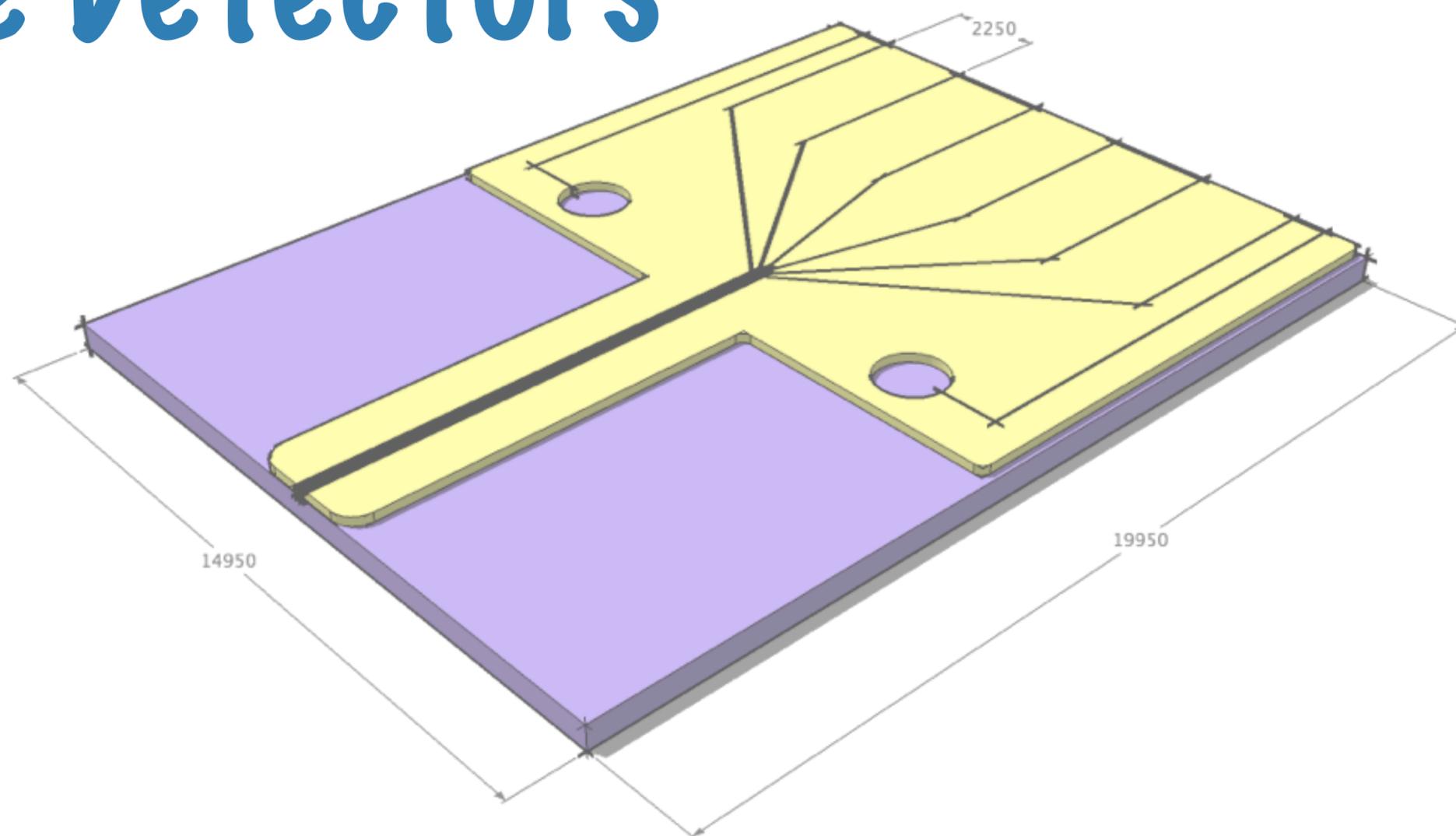




Microfabrication for Particle Detectors



microfabrication projects in PH-DT

- microchannel cooling
- thermo-mechanical mockups
- microfluidic scintillation detectors
- heat transfer of superfluid helium

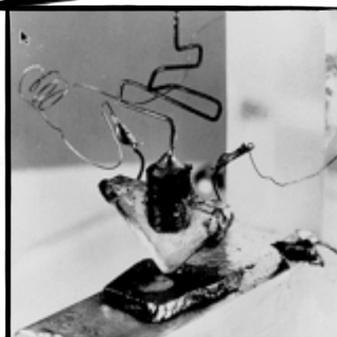
The devices presented hereafter have been fabricated by our CERN PH-DT group members in the university cleanroom of EPFL, Lausanne, Switzerland.

Miniaturization science is the science of making very small things.

It requires a profound understanding of the intended application, different manufacturing options, materials properties, and scaling laws.

Fundamentals of Microfabrication and Nanotechnology, Marc Madou, 2012

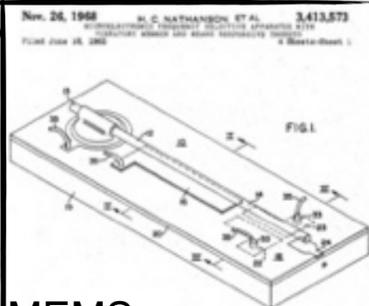
microfabrication milestones



Transistor
 Bell
 1947



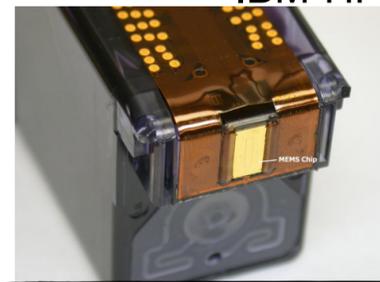
1958
 Integrated Circuit
 Texas Instrument



