

Beam screen design of the triplet magnets

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AGENDA(*)

- 1. Vacuum Requirements**
- 2. Triplet Region Lay-out, Lattice and Vacuum Model**
- 3. Conductance Calculations**
- 4. Static Pressure**
- 5. Synchrotron Radiation Fans**
- 6. SR-Induced Pressure Rise**
- 7. Engineering/Integration Issues**
- 8. Conclusions**
- 9. References**

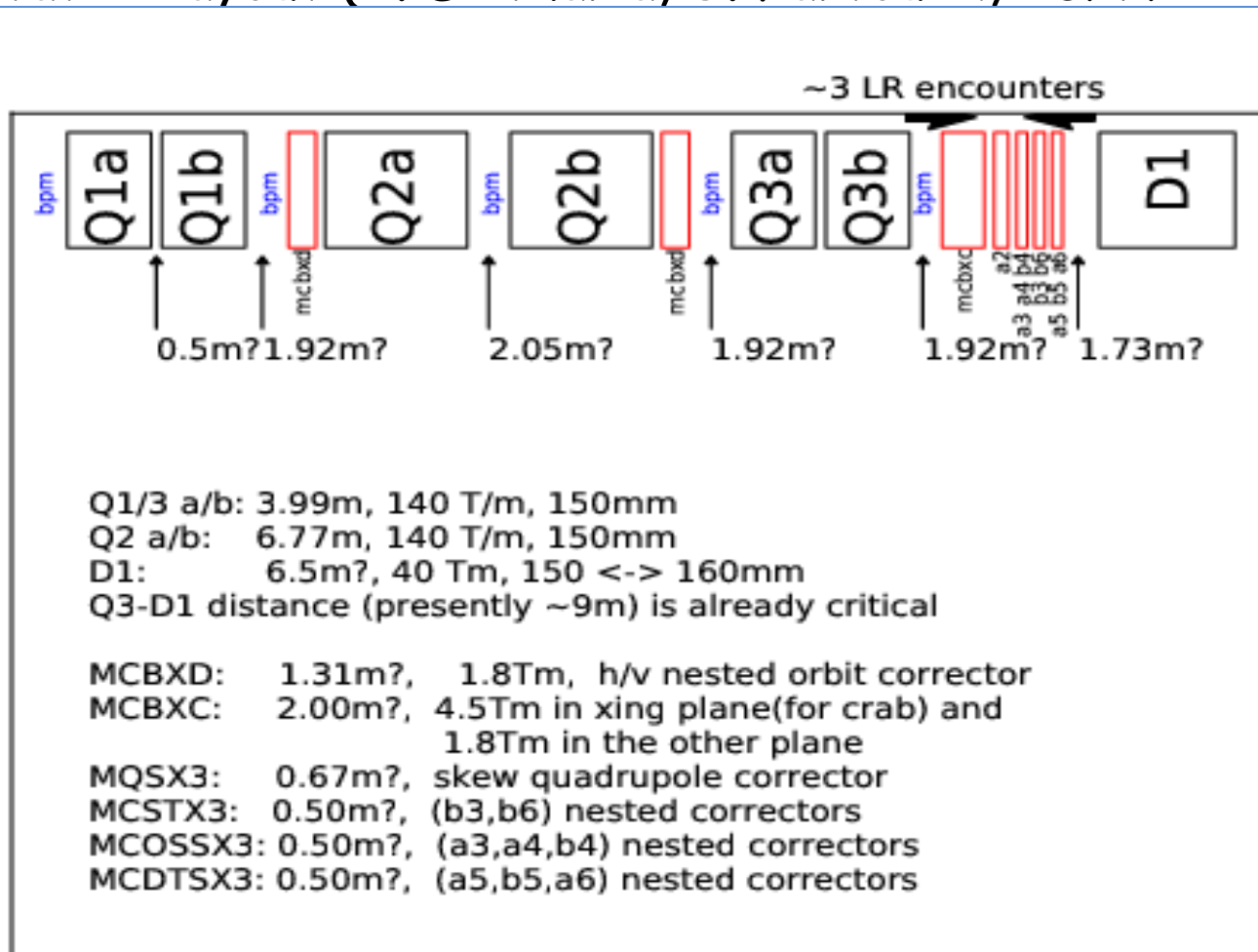
(*) Adapted with modifications from presentation made at HiLumi WP3 meeting of 4/9/12.

1. Vacuum Requirements

- a) Assure a gas pressure better than $6.7 \cdot 10^{-8}$ Pa i.e. better than $9.8 \cdot 10^{14}$ molecules/m³ (H₂-equiv.) @ 5 °K, in order to guarantee a >100 hrs beam lifetime (nuclear scattering from residual gas, as per *LHC Design Report*)
- b) Absorb any **synchrotron radiation-** and **e-cloud-induced** power on a beam-screen at a temperature higher than the 1.9 K of the cold bore
- c) Maintain the pressure below the **critical pressure** limit, where runaway pressure rise may start due to **resonant e-cloud** (to be assessed)

2. Triplet Region Lay-out, Lattice and Vacuum Model

Tentative layout (R. De Maria, S. Fartoukh, 26/7/2012)



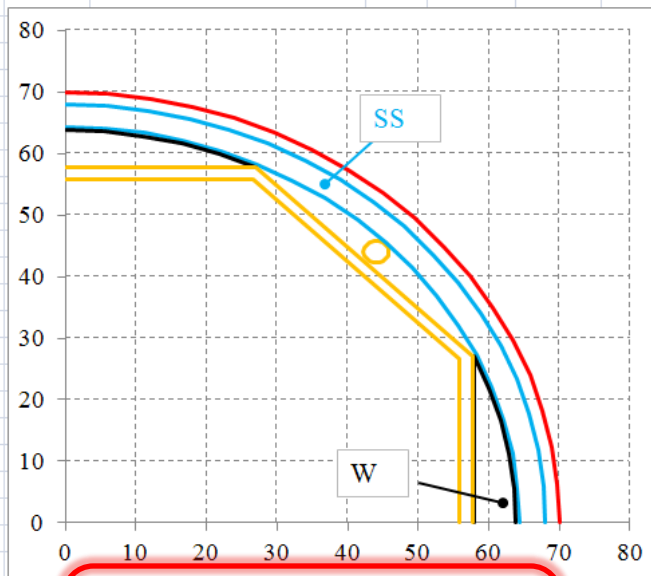
2. Triplet Region Lay-out, Lattice and Vacuum Model

- The area between Q1 and D1 has been modeled using two Montecarlo codes (R. Kersevan, M. Szakacs) :
 - a) **SYNRAD+** , ray-tracing MC code
 - b) **Molflow+**, Test-Particle MC code
- A 3D model has been made, taking the 2D cross-section of the cold-bore (140 mm ID) as per Excel file of E. Todesco (private comm. 10/7/12) and adding the proper number of pumping slots and pumping slot shields as installed on the LHC arc dipole beam-screens.

2. Triplet Region Lay-out, Lattice and Vacuum Model

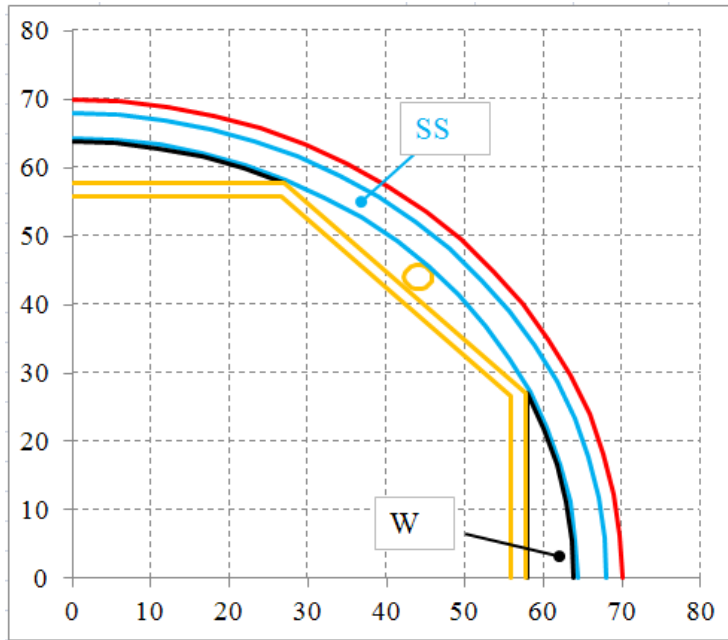
2D model showing the cross-section of the cold-bore (140 mm ID) (E. Todesco, private comm. 10/7/12)

