

Task 2 Cavern Study

Ground model and 3D cavern layout

5 December 2011

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Requirements Document

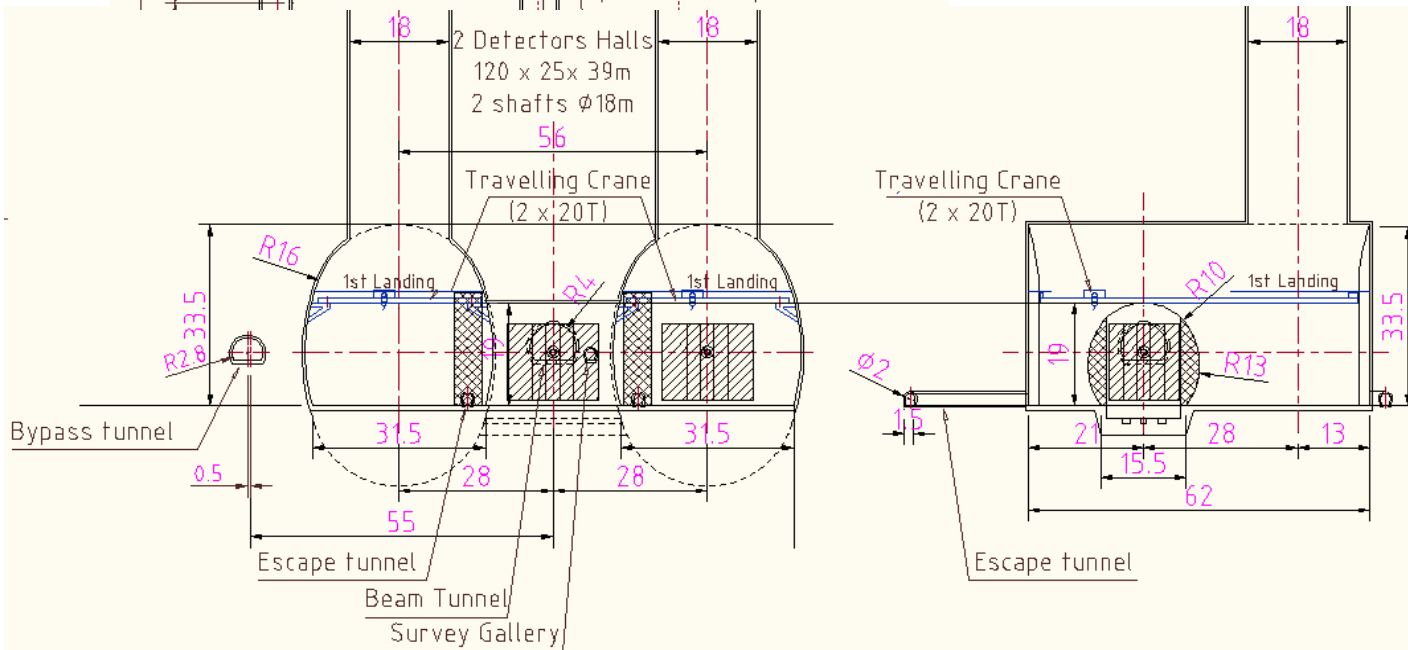
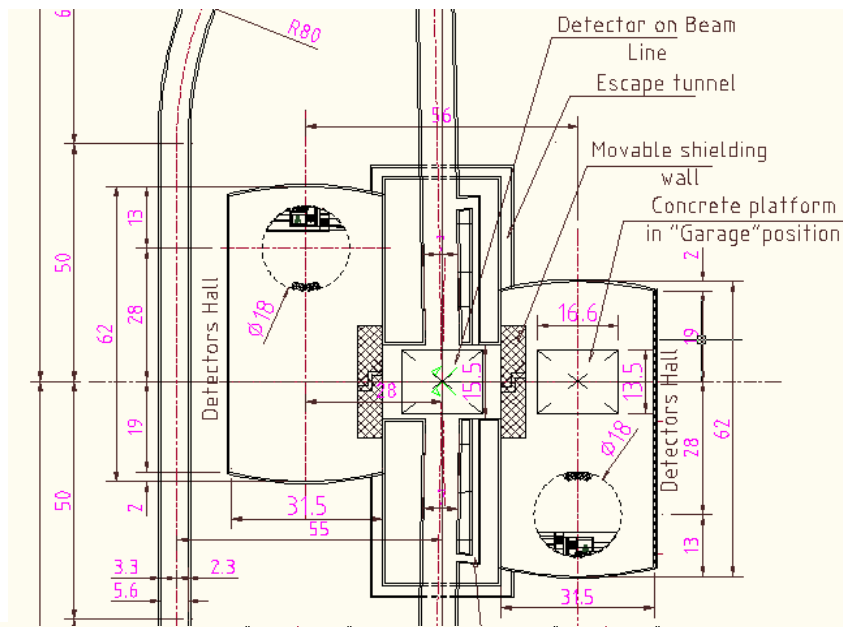
Matt Sykes

This presentation...

1. General Overview
2. Task 2 Study Summary
3. Stress analysis and ground yield
4. Construction sequence
5. CERN Molasse Geological model
6. Short term behaviour – Small strain stiffness
7. 2D Finite Element analysis of interaction cavern
8. 3D bedded-spring model of interaction cavern
9. Conclusions and recommendations

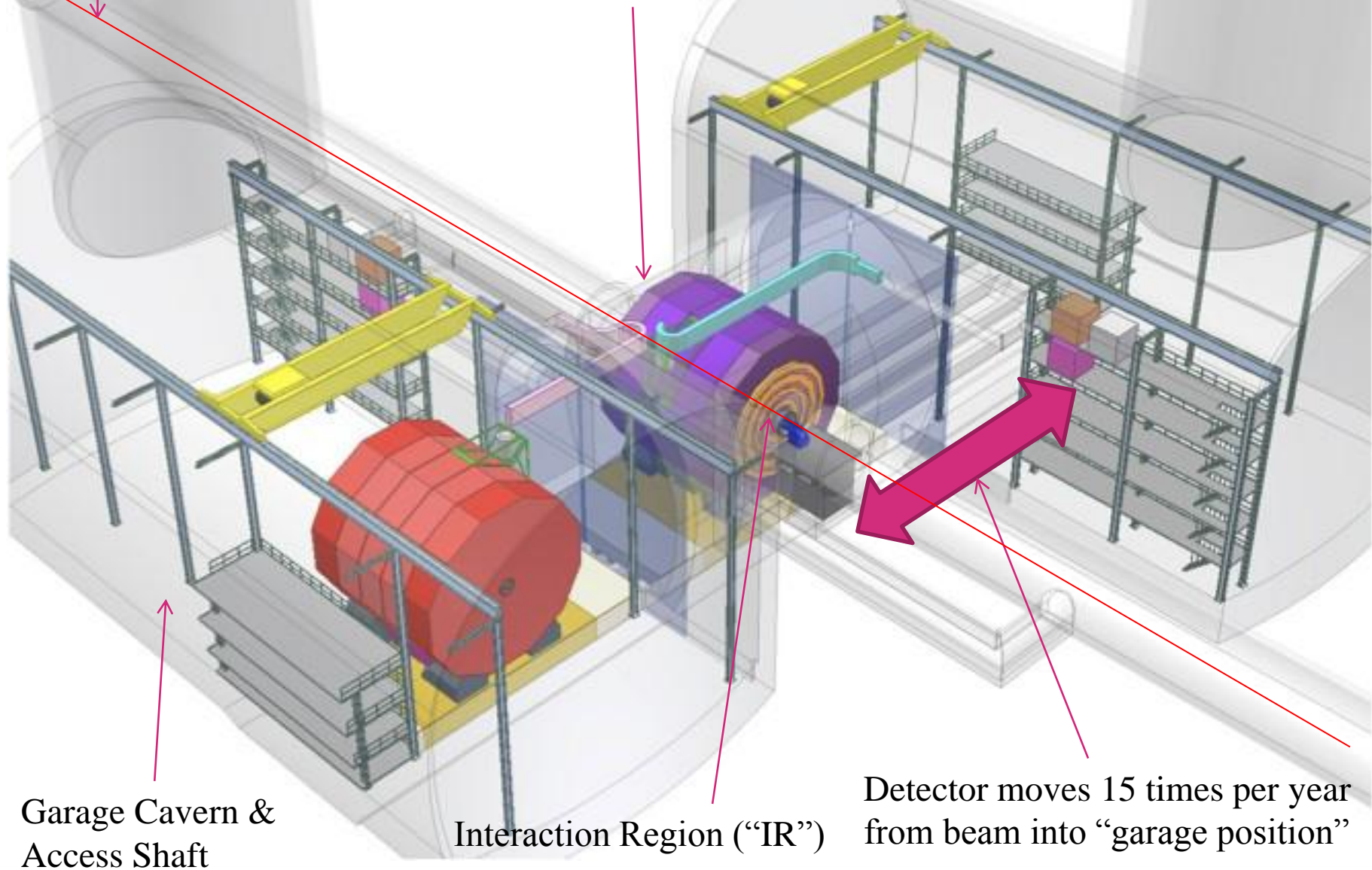
General Overview

CLIC Geometry (G)



Beam Line.

15,000t detector on a slab and movement system.

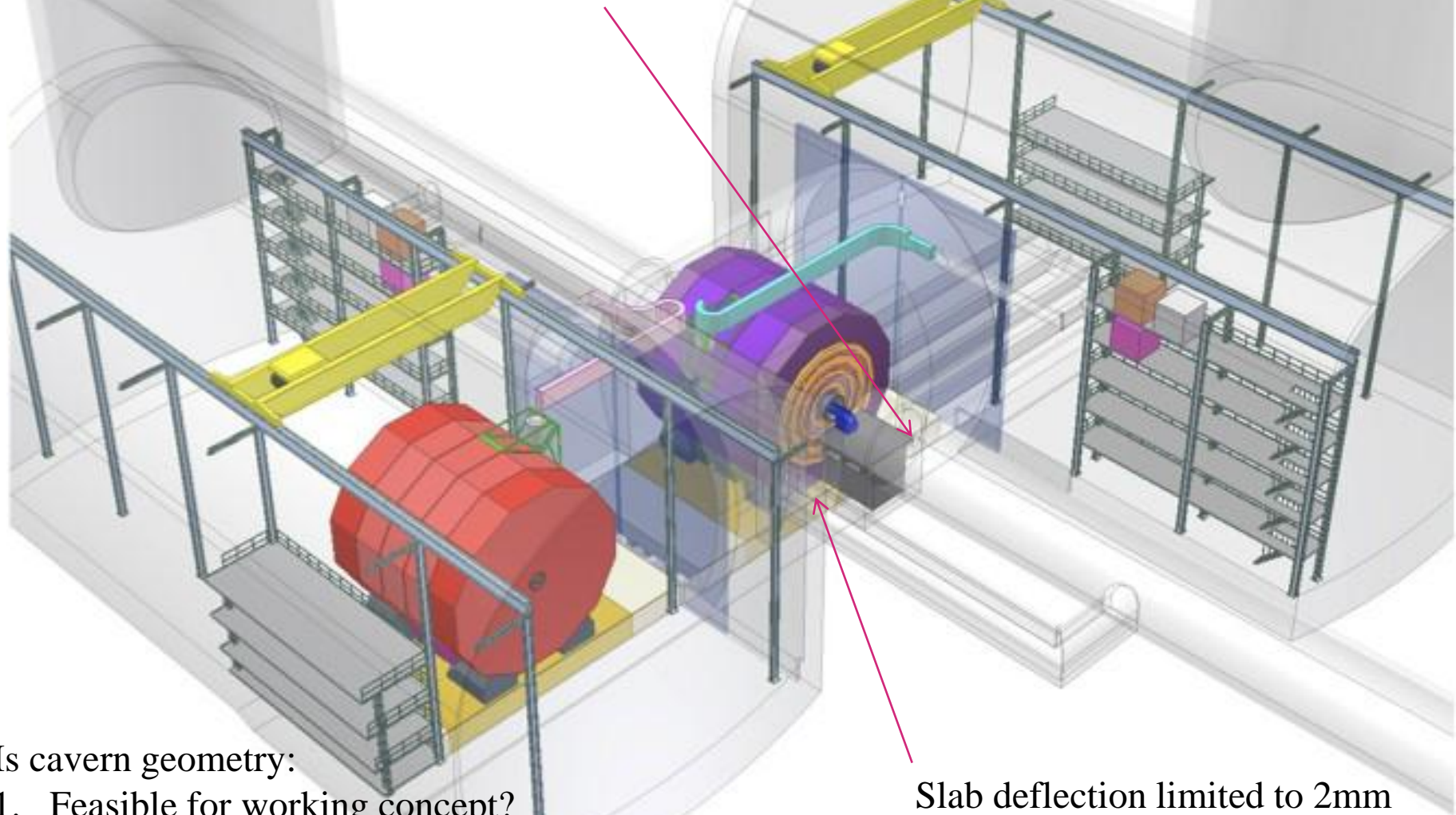


Garage Cavern & Access Shaft

Interaction Region ("IR")

Detector moves 15 times per year from beam into "garage position"

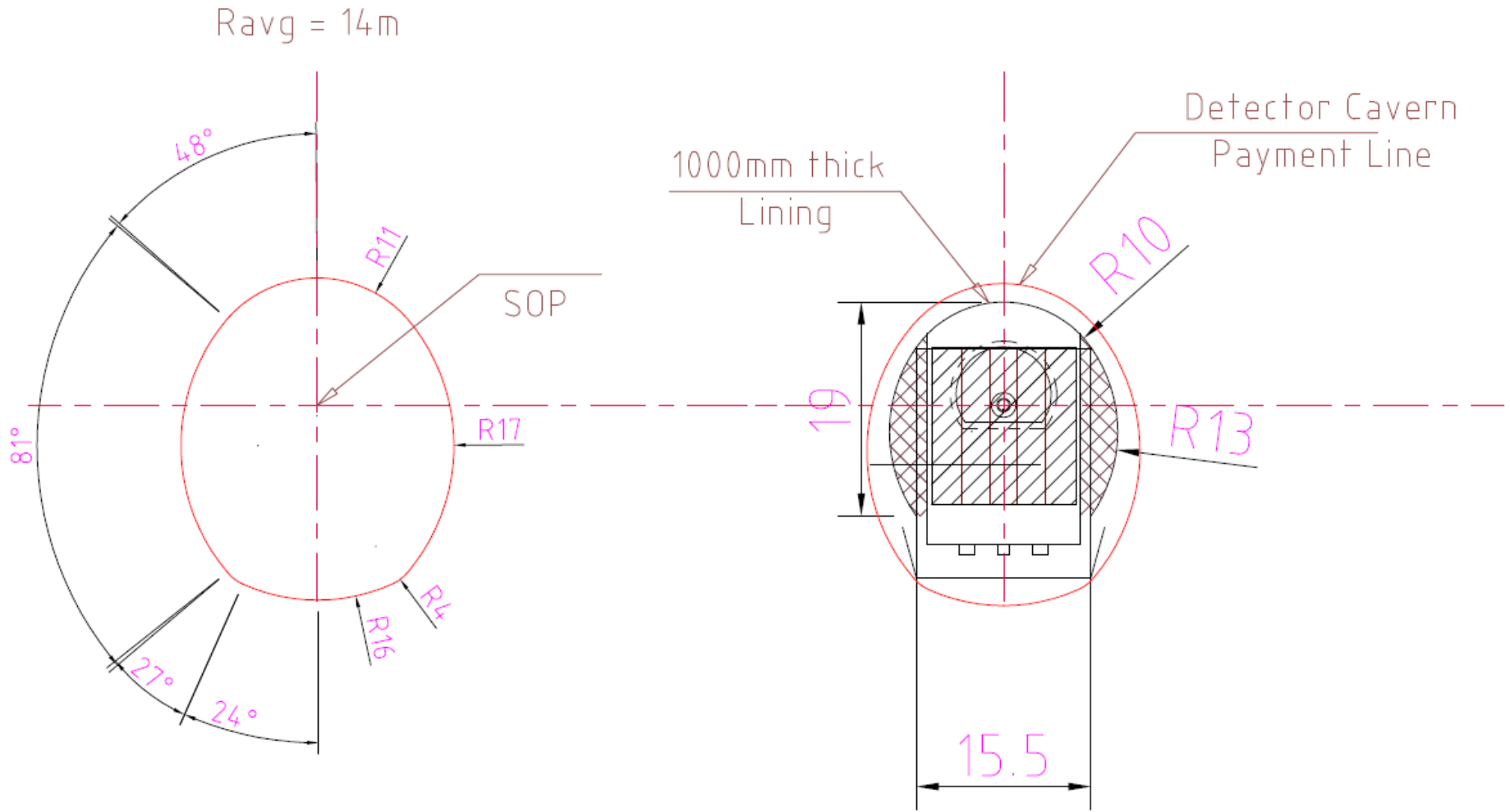
How do we limit cavern invert deflection to less than 0.5mm (creep and absolute)
(Controlled by ground yield and invert stiffness)



- Is cavern geometry:
1. Feasible for working concept?
 2. Influencing yield at IR?

Slab deflection limited to 2mm
(20m by 20m concrete slab)

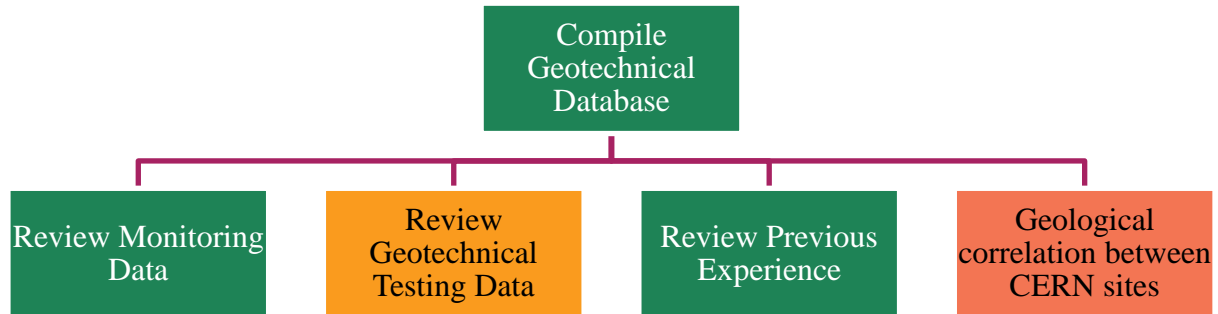
Interaction Cavern Outline Geometry (G)



Task 2 – September Presentation



Geotechnical Review



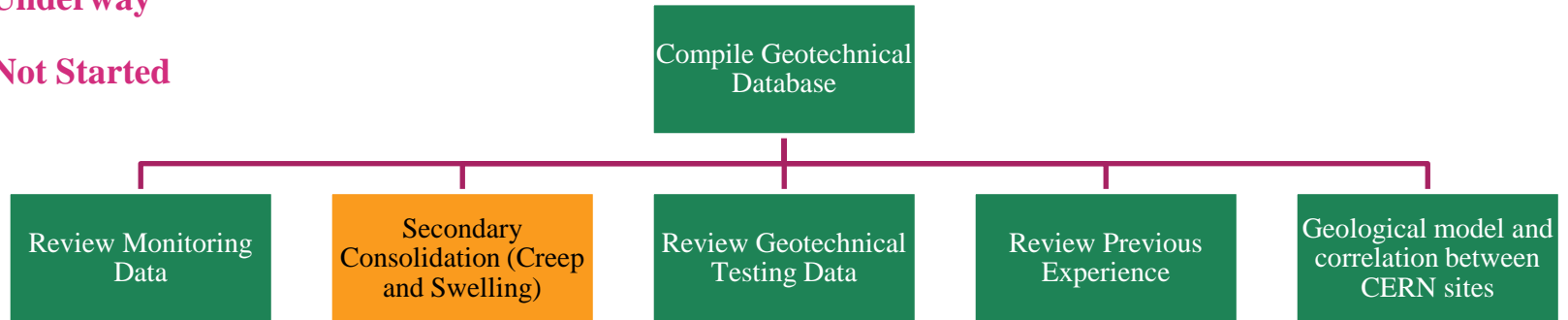
Cavern Design



Task 2 – Study Summary



Geotechnical Review



Cavern Design



Stress Analysis and Ground Yielding

Boundary Element Modelling (3D Stress Analysis)

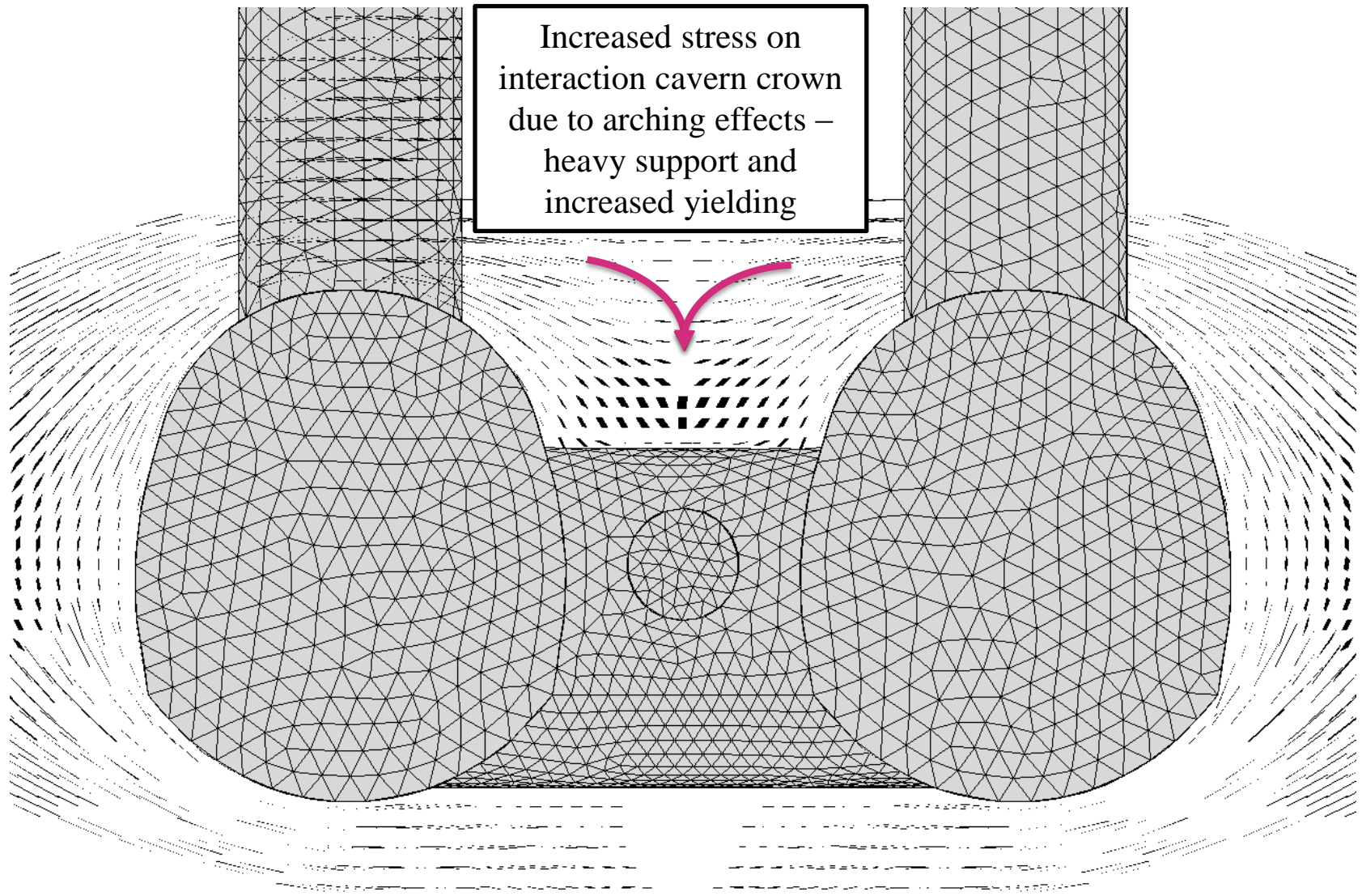
Linear elastic stress analysis in *Examine3D*.

Indication of how stress manifests at the interaction of the cavern's boundary and the ground.

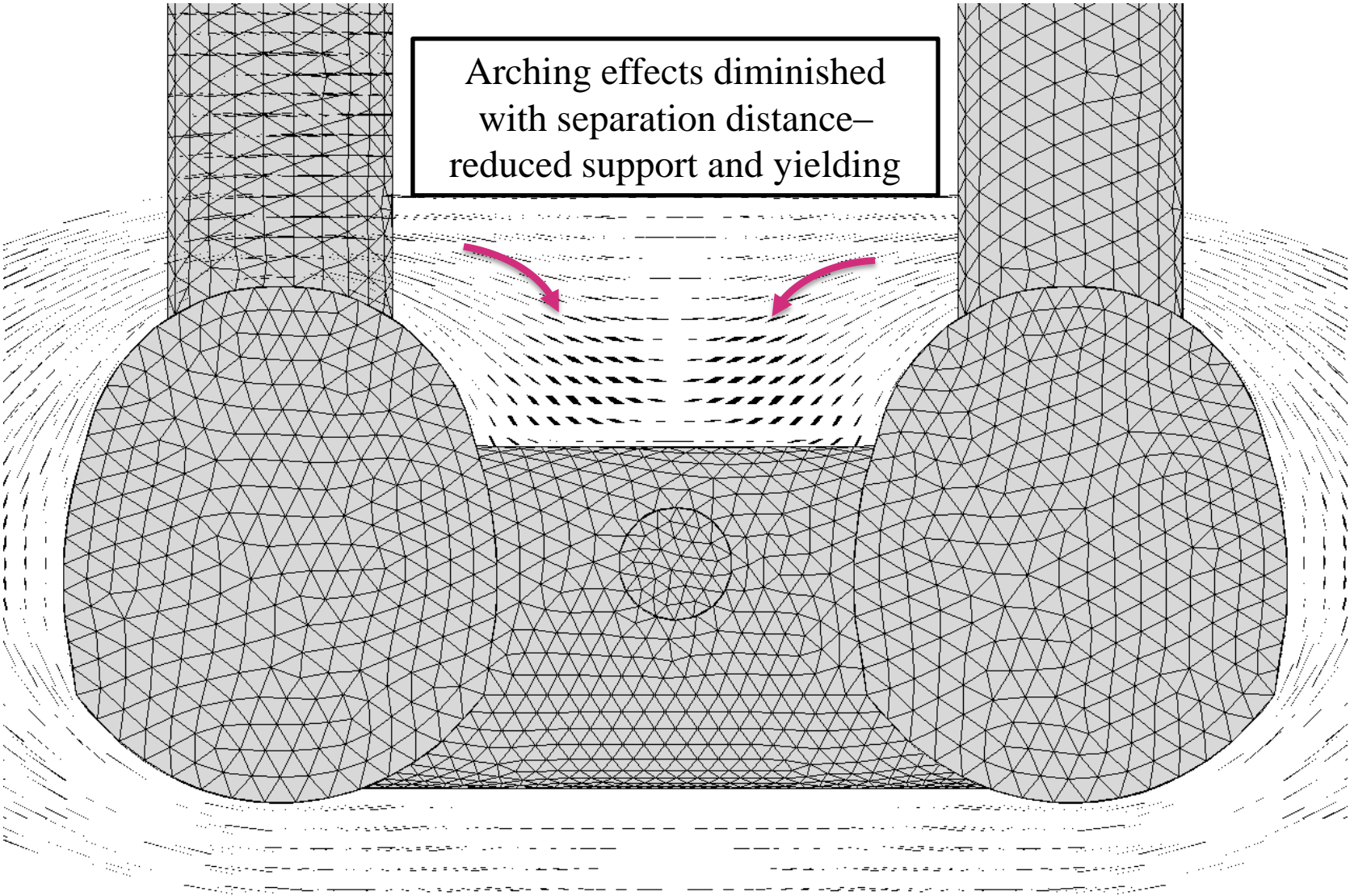
Analyses carried out comparing Layout G and a layout where the caverns are pushed apart by 5m.

Effective strength criteria used to estimate rock mass yielding.

Layout G – Principal Stress Trajectories



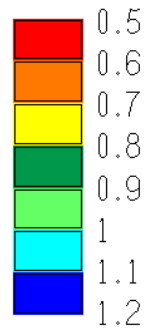
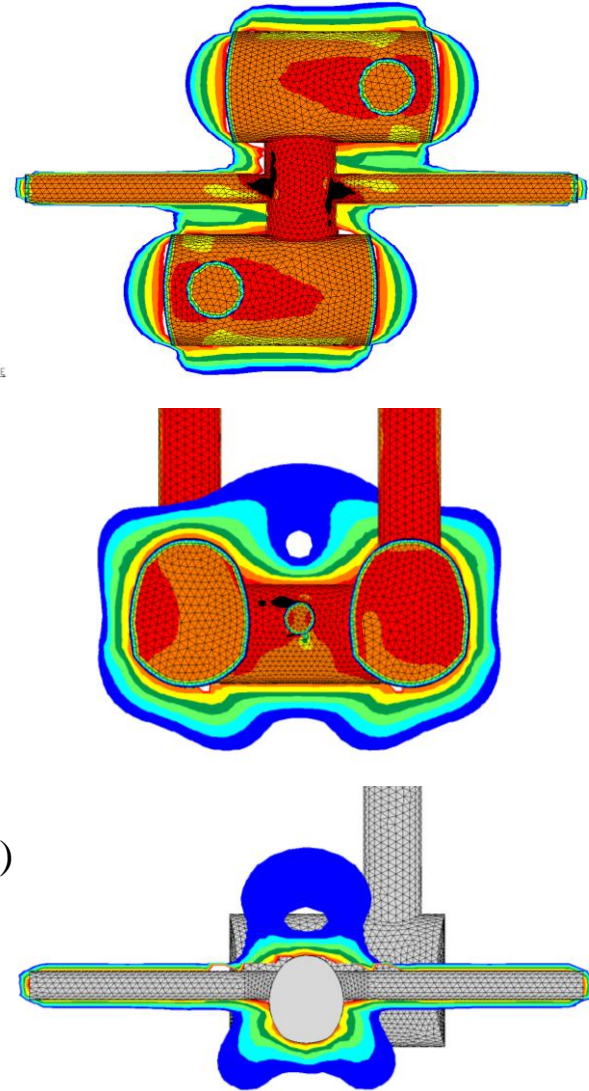
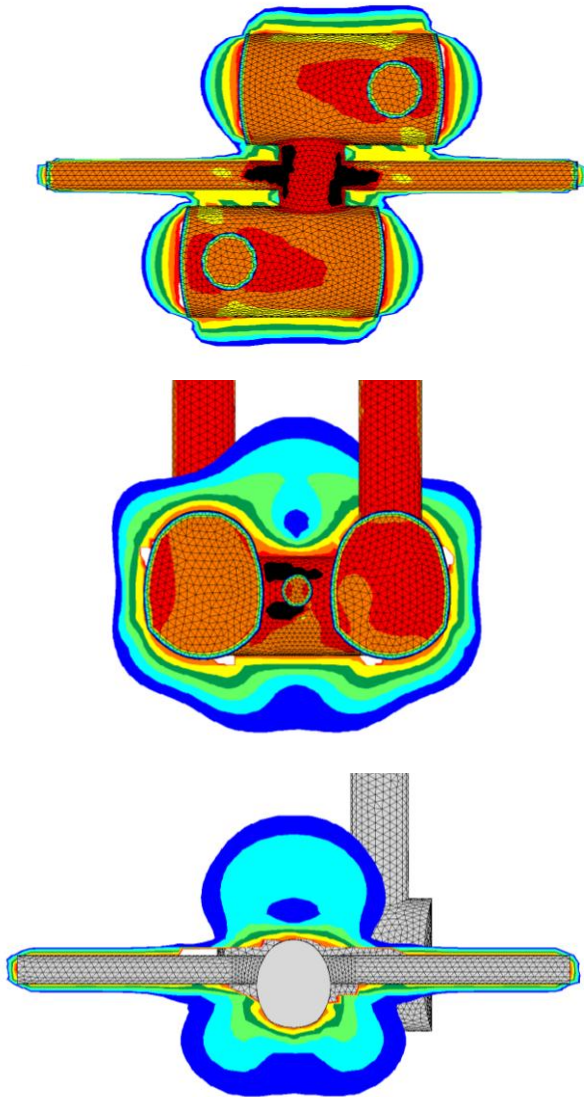
Layout G + 10m – Principal Stress Trajectories



