

THIN FILMS FOR CLIC ELEMENTS

Outline

- Motivation
- The role of MME-CCS
- DB and MB transfer lines
- Main beam
- Main beam quadrupoles
- Other issues
- conclusions

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Motivation

Changes in the vacuum requirements for CLIC:

In 2006: “dynamic vacuum should be 1×10^{-8} mbar, static vacuum $1-5 \times 10^{-9}$ mbar “

<https://clic-meeting.web.cern.ch/clic-meeting/2006>

In 2007: “whispers” of about 1×10^{-10} mbar for the main beam (MB) near the intersection point and for the transfer lines (MB and DB).

For the MB: high luminosity => high electrical field => ionization of the residual gas by tunnel effect => ion induced desorption (IID) => instabilities.

For the transfer lines: high current => ionization of the residual gas by collision => ion induced desorption => instabilities.

Not yet fully studied. Need confirmation from simulations.

Anyway, “always better than 10^{-8} for the main beam...”

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The role of MME-CCS

CCS has expertise in surface analysis, surface treatments and thin film coatings for UHV applications.

induced desorption, (by photons, electrons, ions), is a surface phenomena.

This expertise can be (and has already being) used to find solutions for surface's related problems.

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DB and MB transfer line

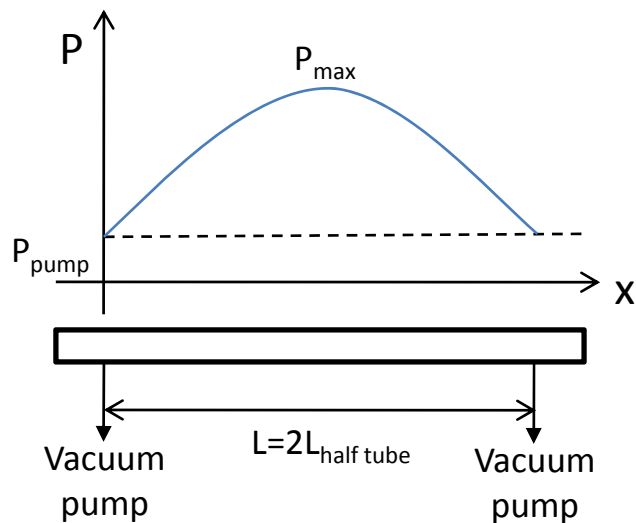
Total length: 2x 21km

2% filled with 1m long magnets: 2x 420 magnets

Diameter of the beam pipe $\phi=40\text{mm}$

Limit pressure to avoid ion stimulated desorption: 10^{-10} Torr ("large" molecules)

Pressure profile in a tube with uniform distributed outgassing



$$P_{\text{max}} = q \cdot 2\pi \cdot R \left(\frac{L_{\text{half tube}}}{S} + \frac{L_{\text{half tube}}}{2C_{\text{half tube}}} \right)$$

q -> outgassing rate

R -> radius of the tube

$L_{\text{half tube}}$ -> length of half tube

S -> pumping speed

C -> conductance of half tube

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Static vacuum

		q [Torr.l.s ⁻¹ .cm ⁻²]	S [l.s ⁻¹]	L [m]	L [m]	
No bakeout: main gas	H₂O	1.4.10⁻¹²	40	1.7	2.3	
With bakeout: main gas	H ₂	5.10 ⁻¹³	46	5.0	6.8	Possible solution...
With bakeout:	CO	5.10 ⁻¹⁴	36	9.6	14	
With NEG: not pumped	CH ₄	10 ⁻¹⁷	28	814	1220	Better solution
With NEG: not pumped	Kr	2.10 ⁻¹⁸	6	1202	1802	

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DB and MB transfer line

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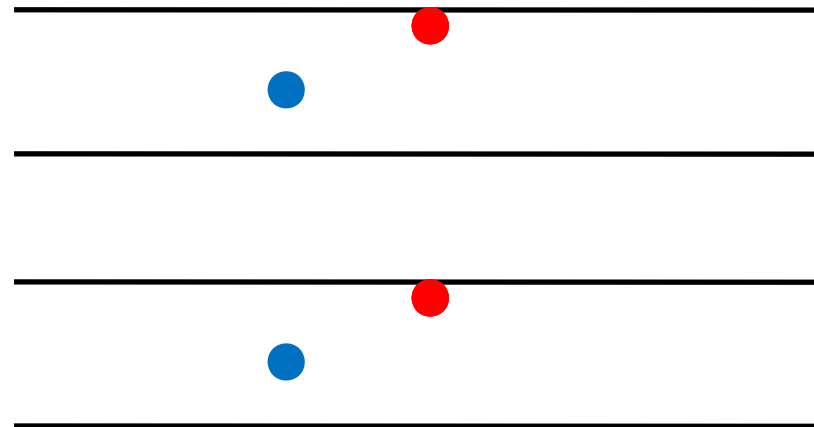
Diameter of the beam pipe $\phi=40\text{mm}$

Limit pressure to avoid ion stimulated desorption: 10^{-10} Torr (“large” molecules)

Why NEG coating solution better than bakeout?