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	
10				Cold bore thickness	(mm)	3.7				25	0.44	29.6	63.4	28.7	61.6	27.2	58.3					27.0	57.8	43.7	45.8	
11				Cold bore inner radius	(mm)	64.3				30	0.52	35.0	60.6	34.0	58.9	32.2	55.7					0.0	57.8	43.2	45.6	
12				Clearance beam screen - cold bore	(mm)	0.5				35	0.61	40.2	57.3	39.0	55.7	36.9	52.7							42.7	45.2	
13				Beam screen thickness	(mm)	2.0				40	0.70	45.0	53.6	43.7	52.1	41.3	49.3							42.4	44.7	
14				Beam screen outer	(mm)	57.8				45	0.79	49.5	49.5	48.1	48.1	45.5	45.5							42.3	44.1	
15				Beam screen inner	(mm)	55.8				50	0.87	53.6	45.0	52.1	43.7	49.3	41.3							42.4	43.4	
16				W inserts thickness	(mm)	6.0				55	0.96	57.3	40.2	55.7	39.0	52.7	36.9							42.7	42.9	
17				Inner radius beam 0 degrees	(mm)	55.8				60	1.05	60.6	35.0	58.9	34.0	55.7	32.2						57.8	0.0	43.2	42.5
18										65	1.13	63.4	29.6	61.6	28.7	58.3	27.2						57.8	27.0	43.7	42.3
19										70	1.22	65.8	23.9	63.9	23.3	60.4	22.0						60.0	21.8	44.4	42.3
20										75	1.31	67.6	18.1	65.7	17.6	62.1	16.6						61.6	16.5	45.0	42.5
21										80	1.40	68.9	12.2	67.0	11.8	63.3	11.2						62.8	11.1	45.4	42.9
22										85	1.48	69.7	6.1	67.7	5.9	64.1	5.6						63.6	5.6	45.7	43.4
23										90	1.57	70.0	0.0	68.0	0.0	64.3	0.0						63.8	0.0	45.9	44.1

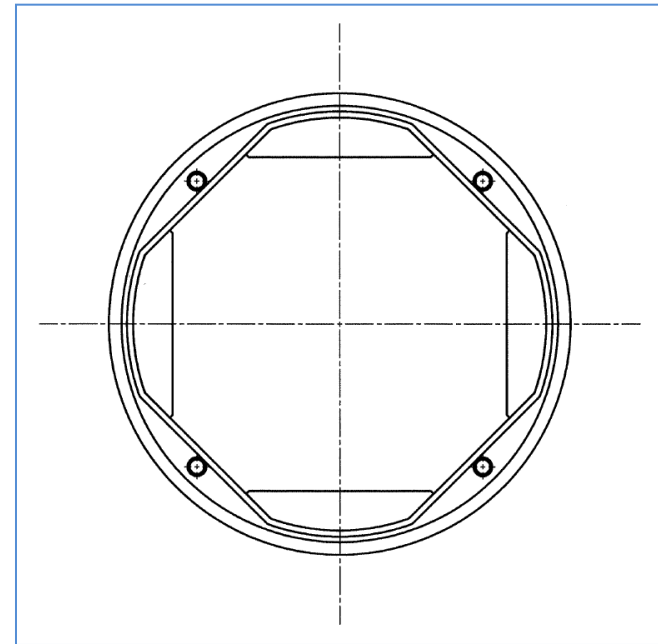


40	Linear weight Cold bore	(kg/m)	12.6
41	Linear weight Cu	(kg/m)	7.2
42	Linear weight W	(kg/m)	7.8
43			26.8

2. Triplet Region Lay-out, Lattice and Vacuum Model



1/4th of 2D model showing the cross-section of the
140 mm ID cold-bore
(E. Todesco, private comm. 10/7/12)

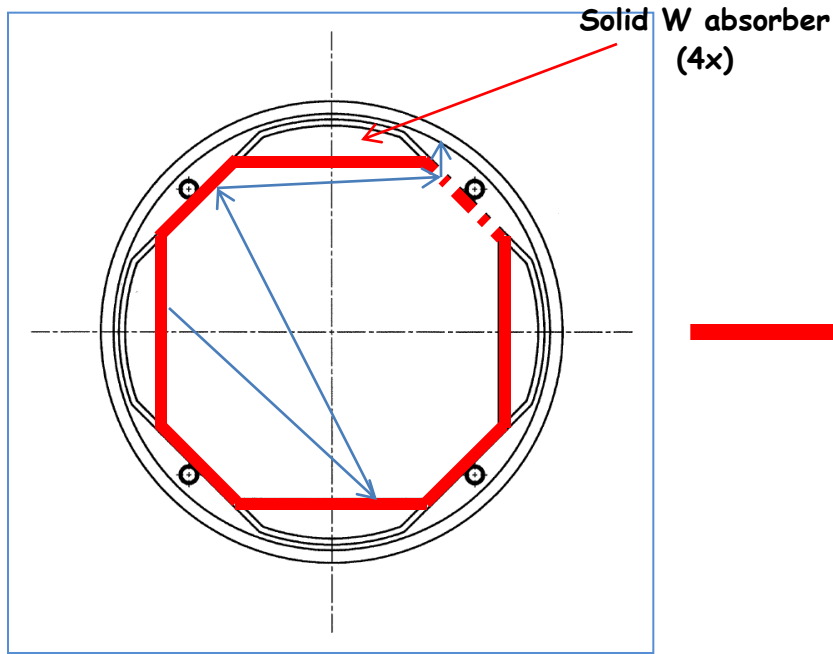


Starting point: drawing LHCVSSX_0004
6/10/2009, "Phase 1 Upgrade"
(re-scaled to 140 mm cold-bore ID, and 6mm W shielding)

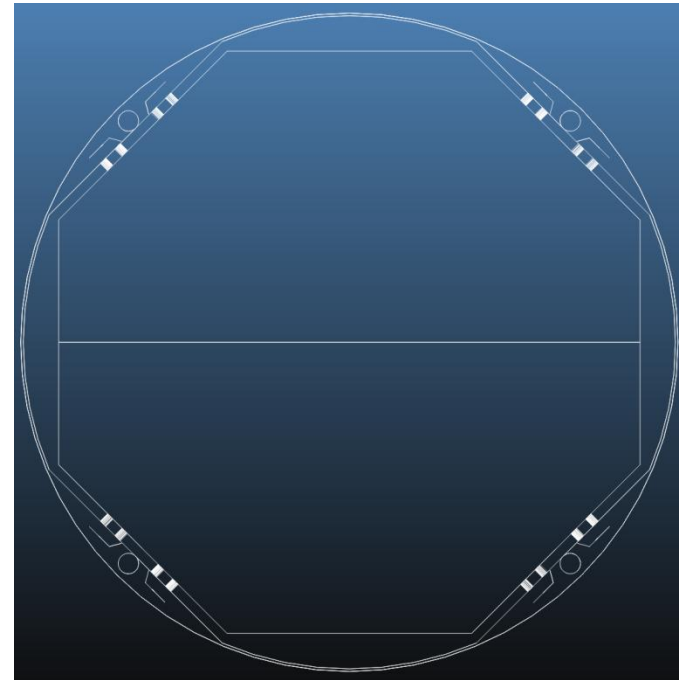
Conceptual 3D Model of 140 mm ID (cold bore, CD) Beam Screen (BS):

- W radiation shield is placed **EXTERNALLY** to the BS (see next slide)
- 4x4 Pumping Slots, racetrack-shaped like in the LHC arcs' BS have been added (see below), with a longitudinal spacing of 16 mm.

3. Conductance calculations



Drawing LHC VSSX_0004
6/10/2009, "Phase 1 Upgrade"
(not to scale) with superposed octagonal BS
(BS shields not shown)

