

CERN

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Development of radiation-tolerant linear voltage regulators and on-detector DC-DC conversion

F. Faccio, S. Michelis

CERN – PH/MIC

Outline

The power distribution puzzle in LHC upgrades (trackers)

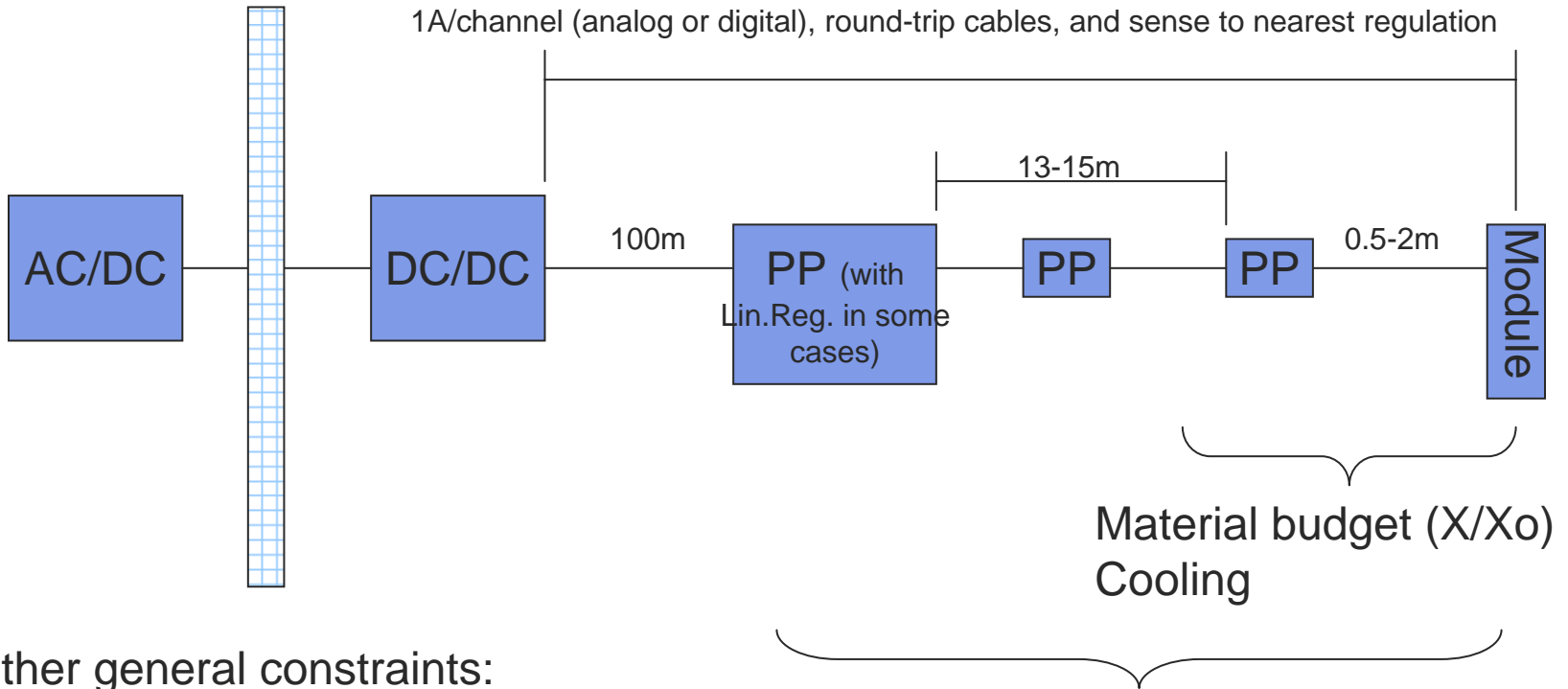


DC-DC converters with air-core inductors

Low Drop Out regulators (LDO)



Present power distribution schemes (in trackers)



Other general constraints:

Overall efficiency

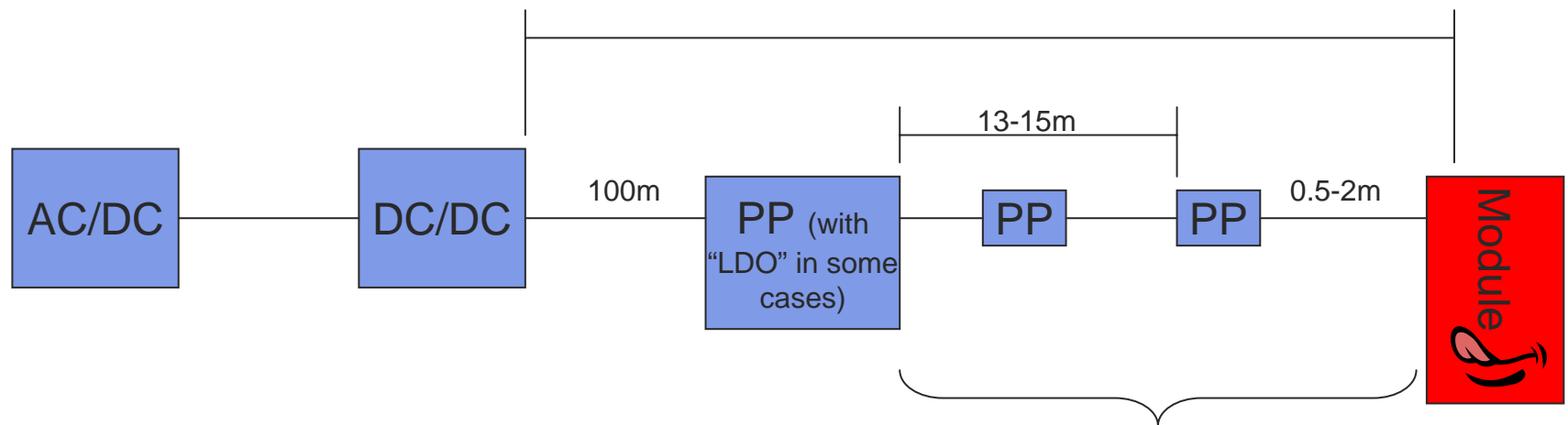
Cost

Reliability (single point of failure)

LHC upgrades - Requirements

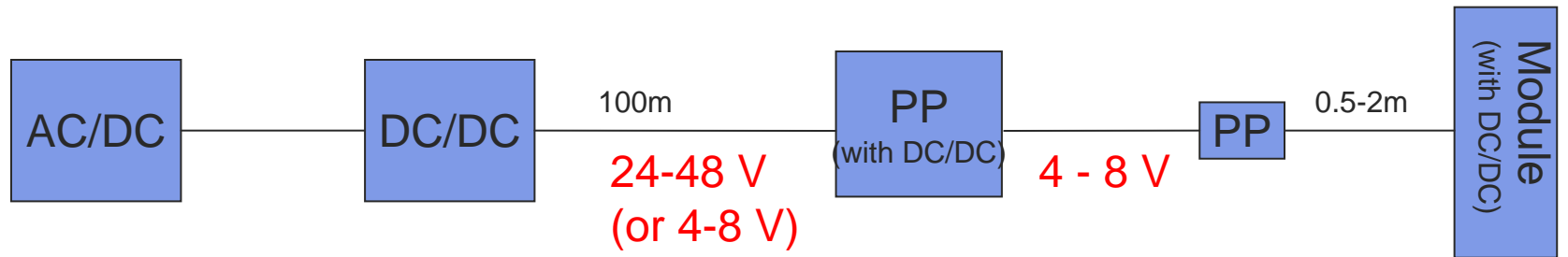
More channels required, at lower V_{dd}, hence overall more current!

Either $\gg 1\text{A/channel}$, or 1A/channel and **more modules**

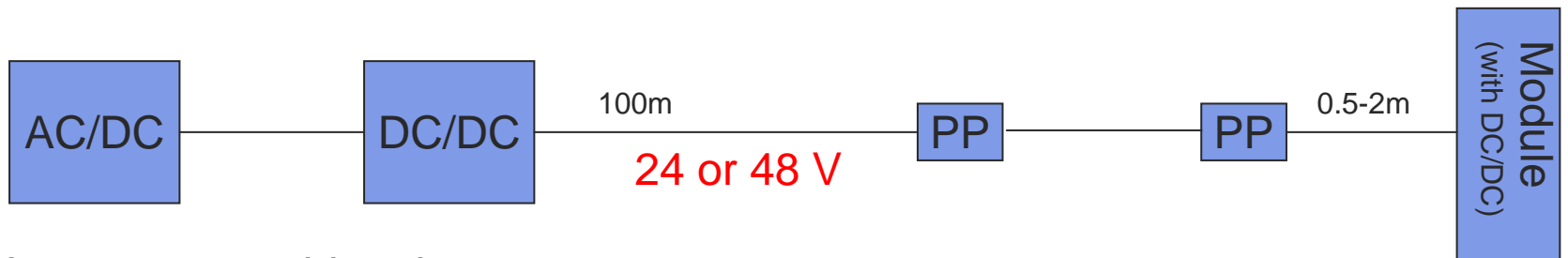


More or thicker cables:
Material budget !
Cooling !
Cable crowding!