Without NEG, desorbed molecules will follow random walk movement until being pumped by localized pumps (extremities of the beam pipe)

With NEG, the pumping power is right there! pressure recovering time is much shorter.



DB and MB transfer lines seems feasible with actual technology.

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Main Beam

Bakeout excluded: tight mechanical tolerances.

Pumping speed in the accelerating structures is limited

If 10^{-10} torr are necessary... this is a feasibility issue for CLIC!

Dynamics of the H₂O pumping in limited conductance systems
must be better understood

- An experimental set-up is being implemented to study H₂O pumping dynamics

Best possible dynamic vacuum must be simulated

- Pumping speed and geometry
- Thermal desorption/adsorption rates
- Surface coverage vs time
- Ion desorption yields
- Ionization efficiency per train
- Ion bombardment of the walls
- Breakdown rate
- Gas released per breakdown
-

We propose monte carlo and electrical network analogy approach

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Main Beam quadrupoles

length: ~1-2m

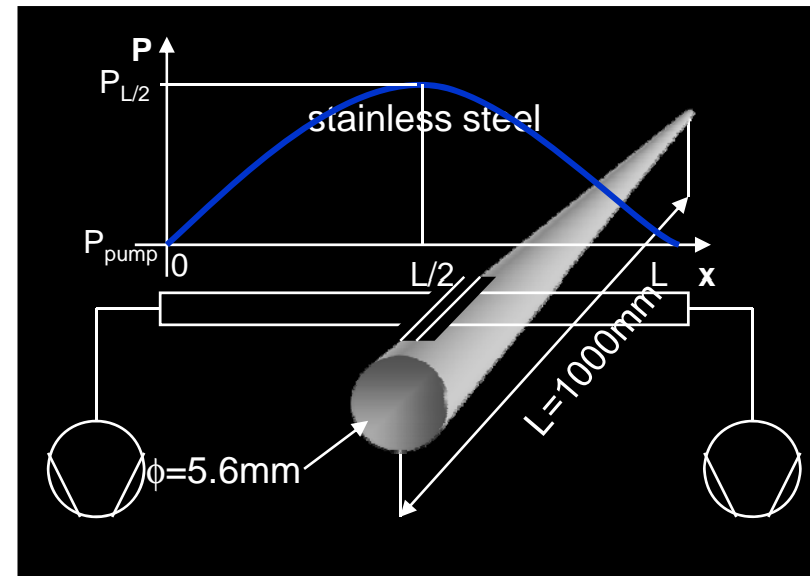
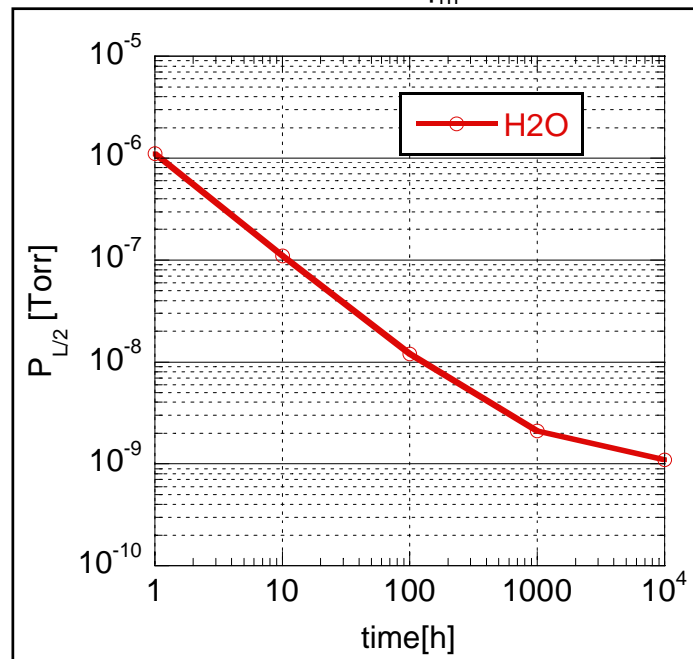
Diameter of the beam pipe ~5-6mm

Limit pressure to avoid ion stimulated desorption: 10^{-10} Torr ("large" molecules)

Bakeout excluded: temperature of the magnets $< 80^{\circ}\text{C}$

$$q(h) = q_{\text{limit}} + q_{1h} \cdot t^{-1}$$

Non baked stainless steel: $q_{1h} = 10^{-9}$ Torr.l/s/cm²



What about q_{limit} ?

