

SMC

Cold Test Results

SMC#1 and SMC#3

M. Bajko, J. Feuvrier, H. Bajas

TE-MS-C-TF for electrical signal analysis

Some info is coming from :

L. Oberli TE-MS-C-SCD concerning the Sc cable

M. Guinchard EN-MME concerning the strain gauge measurements

Discussions during analysis made with :

B. Bordini TE-MS-C-SCD , P. Fessia and A. Milanese TE-MS-C-MDT

M. Bajko and H. Bajas for SMC review

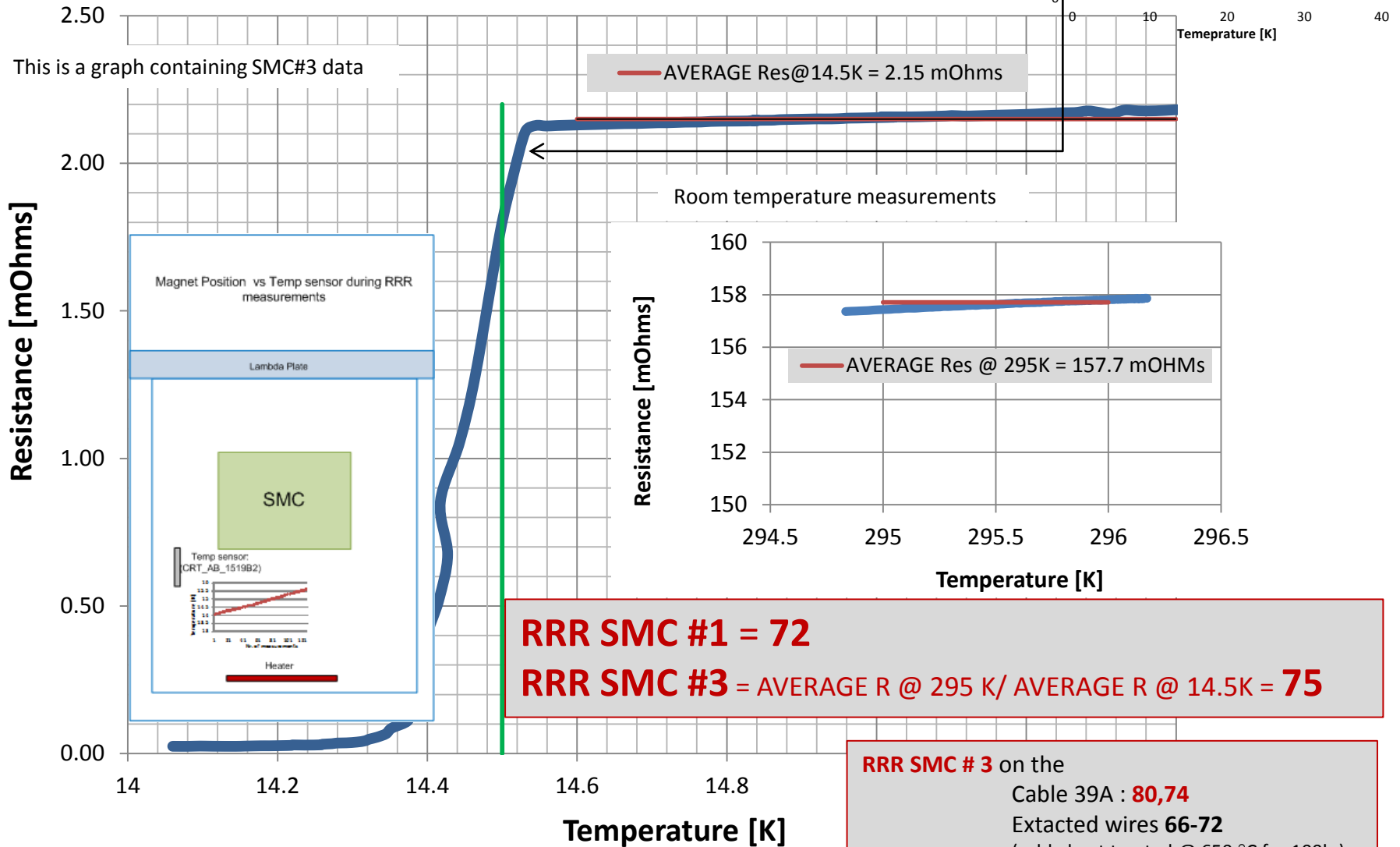
12/12/2011

Summary

- RRR
- Splice Resistance Measurements
- Detection and Protection
- Training history
- Quenches out of the magnet
- Longitudinal quench propagation velocity
- Quench location. Statistics.
- Quenches and Strain
- Temperature estimation during quench (by Hugo Bajas)
- Conclusions

RRR measurements of SMC

Measurements performed while the magnet was powered with 2 A
 During the **WARM UP** from 4.2K to 300K

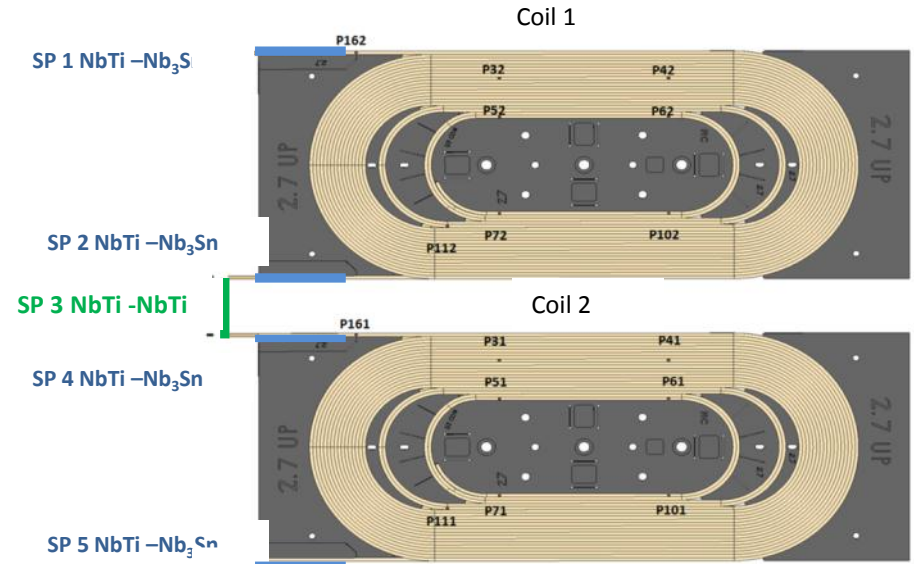
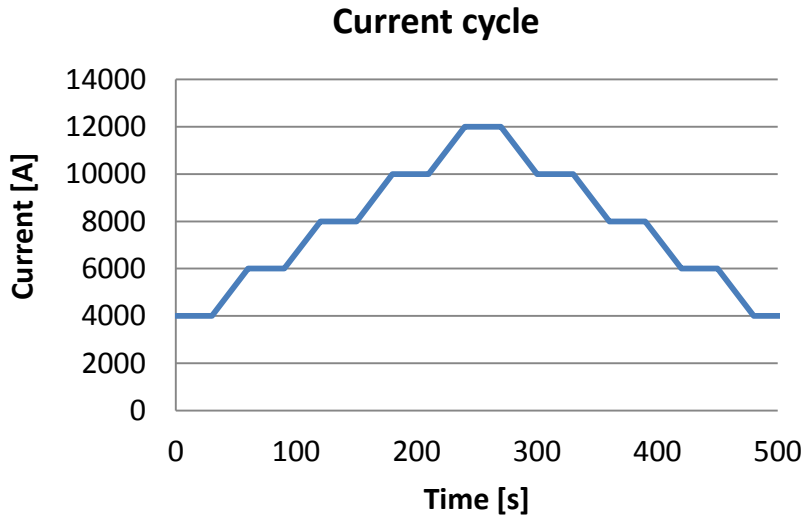


RRR SMC #1 = 72
RRR SMC #3 = AVERAGE R @ 295 K / AVERAGE R @ 14.5K = 75

RRR SMC #3 on the
 Cable 39A : **80,74**
 Extacted wires **66-72**
 (cable heat treated @ 650 °C for 100h.)
Info From Luc Oberli

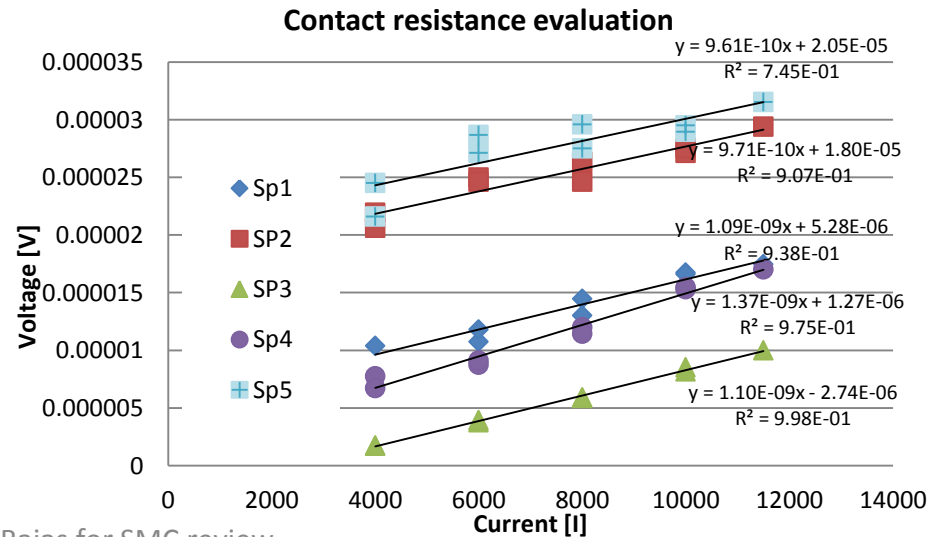
Splice measurements of SMC#3

Measurements performed while the magnet was powered with $I = 2000 - 1000$ A



LHC dipole splice acceptance : 3 nOHM

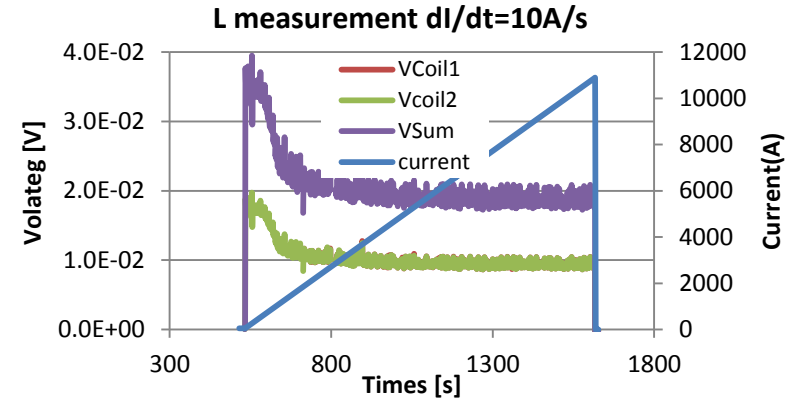
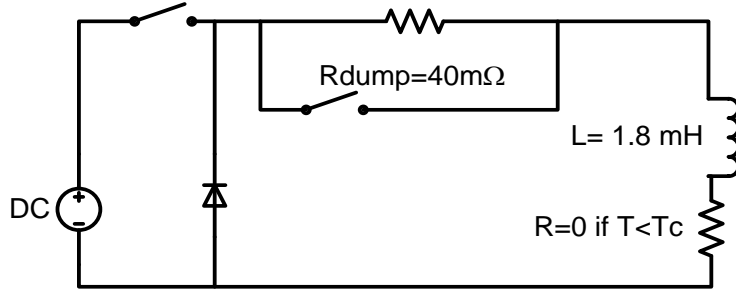
Splice	Resistance [nOhm]
Inter coil Sp3(NbTi-NbTi)	1.1
Coil 1 Sp1 (NbTi-Nb3Sn)	1.0
Coil 1 Sp2(NbTi-Nb3Sn)	0.9
Coil 2 Sp4(NbTi-Nb3Sn)	1.3
Coil 2 Sp5(NbTi-Nb3Sn)	0.9



