
Magnet design, final parameters

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EuCARD ESAC review for the FRESCA2 dipole

CERN

28-29 March, 2012



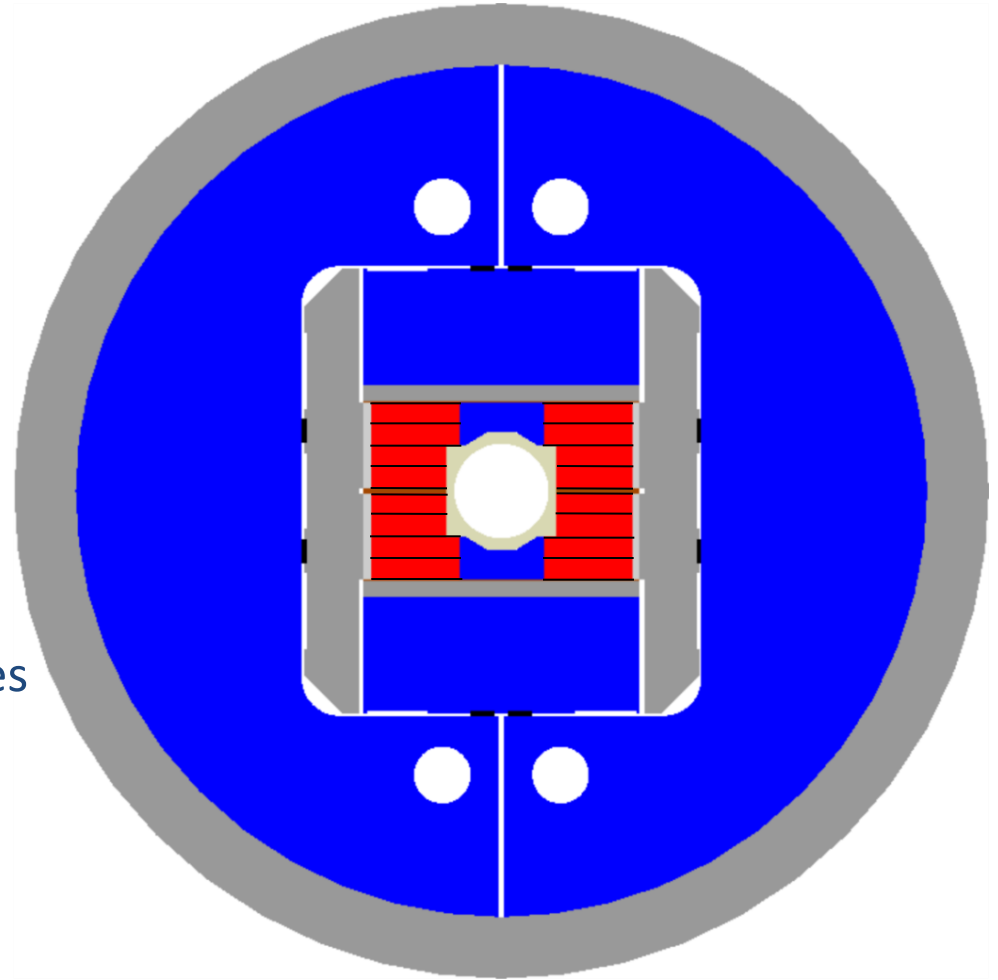
Outline

- Introduction: magnet overview
- Conductor and cable parameters
- Coil design and magnet parameters
- Pre-load and stresses
- End forces and axial support
- Conclusions

Introduction

Overview of magnet design

- OD: 1.030 m
- Al shell, 65 mm thick
- Iron yoke
 - Holes for axial rods
- Horizontal s.s. pad
 - 3 bladders, 75 mm wide
 - 2 load keys
- Vertical iron and s.s. pad
 - 2 bladders, 60 mm wide
 - 2 load keys
- Auxiliary bladders between yokes
- Four double-layer coils
- Iron and Ti alloy central posts
- 100 mm aperture
- Target bore field: 13 T

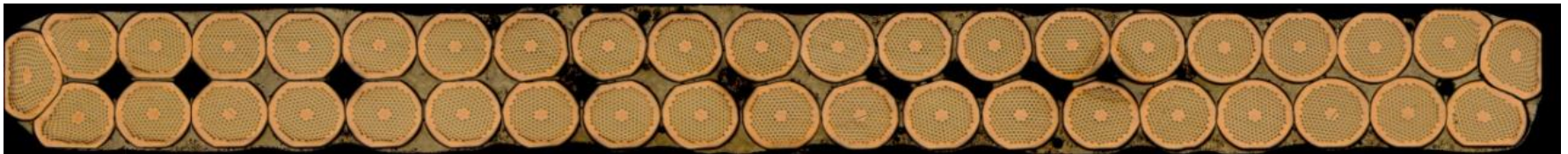
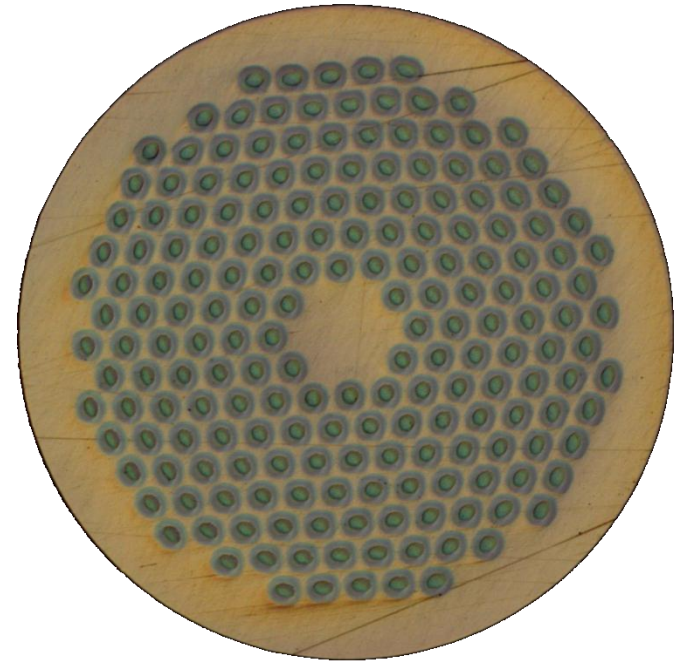


Conductor and cable parameters

- Strand diameter: 1 mm
- Cu/Sc: 1.25 → 56% Cu
- Strand #: 40
- Bare width after cabling: **20.900** mm
- Bare thickness after cabling: **1.860** mm

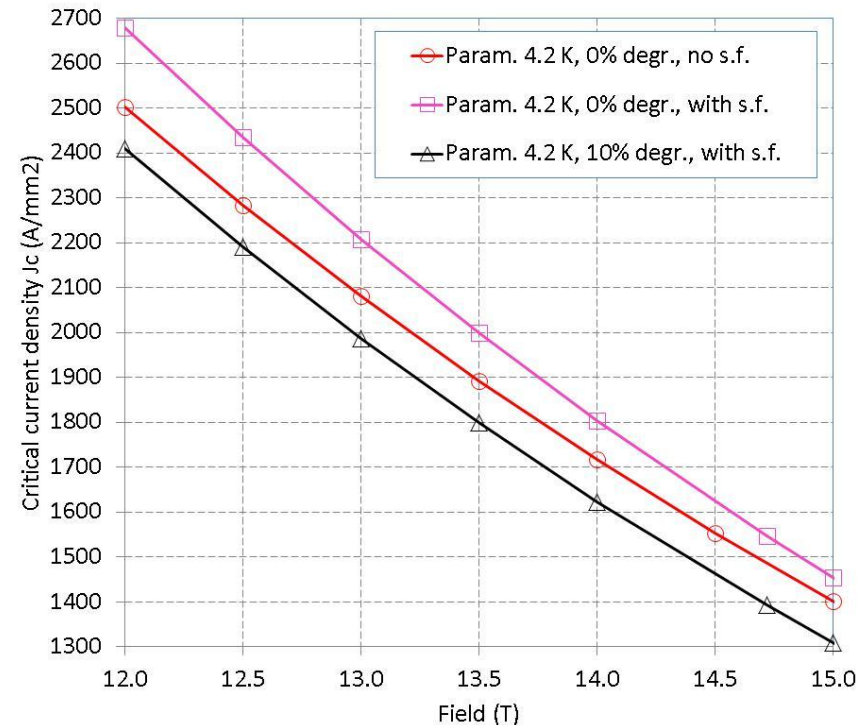
- Insulation: 0.200 mm

- Assumed growth during HT
 - 4% in thickness and 2% in width
- Bare width after HT: **21.400** mm
- Bare thickness after HT: **1.934** mm



