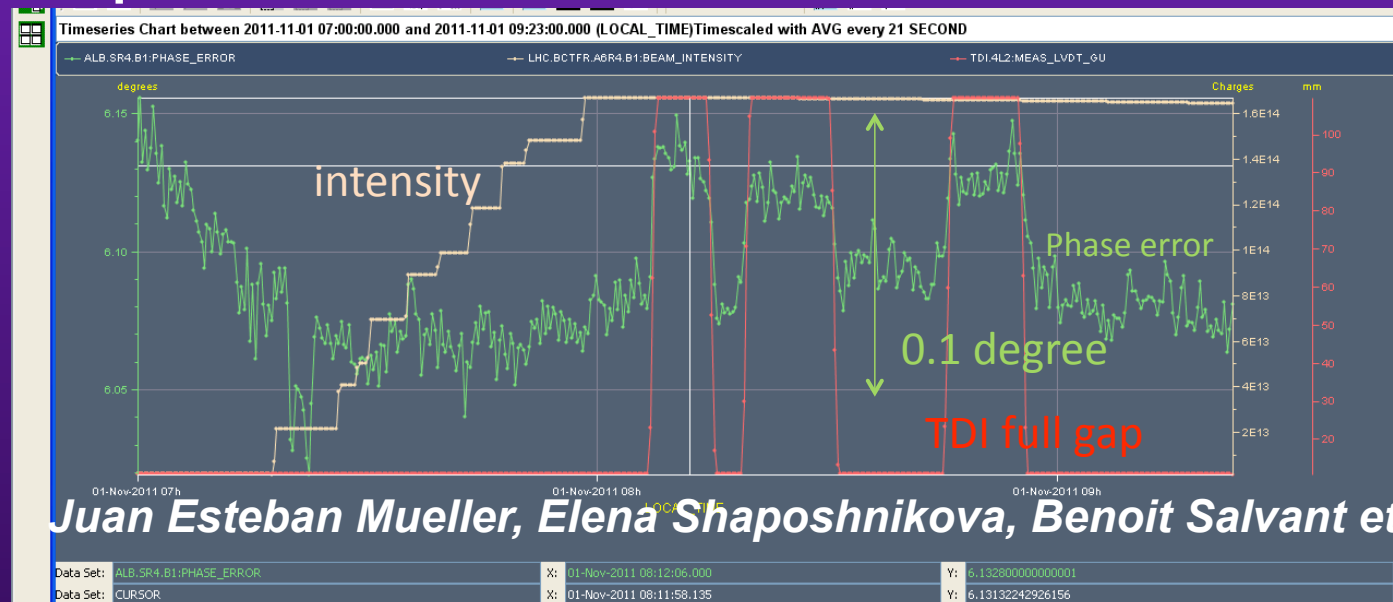


**Delio Duarte Ramos**

# TDI (13/13)

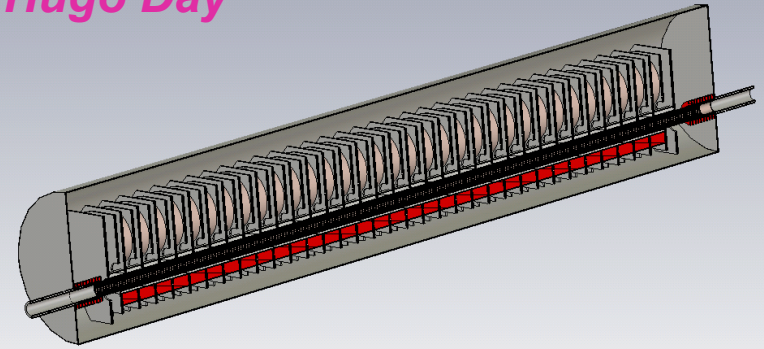
## ◆ Synchronous phase shift measurements during MDs

- Increase of power loss of  $\sim 1$  to  $2$  kW when closing the TDI jaws from parking to  $4.7$  mm half gap
- Seems to be  $\sim$  linear with the number of bunches  $\Rightarrow$  Would mean that it is mainly dominated by a broad-band impedance, i.e. resistive-wall? Reminder:  $\sim 300$ - $400$  W predicted  $\Rightarrow$  Higher Ti resistivity and/or smaller thickness? Could explain also the larger transverse impedance...