Possible solutions based on DC-DC



Same cables as today can bring more power,
It requires efficient DC/DC on module for cooling



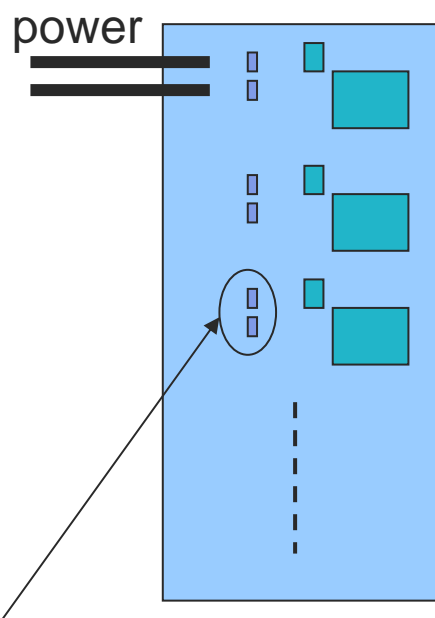
Small cables can bring all the power
It requires efficient DC/DC

Important considerations:

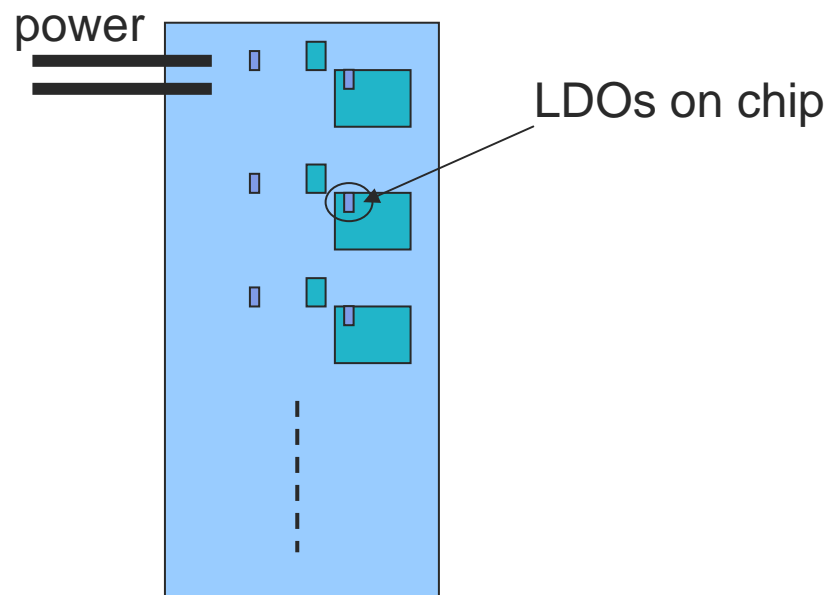
Magnetic field, Radiation
and Material Budget, Noise, plus
EMI if inductor-based DC/DC

On-module or on-chip...

To filter switching noise and/or provide local regulation and protection (over-I, over-V, over-T), LDOs will be very useful – BUT they need to be radiation-hard!



LDOs on module
(analog and digital power)



Present activities within PH-MIC

Feasibility study for the development of an integrated DC-DC buck converter based on air-core inductors

Design of an LDO in 130nm CMOS technology capable of satisfying the radiation tolerance requirements for LHC upgrades. This work is in collaboration with the Ecole Polytechnique Federale de Lausanne, EPFL (1 "stagiaire" for 5 months)



