

CONCEPTUAL DESIGN OF THE BETA = 0.86 CAVITIES FOR THE SUPERCONDUCTING LINAC OF ESS

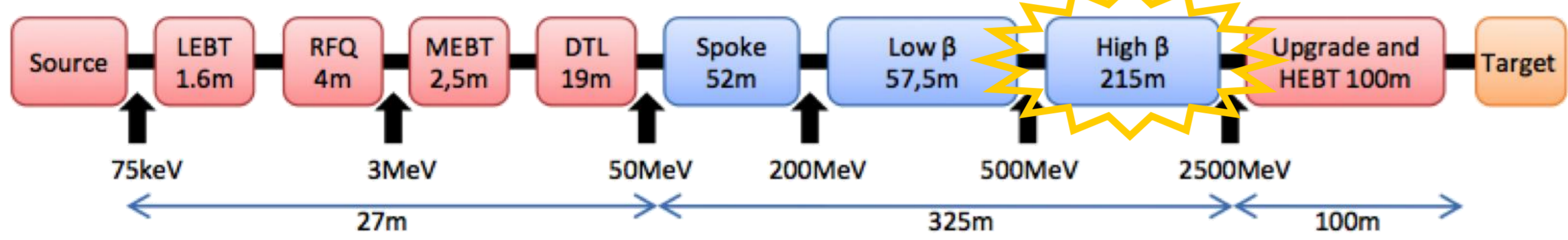
G. Devanz, J. Plouin, CEA-Saclay, 91191 Gif-sur-Yvette, France



CEA-Saclay is in charge of the design, the fabrication and the tests of the superconducting high beta cavities for the high energy part of the ESS (European Spallation Source) linac. This paper reports the actual status of the RF and mechanical design of these cavities. According to ESS specifications, these cavities will be 5-cells elliptical, with frequency 704 MHz and $\beta = 0.86$. They will work in the pulsed mode, with a beam current initially equal to 50 mA.

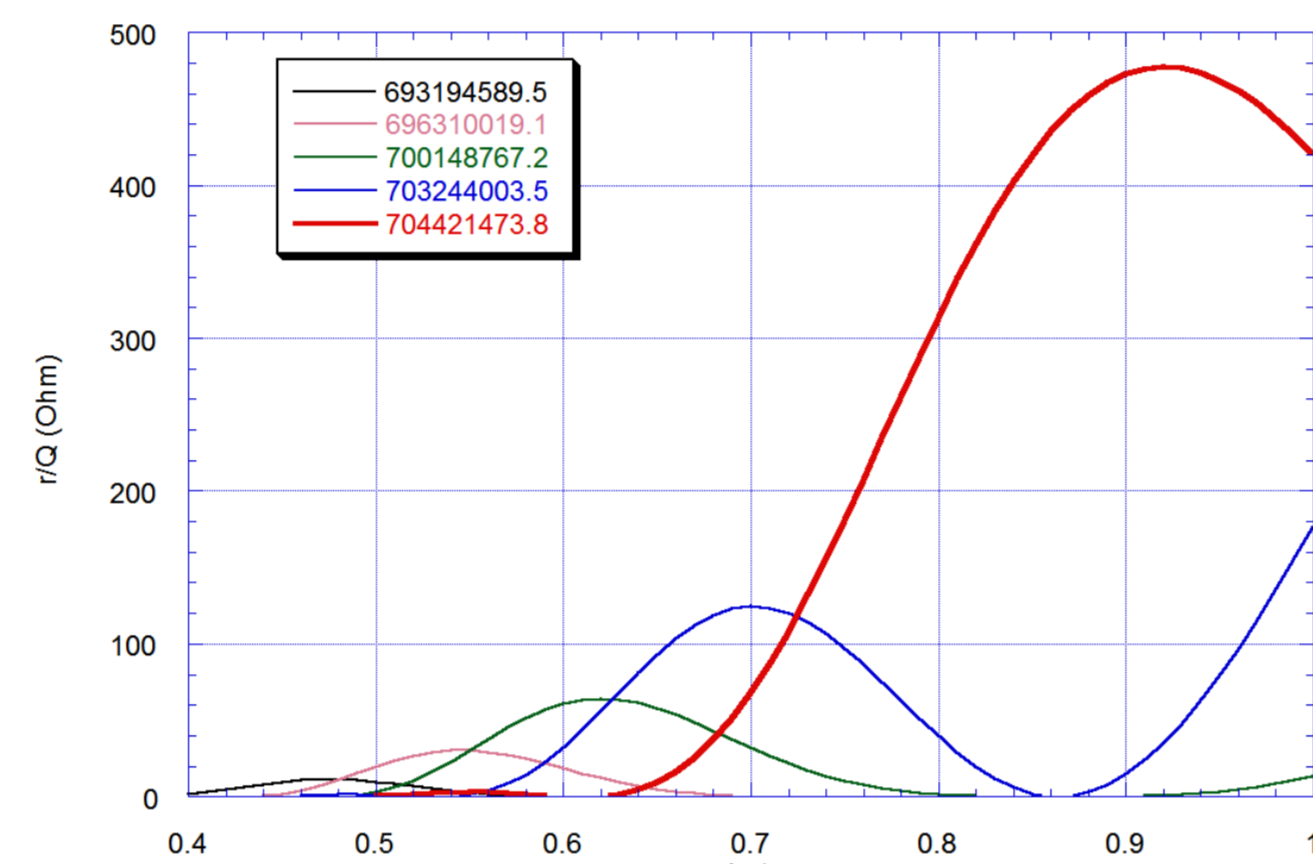
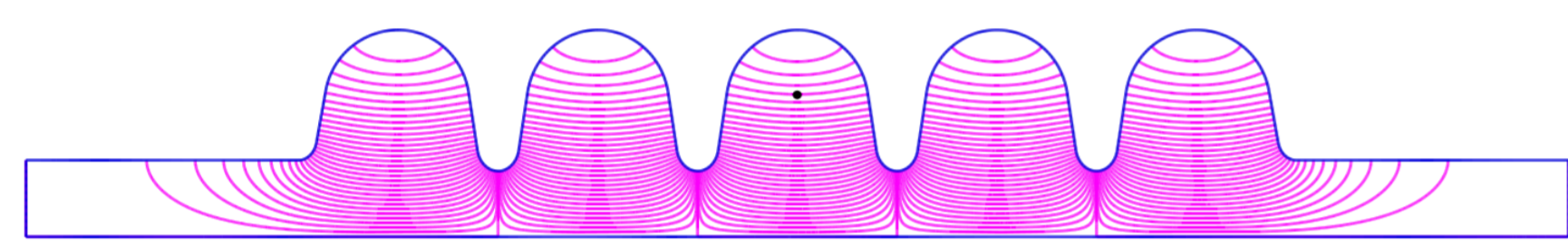