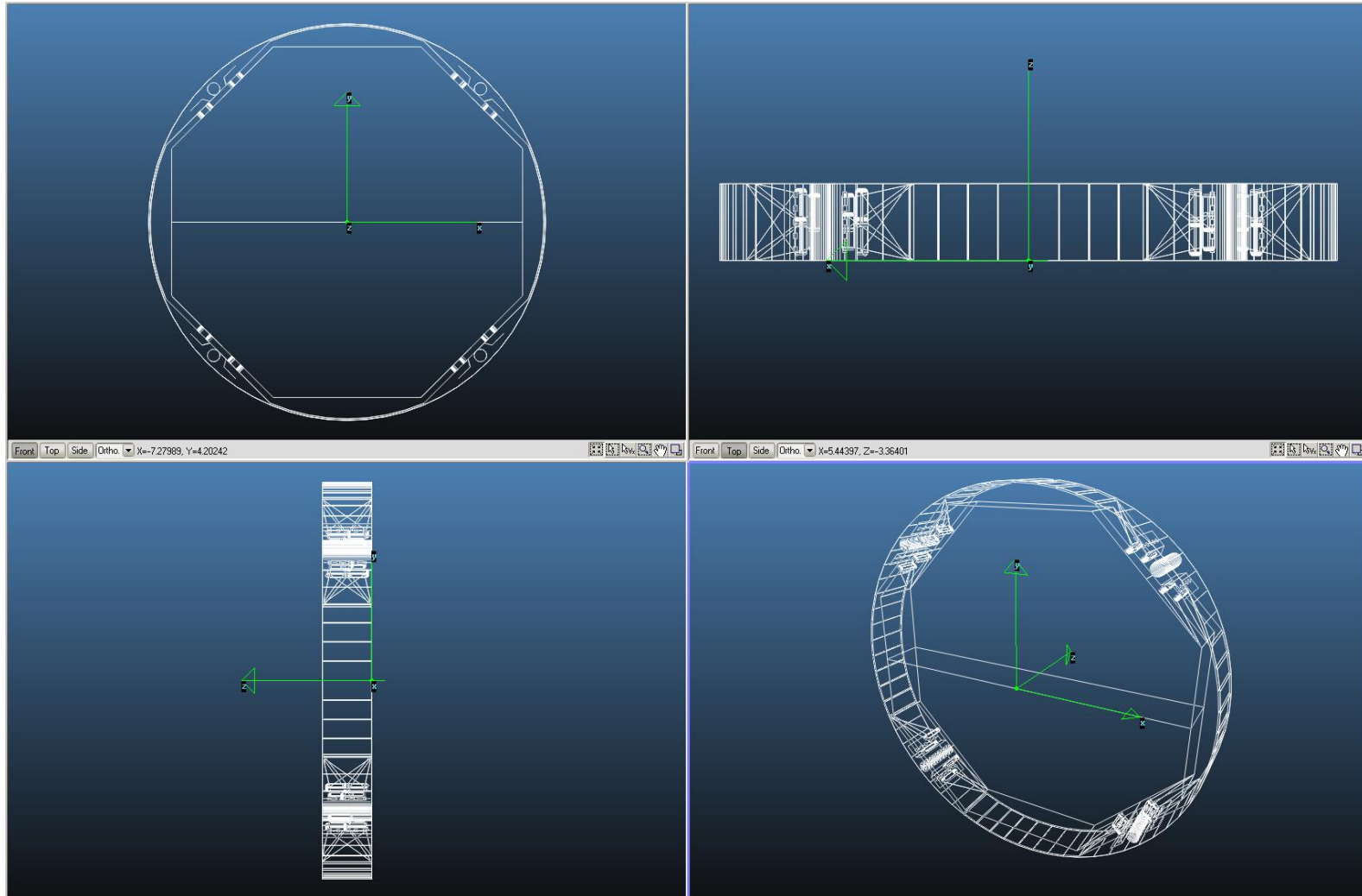


Front-view of 140 mm ID CB BS, with racetrack-shaped
pumping slots and 4x pumping slots shields
(as per LHC's arc BS): Molflow+ model

Conceptual 3D Model of 140 mm ID (cold bore, CD) Beam Screen (BS):

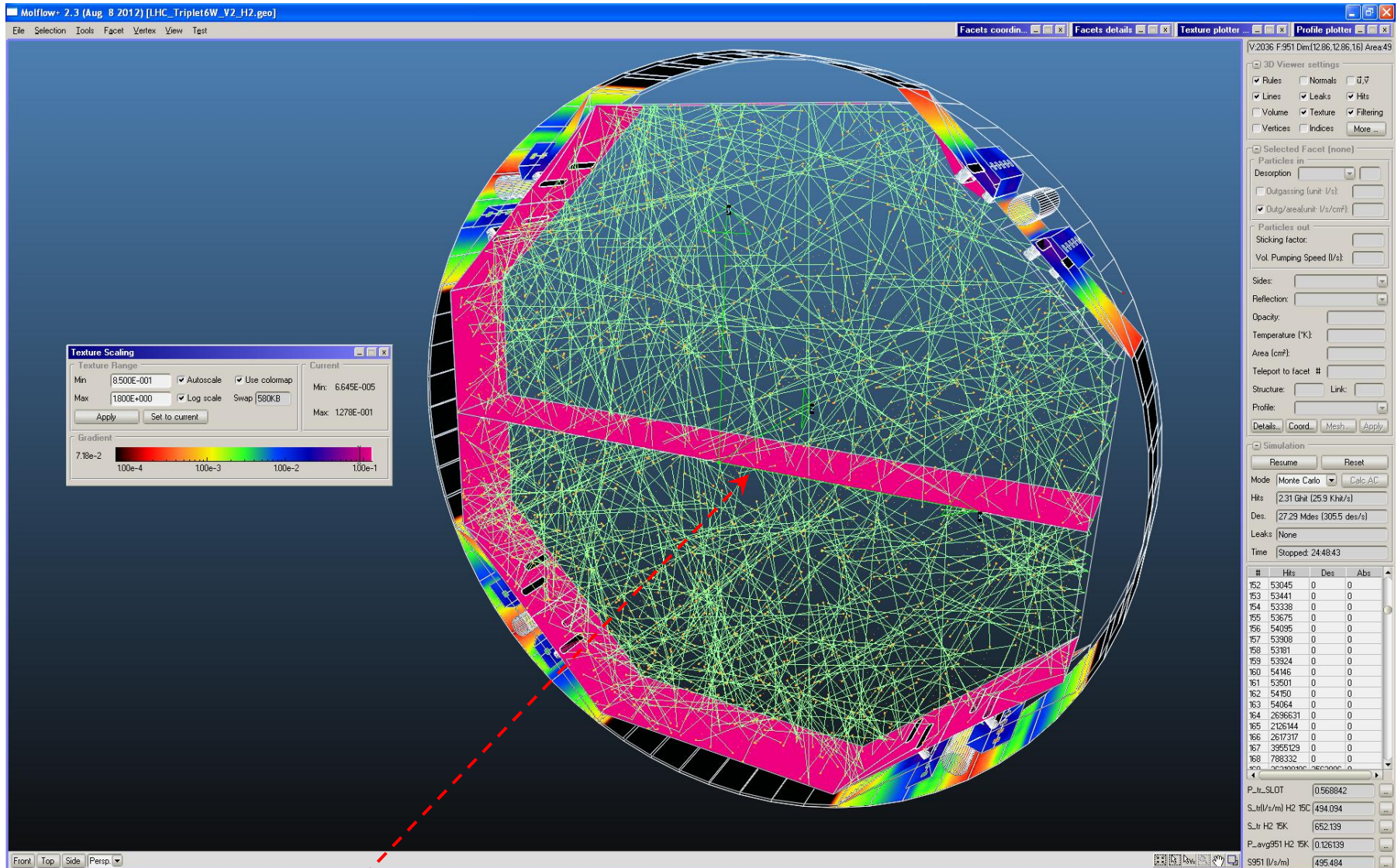
- 2 mm-thick BS is kept at between 5 and 20 °K by means of 4x 3/16" OD stainless steel pipes. Inside surface **must** be copper coated or **SS/Cu co-laminated**
- W radiation shield is fixed **EXTERNALLY** to the BS (see next slide)
- 4x4 Pumping Slots, racetrack-shaped like in the LHC arcs' BS have been added (see below)
- Molecules are cryopumped on the cold-bore

3. Conductance calculations



**Molflow+ screen shot of 1.6 cm long periodic boundary condition slice
The model has 2036 vertices and 951 facets**

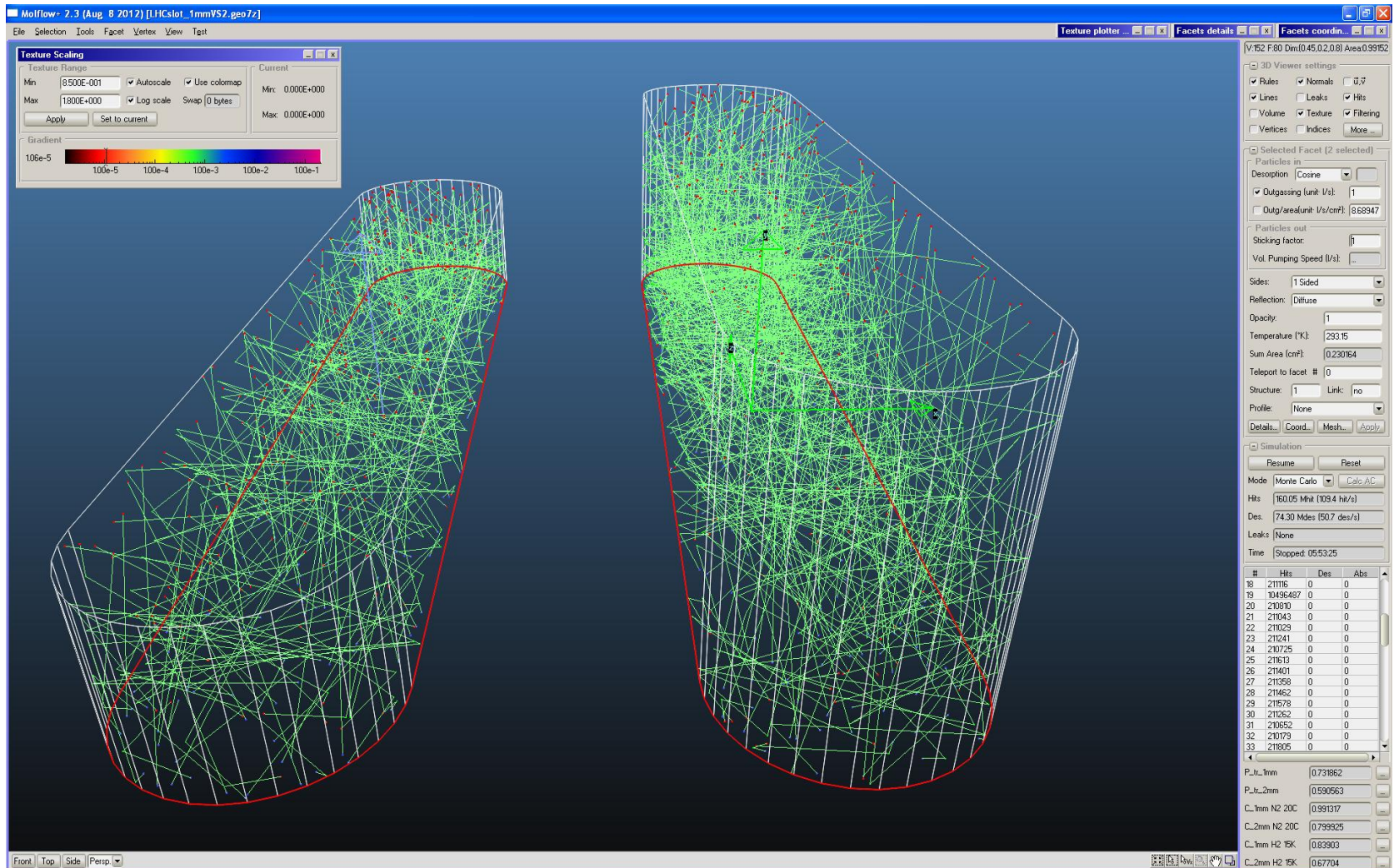
3. Conductance calculations



- The conductance of the 4x4 pumping slots is calculated by computing the transmission probability for molecules to go from inside the BS to outside
- The effective pumping speed for H₂ is calculated by taking the reciprocal of the average pressure along the virtual facet inside the BS.

