



# MEBT dump

## Thermo-mechanical analysis

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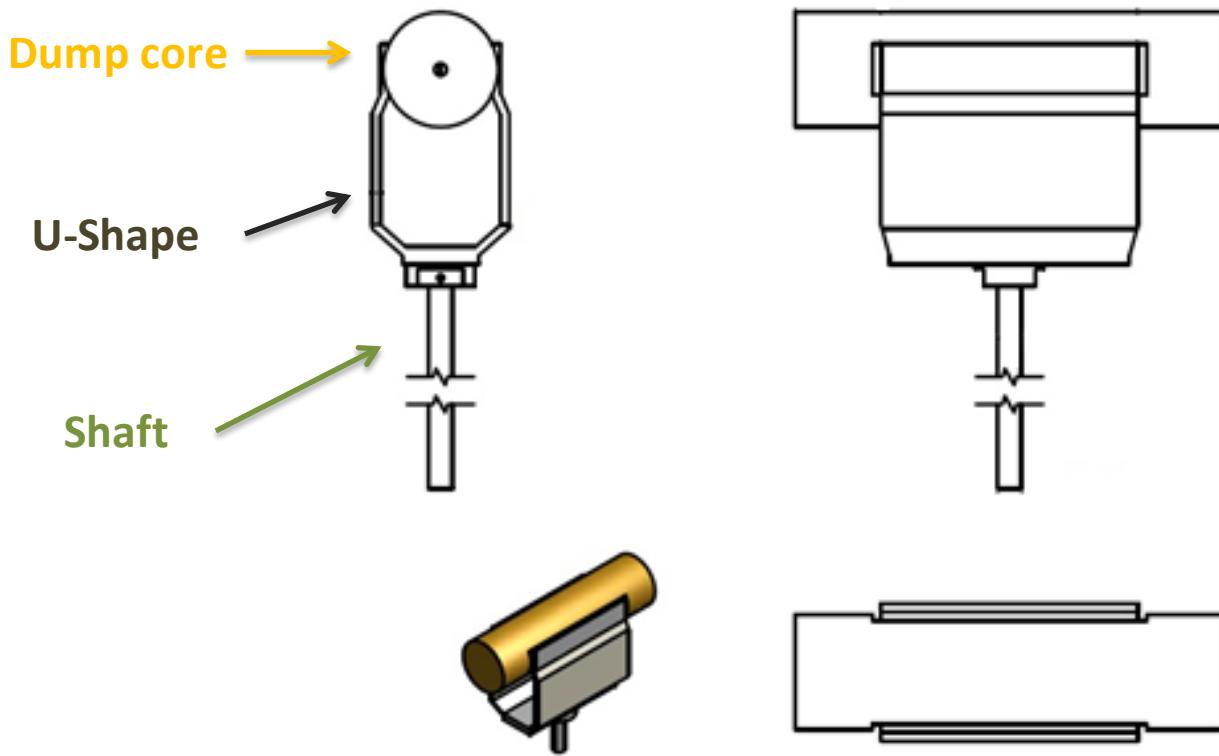
# Preliminary consideration

- The MEBT dump is located in the injection line (7 MeV)

<b><i>Beam Parameters, proton beam</i></b>		
<b><i>Current:</i></b>	0,8	<i>mA</i>
<b><i>Pulse-time:</i></b>	500	$\mu\text{s}$
<b><i>Frequency:</i></b>	2	<i>Hz</i>
<b><i>Pulse-period:</i></b>	0,5	<i>s</i>
<b><i>Np:</i></b>	2,5E+12	-
<b><i>Power beam:</i></b>	5,6	<i>W</i>

- The study focus on the three part of the MEBT dump:
  - The dump core
  - The U-shape part
  - The shaft

