



# SUPERCONDUCTING TECHNOLOGIES

FOR THE NEXT GENERATION  
OF ACCELERATORS

**WORKSHOP**

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Mikko Karppinen

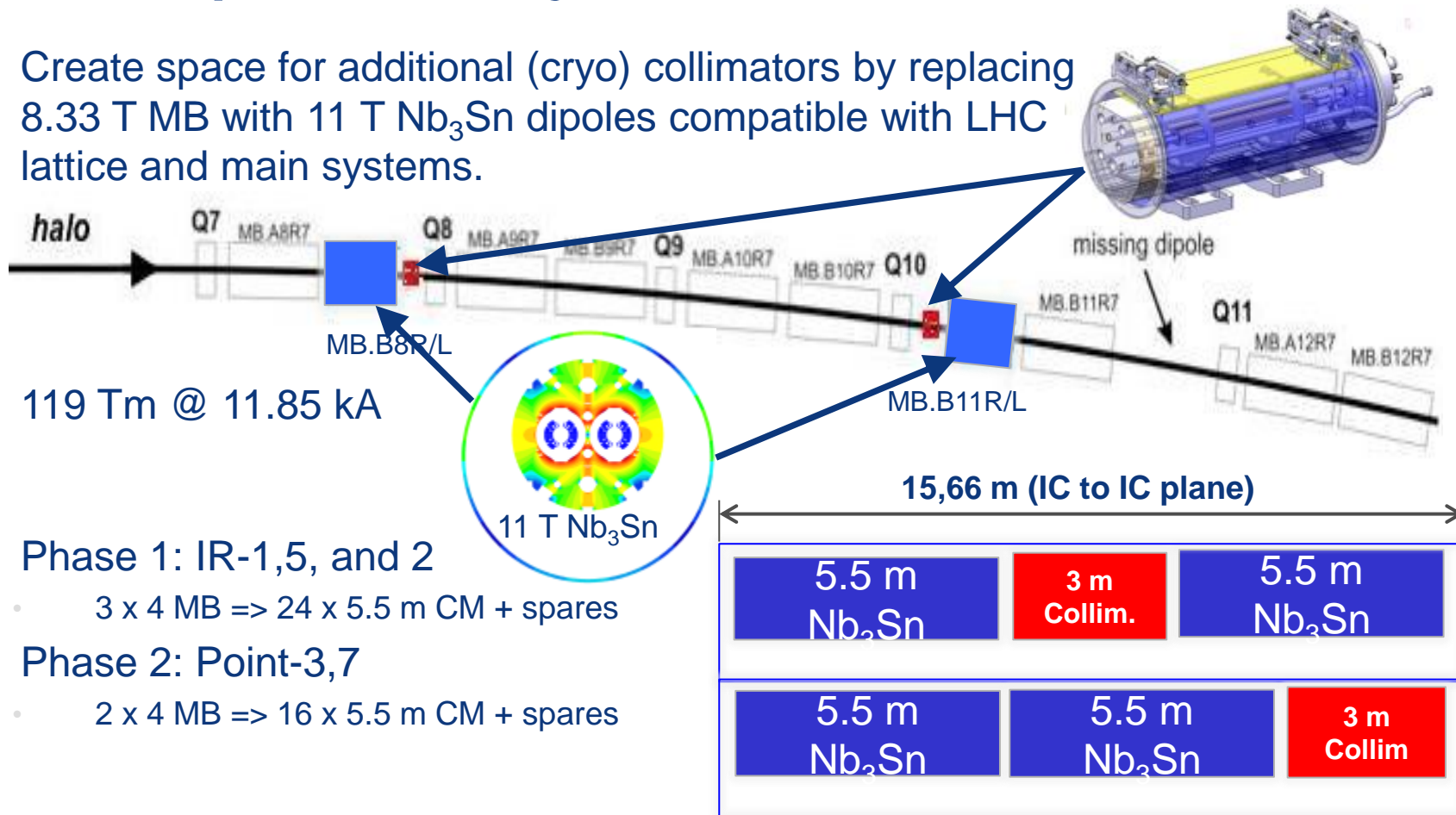
Nb<sub>3</sub>Sn Coil Production for 11 T Dipole Model Magnets

# Outline

- 11 T Project Introduction
- Some Nb<sub>3</sub>Sn features
- Cable insulation
- Coil Fabrication
  - Winding
  - Curing
  - Reaction
  - Splicing
  - Impregnation
  - Instrumentation
  - Handling
- Quality control
- Long tooling procurement plan

# 11 T Dipole Project

- Create space for additional (cryo) collimators by replacing 8.33 T MB with 11 T  $\text{Nb}_3\text{Sn}$  dipoles compatible with LHC lattice and main systems.



- 119 Tm @ 11.85 kA

- Phase 1: IR-1,5, and 2
  - 3 x 4 MB => 24 x 5.5 m CM + spares
- Phase 2: Point-3,7
  - 2 x 4 MB => 16 x 5.5 m CM + spares

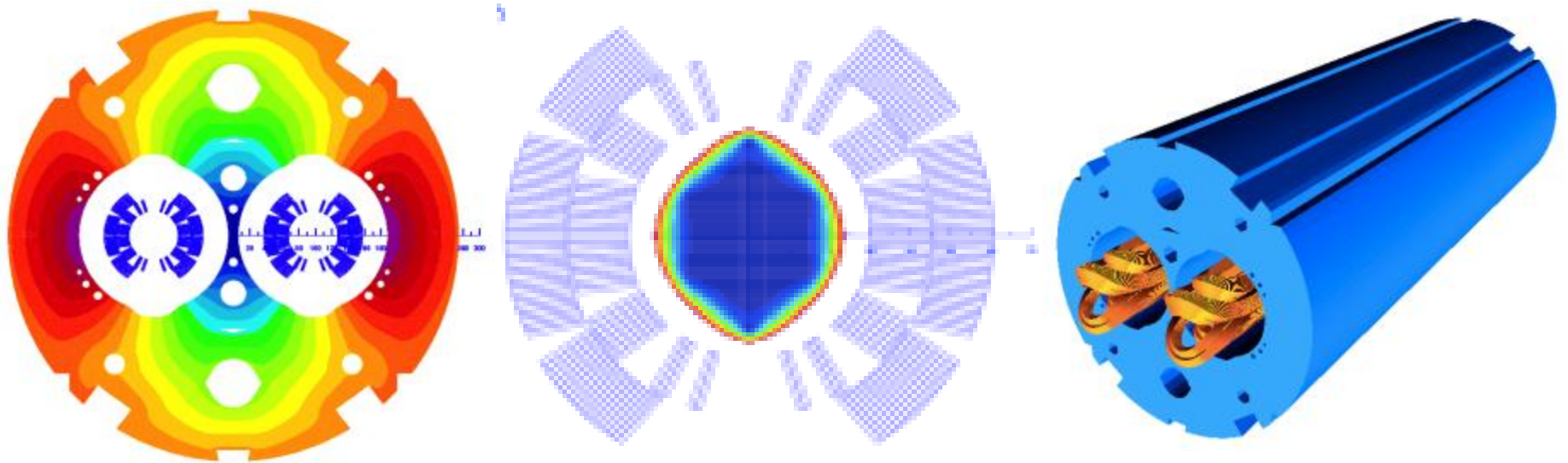
- Joint development program between CERN and FNAL underway since Oct-2010.