Protection of SMC

Training performed at 4.2K and 1.9K , 10-200 A/s RR

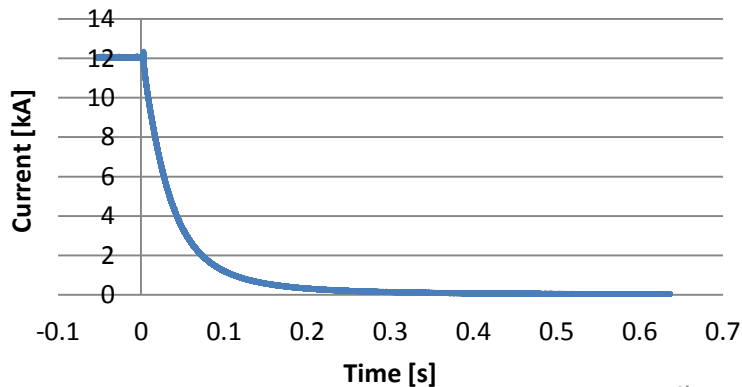
The protection circuit



Estimated inductance is $L = 1.8 \text{ mH}$
Confirmed by the model

For a faster **extraction of the energy** from the magnet, when the quench occurs, an external **dump resistor of 40 mΩ** was used, leading to a coil voltage during a quench of **550 V at 14 kA with a typical time constant of 35 ms.**

Typical current decay after quench



Detection and protection **threshold and time windows**

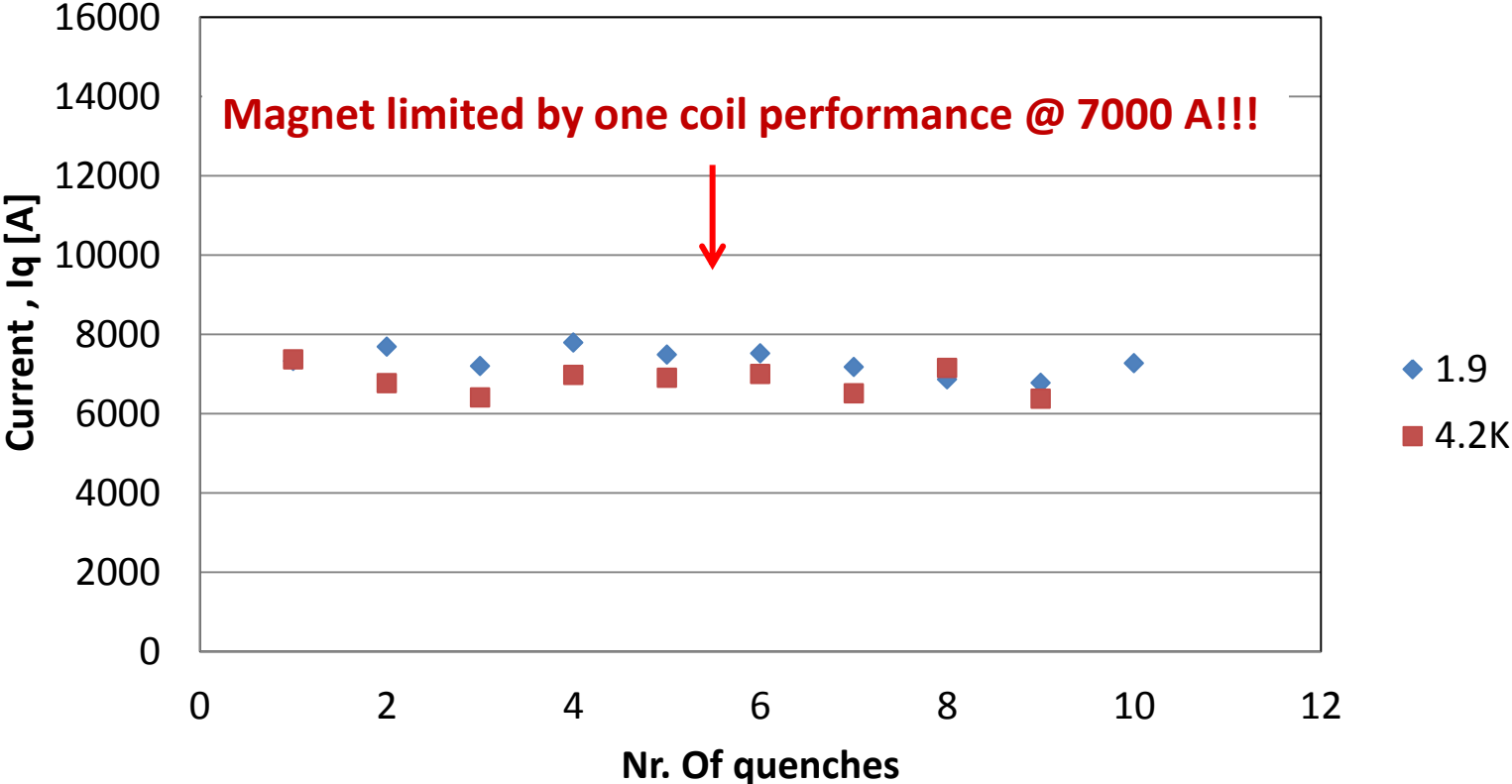
- $U_{\text{coil}_1} - U_{\text{coil}_2} \geq 100 \text{ mV} \times 10 \text{ ms}$
- $U_{\text{upper}_1} - U_{\text{lower}_1} \geq 100 \text{ mV} \times 10 \text{ ms}$
- $U_{\text{upper}_2} - U_{\text{lower}_2} \geq 100 \text{ mV} \times 10 \text{ ms}$
- $U_{\text{splice and leads}} \geq 50 \text{ mV} \times 8 \text{ ms}$

In order to complete the hot spot temperature estimation we performed quenches with variable time windows (see the slides of Hugo Bajas)

Training quenches in the magnet SMC#1

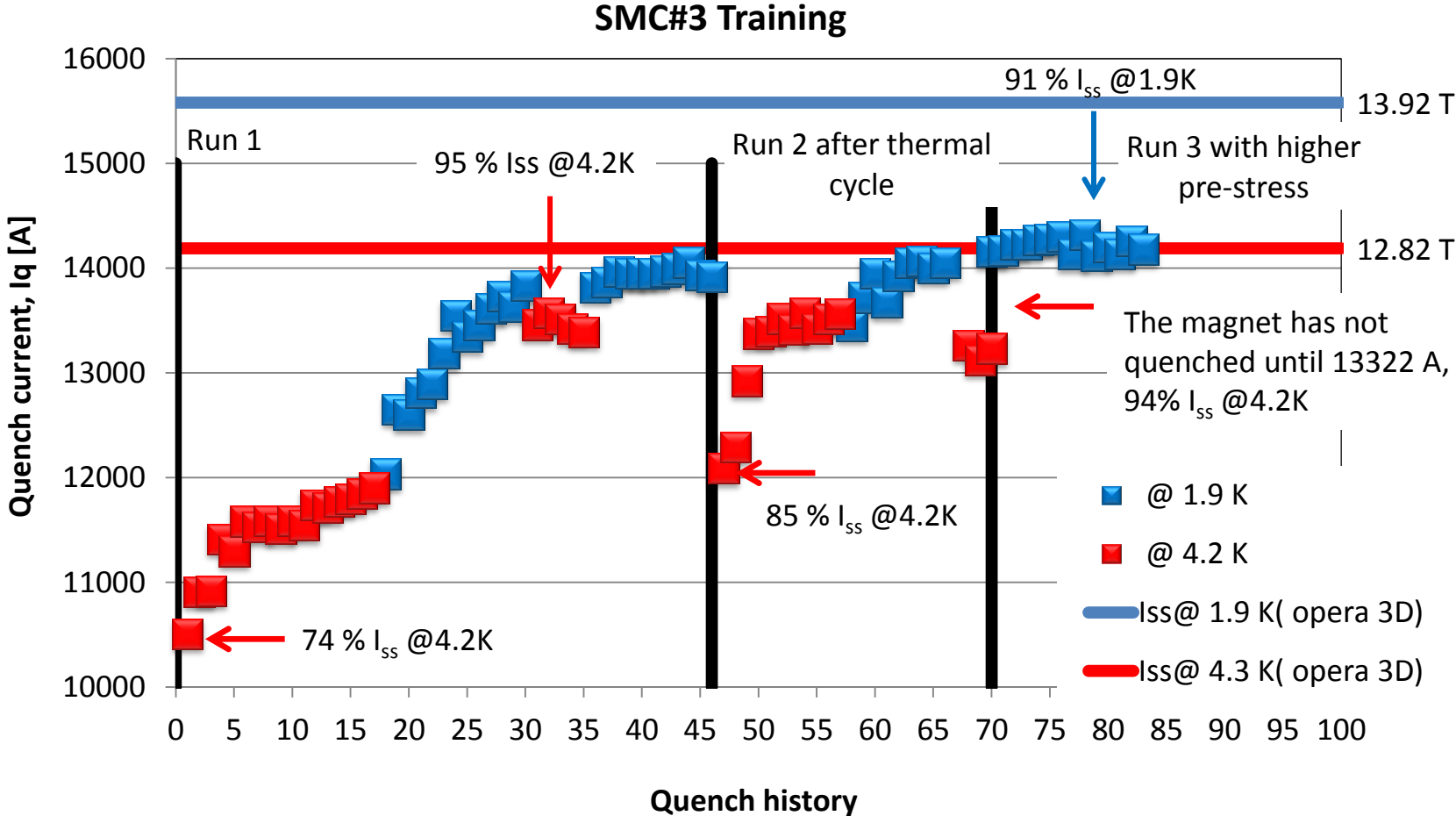
Training performed @4.2K and @1.9K ,
with one single coil to avoid limitation at 3 kA of one splice

SMC#1 Training



Training quenches in the magnet SMC#3

Training performed @4.2K and @1.9K , quenches performed with ramp rate (RR) of 20 A/s

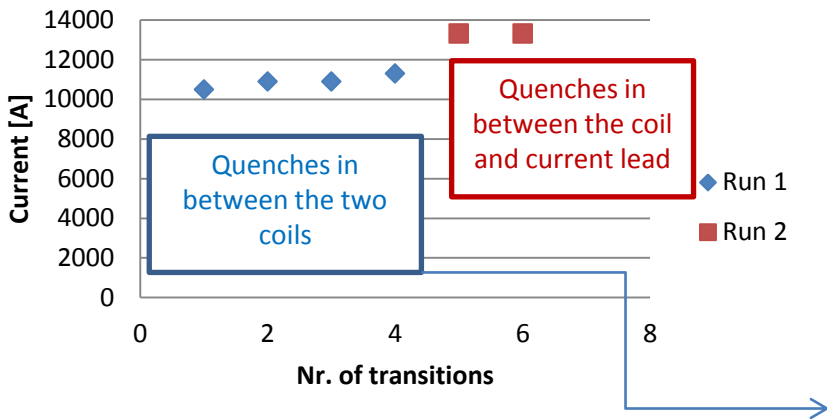


The strain is not considered for the estimate of the I_{ss}

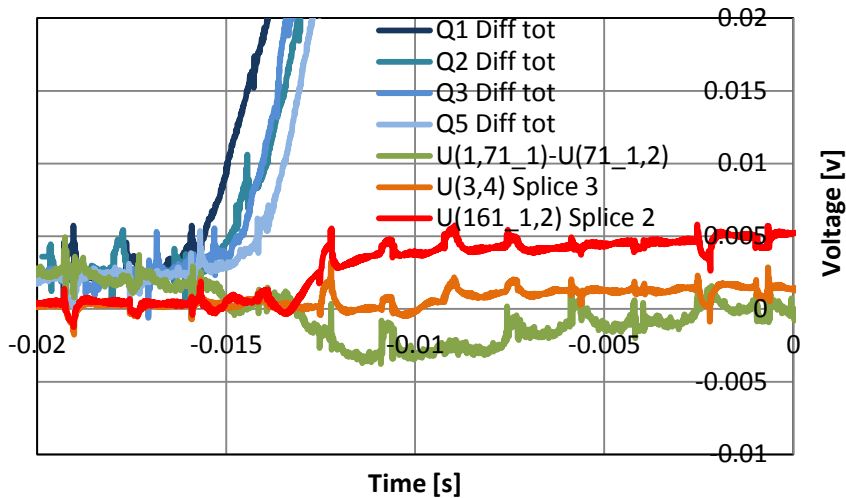
Quenches outside the SMC#3

quenches detected not in the magnet but in the cable connecting the two coils or the coils with the current leads