Contours of Overstress

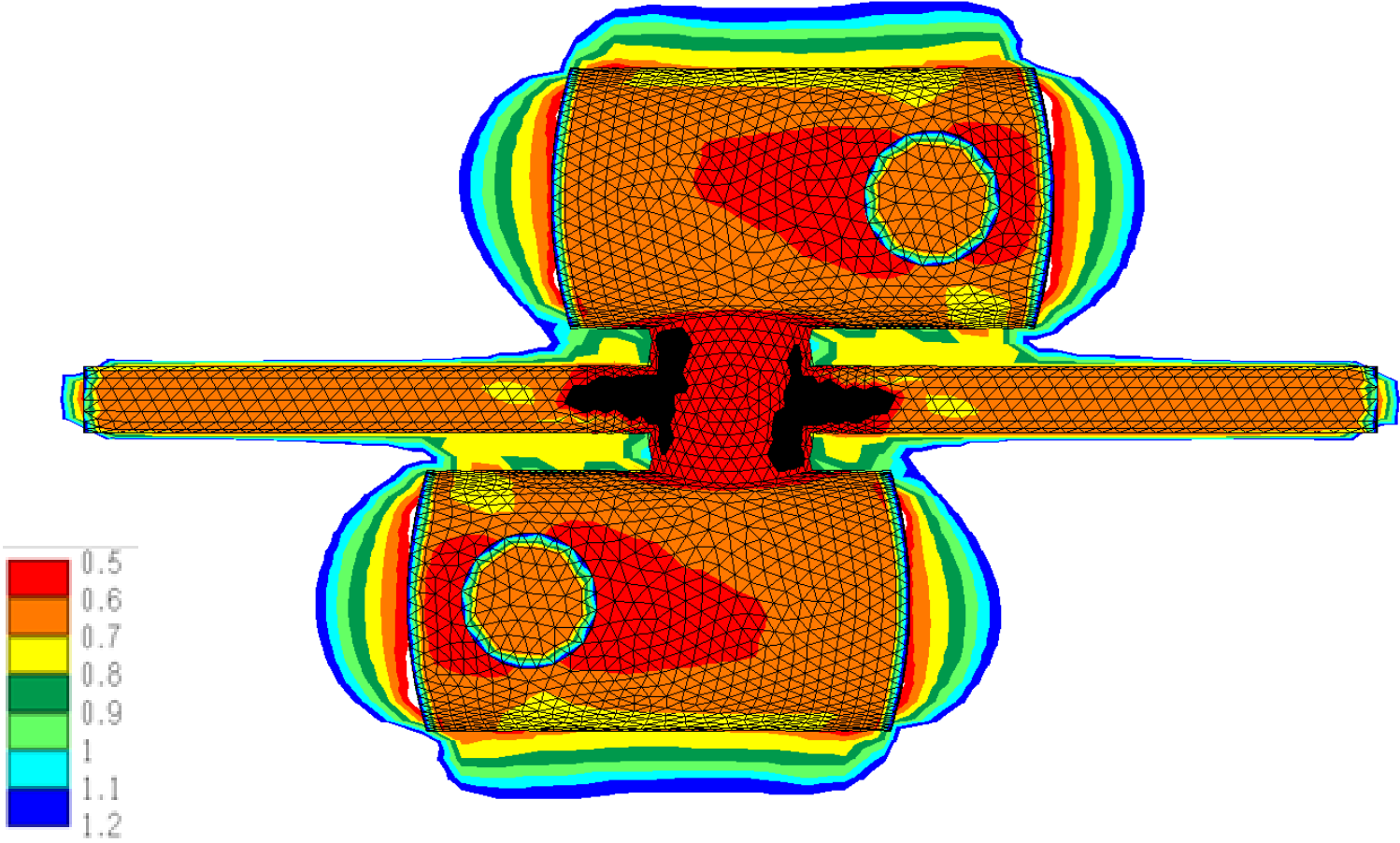
Geometry G

Geometry G + 10m



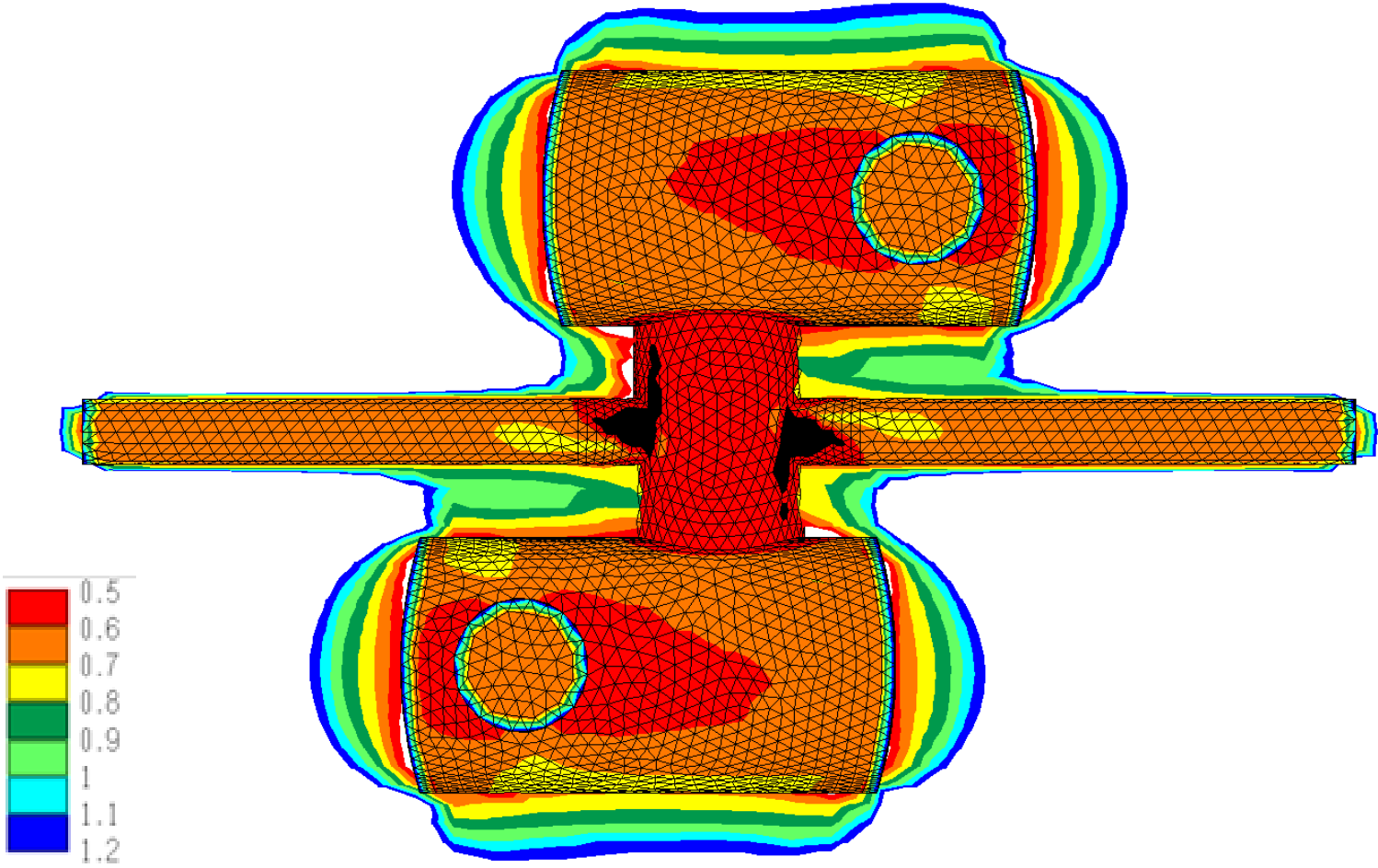
Mobilised Strength
(overstressed when < 1)

Layout G



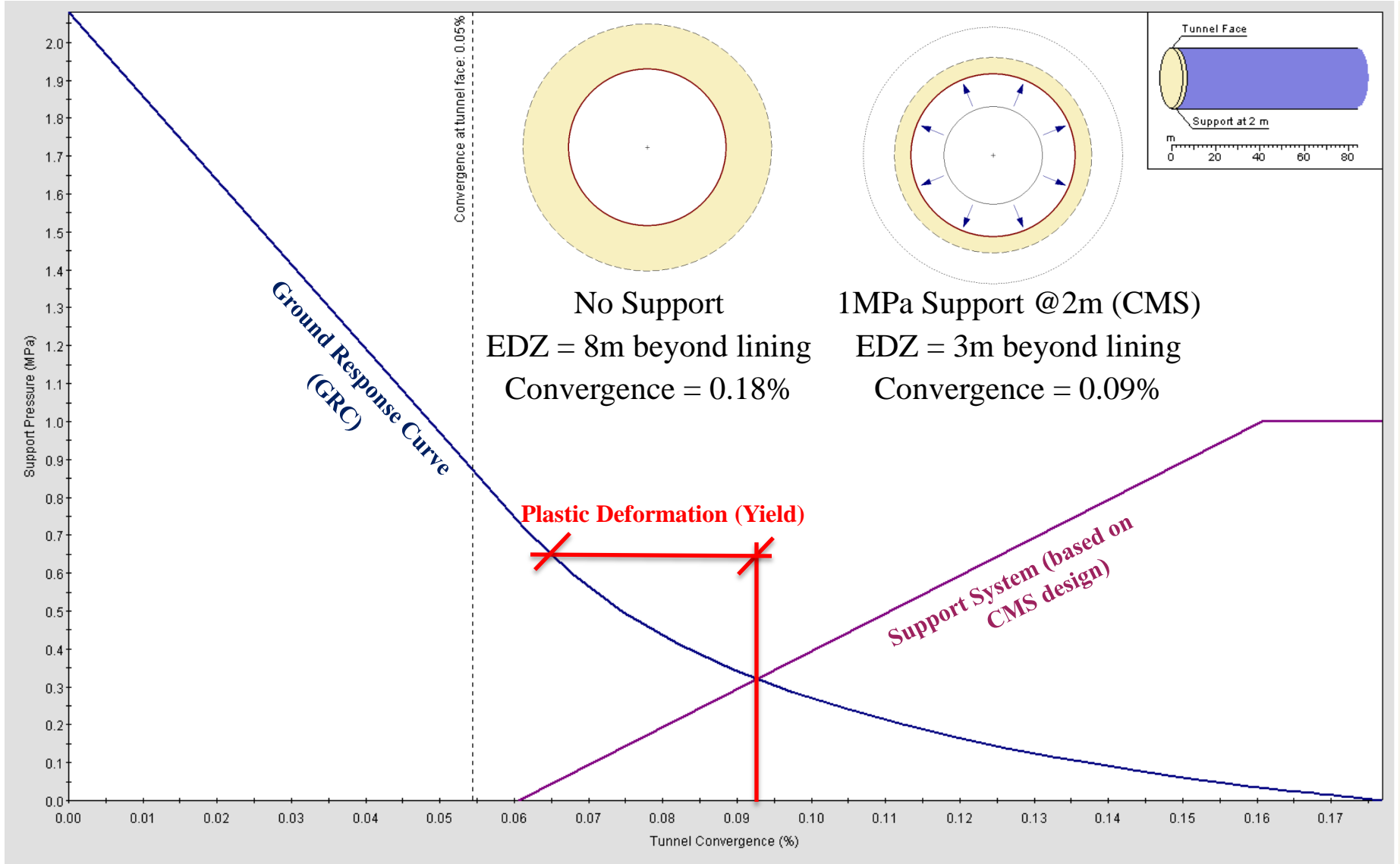
Mobilised Strength
(overstressed when < 1)

Layout G + Interaction Cavern Enlargement



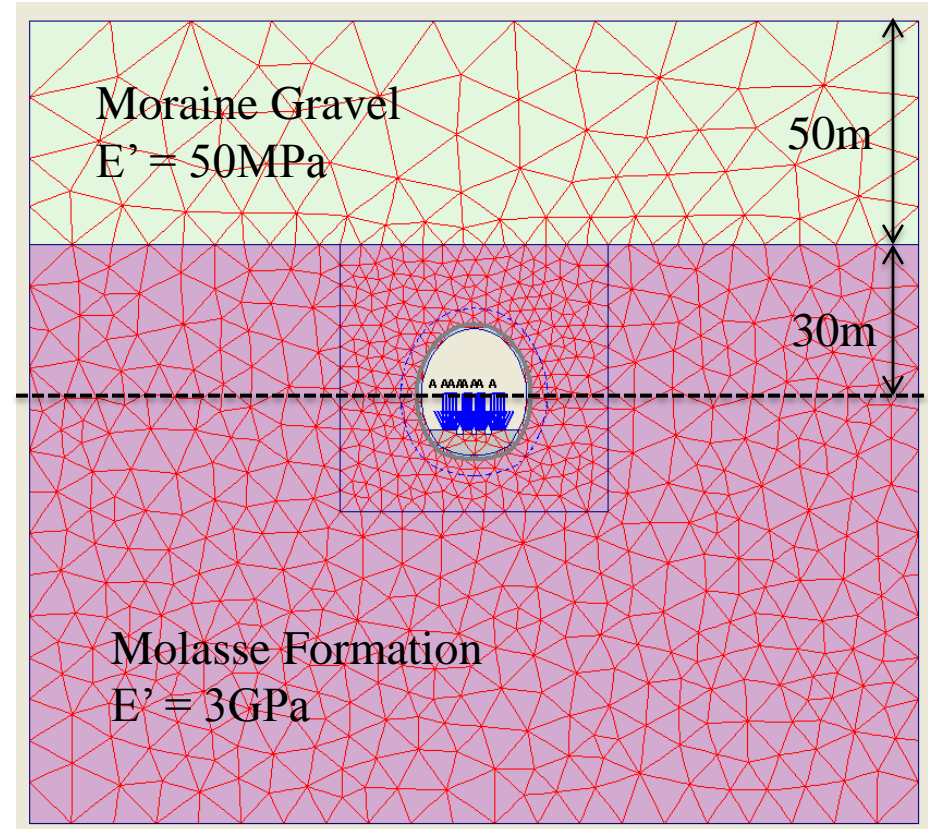
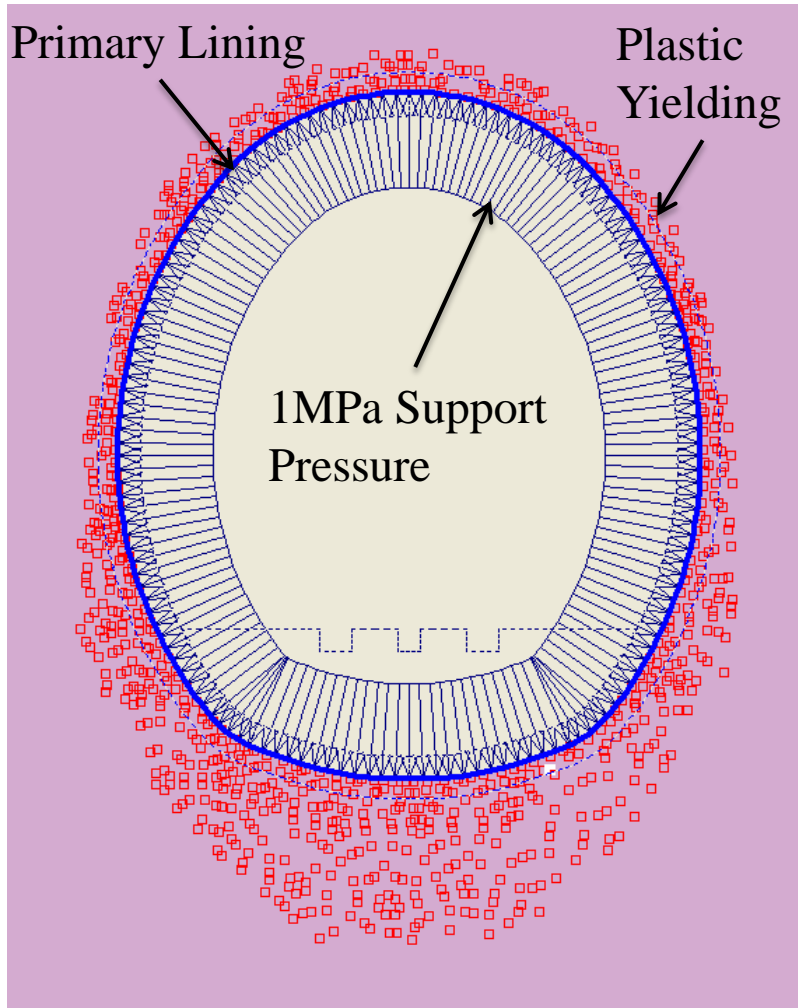
Mobilised Strength
(overstressed when < 1)

SCL Support Design



Final convergence: 0.09%, FS: 3.12
 Convergence at tunnel face: 0.05%, Convergence at support: 0.06%

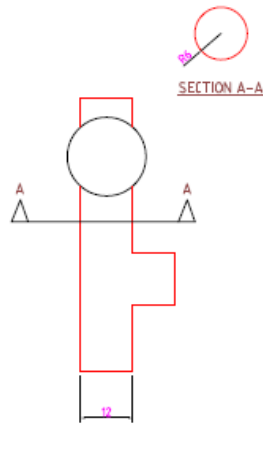
Conservative 2D FE analysis



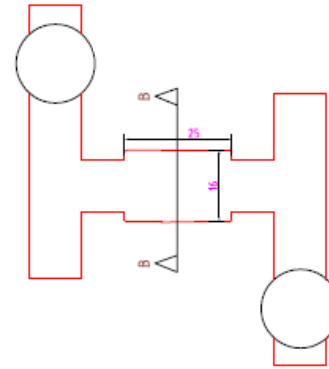
Construction Sequence



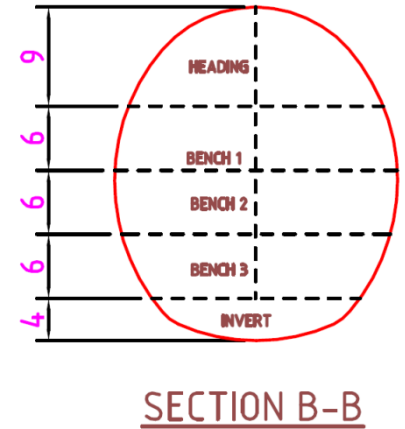
PHASE I - SINK SHAFTS



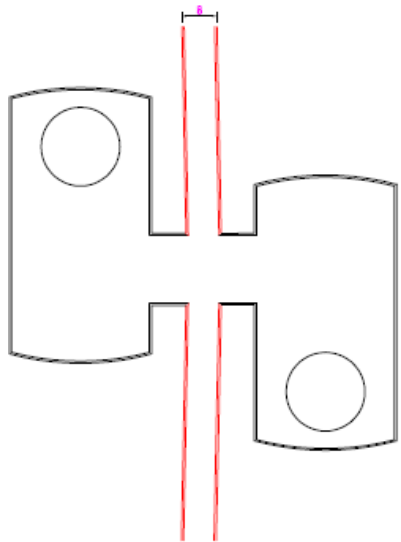
PHASE II - CONSTRUCT PILOT TUNNELS



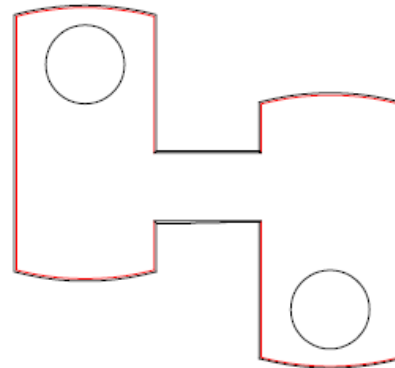
PHASE III - EXCAVATE INTERACTION CAVERN AND
INSTALL TEMPORARY SUPPORT



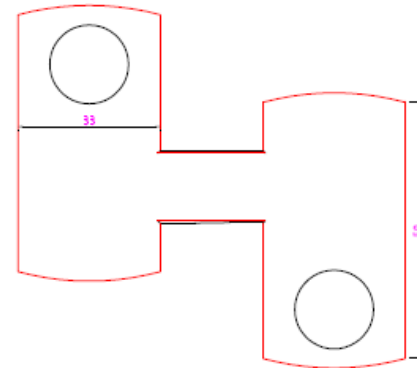
SECTION B-B



PHASE V- CONSTRUCT BEAM TUNNEL



PHASE V- INSTALL PERMANENT SUPPORT
FOR SERVICE CAVERNS



PHASE IV - INSTALL PERMANENT SUPPORT
FOR INTERACTION CAVERN
AND EXCAVATE SERVICE CAVERNS

Ground Model Development

Alison Barmas/ Yung Loo/ Franky Waldron

Outline

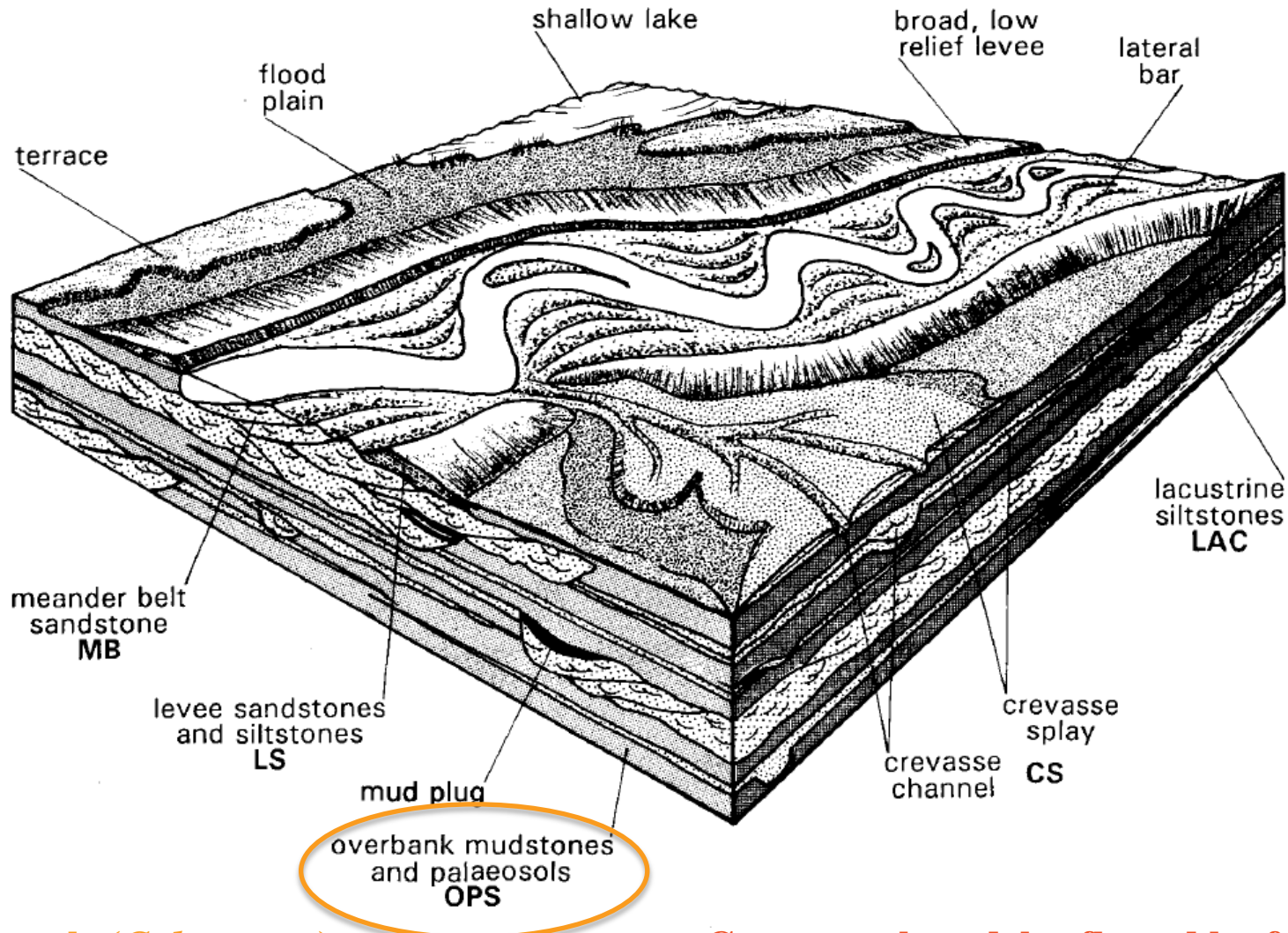
1. Review of new data - Geoconsult Report & GSG Face log data
2. Influence of Geological interpretation to the Cavern Design
3. Geophysical Interpretation using Point 5 data
4. Interpretation of small strain stiffness from P-wave data
5. Recommendations

CMS Point 5 Data Sources

- CERN reports for Point 5 (CMS) including borehole logs, in situ and laboratory testing
- Geoconsult (May 2003) Geological Factual Report and shaft and face logging
- Published geotechnical literature for the correlation of down hole geophysics in Sedimentary basin deposits
- DataPlot and RockWorks15 for 3D modelling of the available geophysics data

Depositional Environment

Lateral and vertical variability

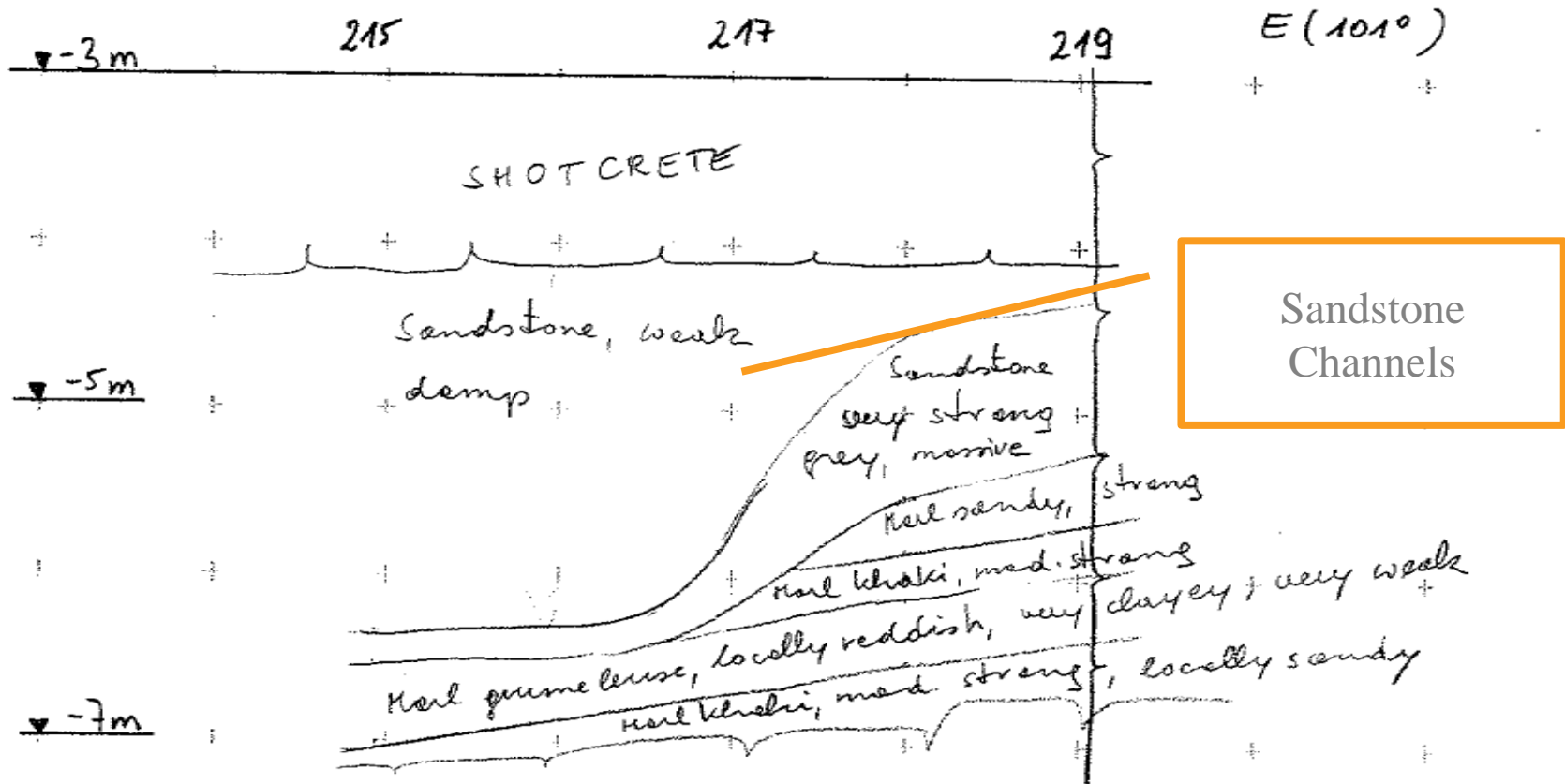


**Paleosols (*Calcareous*)
Potential Marker beds**

Conceptual model reflected by face logging

Confirmation of Depositional Features

- Examples from Point 5 GSG Face logs

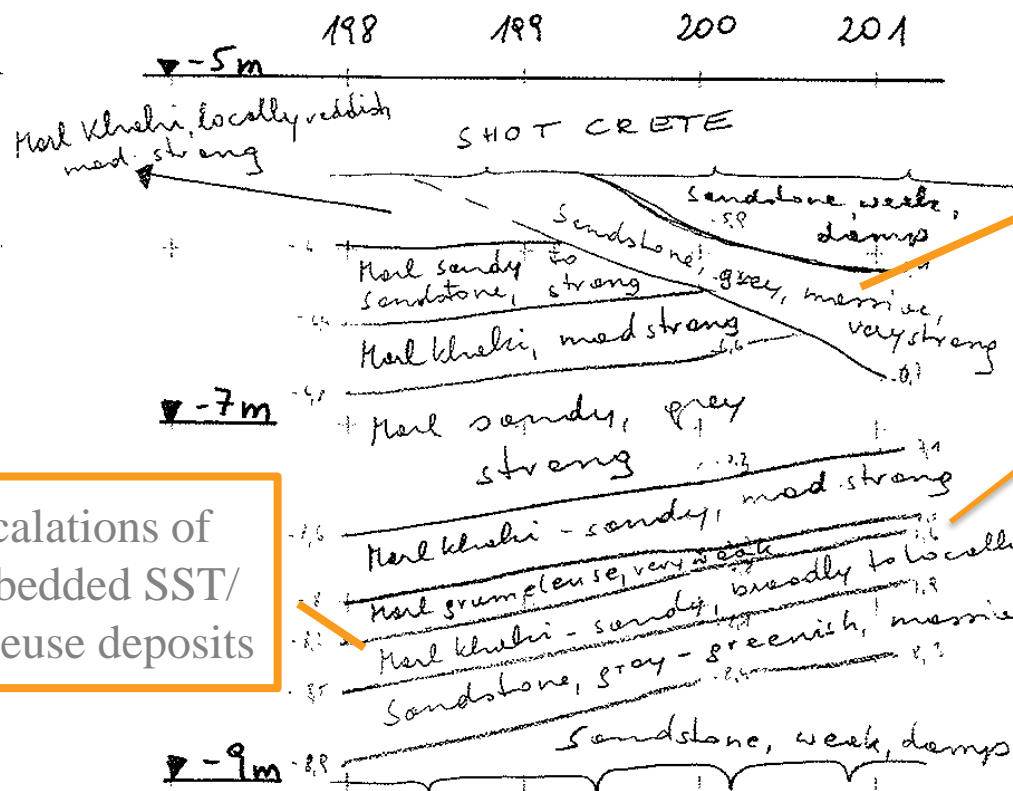


Pillar Ch. 215 – 219m

Confirmation of Depositional Features

- Examples from Point 5 GSG Face logs

E(101°)