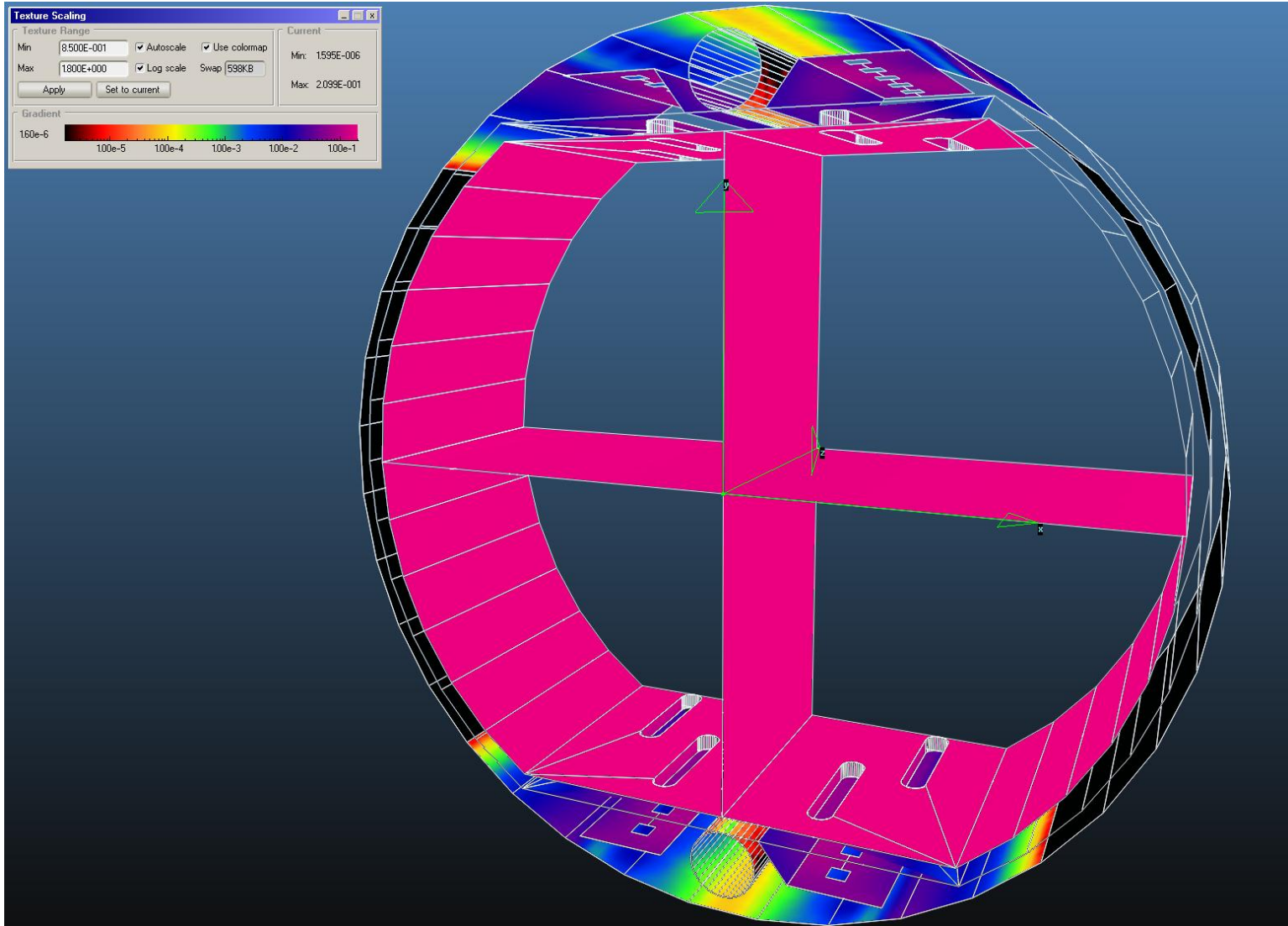
3. Conductance calculations

The conductance of each single slot is obtained here: for the 1 mm-thick slot (left) of the LHC arc dipole BS it is 0.99 l/s (N_2 at $20^\circ C$), while for the 2 mm-thick proposed for the Triplet BS it is 0.80 l/s, 20% less, but there are now 2x as many slots per unit axial length (16 vs 8)



3. Conductance calculations

LHC arc dipole 1.6 cm-long slice, with 1 mm-thick BS and two perpendicular virtual facets showing that pressure/gas density is \sim uniform inside the BS



3. Conductance calculations

- After doing some normalization to account for the gas mass and the temperature of the BS, we can summarize the pumping slot calculations by saying that the Triplet/D1 octagonal BS (at an average temperature of 15°K) has a specific pumping speed for H₂ of 677 l/s/m, vs a speed of 419.5 l/s/m for the LHC arc dipole BS.
- Since we are interested into calculating pressure profiles **ALONG** the beam path, we need also to compute the longitudinal conductance (called specific conductance, units are l·m/s) of the proposed Triplet/D1 BS.
- In general terms, other than for a shape-factor k ($0 < k \leq 1$) taking into account how far from circular the cross-section is, the specific conductance is proportional to the cross-sectional area and inversely proportional to the square of the chamber perimeter.
- The shape-factor k is not in general analytically computable, that's where MC simulations come to the rescue.

3. Conductance calculations

- The specific conductance of the two BS (LHC arc dipole and Triplet/D1) are calculated by means of the transmission probability and, as a confirmation, by fitting the MC-simulated pressure profile to an analytical model of parabolic pressure for uniform longitudinal outgassing yield:

$$P(z) = \frac{A}{2c} (Lz - z^2) + \frac{Q}{S}$$

- Where c is the specific conductance, A the specific outgassing yield (i.e. mbar·l/s/m), L the length of the BS profile (5m here, to reduce end effects), Q the gas load (=A·L), and S the pumping speed at the tube's ends
- The two values are (N₂ at 20°C):