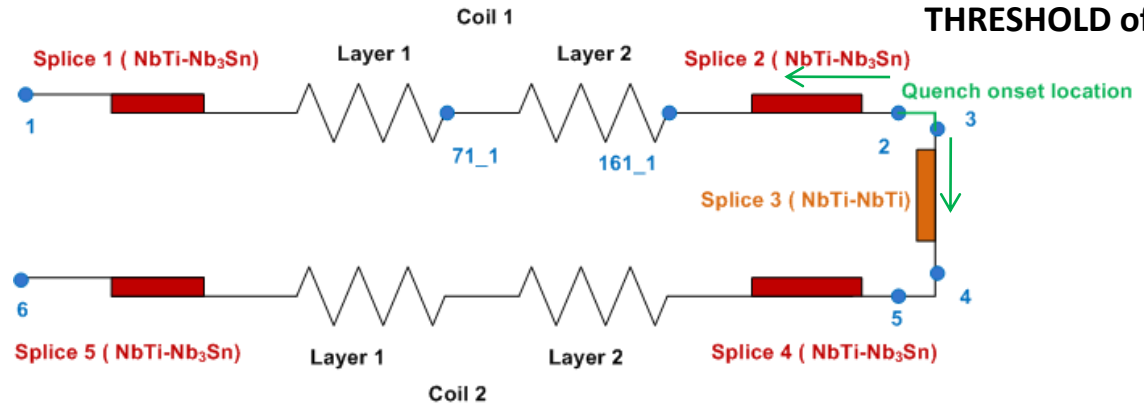
Training of the NbTi cable



Zoomed area of quench signals



THRESHOLD of detection and protection: 50 mV, 10 ms



$$Diff_{tot} = U(1,4) - U(4,6) > 0$$

Indicates a quench onset in: $U(1,4)$
which is composed as following:

$$U(1,4) = U(1,2) + U(2,3) + U(3,4)$$

the signals $U(1,2) = 0$

because:

$$U(1,71_1) - U(71_1,2) = 0$$

and

$$U(3,4) = 0$$

therefore we can only conclude that:

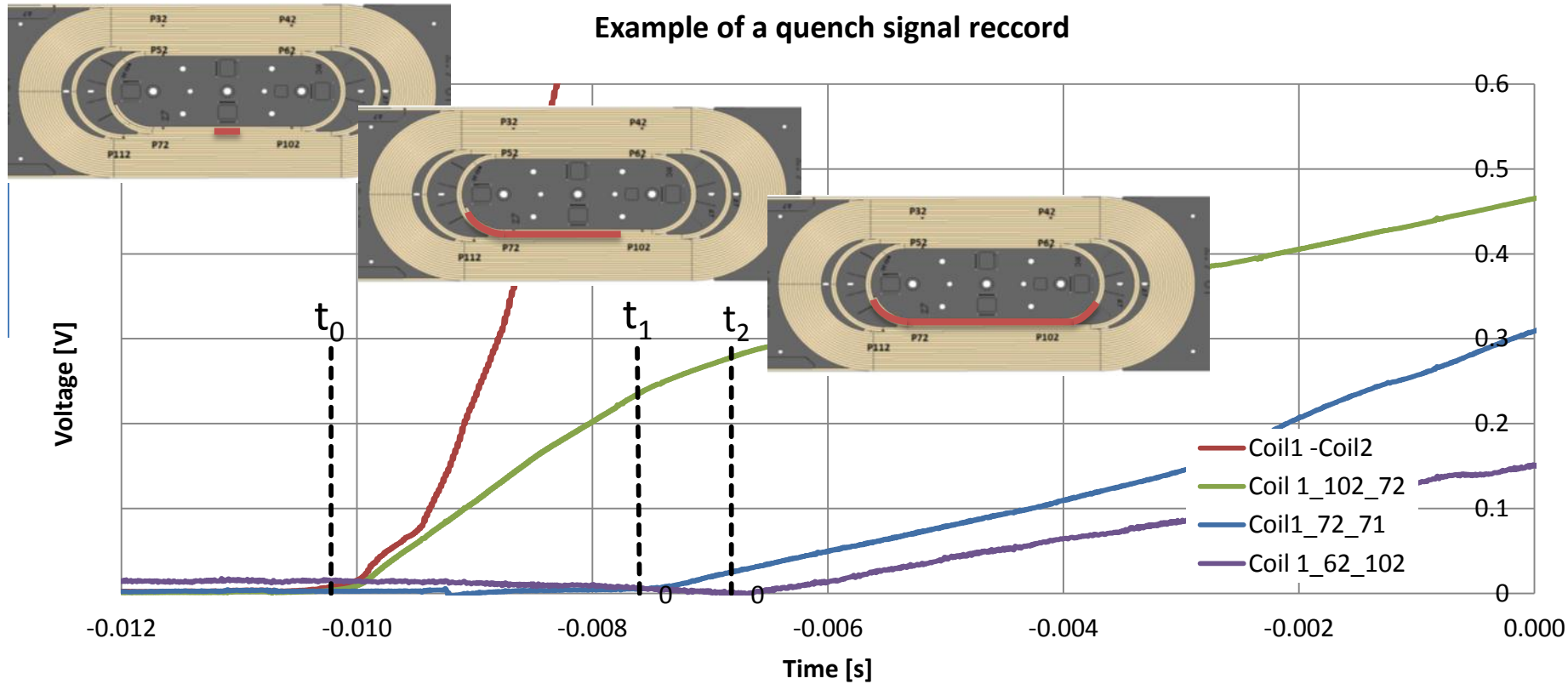
$$U(1,4) = U(2,3)$$

The quench onset is in-between Vtaps 2 and 3 . **Not in the coil** and **not in the splices**. It is located in **the NbTi cable** linking the two coils. Heat is propagating from this portion of cable to Splice 2 and Splice 3.

Quench propagation velocity. Time of Flight (ToF) method. SMC#3

Quench localized in HFS between Vtap72 and 102 of COIL 1

Example of a quench signal record



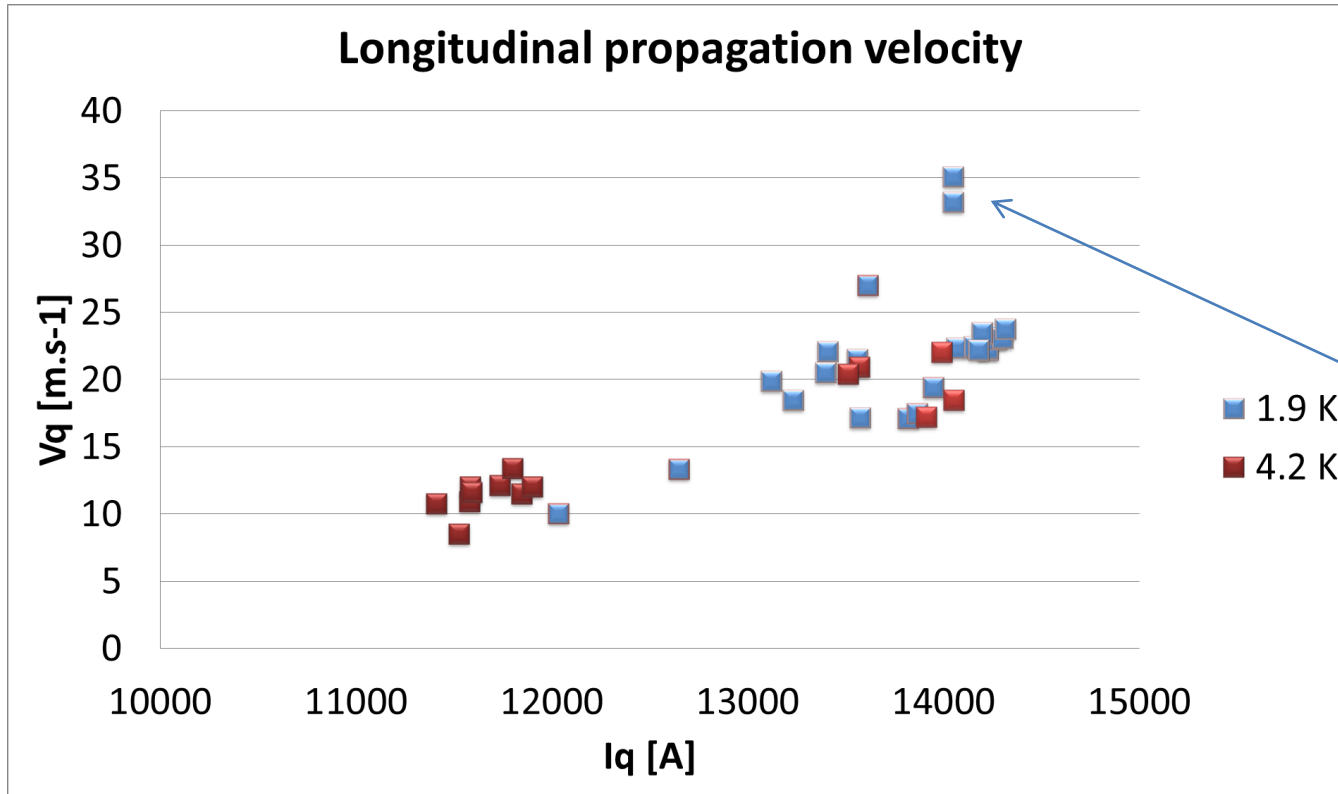
$$v = \frac{d(V_{tap72}, V_{tap102})}{ToF}$$

$$ToF = (t_1 - t_0) + (t_2 - t_0)$$

$$v_{example} = \frac{130mm}{2.6ms + 3.4ms} = 21.6m/s$$

Quench propagation velocity in SMC #3 based on the ToF

Training performed @4.2K and @ 1.9K , 20 A/s ramp rate, localized in HFS between Vtap72 and 102 of COIL 1

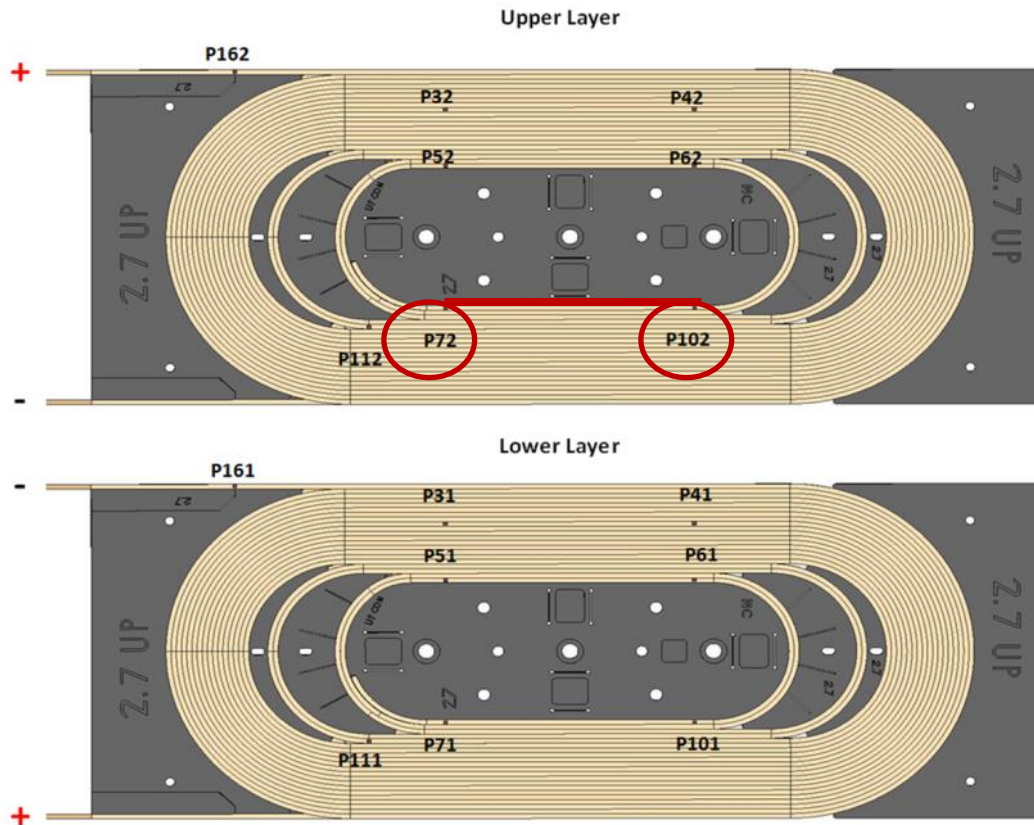


Outliers indicates that there is a transverse propagation effect. To be confirmed by more detailed study.