# Preliminary design



*Design as from K. Asvestas*

# Material configuration

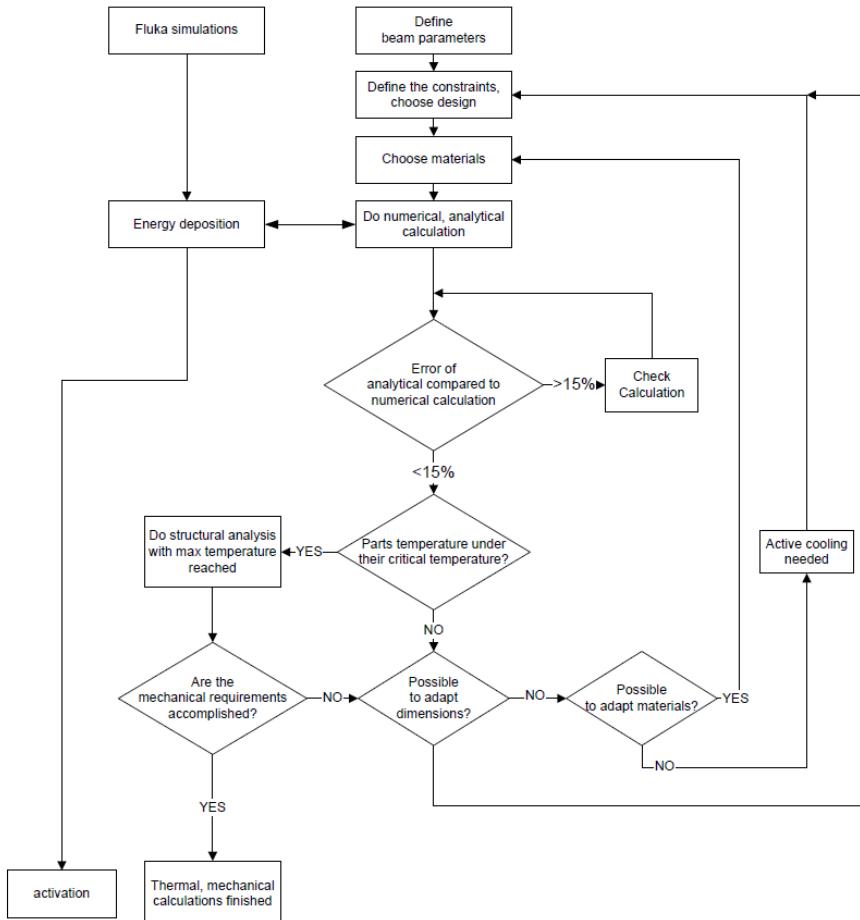
- Initial material configuration:
  - Dump core: Tungsten
  - U-Shape: Aluminium
  - Shaft: Stainless Steel
- Alternative configuration:
  - Dump core: Tungsten
  - U-Shape and Shaft: All Aluminium/ All copper/ All Stainless Steel