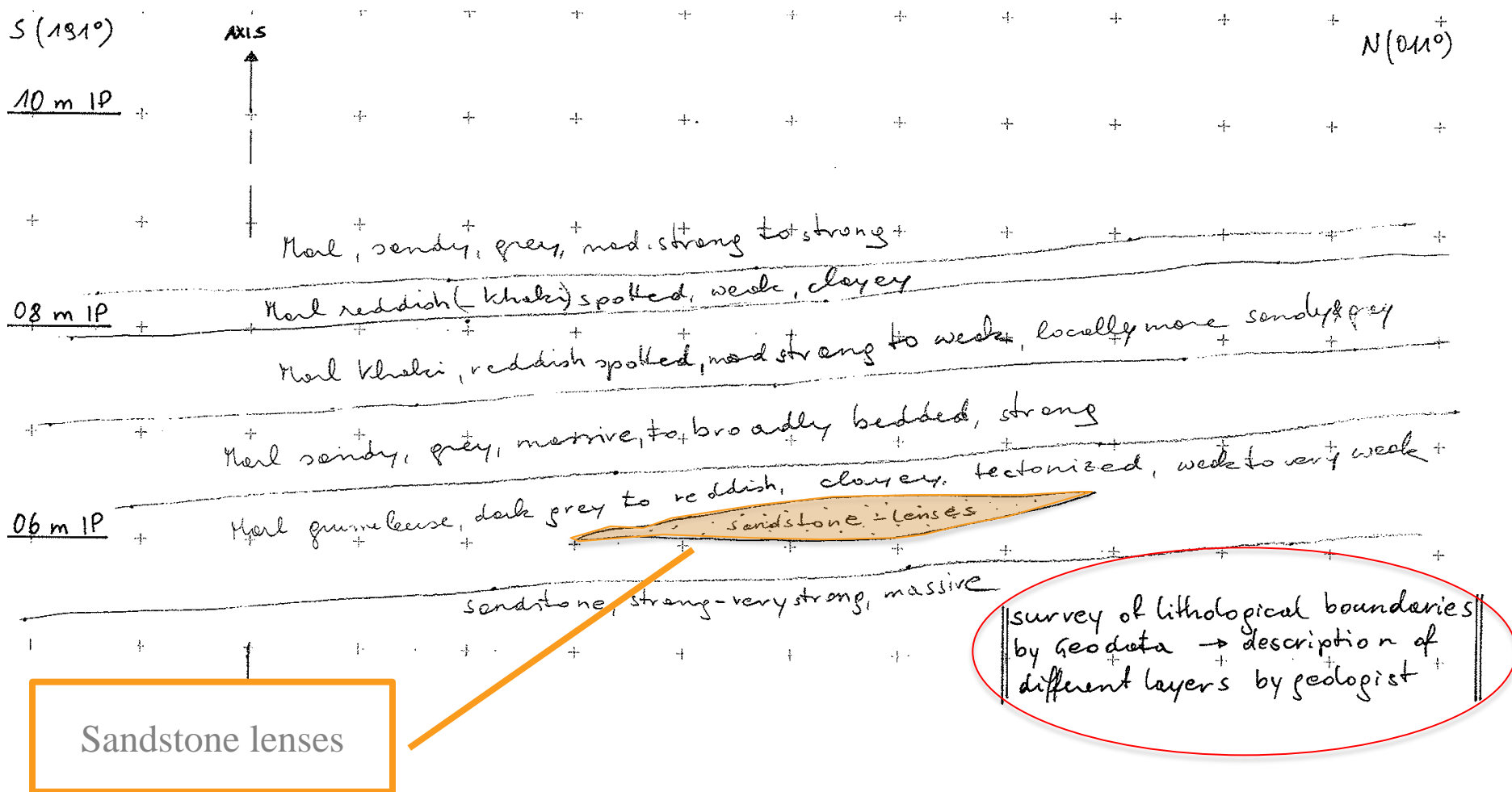


Variable Dip of bedding & Cross-bedding

Intercalations of thinly bedded SST/ Grumleuse deposits

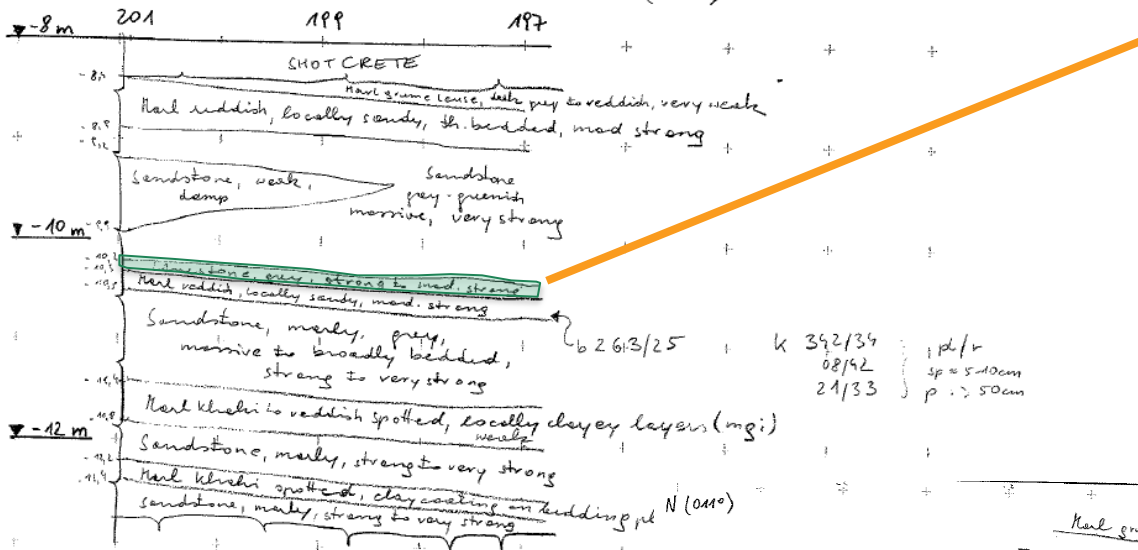
Pillar Ch. 198-201m

UCX 55 West Head Wall - Chainage 170.5 – 172.5

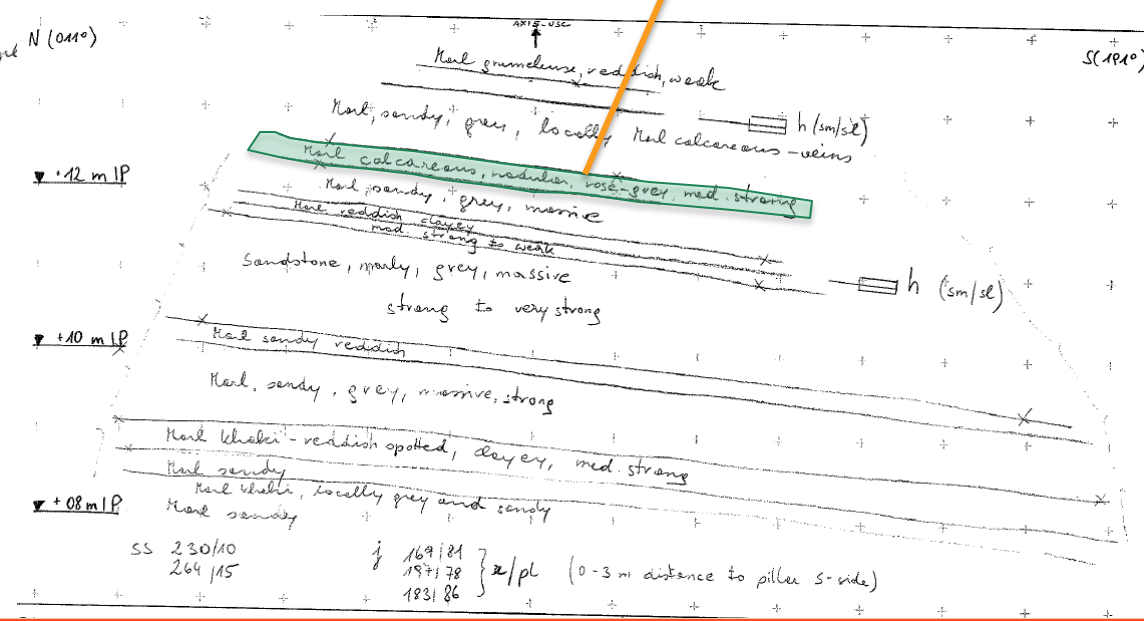


Confirmation of Depositional Features

E (101°) **Pillar Ch. 187-201m** W (281°)



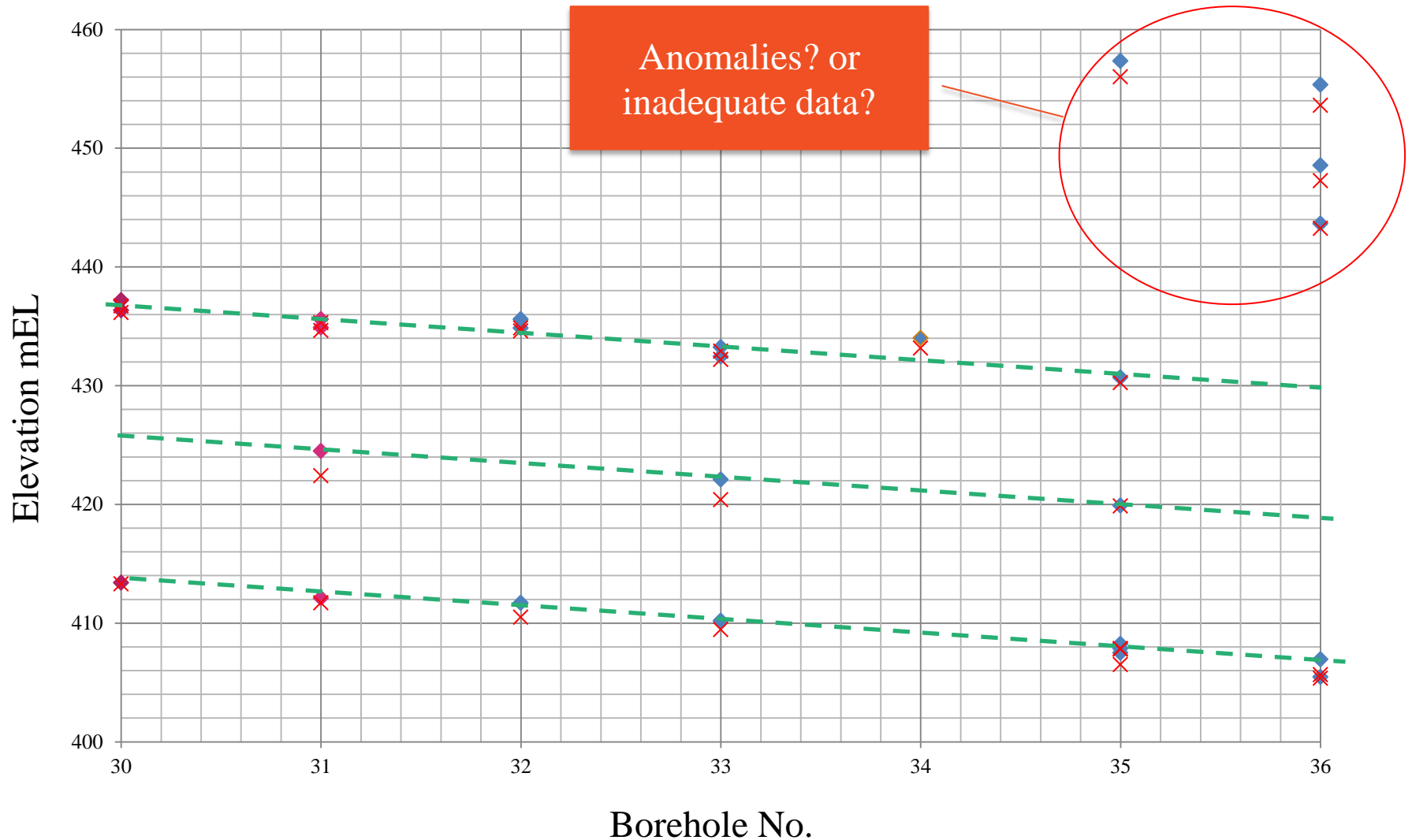
Calcareous Horizons/
Paleosol development



USC 55 Ch. 197.51m

Calcareous & “Limestone” from Point 5 BH data

Data shows an approximation of the top and base of calcareous horizons from BH descriptions



Geoconsult Report and Face mapping

Key Comments:

- Allocation of strength parameters to the stratigraphical layers is **different from predictions**
- Rock mass has a pronounced **Time dependent behaviour**

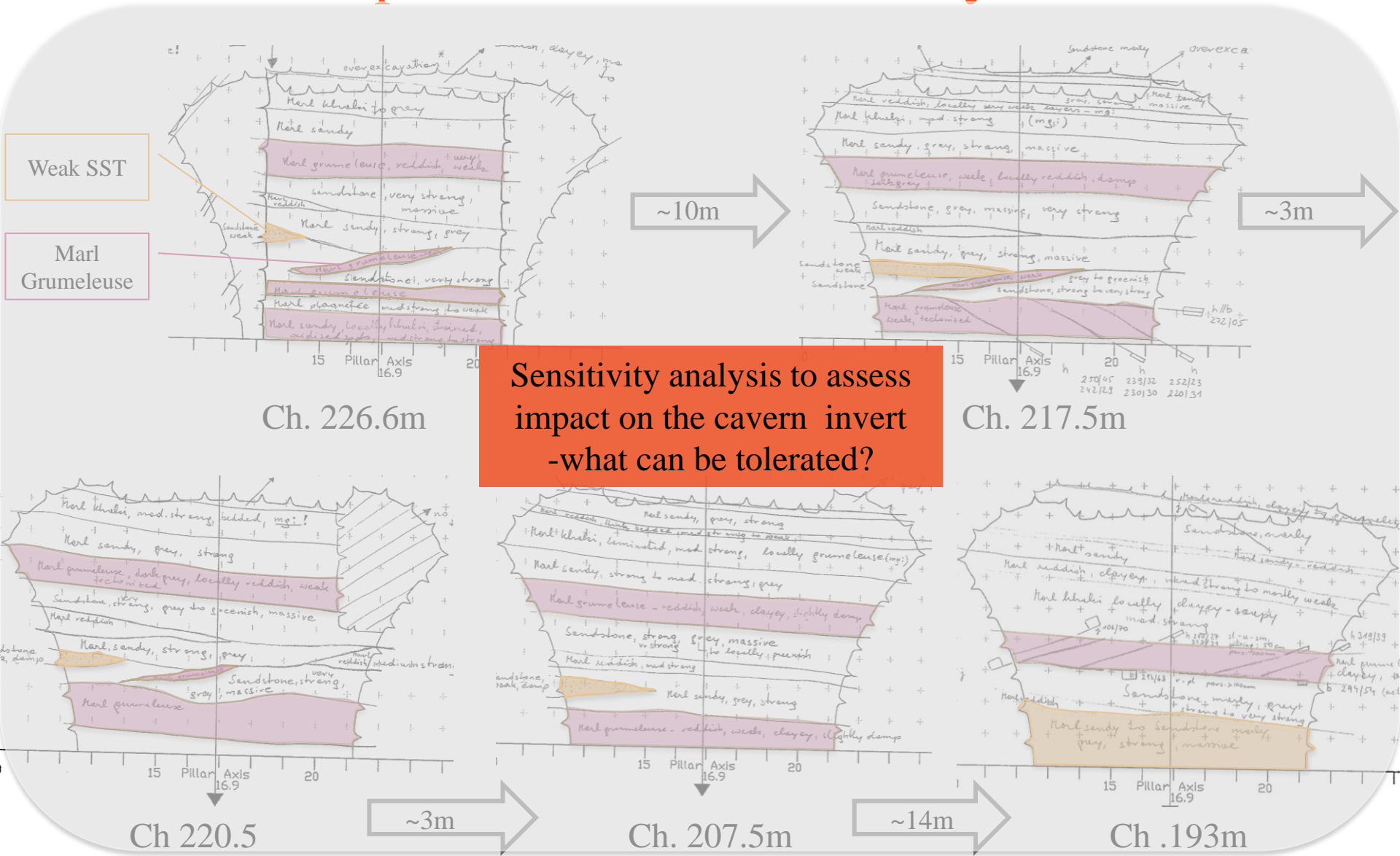
Geoconsult Report and Face mapping

Details:

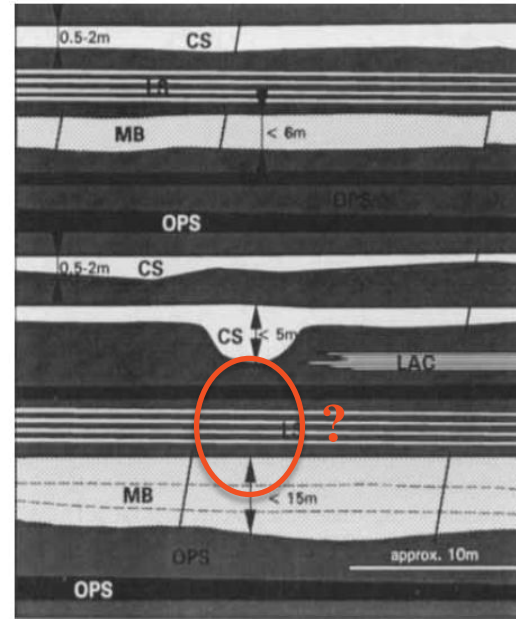
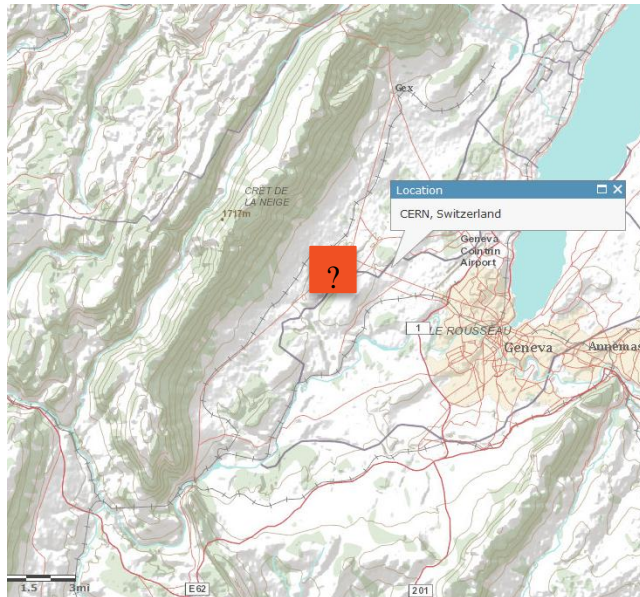
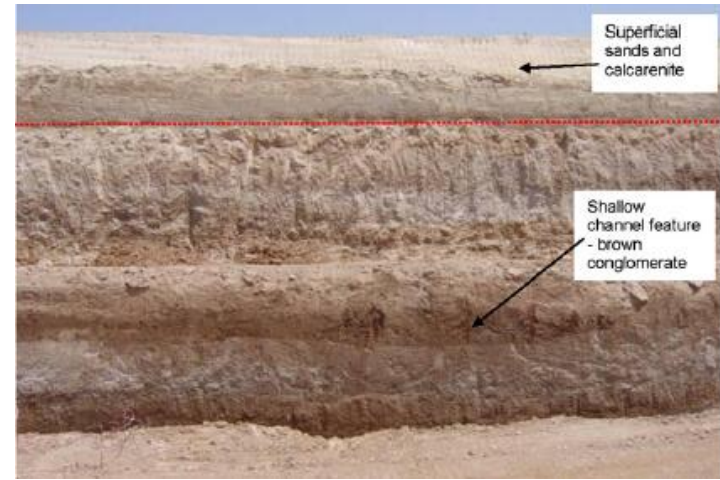
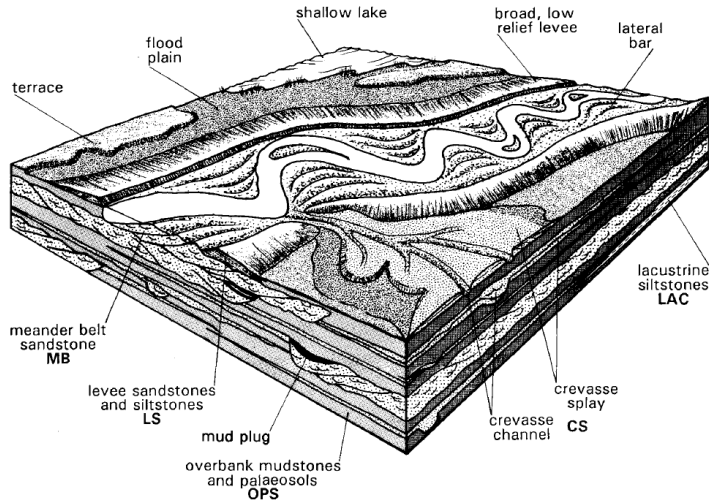
1. Detailed geological mapping from excavations shows the encountered **strength parameters differ** from borehole predictions.
2. Rock mass **less competent** than predicted
3. Anticipated SST layers were not the expected quality & actually marly SST/ sandy MARL (**questions the reliability of borehole logs to verify geophysics**).
4. Anticipated SST **encountered as lenses** not as persistent layer
(**as we predicted in CSM from depositional environment**)
5. Marl Grumeleuse layers in sidewalls were thicker than anticipated and poorer quality

How does this affect the approach to the design?

Pillar Example of Lateral Variability over ~35m

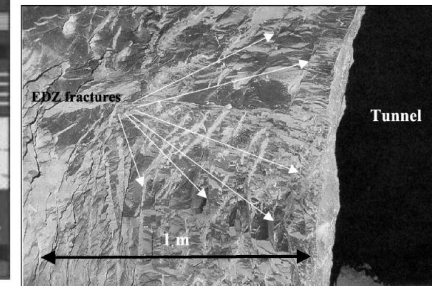


Cavern design approach must account for Scale



Optimise depth & invert conditions

Target the detail!



Geological Interpretation with scale

Regional

- Large scale understand the Depositional Environment
- Predict behaviour, sedimentary structure and variability
- Model affects of large scale variability in terms of the affect on cavern feasibility

Local

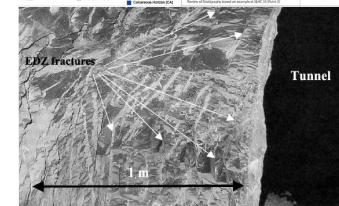
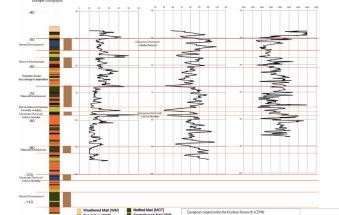
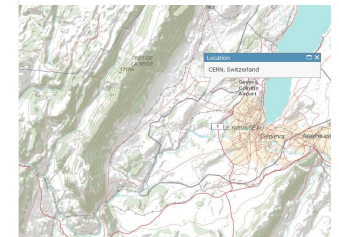
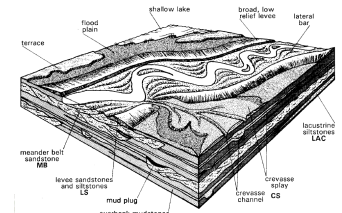
- Develop Conceptual Model from existing Site Data/ Plan Site Selection
- Favourable stress orientation for caverns
- Set-up 3D Conceptual model (Elevation data, existing information for planning SI)

Site Specific

- Characterisation of stratigraphy and Engineering parameters from detailed investigation using a suite of boreholes, in-situ and laboratory testing and monitoring.
- Development of 3D Conceptual model to include all new data sets

Micro

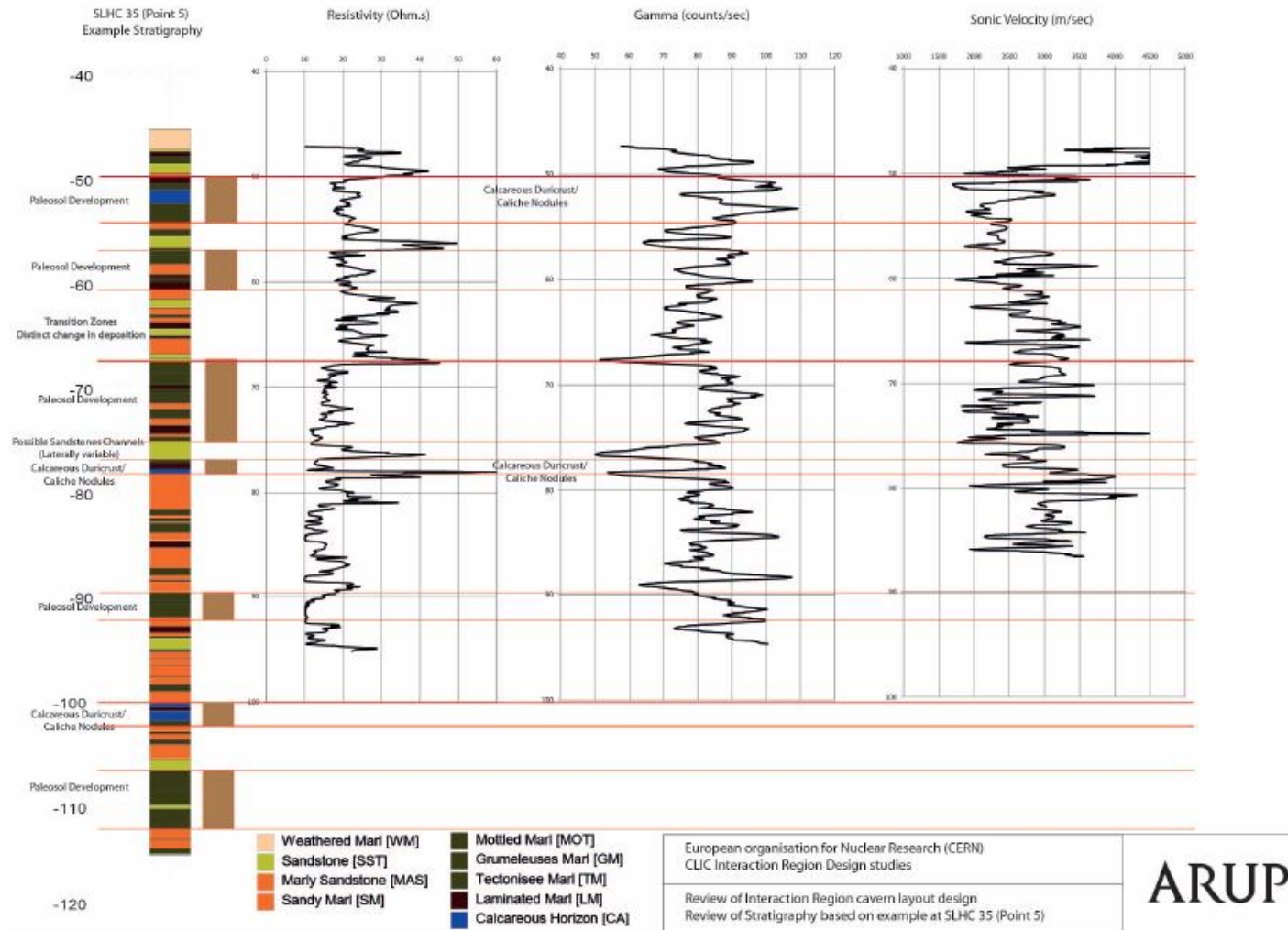
- Optimisation of depth and invert conditions based on interpretation and influence of mineralogy/ sedimentary structure/ lithofacies models and predicted behaviour
- **Target the detail!**



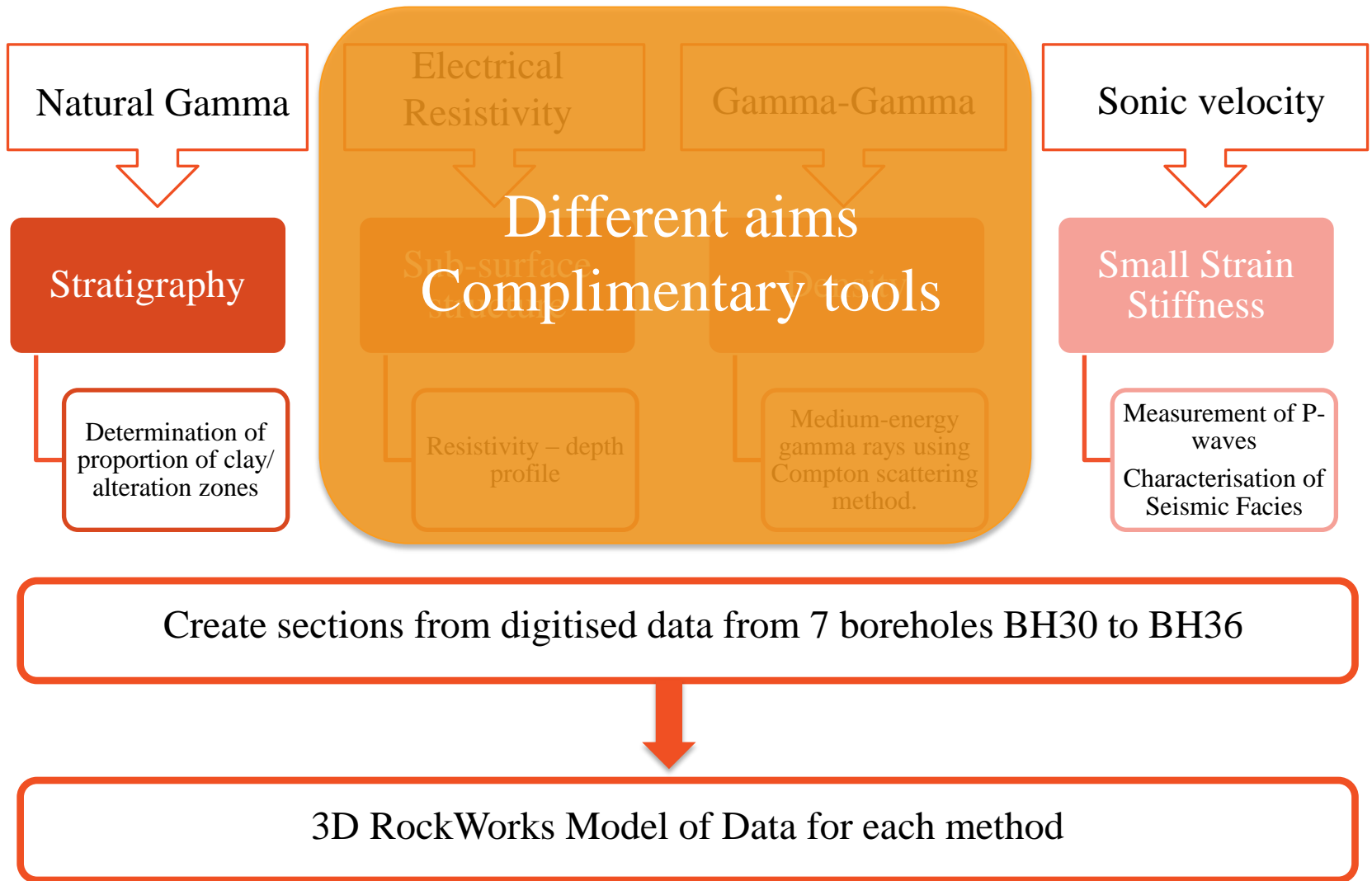
.. verification during excavation!

Geophysical Interpretation


Initial approach to geophysics in July ...