Depends on H₂O desorption-adsorption dynamics

Effects of beam conditioning?...

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Main Beam quadrupoles

length: ~1-2m

Diameter of the beam pipe ~5-6mm

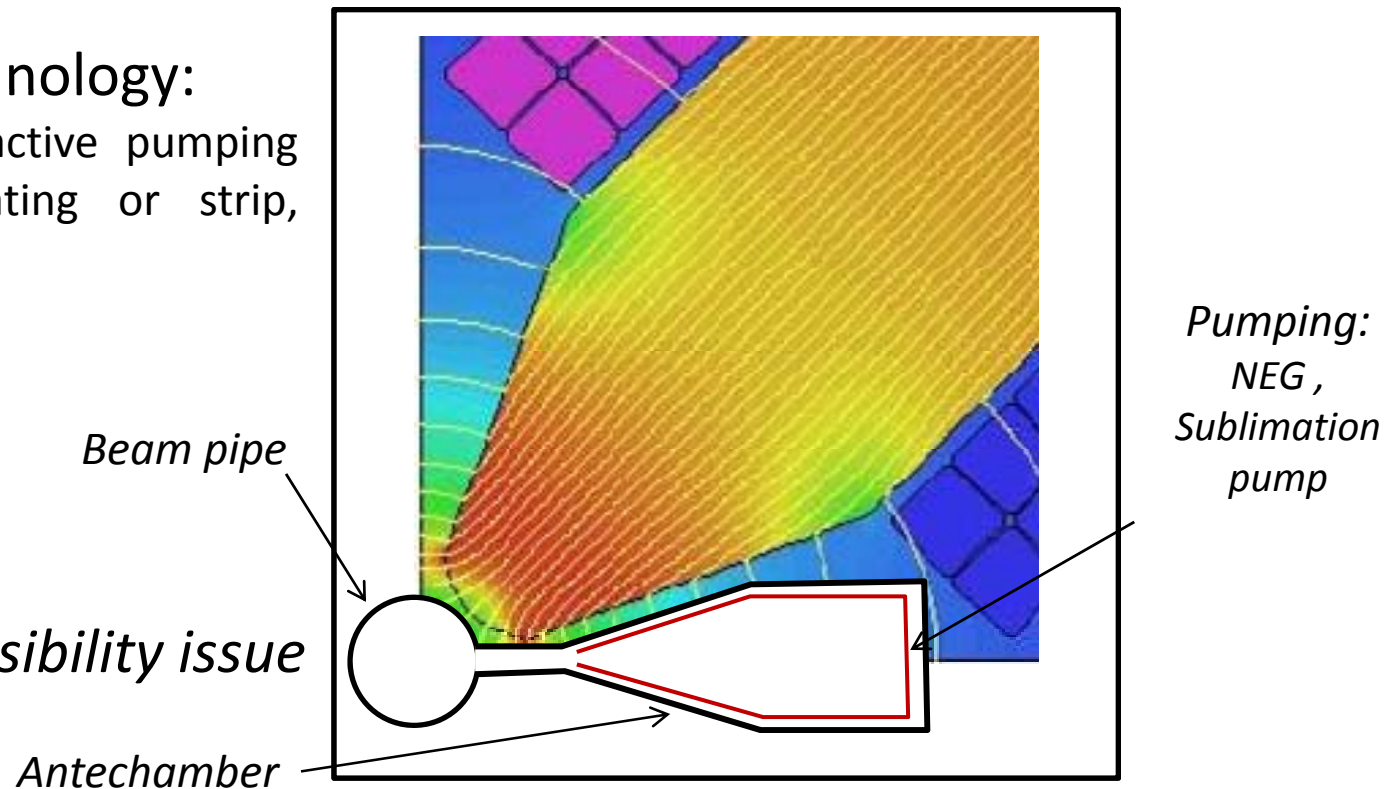
Limit pressure to avoid ion stimulated desorption: 10^{-10} Torr (“large” molecules)

Distributed pumping is required

With actual technology:

Antechamber with active pumping elements (NEG coating or strip, sublimation pump)

Probably not a feasibility issue



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Main Beam quadrupoles

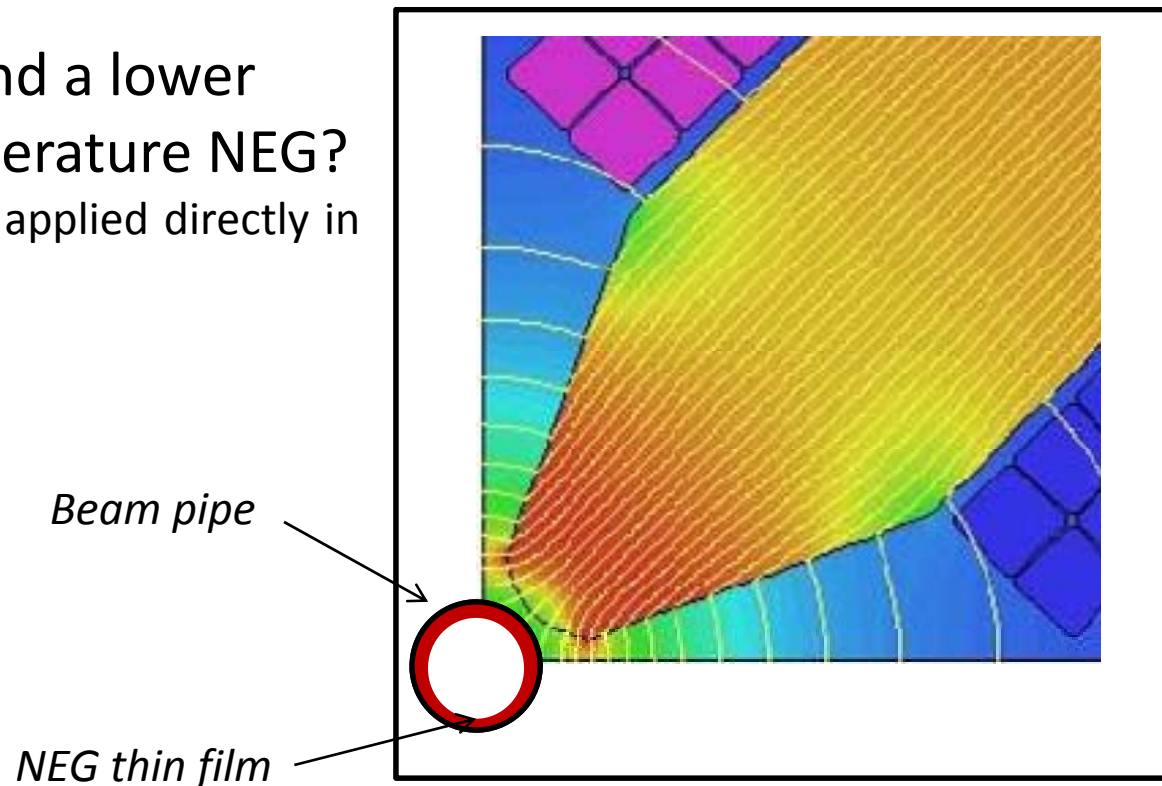
length: ~1-2m

Diameter of the beam pipe ~5-6mm

Limit pressure to avoid ion stimulated desorption: 10^{-10} Torr (“large” molecules)

Distributed pumping is required

And If we find a lower
activation temperature NEG?
The NEG film will be applied directly in
the beam pipe.



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Other issues

Combining rings

- High levels of synchrotron radiation => high photon induced desorption
- Requires high distributed pumping speed
- NEG coatings are widely used in electron storage rings for synchrotron light sources. (ESRF, Elettra...)
- More details are necessary to evaluate situation.

not a feasibility issue

injection lines

- VERY low secondary electron yield (SEY) required (0.9... maybe...)
- CCS is launching a program to develop new materials with low SEY. Nitrides, carbides and borides of transition metals, C:N and other carbon based materials will be studied.