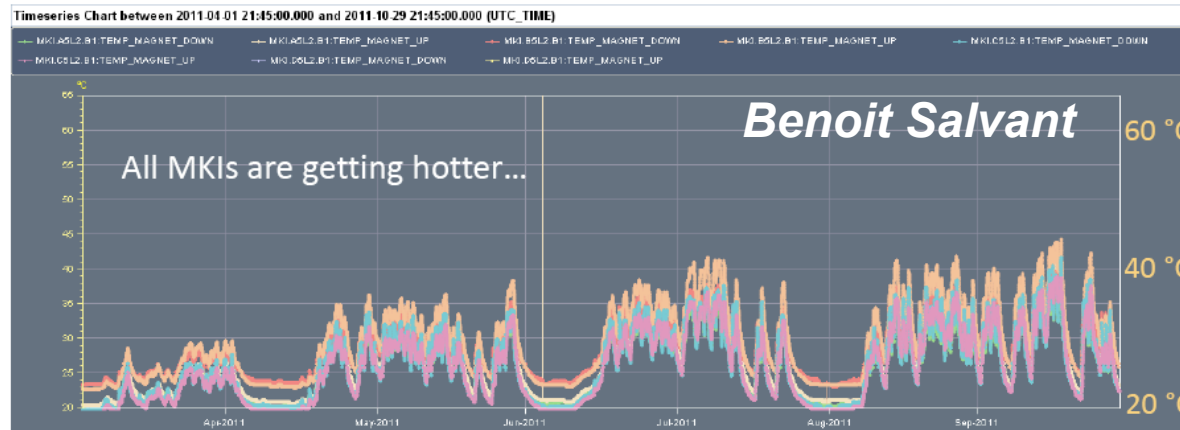
# MKI (1/3)