The target accelerating gradient is 18 MV/m on the linac, and 20 MV/m in vertical tests. For the RF design, the cavity efficiency and the peak fields were optimized, while the feasibility of the external coupling with RF power was taken into account. Attention was also paid to the HOM frequencies and impedances and to their future extraction. Coupled RF/mechanical FEM calculations have been carried out and the Lorentz detuning, critical for a pulsed mode cavity, is lowered by the insertion of stiffening rings.

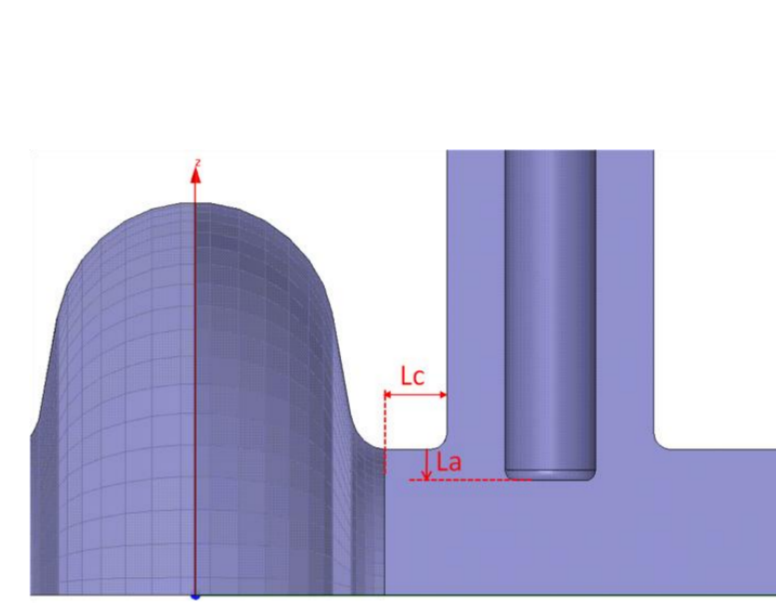
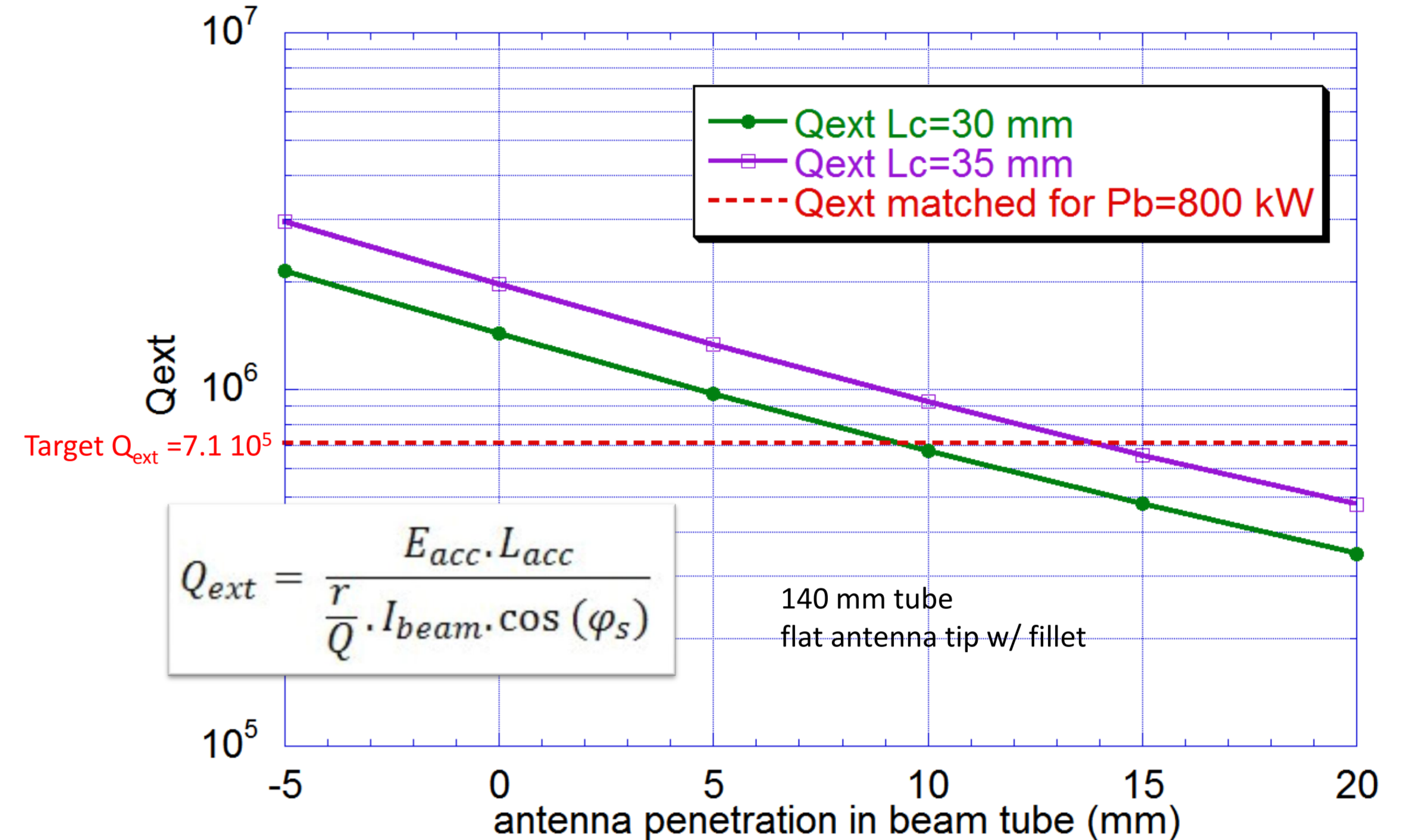