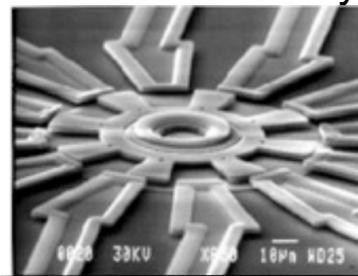
MEMS
 H. Nathanson
 1967



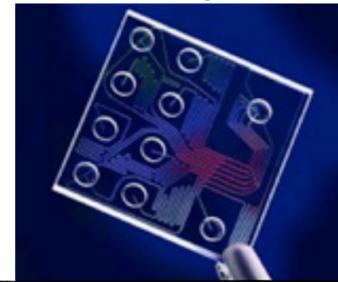
LIGA
 W. Ehrfeld
 1982



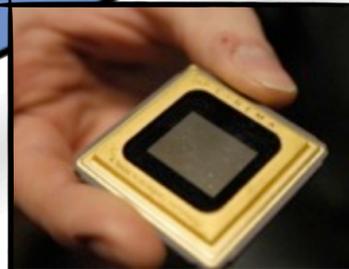
1977
 Inkjet nozzle
 IBM-HP



1988
 Electrostatic Motor
 UC-Berkeley



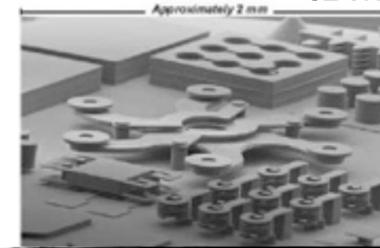
1999
 DNA microarray
 ex. Affymetrix



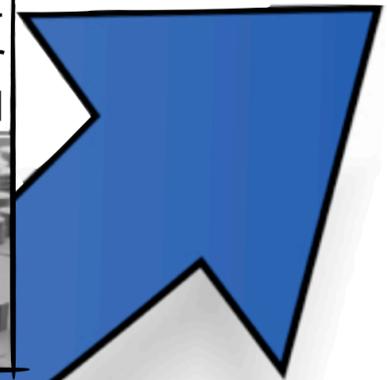
Digital Mirrors Display
 Texas Instruments
 1996



