

Optical Transition Radiation @ CTF3 & ATF2

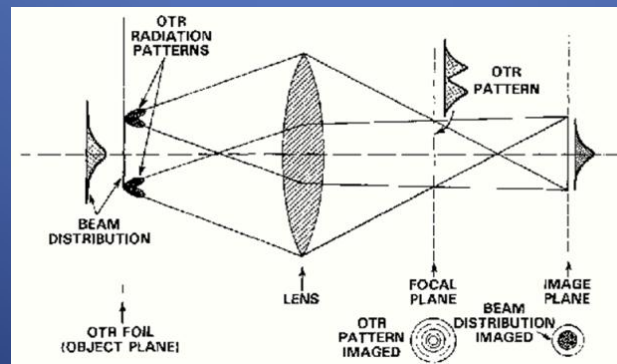
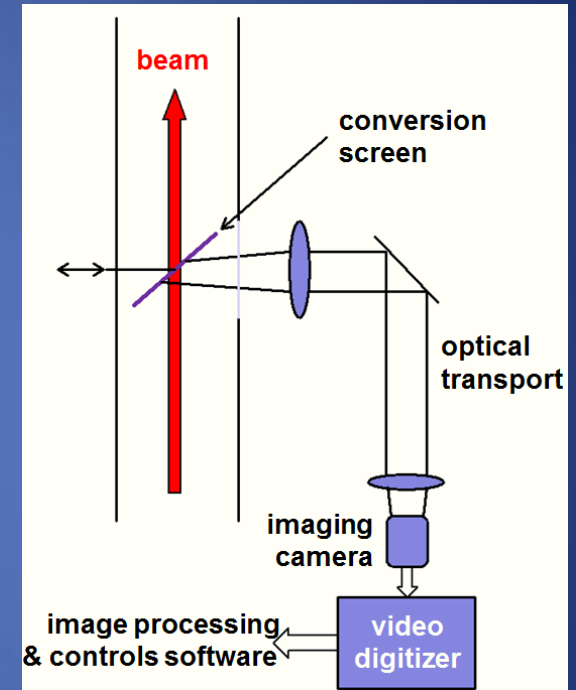
Layout

1. Beam imaging system and choice of Optical Transition Radiation @ CTF3 and ATF2
2. OTR @ CTF3
3. OTR @ ATF2
4. Conclusion

1. Beam imaging system and choice of OTR @ CTF3 and ATF2

Beam imaging systems and OTR

- ✓ The charged-particle beam transverse size and profiles are part of the basic characterizations needed in accelerators to determine beam quality, e.g. transverse emittance
- ✓ A basic imaging system includes:
 - Conversion mechanism (scintillator, optical or x-ray synchrotron radiation (OSR or XSR), Cherenkov radiation (CR), **optical transition radiation (OTR)**, undulator radiation (UR), and optical diffraction radiation (ODR)).
 - Optical transport (lenses, mirrors, filters, polarizers)
 - Imaging sensor such as CCD, CID, CMOS camera, with or without intensifier and/or cooling
 - Video digitizer
 - Image processing software
- ✓ OTR is emitted when a charged particle goes from a medium to another with different dielectric properties.



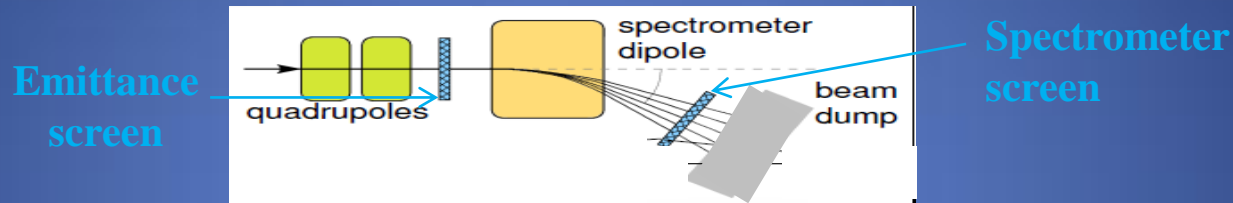
Choice of OTR at CTF3 and ATF2

- ✓ CTF3: Beam intensity from 3.5 A during 1.4 μ s (pulse length), to 28 A during 140 ns
Beam size \sim 1 mm, pulse frequency up to 5 Hz
- ✓ ATF2: Single bunch ($\sim 1 * 10^{10}$ electrons), bunch frequency of 1.56 to 6.24Hz, 30ps bunch length but beam size down to the μ m scale at the location of imaging systems
 - Thermal load too high for scintillating screens
 - High intensity compensates for lower light yield
- ✓ Up to coherence, perfectly linear with beam charge (no saturation)
- ✓ Femto-second time resolution possible
 - *Allows for longitudinal profile imaging (bunch length measurements at CTF3)*
- ✓ Due to properties of the emitted light, it can be used to determine several beam properties (profile/size, position, divergence, energy, relative intensity, bunch length)

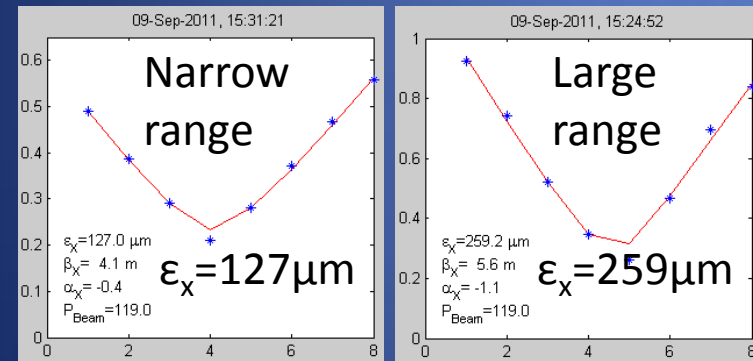
2. OTR @ CTF3

Challenge of OTR at CTF3: vignetting effect

- ✓ 14 TV stations for OTR based emittance measurements (beam size ~few mm)
- ✓ 7 TV stations for OTR based spectrometry (energy): located in spectrometer lines for beam size and energy spread measurements (beam size ~few cm)