ESS DESIGN PARAMETERS	
RF frequency	704.42 MHz
Cavity geometrical beta	0.86
Operating Temperature	2 K
Accelerating gradient	18 MV/m
Q_0	$6 \cdot 10^9$
Maximum surface E field	40 MV/m
Average pulse current	50 mA
Peak RF power	900 kW
Repetition frequency	14 Hz
Beam pulse length	2.86 ms

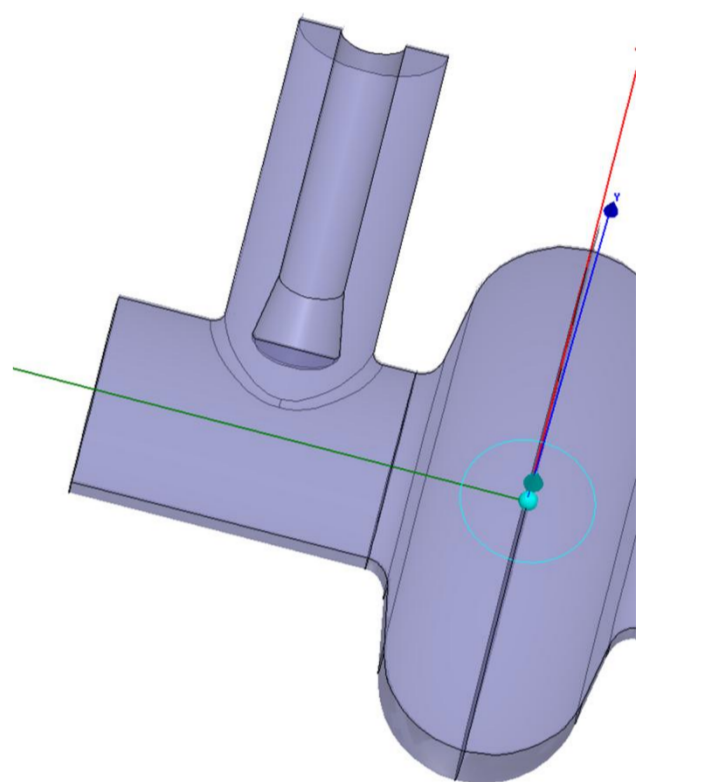
CAVITY RF PARAMETERS	
Bpk/Eacc [mT/(MV/m)]	4.3
Ep/Eacc	2.2
G [Ohm]	241
Cell to cell coupling	1.8 %
π and $4\pi/5$ mode separation	1.2 MHz
r/Q [Ohms]	477
$L_{acc} = N_{gap} \cdot \beta \cdot \lambda / 2$ [m]	0.915
Cell wall angle	$> 8^\circ$