# 11 T Dipole Model Program

Date	Description	Length	Remarks	Goals
May-12	1-in-1 Demonstrator Magnet	2 m	Construction at FNAL	Cable technology Coil Technology Quench performance Magnetization effects
Q3-2013	2-in-1 Demonstrator Magnet 1	2 m	FNAL collared coils CM-Assembly at CERN	2-in-1 structure Field quality: - iron saturation - cross-talk - Magnetization effects Quench performance Reproducibility
Q4-2013	2-in-1 Demonstrator Magnet 2	2 m	CERN collared coils CM-Assembly at CERN	
2015	2-in-1 Prototype Cold Mass	5.5 m	Aperture 1 by FNAL Aperture 2 by CERN CM assembly at CERN	Scale-up Long tooling Fabrication of long coils CM assembly Magnetic performance



# 11 T Dipole Magnetic Design

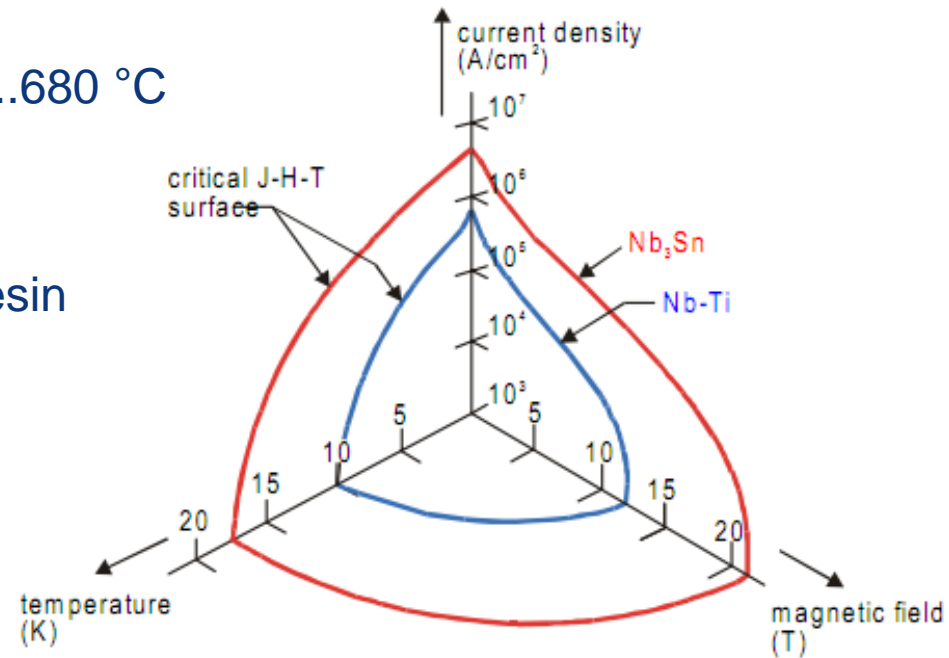


$B_0(11.85 \text{ kA}) = 11.25 \text{ T}$  (20 % margin on the load-line @1.9K)

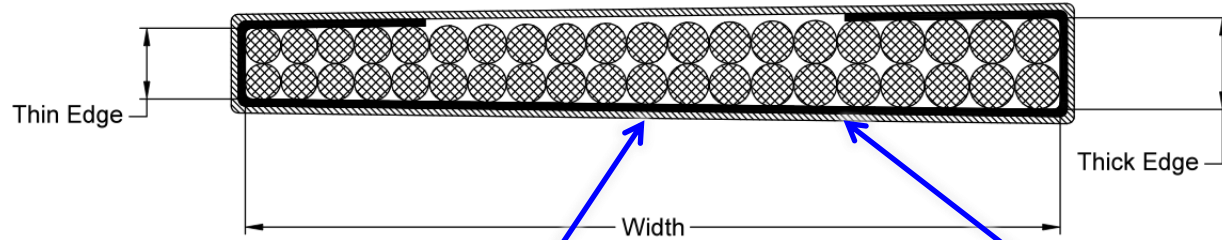
- 60 mm bore and straight cold mass
- Systematic field errors below the  $10^{-4}$  level and conductor positioning at 50..100  $\mu\text{m}$  level
- 6-block design, 56 turns (IL 22, OL 34)
- 14.85-mm-wide 40-strand Rutherford cable, no internal splice
- Coil ends optimized for low field harmonics and minimum strain in the cable

# Nb<sub>3</sub>Sn Superconductor

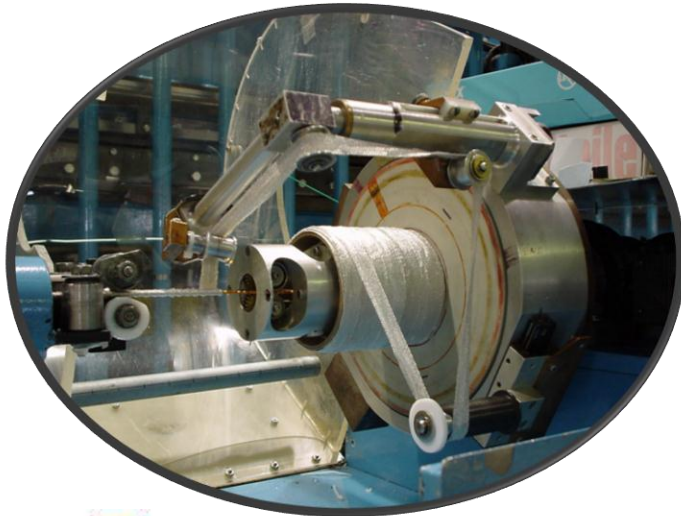
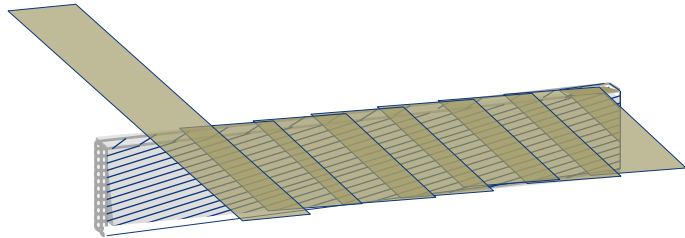
- Nb<sub>3</sub>Sn critical parameters ( $J_c$ ,  $B_{c2}$  and  $T_c$ ) very attractive for accelerator magnets
- Requires (long) **heat treatment** @ 650..680 °C
  - => Only inorganic **insulation** materials
- **Brittle**, strain sensitive after reaction
- Requires **vacuum impregnation** with resin
  - => less efficient heat extraction by He
- Magneto-thermal instabilities
  - => small filaments, small strands, high RRR
- Filaments ~50 μm (NbTi 6 μm)
  - => Persistent current effects
- Sensitive cabling compaction to avoid  $J_c$  degradation (**cable stability**)
- **“Wind and react”**-process most commonly used for accelerator magnets
- Cost ~5 x NbTi