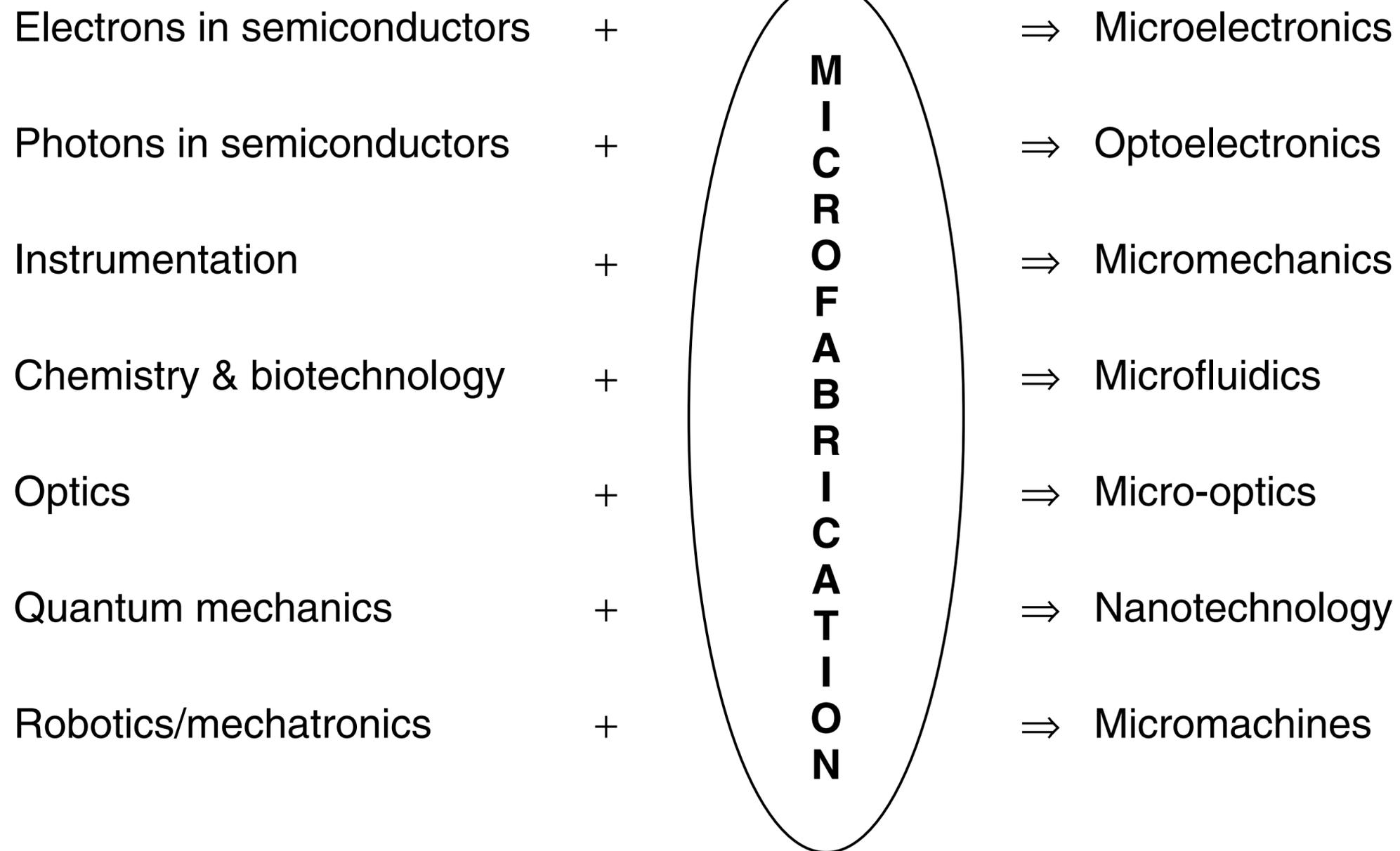
Optical Switch
 Lucent
 2002



2004
 Dual-axis accelerometer
 IBM



microfabrication applications



Introduction to microfabrication, S. Franssila, 2004

microfabrication technologies

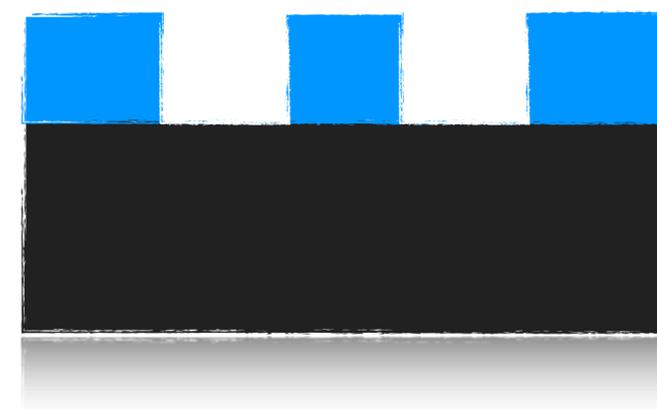
Bulk micromachining

mechanical structures are etched in the substrate



Surface micromachining

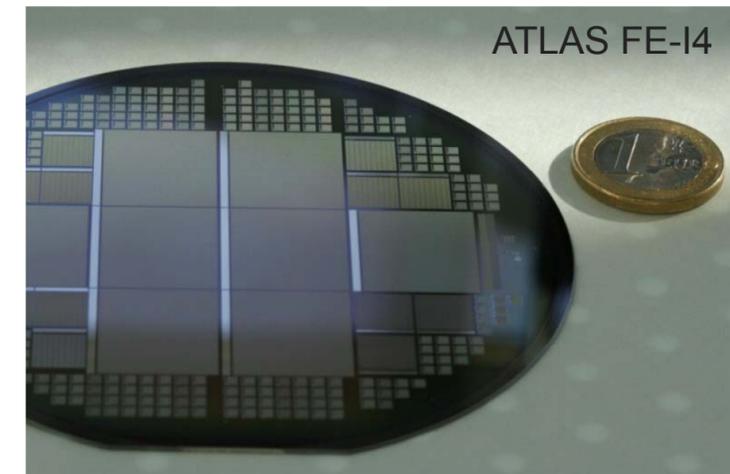
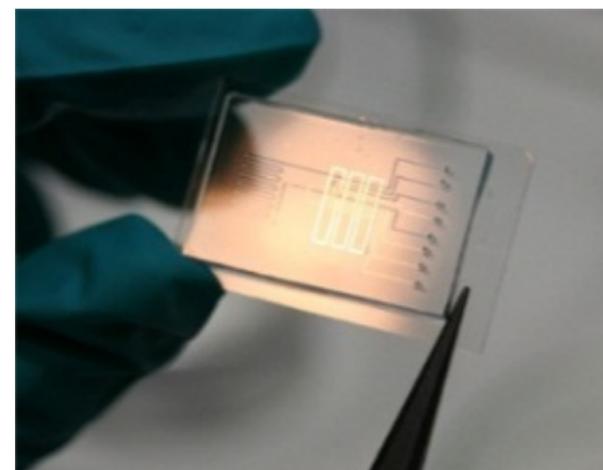
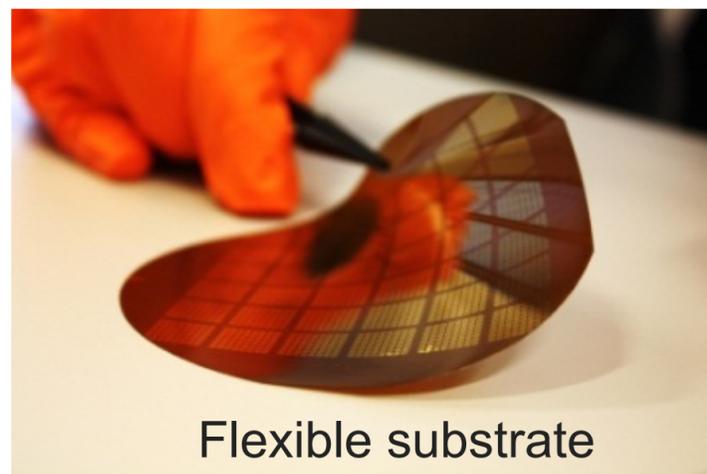
layers of material are deposited on the substrate, patterned and selectively removed



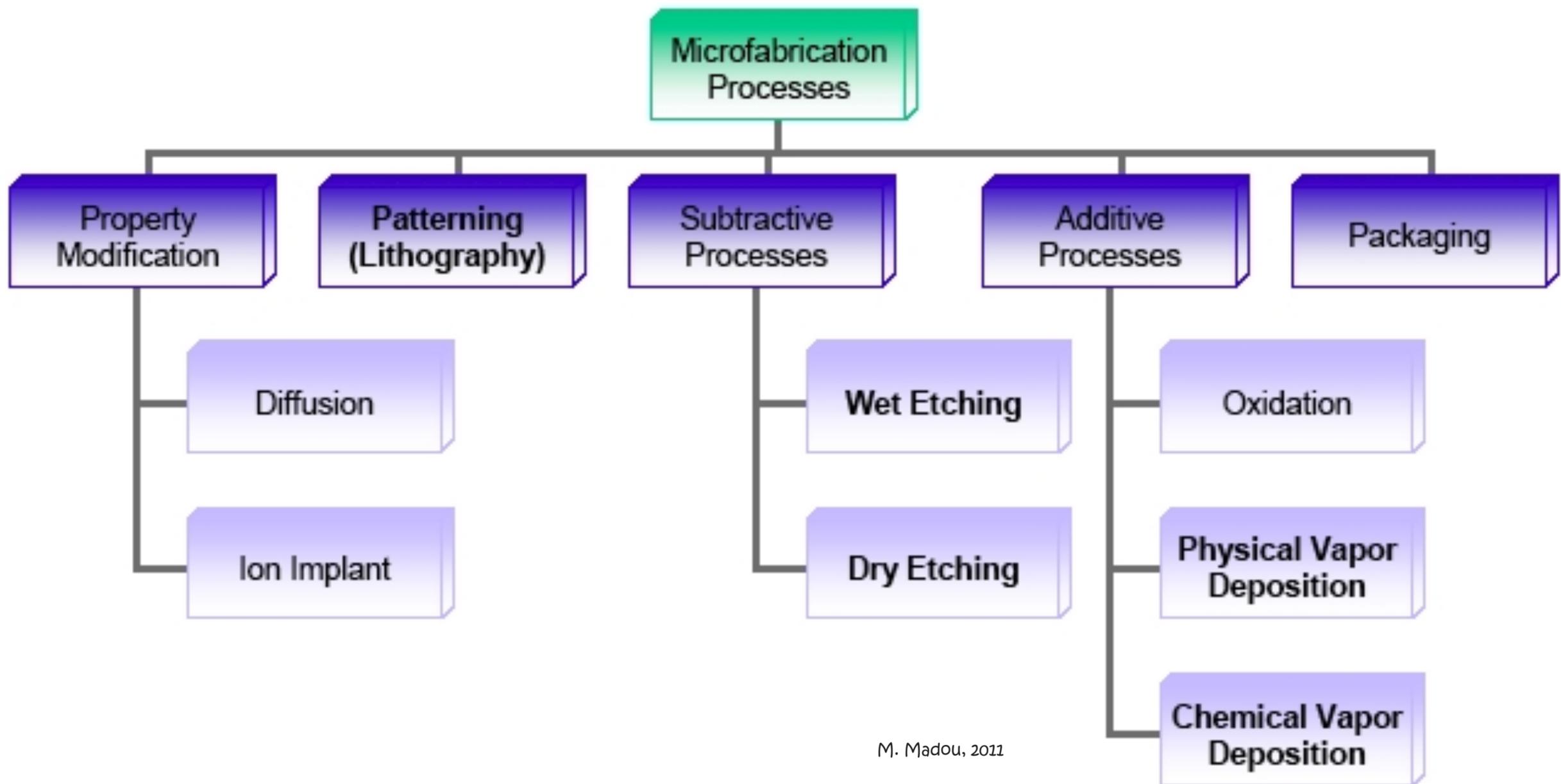
Substrates

round wafers 3", 4", 6", 8", 12"...