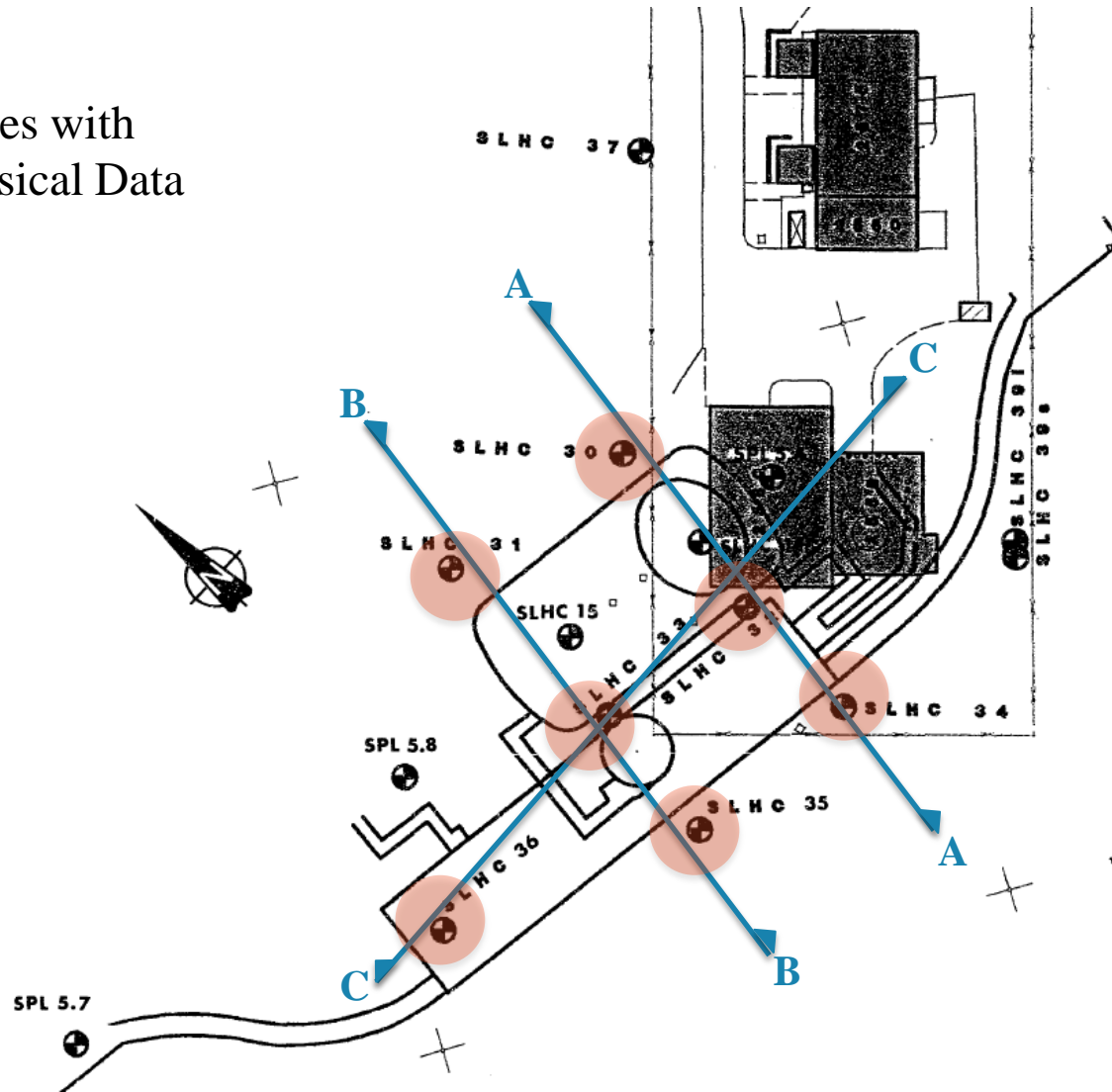


Geophysical Interpretation at CMS Point 5



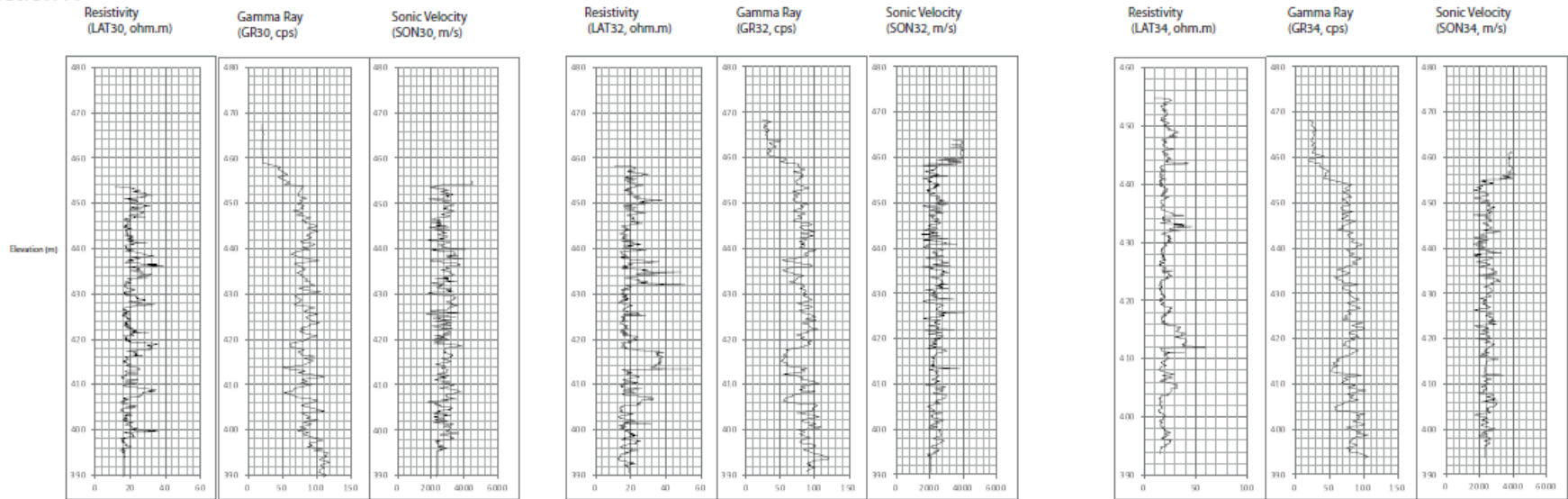
Plan of Point 5 BHs showing analysis sections

 Boreholes with Geophysical Data

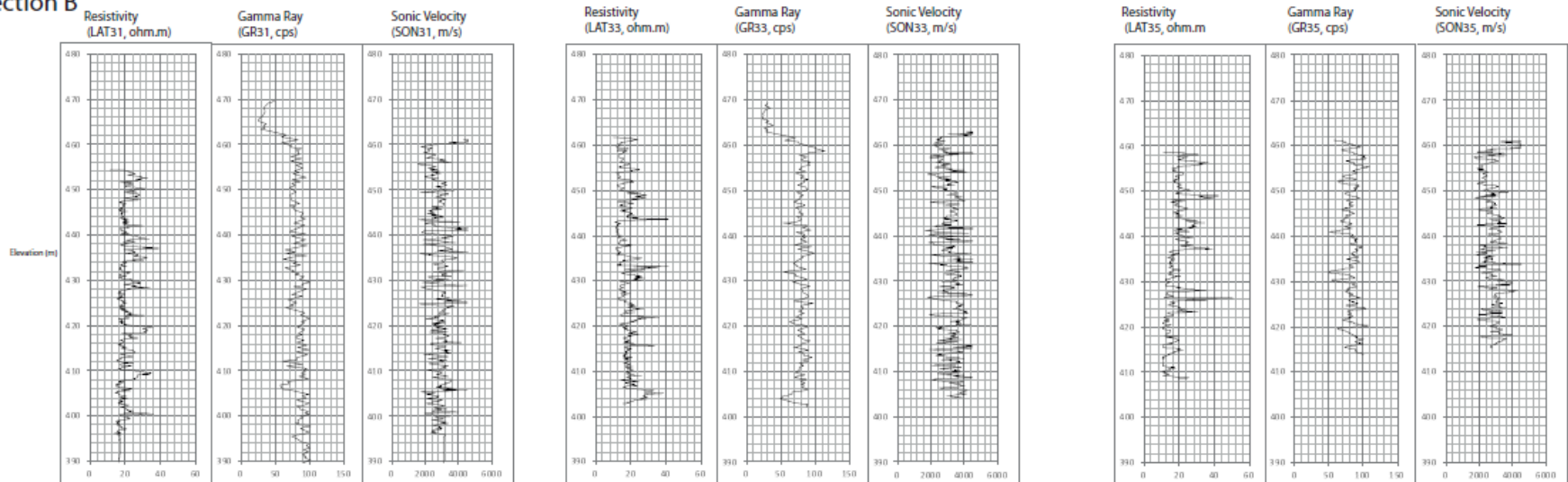


Geophysical Data for Point 5 A-A & B-B

Section A

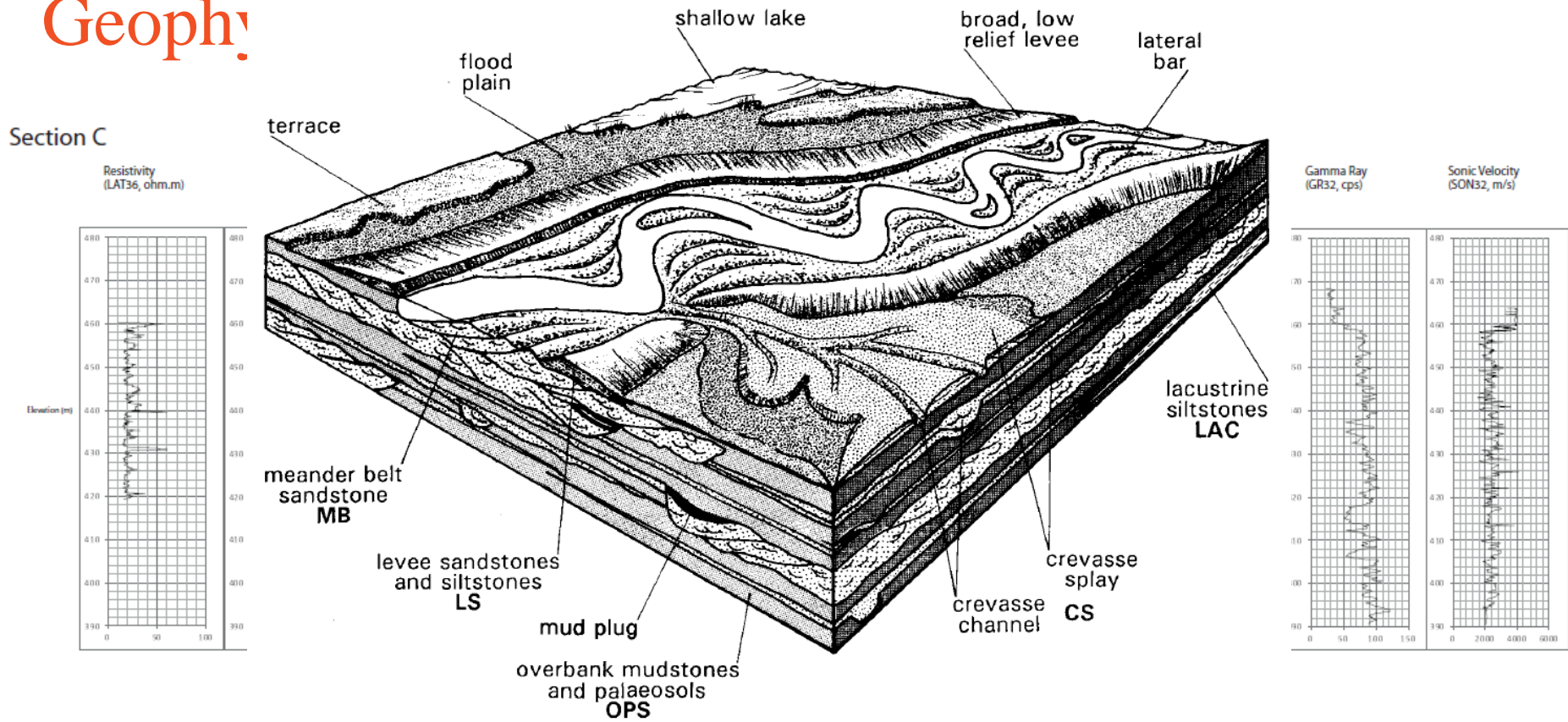


Section B



Geophy

Section C

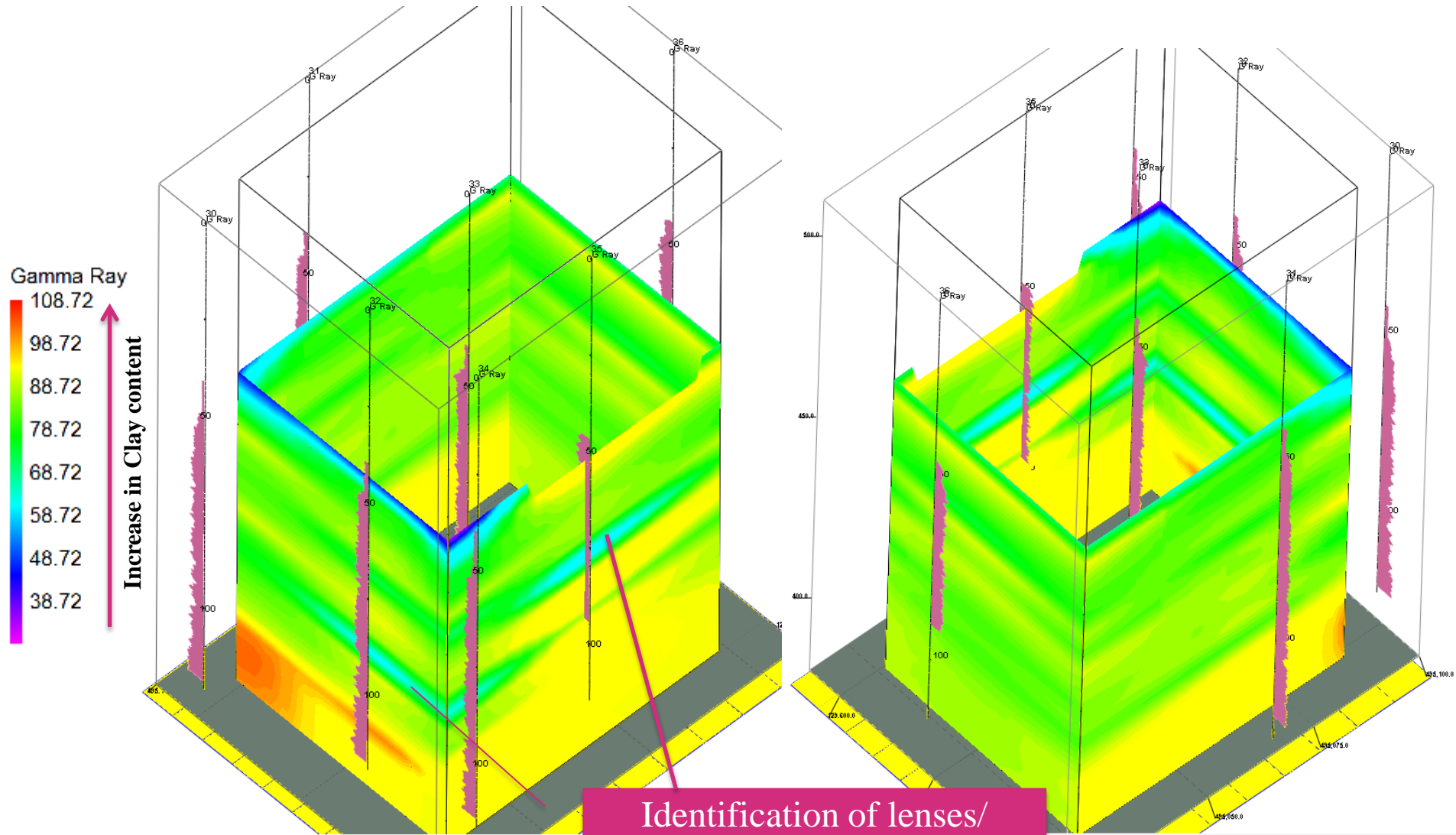


Difficult to visualise variations

Natural Gamma in Rockworks

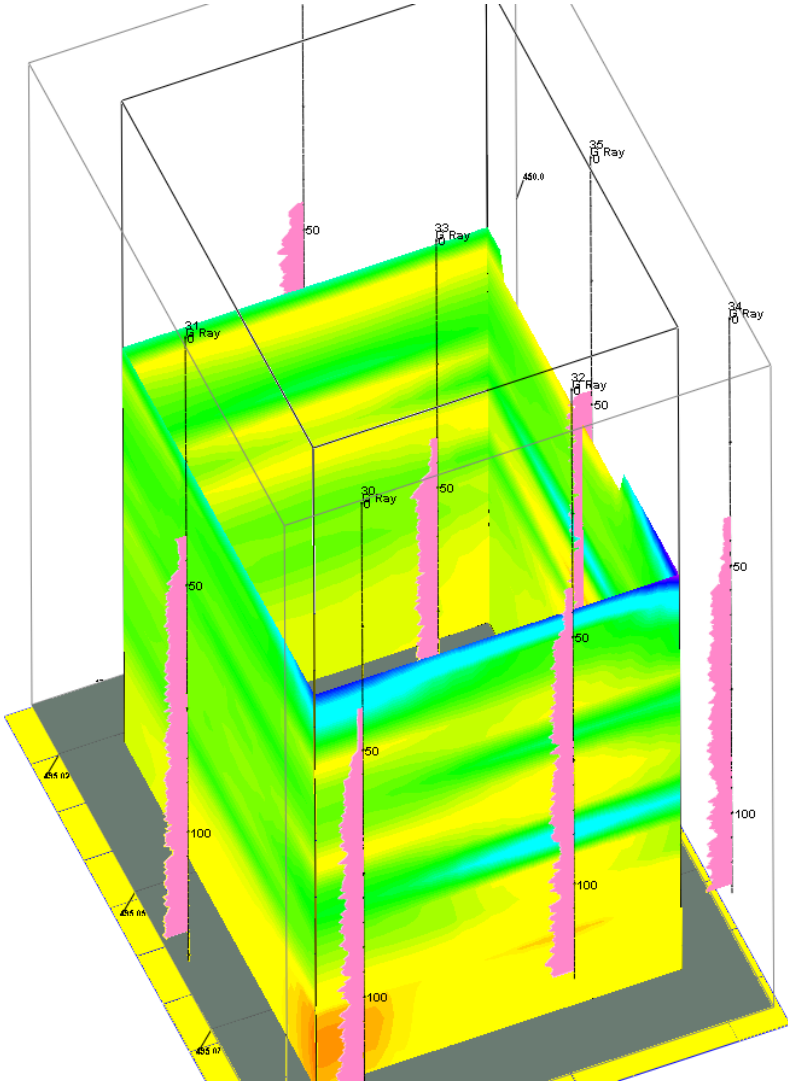
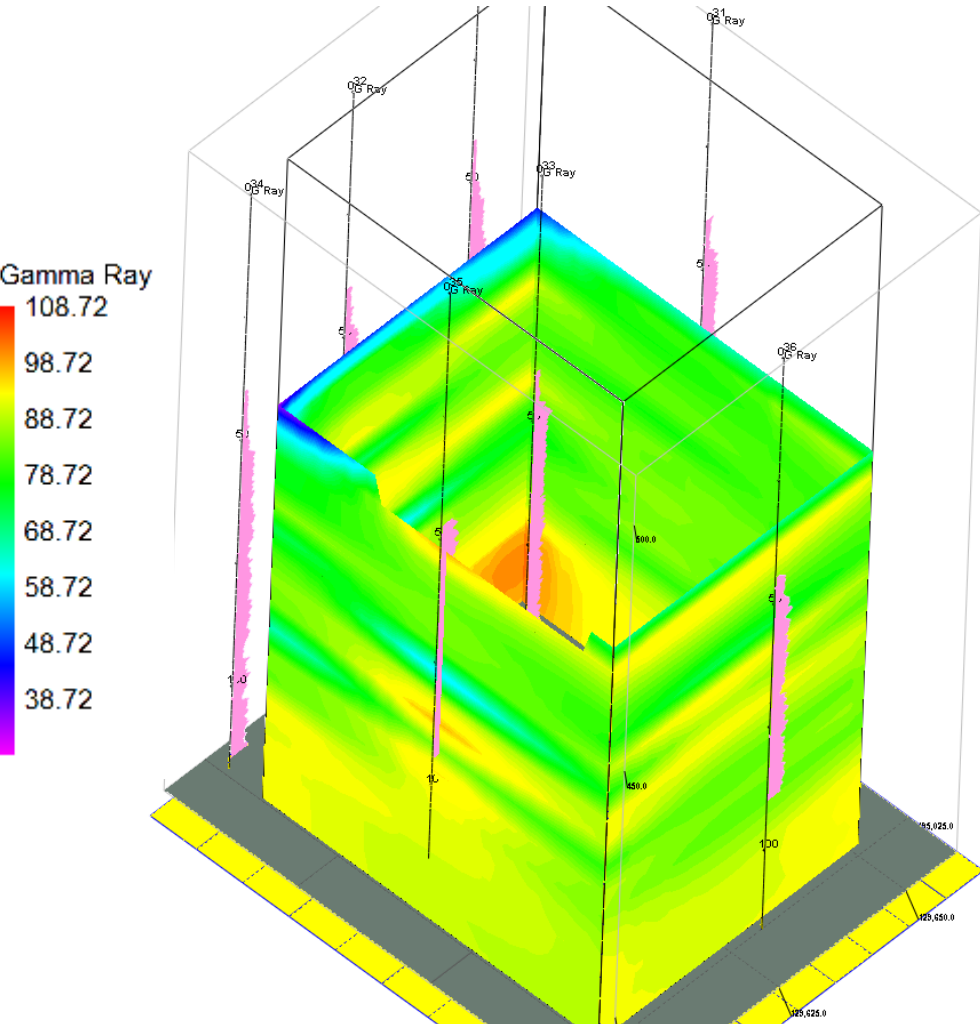
Evaluate stratigraphy

Natural Gamma model slides



Identification of lenses/
bedding structure

Natural Gamma model slides



Limitations

- Quality of data

(correlations/ digitizing)

- Amount of Data (no. Of BHs)

accuracy of interpolation between boreholes / edge effects/
change in detail of results/ incorporate cross hole data in future

- Persistence of horizons

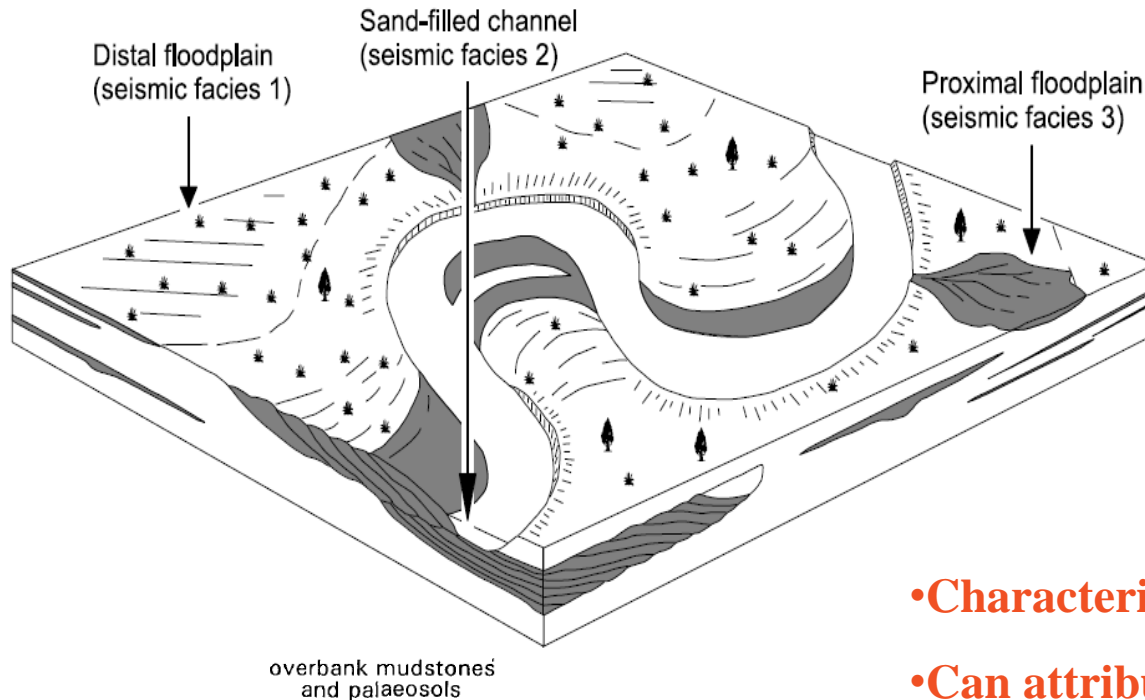
lack of confidence in BH descriptions

BUT it can be achieved ...

Sonic Logging in RockWorks

P-wave output to determine seismic facies

Seismic Facies



Example in Lower Freshwater Molasse From Morend, Pugin and Gorin (1998)

- Seismic facies 1: poorly reflective, low amplitude, discontinuous reflections;
- Seismic facies 2: fairly reflective, high amplitude, continuous reflections;
- Seismic facies 3: highly reflective, high amplitude, moderately continuous reflections.

- **Characterise facies based on reflection**
- **Can attribute small strain stiffness to seismic facies models using P-wave correlations**
- **Add stratigraphy model from natural Gamma, Resistivity and Boreholes**

Seismic Limitations

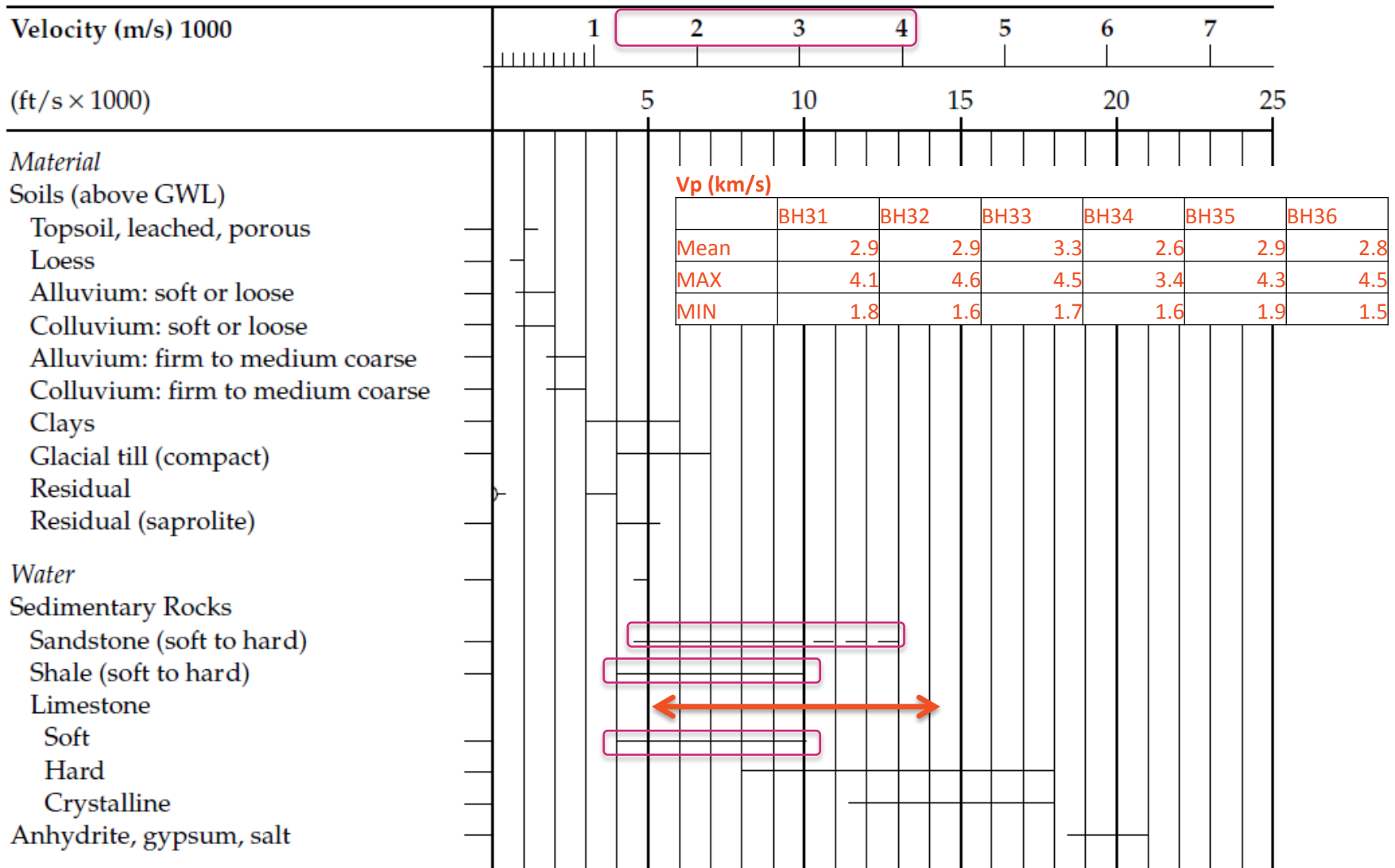
- Intercalated/ thinly bedded deposits can be difficult to pick up using V_p depending on **resolution of data**

Seismic resolution often thinner than bedding thickness/
lithological change

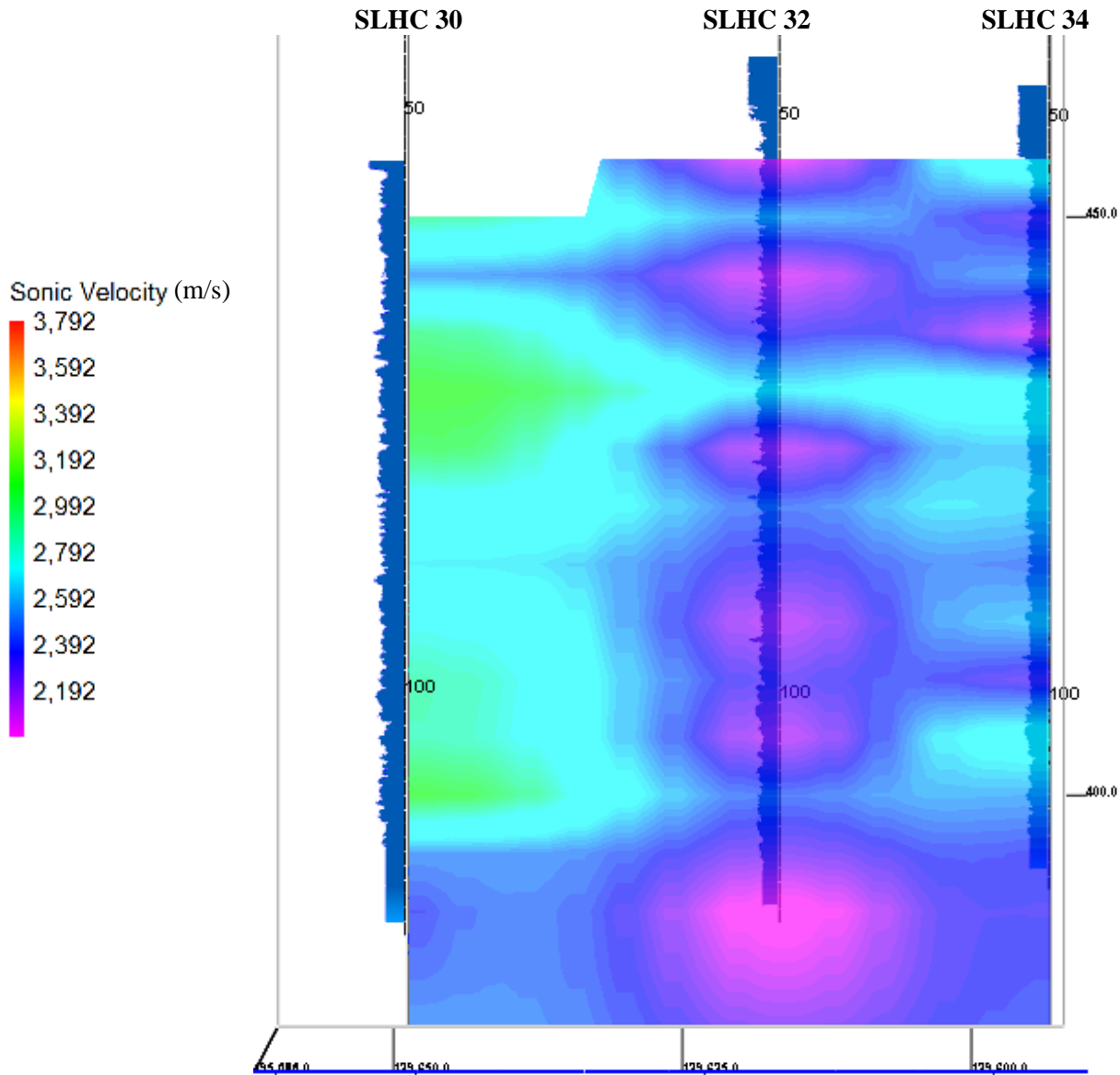
- Limited ability to **develop ‘signature’ values** for each lithology materials can vary within the same range hence adoption of a statistical mean for development of parameters at this stage.