Conductor and cable parameters

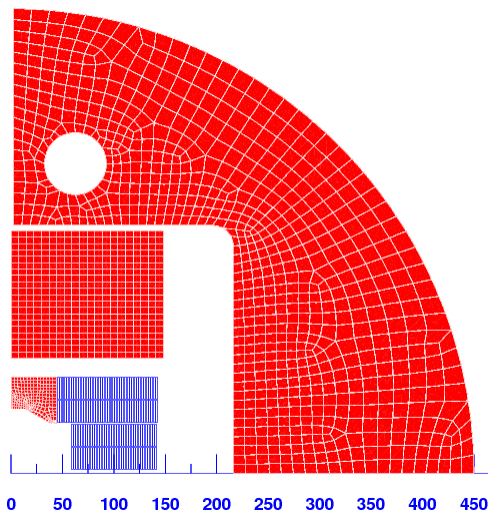
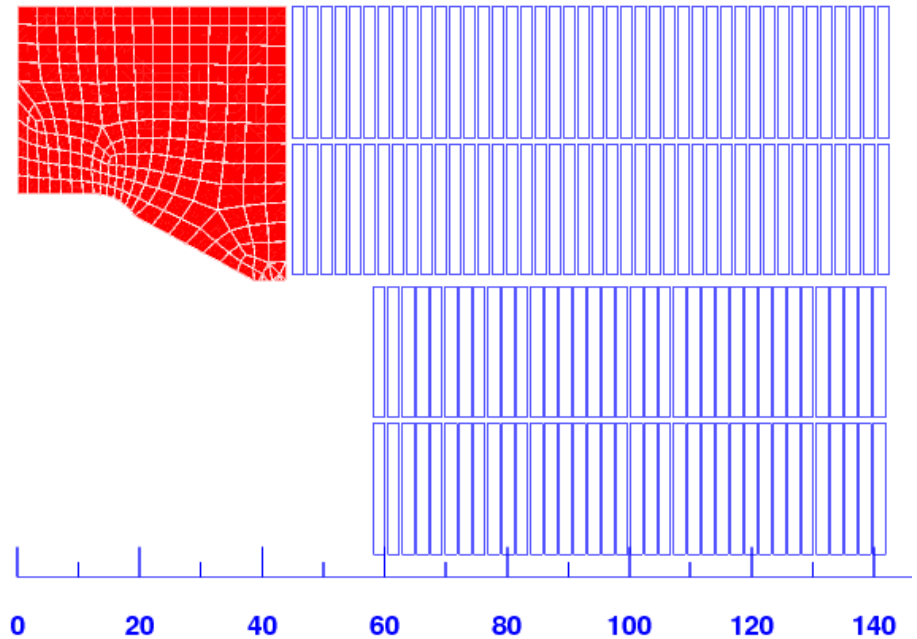
- J_c of virgin strand (4.2 K) from short-sample measurements
 - 2500 A/mm² at 12 T
 - 1400 A/mm² at 15 T
- Self field corr. of 0.41 T/kA (by B. Bordini)
- 10% cabling degradation
- Resulting J_c for computations
 - 2400 A/mm² at 12 T
 - 1300 A/mm² at 15 T



2D magnetic analysis

Coil cross-section

- Two double-layers with 36 and 42 turn
- Iron pole in layer 3-4
- 3.5 mm mid-plane shim
- 1.5 mm inter-coil gap
- 0.5 mm inter-layer shim

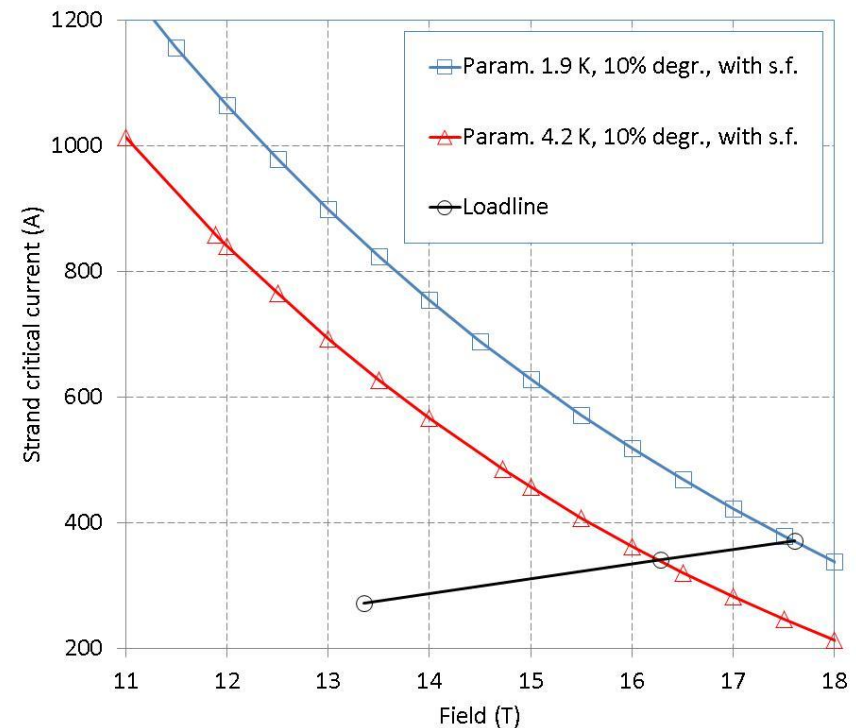


- Coil aperture 116 mm, bore 100 mm
- Iron yoke with OD of 0.9 m
- Iron filler
- S.S. horizontal pads

2D magnetic analysis

Magnet parameters

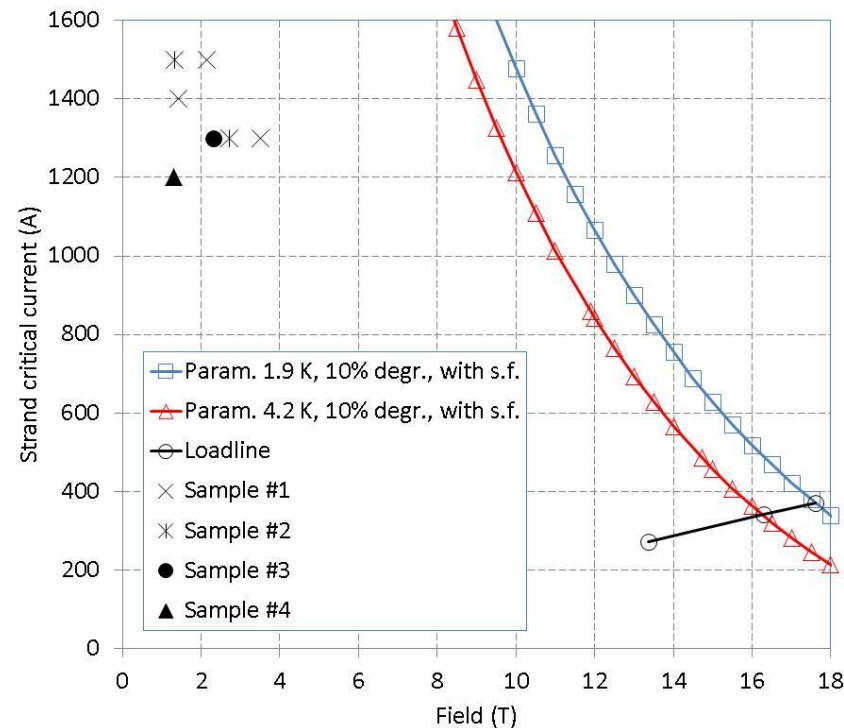
- Short sample conditions
 - 4.2 K, I_{SS} : 13.6 kA
 - B_{bore} : 15.8 T
 - B_{peak} : 16.4 T
 - 1.9 K, I_{SS} : 14.9 kA
 - B_{bore} : 17.0 T
 - B_{peak} : 17.6 T
 - Strain during loading/excitation not included
- Operational conditions
 - 13 T bore field
 - I_{op} : 10.9 kA
 - B_{peak_op} : 13.4 T
 - 80% of I_{SS} at 4.2 K
 - 73% of I_{SS} at 1.9 K