feasibility issue

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Conclusions

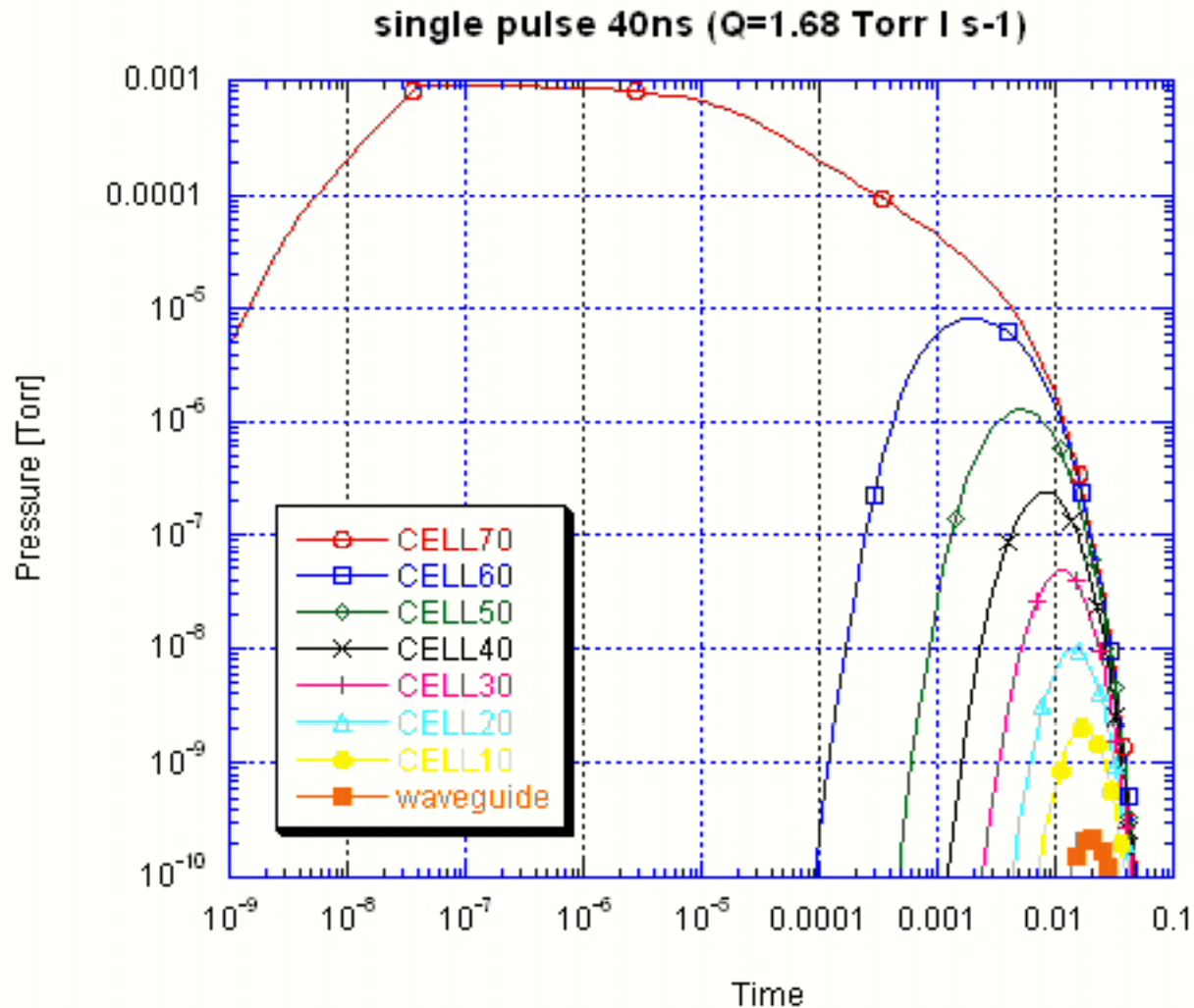
- MB and DB transfer lines: 10^{-10} torr feasible with bakout or NEG. (NEG better for dynamic vacuum). ***Not a feasibility issue.***
- Main beam: 10^{-10} torr not possible without heating the structures. Best possible dynamic vacuum must be simulated. H₂O behavior must be studied. ***feasibility issue.***
- Main beam quadrupoles: distributed pumping required. ***Probably not a feasibility issue.***
- Combining rings: classical NEG solution. Input is necessary to correctly evaluate the situation. ***Not a feasibility issue.***
- injection lines: maybe a SEY of 0.9 is required. ***feasibility issue.***

acknowledgments

Bernard Jeanneret and Daniel Schulte.