Typical P-Wave Velocities

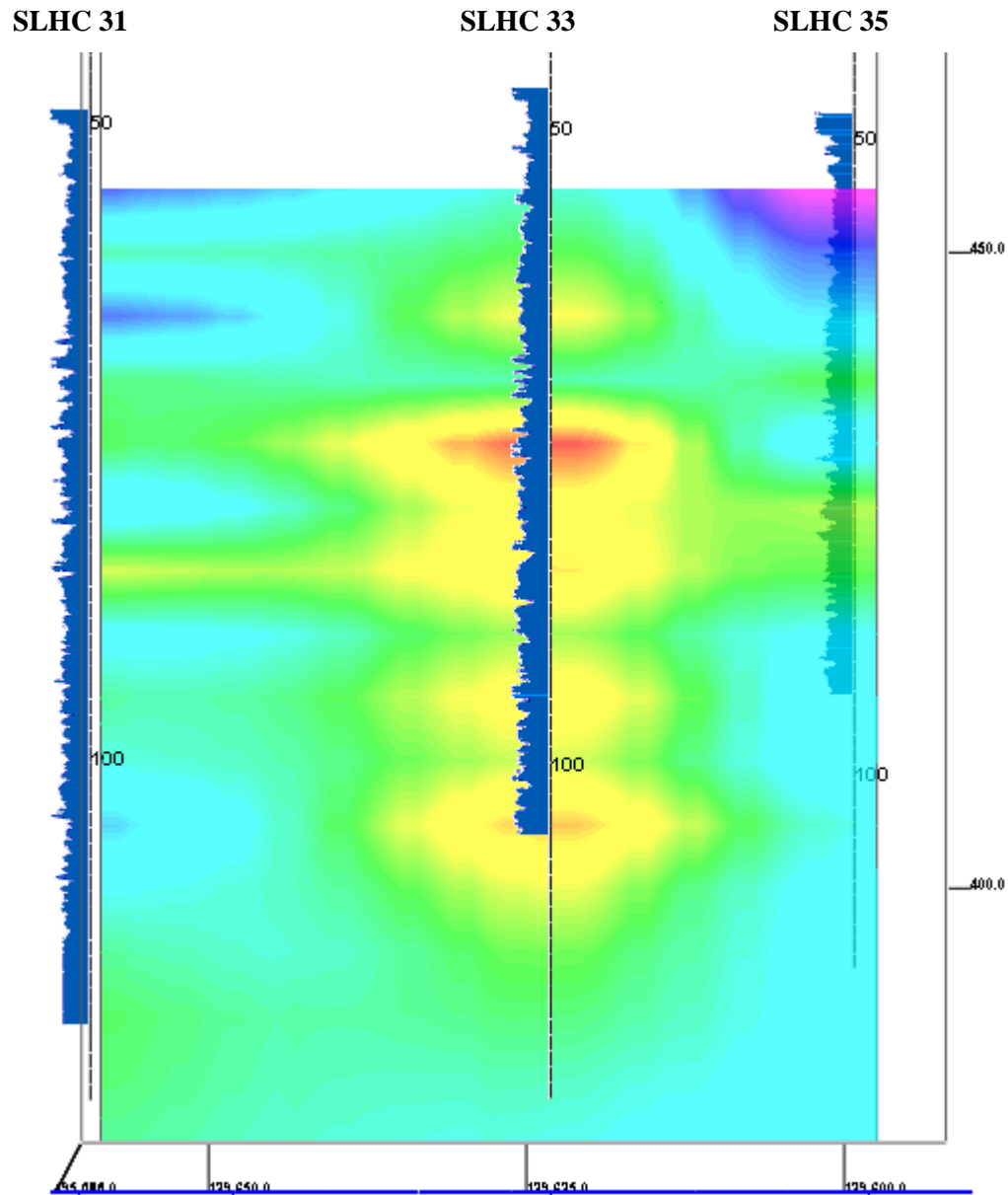
Typical Compression-Wave Velocities in Soils and Rocks



Sonic Velocity – Section A



Sonic Velocity – Section B



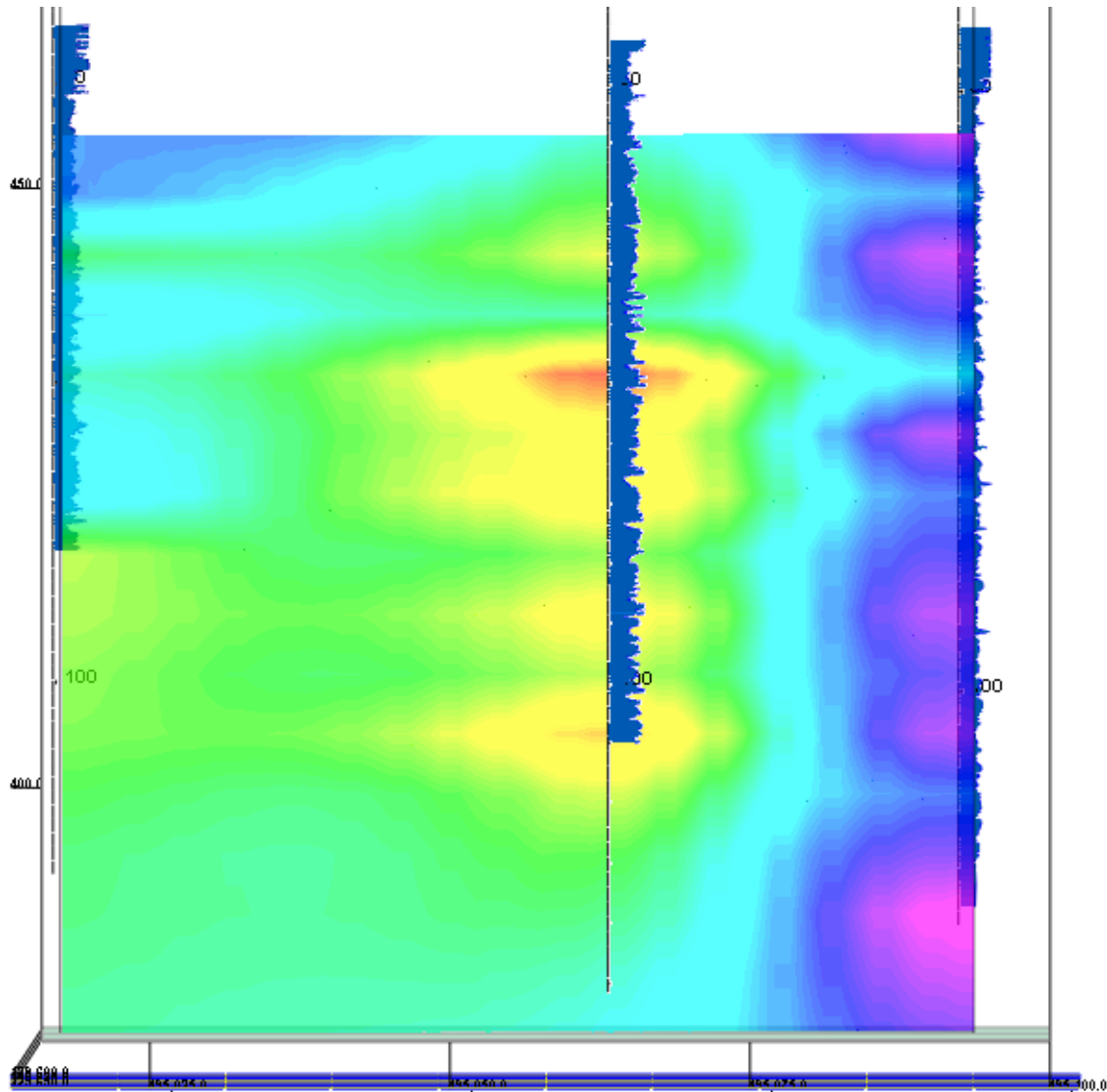
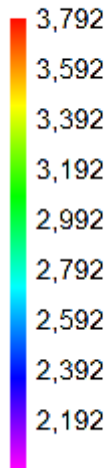
Sonic Velocity – Section C

SLHC 36

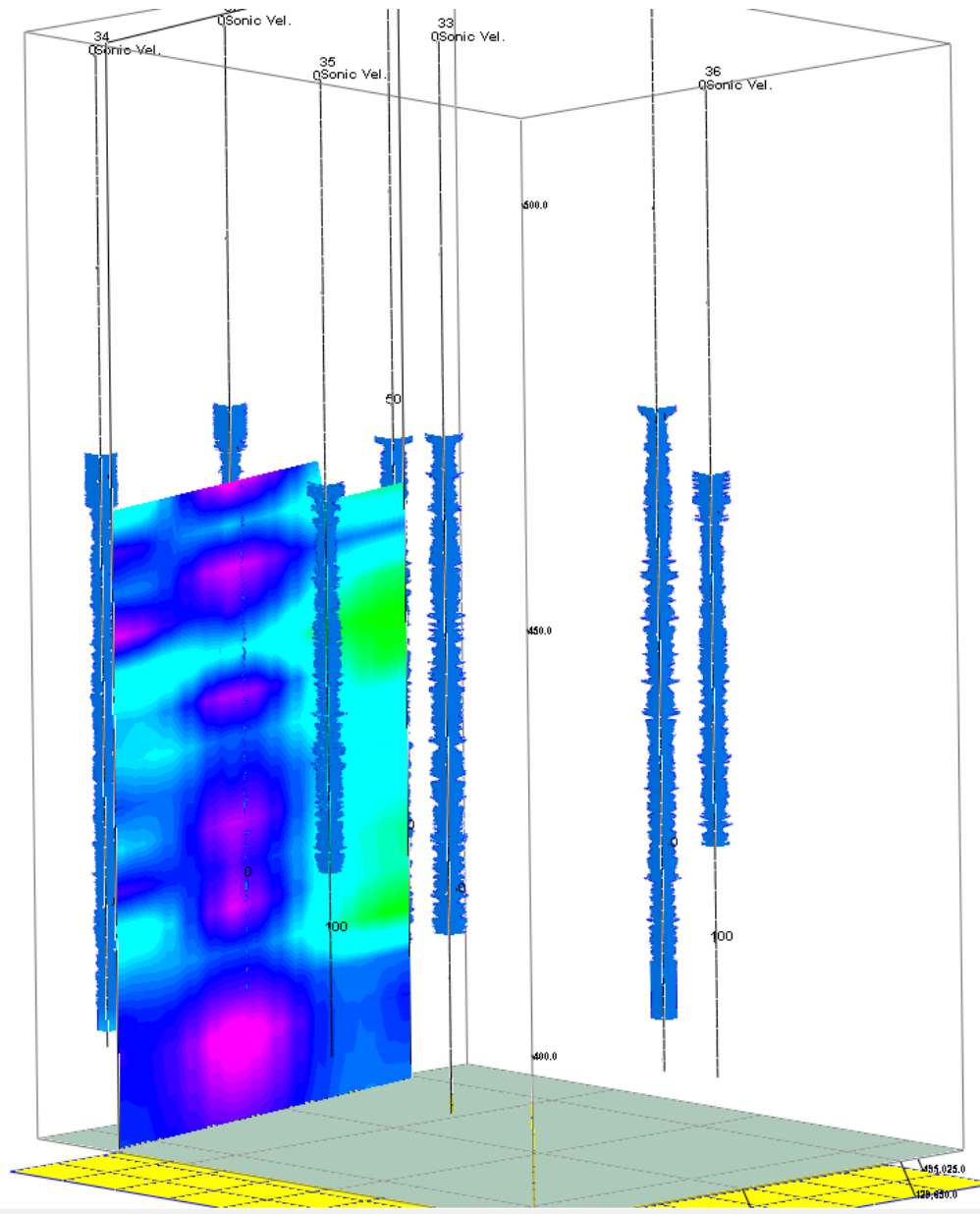
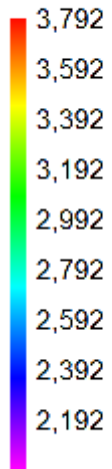
SLHC 33

SLHC 32

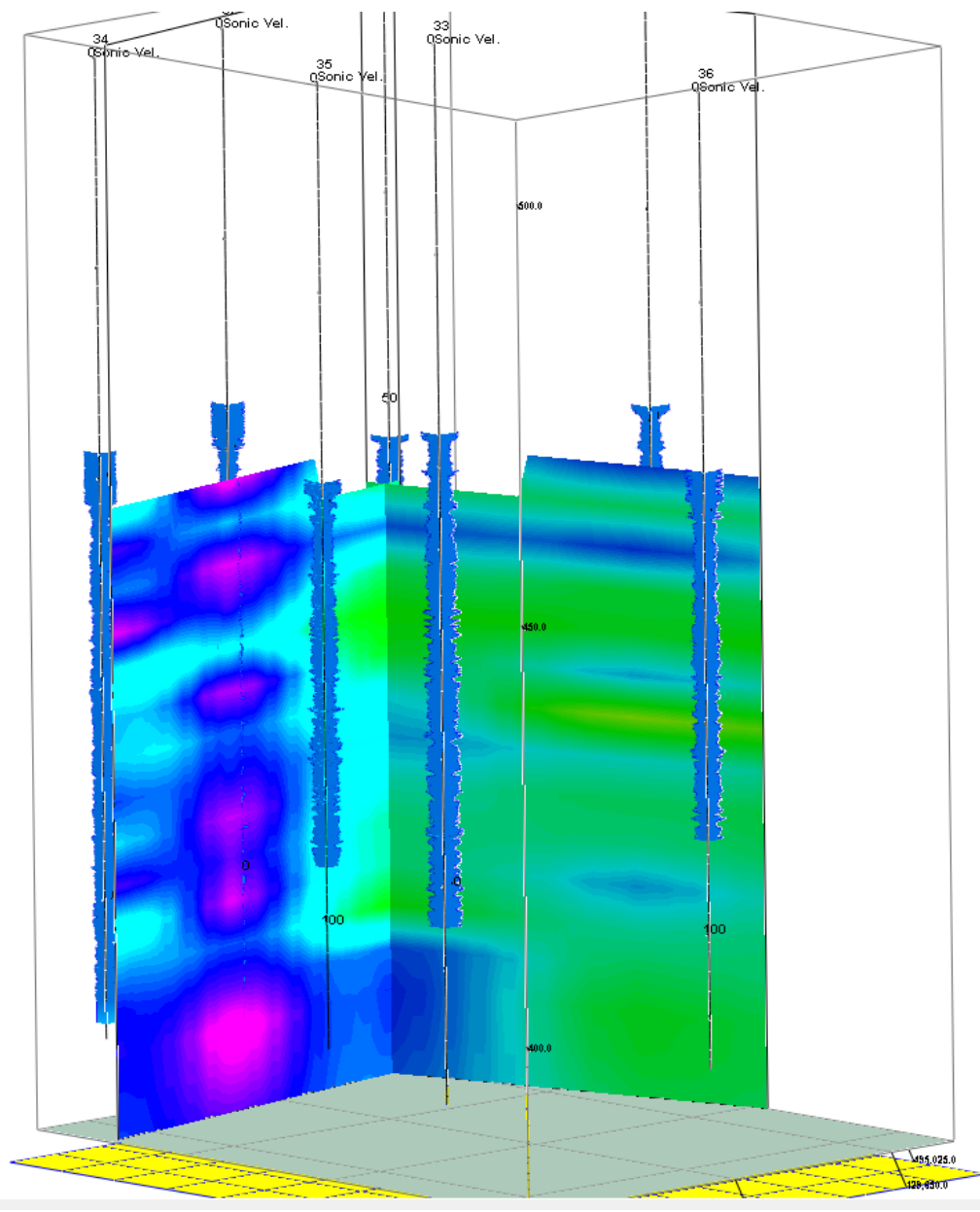
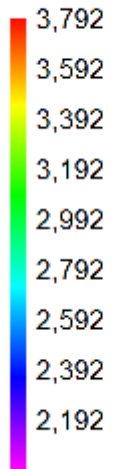
Sonic Velocity (m/s)



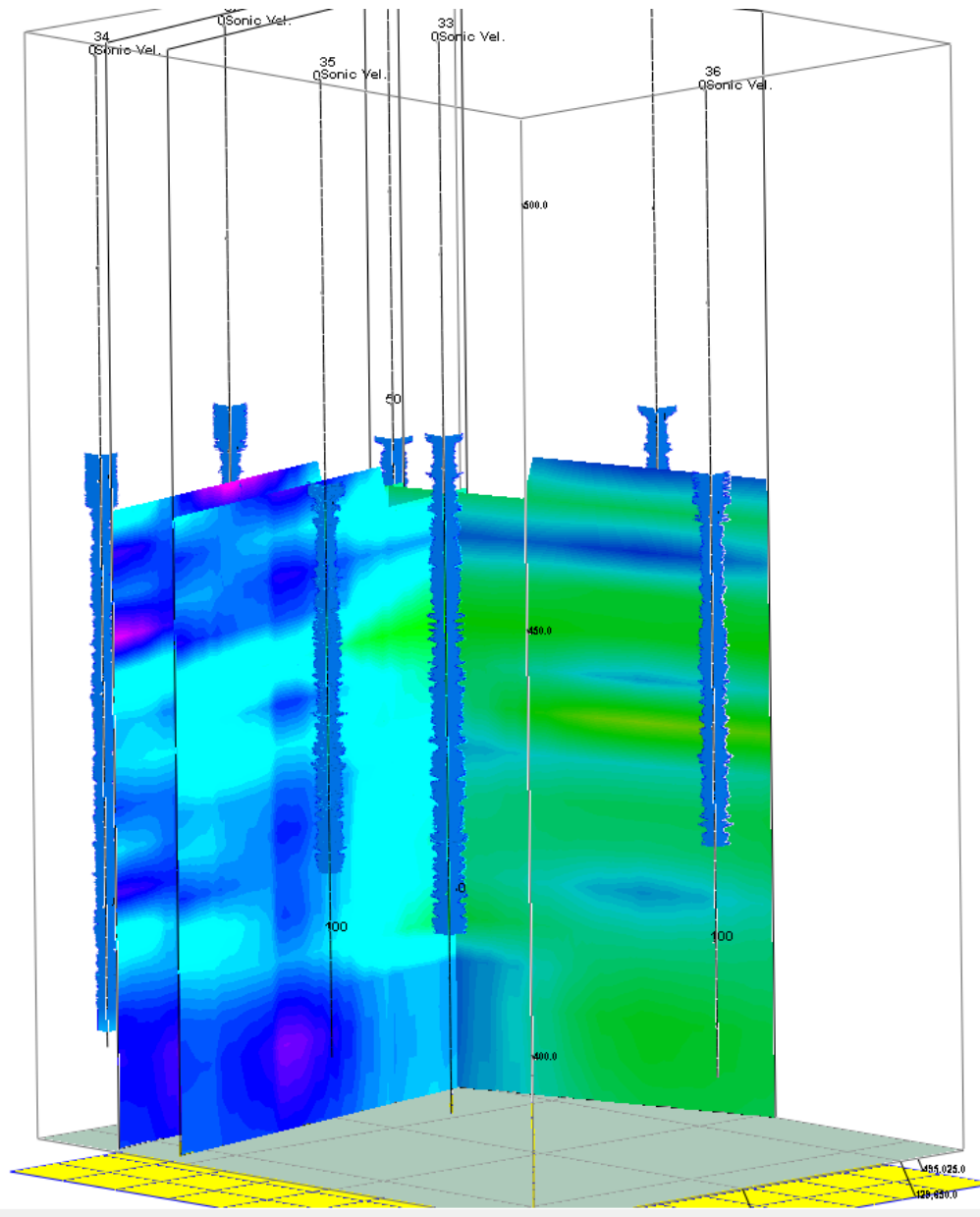
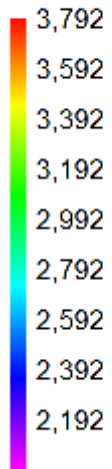
Sonic Velocity (m/s)



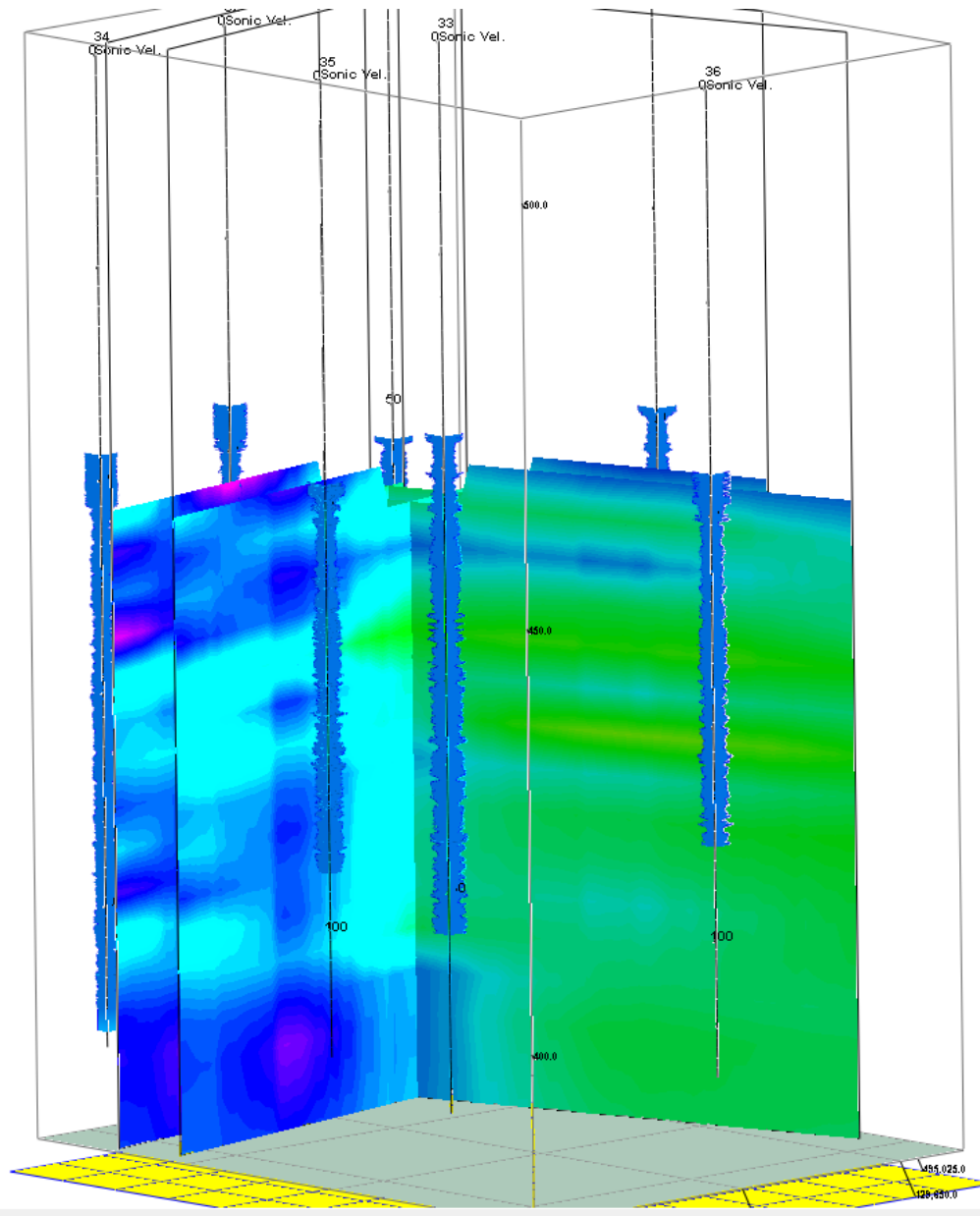
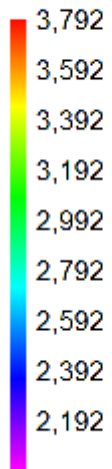
Sonic Velocity (m/s)



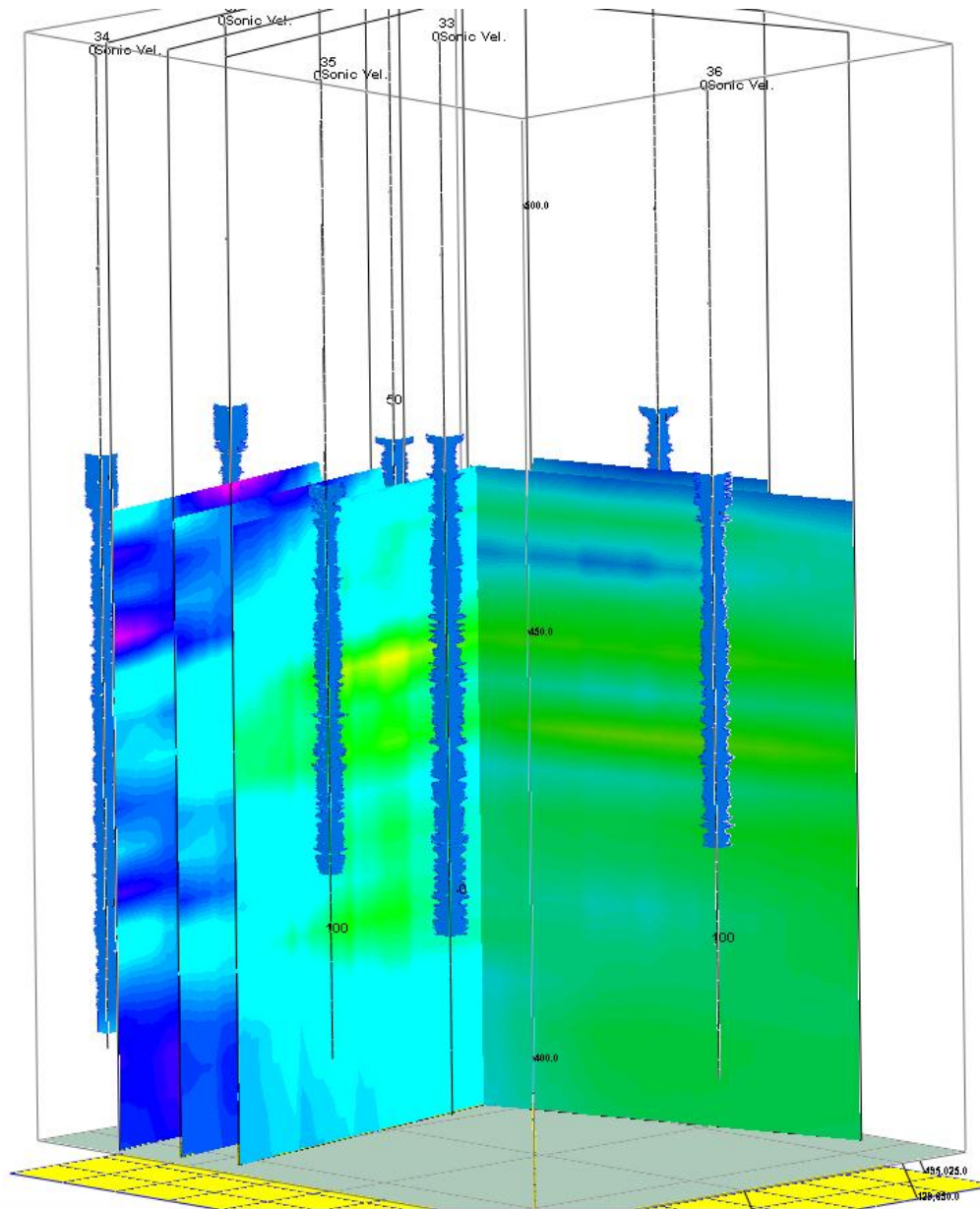
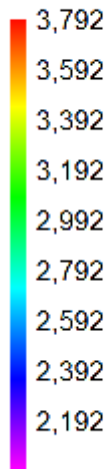
Sonic Velocity (m/s)



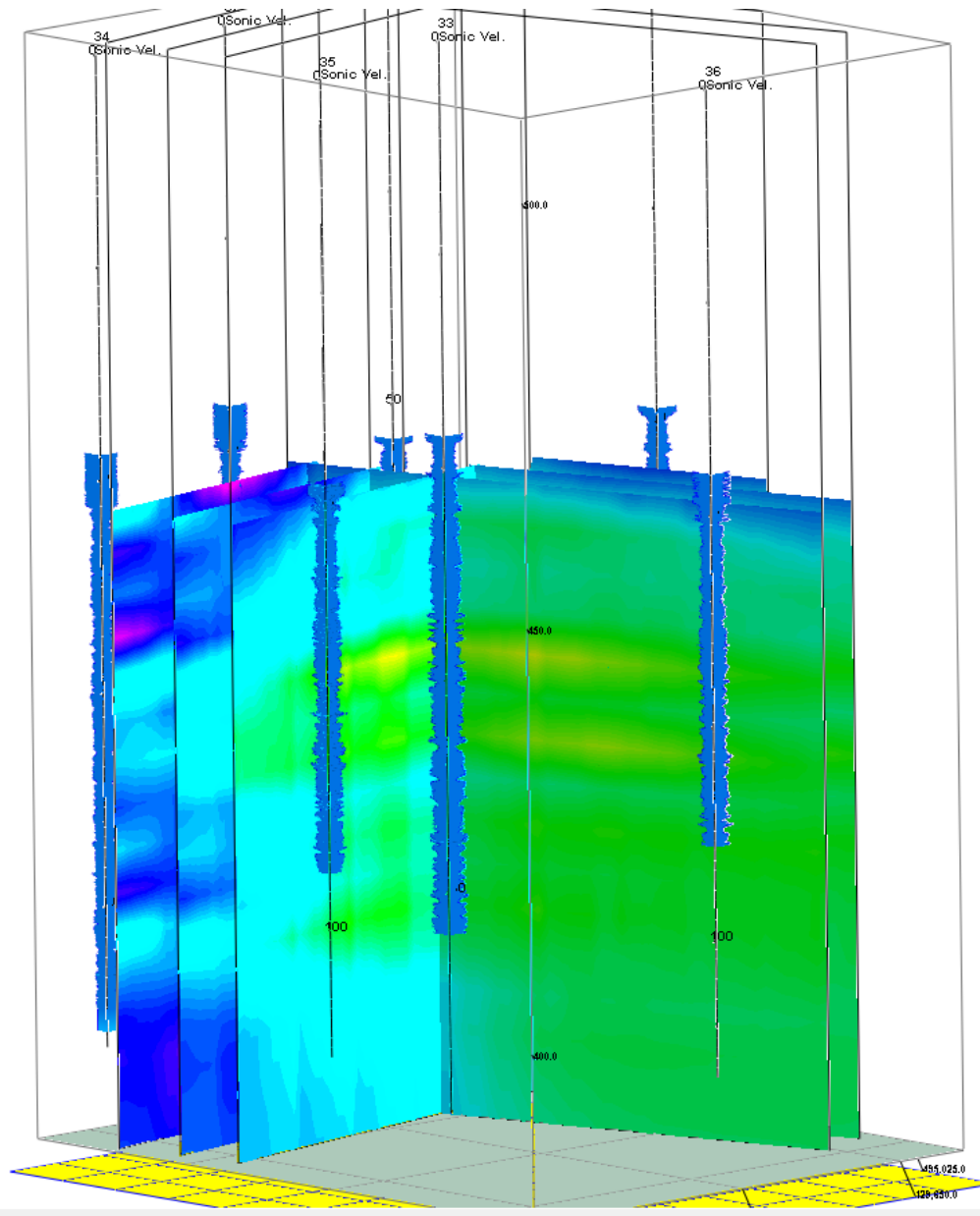
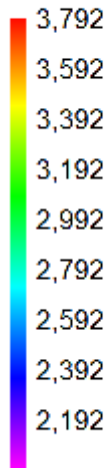
Sonic Velocity (m/s)



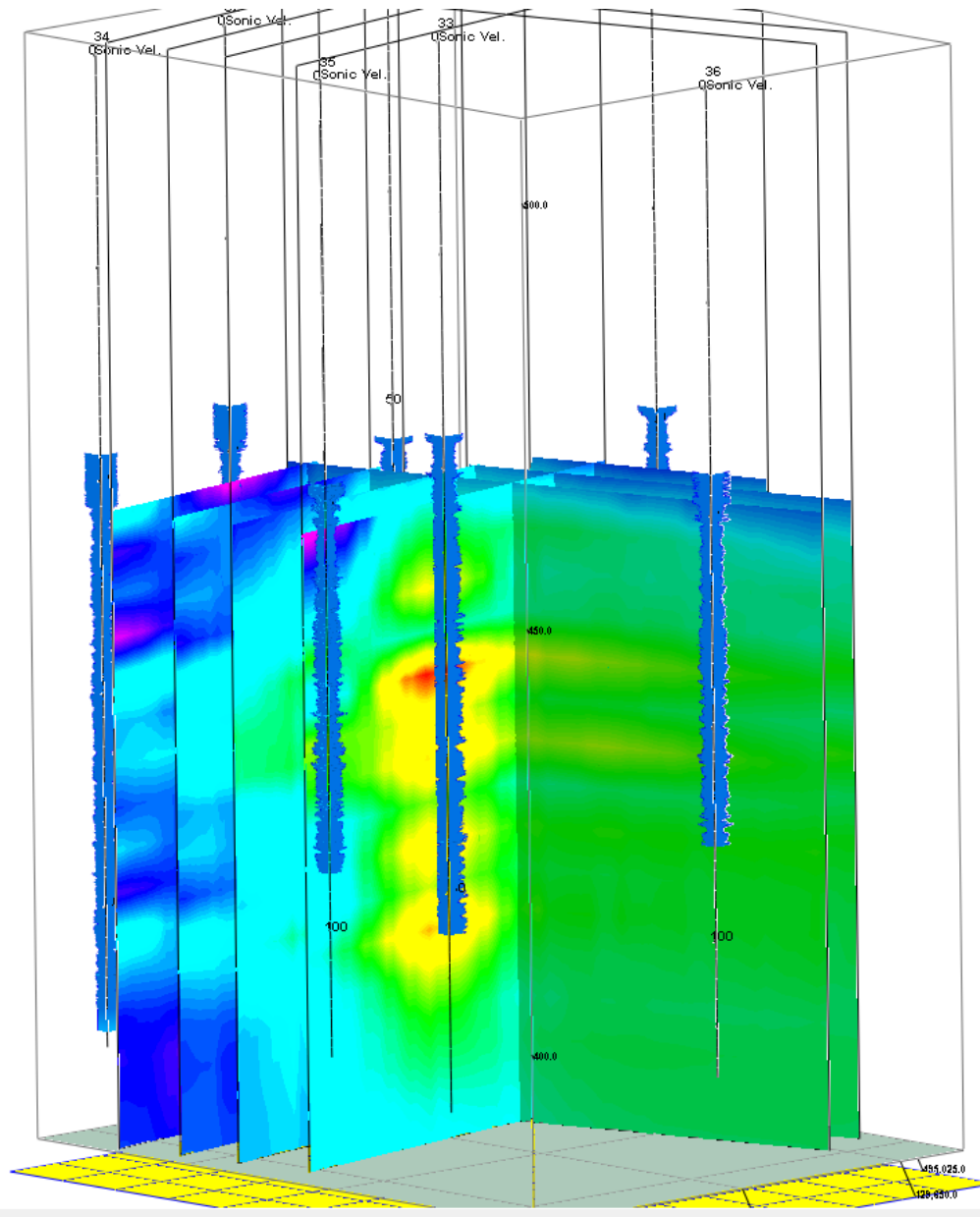
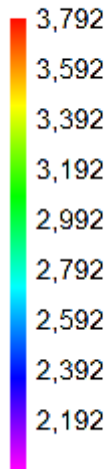
Sonic Velocity (m/s)



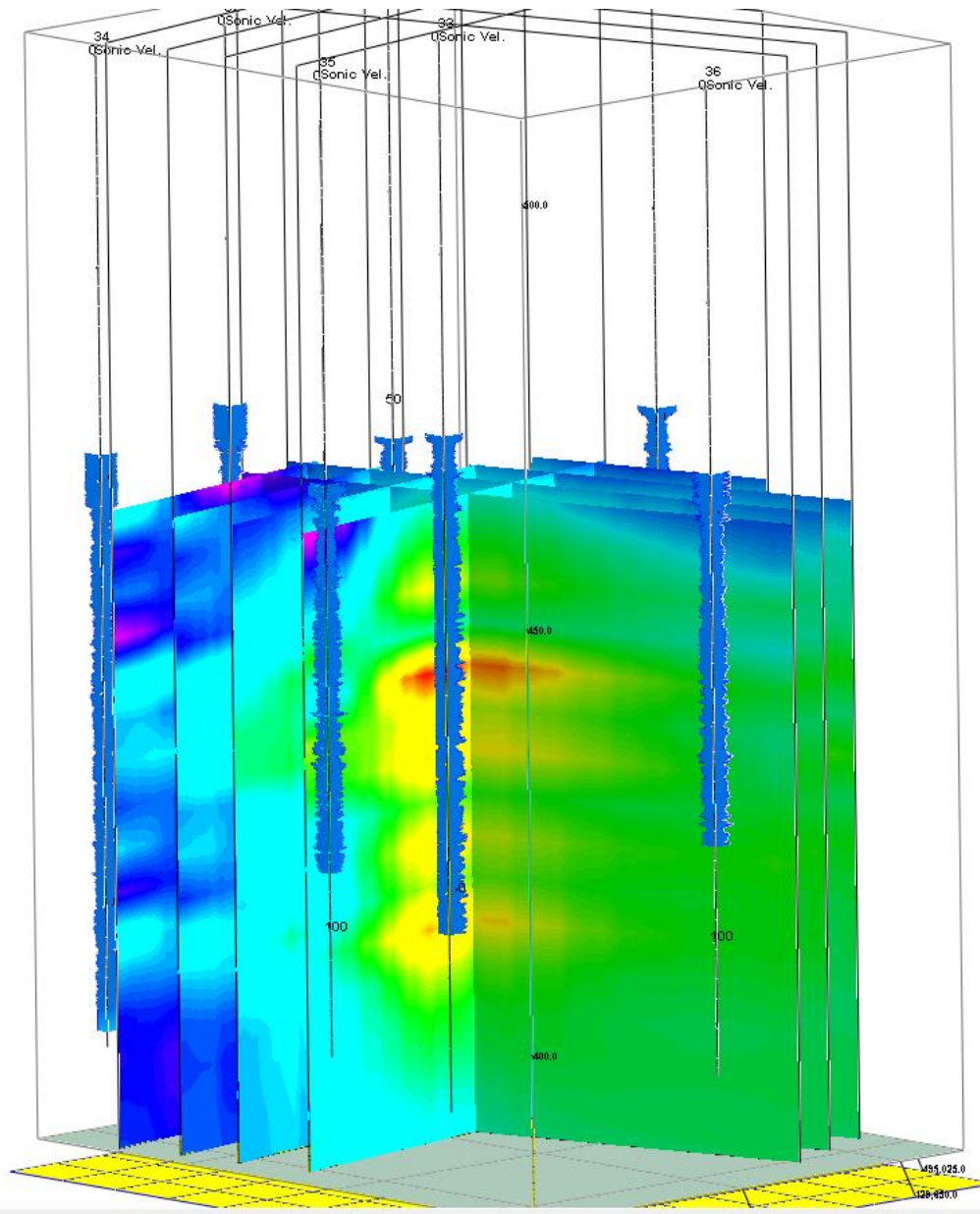
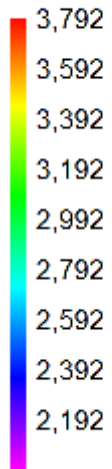
Sonic Velocity (m/s)