2D magnetic analysis

Magnet parameters

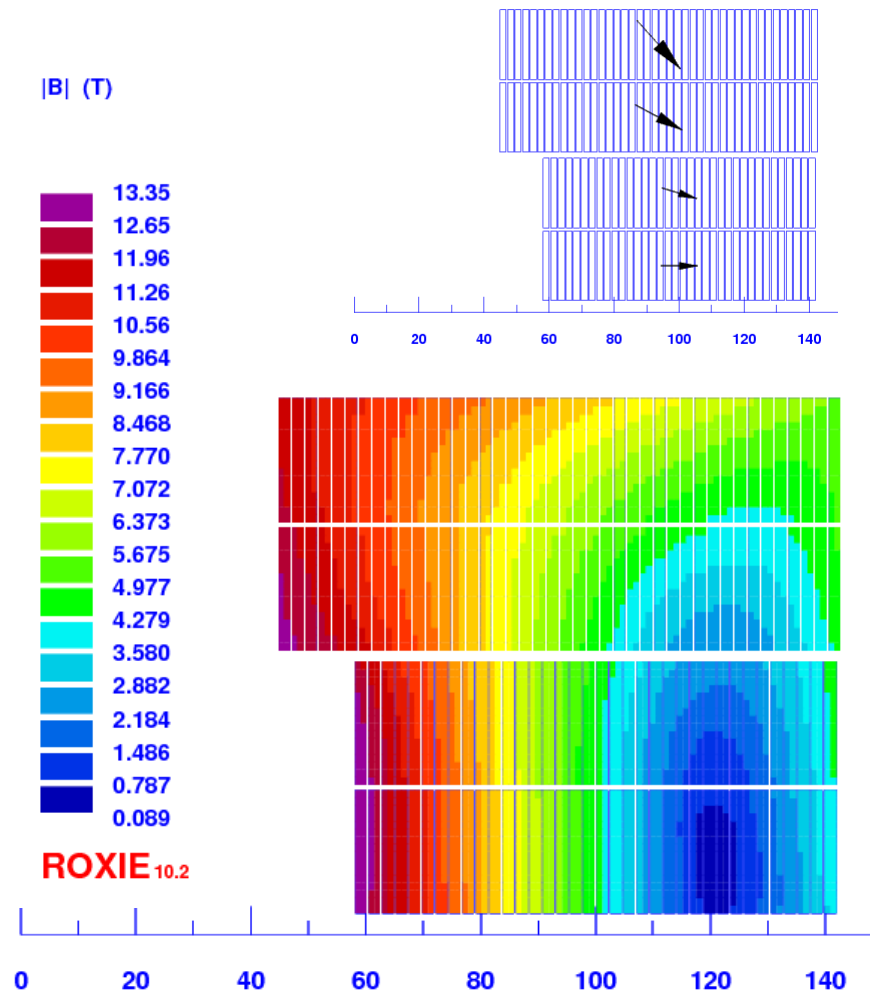
- Stability current I_s a factor of 3 higher than maximum strand current at short sample cond.



2D magnetic analysis

Magnet parameters

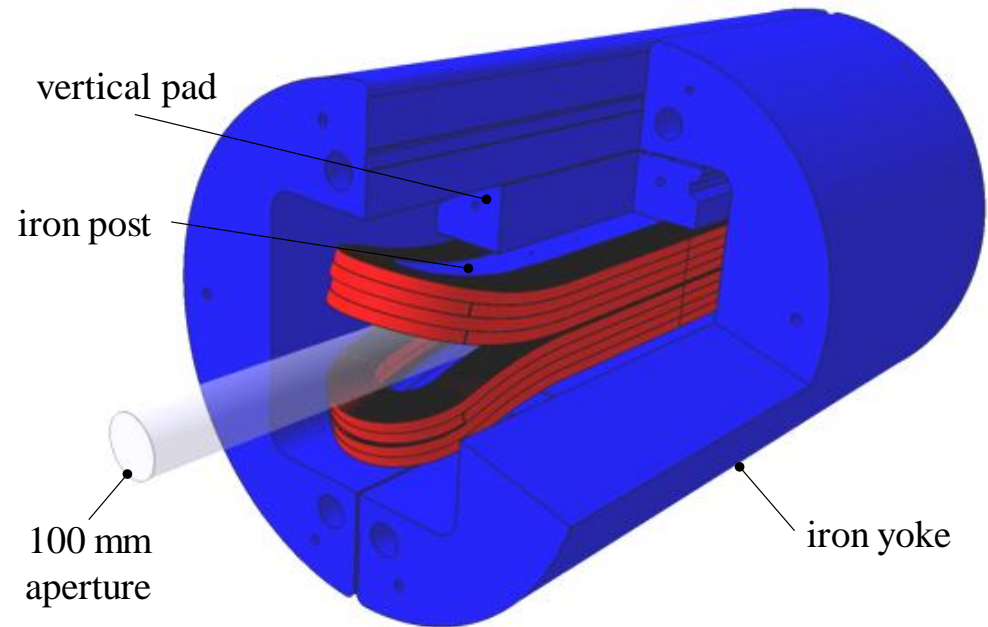
- Peak field in layer 1
 - Layer 2 with field 1% lower
- Margin in L3 and L4
 - From 3 to 9 %
- Field quality at 2/3 of aperture
 - <1% homogeneity
 - ~70 units of b_3 , ~30 of b_5
- E.m. forces directed outwardly
 - Lorentz stress
 - Ranging from 80 MPa in L12 to 100 MPa in L34
 - 150 MPa with 15 T bore field



3D magnetic analysis

Coil design

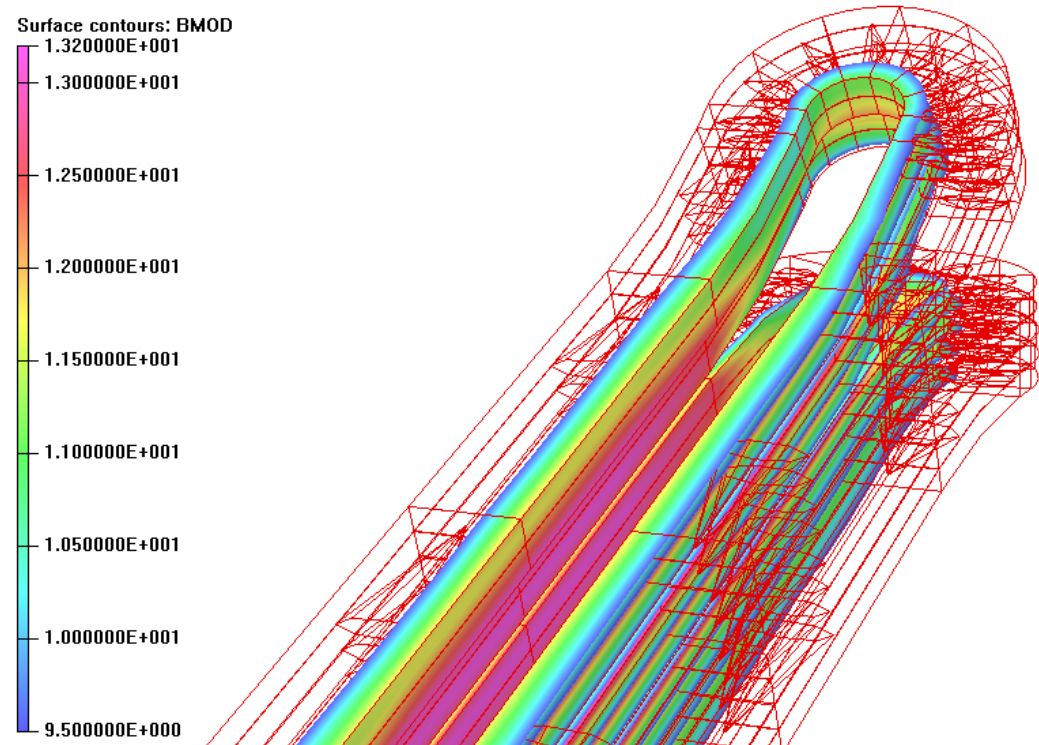
- 730 mm of total straight section
- Hard-way bend with minimum radius of 700 mm
- Inclined straight section (17 degr.) of about 30 mm
- Overall coil length of 1.5 m
- Iron parts
 - Winding post in L34
 - Vertical pad over straight section
 - Full length yoke