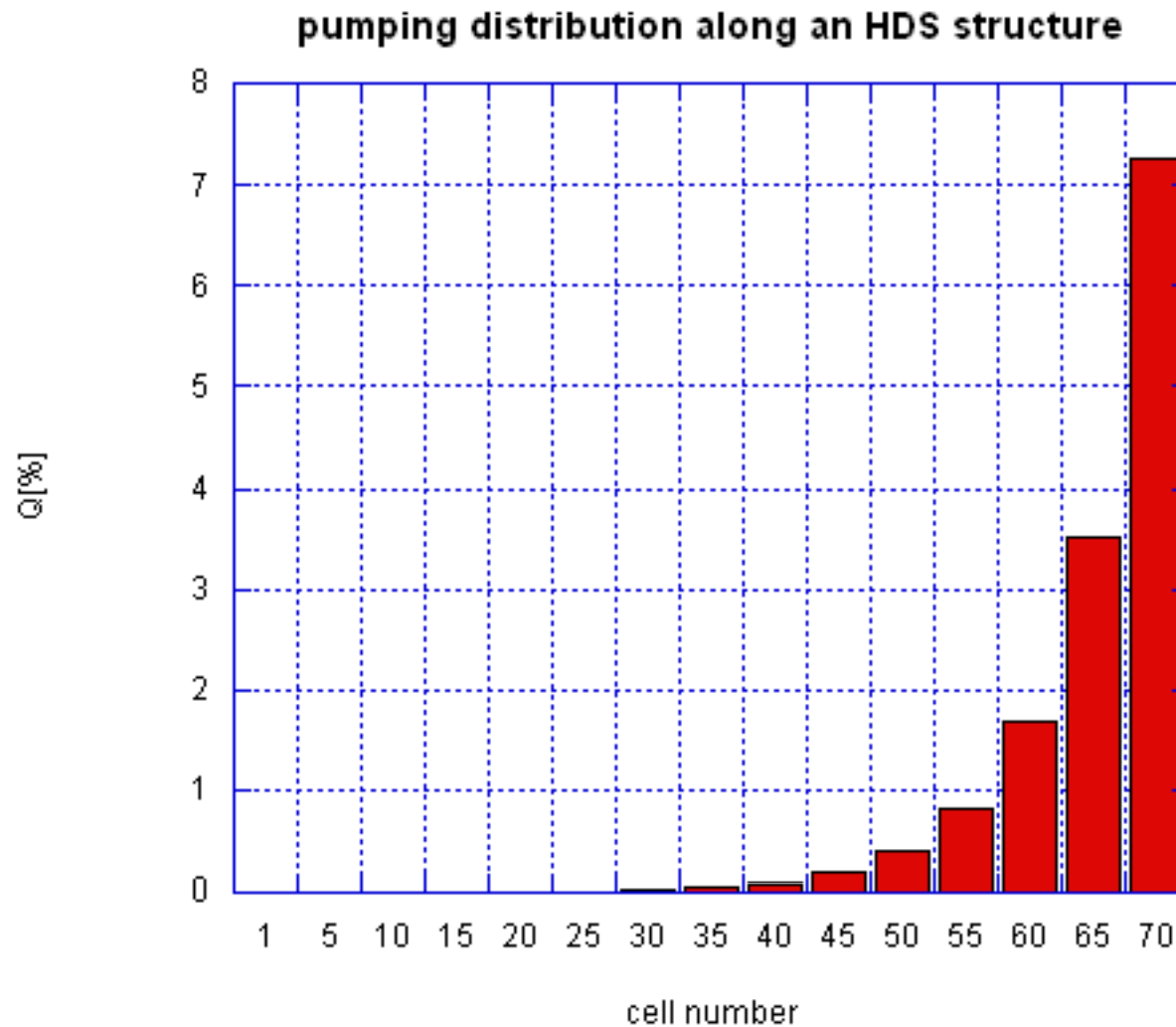
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CO pressure evolution in an 30GHz HDS structure



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Pumping distribution in 30GHz HDS structure



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Introduction

Brief overview of the outgassing in UHV systems

Thermal outgassing:

Driving force: thermal energy.

Non baked systems: mainly H₂O $q(t) \approx q_{\text{limit}} + \frac{10^{-9}}{t[\text{hours}]} [\text{Torr} \cdot \text{l} \cdot \text{s}^{-1} \cdot \text{cm}^{-2}]$

baked systems: mainly H₂ $5 \cdot 10^{-14} < q < 10^{-11} [\text{Torr} \cdot \text{l} \cdot \text{s}^{-1} \cdot \text{cm}^{-2}]$

But also CO, CO₂, CH₄ ...