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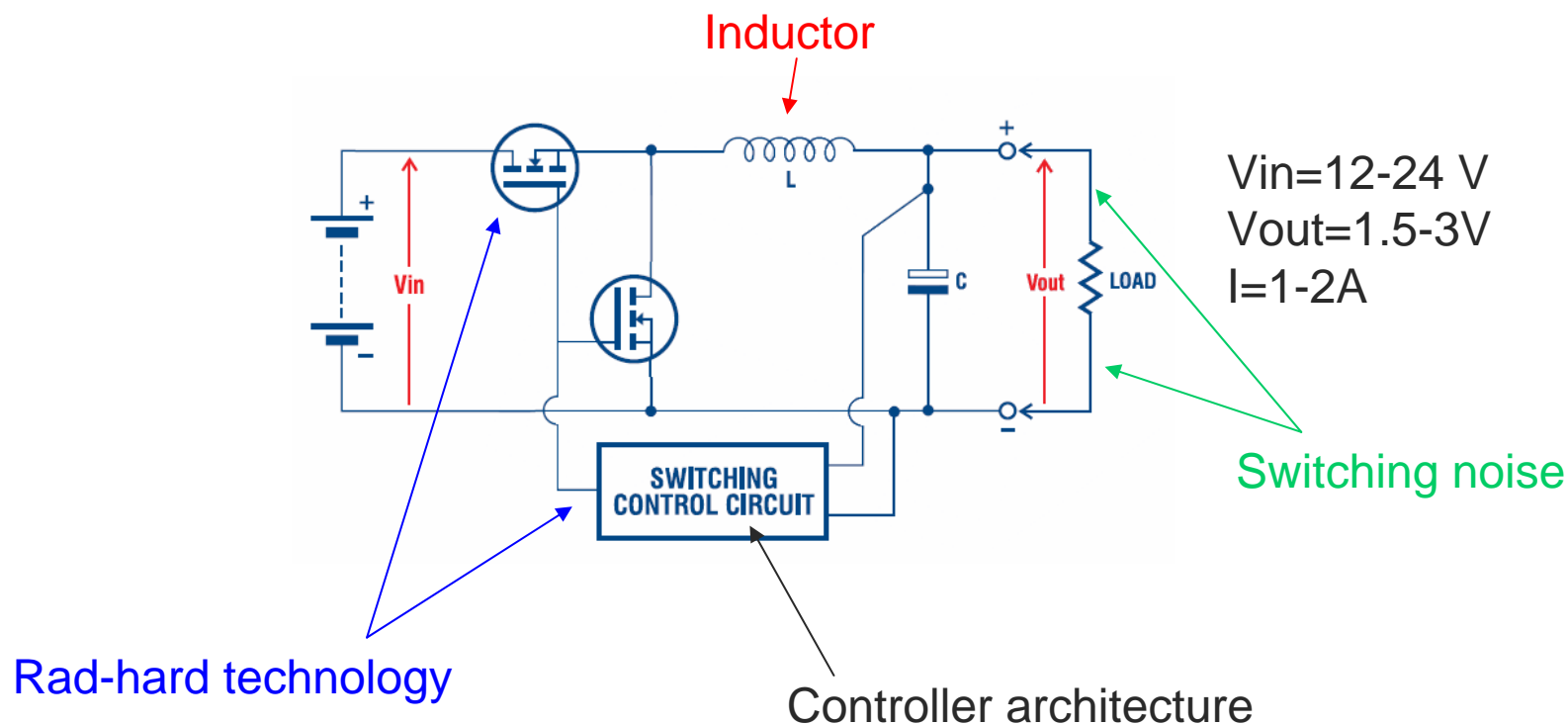
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Low Drop Out regulators (LDO)



DC-DC: Work in progress

- Aiming at demonstrating the feasibility of a fully integrated (except L and passive components) DC-DC buck converter



Selection of a technology

Design and test of transistors in a commercial technology used in automotive applications

Several different transistor topologies available for high-V applications (lateral, vertical)