External coupling

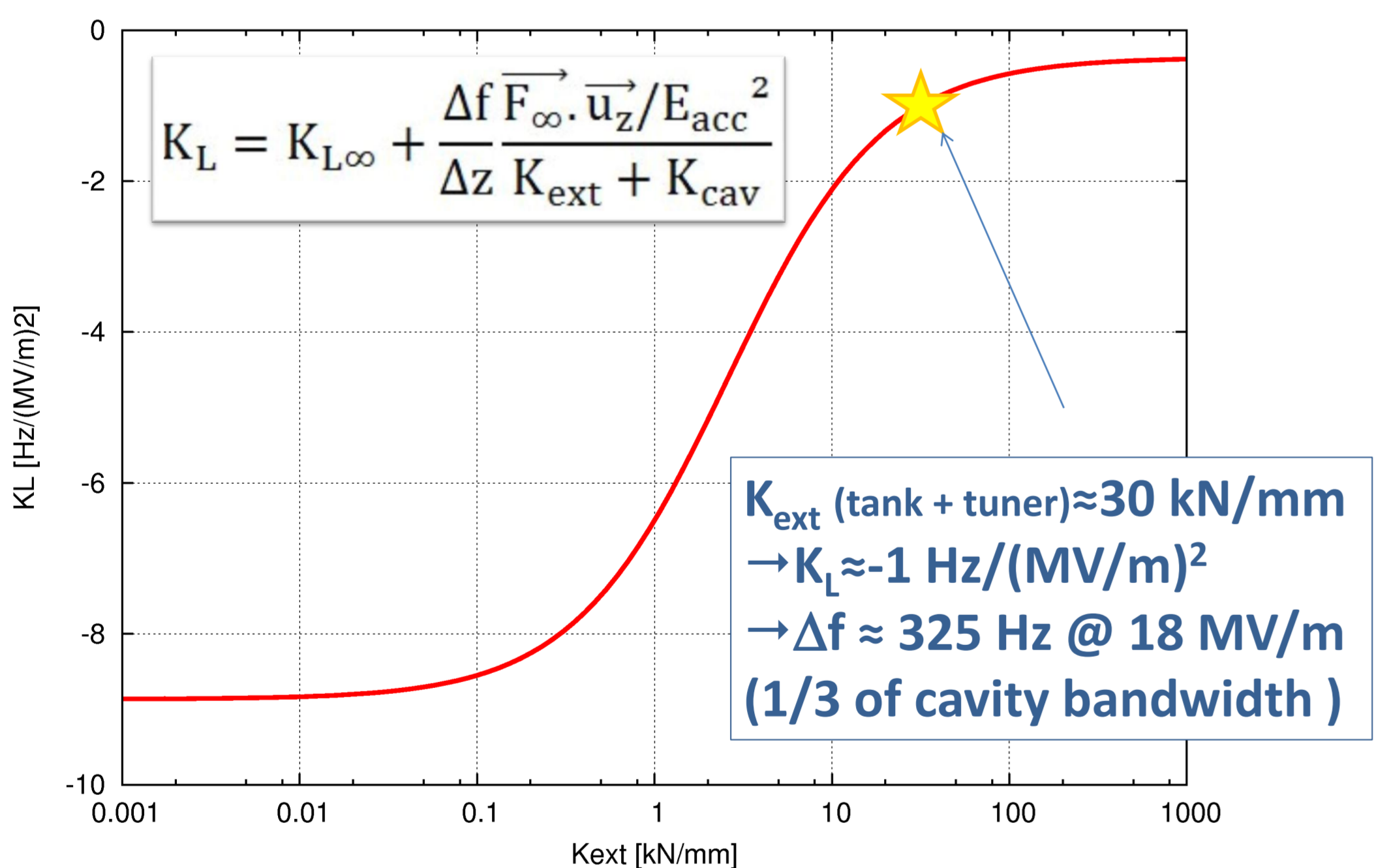


- Lc can be reduced to 30 mm (Ti vessel option)
- Using a conical tip decreases Qext by ~15% for a given antenna penetration