- ✓ For emittance measurements (quad scan), beam size can increase consequently

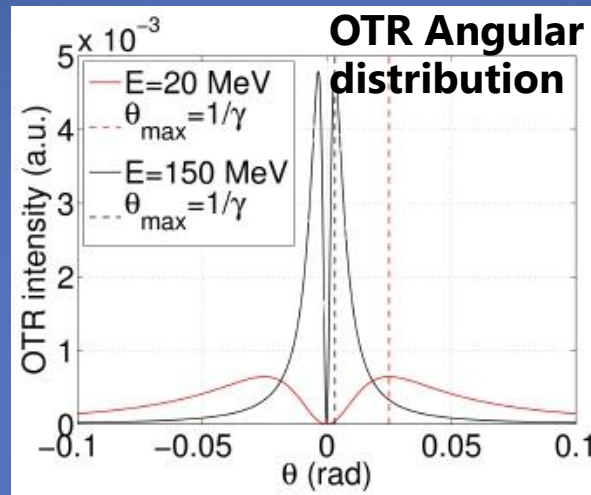
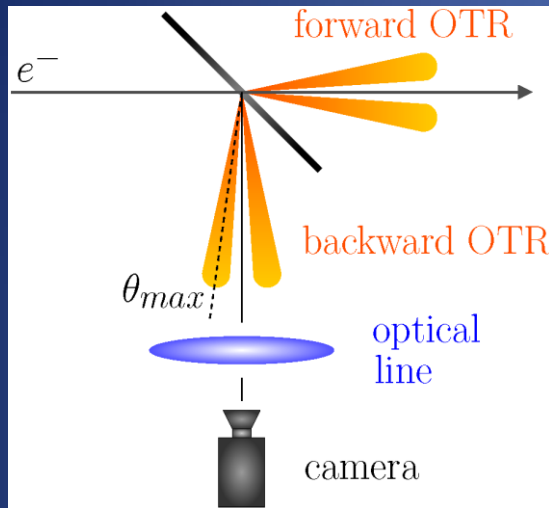


- Large range on quad current: large beam size
- ➔ Vignetting effect underestimating beam size!!
- ➔ Emittance overestimated!!

- ✓ In the spectrometer lines, large beam size of the order of ~ cm due to steering magnet
- Large vignetting factor can decrease the accuracy of measurements

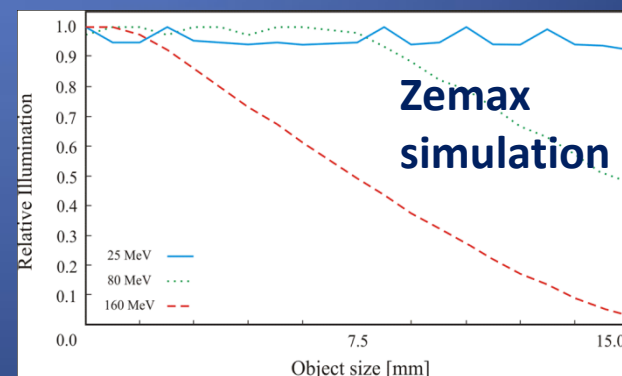
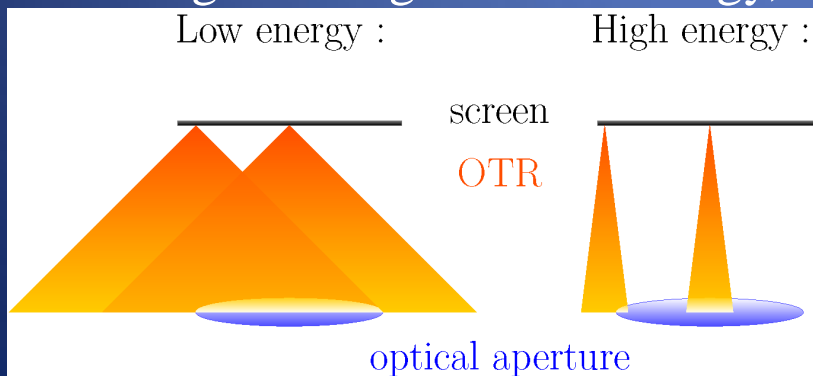
Vignetting effect

- ✓ OTR radiation is emitted in forward and backward direction, of which the latter is generally used due to easier extraction.



→ Emitted light cone gets narrower with increasing beam energy.

- ✓ Vignetting: less light collected from the edges of the screen due to the finite optical aperture of the optical system (first lens: strong limiting factor) and the screen size
- ✓ Effect stronger for higher beam energy, due to the distribution of the OTR emission.



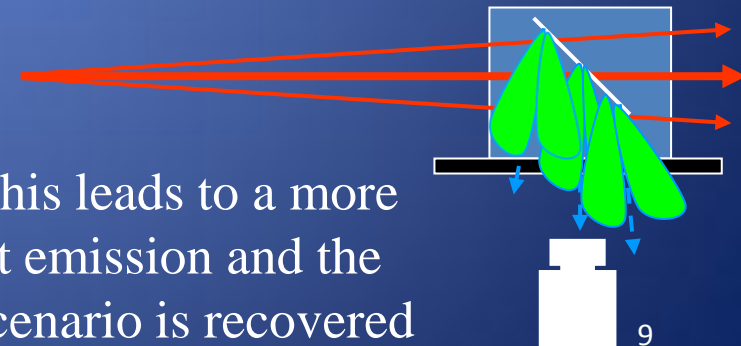
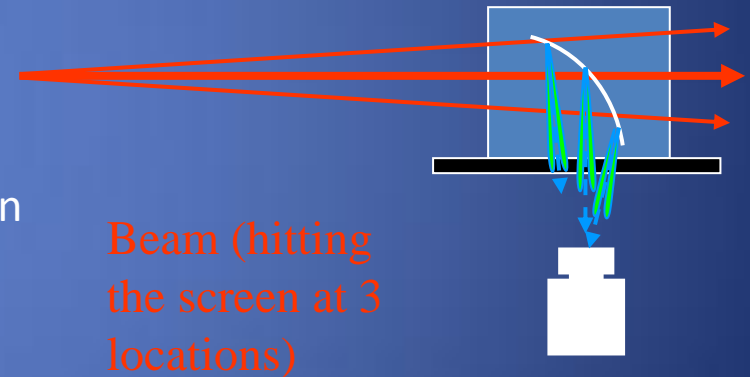
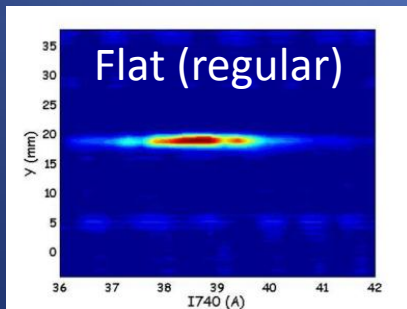
Mitigation of vignetting effect