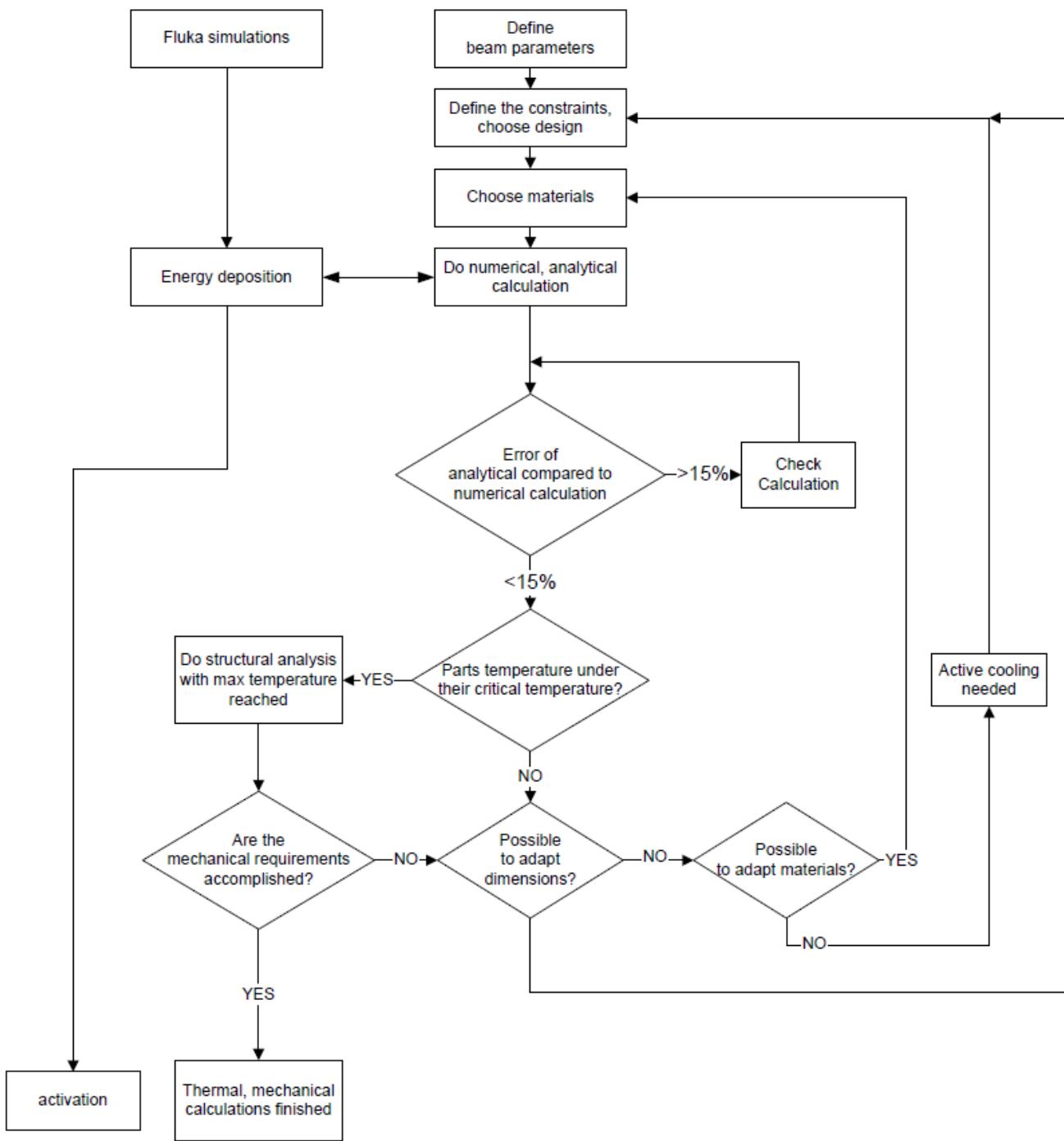
# Material Properties

		Tungsten	Aluminium	Stainless Steel	Copper
<b>Density</b>	$\rho$ (kg/m <sup>3</sup> )	19 299	2 770	7 750	8940
<b>Thermal expansion coefficient</b>	$\lambda$ (°C <sup>-1</sup> )	4.48E-06	2.30E-05	1.70E-05	1.74E-05
<b>Young's modulus</b>	$E$ (Mpa)	3.99E+05	7.10E+04	1.93E+05	1.00E+05
<b>Poisson's ratio</b>	$\nu$ (-)	0.28	0.33	0.31	0.34
<b>Thermal conductivity</b>	$k$ (W/m.°C)	173	149	15.2	387
<b>Specific heat capacity</b>	$C_p$ (J/kg.°C)	132	875	480	383
<b>Emissivity</b>	$\varepsilon$ (-)	0.04	0.2	0.54	0.03
<b>Melting point</b>	$T_m$ (°C)	3410	660	1750	1050
<b>Maximum service temperature</b>	$T_c$ (°C)	927	160	300	300

**Note:** the emissivity values are taken for not surface treated material (oxidation/polishing/...) and have to be checked after final choice and configuration of the material

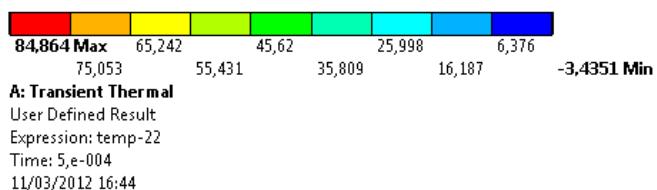
# Methodology of analysis





# One pulse analysis

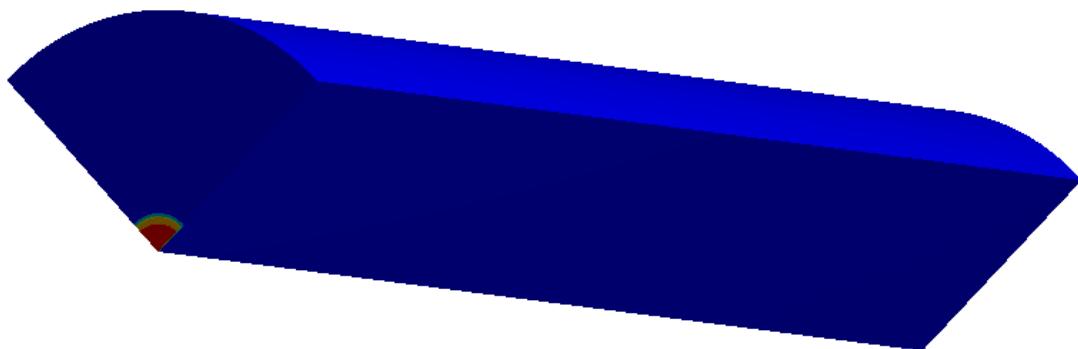
- Increase of temperature for one-pulse



ANSYS  
14.0

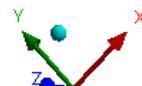
$$\Delta T \text{ Max} = 84,9 \text{ }^{\circ}\text{C}$$