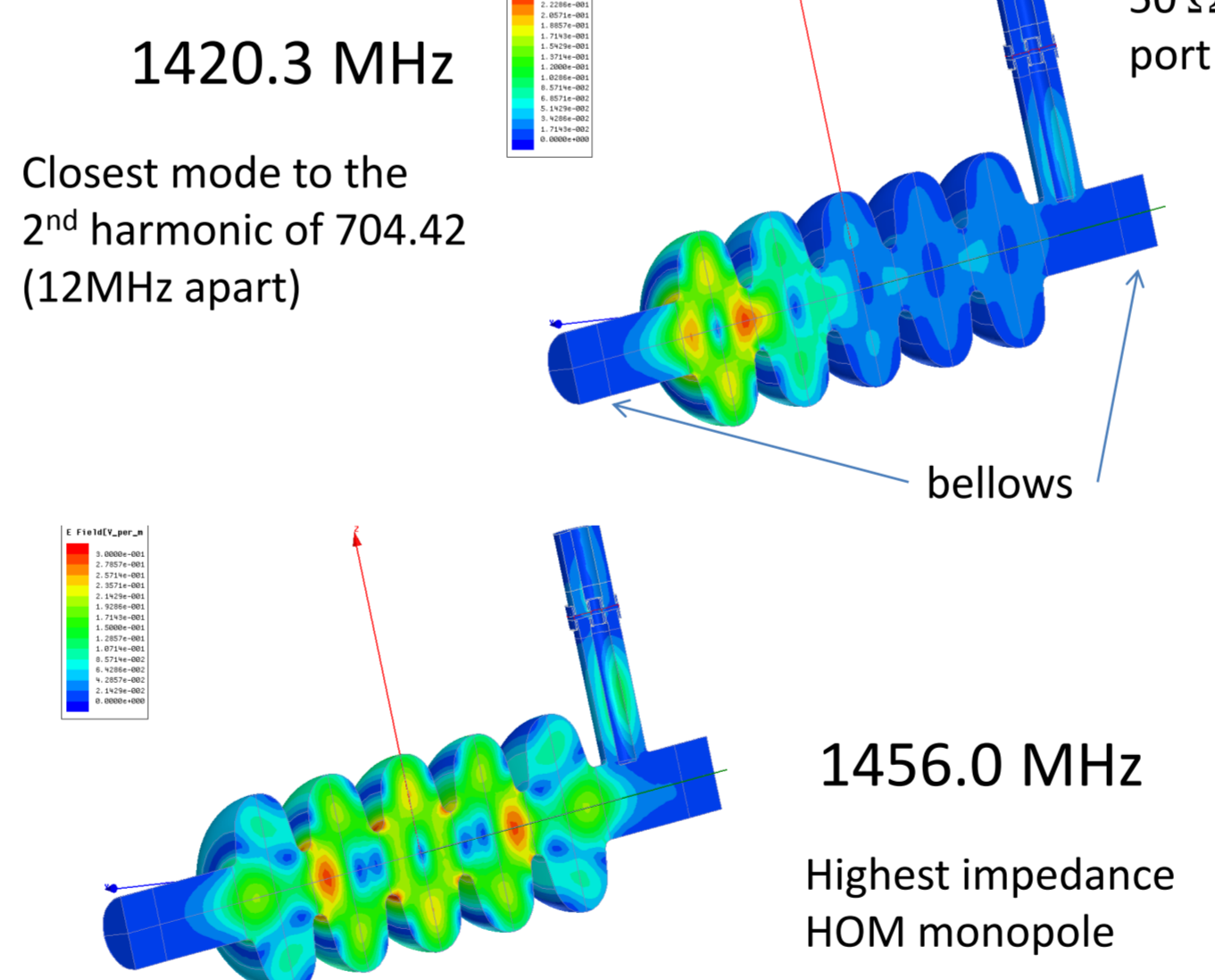
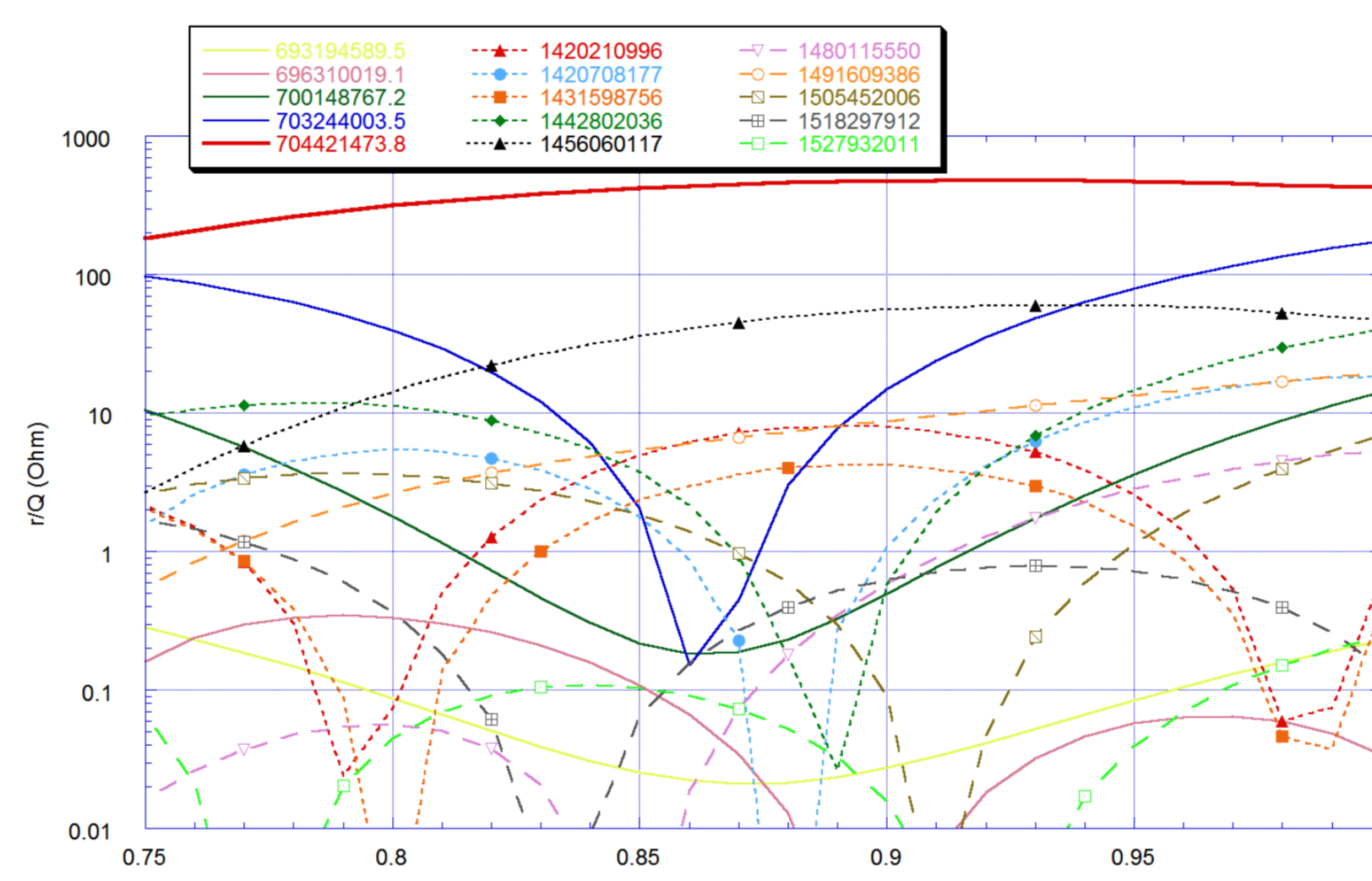


Reduction of K_L with stiffening rings

MECHANICAL PARAMETERS	
Nominal wall thickness [mm]	3.6
Cavity stiffness K_{cav} [kN/mm]	2.59
Tuning sensitivity $\Delta f / \Delta z$ [kHz/mm]	197
K_L with fixed ends [Hz/(MV/m) ²]	-0.36
K_L with free ends [Hz/(MV/m) ²]	-8.9
Pressure sensitivity K_P [Hz/mbar] (fixed ends)	4.85



Monopole modes below 1.64GHz (TM01 cut-off frequency for $\varnothing 140$ mm tube)