3D magnetic analysis

Magnet parameters

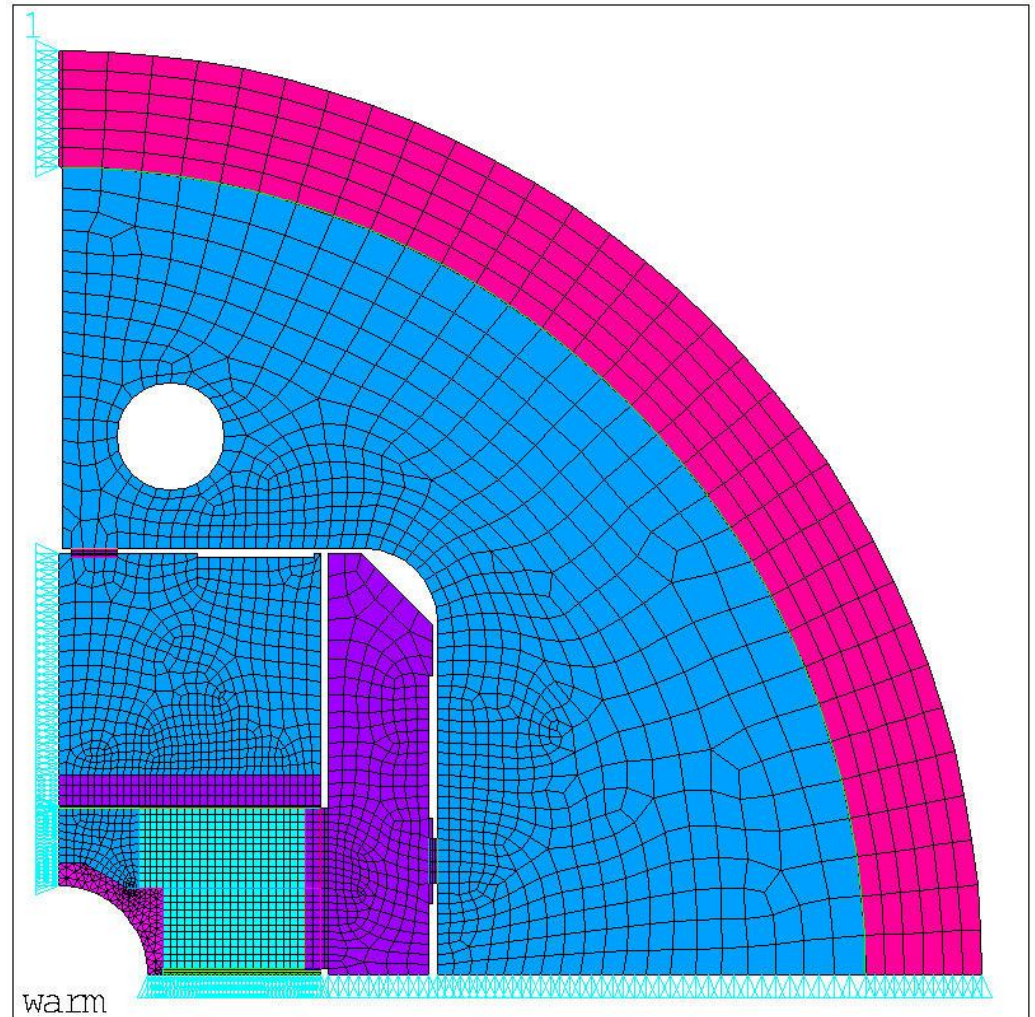
- 10% (about 1.5 T) of margin in the ends
- 1% uniformity of B_y over 540 mm along z
- Stored energy
 - FRESCA2 (13 T): **3.8 MJ**
 - HD2 (13 T): 0.6 MJ
 - LQ (240 T/m): 1.4 MJ
 - HQ (170 T/m): 0.8 MJ
- Stored energy density (J/cm^3 of coil)
 - FRESCA2 (13 T): **80 J/cm^3**
 - HD2 (13 T): 78 J/cm^3
 - LQ (240 T/m): 101 J/cm^3
 - HQ (170 T/m): 97 J/cm^3



2D mechanical analysis

Load sequence and assumptions

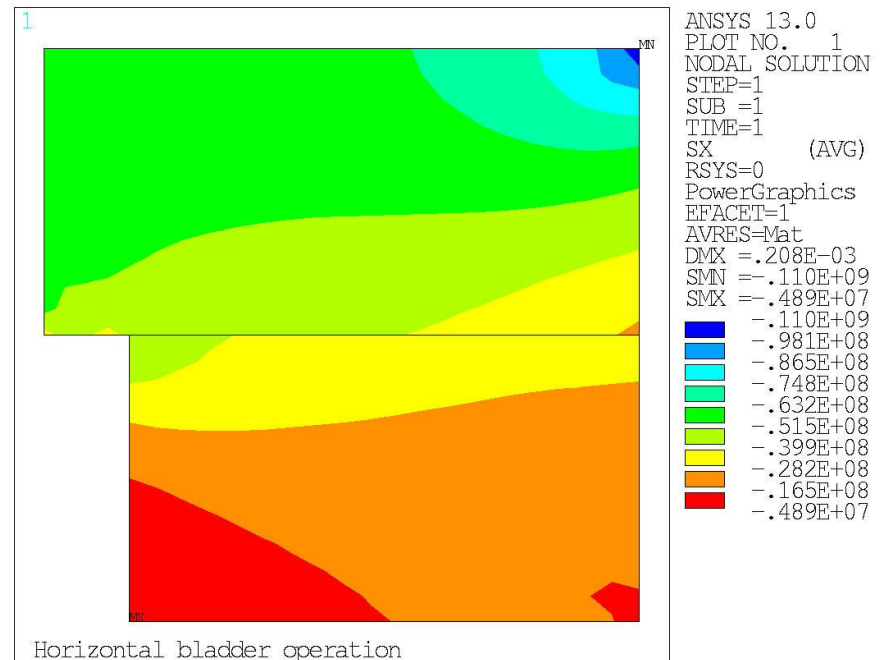
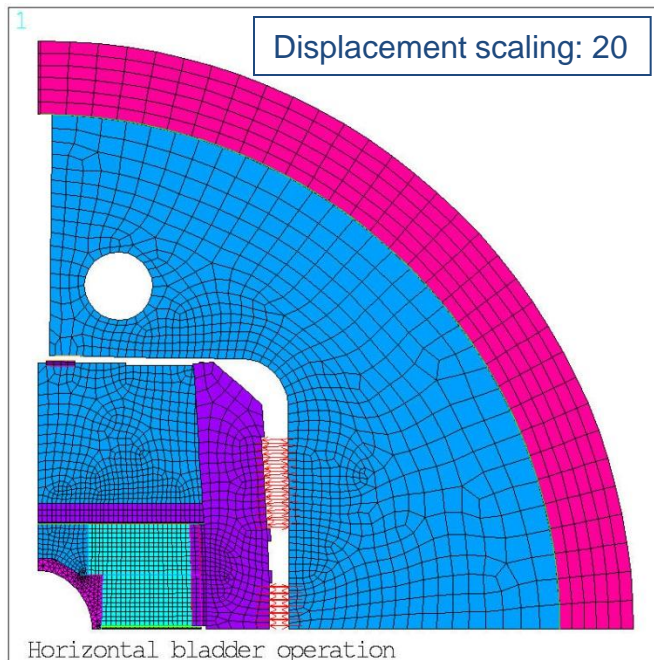
1. Bladders inflated to open clearance between pads and yoke
 2. Load key shimmed
 3. Bladder deflated to lock the keys
 4. Cool-down
 5. E.m. forces
- Coil pre-load to **prevent separation/tension** between pole turn and post with e.m. forces
 - 0.2 friction between component
 - Coil parts bonded