a) LHC arc dipole BS:	10.43 l·m/s
b) Triplet BS:	186.90 l·m/s

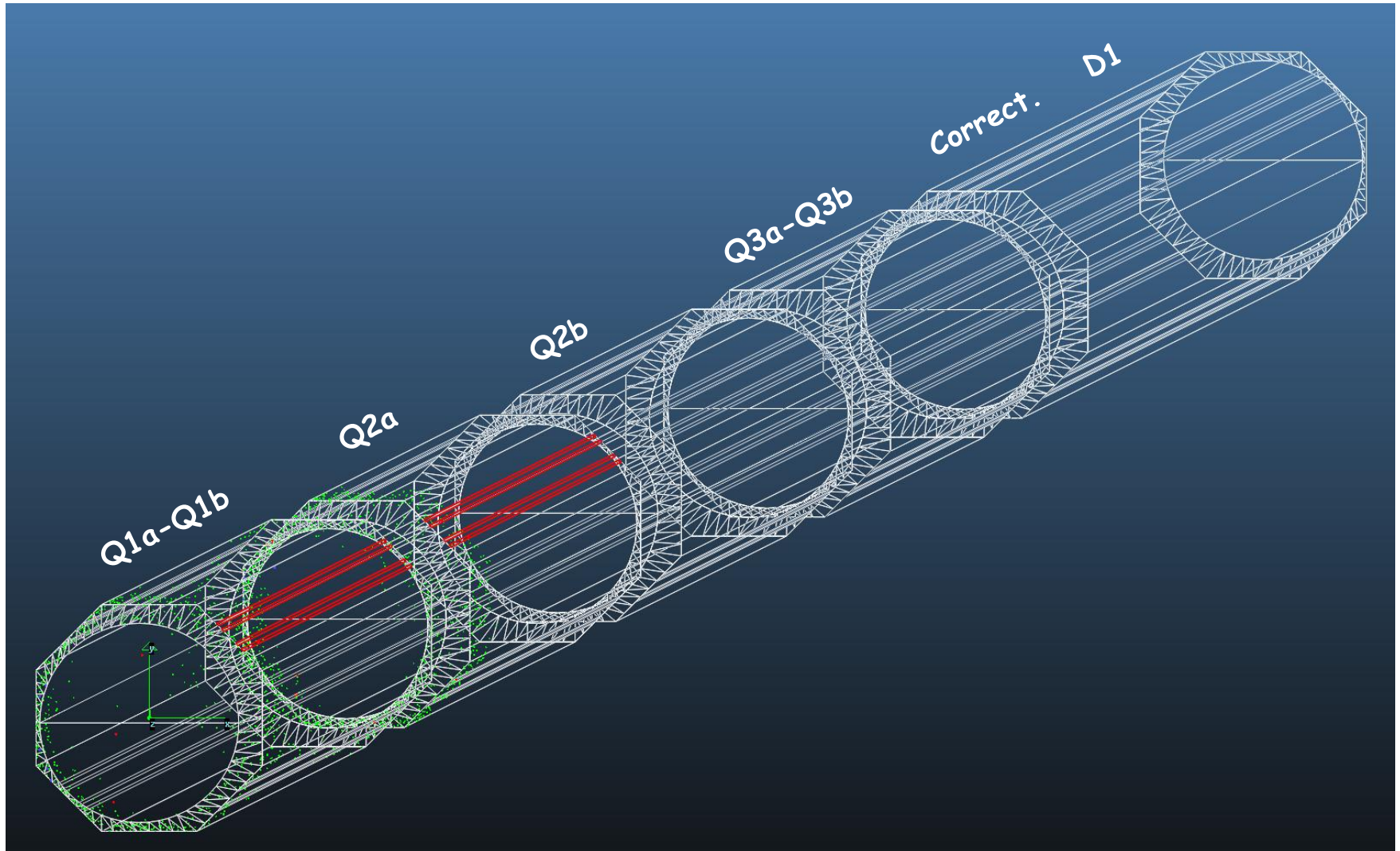
4. Static Pressure

- According to the lattice discussed in sec.2, a 3D model has been made of the internal geometry of the Triplet/D1 area BS
- To speed-up the calculation, the $16 \times 62.5 = 1000$ slots per meter of axial length are simulated by long rectangular strips having an *equivalent* sticking coefficient s_{equiv} which takes into account the transmission probability of the real slots: $s_{equiv} = 0.27284$
- There are 5 independent BSs, one for each of the Q1a-Q1b, Q2a, Q2b, Q3a-Q3b and D1 (including 5 correctors^(*)), connected by 100 mm ID circular pipes with tapered conical transitions (see below)
- Uniform thermal outgassing is supposed to take place on all non-pumping surfaces. Octagonal-to-round conical transitions of 0.5 m axial length are placed at either end of each cryostat
- Pumping of some sort is simulated at both ends (50% sticking probability). No pumping in the interconnects (NO BS, BPMs, sliding bellows: possibility of "floating" temperature NOT modeled)

(*) The 5 correctors have NOT been modeled as a stand-alone cryostat

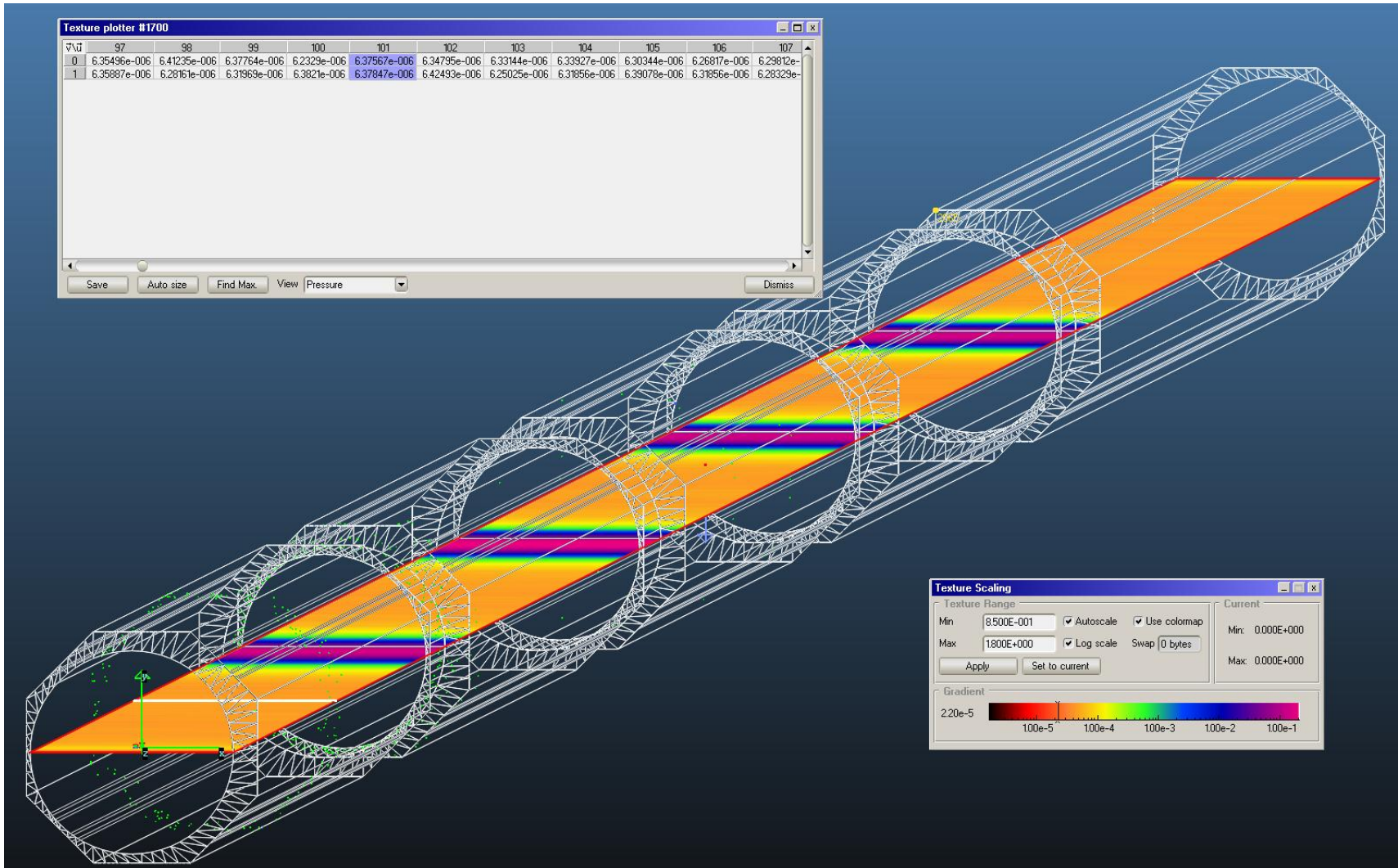
4. Static Pressure

The model looks like this. Highlighted in red are 8 of the equivalent pumping slot areas, 4 on each of the leftmost 2 cryostats



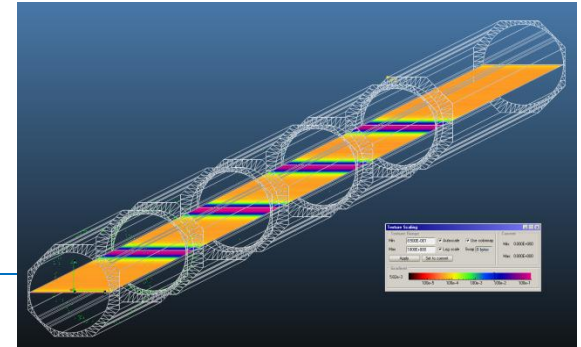
4. Static Pressure

The pressure can be visualized by using a colored texture along a virtual facet placed along the axis of the chamber