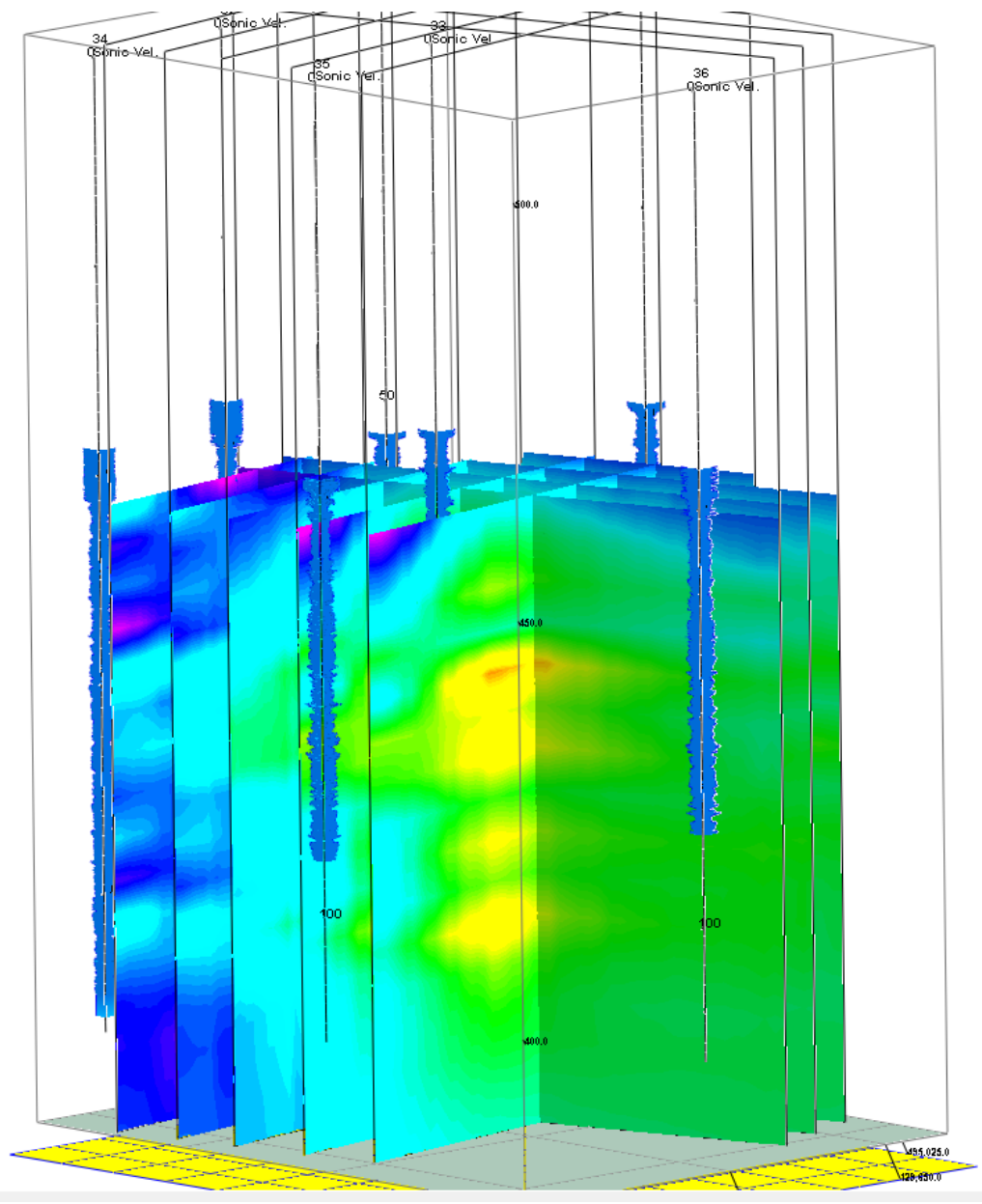
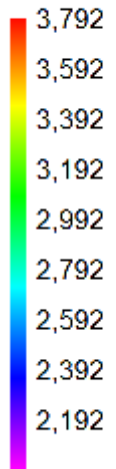
Sonic Velocity (m/s)



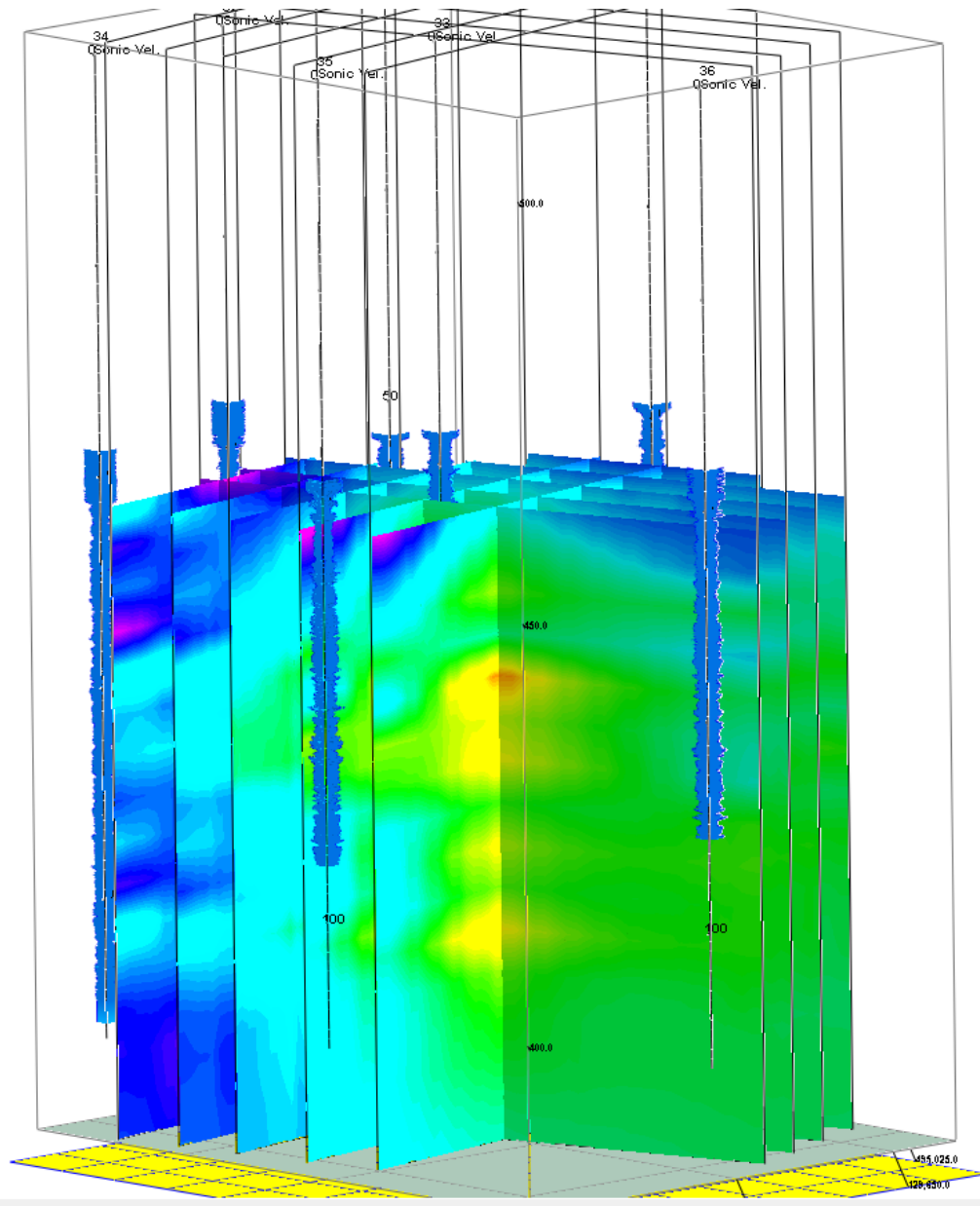
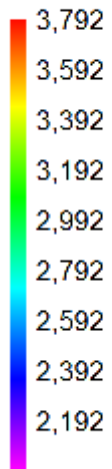
Sonic Velocity (m/s)



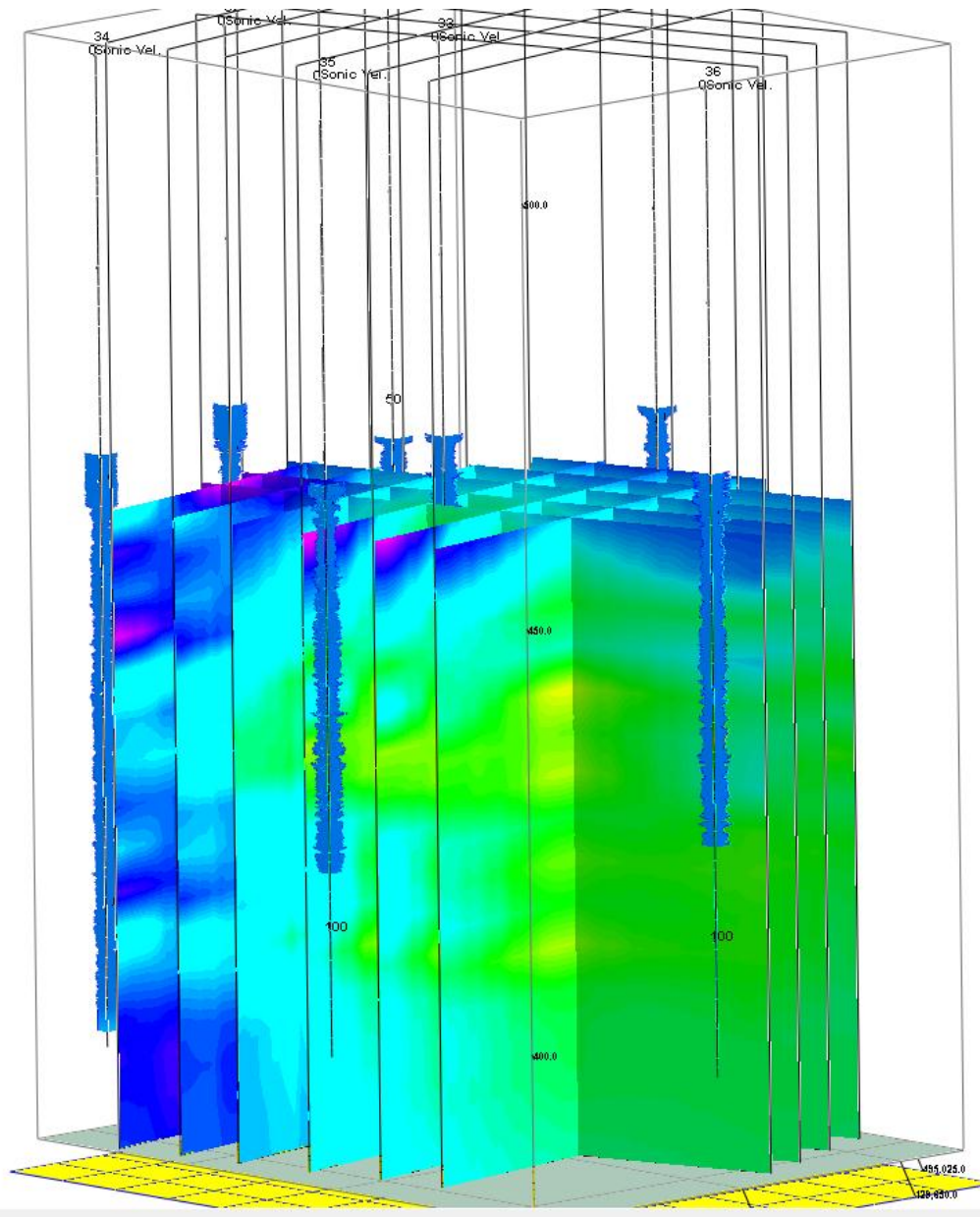
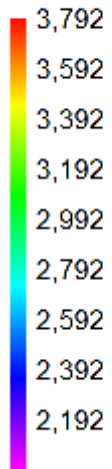
Sonic Velocity (m/s)



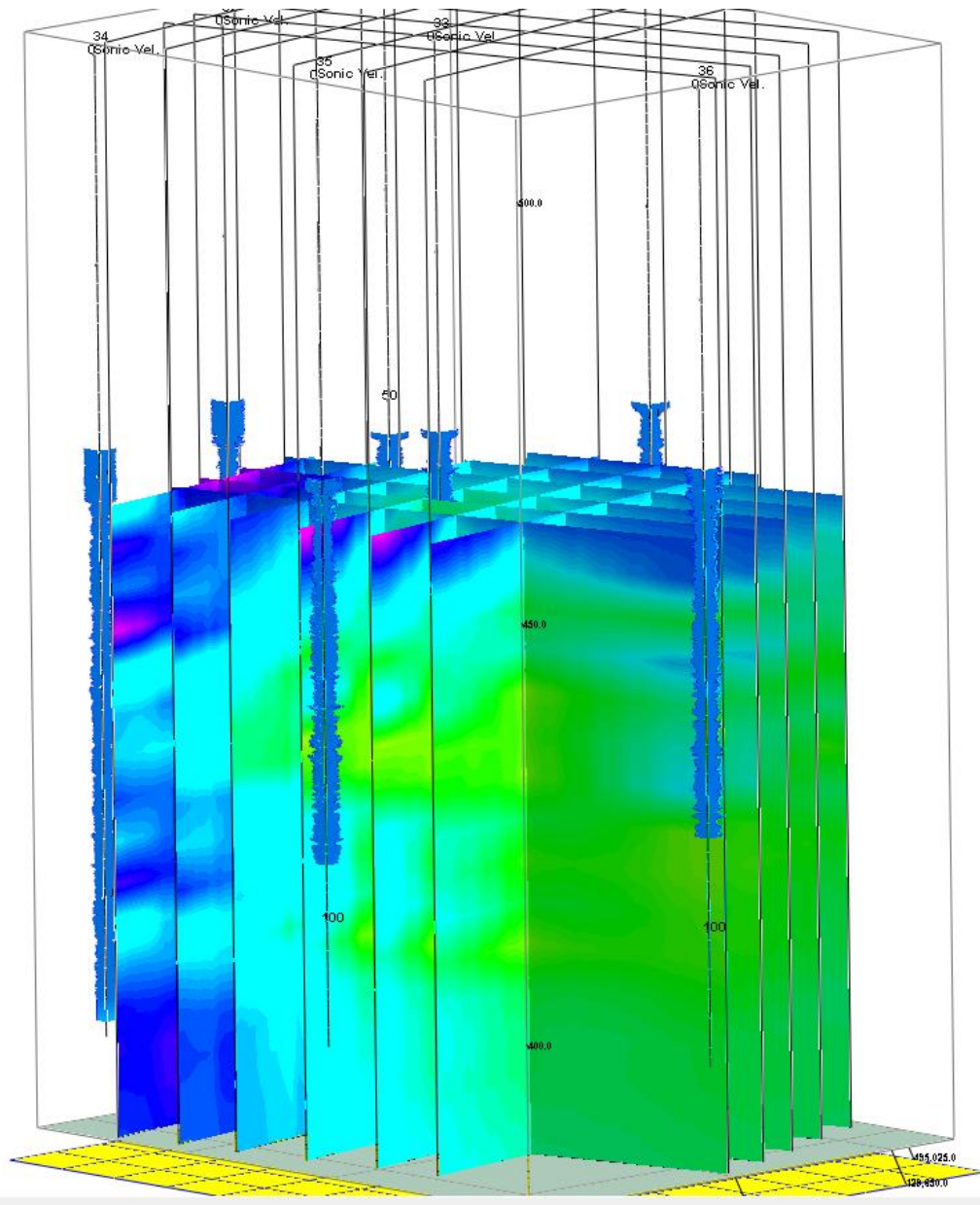
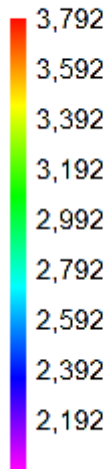
Sonic Velocity (m/s)



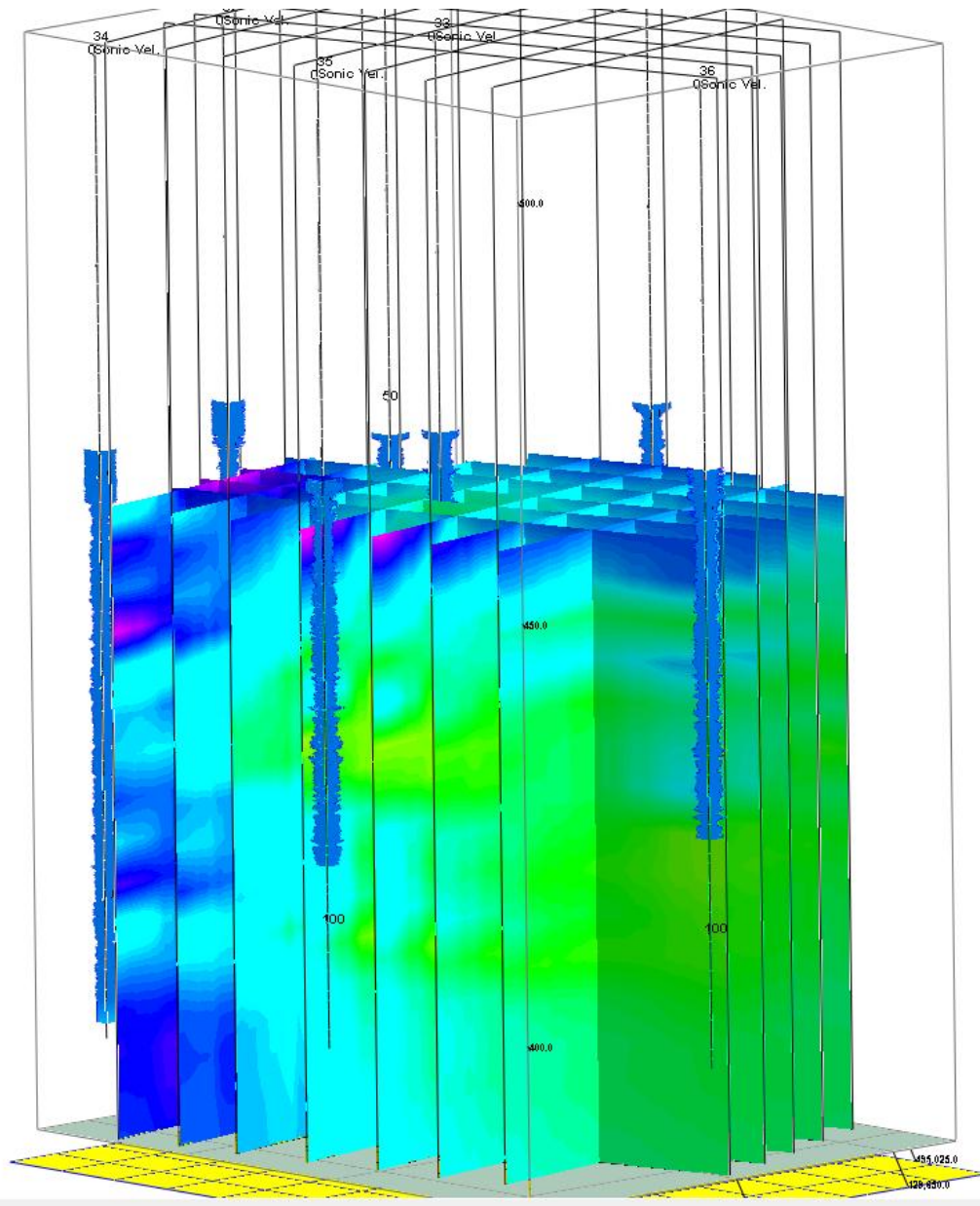
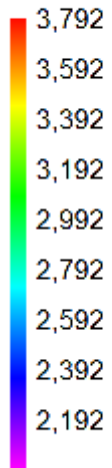
Sonic Velocity (m/s)



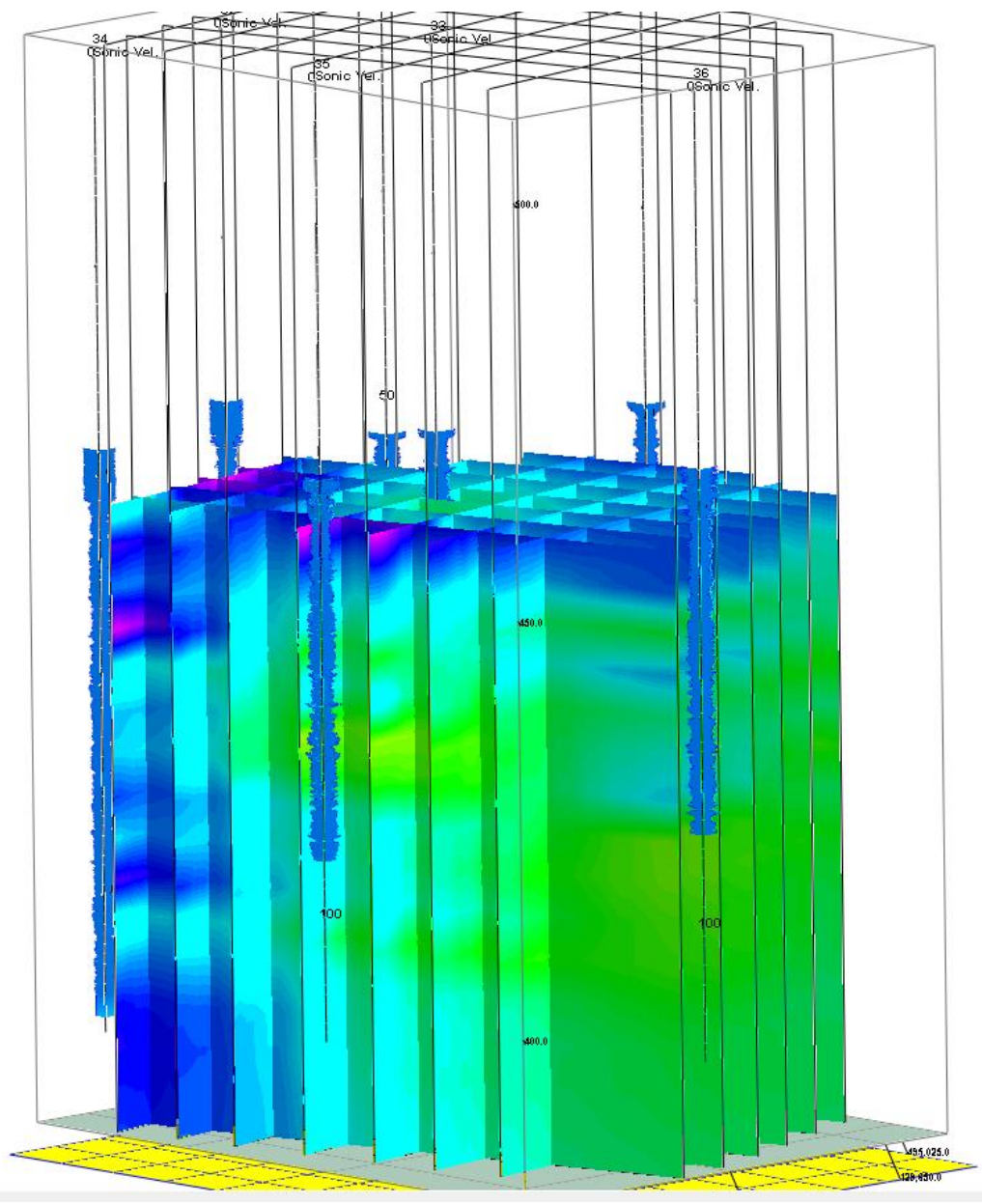
Sonic Velocity (m/s)



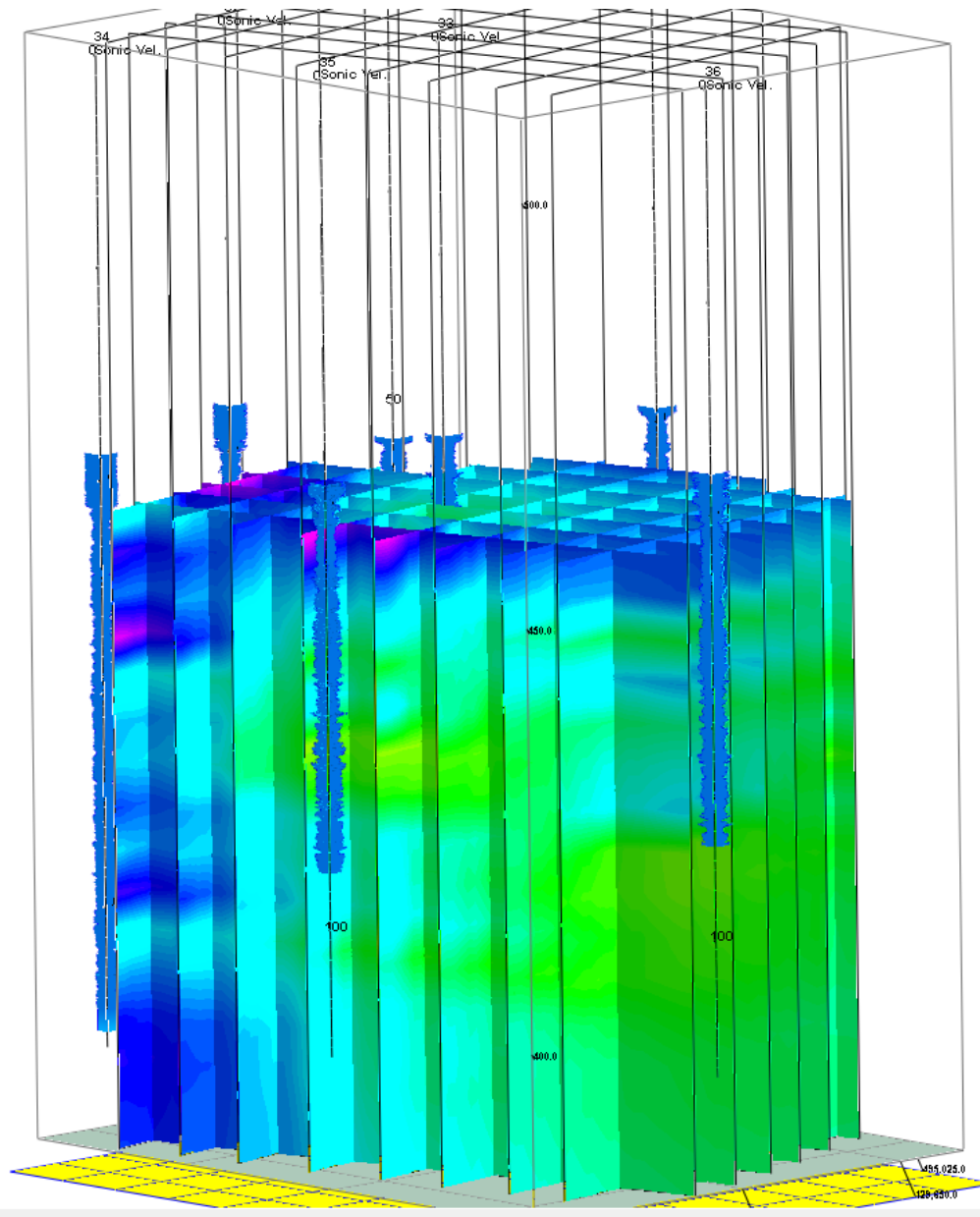
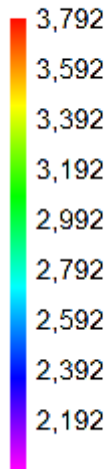
Sonic Velocity (m/s)



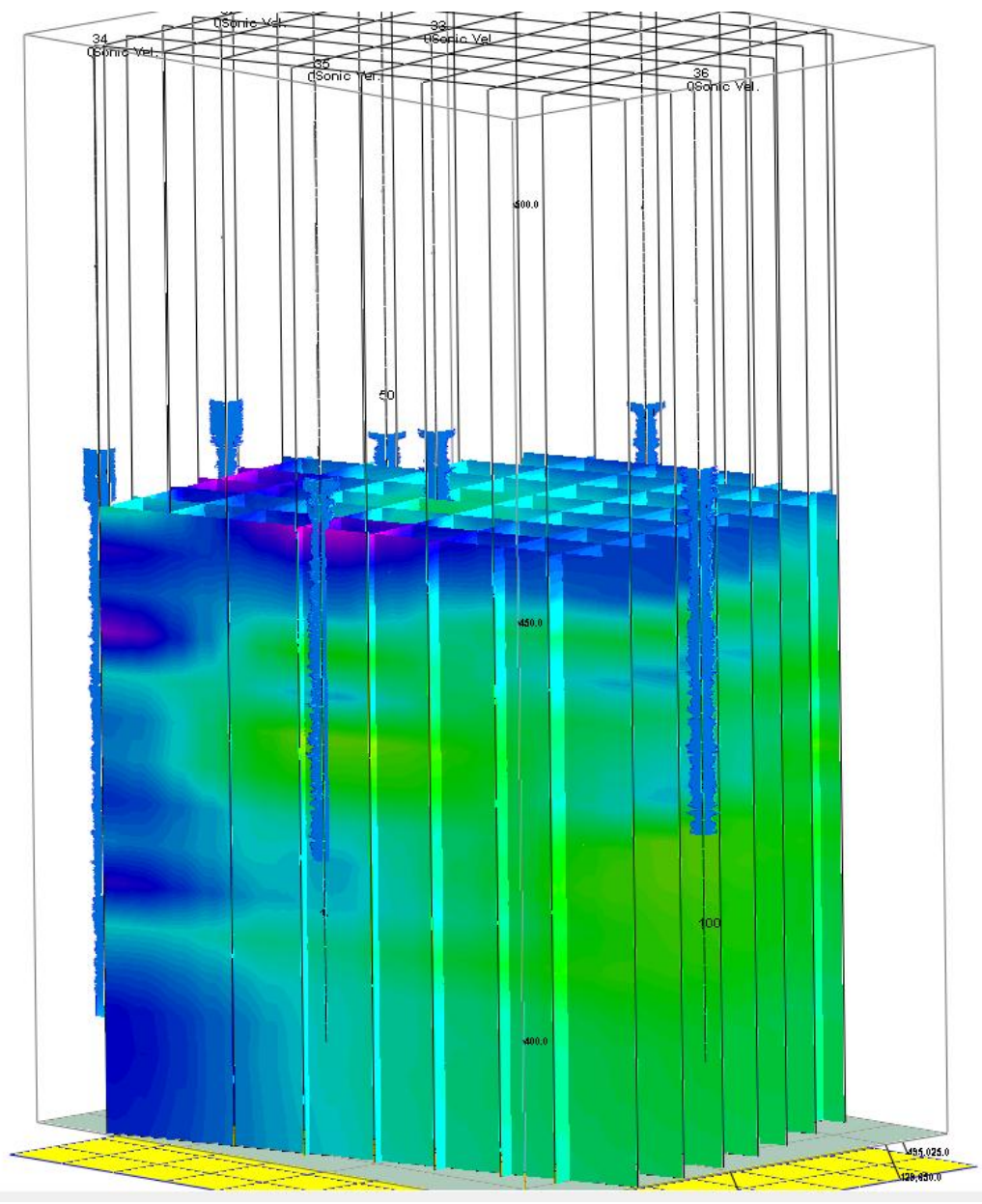
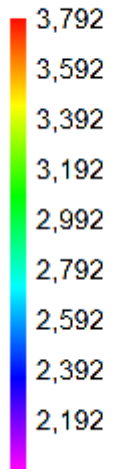
Sonic Velocity (m/s)