Layout "modified" to increase radiation tolerance

Comparison between the available MOS transistors

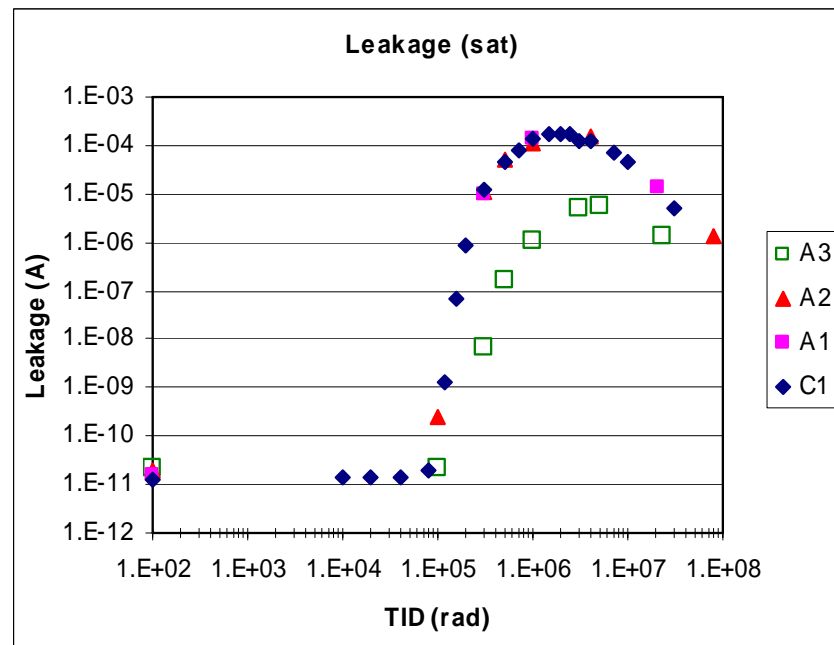
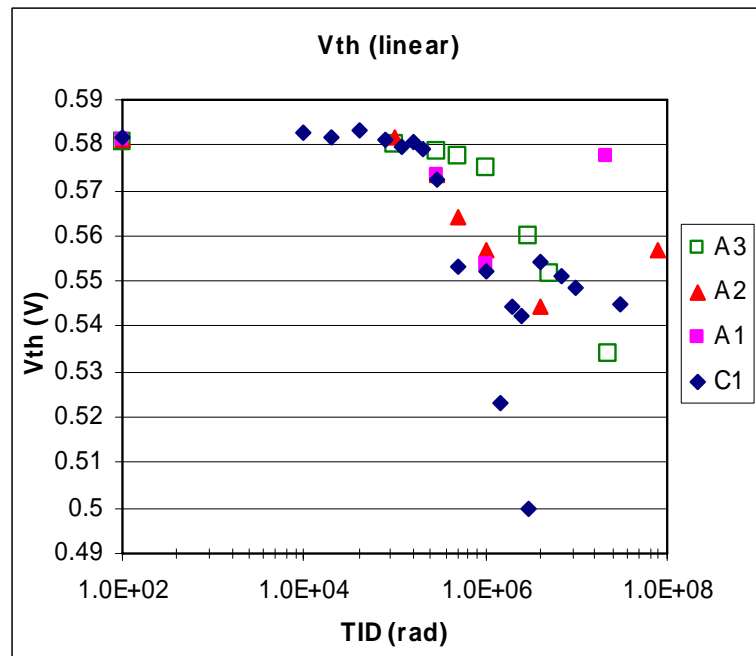
<i>Parameters</i>	<i>NMOS</i>	<i>PMOS</i>	<i>Units</i>
$R_{on} * W @ V_{GS}=3.3V, V_{DS}=0.5V$	25	42	$K\Omega \cdot \mu m$
$C_{gs}/W @ V_{GS}=0V, V_{DS}=0V$	1.5	17.5	fF/ μm
$C_{gd}/W @ V_{GS}=0V, V_{DS}=0V$	8.5	37.5	fF/ μm
$C_{gs}/W @ V_{GS}=0V, V_{DS}=15V$	1.5	17.5	fF/ μm
$C_{gd}/W @ V_{GS}=0V, V_{DS}=15V$	0.125	0.337	fF/ μm

NMOS better performance (lower gate and R_{on} power dissipation)

Difficult to drive in the buck converter configuration (the main switch has the source floating => need of a bootstrap)

NMOS transistors (vertical)

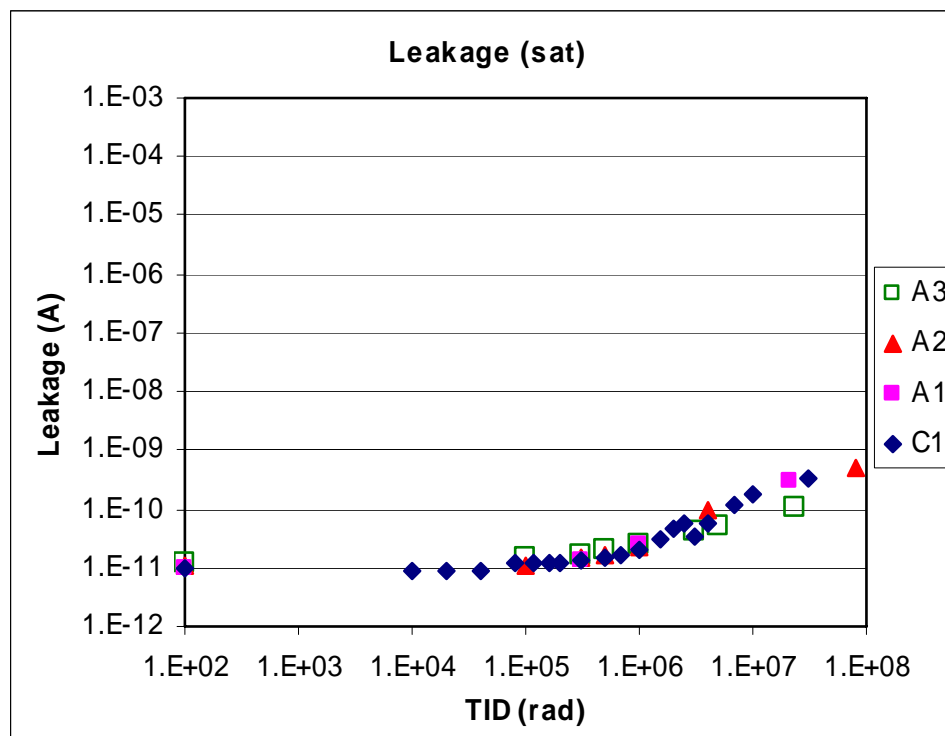
The main radiation-induced problem for the NMOS is the source-drain leakage current. Irradiation in all cases under bias, with $V_{gs}=2$ or $3.3V$ and $V_{ds}=0$ or $14V$.