- ✓ Mitigating the effect means removing the correlation between position on the screen and the amount of light seen by the camera.
- ✓ Two ways: concentrate the light (parabolic screens) or diffuse the light (diffusive screens).

- Parabolic screen: it is possible to – already from the emission point – concentrate the light onto the optical aperture.

Curvature: $z=x^2/f$ (f: distance between the screen and the first lens)

- Diffusive screen: A depolished screen will diffuse the generated light.



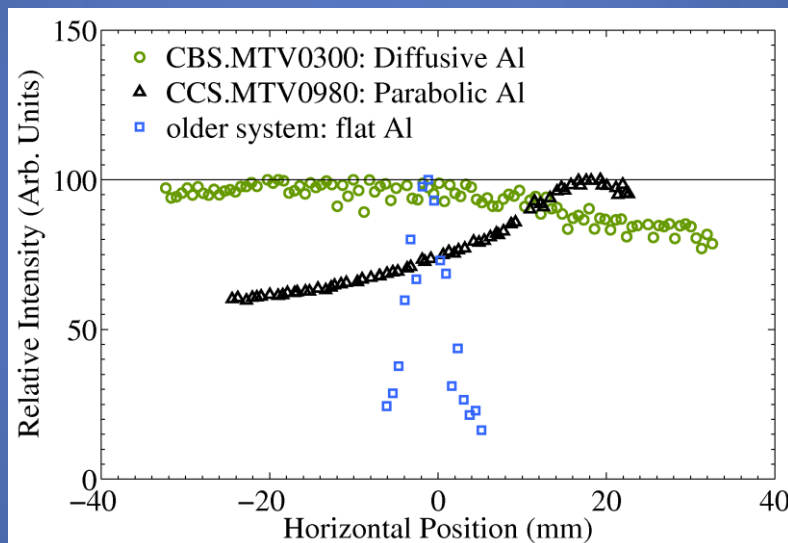
Mitigation results with spectrometer screens

- ✓ Beam size relatively large (order of cm) for spectrometer screens
 - Vignetting effect should be important with standard high reflectivity flat screens
- ➔ Parabolic and diffusive screens have been installed in order to mitigate vignetting

Parabolic

- ✓ The vignetting effect is reduced
- ✓ But maximum of light intensity when the beam is off-centered
 - Misalignment on both screens certainly

Results



Diffusive

- ✓ The vignetting effect is efficiently reduced compared to a standard flat screen

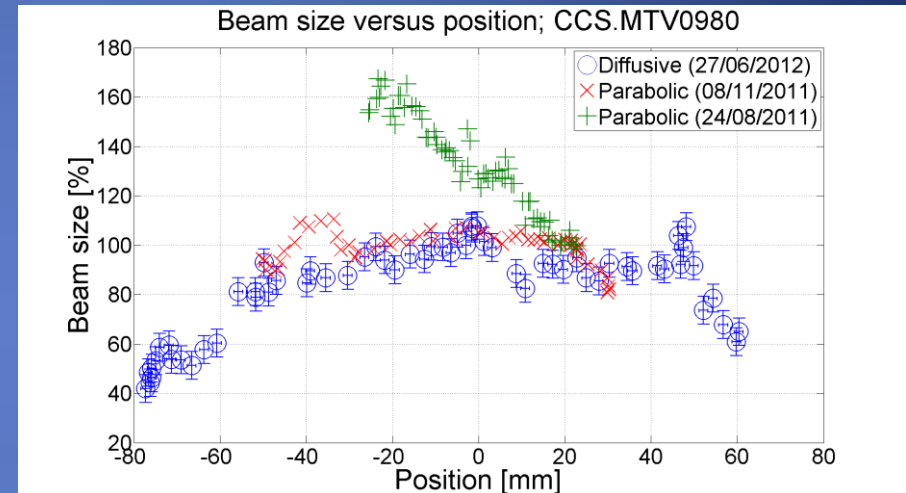
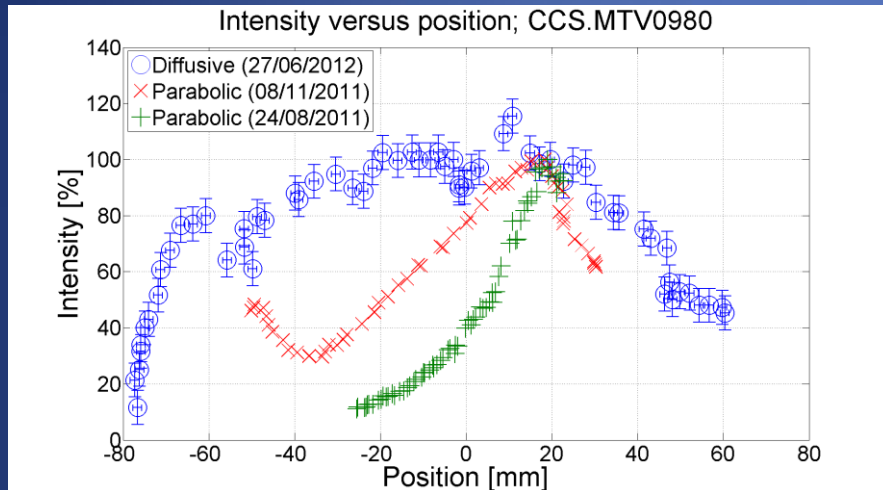
Conclusion

Harder requirements for manufacturing and alignment.
Parabolic screens should only be considered where light intensity is an issue.