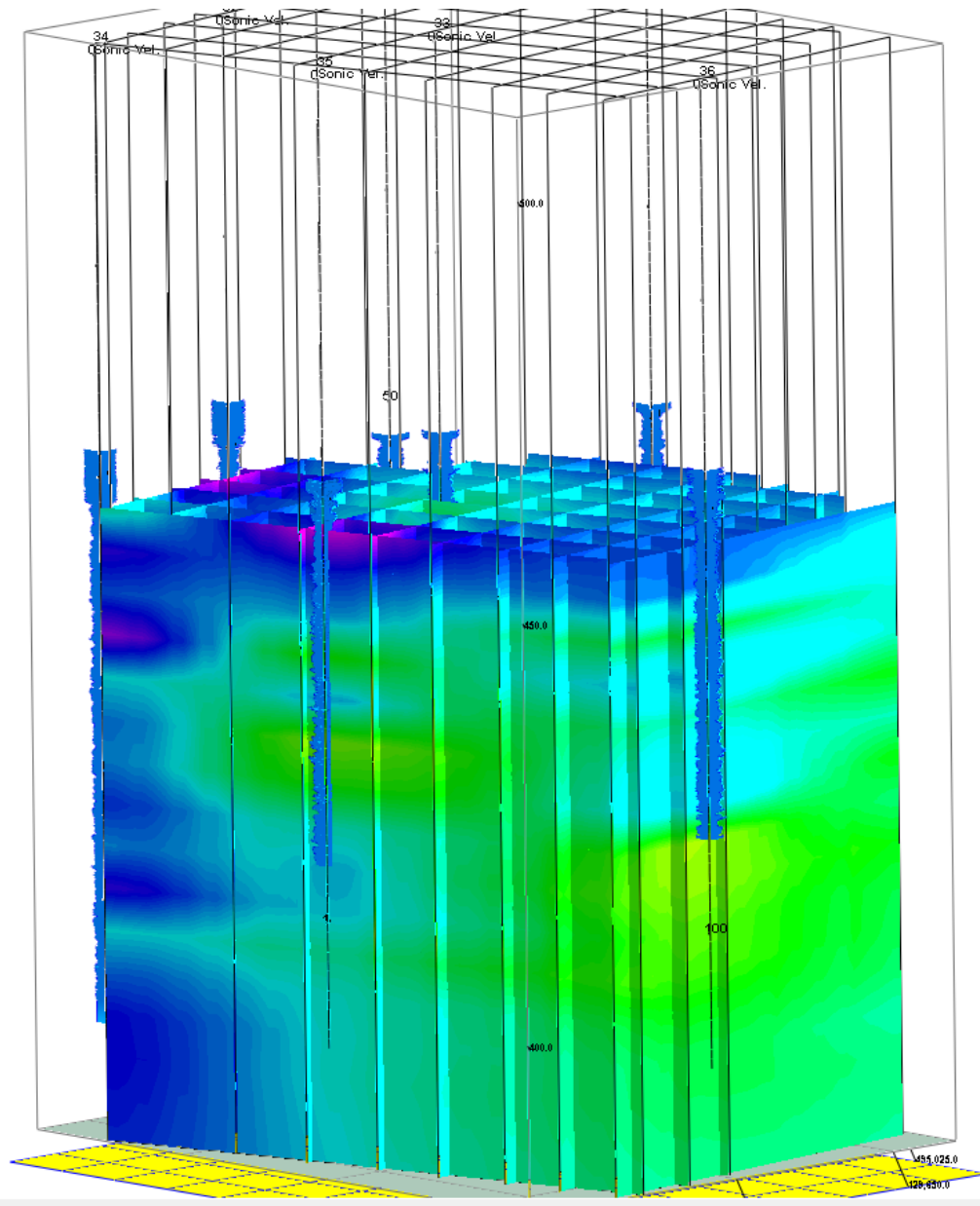
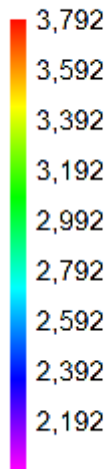
Sonic Velocity (m/s)



Sonic Velocity (m/s)



Sonic Velocity (m/s)



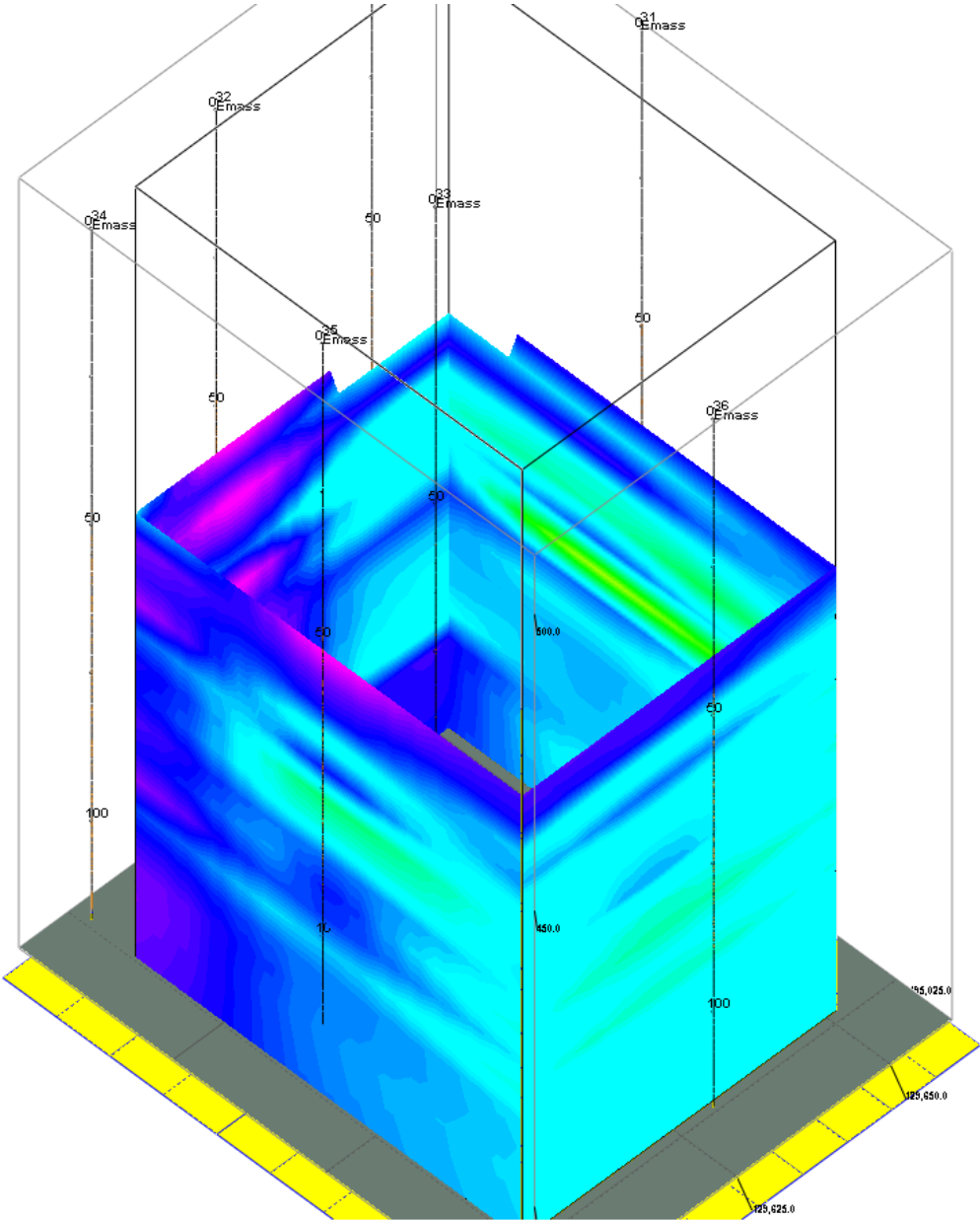
Small Strain Stiffness

Statistical Approach for Small Strain Stiffness

- Calculation of small-strain stiffness from Sonic Velocity Data (using Barton 2002)
- Determination of Conservative Assessed Mean (CAM)
- Current approach to analyse range and CAM for Geotechnical & Structural Models

(Example for BH 30 using Barton 2002)	Vp m/s	E _{mass} Small strain Young's Modulus (Gpa)
CAM	2606.6	5.2
Mean	2871.5	6.5
Standard Dev.	441.6	2.1
Maximum	4094.5	15.8
Minimum	1756.7	2.6

Looking East



Conclusions & Further Ideas

- Assess sensitivity of design to thickness and frequency of weak/ grumuleuse horizons
- Targeted geophysics at Calcareous horizons as potentially most laterally persistent horizons - marker beds.
- Optimise tunnel depth following site selection based on Detailed logging and Geophysical models.
- Development of 3D Model for interpretation all data sets
- Use of Seismic data to define critical small strain stiffness to predict yield behaviour in Geotechnical & structural models

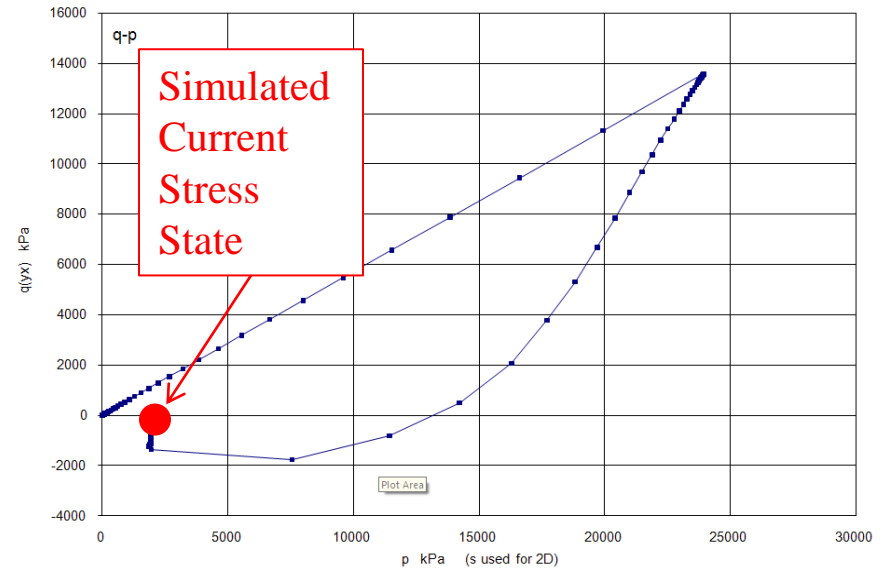
2D FE Geotechnical Modelling

Eden Almog

Stress History and Ground Parameters

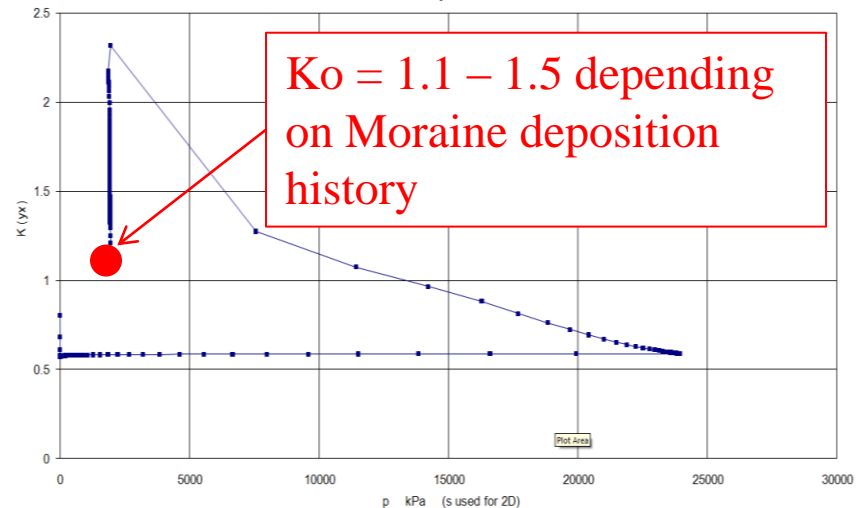
Assumed stress path:

Stage	Name	Cavern Depth (m)	Soil Effective Weight (kN/m ³)	Vertical Effective Stress (kPa)
1	Deposition of Molasse Rocks (2km)	2060	16	33000
2	Erosion	60	16	1000
3	Assumed deposition of 20m Moraine deposits	80	11	1200



Soil mass parameters:

Name	γ	k	ν	E_{mass}	c'	ϕ'
	[kN/m ³]	[m/s]	[-]	(LB) [kN/m ²]	[kN/m ²]	[°]
Molasse Rock Mass	23	1.00E-09	0.2	2800000	220	35
Moraine Gravel	23	1.00E-05	0.25	50000	0.01	35



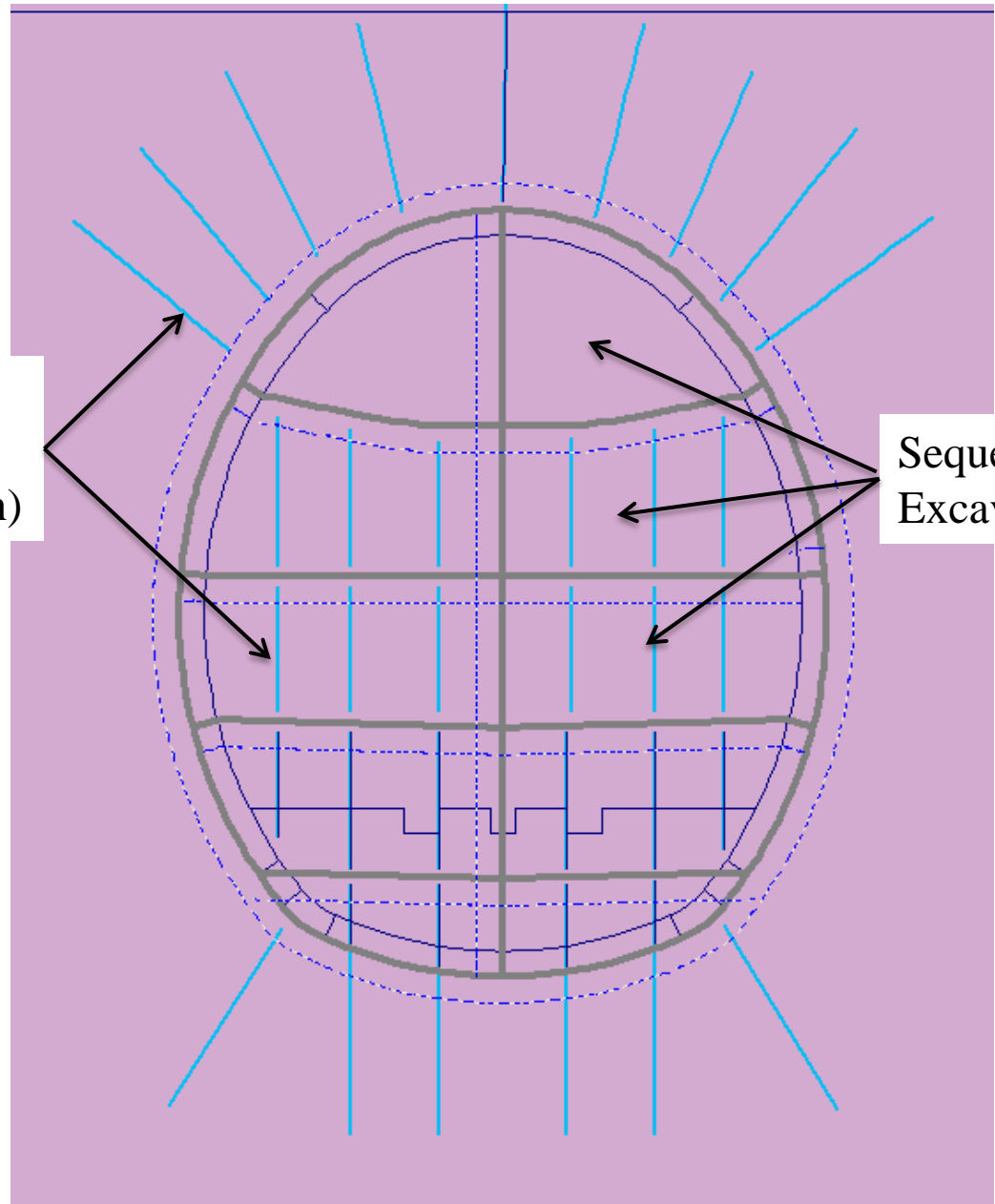
Detailed 2D FE Analysis

Pressure relief
holes (pore-water
-pressure reduction)

Sequential
Excavation

Other features:

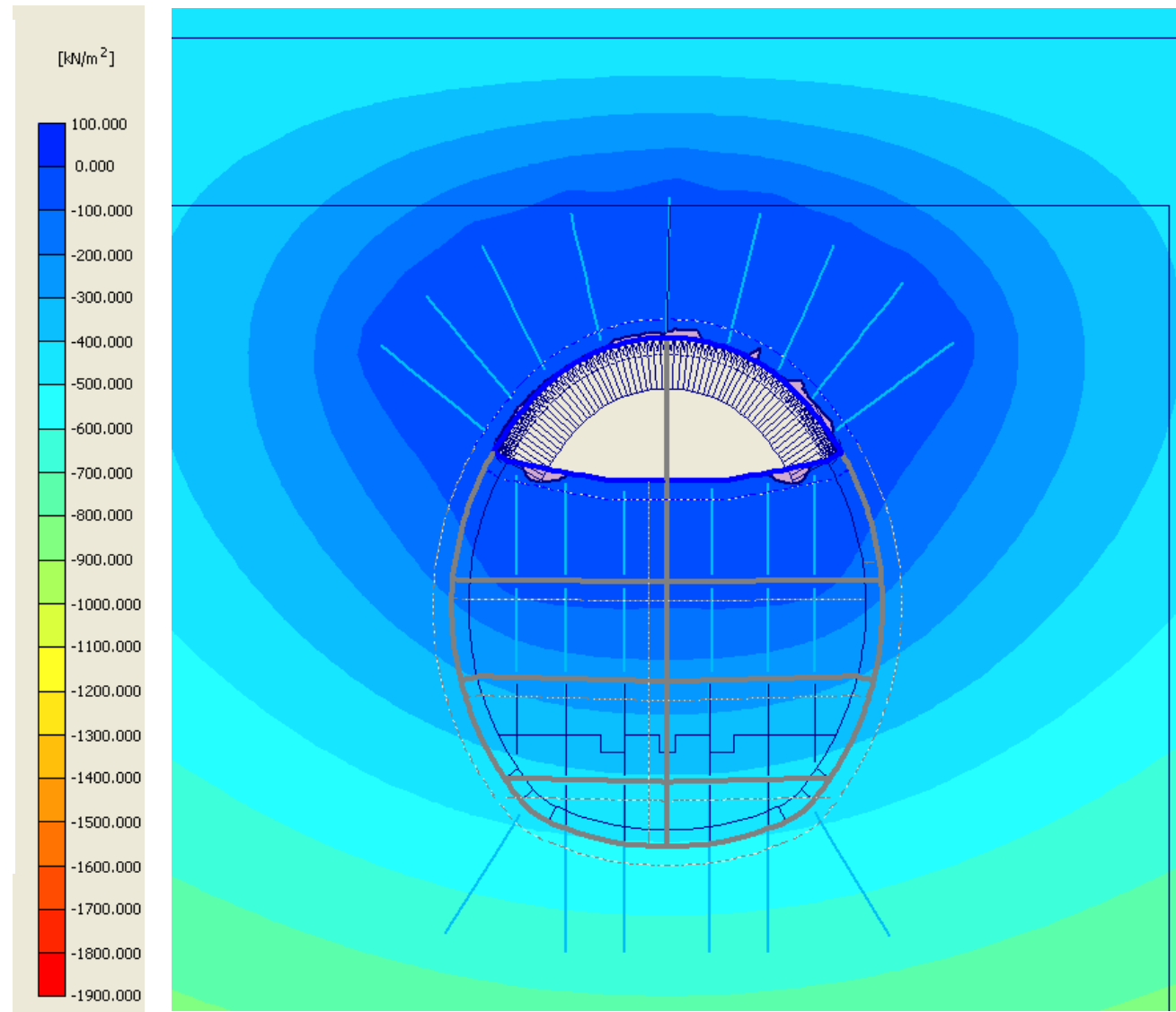
- Molasse drained behaviour with steady state seepage forces
- Stress relaxation per stage
- Shotcrete hardening with time



Example – Top Heading Excavation

Ground water modelling

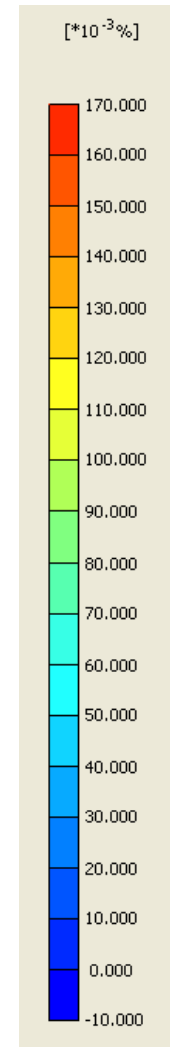
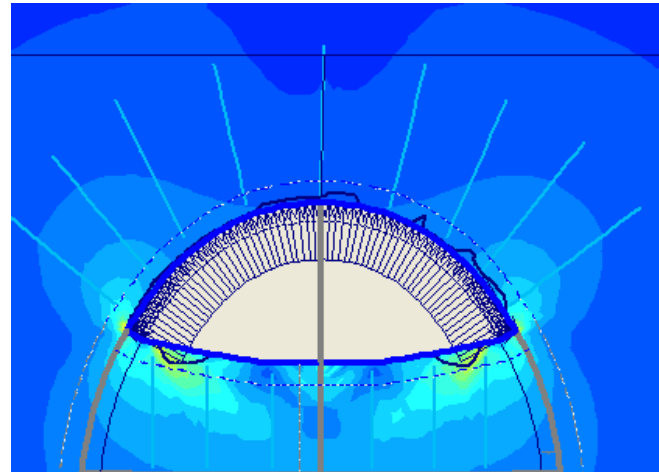
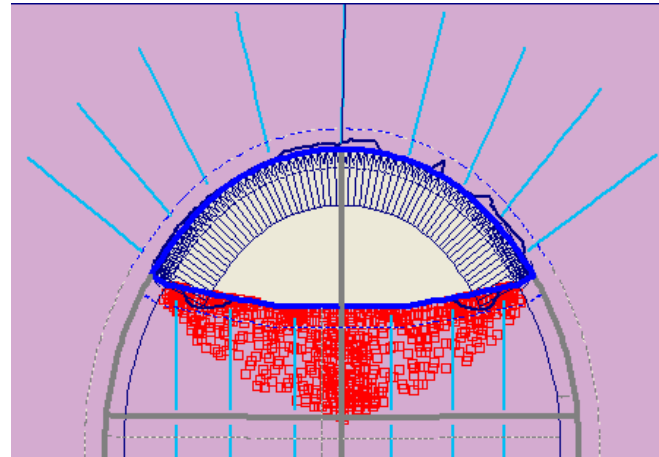
- Reduced pore-pressure around excavation to minimise yielding
- Low permeability coupled with relatively high stiffness with slow construction require drained analysis (little excess pore pressures)
- Steady state seepage but with very low flow rate due to low permeability



Example – Top Heading Excavation

Ground Yielding

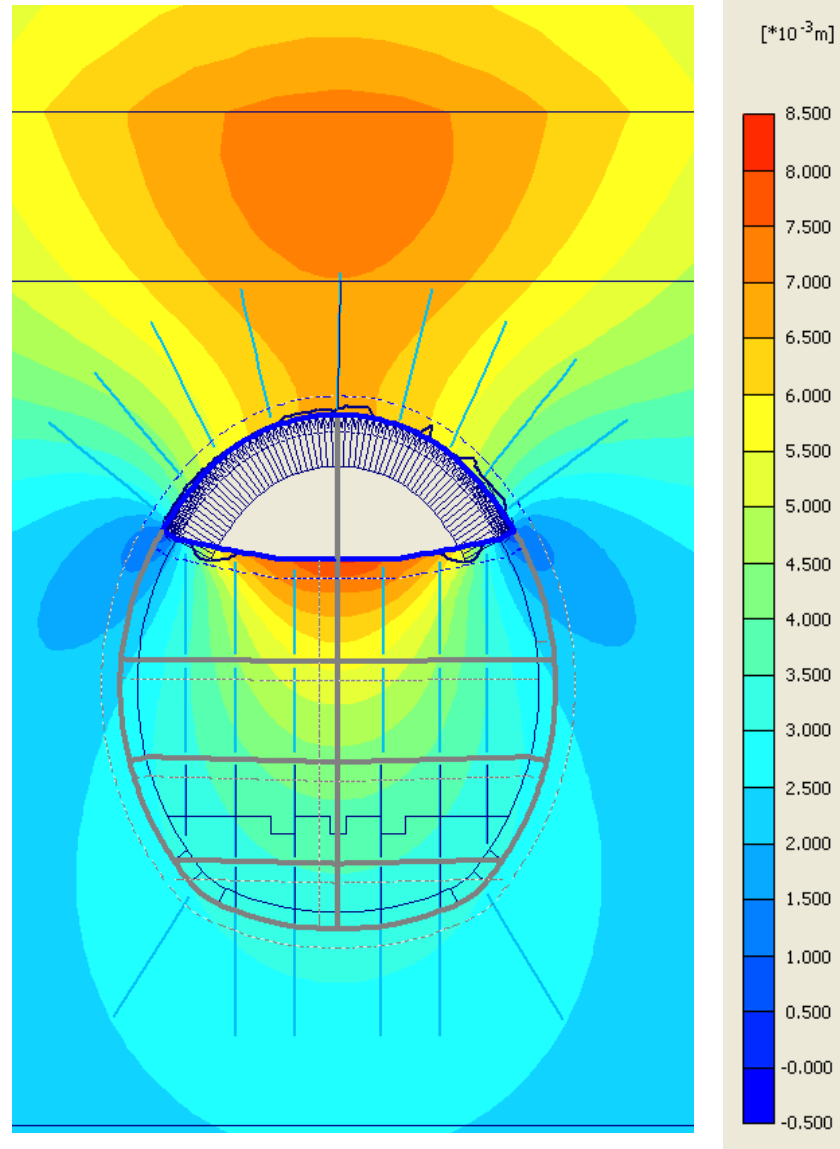
- Full face heading excavation is conservative
- Radial support minimises yielding.
- Most yielding occurs at invert and can be reduced by further sequencing and curvature
- Shear strains values acceptable and no slip surfaces generated (global FoS = 3.5)



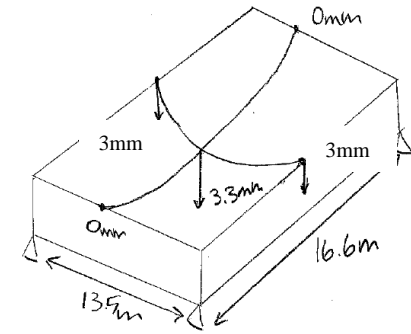
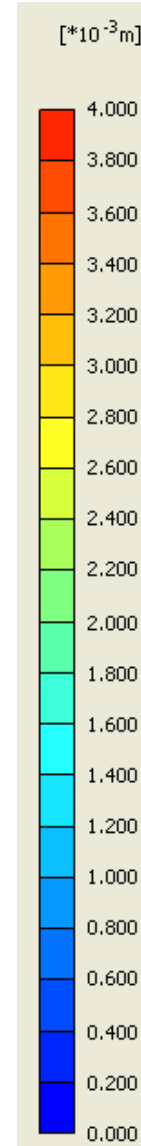
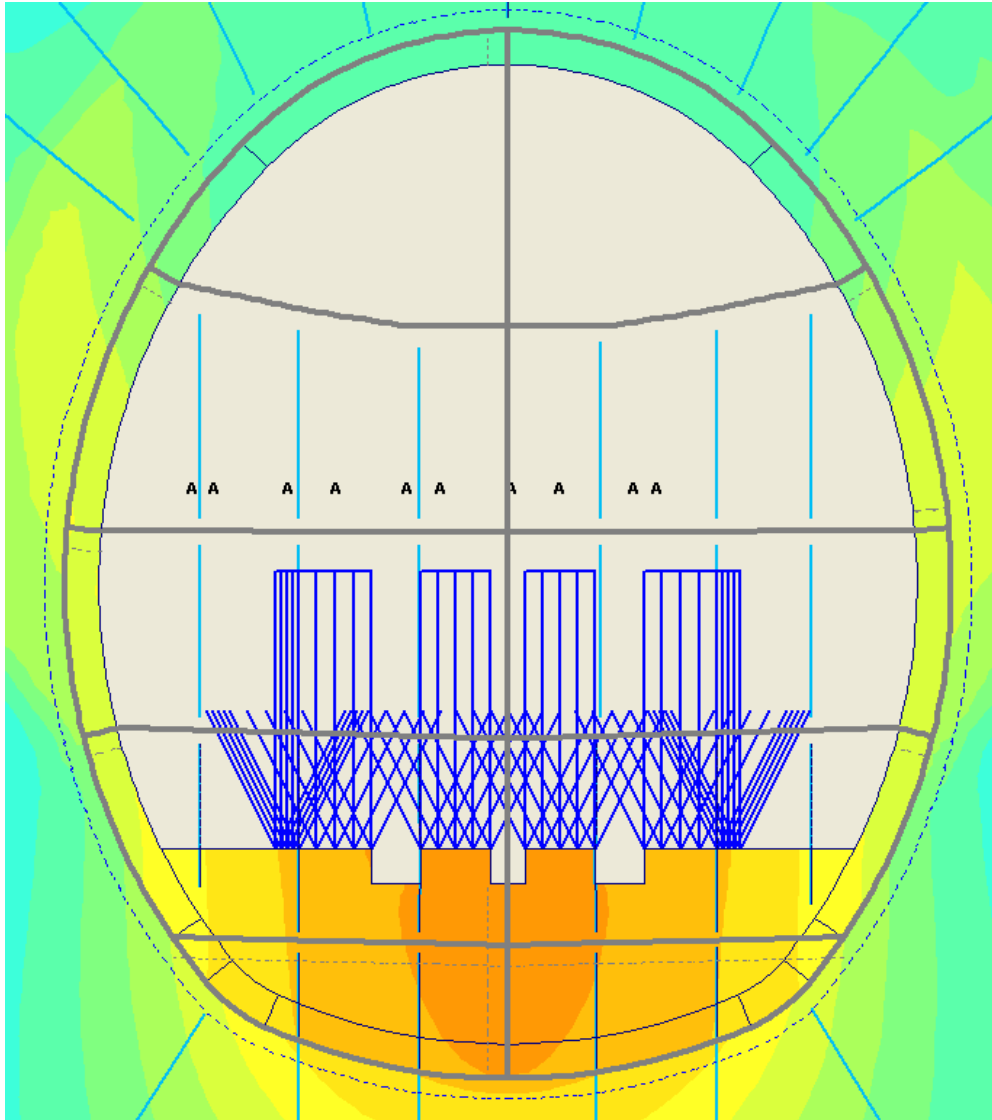
Example – Top Heading Excavation

Ground Deformations

- Invert deformations are in accordance with measured displacements at CMS.
- Maximum tunnel convergence = 0.2% which is acceptable



2D Invert Deformations



Longitudinal: $3.3\text{mm} / 16.6\text{m}$
 $= 0.2\text{mm/m} \times 20\text{m} =$
 $4\text{mm}/20\text{m} > 0.5\text{mm}/20\text{m}$.

Transversal: $3.3\text{mm}-3\text{mm} / 13.5\text{m} = 0.023 \times 20 =$
 $0.45\text{mm}/20\text{m} < 0.5\text{mm}/20\text{m}$.