# Cable Insulation

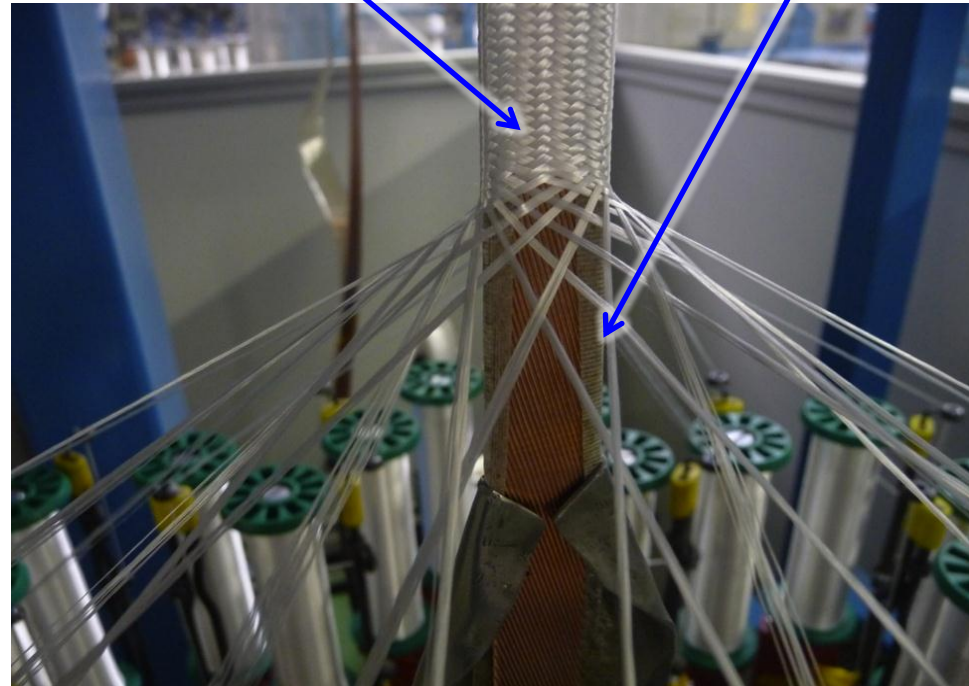


E-glass wrapping



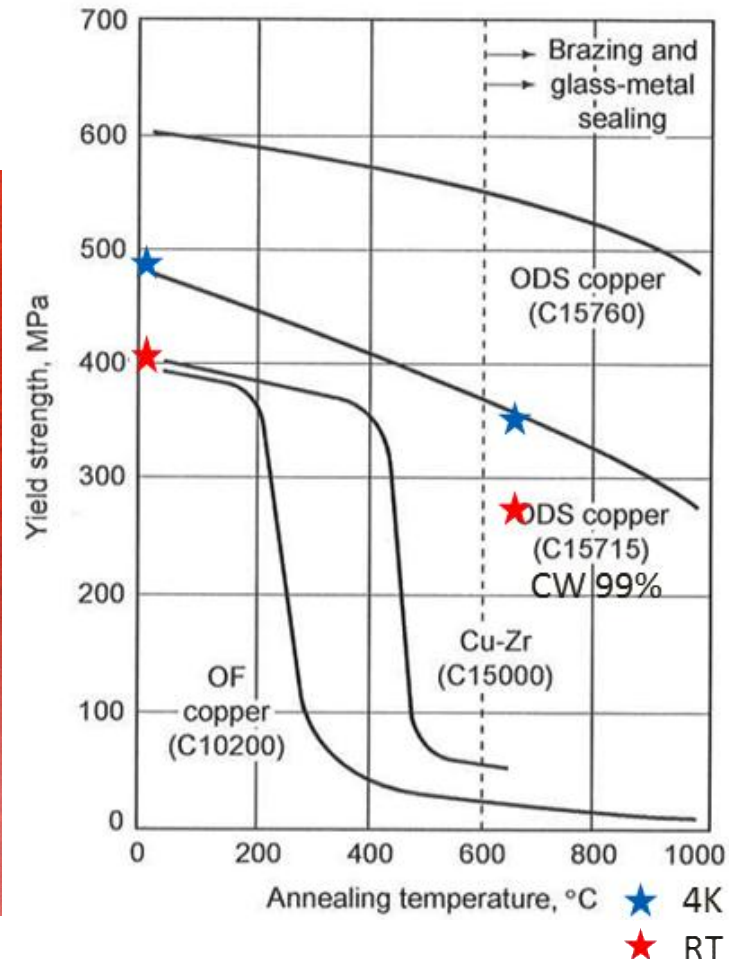
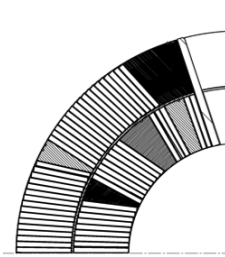
S-2 Glass sleeving

Mica tape



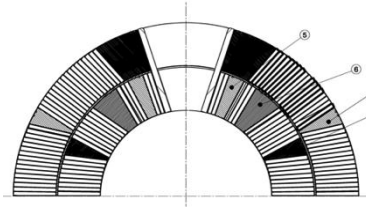
# Coil Components

- 316L End spacers (Selective Laser Sintering)
- ODS (Oxide Dispersion Strengthened) Cu-alloy wedges