In terms of manufacturing and installation, this is a less complicated improvement, compared to parabolic screens. Where the light density allows it, diffusive screens should be the primary choice.

Improvement of the spectrometer screens

- ✓ Change of the four parabolic screens of the CTF3 spectrometer lines by diffusive screens during the last winter shutdown
- ✓ Comparison between diffusive and parabolic screens for the same MTV

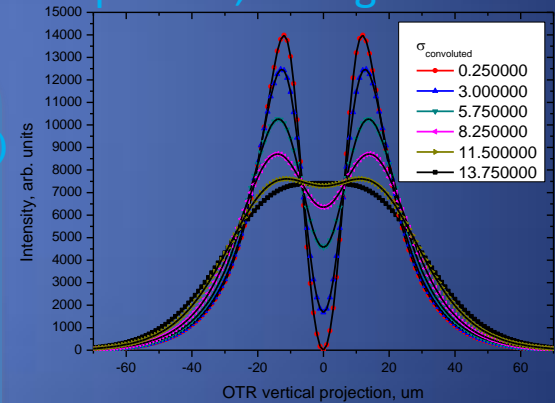
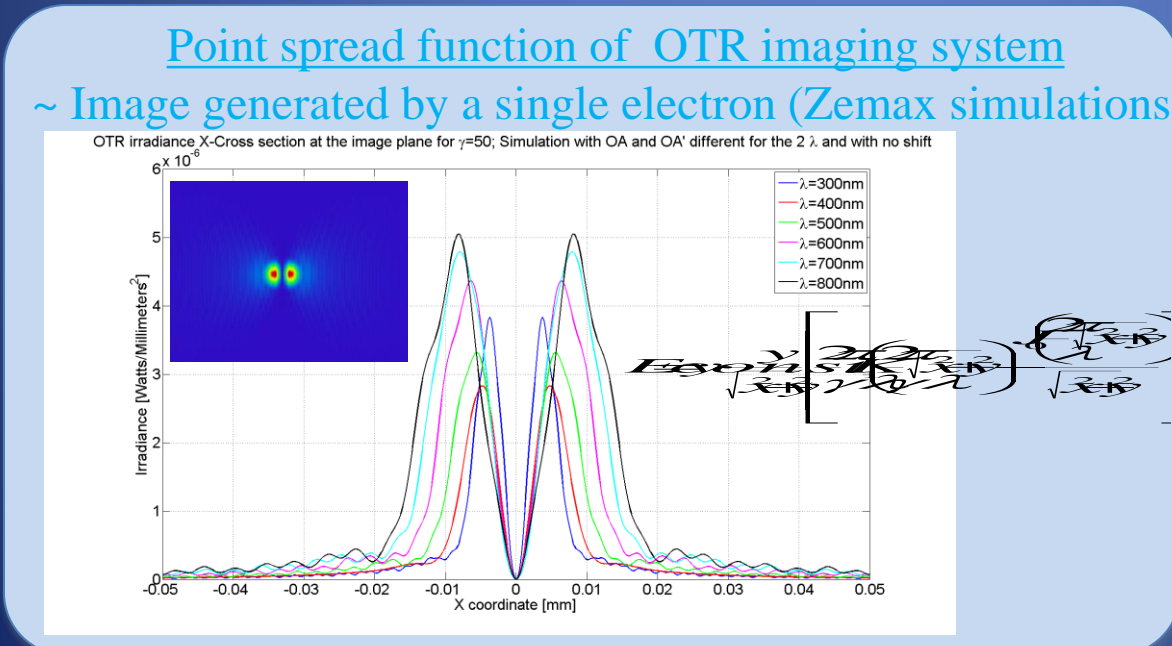


- ✓ With parabolic screens:
 - Different responses versus position for different beam steerings (measurements done on different days) since these screens are much sensitive to misalignments
 - Maximum of intensity off-centered, fast intensity fall, beam sizes can vary much
- ✓ With diffusive screens:
 - Maximum of intensity at the screen center
 - Constant intensity and beam size within $\pm 10\%$ over a large position range₁₁

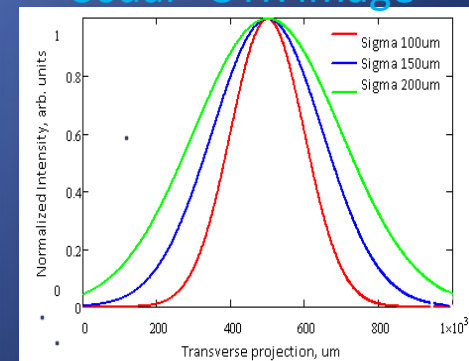
3. OTR @ ATF2

- ✓ Challenge of OTR system at ATF2: measurements of micrometer beam size
- ✓ The resolution (PSF) is determined by the source dimensions induced by a single particle plus distortion caused by the optical system (diffraction of OTR tails)
- ✓ If we consider physical beam size, the resulting image on the camera is the convolution of the beam spatial distribution with the optical system PSF
 - To visualize the beam, PSF has to be smaller than the beam size (➔ aberrations/diffraction reduction)