2D mechanical analysis

Bladder operation

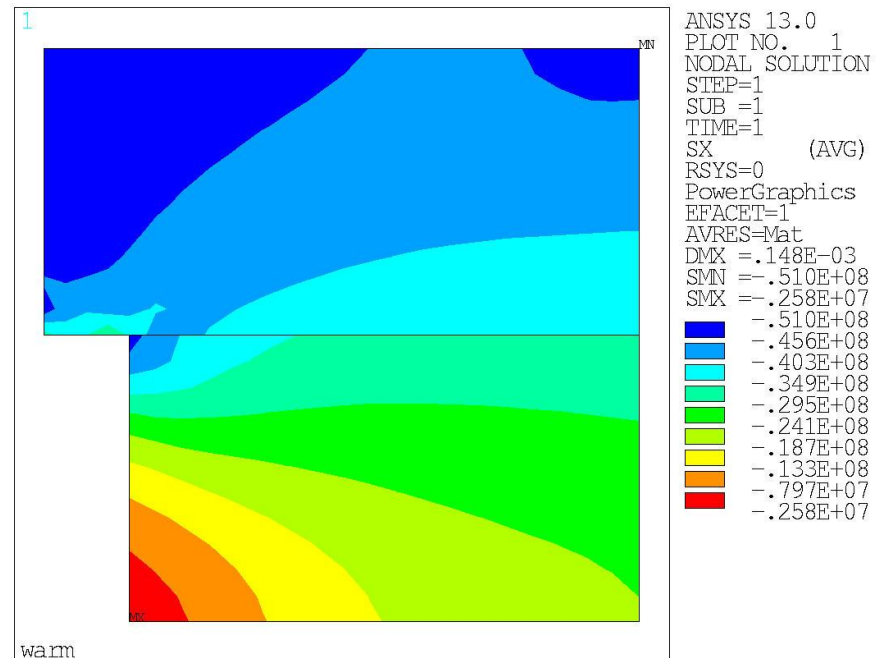
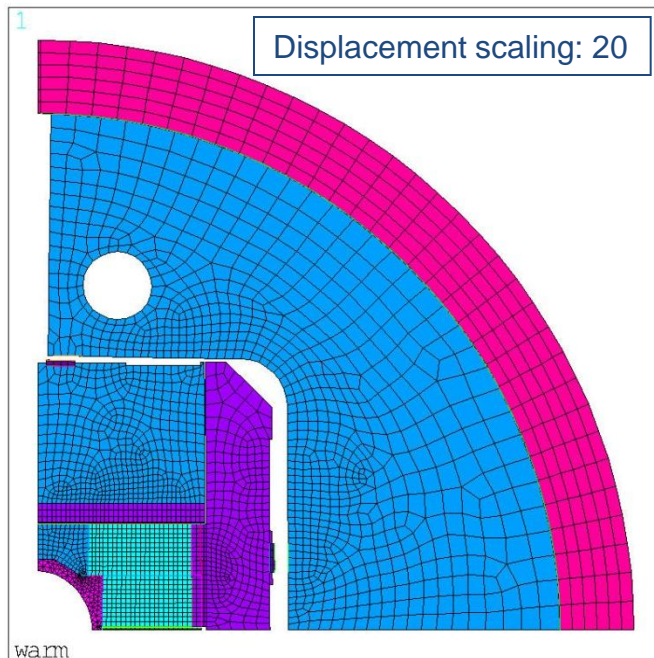
- Clearance of 0.7 mm created by horizontal bladders pressurized to about 30-40 MPa
- Coil peak stress ~ 100 MPa
 - Mainly due to bending of horizontal pad



2D mechanical analysis

Key insertion

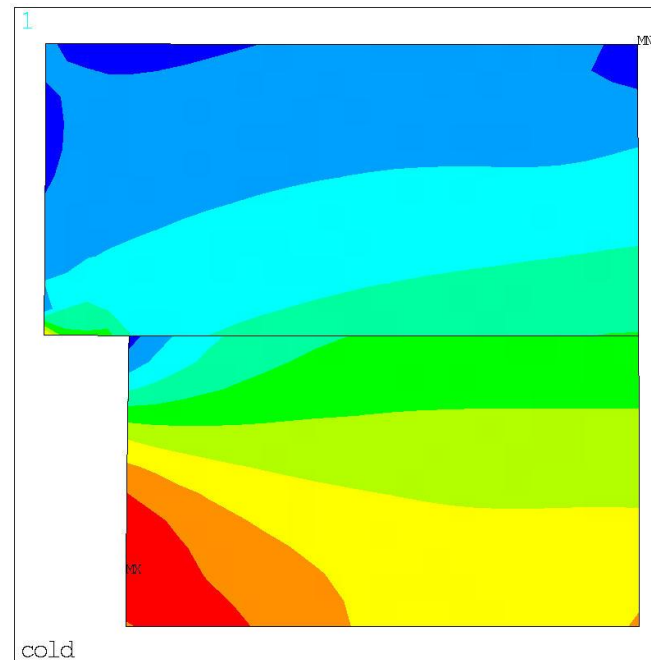
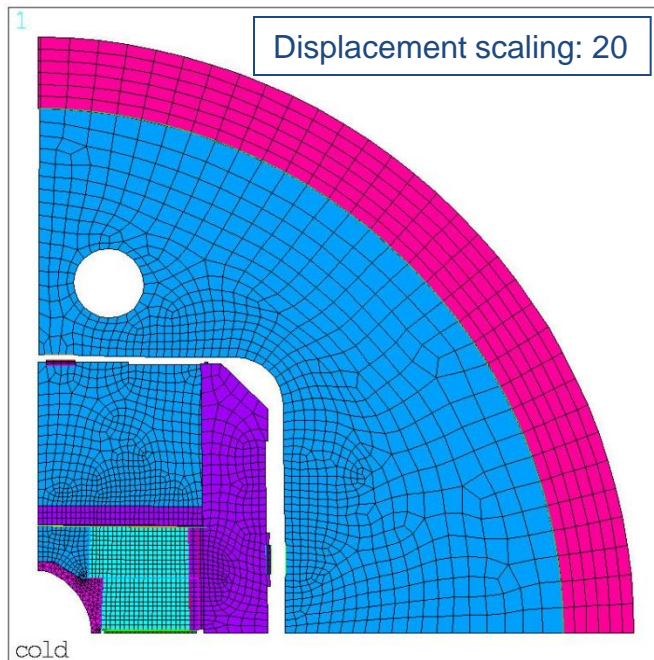
- Insertion of a shim in hor. load keys of about 0.6 mm
- Coil peak stress reduced to ~ 50 MPa
 - No pad bending \rightarrow more uniform pre-load from



2D mechanical analysis

Cool-down

- Increase of average shell stress from 50 to 150 MPa
- Coil peak stress ~ 130 MPa
 - Deformation of L12 post