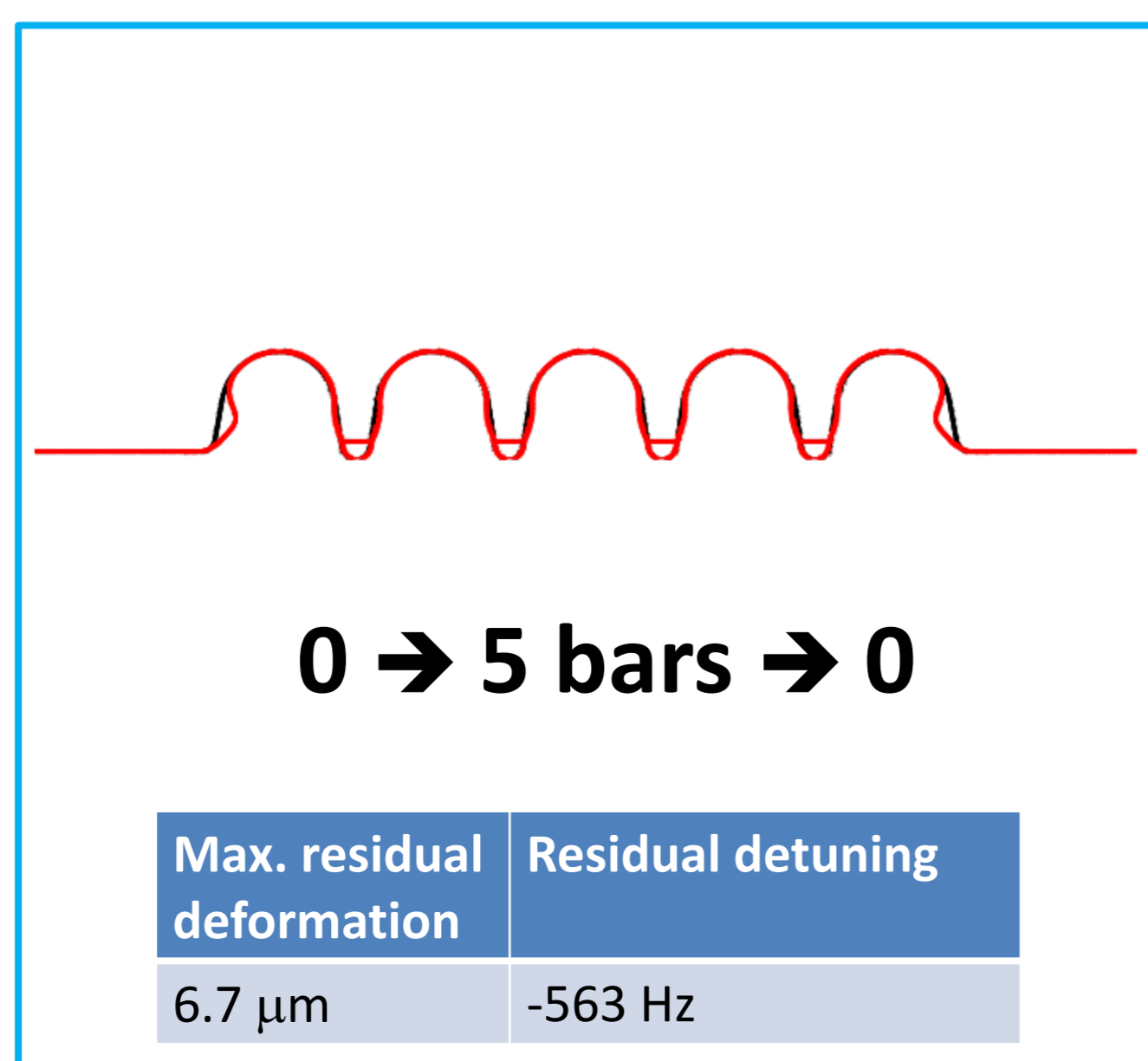
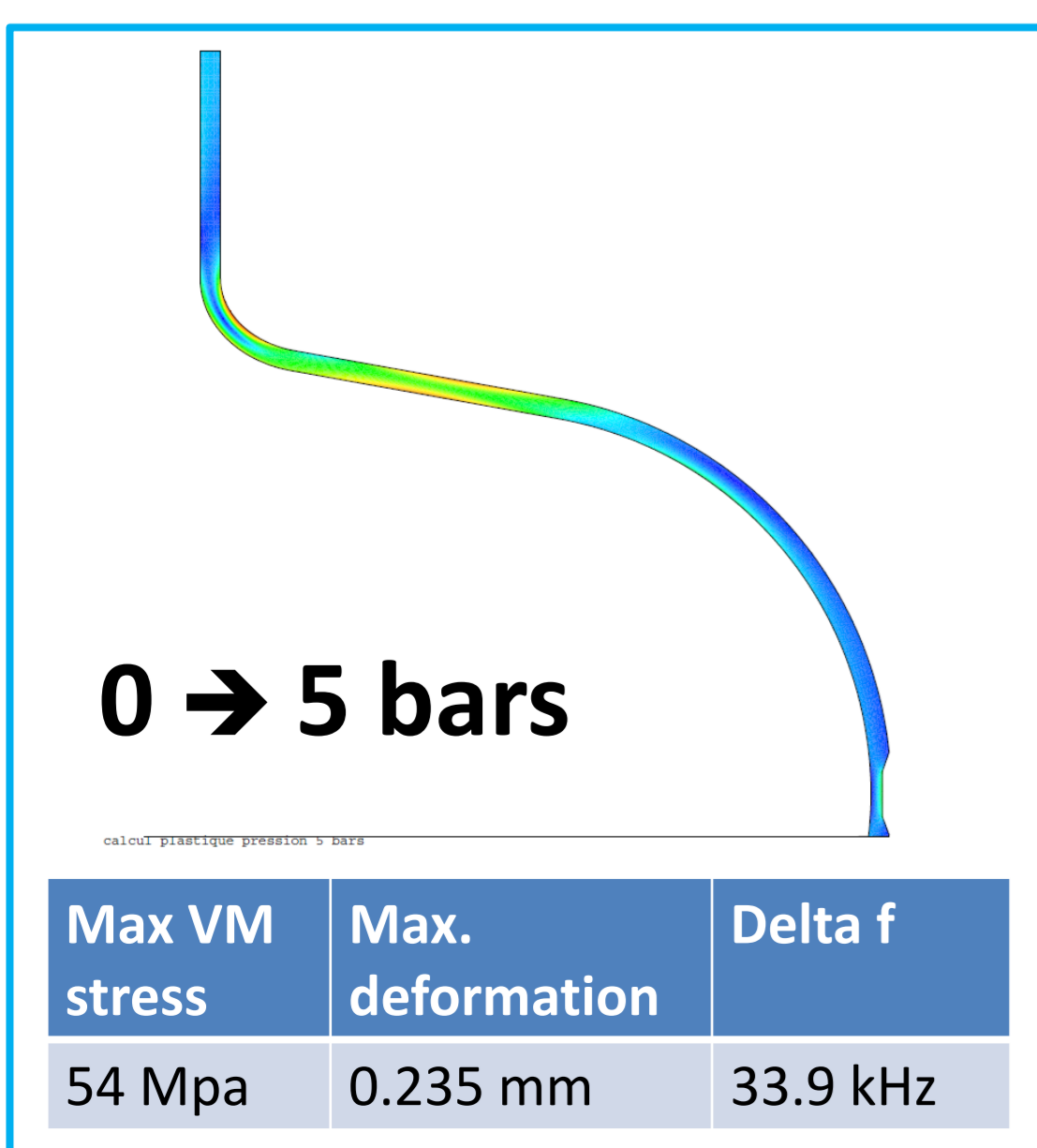
FIRST MONOPOLAR BAND		
Frequency (MHz)	Max. r/Q (Ohm)	Q
1420.3	8	$1.58 \cdot 10^5$
1421.9	17	$4.30 \cdot 10^3$
1431.7	4	$3.22 \cdot 10^4$
1442.8	29	$3.30 \cdot 10^4$
1456.0	60	$4.41 \cdot 10^4$