Outgassing rates

Stimulated outgassing:

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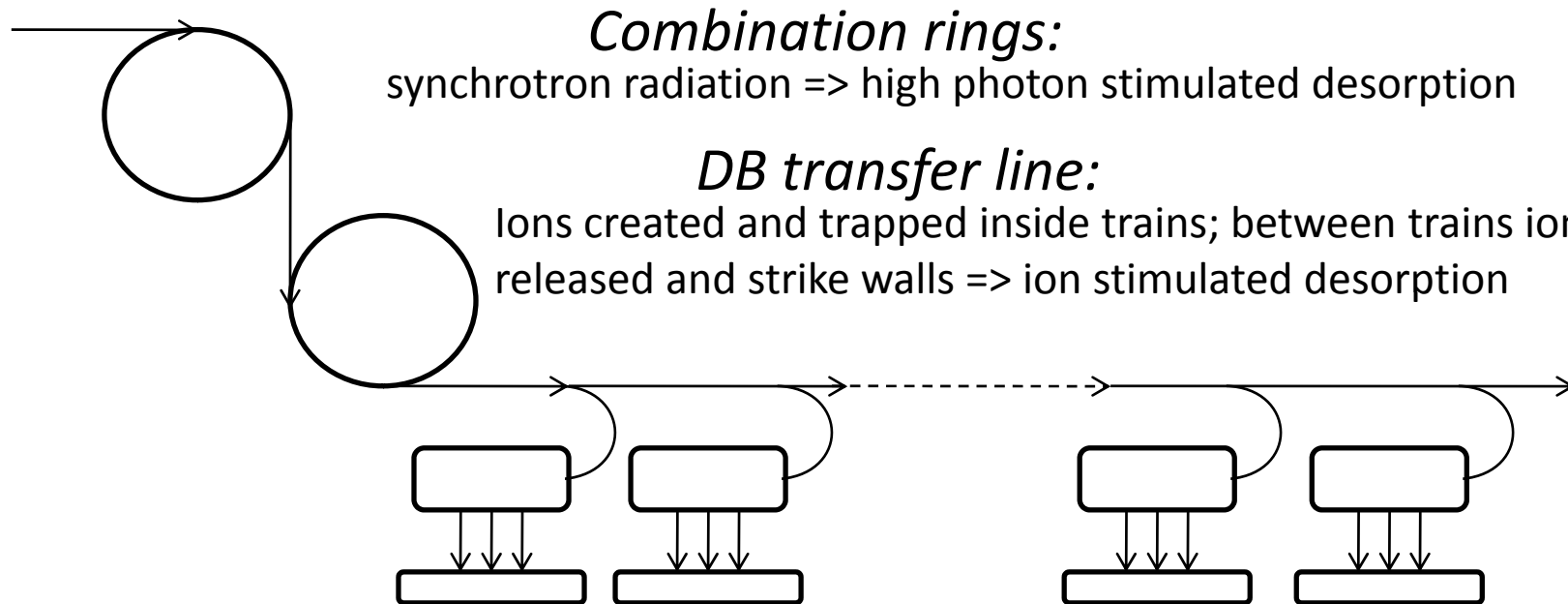
Introduction

Brief overview of the outgassing in UHV systems

- Thermal outgassing:* Driving force: thermal energy.
Non baked systems: mainly H₂O
baked systems: mainly H₂, but also CO, CO₂, CH₄ at lower rates
- Stimulated outgassing:* Driving force: particles striking the surfaces of the system
(photons, electrons, ions)
Strongly dependent
baked systems: mainly H₂, but also CO, CO₂, CH₄ at lower rate:

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Introduction



Combination rings:
synchrotron radiation => high photon stimulated desorption

DB transfer line:
Ions created and trapped inside trains; between trains ions are released and strike walls => ion stimulated desorption

MB transfer line: Roughly the same as DB transfer line

Main beam: Near the interaction point beam's electrical field is enough to ionize residual gas => ion stimulated desorption

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DB and MB transfer line

Total length: 2x 21km

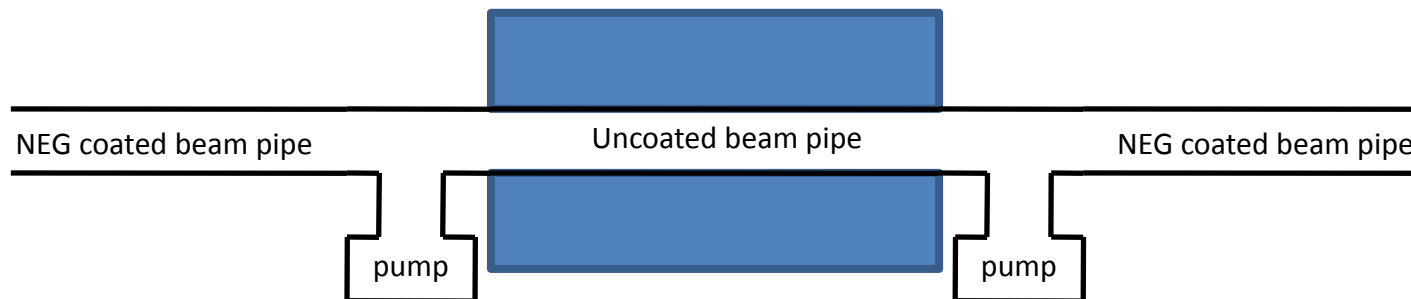
2% filled with 1m long magnets: 2x 420 magnets