$$\Delta T \text{ Max analytical} = 85 \text{ }^{\circ}\text{C}$$



$$\text{Melting point} = 3410 \text{ }^{\circ}\text{C}$$

*% of the geometry*



# Steady State analysis

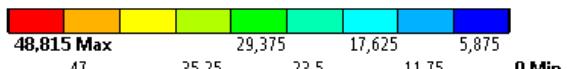
- Evaluation of TCC:
  - Between the Shaft and the U-Shape, the contact is considered as perfect
    - $TCC = 10\,000 \text{ W/m}^2\text{K}$
  - Between the Dump core and the U-Shape: pressure of contact estimated at about 11 Mpa
    - The TCC between two surfaces depends on the pressure of contact and the material properties

	S.S/Tu	Al/Tu	Cu/Al
<b>TCC</b>	2240	62	35900

# Steady State analysis

**U-Shape : Aluminium**

**Shaft : S. Steel**



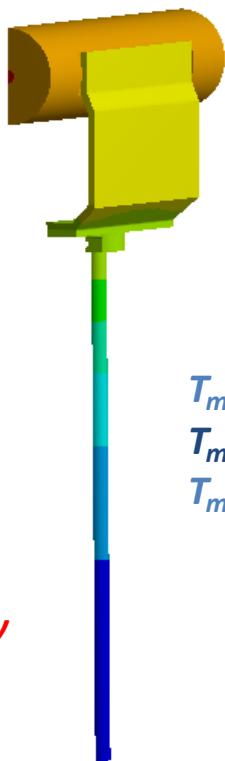
C: support Al et ss

User Defined Result

Expression: temp-22

Time: 1

11/03/2012 17:25



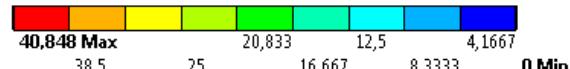
$T_{max} \text{ Tu} = 70,8 \text{ }^{\circ}\text{C}$   
 $T_{max} \text{ Al} = 58 \text{ }^{\circ}\text{C}$   
 $T_{max} \text{ ss} = 56 \text{ }^{\circ}\text{C}$

*half of the geometry*



**U-Shape : Aluminium**

**Shaft : Aluminium**



E: support tout Al

User Defined Result

Expression: temp-22

Time: 1

11/03/2012 16:58



$T_{max} \text{ Tu} = 62,8 \text{ }^{\circ}\text{C}$   
 $T_{max} \text{ Al} = 50 \text{ }^{\circ}\text{C}$

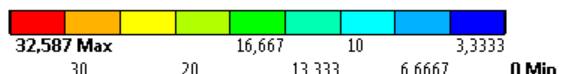
*half of the geometry*



# Steady State analysis

**U-Shape : Copper**

**Shaft : Copper**



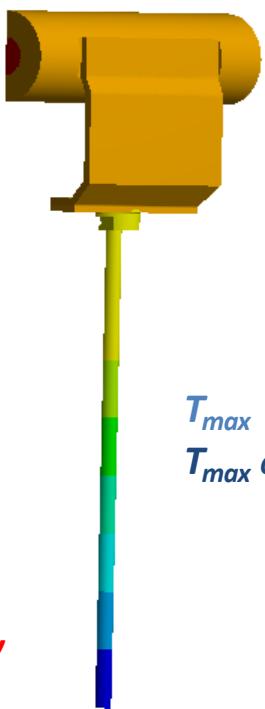
D: support tout Cu

User Defined Result

Expression: temp-22

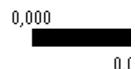
Time: 1

11/03/2012 16:56



$$T_{max} \text{ Tu} = 54,6 \text{ }^{\circ}\text{C}$$
$$T_{max} \text{ Cu} = 51 \text{ }^{\circ}\text{C}$$

*half of the geometry*



**U-Shape : S. Steel**

**Shaft : S. Steel**



F: support tout SS

User Defined Result

Expression: temp-22

Time: 1

11/03/2012 17:37



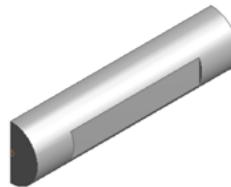
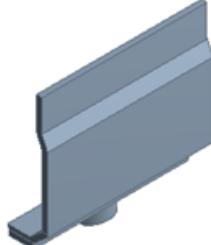
$$T_{max} \text{ Tu} = 49,4 \text{ }^{\circ}\text{C}$$
$$T_{max} \text{ SS} = 45 \text{ }^{\circ}\text{C}$$