The RF window of the power coupler is included in the HFSS computations
 The low Q of HOMs is explained by losses on copper surfaces of the power coupler and inter-cavity bellows, and transmission through the RF window. The matched termination on the power coupler coaxial line
 None of monopole mode below cutoff need extra damping

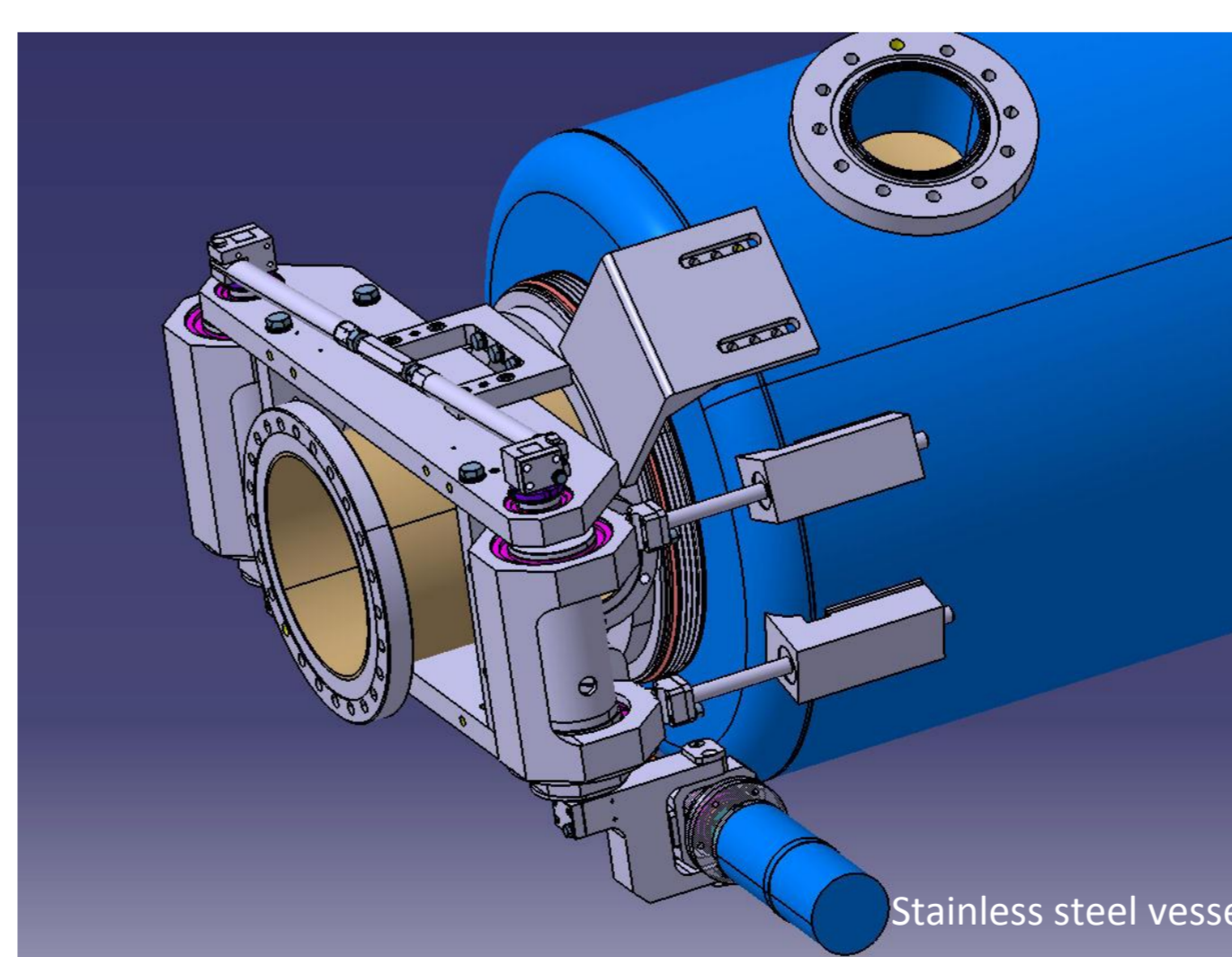
SECOND MONOPOLAR BAND		
Frequency (MHz)	Max. r/Q (Ohm)	Q
1480.1	5	$1.98 \cdot 10^4$
1491.5	17	$1.33 \cdot 10^4$
1431.7	4	$1.40 \cdot 10^4$
1518.2	4	$1.87 \cdot 10^4$
1527.9	0.2	$4.57 \cdot 10^4$