Unacceptable invert deformation in longitudinal direction. Highlights the need to consider 3D structure effects

3D Bedded Spring Model

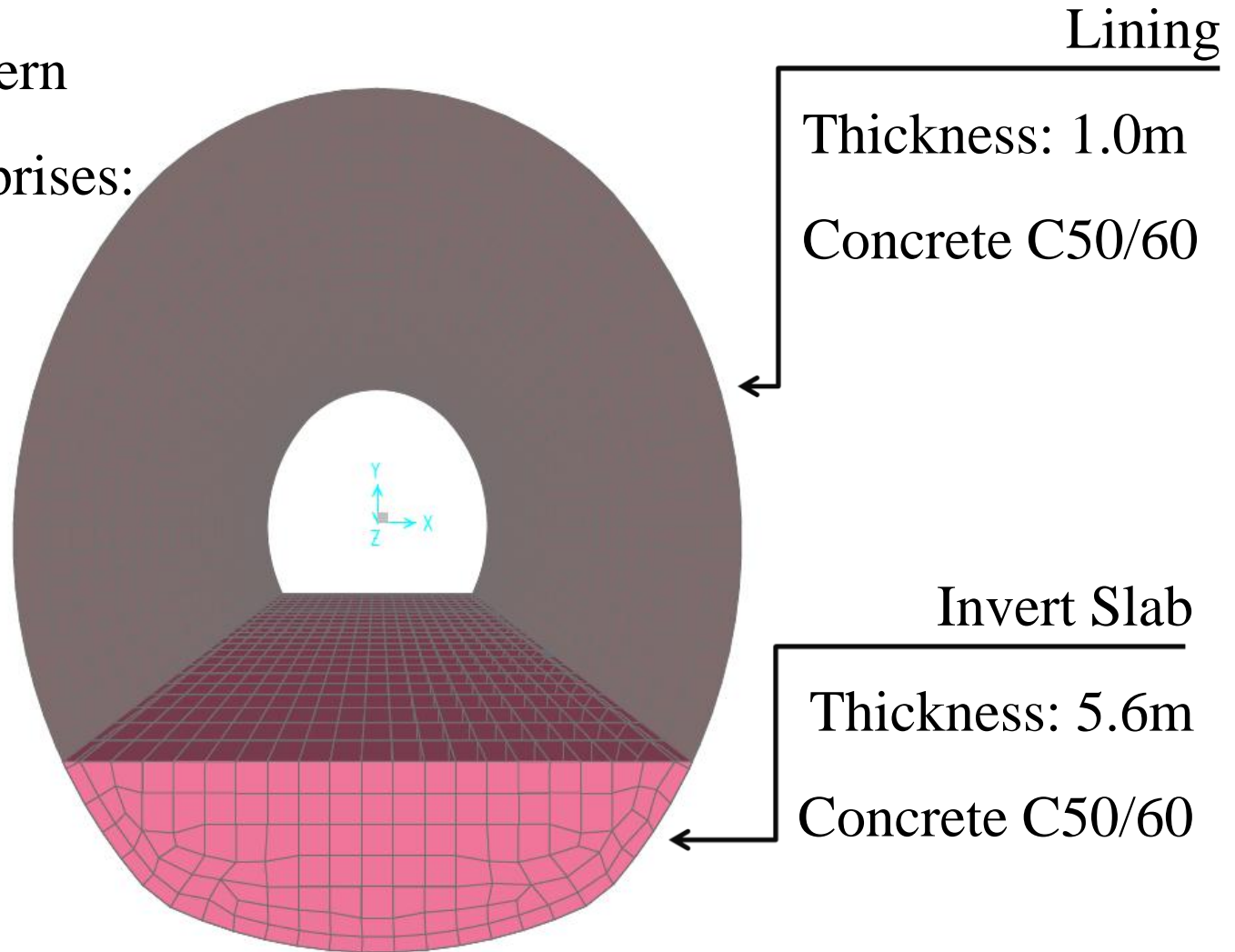
Agnieszka Mazurkiewicz

3D Finite Element Analysis Structural Design

Interaction Cavern

3D-model comprises:

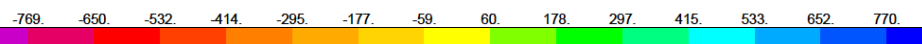
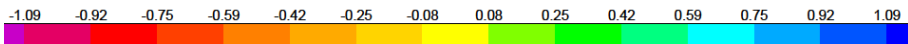
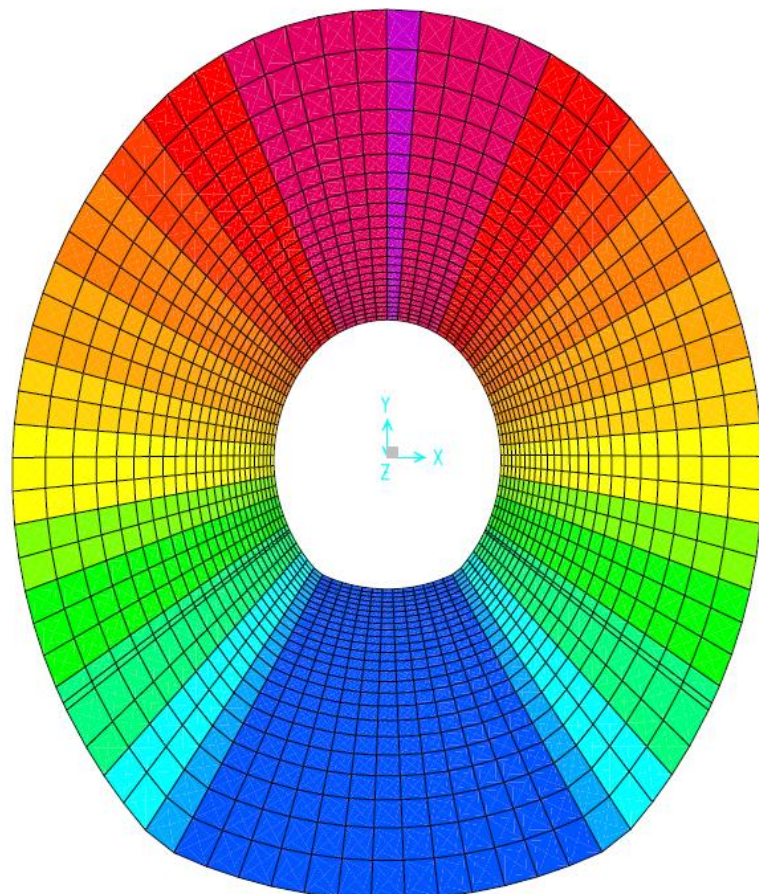
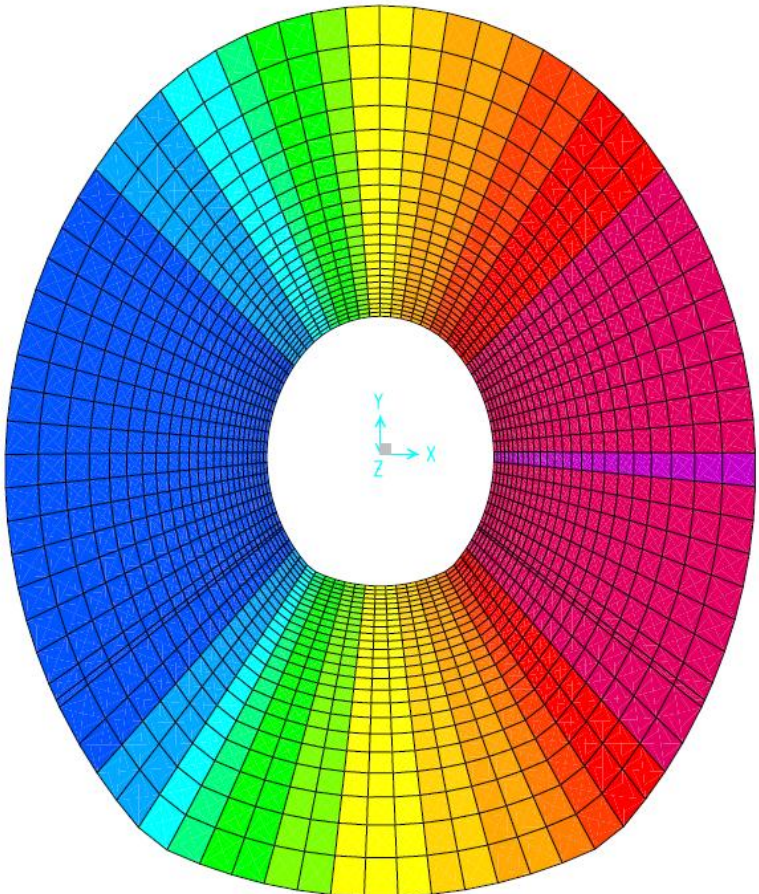
- Lining
- Invert Slab



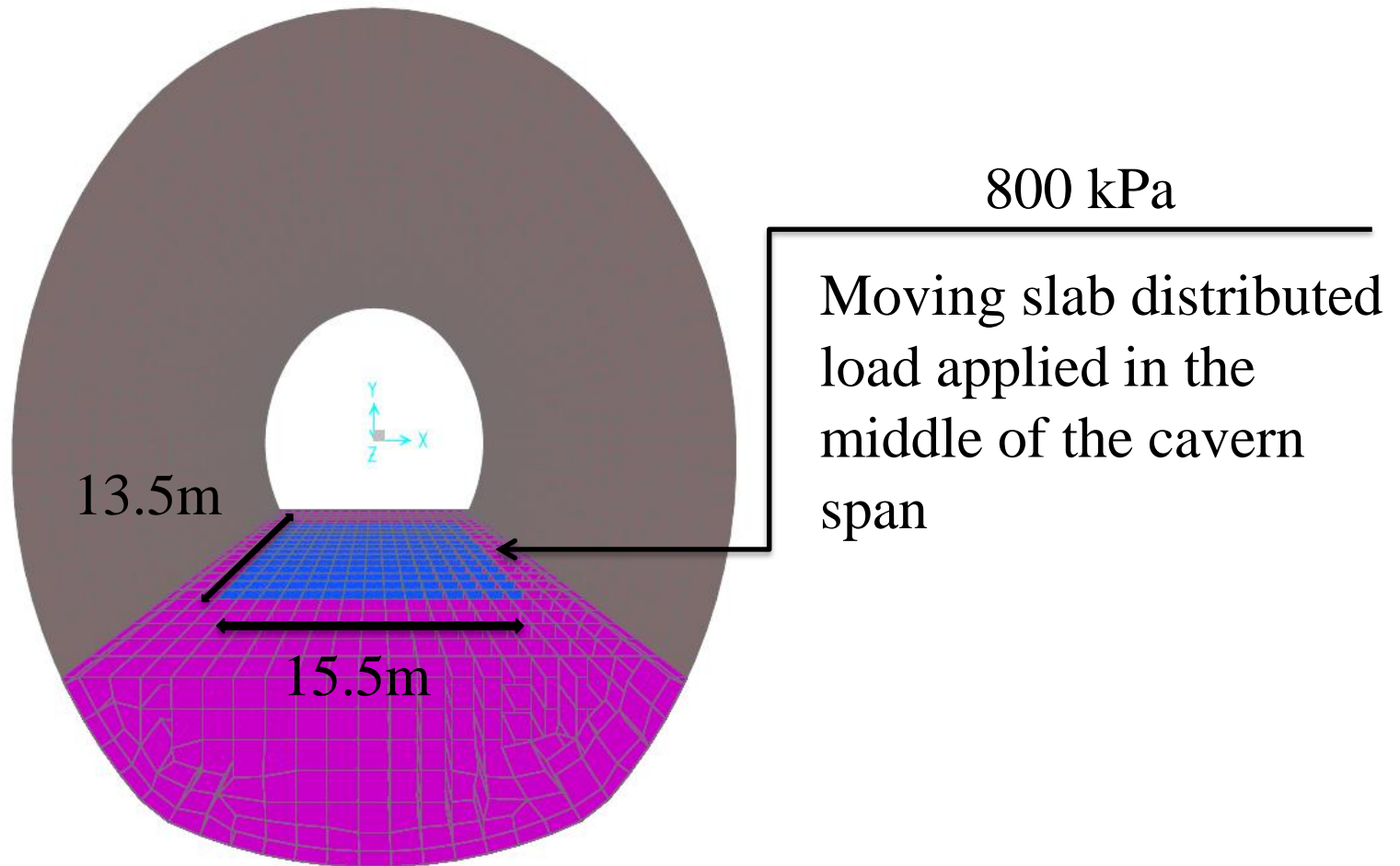
Ground Pressure (Including Stress Arching)

Max Horizontal Pressure: 1090 kPa

Max Vertical Pressure: 770 kPa

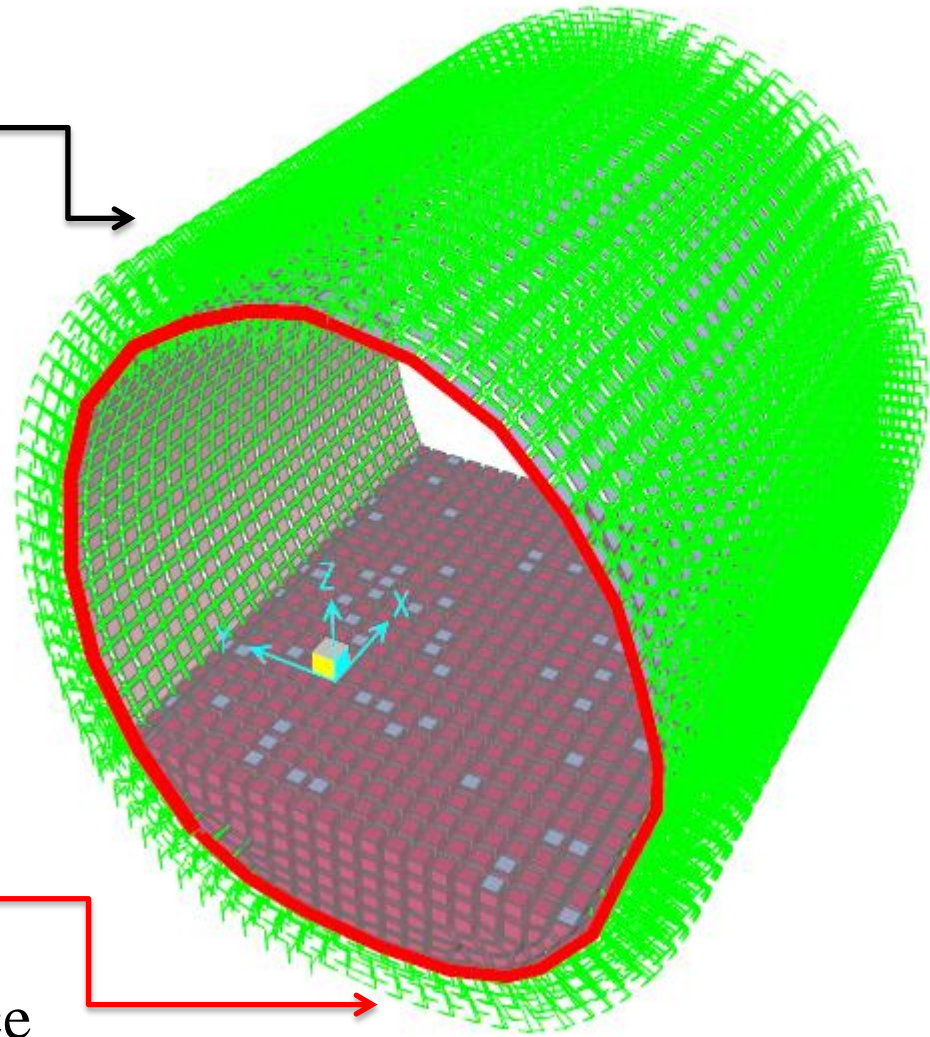
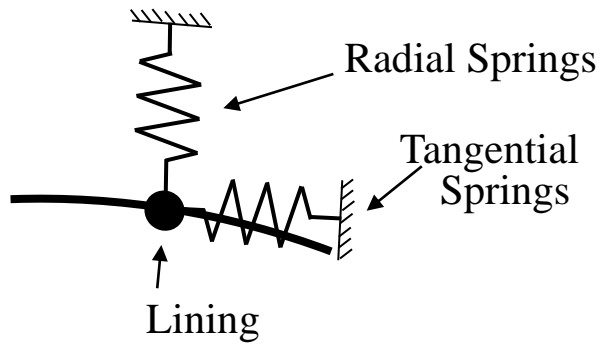


Moving Slab Distributed Load



Boundary Conditions

Springs represent
ground stiffness

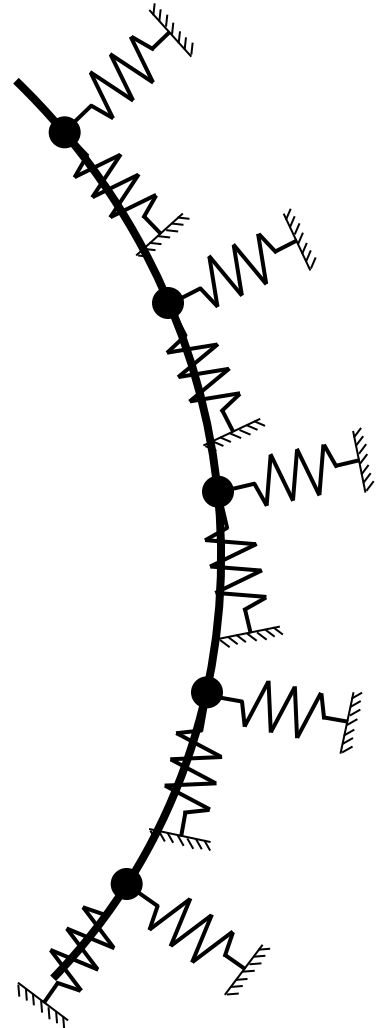


Pinned connection at
interaction cavern and the
service caverns interface

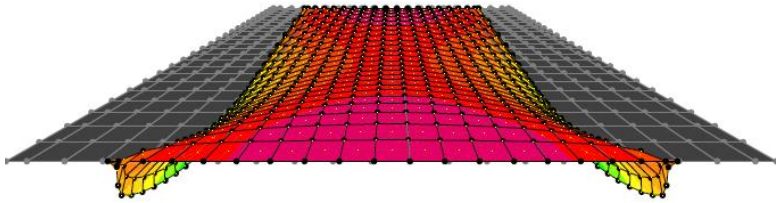
Boundary Conditions

Three following ground stiffness has been investigated in order to evaluate the ground-structure interaction:

- 2D FE non-linear model stiffness:
 - Radial Springs: 100 kPa/mm
- 2x FE model stiffness
 - Radial Springs: 200 kPa/mm
- 3x FE model stiffness
 - Radial Springs: 300 kPa/mm

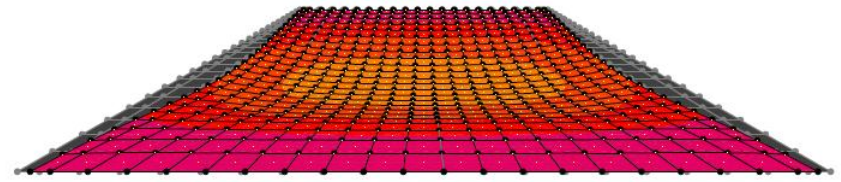


Serviceability Limit State Analysis Invert Slab Deformed Shape



Ground Pressure

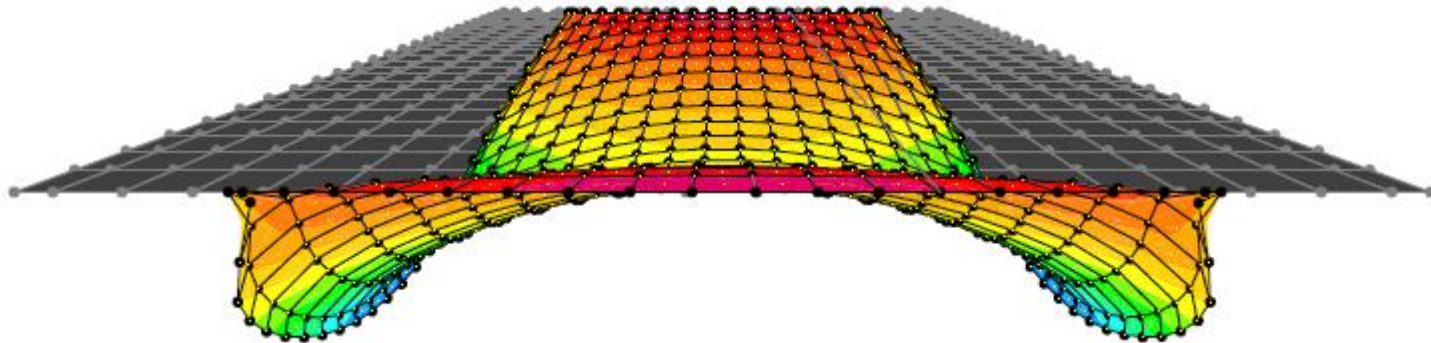
+



Moving Slab

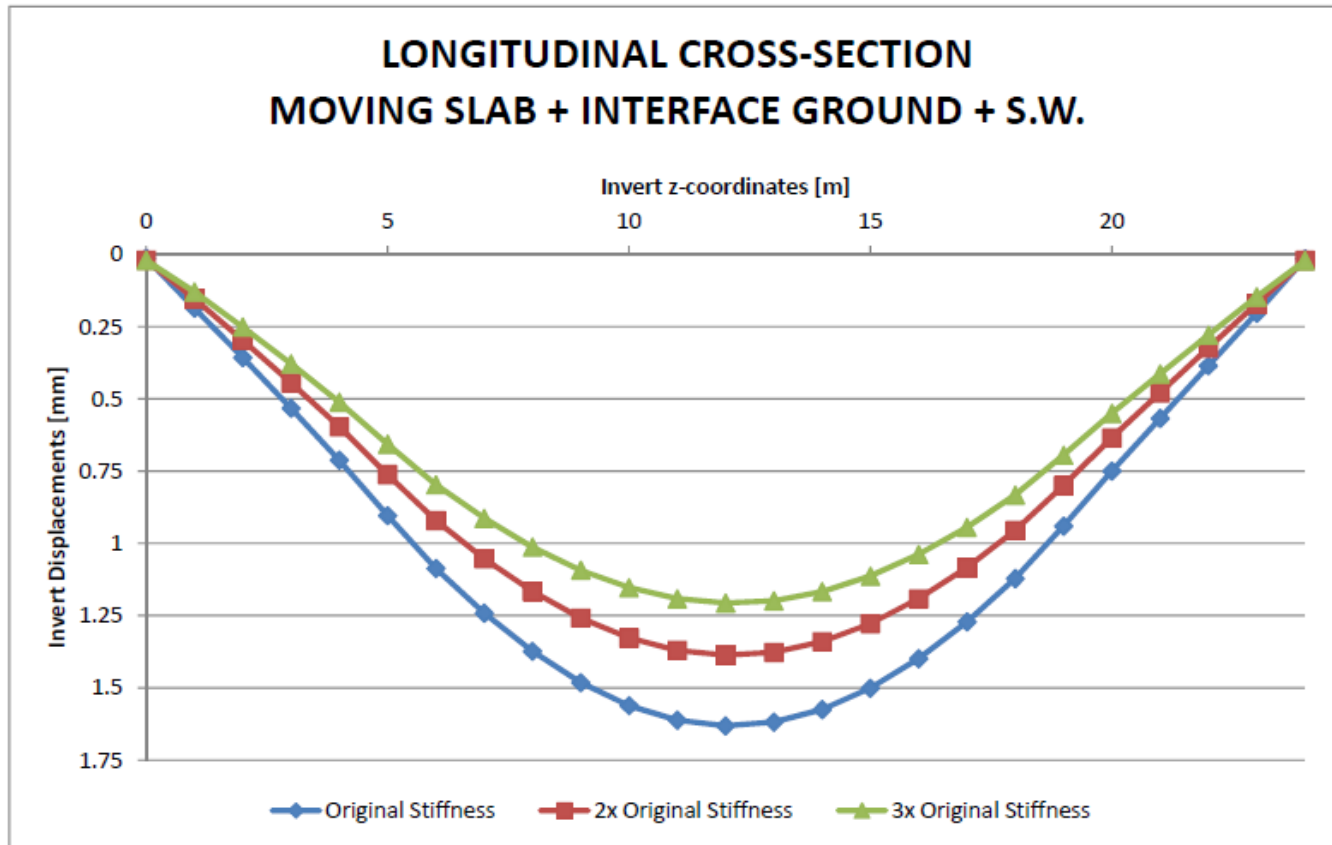
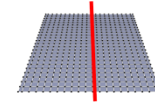
+

+ Self Weight



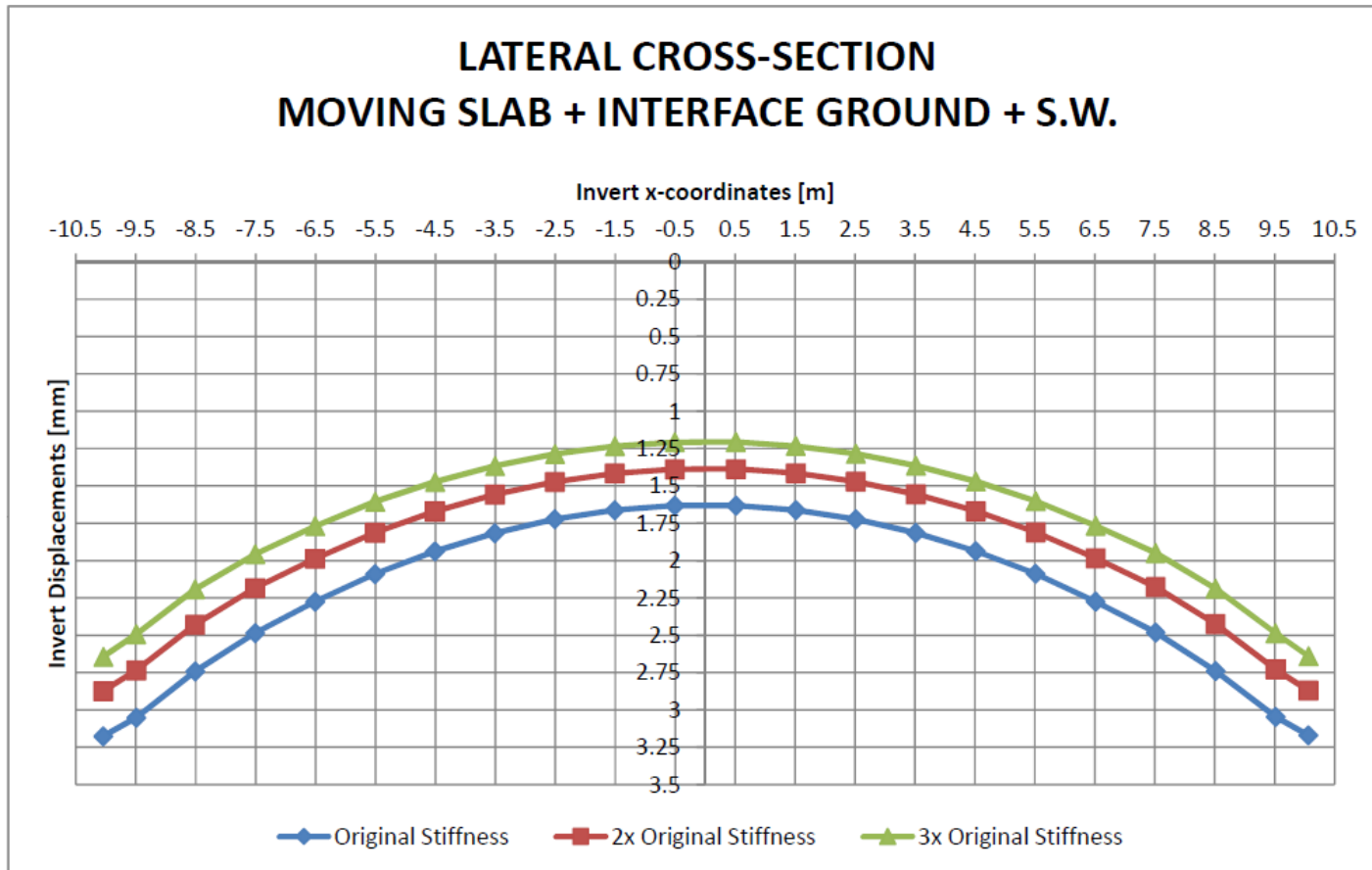
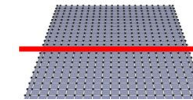
Final Deformation

Longitudinal Cross Section



2D FE model stiffness	2x FE Stiffness	3x FE Stiffness
1.6 mm	1.4 mm	1.2 mm

Lateral Cross Section



2D FE model stiffness	2x FE Stiffness	3x FE Stiffness
1.55mm	1.5mm	1.44mm

Conclusions and Recommendations

Interaction Cavern – Conclusions & Recommendations

Assuming a conservative “full face” construction sequence invert static deformations exceed acceptable limits.

This depends on extent of yielding around cavern during construction (i.e. EDZ). An appropriate construction sequence should limit this.

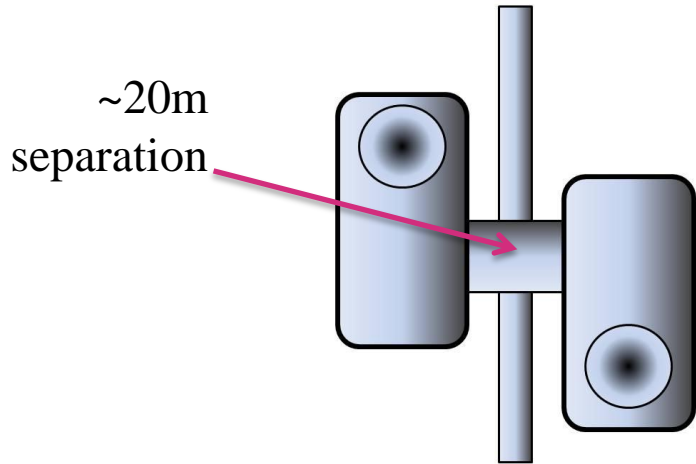
EDZ expected to be larger than the simulated in the 2D FE models due to 3D stress arching resulting from service caverns.

Construction of shaft and interaction cavern prior to service caverns sequence would limit soil yielding at the invert.

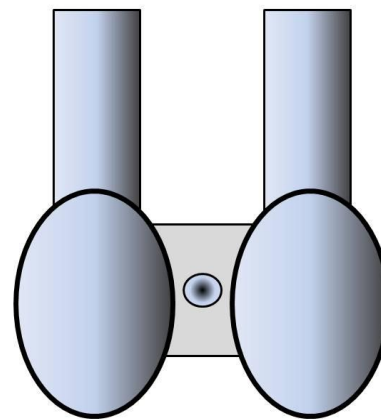
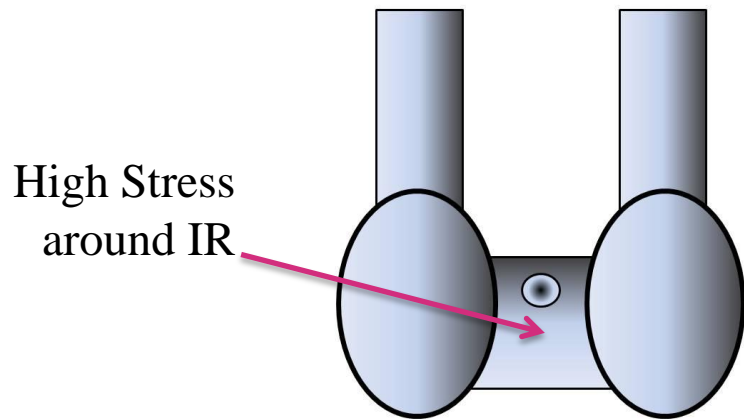
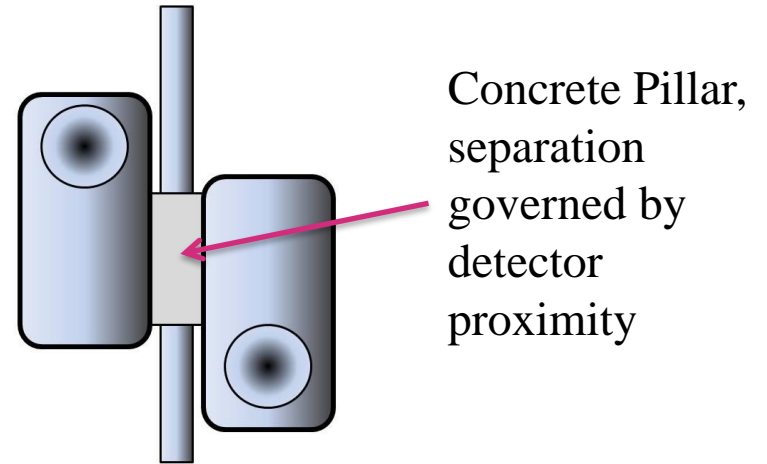
But...significant support will be required!

Alternatives to consider...

Revision G

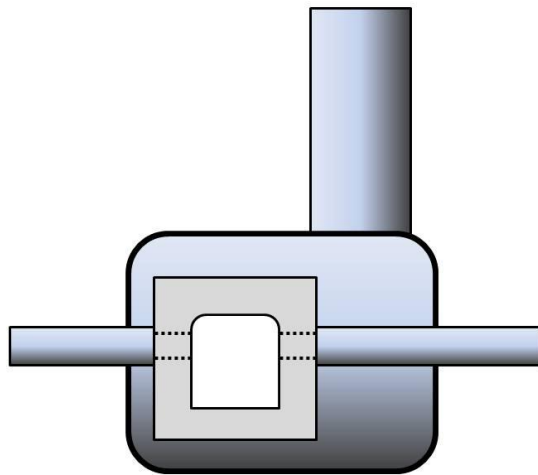
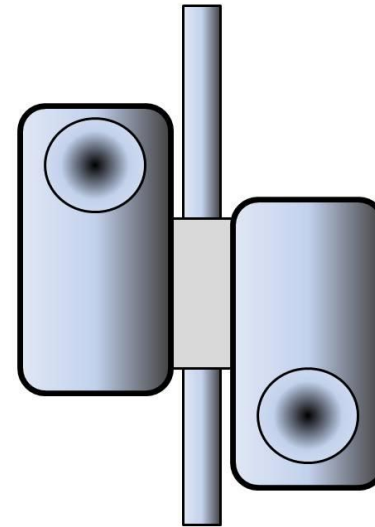


Caverns Moved Closer



Potential Advantages:

- Reduces lining stress around caverns
- Slab foundations likely to be extremely stiff
- Vertical walls at IP, machine/detector interface can be optimised
- Slab size potentially independent of detector width
- Minimum travel time and umbilical lengths



Section A-A