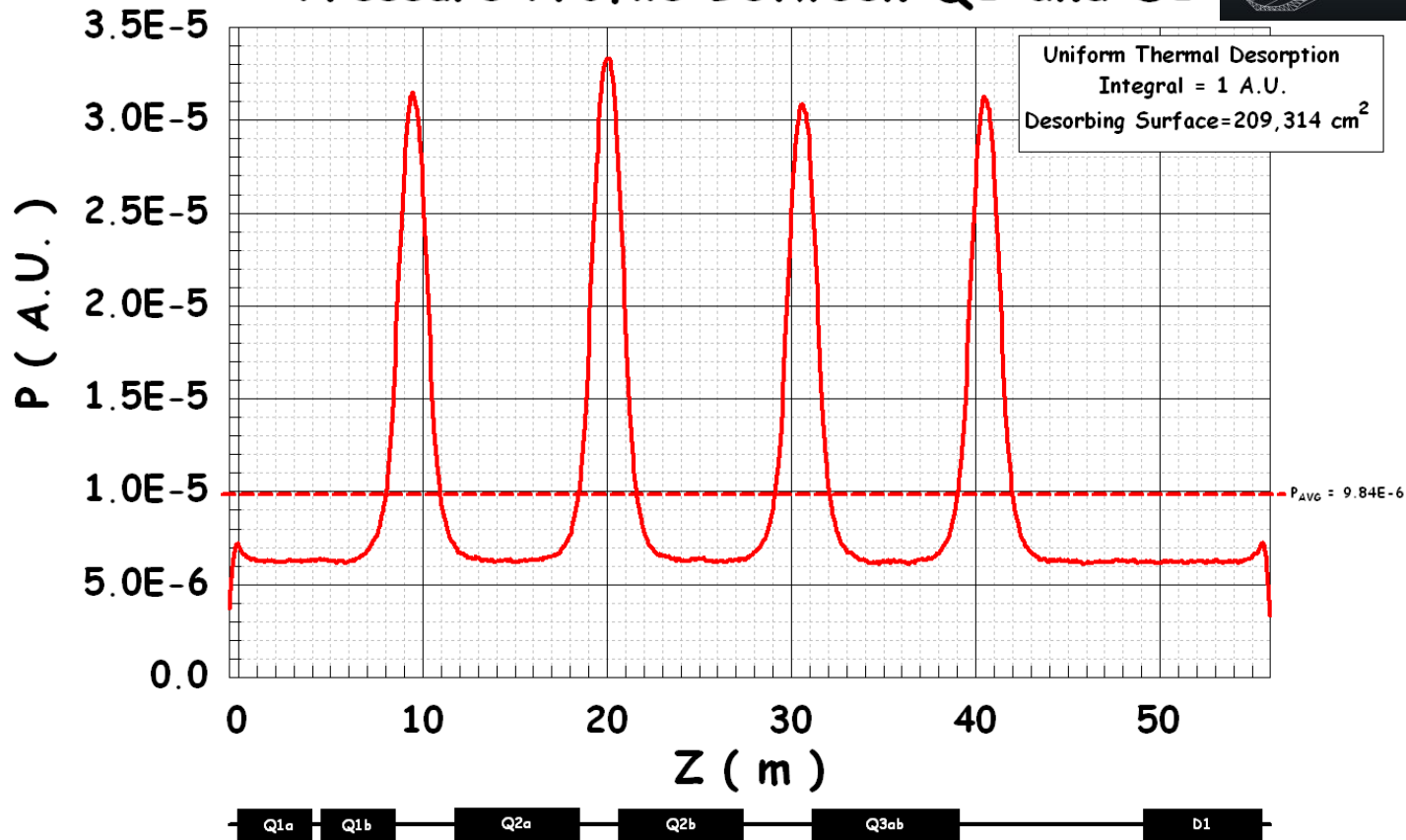


4. Static Pressure

The longitudinal pressure profile, averaged across the 5 cm width, is the following

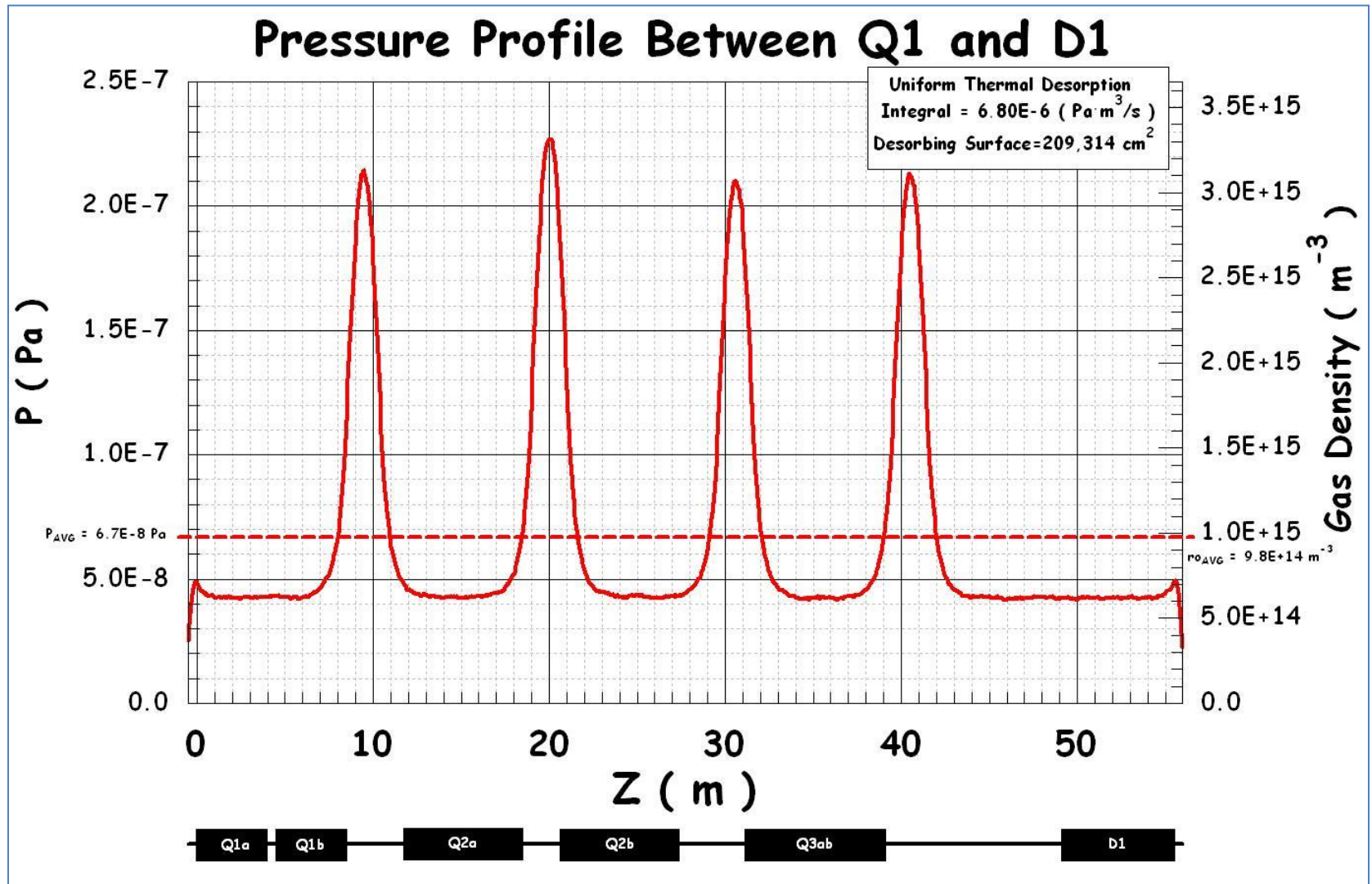


Pressure Profile Between Q1 and D1



4. Static Pressure

Normalizing the average pressure, and gas density, to the H₂ 100 hrs lifetime (6.71E-8 Pa and 9.81E+14/m³), we obtain the equivalent thermal outgassing load desorption rate: 3.25E-10 mbar·l/s/cm², easily obtainable.



5. SR Fans

- The ray-tracing MC code SYNRAD+ has been used. It calculates the orbit of the reference lattice (7 TeV, incoming beam) and traces the SR rays
- Two cases, with an average reflectivity of 0 and 50% have been computed
- The 5.2 T, 40 T·m D1 magnet has been assumed as the source of SR
- The critical energy of D1 SR is $E_{\text{crit}} = 27.4 \text{ eV}$
- Only photons in the (4-400) eV interval are generated. According to well known formulae, only 38% of the D1 photon flux and 93% of the photon power fall within this range
- The integrated D1 flux along the $\sim 7692 \text{ mm}$ -long orbit is $F=2.84\text{E}+17 \text{ ph/s}$, and the integrated power is $P=0.88 \text{ W}$ (for the nominal HiLumi current of 860 mA). Critical energy is 27.4 eV, and the fraction of photons above 4 eV cut-off for gas desorption is 0.393.
- The flux F can be converted into a SR-induced outgassing load Q_{SR} by means of the formula

$$Q_{\text{SR}} = F \cdot \eta \cdot k$$

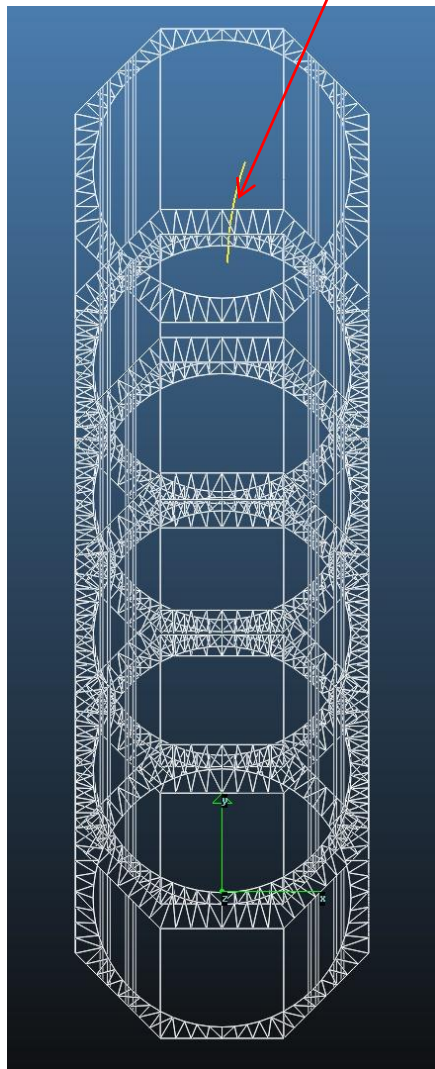
where η is the SR-induced outgassing coefficient (molecules/ph), subject to beam conditioning effects, and k is a conversion factor $k=4.047\text{E}-20 \text{ (mbar}\cdot\text{l/molec.)}$

- Assuming a rather high final value of $\eta=1.0\text{E}-4 \text{ (molec./ph)}$, we get $Q_{\text{SR}} = 1.15\text{E}-6 \text{ (mbar}\cdot\text{l/s)}$... a rather small lumped gas load. Smaller additional gas loads can be assumed as the result of SR coming from the triplet magnets (lower E_{crit}), and are therefore neglected here.