Increase of the velocity with training and current.

Quench location. Statistics on run 2. SMC#3

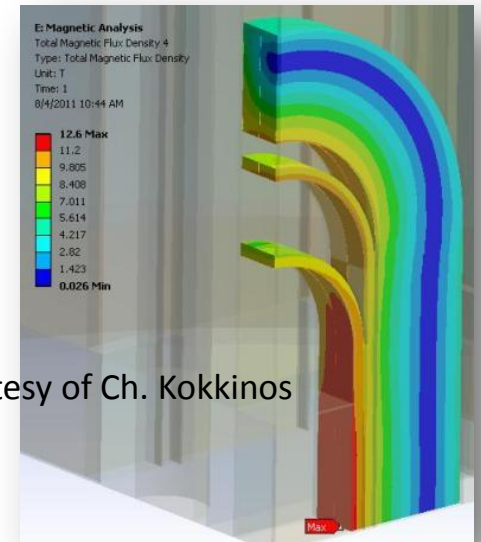
Training performed @ 4.2K and a@1.9K , quenches performed with 20 A/s ramp rate



4.2 K	72-102	HFS	14
	112-52	MT HF	1
	51-111	MT HF	1
	52-62	HFS	1
	101-61	H	1
	71-101	HFS	2
	71-72		1

1.9 K	72-102	HFS	11
	112-52	MT HF	1
	51-111	MT HF	1
	52-62	HFS	3
	101-61	H	1
	71-101	HFS	1
	62-102	H	1
	71-72	LJ	4
	61-51	HFS	2

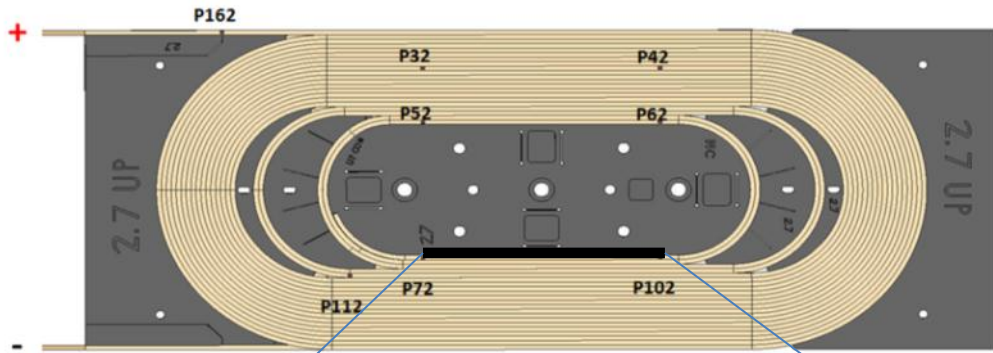
- approx. **74 %** of quenches occurs in the High(H) Field(F) zone on the Straight(S) part (**HFS**) in coil1
- approx. **73%** of HFS occurs in between **Vtap 72 and V tap 102** in coil 1
- No quenches in the splices !!!!**
- Only 10% of quenches on the Layer Jump; few are on coil 2.



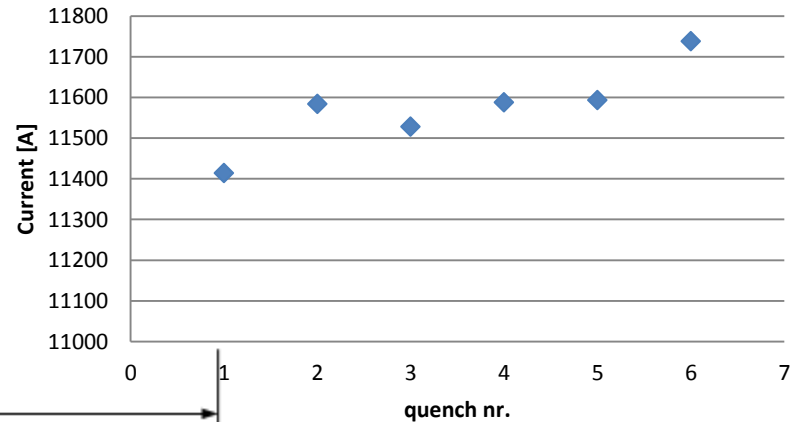
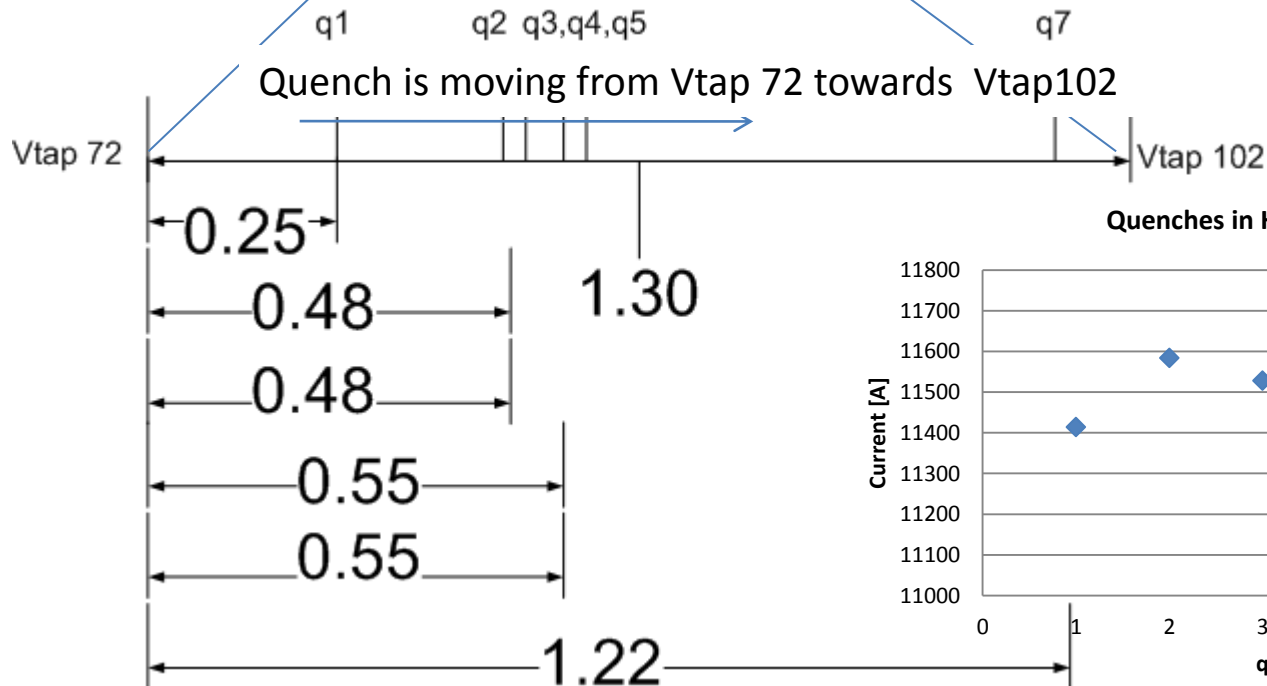
Courtesy of Ch. Kokkinos

Quench location during training in run 2: HFS SMC#3

Training performed at 4.2K , 20 A/s ramp rate, localized in HFS between Vtap72 and 102 of COIL 1

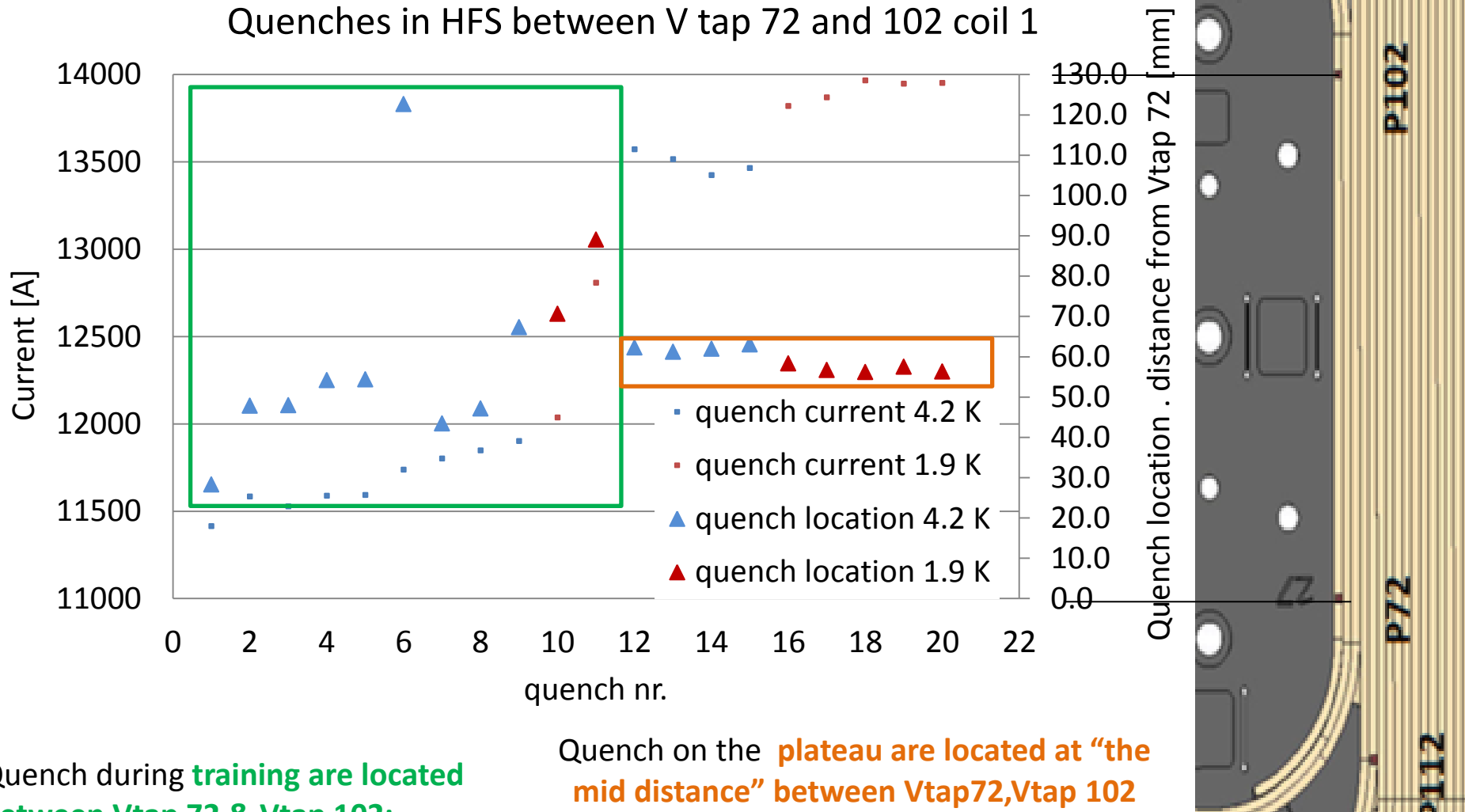


Quench propagation velocity: **12 m/s**



Quench location in run 2 :HFS SMC#3

Training performed at 4.2K and 1.9K , 20 A/s ramp rate, localized in HFS between Vtap72 and 102 of COIL 1