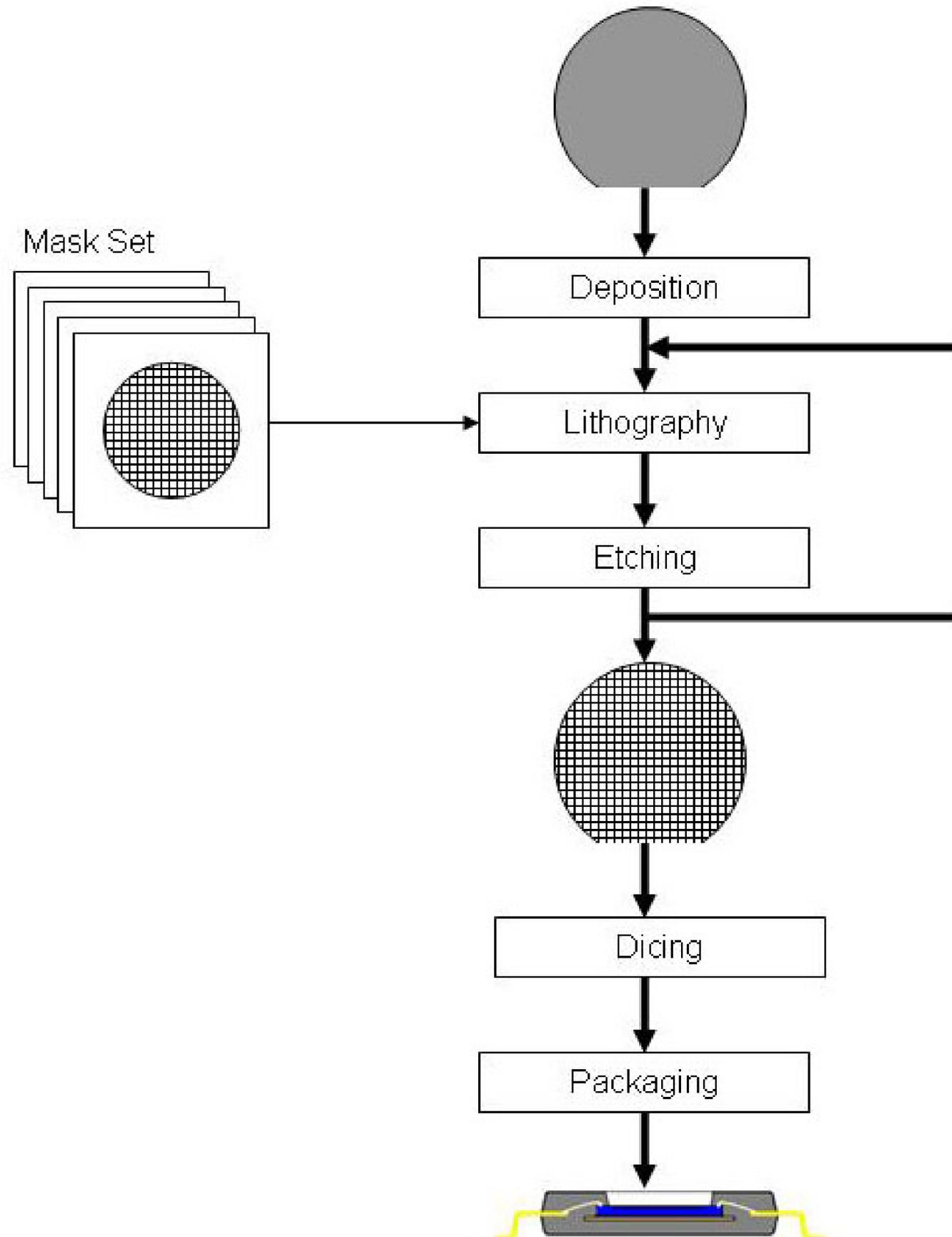
Silicon, SOI, glass, GaAs, SiC, Ge, polymers...



microfabrication processes



microfabrication process-flow



<http://www.electronicproductskth.org.uk>, 2007

microcooling for trackers... long-awaited

Mechanics and cooling of pixel detectors

54

M. Olcese / Nuclear Instruments and Methods in Physics Research A 465 (2001) 51–59

The most advanced raw materials, the same adopted in aerospace industry, are widely used: Ultra High Modulus carbon fibres with low moisture adsorption cyanate ester resin matrix to minimise swelling due to change in moisture content.

A typical weight of a well designed global support structure ranges from 10% to 15% of the total weight of the detector.

6. Thermal management

The problem to be solved, common to all detectors, is shown schematically in Fig. 4.

The heat is produced quasi-uniformly over the relatively wide module area and has to be efficiently transferred to the coolant flowing inside a small cooling pipe, which must minimise the material.

The thermal design of the local support has to achieve:

- a good temperature uniformity over the module
- a good heat transfer efficiency to minimise the module-to-coolant temperature difference.

To accomplish the temperature uniformity goal the local support structure material has to have a good in plane as well as transverse thermal conductivity.

High X_0 metallic materials, typically beryllium or aluminium, are in principle good options for the module thermal management.

However the metallic materials make the thermal stability issue more critical due to their relatively high CTE, limiting the application range to small structural parts.

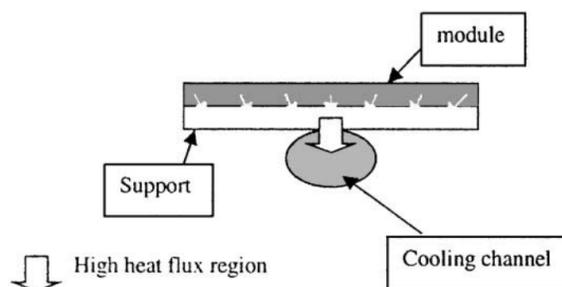


Fig. 4. Module thermal management fundamentals.

Moreover the Al is usually not adopted as stand alone structural material due to its poor mechanical properties.

Attractive alternatives to metals are the carbon-based materials. Standard CFRP are difficult to be adopted in an efficient thermal design due to their poor transverse thermal conductivity.

Carbon–Carbon materials are in principle the best option combining good thermal properties even in transverse direction to fibres (thermal conductivity 1 or 2 order of magnitude better than standard CFRP) with excellent mechanical properties, stability and transparency to particles. The C–C materials have essentially two technological drawbacks limiting the application range: porosity and difficulty to achieve complex and accurate geometry due to the high temperature manufacturing process.

The selection of the material for the cooling channel and of the coupling method to the module support is a critical issue for the local support thermal efficiency and stability.

There are three possible options:

1. pipe material with the same CTE of the support: hard and reliable thermal joint is possible
2. pipe material with different CTE: elastic joint is necessary, but reliability becomes an issue
3. cooling fluid in direct contact with the module support (integrated cooling channel)

Solution 1 is the safest design but possible just in very limited cases.

Solution 2 is the most widely adopted, because it leaves the maximum freedom in the design choices.

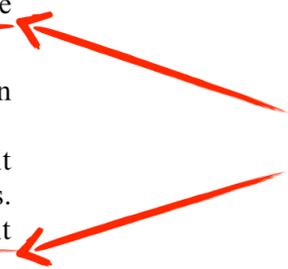
Solution 3 minimises the material, but is difficult to be implemented.

Additional stability constraints as well as specific design solutions will be discussed in the following sections.