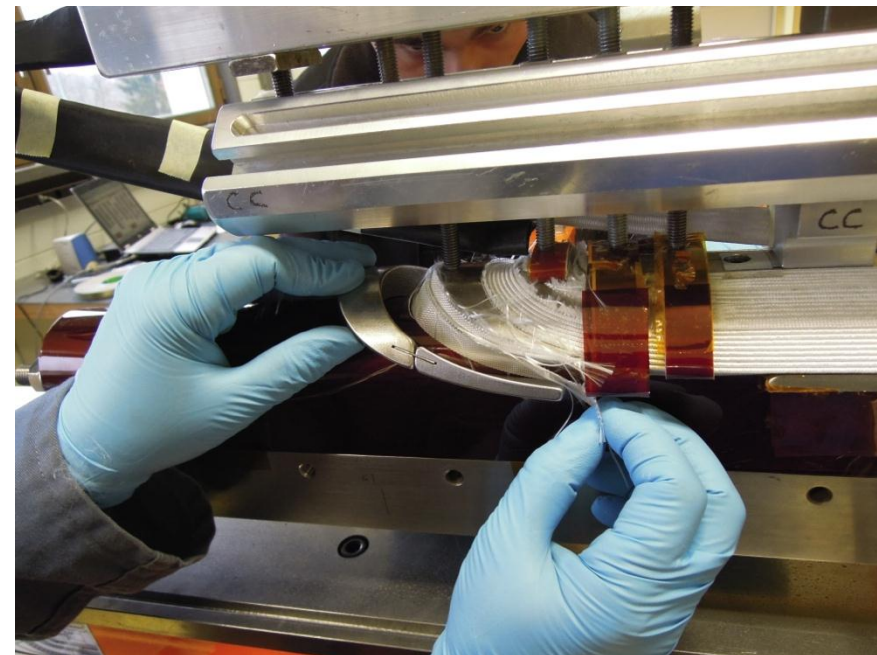
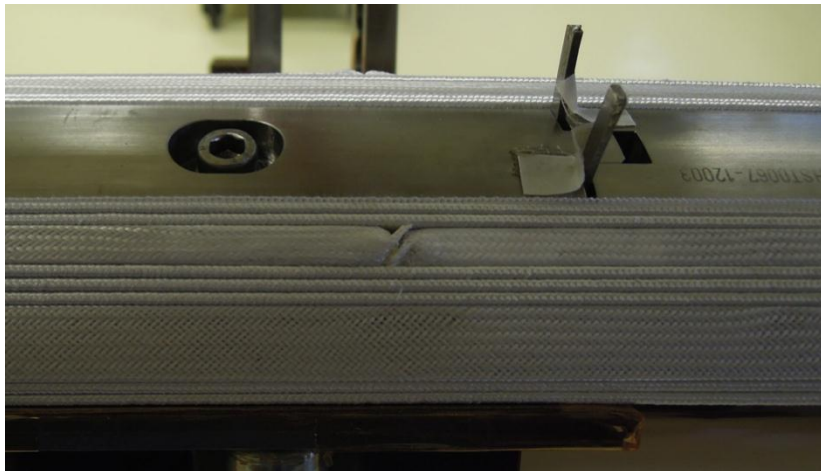
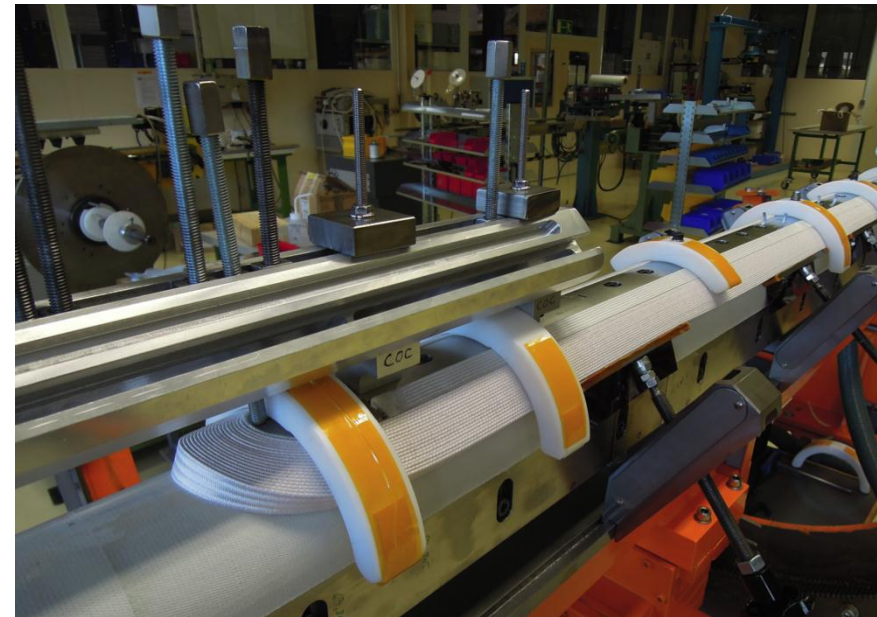




# Winding

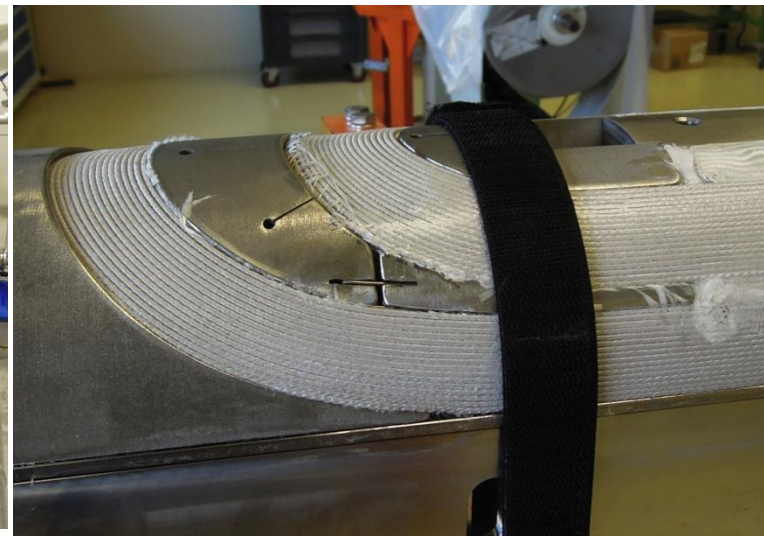
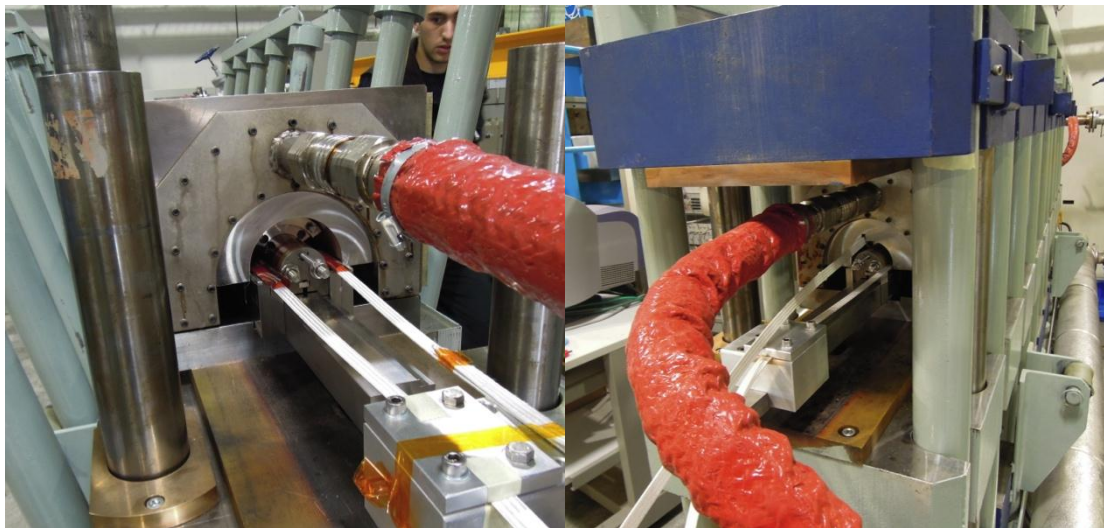