Diameter of the beam pipe $\phi=40\text{mm}$

Limit pressure to avoid ion stimulated desorption: 10^{-10} Torr (“large” molecules)

And for the magnets?

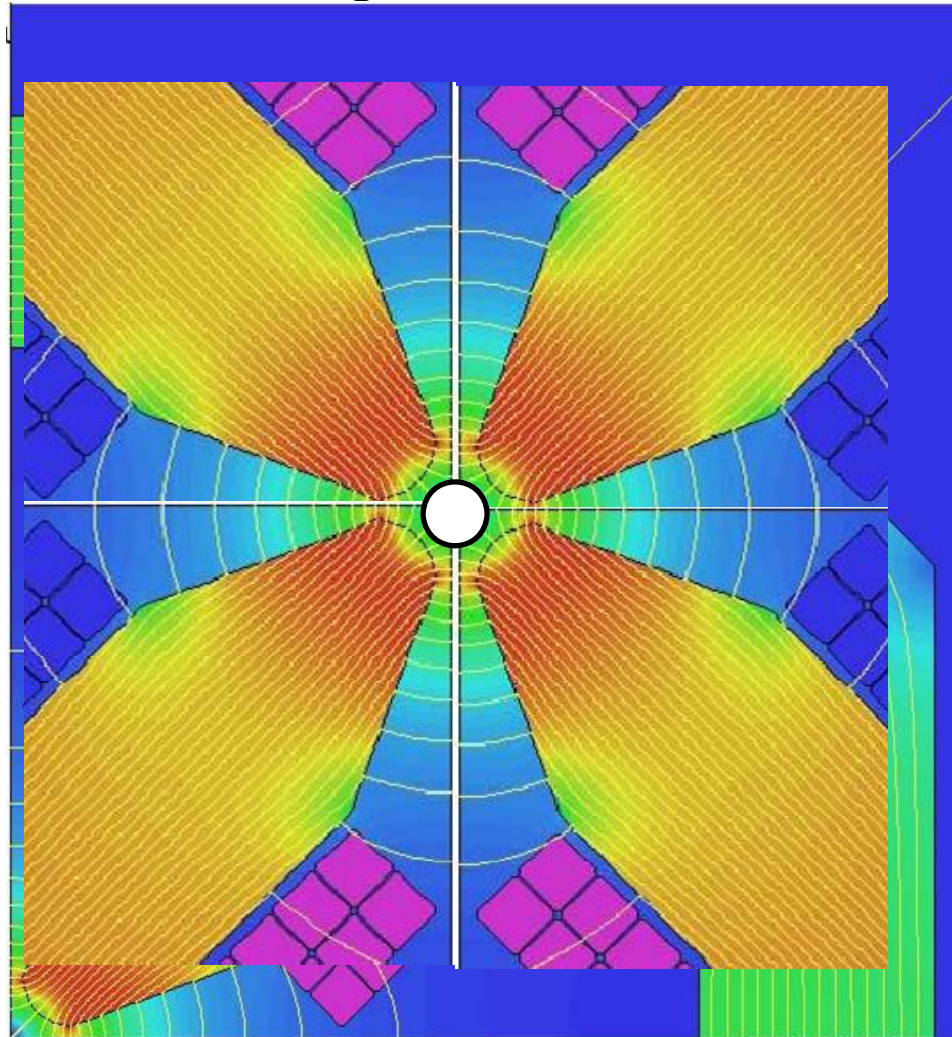
- if $T_{\text{max}}=200\text{C}$ ok for existing NEG
- If not, *hybrid* solution!



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Main Beam quadrupoles

Bakeout excluded: tight mechanical tolerances.



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Main Beam quadrupoles

length: ~1-2m

Diameter of the beam pipe ~5-6mm

Limit pressure to avoid ion stimulated desorption: 10^{-10} Torr (“large” molecules)

Distributed pumping is required