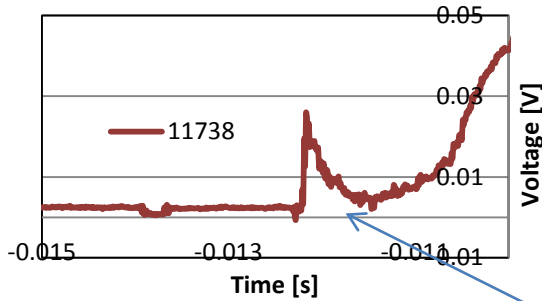


Quench during training are located between Vtap 72 & Vtap 102:

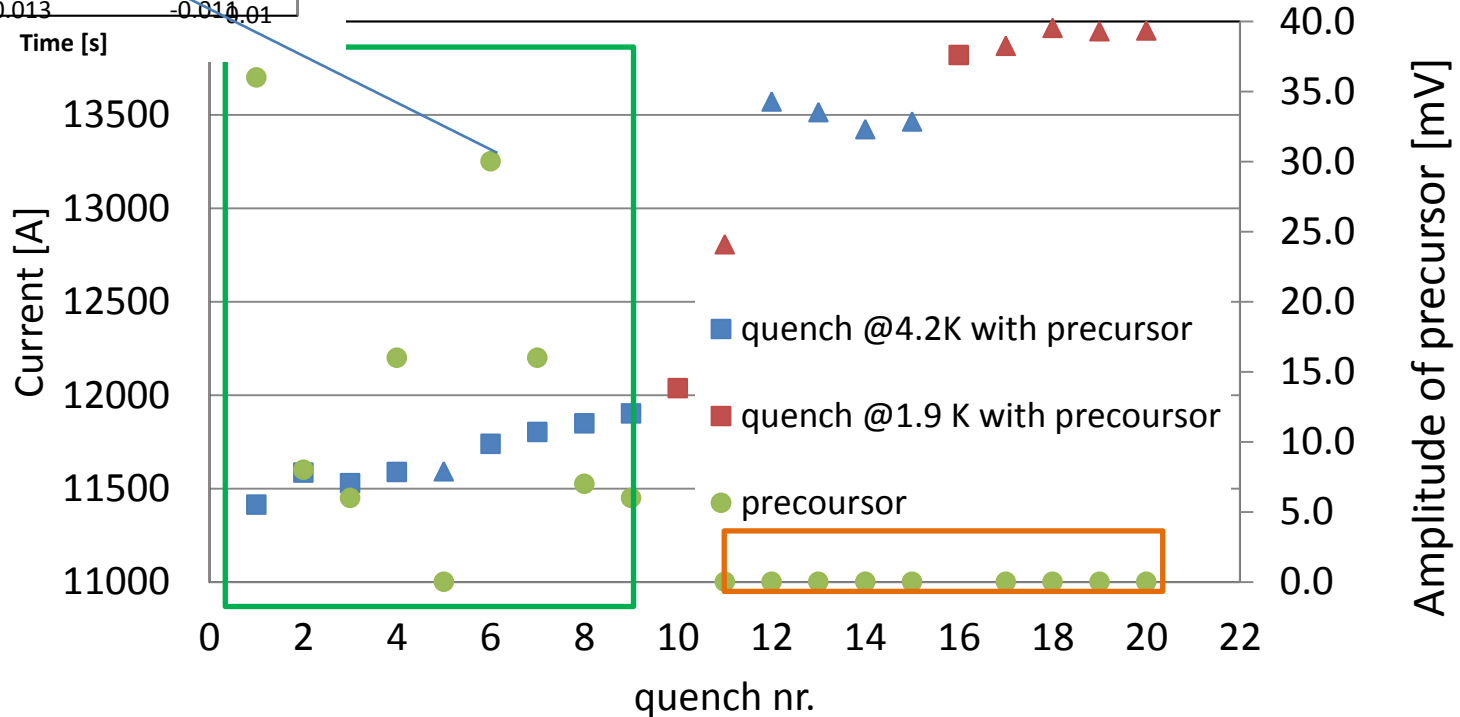
Quench on the plateau are located at “the mid distance” between Vtap72,Vtap 102 To be linked to the highest field and strain

Quenches with and without precursors in run 2 :m HFS SMC#3

Training performed at 4.2K and 1.9K , 20 A/s ramp rate, localized in HFS between Vtap72 and 102 of COIL 1



Quenches in HFS between V tap 72 and 102 coil 1



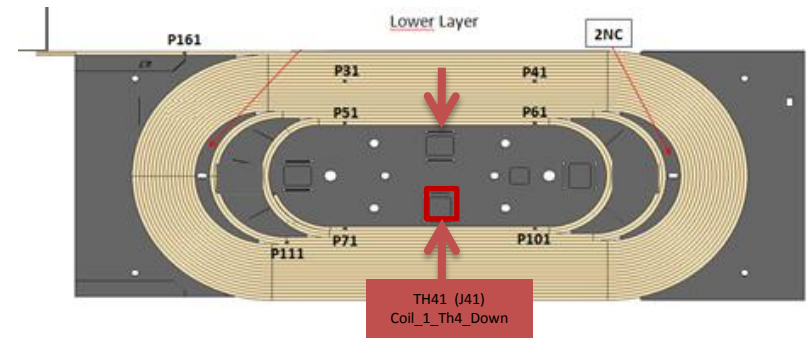
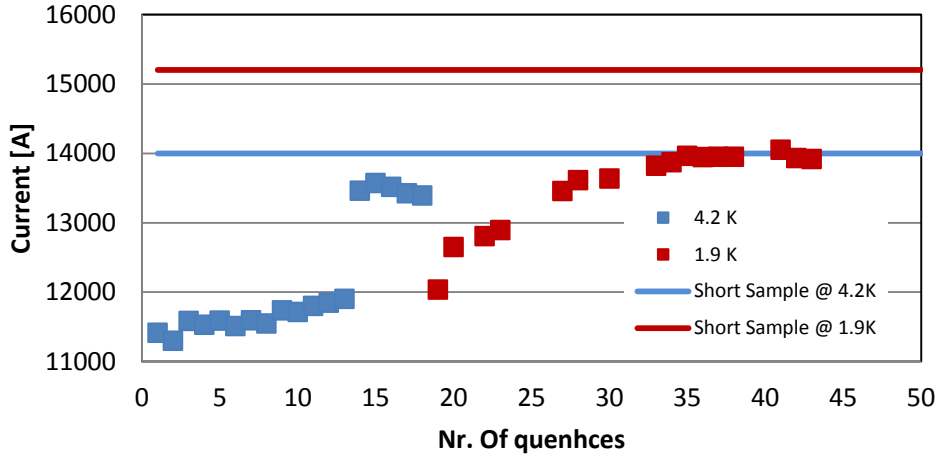
Quench during **training has precursors**
of an amplitude between 6-30 mV

Quench on the **plateau are not having precursors**
Or they are very small !!!

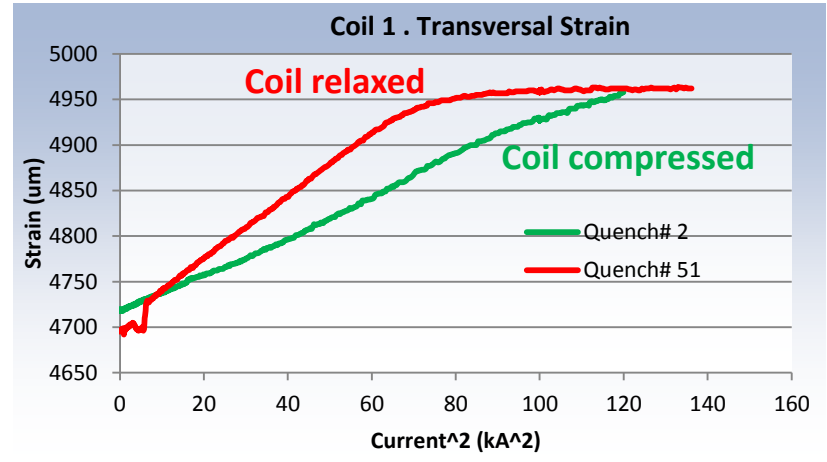
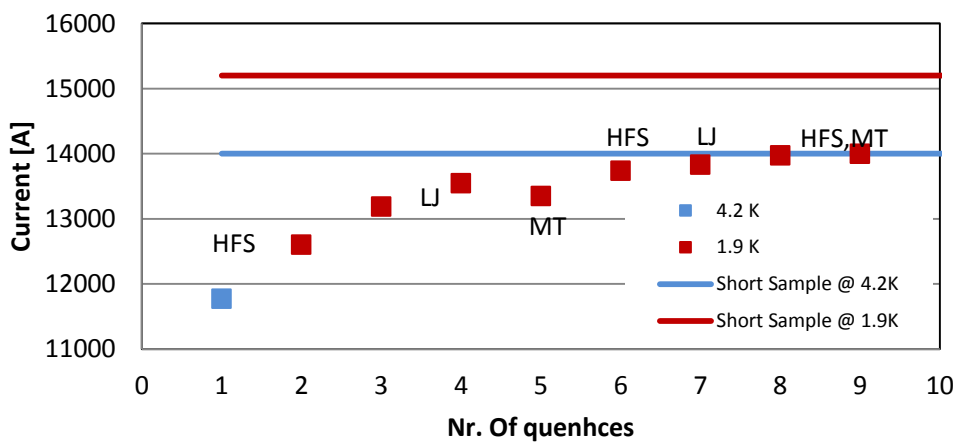
Training quenches coil by coil. Strain on the coil 1 of run 2. SMC#3

Training performed at 4.2K and at 1.9K , quenches performed with 20 A/s ramp rate

Coil 1 Training



Coil 2 Training

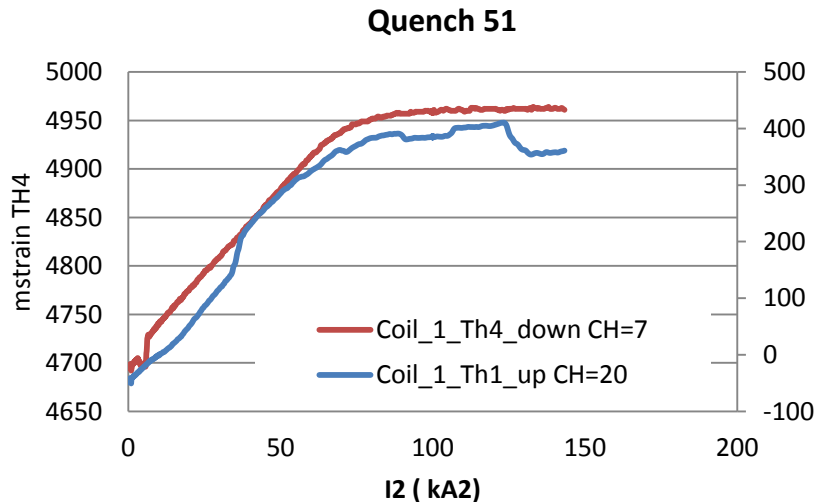
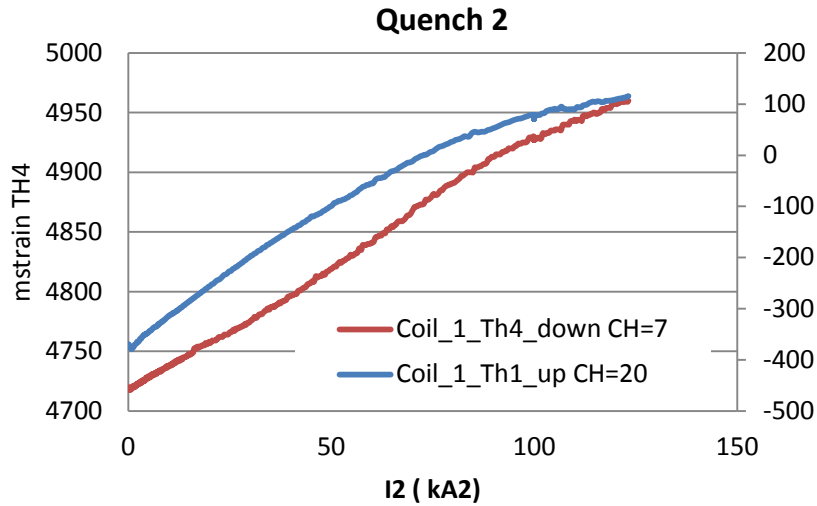


Nothing special for the moment was seen on the gauges on COIL 2

Quenches are on LJ or HFS

Training quenches coil by coil. Strain on the coil 1 in run 2. SMC#3

Training performed at 4.2K and at 1.9K , quenches performed with 20 A/s ramp rate



These two gauges should measure the same value....