- Relatively low winding tension of 15..30 kg (cable stability)
- End regions require great care to avoid insulation defects
- Outer layer wound on cured inner layer and pre-formed inter-layer insulation



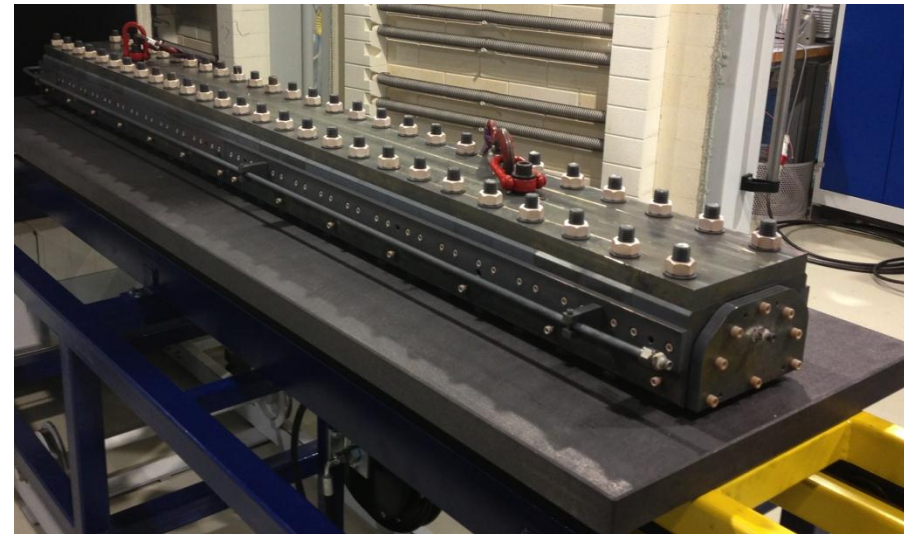
# Ceramic Binder

- After winding of each layer ceramic binder CTD-1202 is applied on the cable insulation
- Coils are cured at at 80°C for 1 h and 150°C for 2h in a closed cavity mold.
- Azimuthal coil pressure is approx. 20 MPa



# Reaction

- Coil size precisely defined by closed cavity mold
- Tooling design allows for coil expansion of 3%/1% in azimuthal/radial direction
- Reaction with positive argon pressure in the tooling
- Modular tooling for easy scale-up



# Reaction..

~10 days

Step #	Type	Start	Rate/time
1	Ramp	20C	25C/hour
2	Soak	210C	72 hours
3	Ramp	210C	25C/hour
4	Soak	400C	48 hours
5	Ramp	400C	50C/hr
6	Soak	640C	48 hours
7	Ramp	640C	-100C/hr



Characteristics	
Available space in the retort (Lxlxh)	2.5m x 0.6m x 0.5m
Max. operating temperature	1000 °C
Temperature uniformity	± 3 °C (25 °C - 750 °C)
Max. temperature ramp up	70 °C/h (20 °C - 900 °C)
Maximum load	600 kg/m
Inert gas atmosphere	YES
Temperature sensor qty / absolute accuracy	20 / ±1 °C Typ K (to 1150°C)
Power	165 kW
Heating zones	5 (controlled and separated in vertical direction)
Manual and Automatic control	YES
Ventilation fan	Yes
Cooling flaps	Yes
Transfer table	Yes

# Splicing

- After reaction the  $\text{Nb}_3\text{Sn}$  leads are carefully cleaned avoiding any mechanical strain to the brittle cables
- The splices between Nb-Ti and  $\text{Nb}_3\text{Sn}$  cables are soldered within the reaction tooling.