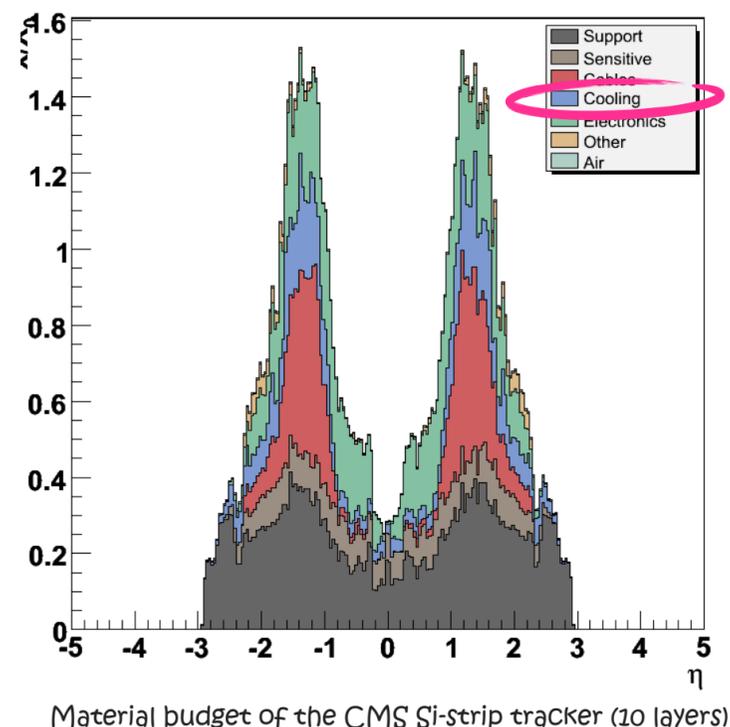
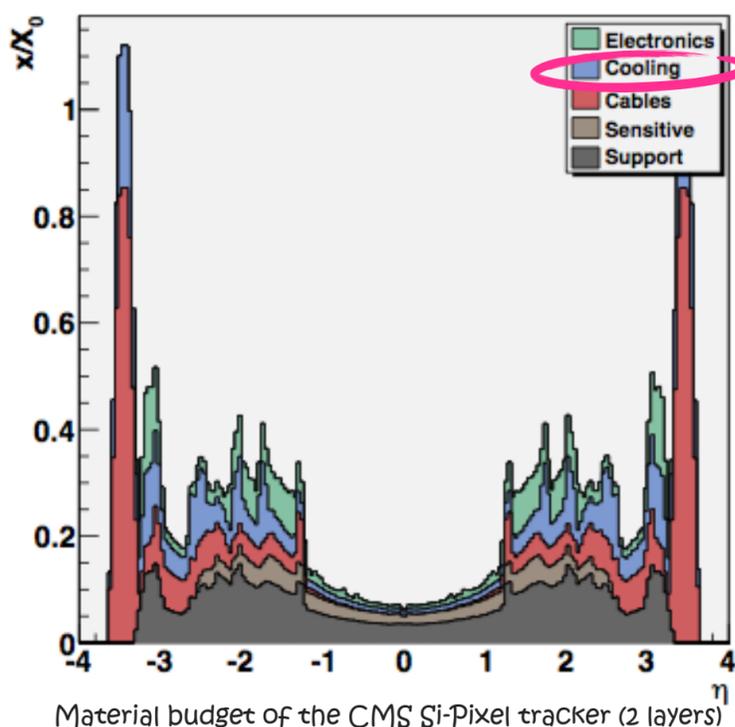
7. Cooling options

The minimisation of the material of the cooling circuit (pipes, connections) and the need of a good heat transfer efficiency to meet the temperature requirements on the module, restricts the choice to

μ-Channel cooling



why silicon microcooling for trackers ?



LHC large Si trackers (ATLAS and CMS)

2% X_0 per layer



SLHC “phase II” upgrade:
“significant” reduction needed



Future trackers at ILC
0.1÷0.2% X_0 per layer

no CTE mismatch

o Minimization of material budget:

- o Micro-channel cooling naturally addresses this issue through the use of thin Si cooling plate

o For a given material budget, increase the cooling power:

- o High heat transfer coefficients in laminar flows (prop. to $1/D_h$ with very small D_h)
- o High heat flux with large exchange surface

o Reduce ΔT between heat source and heat sink:

- o Micro-channels embedded in Si plate -> large exchange surface
- o Thinned Si plates -> ΔT minimized
- o Local cooling only where heat transfer required

$X_0 = X_0/\rho$ [cm]