Hugo Day

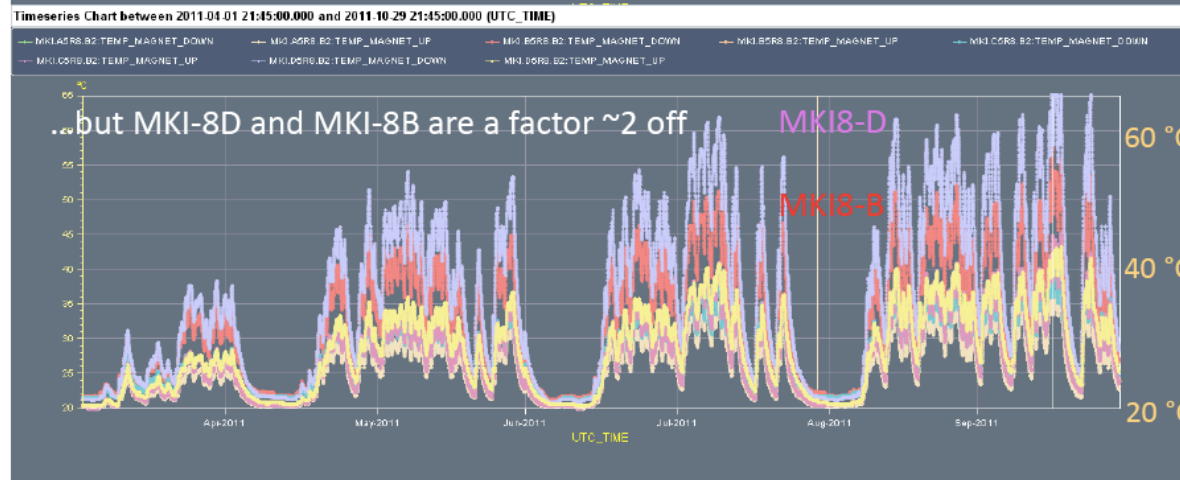


## MKIs: steady temperature increase over 2011

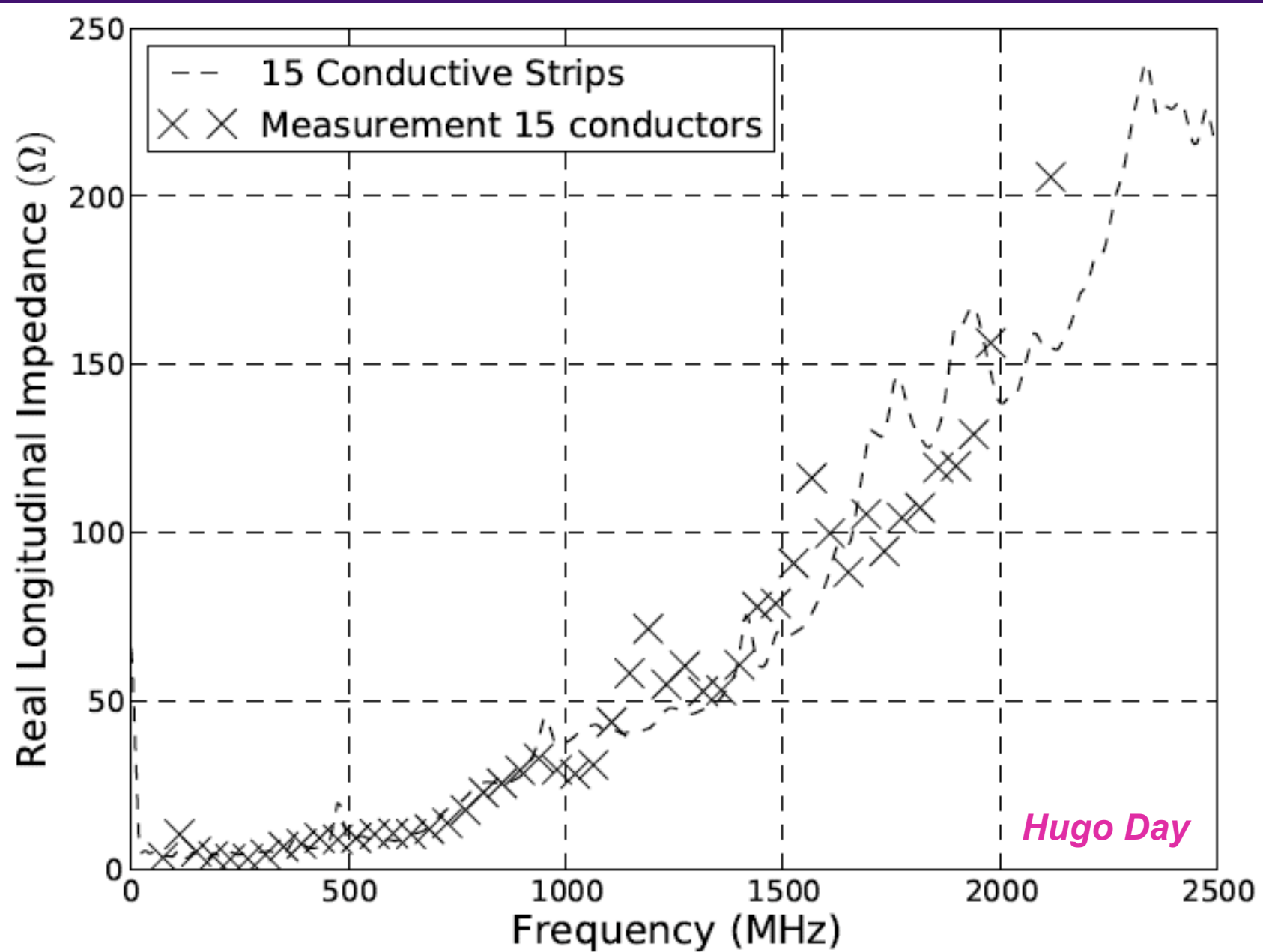
MKI  
in point 2



MKI  
in point 8



# MKI (2/3)





## MKI (3/3)

*Hugo Day*

Original design but then reduced to 15 due to HV electrical breakdown

|                      | 25ns      |           | 50ns      |           |
|----------------------|-----------|-----------|-----------|-----------|
|                      | 1.1ns (W) | 1.2ns (W) | 1.1ns (W) | 1.2ns (W) |
| 24 Screen Conductors | 44        | 43        | 17        | 16        |
| 15 Screen Conductors | 150       | 133       | 78        | 68        |
| No Screen Conductors | 4817      | 3703      | 3067      | 2663      |
| 15 long, 9 short     | 138       | 127       | 69        | 62        |
| No Metalisation      | 47660     | 40637     | 30187     | 27841     |
| No Damping Ferrites  | 28        | 27        | 15        | 14        |
| No Screen            | 4904      | 4314      | 3120      | 2745      |
| Alt Screen 1         | 75        | 74        | 33        | 33        |

Assuming  $1.15E11$  p/b  
=> It is 1.7 times higher  
for  $1.5E11$  p/b

## LESSONS FOR 2012 (AND AFTER)

- ◆ **VMTSA: No impedance problem if good RF contacts => Task force suggested / approved by recent LMC to check all the RF contacts => Discussion with MiguelJ ongoing**
- ◆ **TDI: Jaws should be IN only for injection (~ 20 min in nominal case) and then should be fully retracted. Is the beam screen deformation a consequence of the impedance with small gap? Can we add a Cu coating on the Ti flash? => Would gain a lot if needed for scrubbing...! Cooling?**
- ◆ **MKI: Impedance simulations now in very good agreement with past measurements => No surprise with the impedance. Might need to wait few h before injecting. MKI8D should be changed in August 2012 with 24 screen conductors instead of 15, i.e. lower heating. Future: improve cooling system? high-Curie temperature ferrite? etc.**
- ◆ **ALFA detector (not a worry for the LHC machine but for the experiment): Remove it for high intensity? (as in the design report?) => Time needed to remove and re-install it: few days?. Install some cooling (as TOTEM) during LS1**