# Impregnation

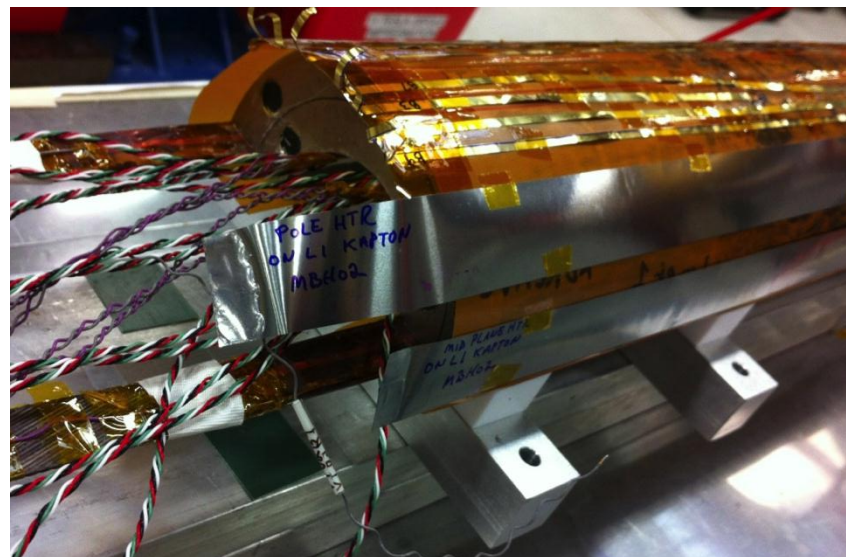
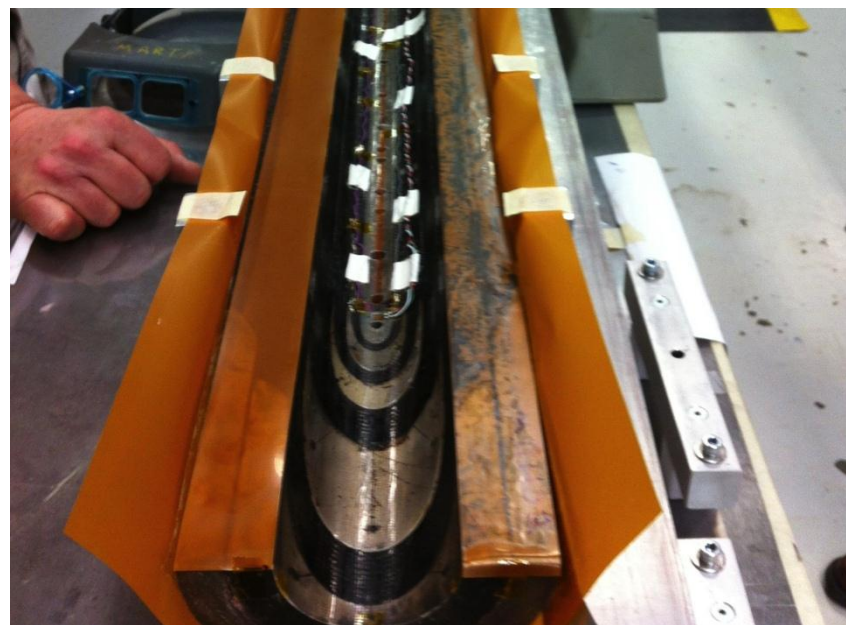
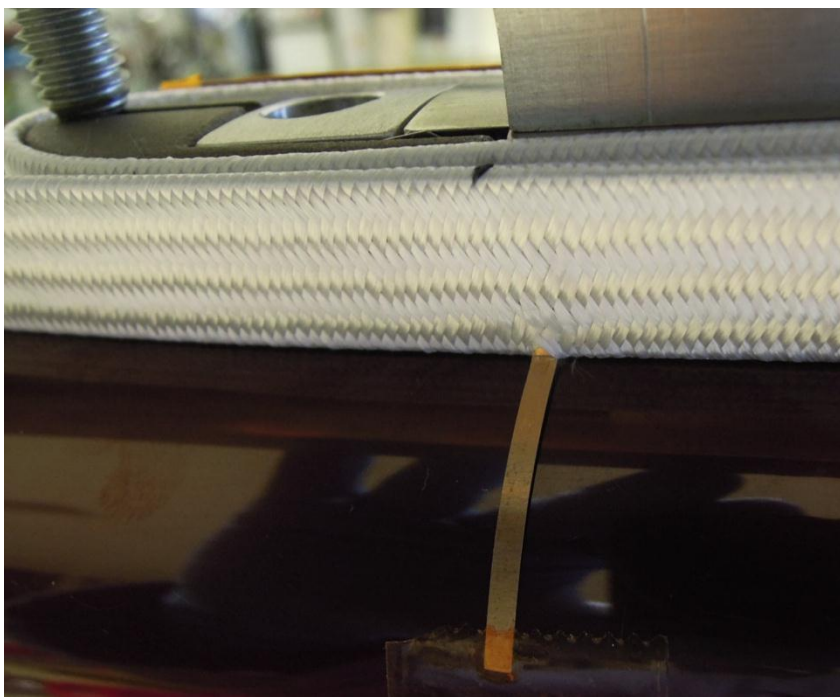
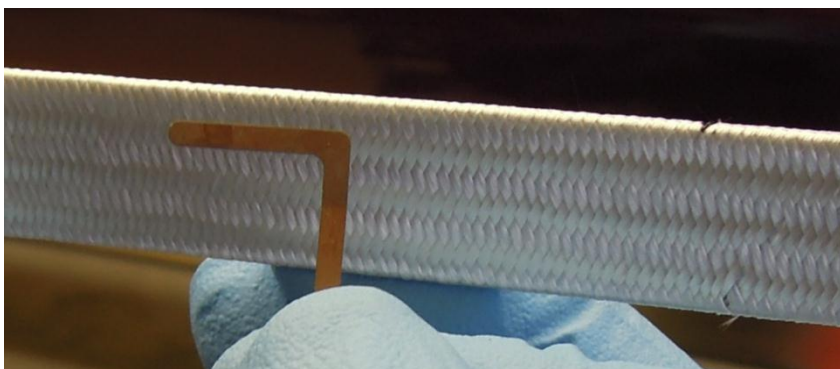
- Reacted coil is transferred from reaction tool into the impregnation mold
- All voids are filled with glassfiber and/or ceramic putty, and possible insulation defects are repaired
- 0.2 mm S2-cloth is applied on the outer surface
- Impregnation with CTD101K in the a vacuum oven at 30-50 mm Hg with epoxy temperature of 60° C
- Curing at 125° C for 21 h



# Impregnation..

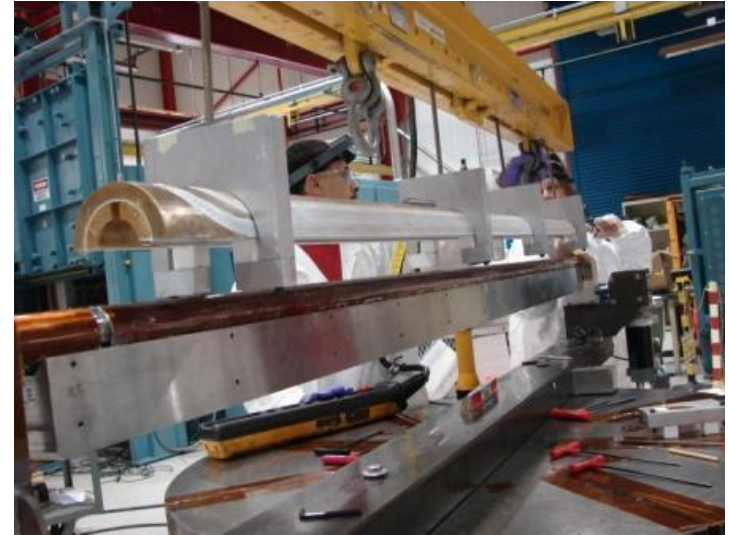
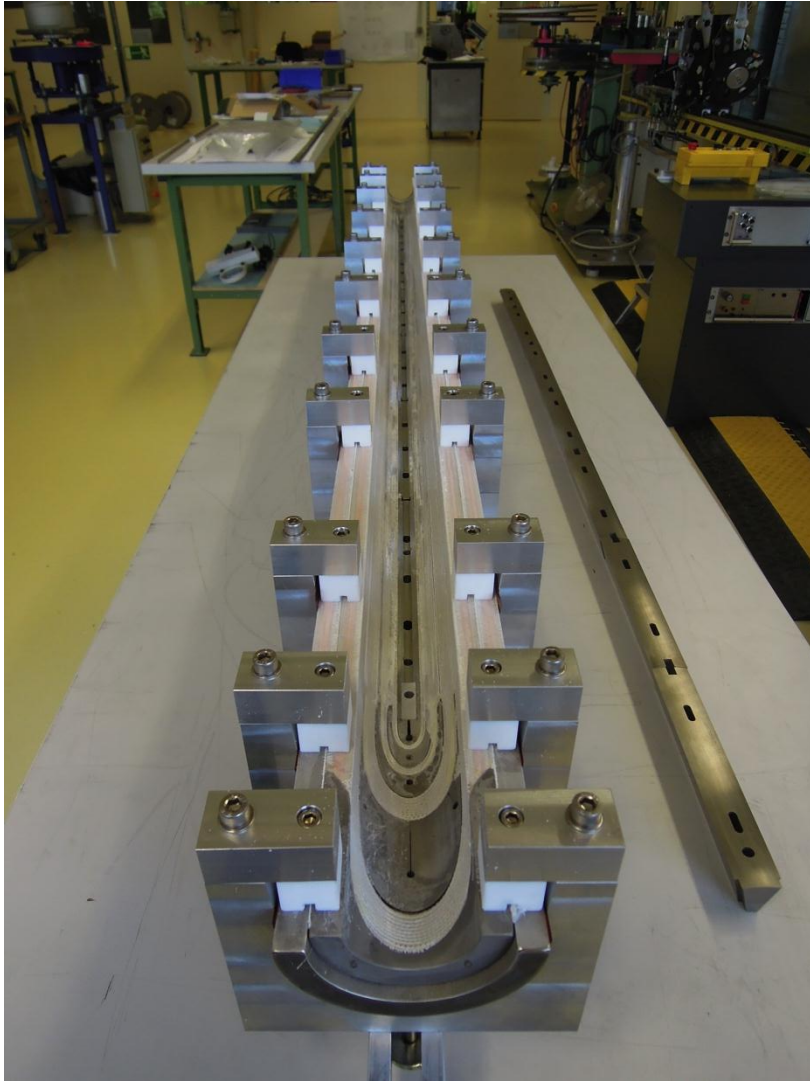