Cu: 1.4

Steel: 1.7

Ti: 3.6

Al alloy: 8.9

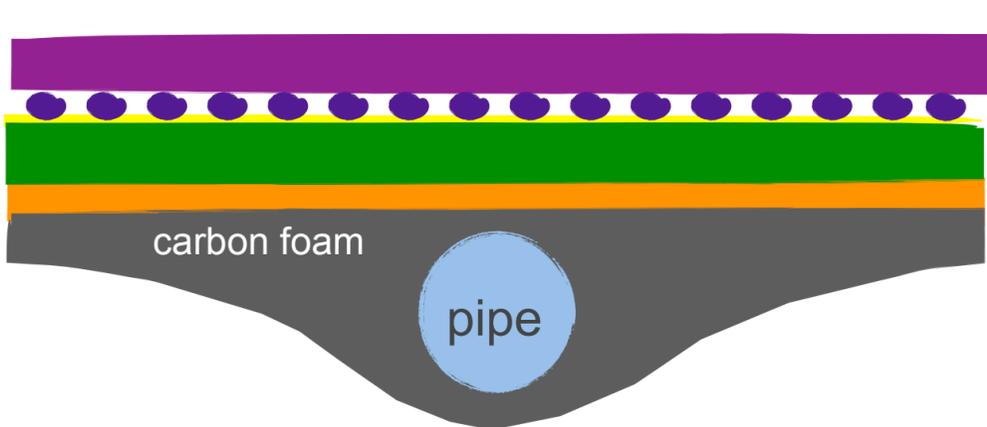
Si: 9.4

C_6F_{14} @ -20 C : 19.3

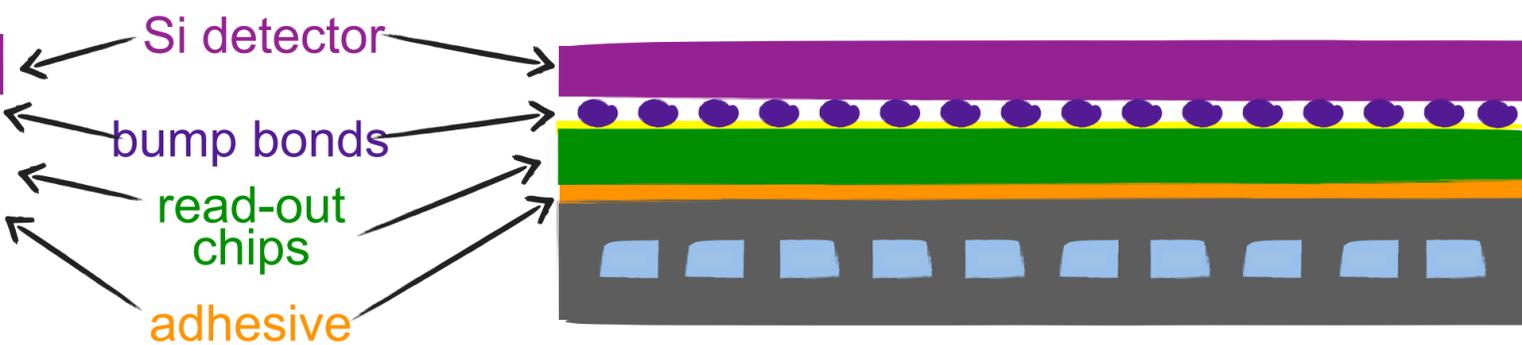
CO_2 (liquid) @ -20 C: 35.8

cooling of future detectors

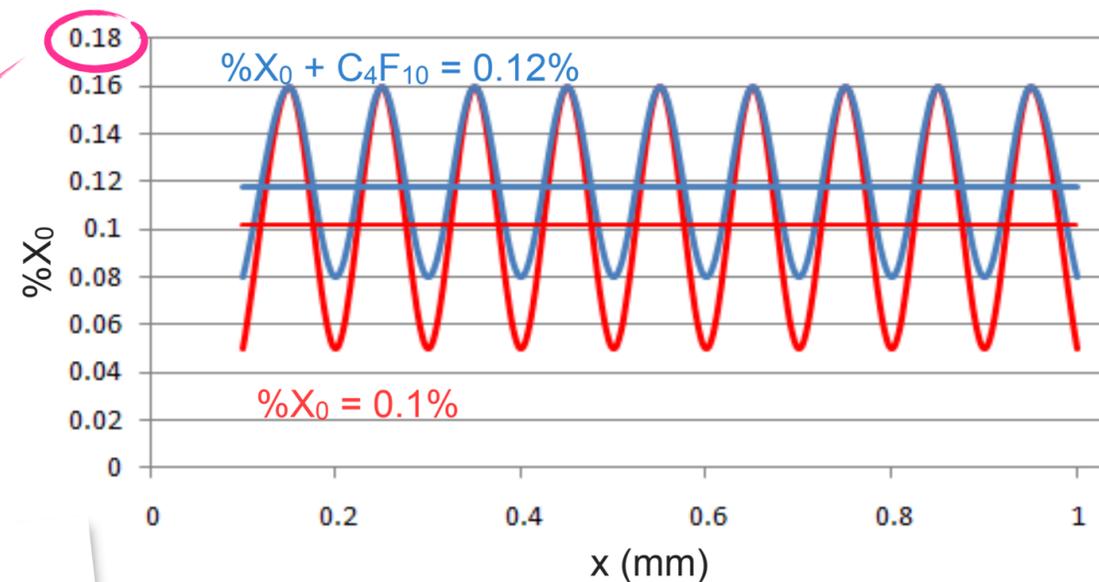
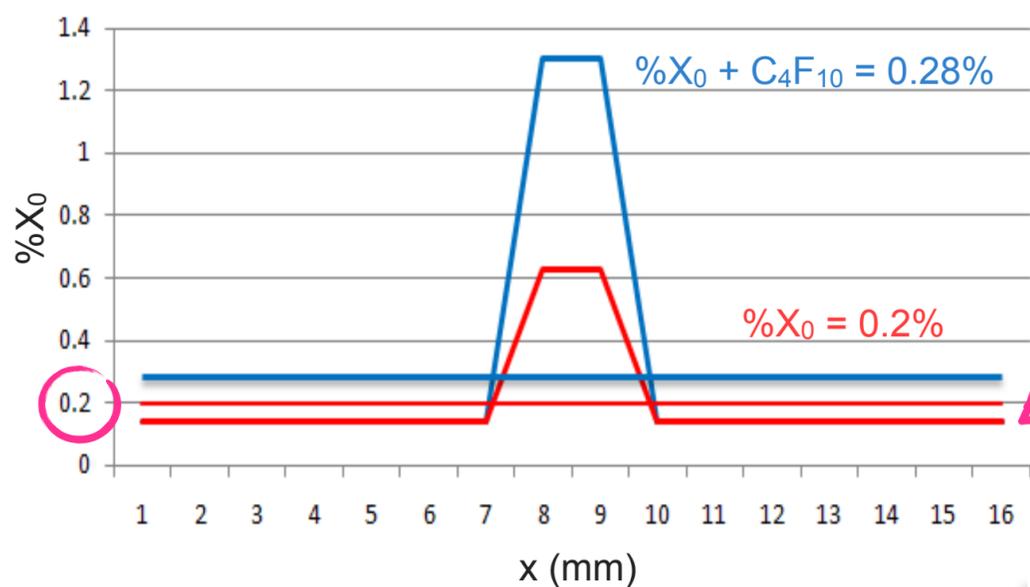
Carbon Foam + Metal Pipe



Silicon Microchannels



drawings not to scale



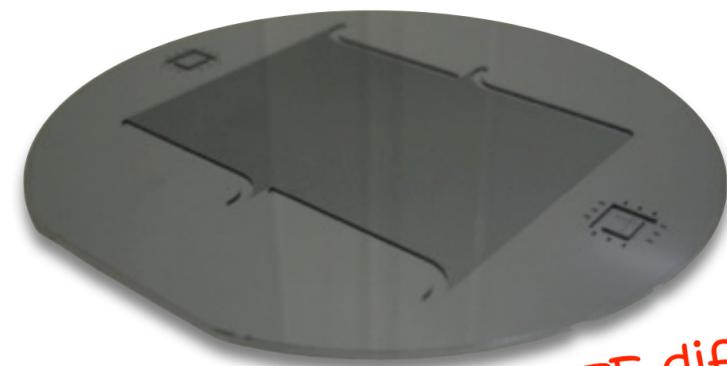
Metal Pipe

Carbon Foam

ΔT between heat source and heat sink for power dissipations of $\sim 1\text{W}/\text{cm}^2$

10°C

5°C



no CTE difference

microcool projects

CERN PH-DT

Andrea Catinaccio
Raphael Dumps
Alan Honma
Luc Kottelat
Camille Ligneau
Alessandro Mapelli
Ian McGill
Jérôme Noel
Paolo Petagna
Giulia Romagnoli
Bart Verlaat