*half of the geometry*



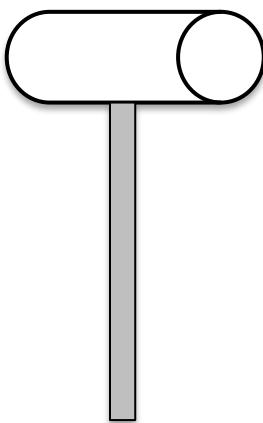
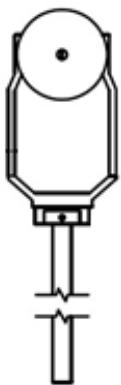
# Steady State analysis

- Summarize of results

Config. Number	Dump Core	U-Shape	Shaft
			
1	<b>Material</b> Tungsten	Aluminium	S.Steel
	<b>Temp. Maxi</b> $70,8 + 85 = 155,8 \text{ }^{\circ}\text{C}$	$58 \text{ }^{\circ}\text{C}$	$56 \text{ }^{\circ}\text{C}$
2	<b>Material</b> Tungsten	Aluminium	Aluminium
	<b>Temp. Maxi</b> $62,8 + 85 = 147,9 \text{ }^{\circ}\text{C}$	$50 \text{ }^{\circ}\text{C}$	Same material
3	<b>Material</b> Tungsten	Copper	Copper
	<b>Temp. Maxi</b> $54,6 + 85 = 139,8 \text{ }^{\circ}\text{C}$	$51 \text{ }^{\circ}\text{C}$	Same material
4	<b>Material</b> Tungsten	S.Steel	S.Steel
	<b>Temp. Maxi</b> $49,4 + 85 = 134,4 \text{ }^{\circ}\text{C}$	$45 \text{ }^{\circ}\text{C}$	Same material
	Tungsten	Aluminium	Copper
	S. Steel		
Reminder:	<b>Service temp.</b>	$927 \text{ }^{\circ}\text{C}$	$160 \text{ }^{\circ}\text{C}$
		$300 \text{ }^{\circ}\text{C}$	$300 \text{ }^{\circ}\text{C}$

# Buckling analysis

- Considering the geometry: risk of buckling



$\sigma$  due to proper weigh of the set  
“dump core + U-shape” = 1,1 MPa



	S.S	Al	Cu
$\sigma_{adm}$ (Mpa)	326	120	169



Best material choice  
: ***Stainless Steel***

# Conclusion for MEBT dump

- The best material choice is to have the U-Shape and the Shaft with the same material. The **Stainless Steel** seems to be a good candidate.
- The **emissivity** value of the material will have to be checked with the supplier since it can have a significant impact on the results.
- To ensure a good heat evacuation, the **contact** between the dump core and the U-Shape has to be properly ensured.
- Considering the increase of temperature, the thermal stresses are not an issue. However, it is advised to use a **spring washer** to partially limit a part of the stresses due to the thermal expansion.

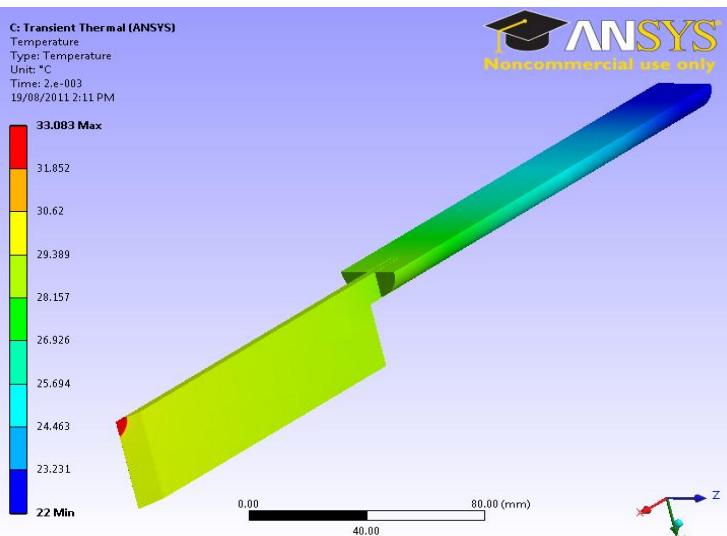
# Other devices

- The others devices of the facility:
  - The Scarpers: *located in the Synchrotron*
  - The internal beam Dumps: *located in the Synchrotron*
  - The chopper dump: *located in the extraction line*
  - The Beam Stopper: *located in the extraction line*
  - The EX dump: *located in the extraction line*