# Instrumentation

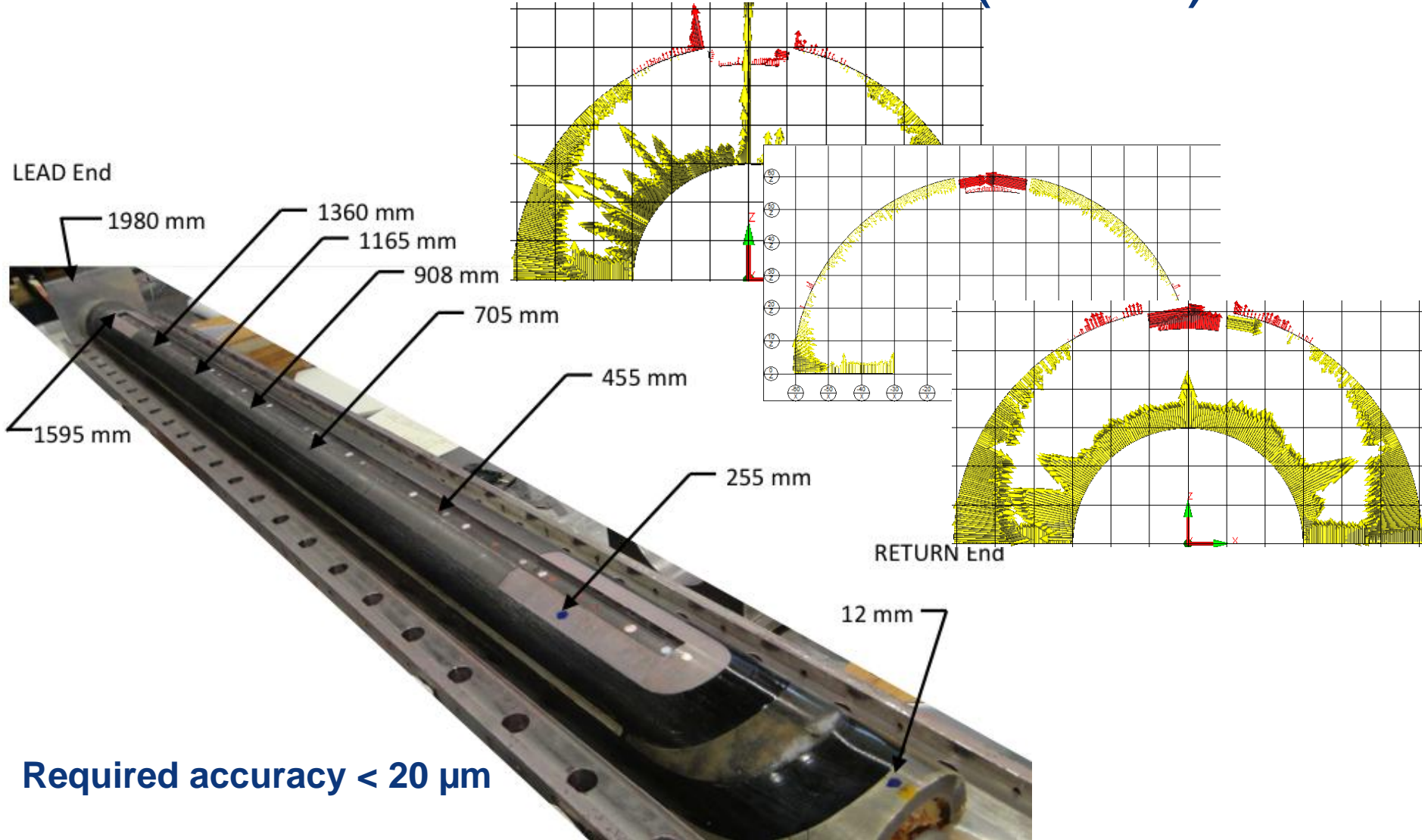




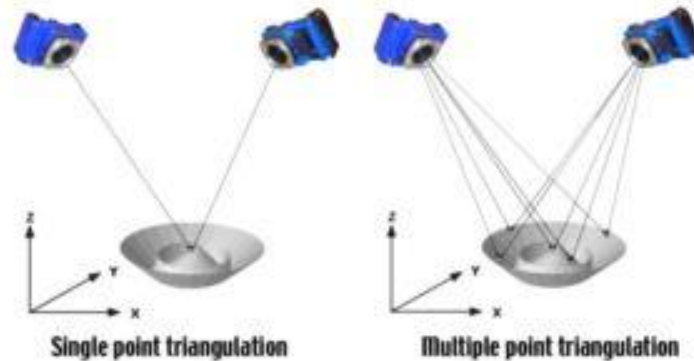
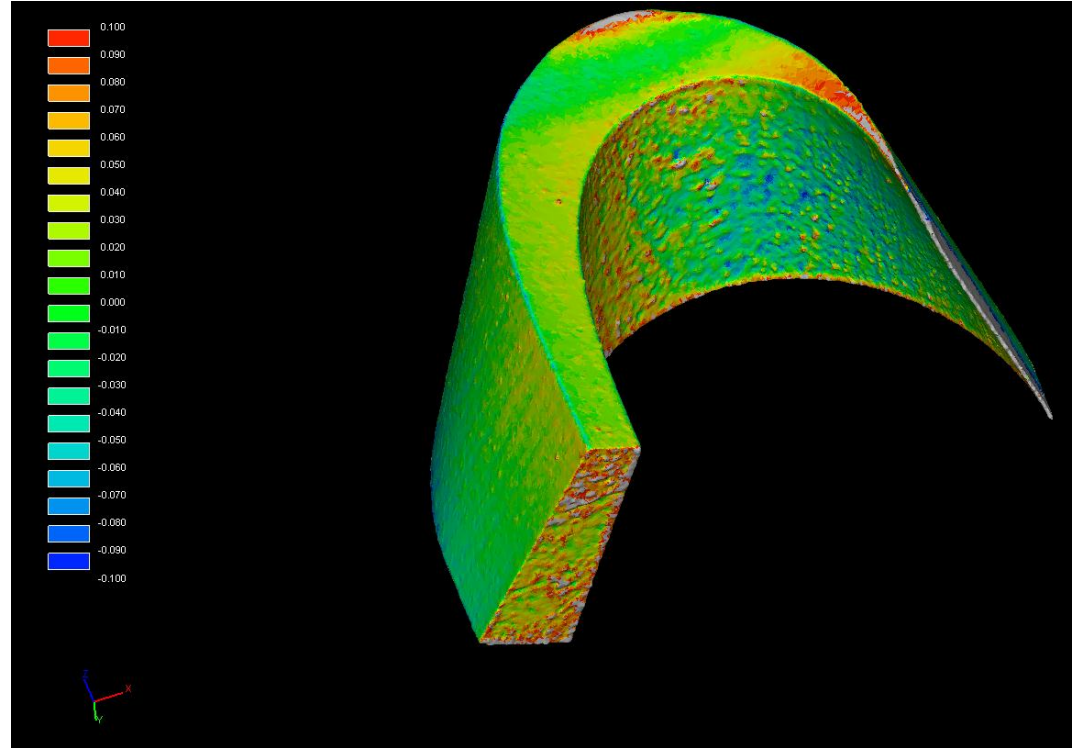
# Handling



# QC: Dimensional Control (CMM)



# QC: Photogrammetry



# Some Cost Indications



220 m of insulated 40-strand Nb<sub>3</sub>Sn cable:  
40 kCHF

A set of 23 end spacers:  
10 (SLS) .. 20 kCHF  
(CNC)

Impreg. Tool (2.5 m):  
50 kCHF

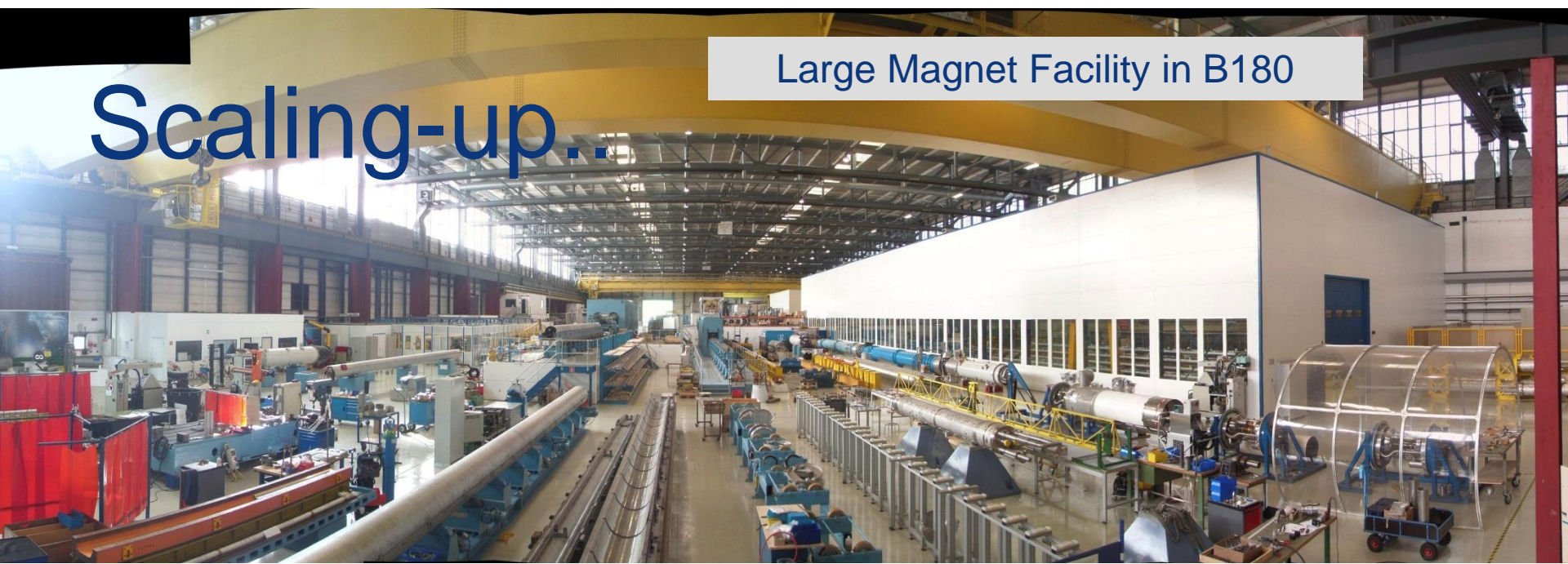
Impreg. System (2.5 m):  
200 kCHF

Reaction furnace (2.5 m):  
250 kCHF

Reaction tool (2.5 m):  
50 kCHF



# Scaling-up..



Curing press – 15 m



Winding machine – 10 m

# Long Tooling Procurement Plan

- Winding machine available
  - Needs to be adapted: length, winding mandrel, integration of the additional spool, process control system upgrade
  - Design work to start in early December
  - First winding trials (with dummy cable) scheduled as from mid-2013
- Curing press available
  - Curing moulds to be developed, design work to start in mid-2013
- Reaction furnace (6.5 m)
  - Market Survey completed
  - Invitation to tender, IT-3861/TE, completed
  - Contract signature expected in January 2013
  - Delivery to CERN expected in the end of 2013
- Impregnation chamber
  - Market Survey, MS-3898/TE, completed
  - IT to be launched in January 2013
  - Contract signature expected in late April 2013
  - Delivery to CERN expected in first quarter of 2014



# Acknowledgements

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