OTR vertical polarization component, for sigma < ~15 μm

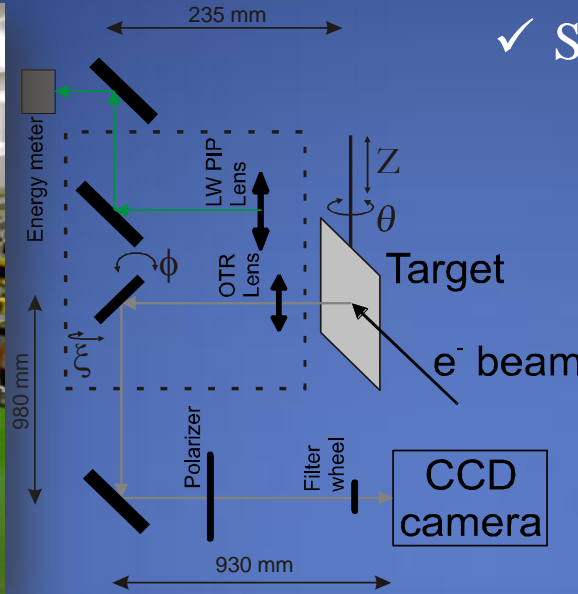
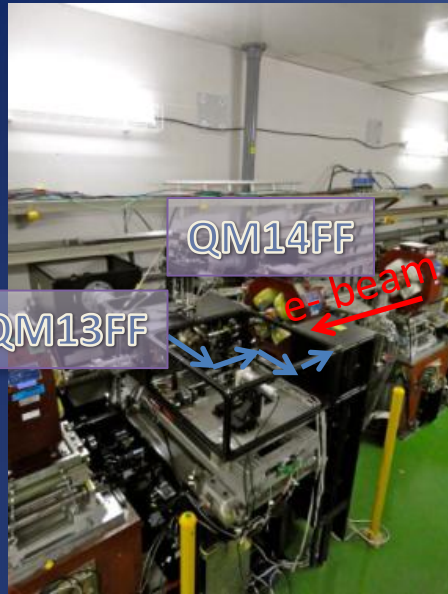


“Usual” OTR image



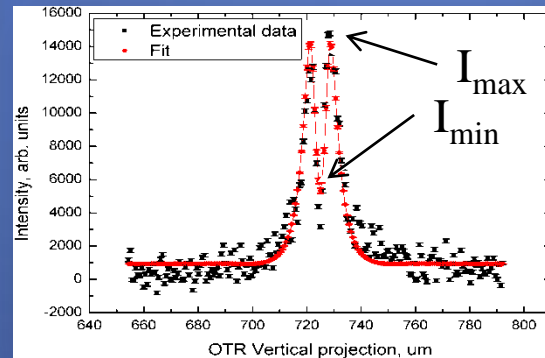
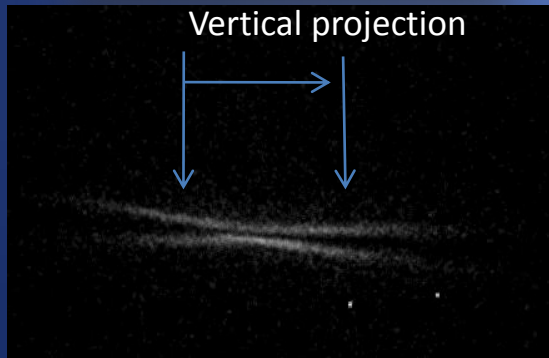
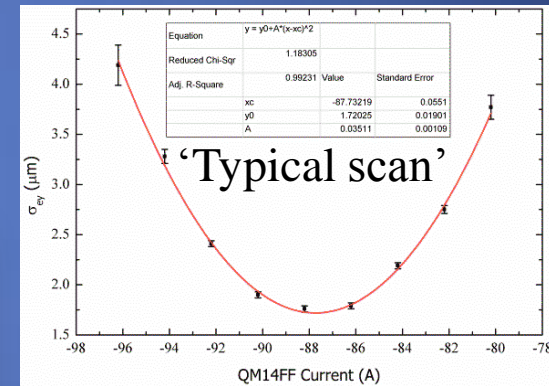
A. Aryshev, N. Terunuma, J. Urakawa, S. Boogert, P. Karataev, L. Nevay, T. Lefevre, B. Bolzon

High resolution OTR measurements at ATF2



✓ Simple system composed of:

- An OTR target (Silicon, coated Al)
- A plano-convex lens and mirrors
- A vertical polarizer ($\sigma_x \gg \sigma_y$)
- A filter wheel (chromatic aberration)
- CCD camera



$$f(x) = a + \frac{b}{1 + [c(x - \Delta x)]^4} \left[1 - e^{-2c^2 \sigma^2} \cos[c(x - \Delta x)] \right]$$

- a** 522.981 +/- 4.43887
- b** 37773.1 +/- 116.182
- c** 0.231221 +/- 0.00049
- Δx** 786.905 +/- 0.00679
- σ calibrated** 1.28202 +/- 0.0479

➤ Need of a vertical polarizer to see the PSF ($\sigma_x \gg \sigma_y$)

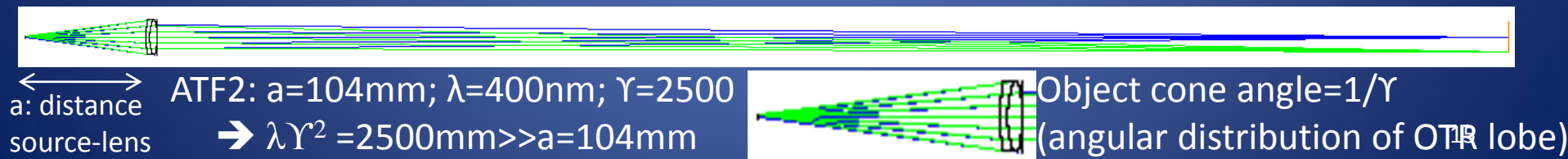
P. Karataev et al, Phys. Rev. Letters 107, 174801 (2011)

A. Aryshev, et al, Journal of Physics: Conference Series 236 (2010) 012008

- Improving image quality (aberration, field of depth,..)
- Propose to test similar system close to final focus (<300nm)