Pressure certification test : mechanical calculations

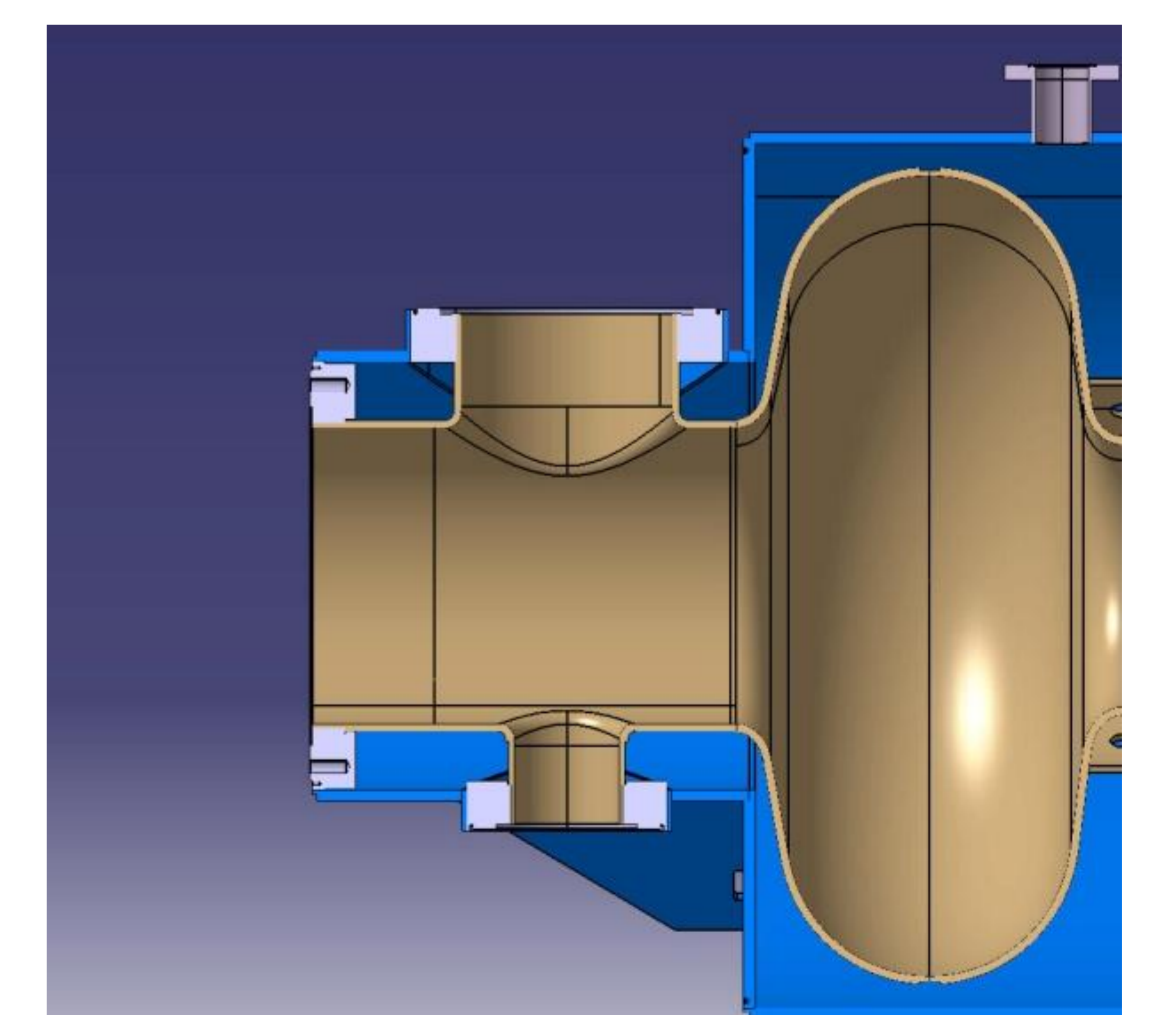
- We foresee a pressure test of the He tank/cavity will be carried out for certification
- Simulation of cavity deformation with a *plastic* model, 3.6 mm thickness
- The differential pressure is cycled : 0-5-0 bars
 - external rig used to maintain cavity length : fixed ends
 - max residual deformation after 1 cycle : $7 \mu\text{m}$ for 1 cycle, detuning 560 Hz



Helium tank and tuner integration



- Nb RRR > 250
- NbTi flanges, Al Hex seals



- ❖ Saclay V type
- ❖ 1 piezo
- ❖ Planetary gearbox (1/100e)
- ❖ Piezo preload at 2K is independant of the cavity springback force