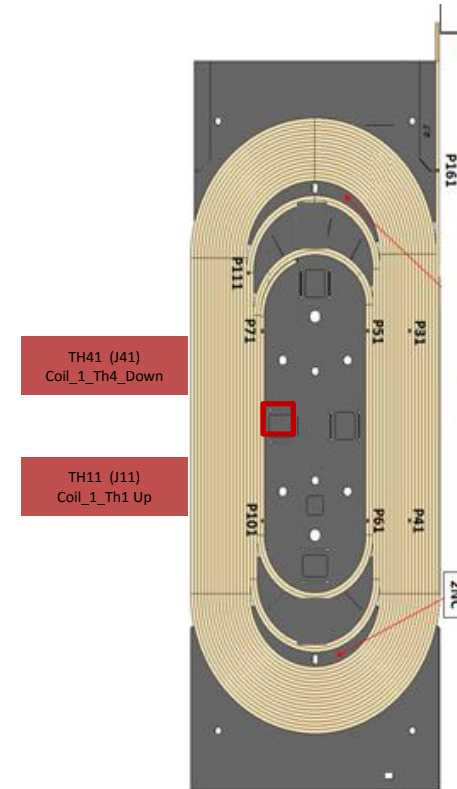
Is not the casesee the scales

BUT

They have the same variation with current ² ...see the shape

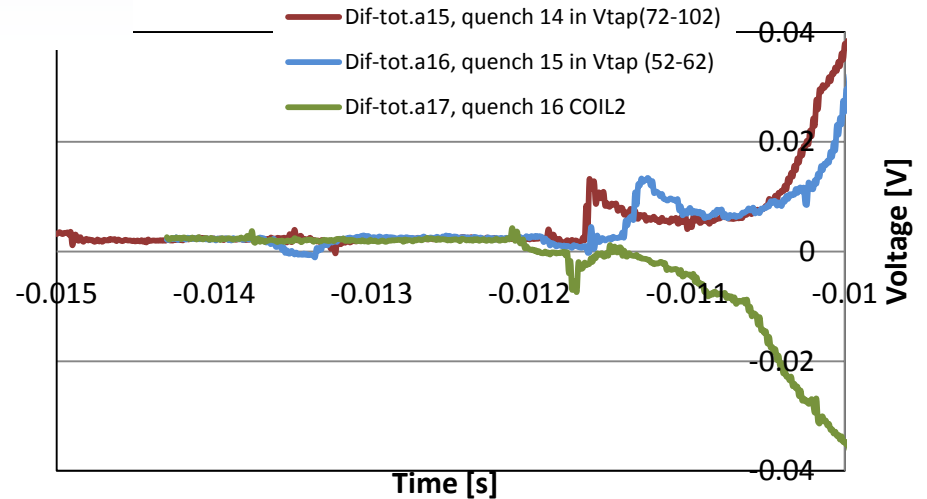
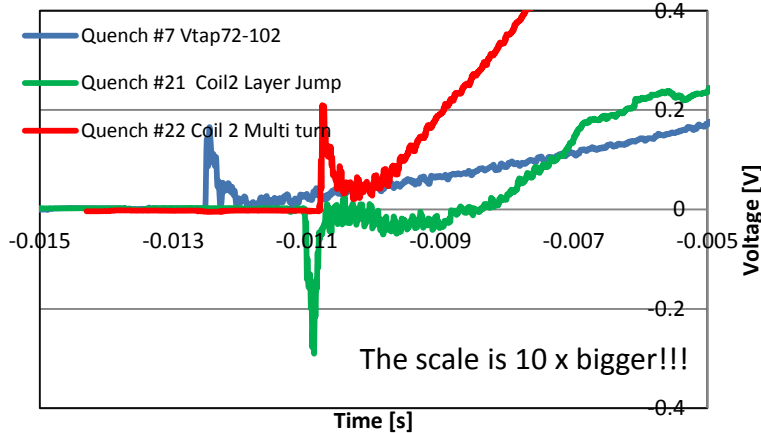
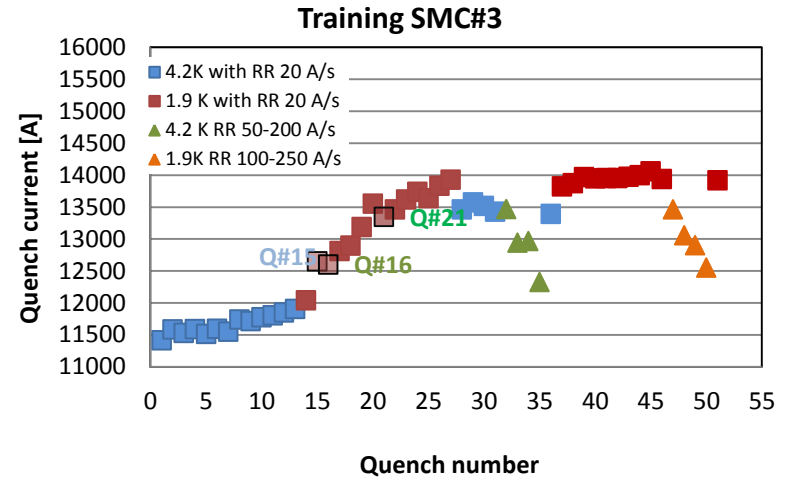
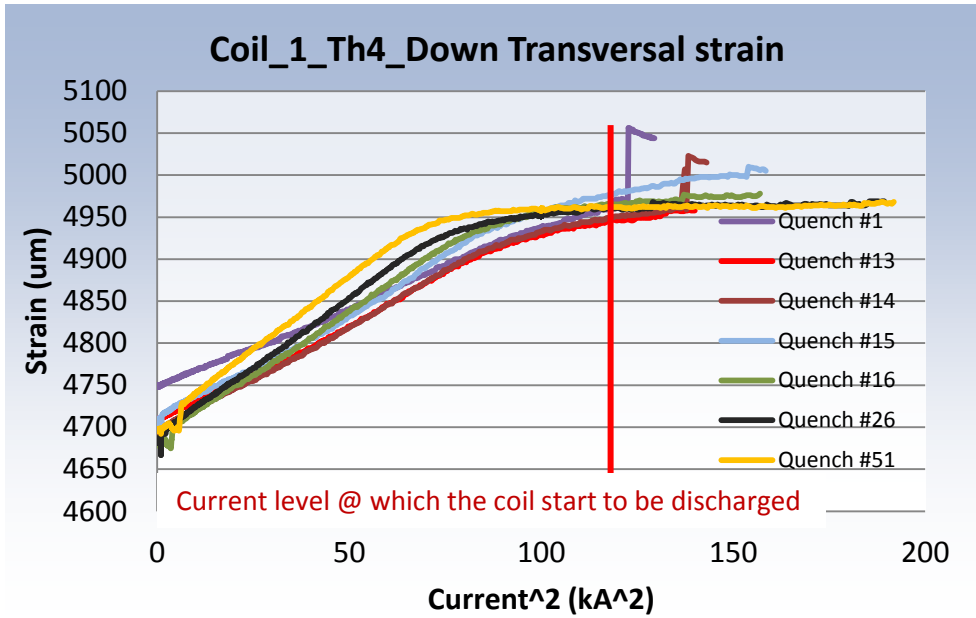
μstrain TH1

μstrain TH1



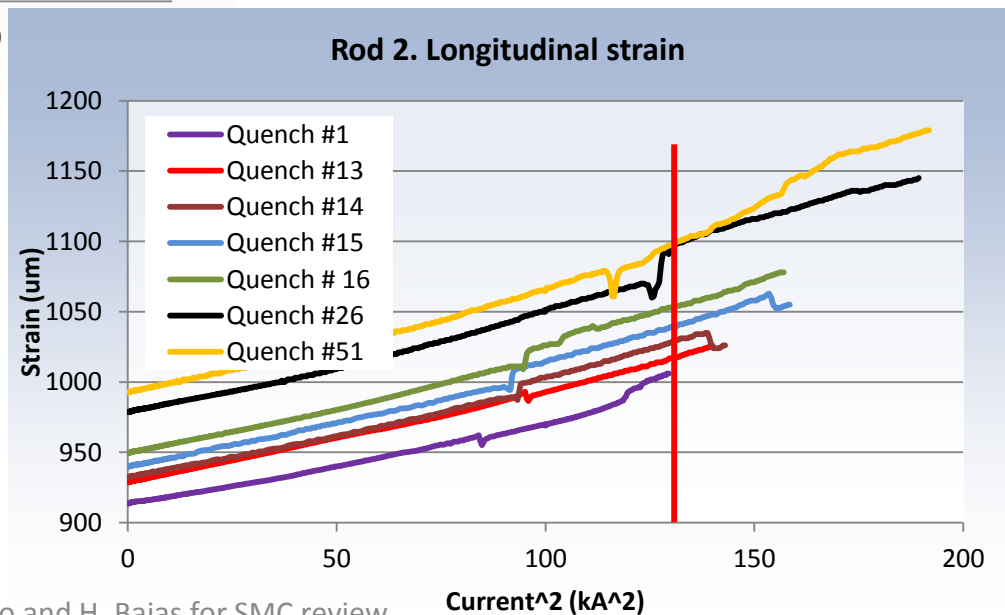
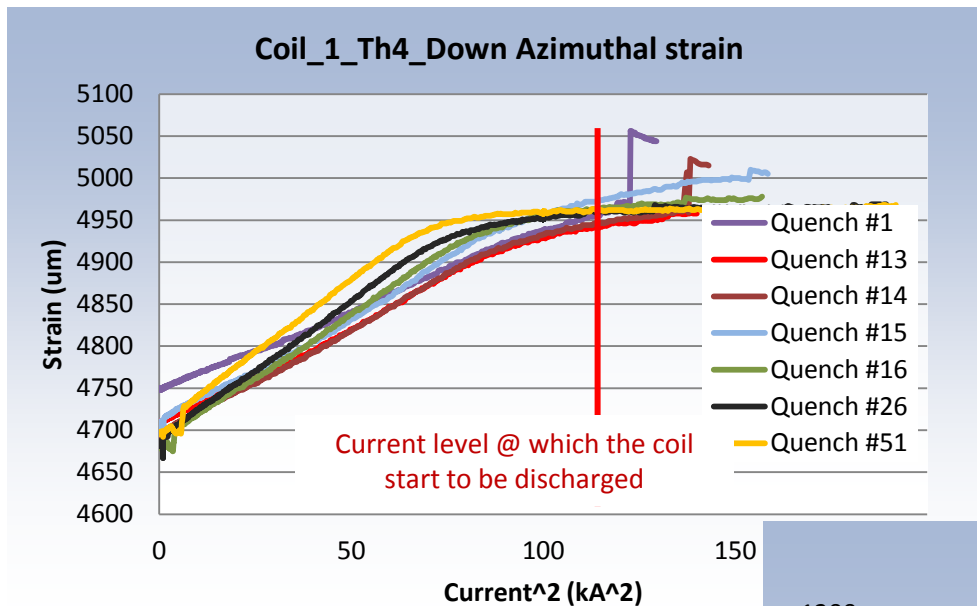
Strain gauges on COIL and spikes in the V signals I run 2. SMC#3