Need of a simulation tool for OTR

- ✓ To improve the current optical line (minimization of aberrations and diffractions to minimize the PSF), need of an optical design tool with the simulation of OTR source
- ✓ For now, analytical calculations enable to simulate very accurately diffractions, but not aberrations (use of thin lens approximation)
- ✓ Zemax commercial optical software can simulate real commercial lenses and take into account both diffractions and aberrations
- ✓ In the BI group, Zemax was used in the ray-tracing mode with an object cone angle as source in order to simulate the angular distribution of OTR, but:
 - ➔ The object cone angle does not include the tails of OTR which have an important impact on the aberrations and diffractions
 - ➔ Ray-tracing mode only takes into account diffractions from the exit pupil of an optical system to the image plane (diffractions through the lens not taken into account)
 - ➔ Ray-tracing mode uses Fraunhofer diffraction algorithm for far field while the OTR system of ATF2 is in near field (near field conditions: $\lambda Y^2 \gg a$)



Physical Optics Propagation mode of Zemax

- ✓ Physical Optics Propagation mode of Zemax: Use of diffraction calculations to propagate a wavefront through an optical system surface by surface
- ✓ As a wavefront travels through free space or optical medium, the wavefront coherently interferes with itself and the coherent nature of light is fully accounted
- ✓ To propagate the beam from one surface to another, either a Fresnel diffraction propagation (beam out of focus) or an angular spectrum propagation is used (in focus)

Fresnel diffraction (near field)

- ✓
$$E(x_2, y_2, z_2) = \left[\frac{e^{ikz}}{i\lambda\Delta z} \right] q(r_2, \Delta z) \iint_{-\infty}^{\infty} E(x_1, y_1, z_1) q(r_1, \Delta z) e^{-\frac{i2\pi}{\lambda\Delta z}(x_1x_2 + y_1y_2)} dx dy, \text{ where}$$
$$q(r, \Delta z) = e^{(i\pi r^2)/(\lambda\Delta z)}$$

- ✓ $E(x_1, y_1, z_1)$: electric field at the source
 - Zemax provides already some DDLs for electric field of Gaussian beams
 - But it is possible to specify our own electric field in a C source file and to compile it in order to be used as a DDL in Zemax

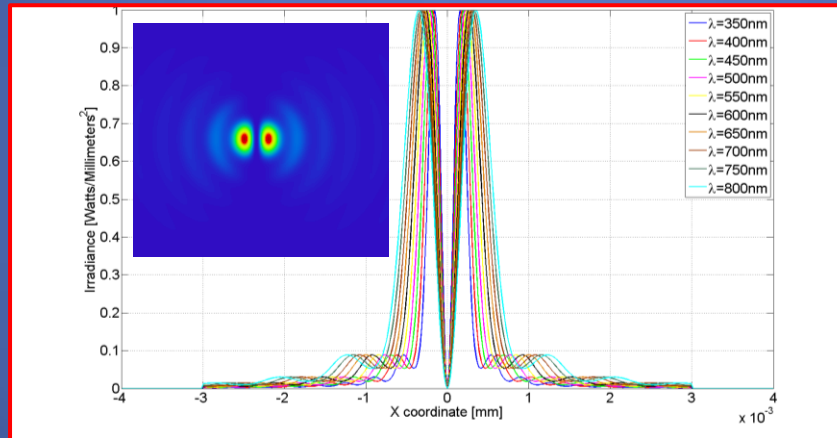
Physical Optics Propagation mode of Zemax

- ✓ Electric field for vertical polarization component induced by a single electron on a target surface can be approximated as:

$$E_{yreal} = const. \frac{y}{\sqrt{x^2+y^2}} \left[\frac{2\pi}{\gamma\lambda} K_1 \left(\frac{2\pi}{\gamma\lambda} \sqrt{x^2 + y^2} \right) - \frac{J_0 \left(\frac{2\pi}{\lambda} \sqrt{x^2+y^2} \right)}{\sqrt{x^2+y^2}} \right] \text{ where:}$$

γ : charged particle Lorentz factor and λ : radiation wavelength

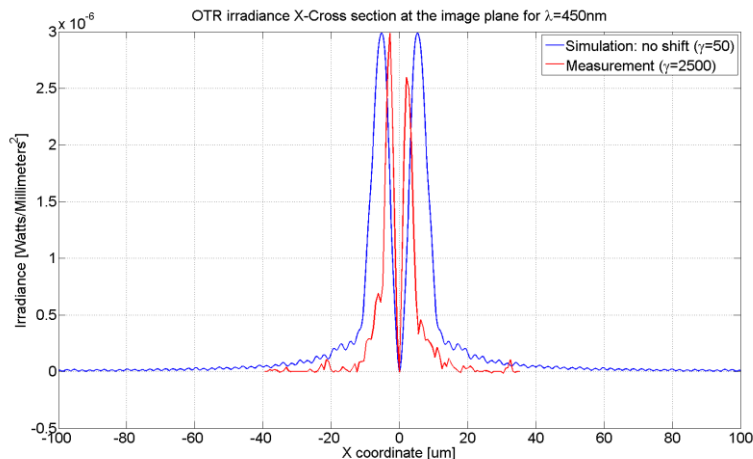
- ✓ In Zemax, simulation of the electric field at the source for different wavelengths:



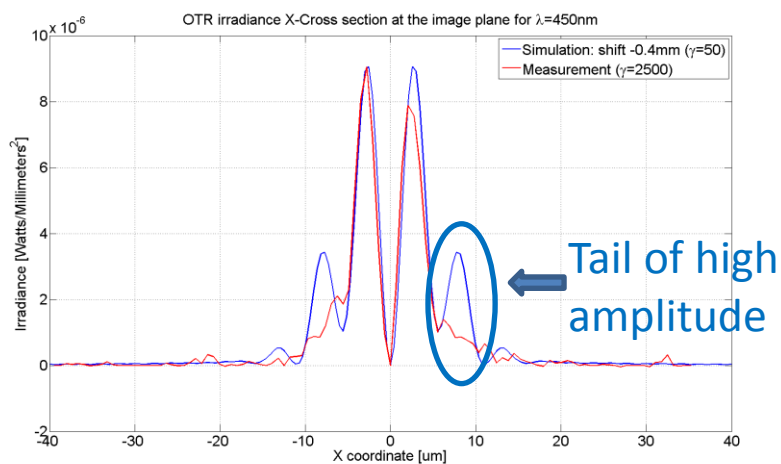
- ✓ Then, Zemax propagates this electric field through the designed optical line up to the image plane by taking into account both diffractions and aberrations
- ✓ At the image plane, we get the Point Spread Function, which represents the resolution of our system since the electric field at the source comes from 1 electron
- ✓ N.B: I have created an option in the DLL which allows to perform the convolution of the OTR electric field (for a single electron) by the electric field of a Gaussian beam

Measurements/simulations for the current set-up

- ✓ Experimentally, the lens is shifted longitudinally by step of $50\mu\text{m}$ to find the real focus (aberrations minimum \rightarrow lobes width and distance between 2 peaks minimum)



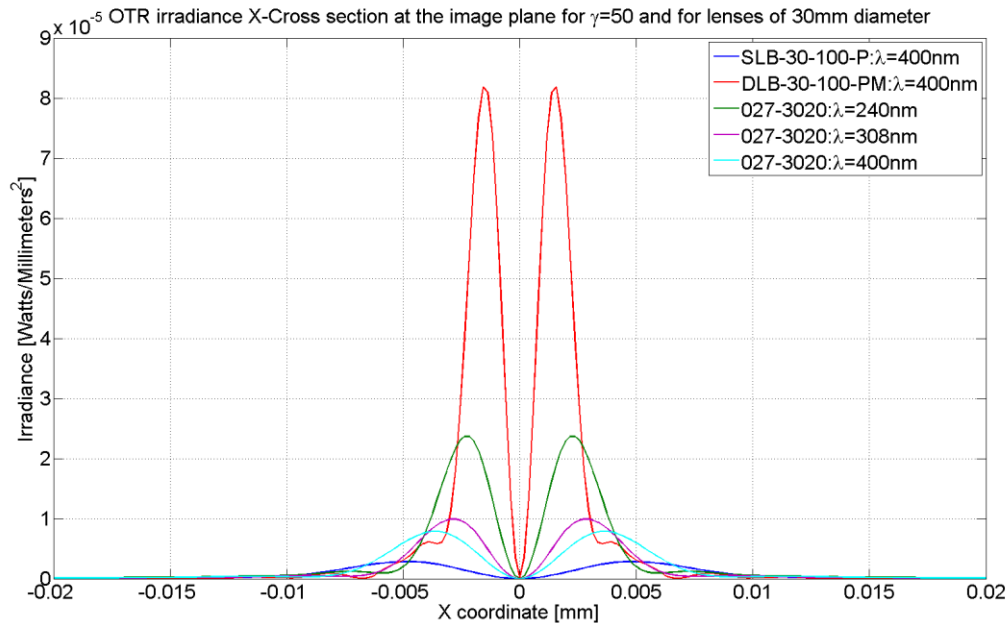
- ✓ Distance between the two peaks:
 - Simulation (paraxial focus): $8\mu\text{m}$
 - Measurement: $4\mu\text{m}$
- ✓ Lobes width:
 - Simulation (paraxial focus): $40\mu\text{m}$
 - Measurement: $20\mu\text{m}$



- ✓ For a longitudinal shift of the lens position of -0.4mm (simulation):
 - Same distance between the 2 peaks ($4\mu\text{m}$)
 - Same width of the main lobes ($\sim 10\mu\text{m}$)
- ✓ N.B: A large tails appears in simulations \rightarrow Probably due to a higher angular divergence in simulations since $\Upsilon=50$ (in the process to order a very powerful computer to go up to $\Upsilon=2500$)

\rightarrow This is very encouraging results in terms of simulations!!

Simulations of the PSF for different kind of lenses



- SLB-30-100-P: plano-convex lens (current lens)
- DLB-30-100-PM: visible classical achromat doublet
- 027-3020: Precise Ultra-Violet achromat doublet

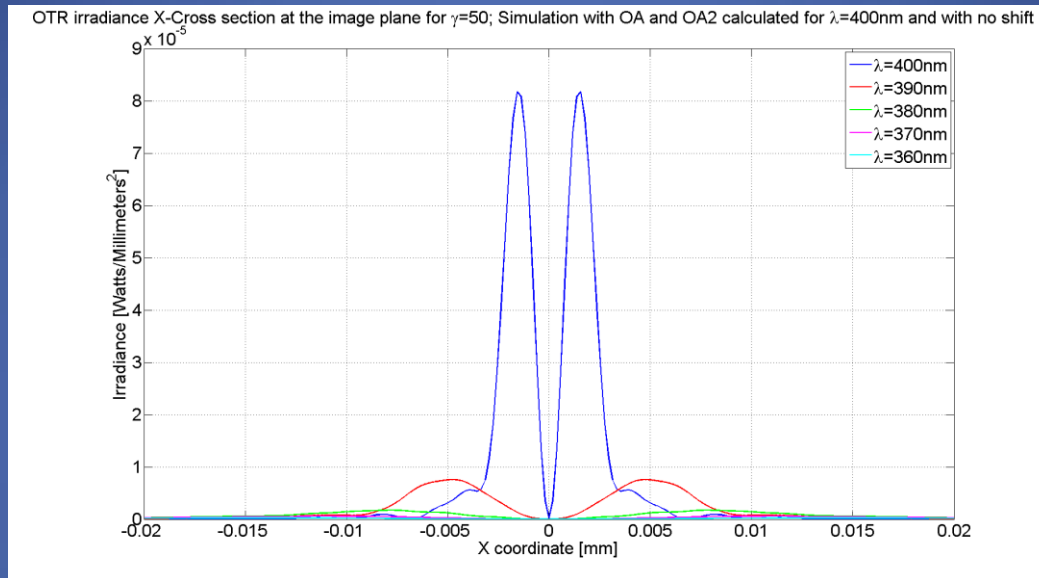
- ✓ In ATF2, the current lens is a plano-convex lens with large aberrations (large PSF)
- ✓ With a visible classical achromat doublet, aberrations are much reduced and we are close to the diffraction limitation for this kind of lens
- ✓ With a precise ultra-violet achromat doublet, PSF is reduced when reducing the wavelength but PSF is still larger than with the visible achromat doublet at 400nm
 - Certainly due to the materials used for ultra-violet lenses