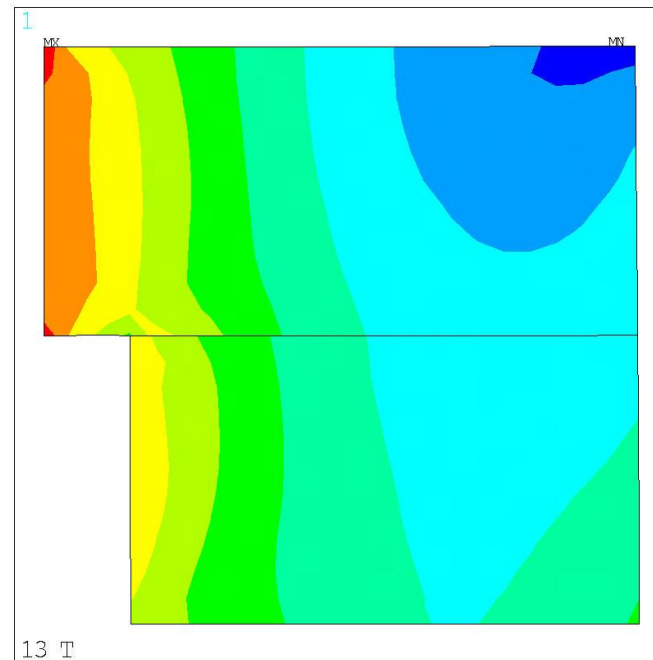
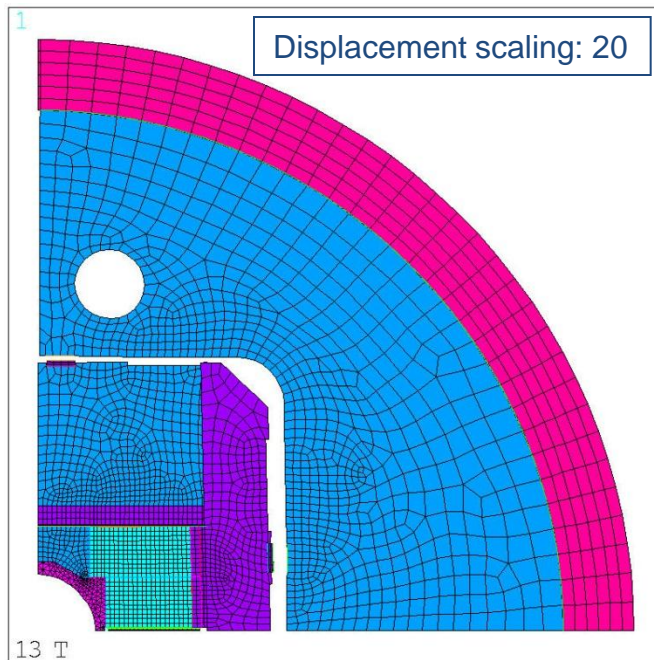


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PLOT NO. 1
NODAL SOLUTION
STEP=2
SUB =1
TIME=2
SX (AVG)
RSYS=0
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.745E-03
SMN =-.130E+09
SMX =-.242E+08
■ -.130E+09
■ -.118E+09
■ -.106E+09
■ -.945E+08
■ -.828E+08
■ -.710E+08
■ -.593E+08
■ -.476E+08
■ -.359E+08
■ -.242E+08
```

2D mechanical analysis

Excitation

- Coil pole turns still in contact with posts
- Coil peak stress <150 MPa
 - Maximum stress moved to low field region

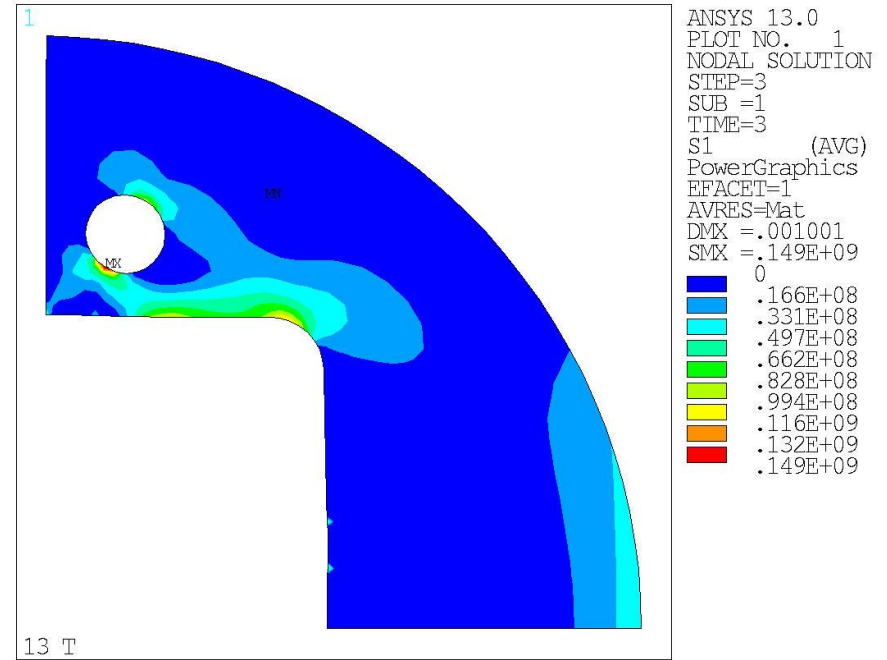
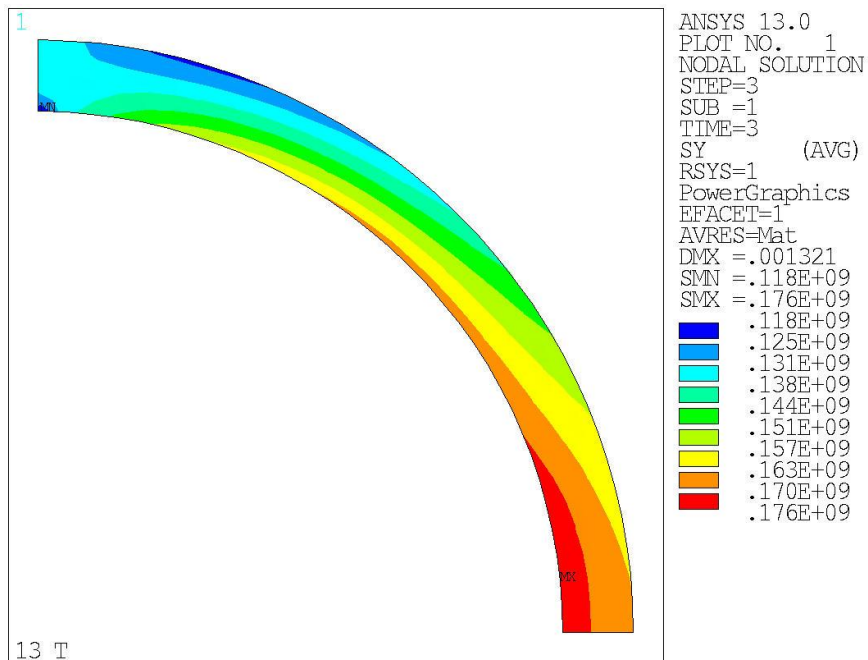


```
ANSYS 13.0
PLOT NO. 1
NODAL SOLUTION
STEP=3
SUB =1
TIME=3
SX (AVG)
RSYS=0
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.684E-03
SMN =-.147E+09
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2D mechanical analysis