# Thermal behavior

- The scrapers: **Aluminium** core, **Stainless Steel** shaft

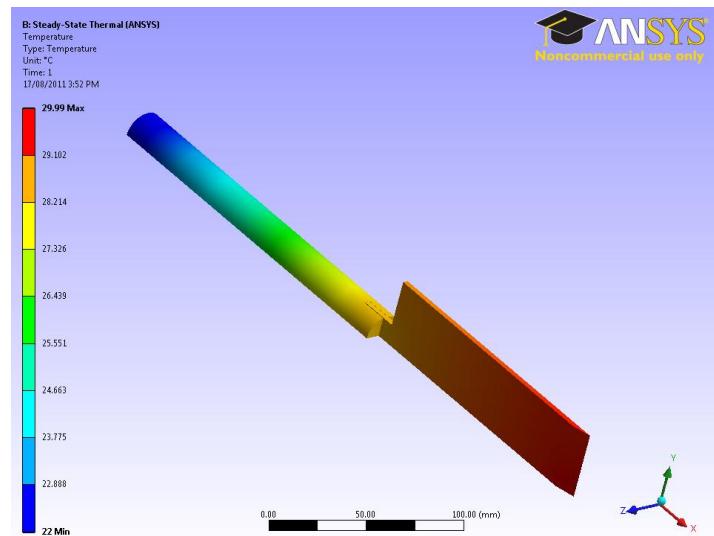
1 Pulse:



$$T_{max\ Al} = 33,1\text{ }^{\circ}\text{C}$$
$$T_{max.\ use\ Al} = 160\text{ }^{\circ}\text{C}$$

NB: results from K. Asvestas

Steady State:



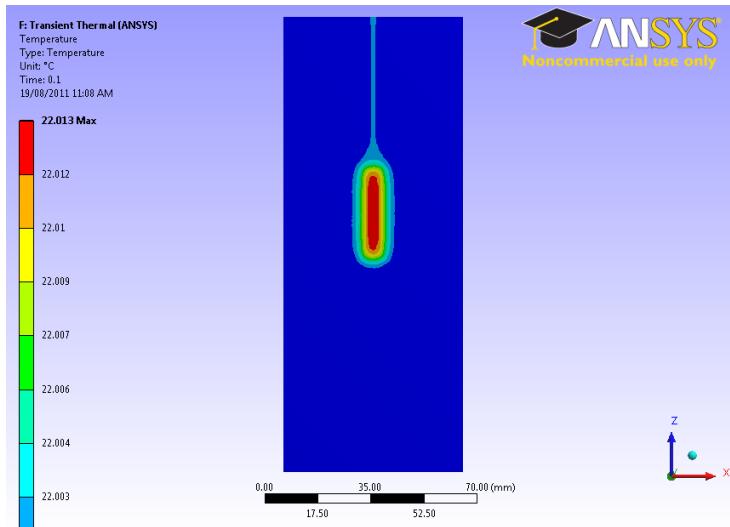
$$T_{max\ Al} = 30\text{ }^{\circ}\text{C}$$
$$T_{max.\ use\ Al} = 160\text{ }^{\circ}\text{C}$$
$$\rightarrow T_{max\ Total} = 63,1\text{ }^{\circ}\text{C}$$

The contact between the two parts is assumed perfect.

# Thermal behavior

- The Chopper dump: Core in *graphite*, external part in *Tungsten*, *metallic* support

1 Pulse:

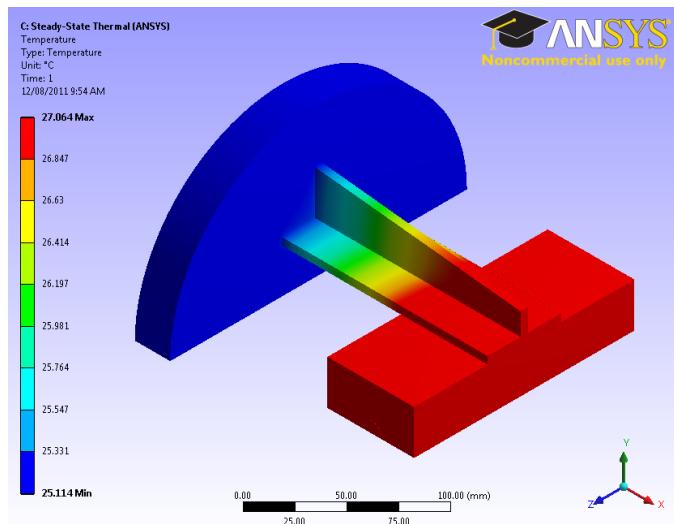


$$T_{max} Gr = 22,1 \text{ } ^\circ\text{C}$$

$$T_{max. \text{ use}} Gr = 3800 \text{ } ^\circ\text{C}$$

NB: results from K. Asvestas

Steady State:



$$T_{max} Gr = 27,1 \text{ } ^\circ\text{C}$$

$$T_{max. \text{ use}} Gr = 3800 \text{ } ^\circ\text{C}$$



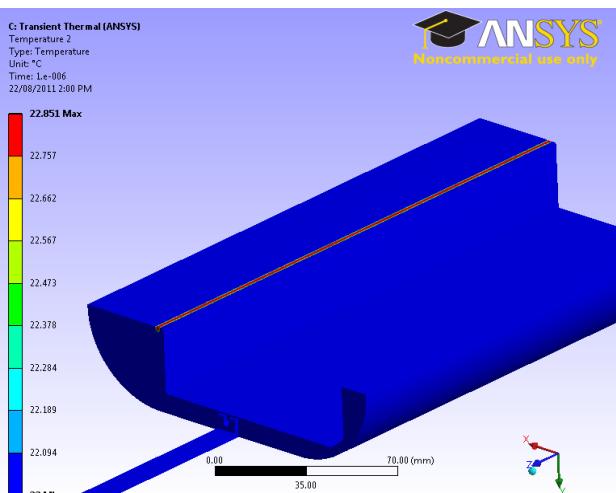
$$T_{max} \text{ Total} = 49,2 \text{ } ^\circ\text{C}$$

The contact between the two parts is assumed perfect.

# Thermal behavior

- The Internal dump: core in **Tungsten, metallic** spacers

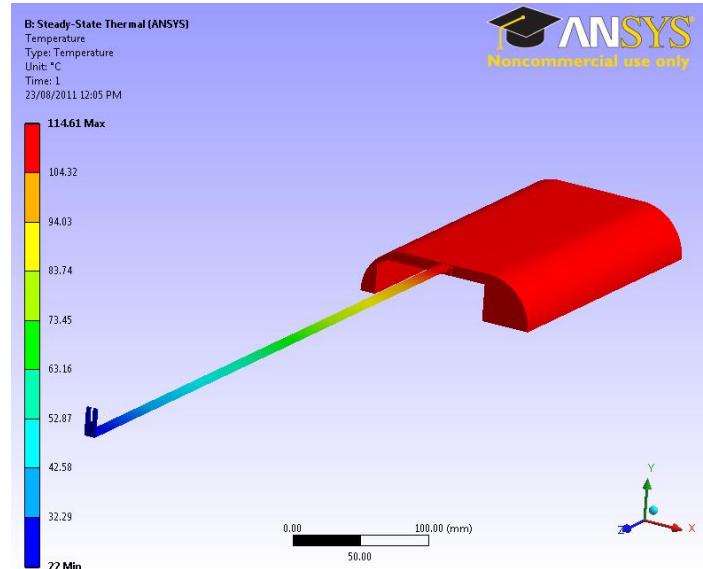
1 Pulse:



$$T_{max} \ Tu = 22,9 \text{ } ^\circ\text{C}$$
$$T_{max. \ use} \ Tu = 927 \text{ } ^\circ\text{C}$$

NB: results from K. Asvestas

Steady State:



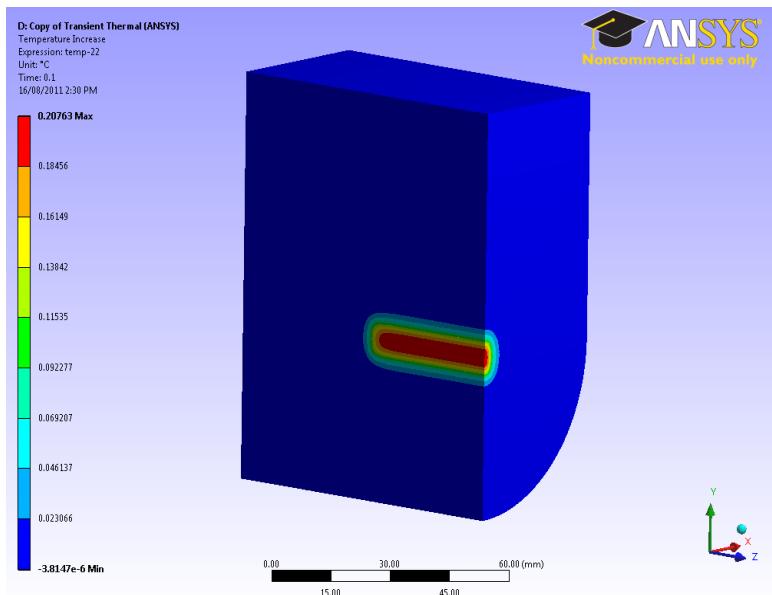
$$T_{max} \ Tu = 115,5 \text{ } ^\circ\text{C} \rightarrow T_{max} \ Total = 138,4 \text{ } ^\circ\text{C}$$
$$T_{max. \ use} \ Tu = 927 \text{ } ^\circ\text{C}$$

The contact between the two parts is assumed perfect.