ALICE ITS upgrade

Andrea Francescon



ATLAS IBL upgrade

Cinzia Da Via'
Vladyslav Tyzhnevyy



LHCb VeLo upgrade

Jan Buytaert
Paula Collins
Ed Greening
Sasha Leflat
Andrei Nomerotski



Microengineering

Aurélie Pezous



NA62 GTK

Enrico Da Riva
Kaitlin Howell
Alex Kluge
Michel Morel
Georg Nuessle
Vinod Rao



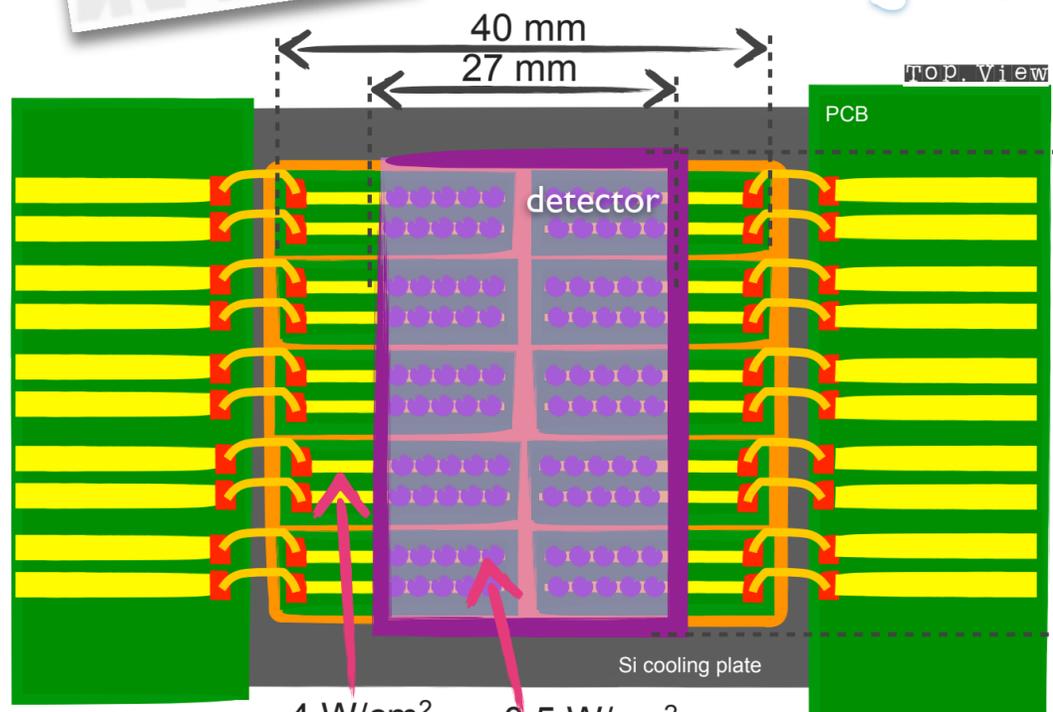
Microsystems Laboratory

Philippe Renaud
Harald van Lintel

experiment	material	temperature	coolant phase	pressure	coolant fluid
ALICE	0	20°C	evaporative	2 bars	C ₄ F ₁₀
ATLAS	TBD	TBD	TBD	TBD	TBD
LHCb	500 μm	-30°C	evaporative	60 bars	CO ₂
NA62	150 μm	-10°C	liquid	10 bars	C ₆ F ₁₄

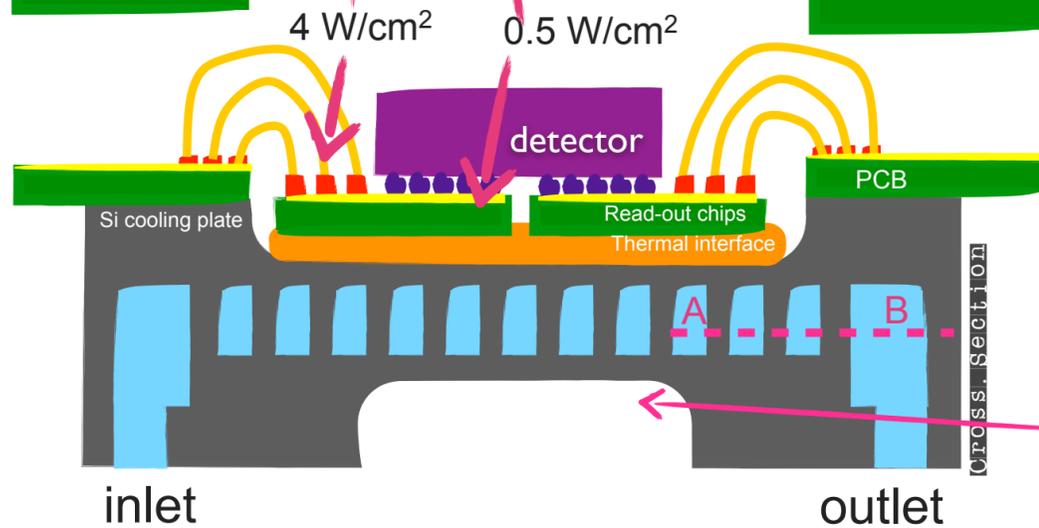
approved !