Stress in the support structure

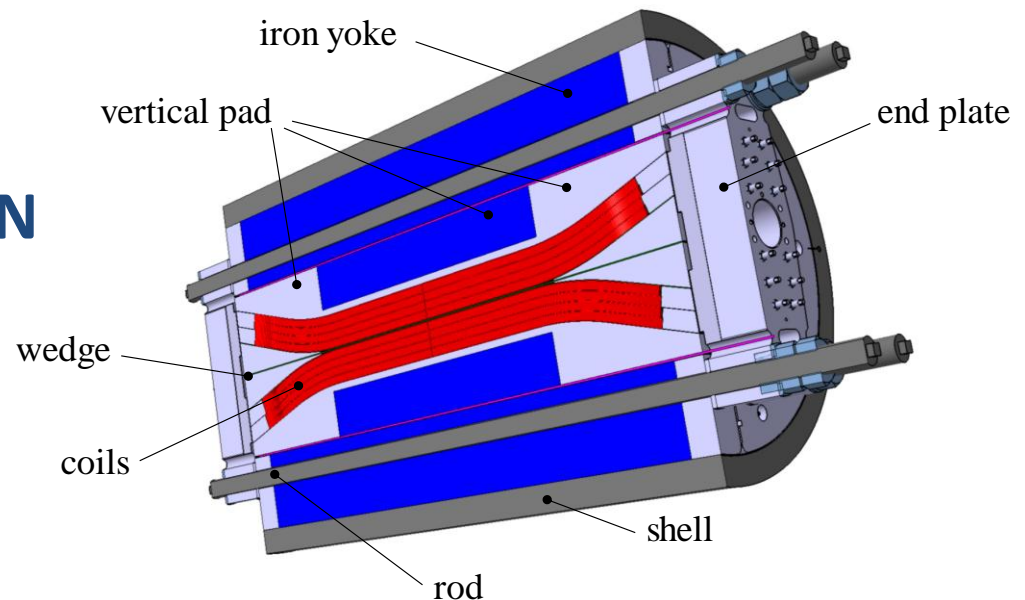
- Peak shell stress: from 70 to 180 MPa
- Maximum tensional stress in the iron: 150 MPa
- All other components within yield stress limits



3D mechanical analysis

Support structure design

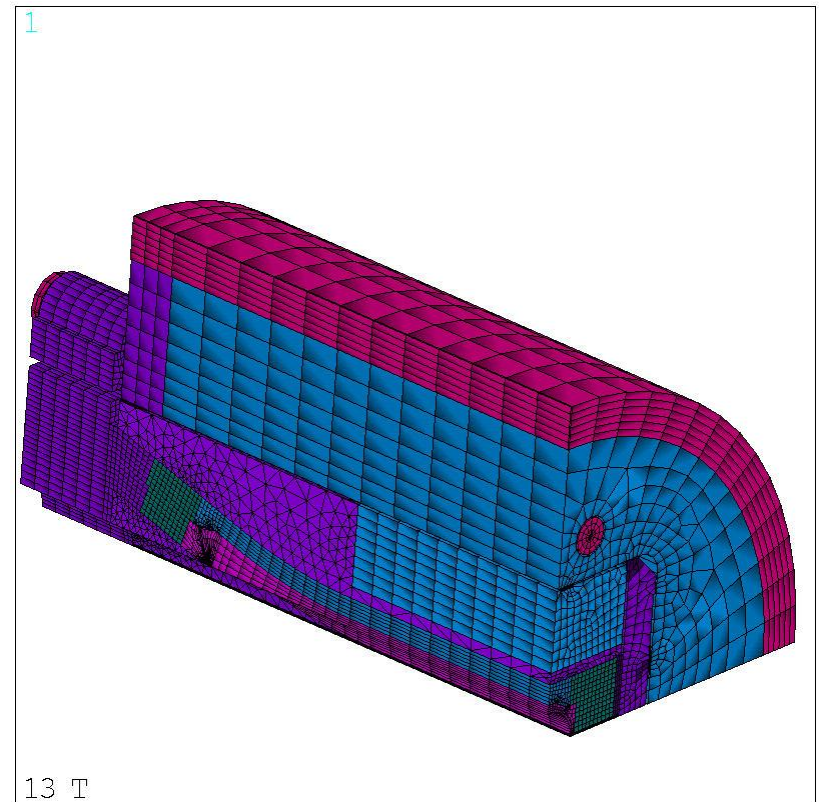
- Axial support composed by
 - Aluminum rods with a diameter of 60 mm
 - Nitronic 50 end plate 150 mm thick
 - Bullets to deliver pre-load to end-shoes and wedge
- Axial force
 - FRESCA2 (13 T): **2.8 MN**
 - HD2 (13 T): 0.7 MN
 - LQ (240 T/m): 0.5 MN
 - HQ (170 T/m): 0.8 MN



3D mechanical analysis

Load sequence and assumptions

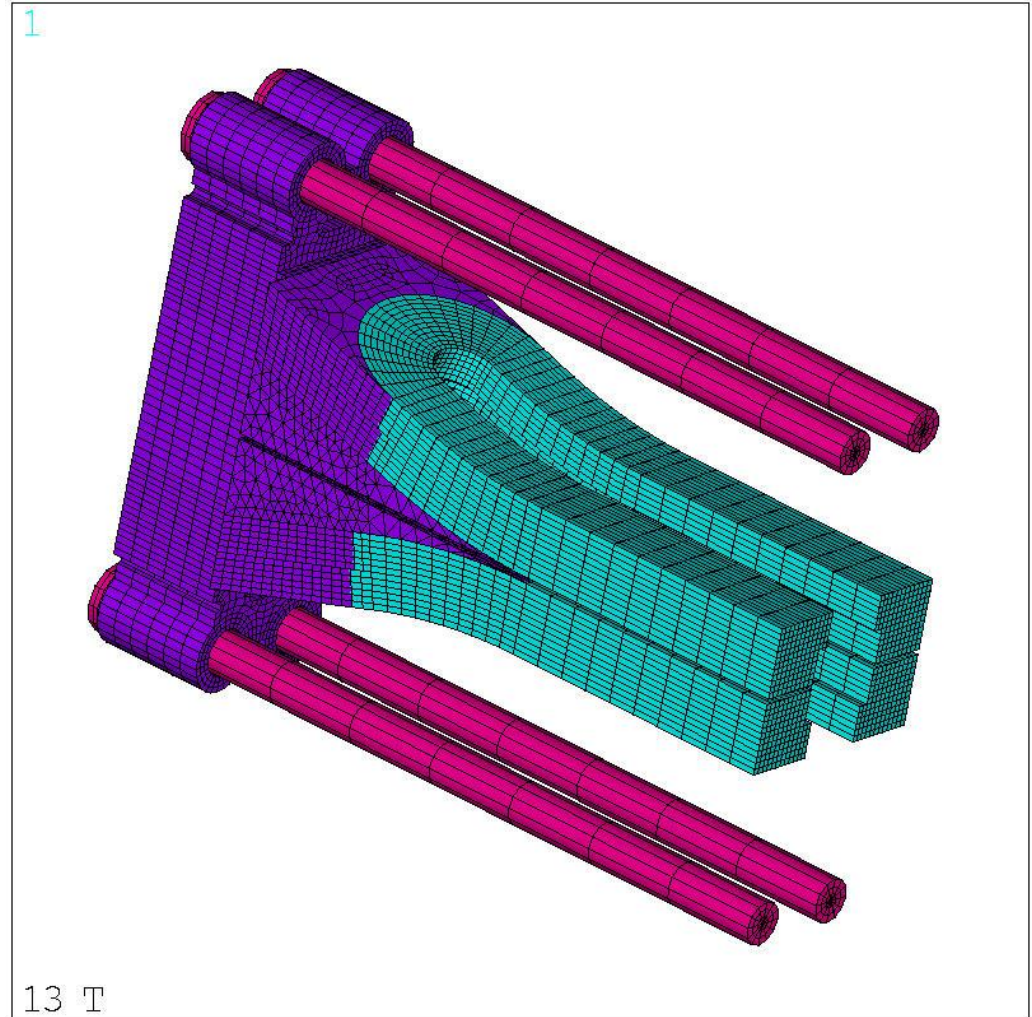
1. Piston system to pre-tension axial rods
 2. Rod nuts torqued
 3. Piston system released
 4. Cool-down
 5. E.m. forces
- Coil axial pre-load to **prevent separation/tension** between pole turn and post with e.m. forces
 - 0.2 friction between component
 - Coil parts bonded