# Thermal behavior

- The Beam Stopper: **Tungsten**

1 Pulse:



$$T_{max} \tau_u = 22,2 \text{ } ^\circ\text{C}$$

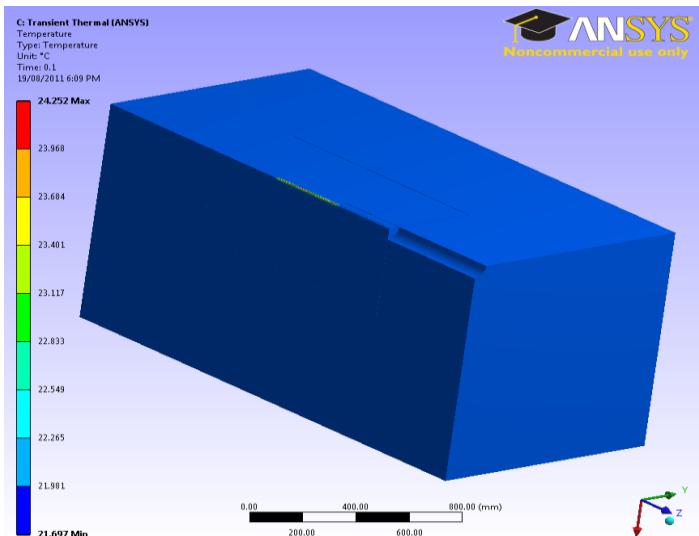
$$T_{max. \text{ use}} \tau_u = 927 \text{ } ^\circ\text{C}$$

NB: results from K. Asvestas

# Thermal behavior

- The Ex dump: Core in **graphite**, second part in **Iron**

1 Pulse:

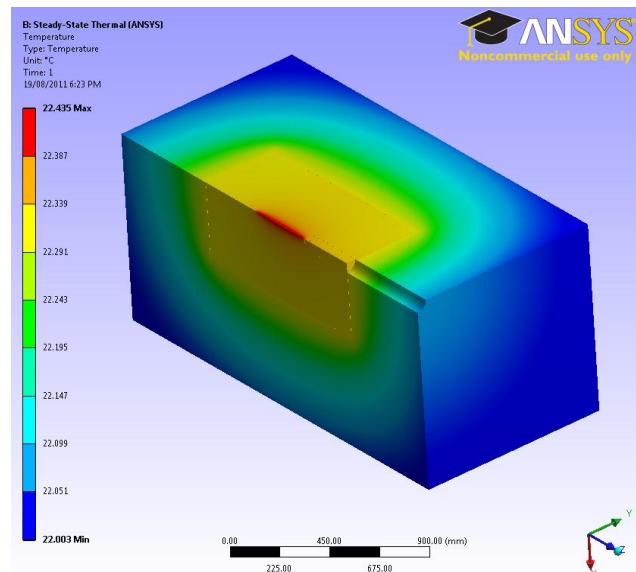


$$T_{max} \text{ Ir} = 24,2 \text{ }^{\circ}\text{C}$$

$$T_{max. \text{ use}} \text{ Ir} = 1530 \text{ }^{\circ}\text{C}$$

NB: results from K. Asvestas

Steady State:



$$T_{max} \text{ Ir} = 22,5 \text{ }^{\circ}\text{C}$$

$$T_{max. \text{ use}} \text{ Ir} = 1530 \text{ }^{\circ}\text{C}$$



$$T_{max} \text{ Total} = 46,7 \text{ }^{\circ}\text{C}$$

The contact between the three parts are assumed perfect.

# Summarize of results

	Temp. Maxi	Service Temp.	Safety Factor	Detailed study needed
<b>Scrapers</b>	63,1	160	<b>2,5</b>	✓
<b>Chopper dump</b>	49,2	3800	<b>77,2</b>	
<b>Internal Dump</b>	138,4	927	<b>6,7</b>	✓
<b>Beam Stopper</b>	22,2	927	<b>41,8</b>	
<b>Ex Dump</b>	46,7	1530	<b>32,8</b>	

➤ **Next step:** the pre-calculation already performed **may be sufficient**. However, it is advised to study more carefully the **Scrapers** and the **Internal dump**.



Thank you for your  
attention.