$V_{ds}=30V$ during measurement

NMOS transistors (vertical)

But leakage current can be effectively controlled with smart layout techniques



Vds=30V during measurement

Inductor core material

Inductor: need of air core inductor because of high magnetic field (up to 4 T for CMS); ferromagnetic materials additionally can distort the static magnetic field

<i>Material</i>	<i>Max. μ</i>	<i>Sat B(T)</i>
<i>Coldrolled steel</i>	<i>2,000</i>	<i>2,1</i>
<i>Iron</i>	<i>5,000</i>	<i>2,15</i>
<i>Purified iron</i>	<i>180,000</i>	<i>2,15</i>
<i>4% Silicon-iron</i>	<i>30,000</i>	<i>2,0</i>
<i>45 Permalloy</i>	<i>25,000</i>	<i>1,0</i>
<i>Hipernik</i>	<i>70,000</i>	<i>1,6</i>
<i>Monimax</i>	<i>35,000</i>	<i>1,5</i>
<i>Permendur</i>	<i>5,000</i>	<i>2,45</i>
<i>2V Permendur</i>	<i>4,500</i>	<i>2,4</i>
<i>Hiperco</i>	<i>10,000</i>	<i>2,42</i>

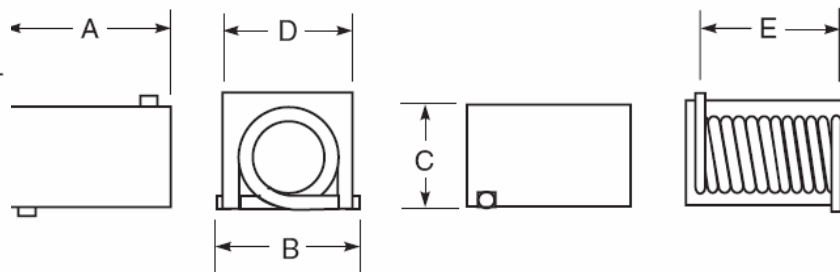
Air-core inductors

Different commercial choices

Coilcraft



Inductance ² (nH)	DCR max ⁵ (mOhm)	I _{rms} ⁶ (A)
90	15	3.5
206	30	3.0
380	50	2.5
538	90	2.0

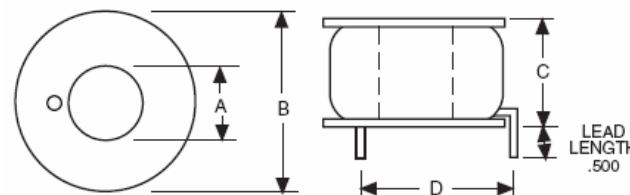


A max	B max	C max	D	E
10,55	6,60	5,97	5,74 ±0,08	7,98 ±0,51

RL-1233

RL-1238, RL-1239
AIR CORE INDUCTORS
BOBBIN WOUND

RL-1233 Renco Part No.	L ±15%* μH	RDC Max. (Ohms)	Suggested RMS Current Rating
RL-1233-0.56	.56	0.006	8.0
RL-1233-1.2	1.2	0.010	8.0
RL-1233-3.3	3.3	0.016	8.0
RL-1233-8.2	8.2	0.026	8.0