3D mechanical analysis

Axial pre-load

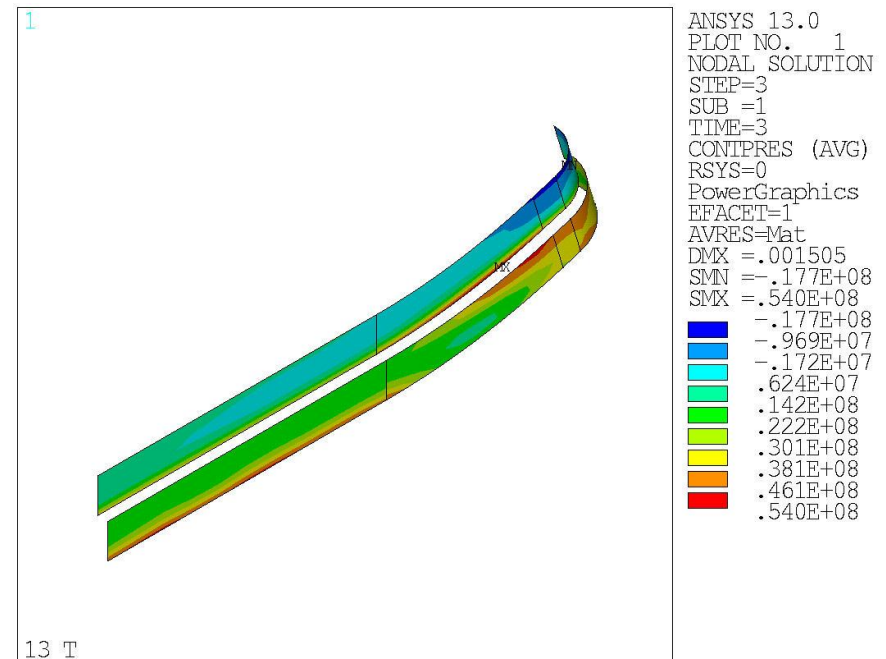
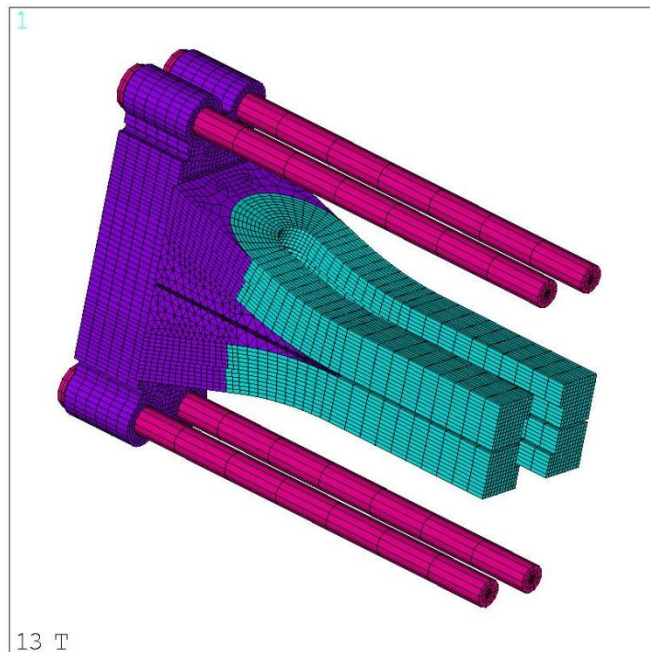
- E.m. axial force
 - 2.8 MN
- Room temperature pre-load
 - Rod stress: 150 MPa
 - 1.7 MN
 - Provided by 150-200 t piston
- 4.2 K pre-load
 - Rod stress: 260 MPa
 - 2.8 MN
 - Provided to end-shoes and wedge (glued)



3D mechanical analysis

Contact pressure coil-pole

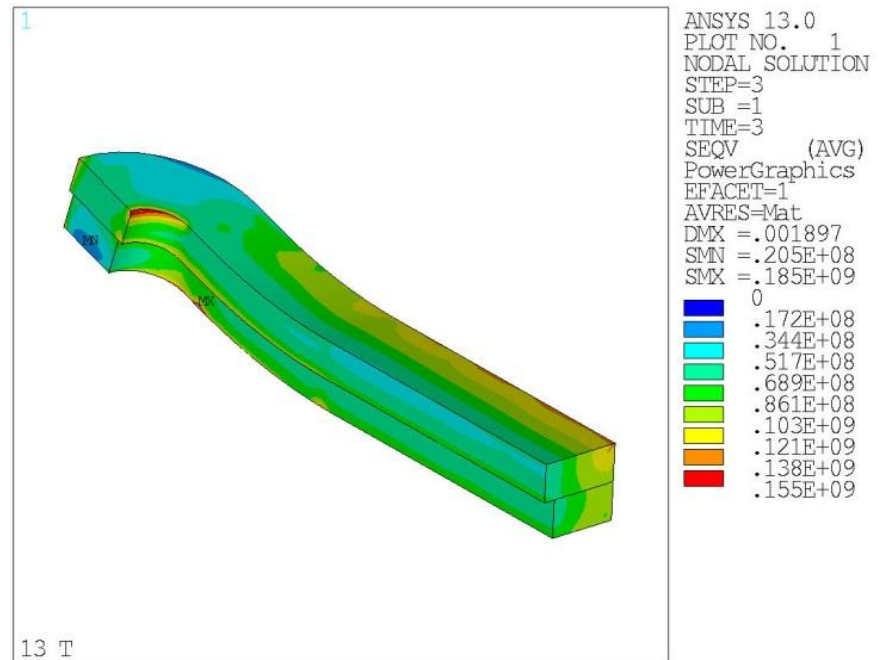
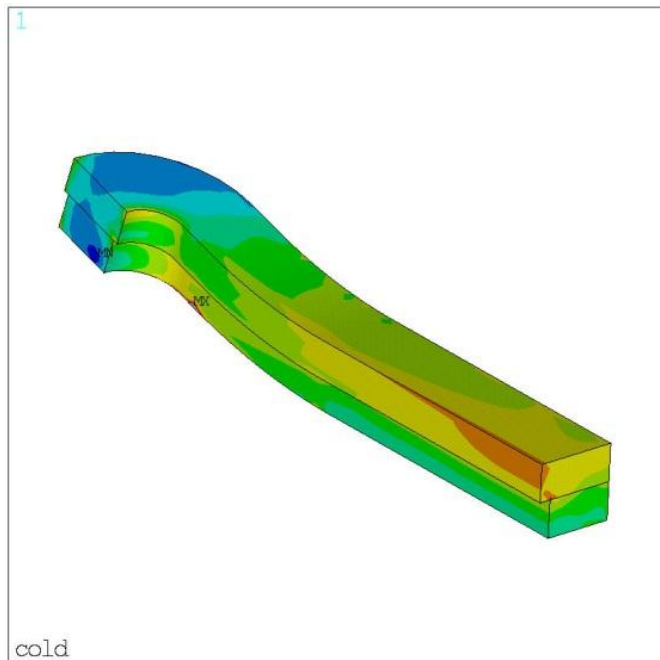
- Contact pressure (or tension <20 MPa) between pole turn and pole pieces
 - From straight section to hard-way and easy-way bent



3D mechanical analysis

Stress in the coil

- Von Mises stress in the coil <150 MPa after cool-down and with e.m. forces



Conclusions

- 2D and 3D magnetic and mechanical analysis performed
 - Updated computations with cable growth during reaction and recent extracted strand measurements
- Operational conditions: 13 T bore field
 - 80% of I_{ss} at 4.2 K
 - 73% of I_{ss} at 1.9 K
 - Large magnetic stability margin
- Coil peak stress below 150 MPa during all magnet operations
- Support structure capable of providing full pre-load (up to 15 T) in straight section, ramp, and end region

Appendix



3D mechanical analysis

Stress in axial support components

- Stress in axial rod (aluminum) and end-plate (Nitronic 50) within yield stress limits