➔ Choice done for beginning of next year: we will stay in the visible light but we will change the current plano-convex lens by the achromat doublet DLB-30-100-PM 19

Study of the filter bandwidth (40nm) on the PSF

Achromat doublet DLB-30-100-PM

Focus for $\lambda=400\text{nm}$ only



λ [nm]	400	390	380	370	360	350
Distance between the 2 peaks [μm]	2.89	10.05	15.61	22.58	28.18	----

- Very important to select a filter wheel with a bandwidth as narrow as possible
- ➔ Compromise between intensity and filter bandwidth (intensity already not that high)
- Since the achromat doublet allows a PSF size twice smaller than with the current plano-convex lens, we should have twice more light per pixel and we will test a filter wheel with a bandwidth twice narrower than the current one (from 40nm to 20nm)

4. Conclusion

OTR @ CTF3

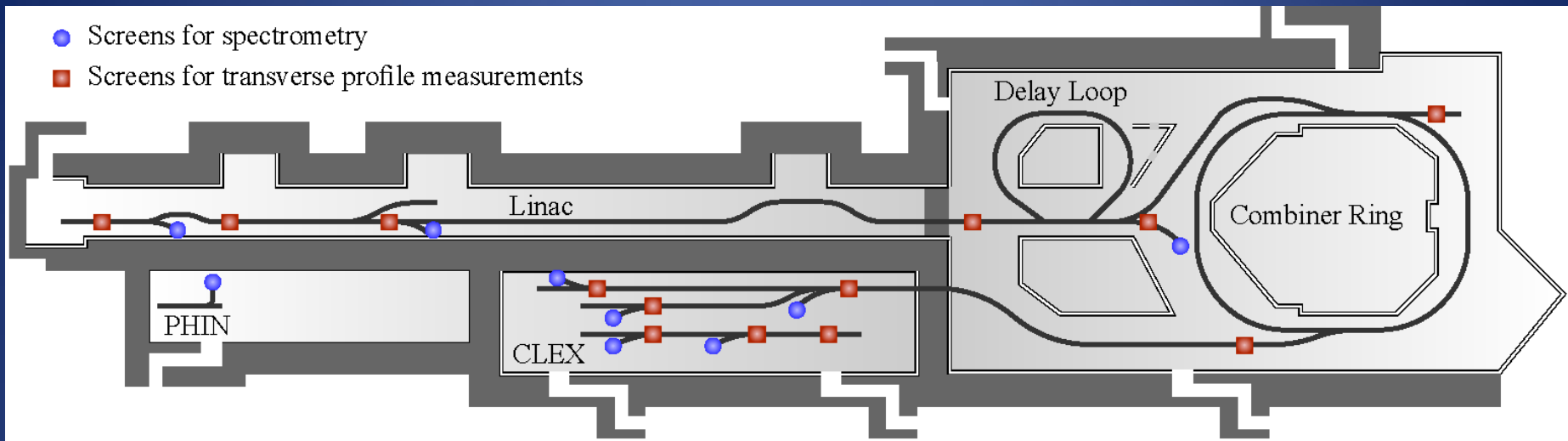
- ✓ Almost all OTR screens have been characterized experimentally (in terms of vignetting, misalignment and damages) using a dipole scan technique
 - Emittance screens: constant beam size within $\pm 10\%$ over a large position range
 - Spectrometer screens: after having changed parabolic screens by diffusive ones during the last winter shutdown, same conclusion than for emittance screens
 - With the development of the OTR simulation tool (see below...), possibility to study very accurately vignetting now (before, object cone angle: $1/\Upsilon$ (ray tracing))

OTR @ ATF2

- ✓ Development of a very accurate simulation tool of the OTR Point Spread Function taking into account all diffractions and aberrations occurring through an optical line
- ✓ This kind of simulations has never been done in the past and can be very useful for the BI group, especially when encountering problems of diffraction (and aberrations)
- ✓ Simulations had reproduced the PSF measurements, which is very encouraging for the validity of the source model and for the accuracy of diffractions/aberrations prediction
- ✓ Next step: Change the plano-convex lens by an achromat doublet and try to reduce the filter bandwidth by two in order to increase the resolution (reduction of PSF size)
 - I should go to ATF2 next February to perform PSF measurements and validate simulations with these new measurements

SPARES

Locations and types of the OTR screens at CTF3



Screens	Screen type	Materials	Energy (MeV)	Current (A)
CT.MTV0435	Flat, reflective	Al, C	118.5	3.5
CL.MTV0500	Flat, reflective	Al, C	18.5	3.5
CL.MTV1026	Flat, reflective	Al, C	65.4	3.5
CC.MTV0253	Flat, reflective	Si, SiC	118.5	28
CC.MTV0970	Flat, reflective	Si, SiC	118.5	28
CTS.MTV0550	Flat, reflective	Si, SiC		7
CLS.MTV0440	Flat, reflective	Al		3.5
CLS.MTV1050	Parabolic	Al	60-75	3.5
CTS.MTV0840	Flat, diffusive	Al	100-150	7
CCS.MTV0980	parabolic	Al	100-150	28
CMS.MTV0630	parabolic	Al	100-150	28
CBS.MTV0300	Flat, diffusive	Al	60-150	28

Emittance screen

Spectrometer screen

➤ Different screen shapes, screen materials, energies, current and optical lines