A	B	C	D
16mm	30mm	14mm	21mm

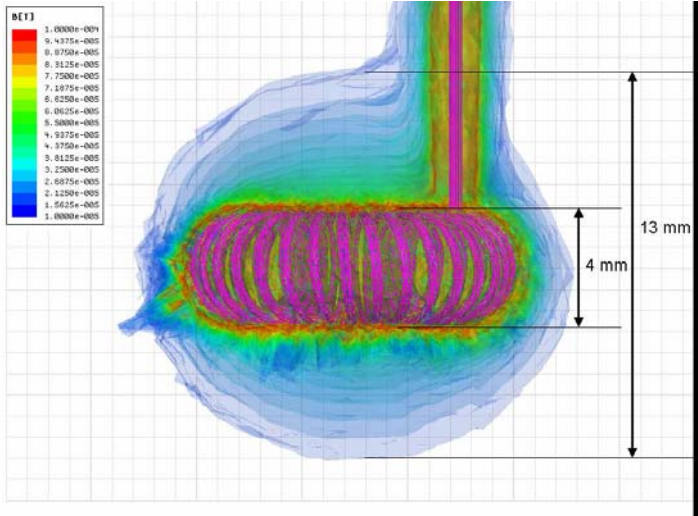
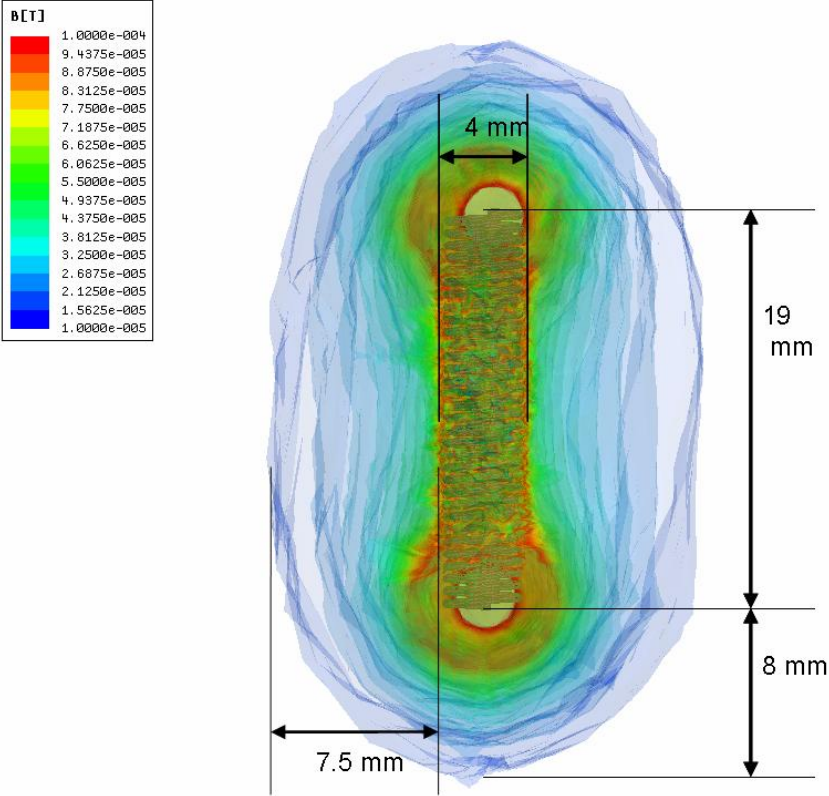
Study of noise implications

Simulation of magnetic field to have a feeling of the physical extension of the field

Hardware implementation of a DC-DC converter based on commercial components (controller, switchers, inductors). Evolutive concept where each component can be replaced by a custom developed one.