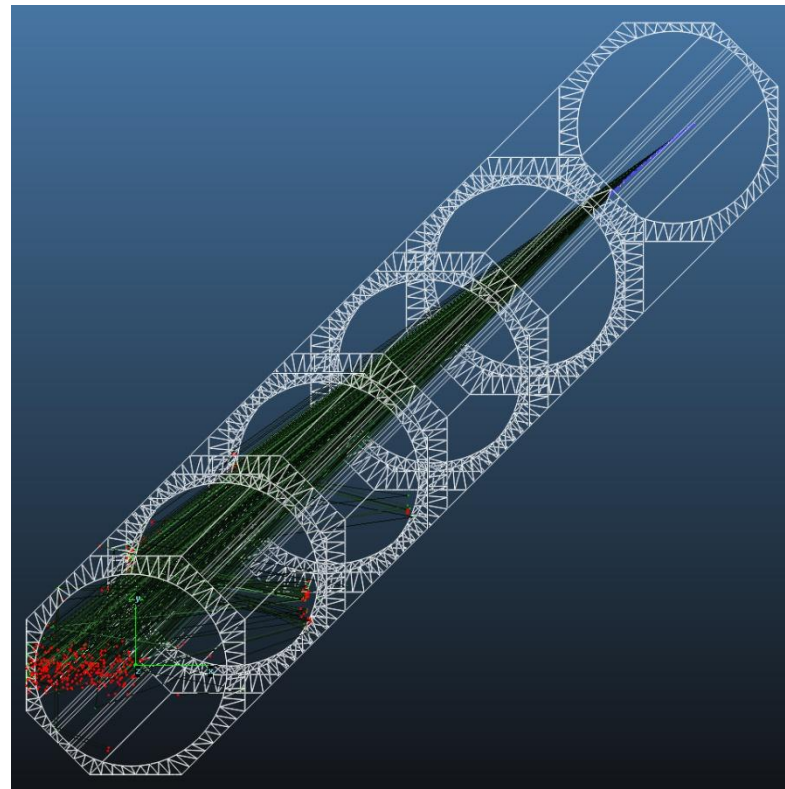
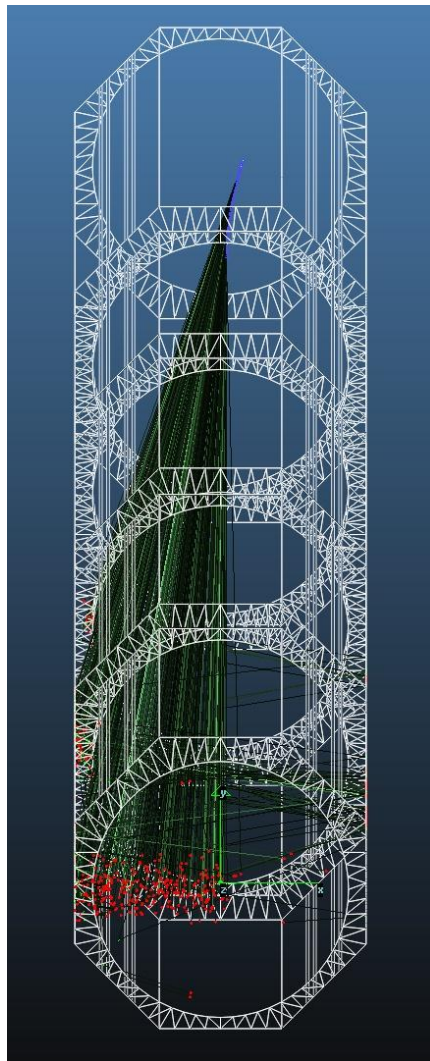
5. SR Fans

SYNRAD+ uses the same 3D geometrical model of Molflow+ (planar facets)

Orbit: photons are generated every 0.01 mm



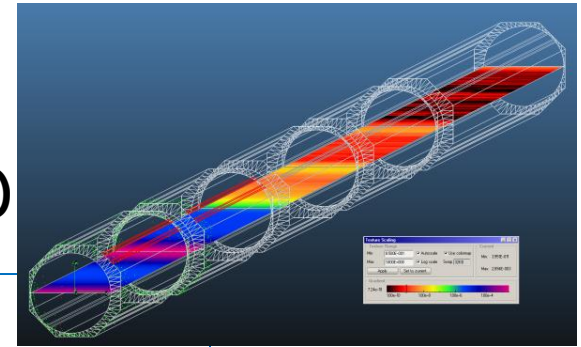
Ray-tracing with scattered photon (50% reflectivity)



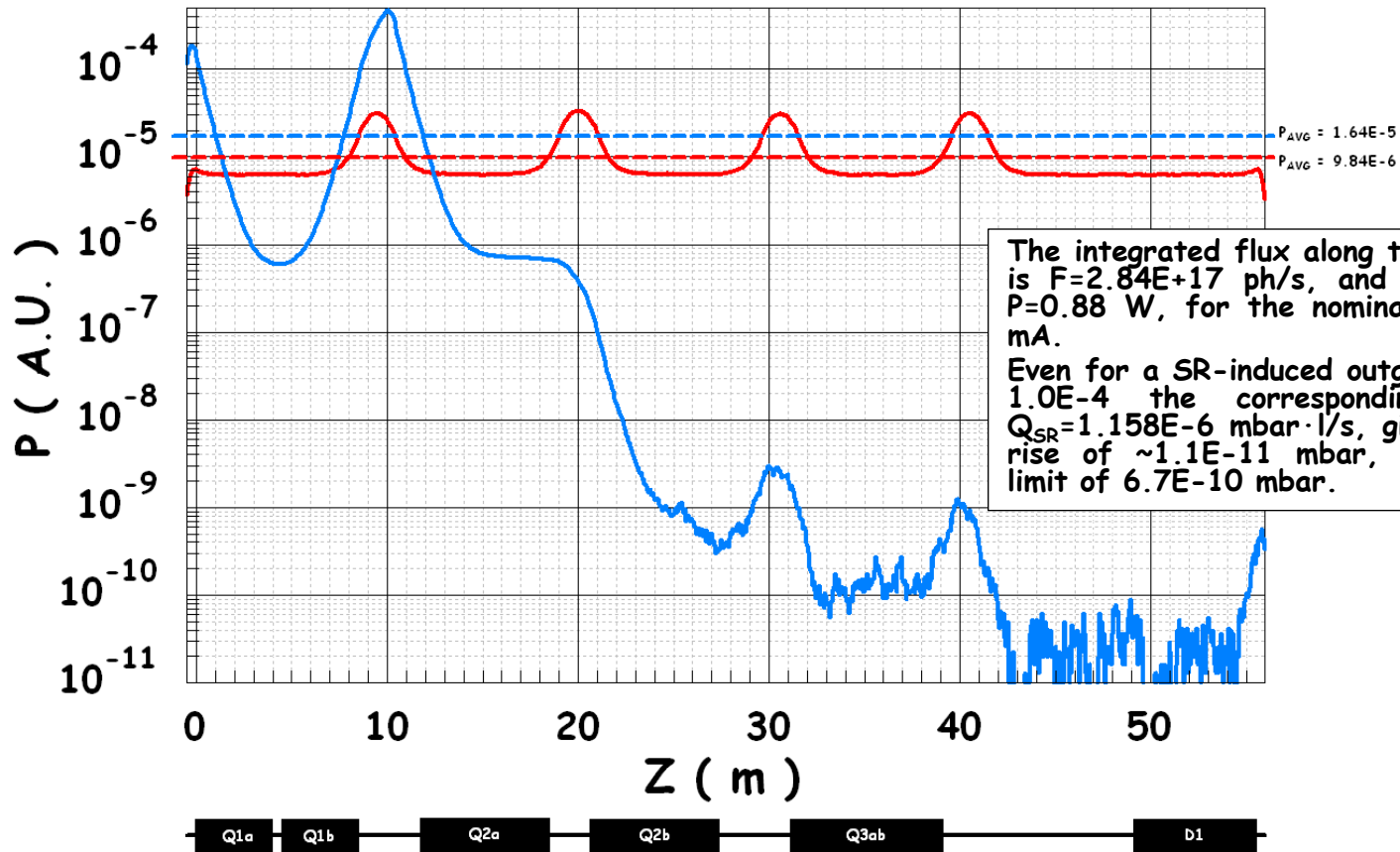
The SR-induced gas load is proportional to the photon flux absorbed on the facets

6. SR-Induced Pressure Rise

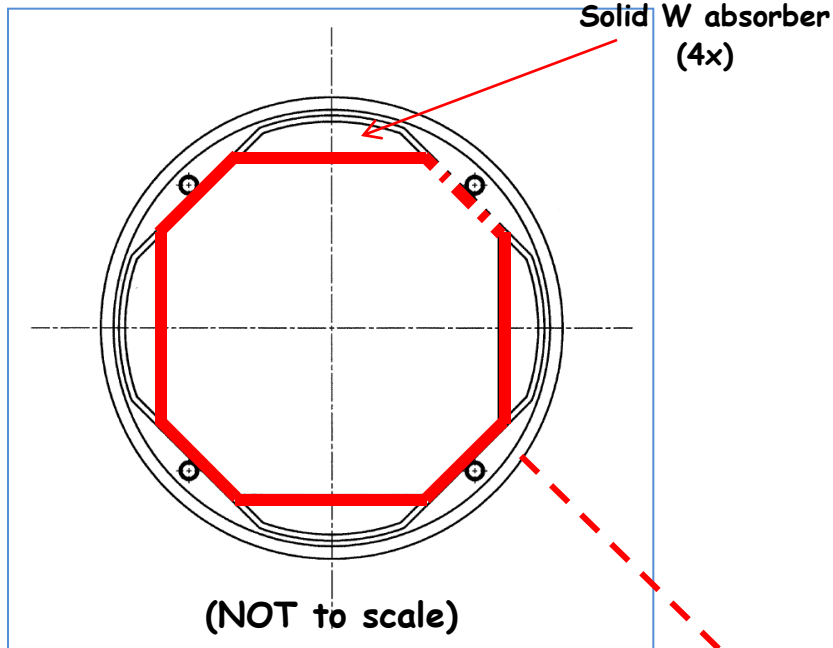
The longitudinal pressure profile is shown in blue after having been normalized to the same $Q=1$ (A.U.)