Training performed at 4.2K and 1.9K , 10-20 A/s RR, and variable RR



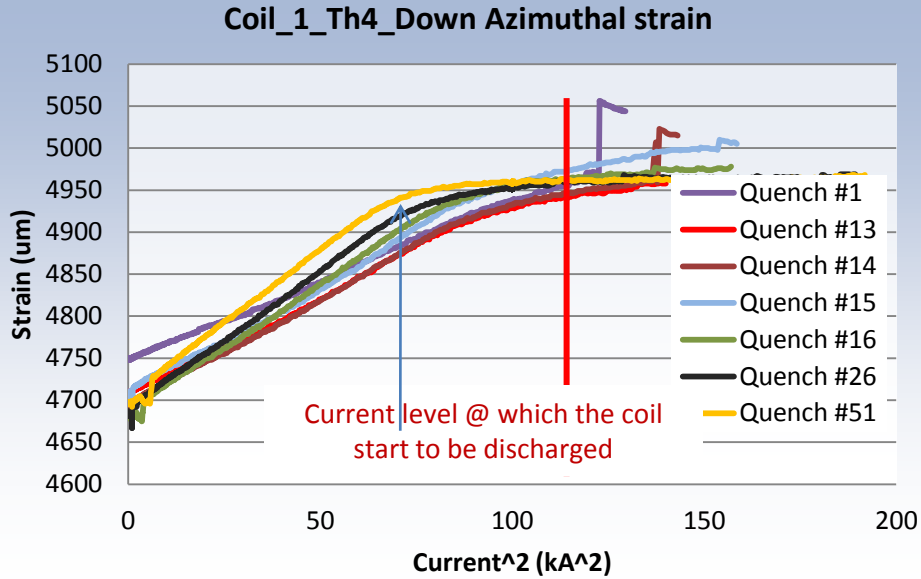
Strain gauges on Coil and Rod In run 2. SMC#3

Training performed at 4.2K and 1.9K , 10-20 A/s RR, and variable RR

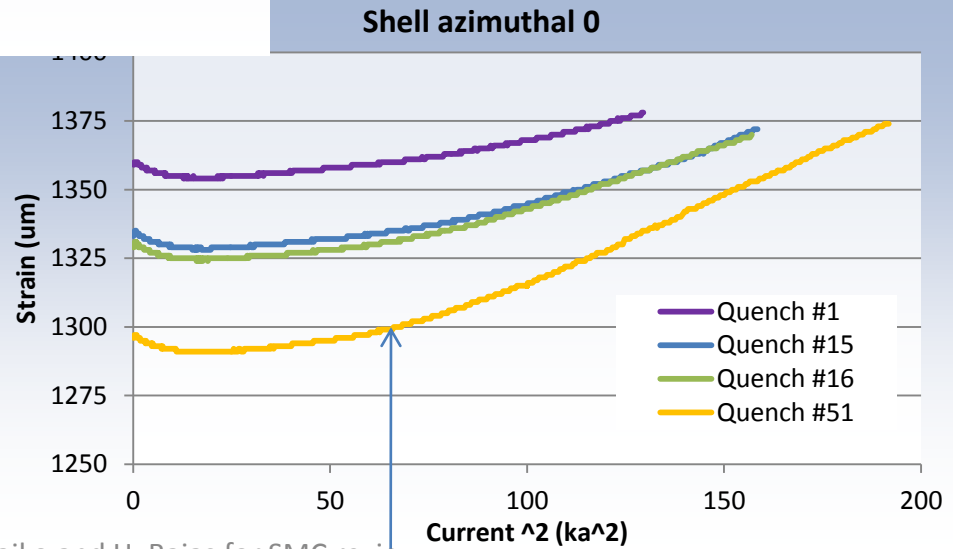


Strain gauges on Coil and Shell in run 2. SMC#3

Training performed at 4.2K and 1.9K , 10-20 A/s RR, and variable RR

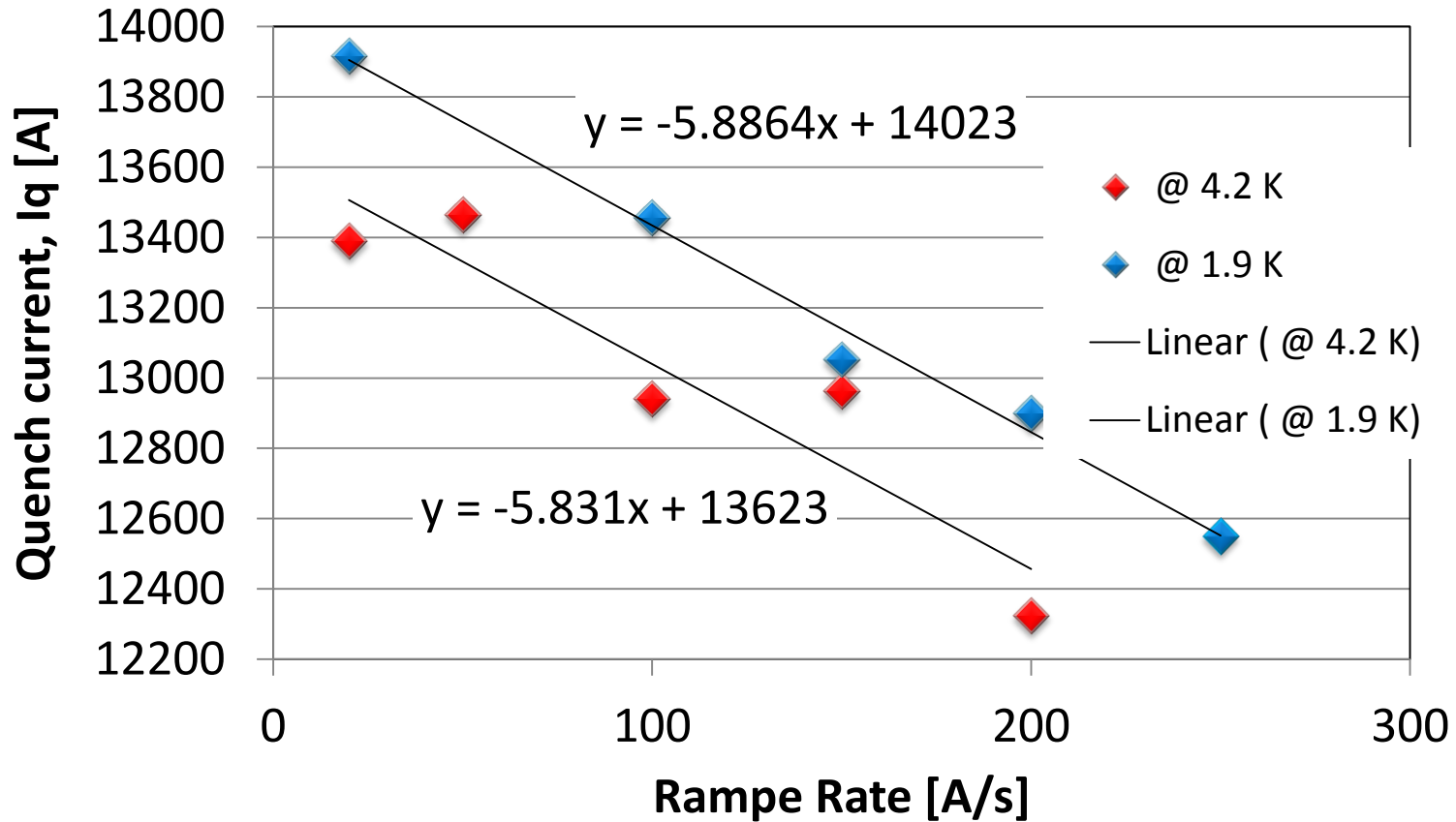


In the shell : $100 \mu\epsilon = 7 \text{ MPa}$



High Ramp Rate quenches. SMC#3

Training performed at 4.2K and at 1.9K , quenches performed with ramp rates up to 250 A/s



High propagation velocity **30-60 m/s**

and multi zones quench :

in the **high field zone** first then in the low field zone

Temperature rise in the coil after quench. Run 1, 2 and 3. SMC#3

Goal: Assessment of the temperature rise in the cable during a quench using analytical method.

Mean : Resolution of the energy balance between Joule effect and rate of heat.

Rearranged equation:

$$\int_0^{t_{trigger}} I(t)^2 dt = a_{Cu} a_t \int_{T_0}^{T_{max}} \frac{\rho \cdot c_p(T)}{\rho_E(RRR, B, T)} dT$$

Volumetric heat capacity of the total cross-section [$J K^{-1} m^{-3}$]

Electrical resistivity of copper [Ωm]

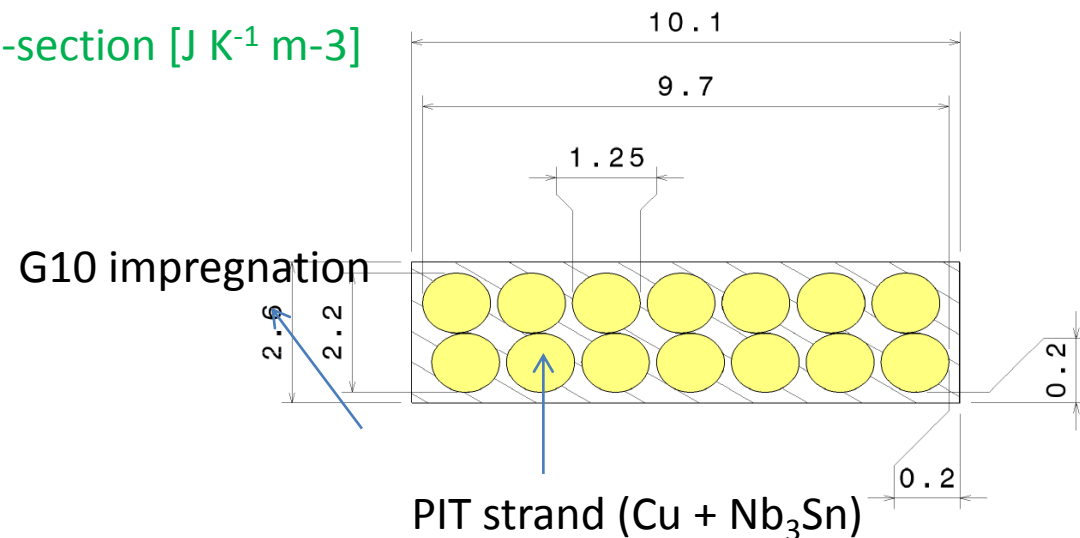
Solve the equation to retrieve T_{max} [K]

[1]

Stephan Russenschuck

[2]