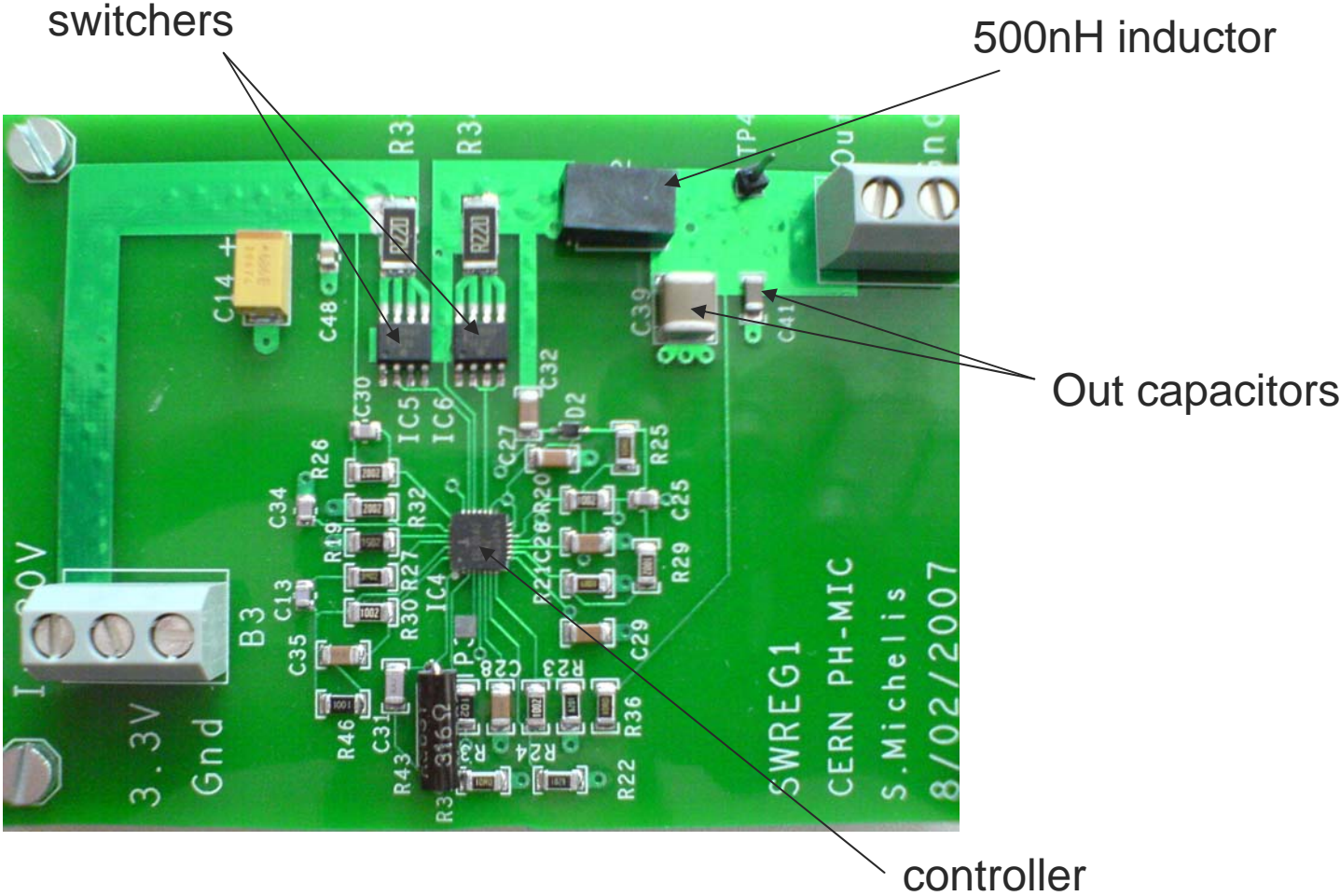
Simulation of magnetic field

Simulation of magnetic field for $I=1A$ in 500nH air core-inductors (solenoid or toroid)



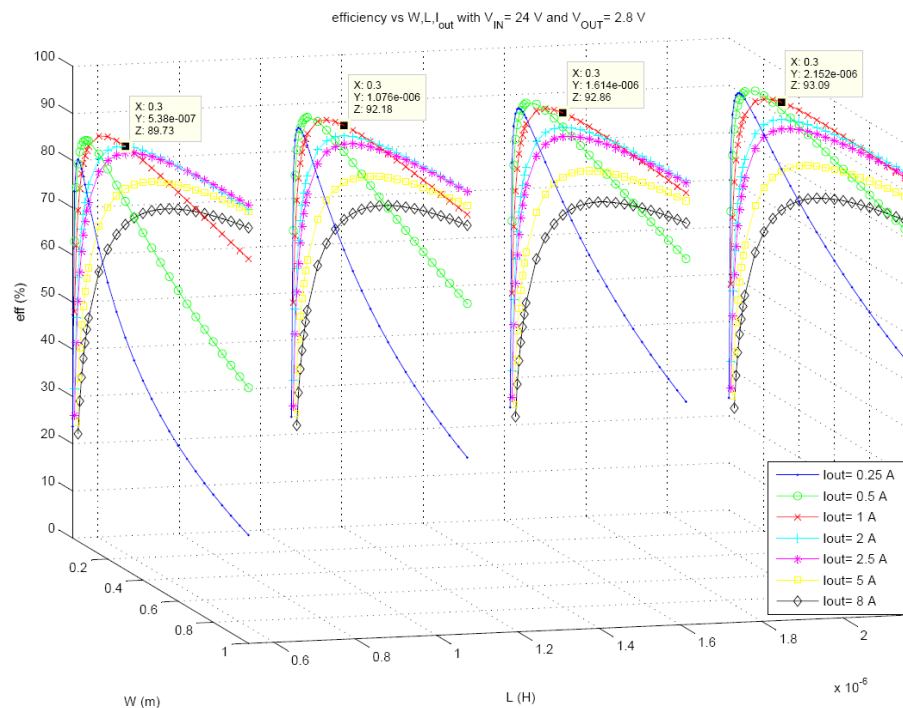
Scale 10-100uT

Hardware implementation



Selection of an architecture for the controller

Evaluation of the losses, and optimization



Review of the adequate architectures and choice

Full-custom implementation in an ASIC

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Design of LDO linear regulator

2 concepts carried on in parallel:

- Stand-alone component (300mA, $V_{out}=1-1.5V$)
- On-chip macro (150mA, $V_{out}=1.2V$)

Both in 130nm CMOS technology, and designed to be radiation tolerant

Macros will be validated and can be modified for different specs

Conclusion

Developments aiming at solving the power distribution problem with integrated components:

- Integrated DC-DC buck converter ($V_{in}=12-24V$, $I=1-2A$)
 - Based on air-core inductor and use of high-V CMOS technology with radiation tolerant design
- LDOs
 - Stand-alone component, $I=300mA$
 - On-chip "IP block"

Work is in progress in both areas, and an R&D programme is being finalized