Pressure Profile Between Q1 and D1

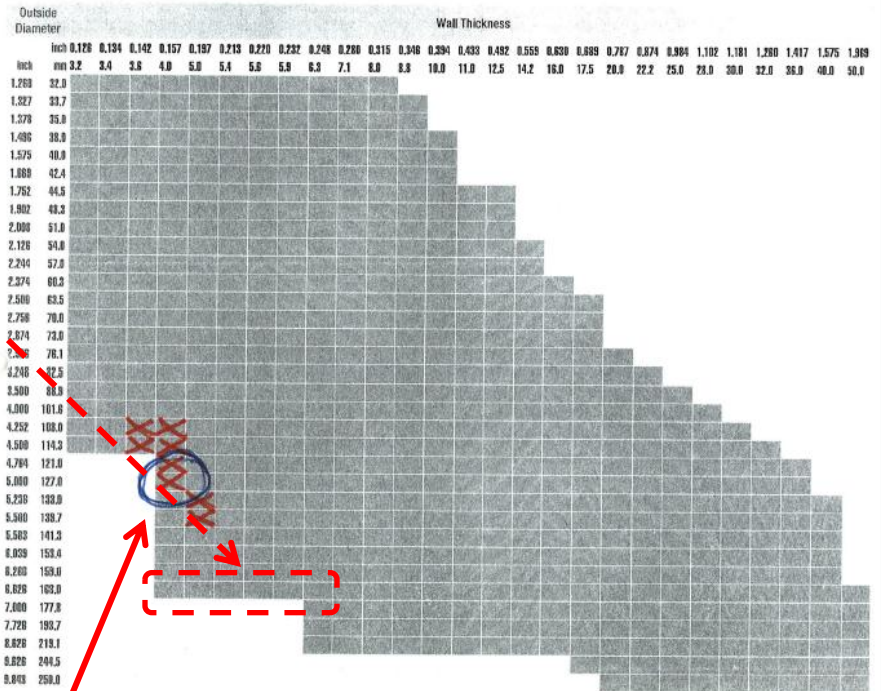


7. Engineering/Integration Issues



ISO-Dimensions and Tolerances for seamless Tubes and Pipes

Outside Diameter	Hot Extruded		Cold Finished	
	D2	D3	D3	D4
EN ISO tolerance class	± 1.0%	± 0.75%	± 0.75%	± 0.5%
Permissible deviation	(min. ± 0.5 mm (± 0.0197"))	(min. ± 0.5 mm (± 0.0197"))	(min. ± 0.3 mm (± 0.0012"))	(min. ± 0.1 mm (± 0.0039"))
Wall thickness	Hot Extruded		Cold Finished	
	T1	T2	T3	T3
EN ISO tolerance class	± 15.0%	± 12.5%	± 10%	± 10%
Permissible deviation	(min. ± 0.6 mm (± 0.0236"))	(min. ± 0.4 mm (± 0.0157"))	(min. ± 0.2 mm (± 0.0074"))	(min. ± 0.2 mm (± 0.0074"))



ISO standard for seamless tubing for the CB dictates fabrication tolerances:

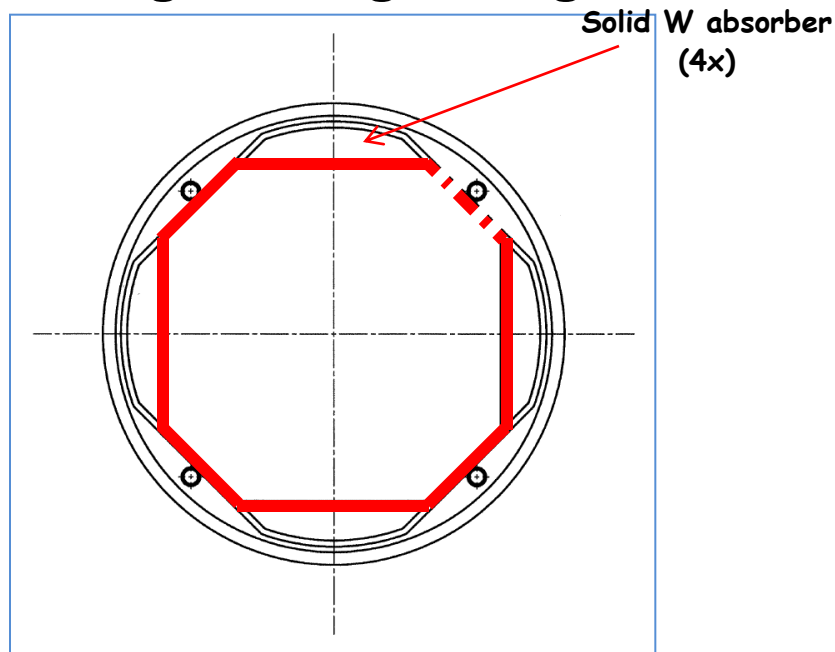
- +/- 0.5% on OD
- +/-10% on thickness

For the case of an 8.8 mm-thick 160 mm OD tube the combined tolerances on the OD of the cold bore are

$$\pm 0.889 \pm 0.88 \Rightarrow \pm 1.77 \text{ mm}$$

ISSUE #1: Is this compatible with the design of the Q1, Q2, Q3 and D1 cold masses and coils?

7. Engineering/Integration Issues



- The BS of the LHC arc dipoles, 1 mm-thick with no W shielding, is relatively easy to insert, being rather flexible and weighing about ~ 1.2 kg/m (sliding on ~ 50 cm/spaced stainless/bronze rings)

ISSUE #2: since similar tolerances apply also to the INSIDE of the cold bore, are the Horiz and Vert size of the BS big enough to accommodate the two beams and their halos?

ISSUE #3: How is a ~ 16 kg/m and stiff shielded beam-screen going to be inserted along the cold bores, some of them being 8~9 m-long?

8. Conclusions

- A proposal for the beam-screen shape for the Triplet/D1 area of HiLumi LHC has been made
- It is a re-scaled version of the "Phase 1" LHC upgrade proposal
- It has 4x 6mm tungsten shielding fixed on the outside face of an octagonal, 2mm-thick BS, which is either copper coated SS or co-laminated Cu/SS, with 4 GHe cooling tubes and rows of 16 pumping slots, similar to LHC arc dipoles' design
- The pumping speed of the slots has been assessed, and found sufficient
- The SR fans generated by D1 have been calculated, and potential SR-induced gas load estimated
- The longitudinal pressure profile for the two cases of uniform thermal desorption and SR-induced desorption have been calculated. There should be no major problems to obtain an average pressure avoiding any beam-lifetime issues
- Three fabrication/engineering issues have been identified, which could affect not only the design of the BS, but also the design of the lattice, and of the Triplet and D1 magnets coils

9. References & Acknowledgements

- *LHC Design Report*, CERN-2004-003, June 2004
- *Beam Screens for the LHC Long Straight Sections*, LHC-VSS-ES-0002 Rev.1.3
- *Pumping Slot Shields for the LHC Beam Screens*, Vac. Tech. Note 03-12, July 2003
- *Finishing of LSS Beam Screens*, LHC-VSS-ES-0004 Rev.2
- *Technical Description for Co-Lamination of SS Strip for the Manufacture of Beam Screens for LHC Cryo-Magnets*, MS-3700/TE/LHC
- *Analytical and numerical tools for vacuum systems*, CAS Vacuum School, Platja d'Aro, 2006, <http://cdsweb.cern.ch/record/1047071/>
- *Introduction to MOLFLOW+: New graphical processing unit-based Monte Carlo code for simulating molecular flows and for calculating angular coefficients in the compute unified device architecture environment*, J. Vac. Sci. Technol. A **27**, 1017 (2009); (7 pages)
- Molflow+ web site: <http://test-molflow.web.cern.ch/>
- *Monte Carlo Simulation of the Pressure and of the Effective Pumping Speed in the Large Electron Positron Collider (LEP)*, CERN-LEP-VA/86-02
- *SYNRAD, a Montecarlo Synchrotron Radiation Ray-Tracing Program*, proc. PAC-03, Washington D.C.

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