Pierre Manil, Federico Regis,

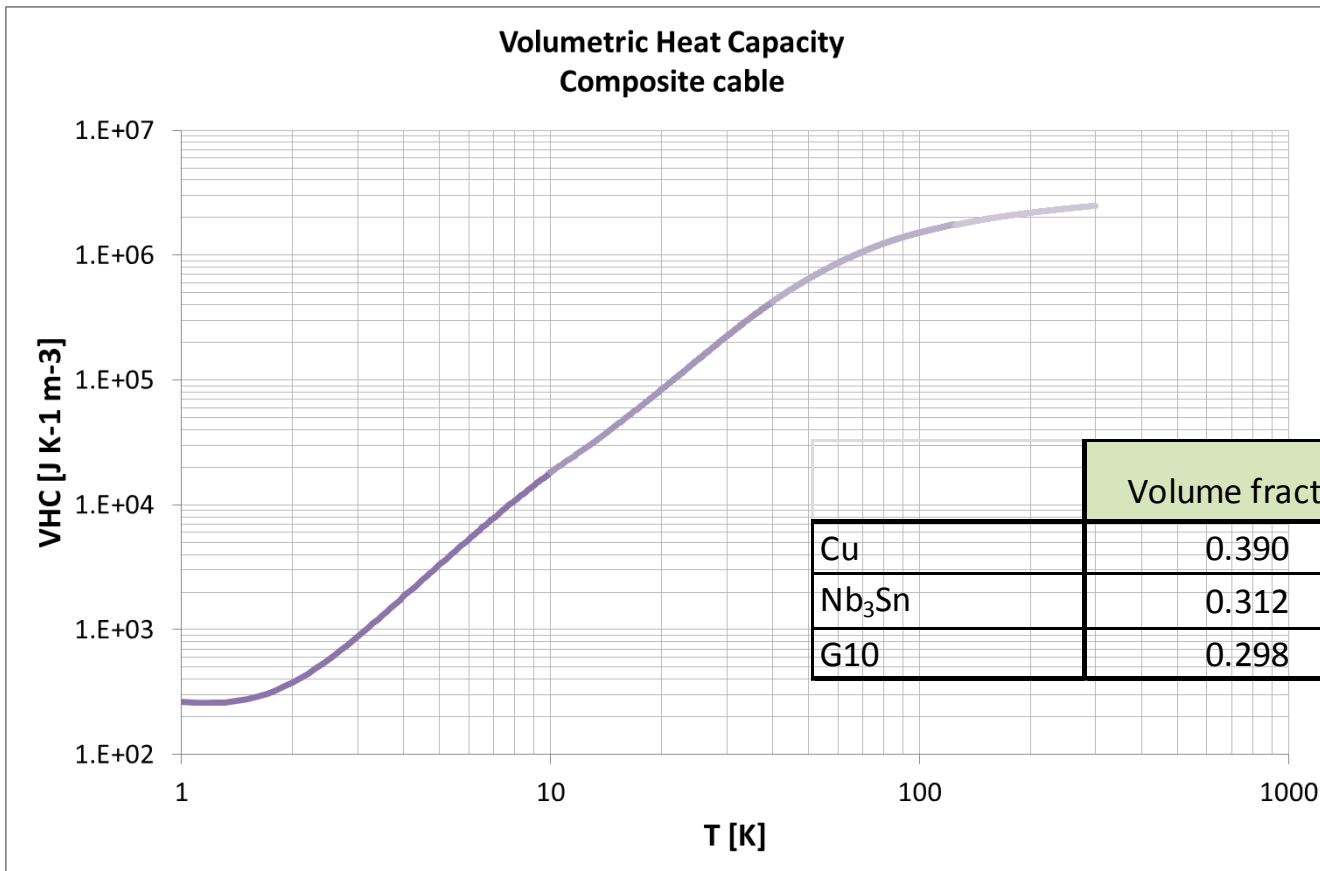


Temperature rise in the coil after quench. Run 1, 2 and 3. SMC#3

Volumetric Heat Capacity [J K⁻¹ m⁻³]

Mixture law:

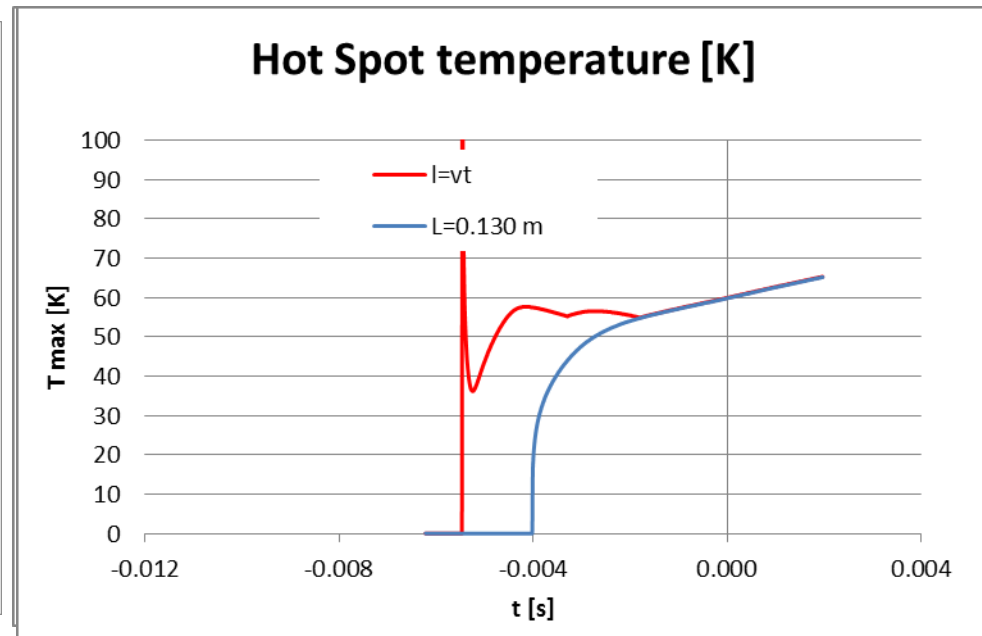
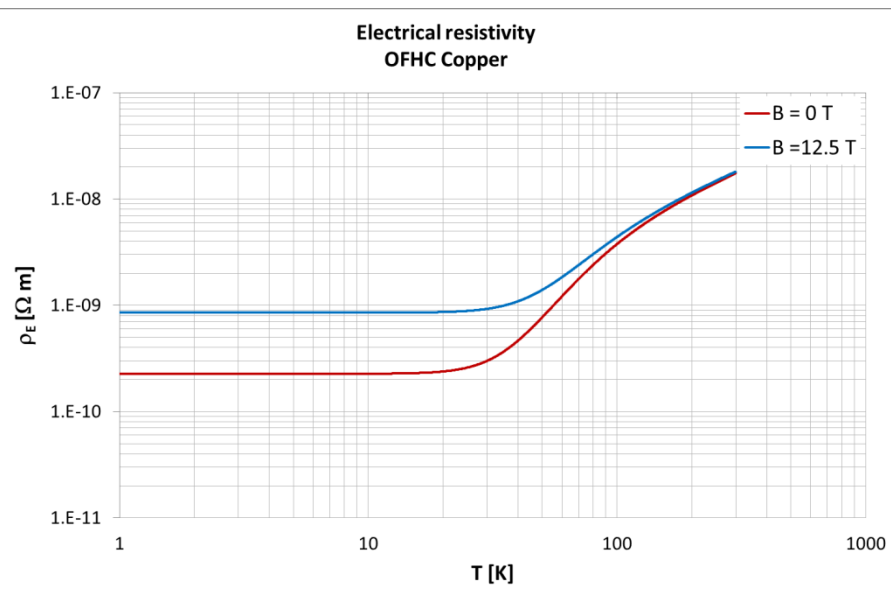
$$\mathbf{VHC}_{\text{composite}} = v_{\text{Cu}} * \mathbf{VHC}_{\text{Cu}} + v_{\text{Nb}_3\text{Sn}} * \mathbf{VHC}_{\text{Nb}_3\text{Sn}} + v_{\text{G10}} * \mathbf{VHC}_{\text{G10}}$$



Temperature rise in the coil after quench. Run 1, 2 and 3. SMC#3

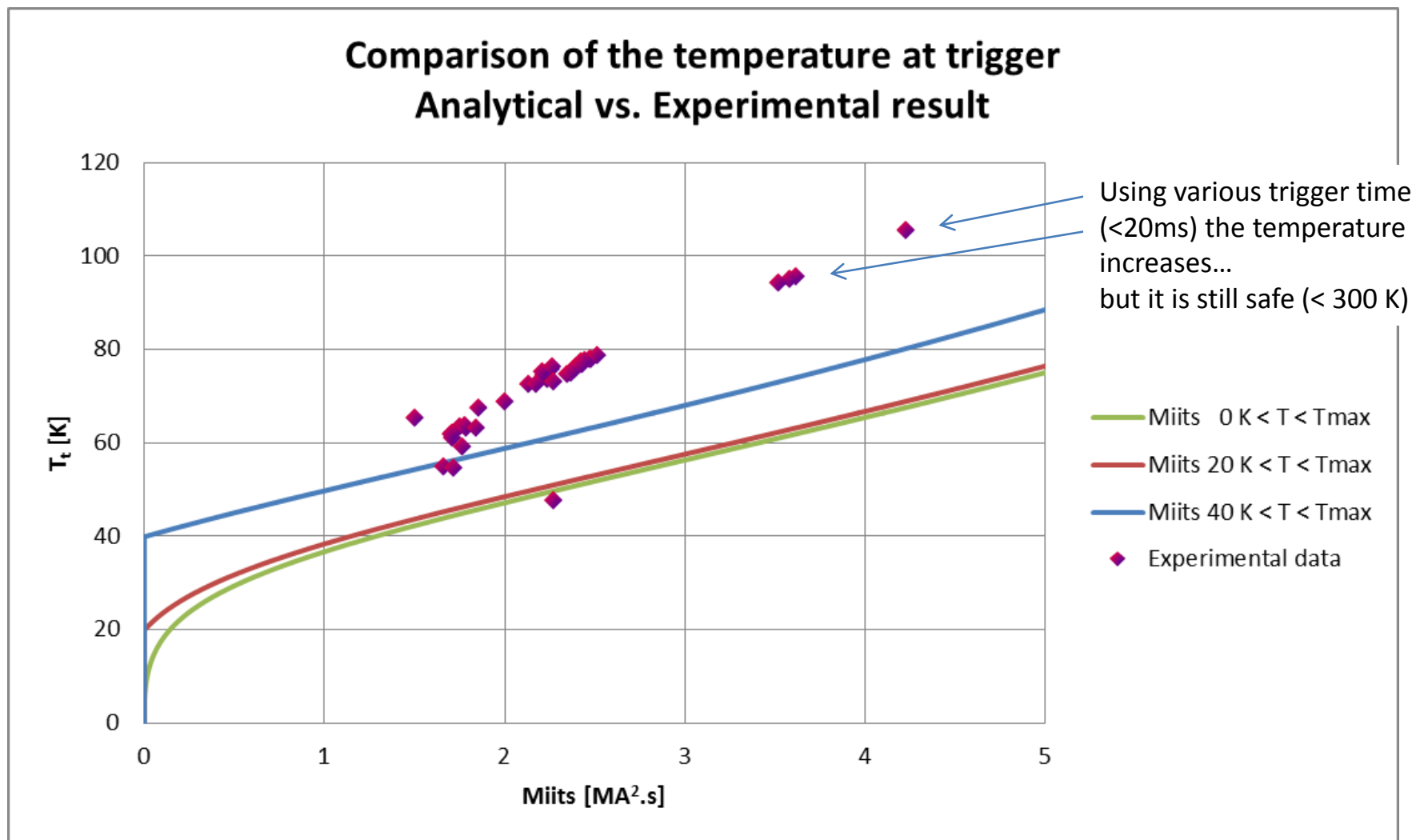
Electrical resistivity of copper

$$\rho_E [\Omega \text{ m}] = f (B(I), T, RRR)$$



Assessment of the temperature in the copper using the measured resistivity between V_72-102. Attempt to using propagation velocity...

Temperature rise in the coil after quench. Run 1, 2 and 3. SMC#3



Simple model in relatively good agreement ... FEM to go any further.

SMC. Conclusions

- ❑ SMC#1 could tell us little info as it was limited by a splice at 7 kA @ < 50% of the I_{ss}

- ❑ **SMC#3 is a nice magnet TELLING US A LOT ABOUTH THE Nb₃Sn CABELS!**
 - ❑ Most of the quenches occurs in the HFS so the correlation between max. filed and stress can be studied
 - ❑ 95% of SS current attained at 4.2K
 - ❑ No quenches in the splices (Nb₃Sn-NbTi). Low contact resistance, comparable with those made with NbTi cables.
 - ❑ NbTi lead cable is limiting the SMC #3 performance at 4.2K
 - ❑ Measurement results:
 - ❑ RRR= 75
 - ❑ Splice resistances < 1 nOhm
 - ❑ Inductance = 1.8 mH/coil and symmetric
 - ❑ Protection with external dump resistor of 40 mOhm: ok, Temperature < 100 K
 - ❑ Detection threshold 100 mV for 10 ms: adequate for propagation study
 - ❑ Longitudinal quench propagation velocity 10-20 m/s
 - ❑ 74 % of quenches occurs in the HFS mainly in coil1
 - ❑ No flux jumps at low or intermediate currents
 - ❑ Most of the quenches occurs in coil1.

- ❑ **SMC#3 run 3 test results should be carefully analyzed in the next coming weeks to correlate its quench behavior with its new strain status**