NA62 GigaTracker silicon pixel detector cooling

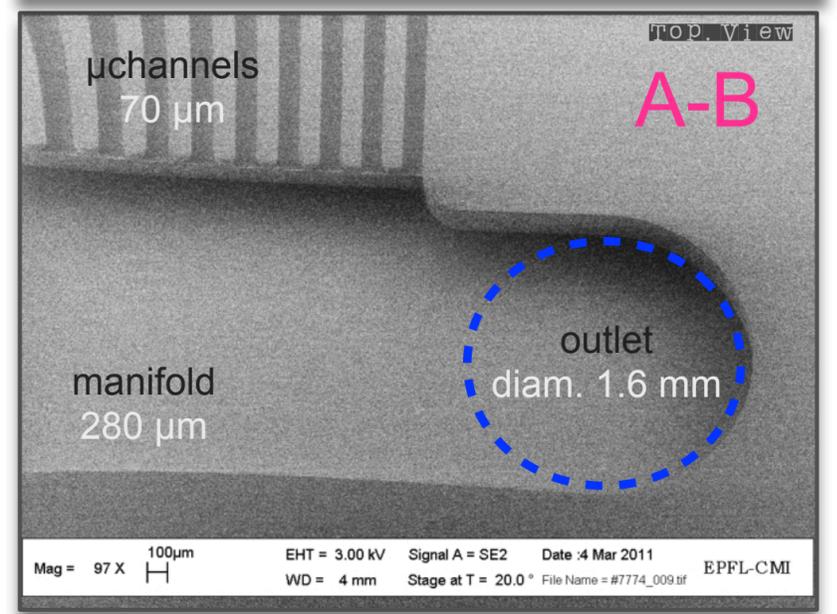
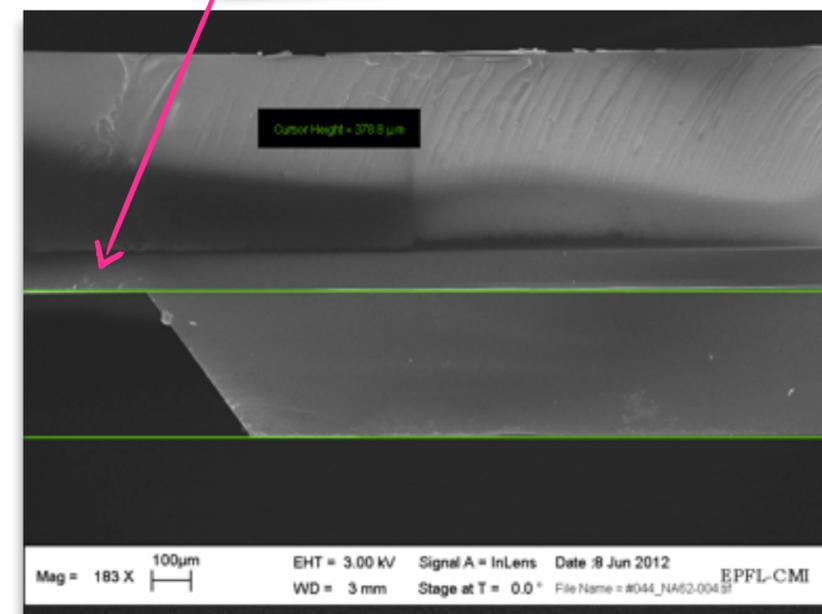
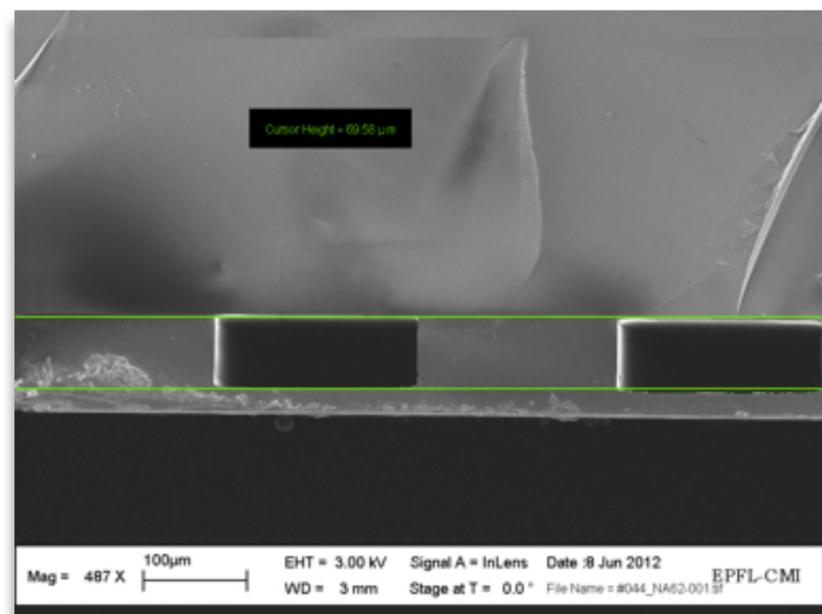
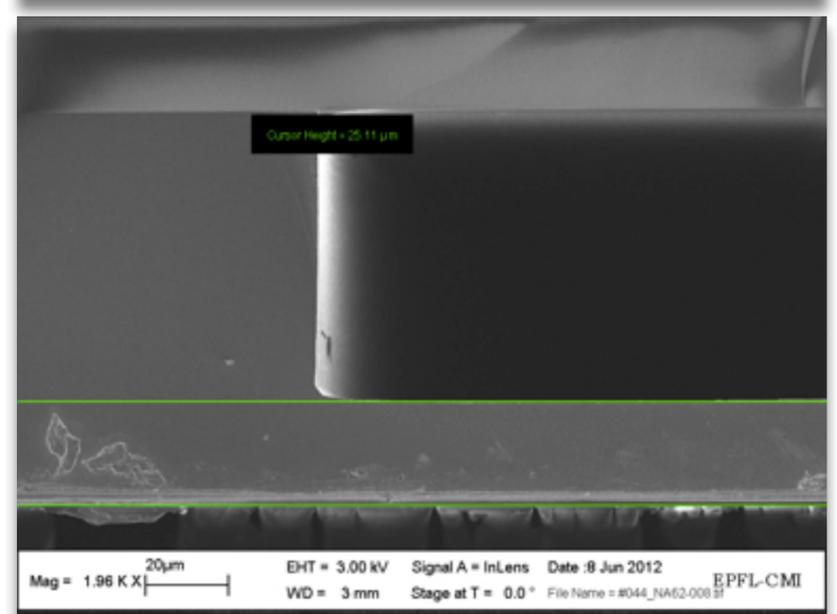
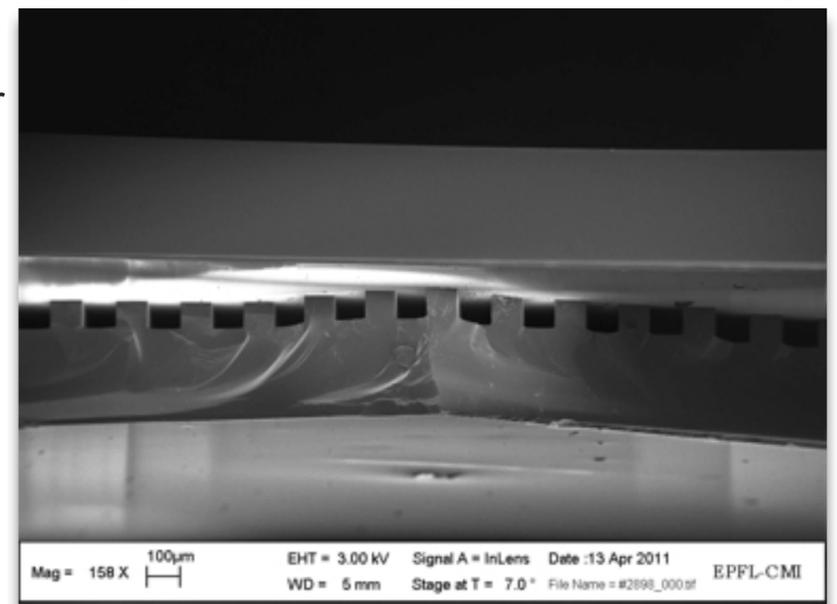


- Cooling requirements
 - minimize material below detector
 - detector area: 60 x 27 mm
 - T on Si detector: $-20^{\circ}\text{C} \pm 5^{\circ}\text{C}$
 - ΔT over detector: 6°C
 - Heat dissipation by read-out chips:
 - 4 W/cm² in the periphery (Digital)
 - 0.5 W/cm² in the center (Analog)
 - total 48 W

- Cooling solution adopted by the NA62 collaboration
 - thin silicon plate (130 μm)
 - C₆F₁₄ liquid



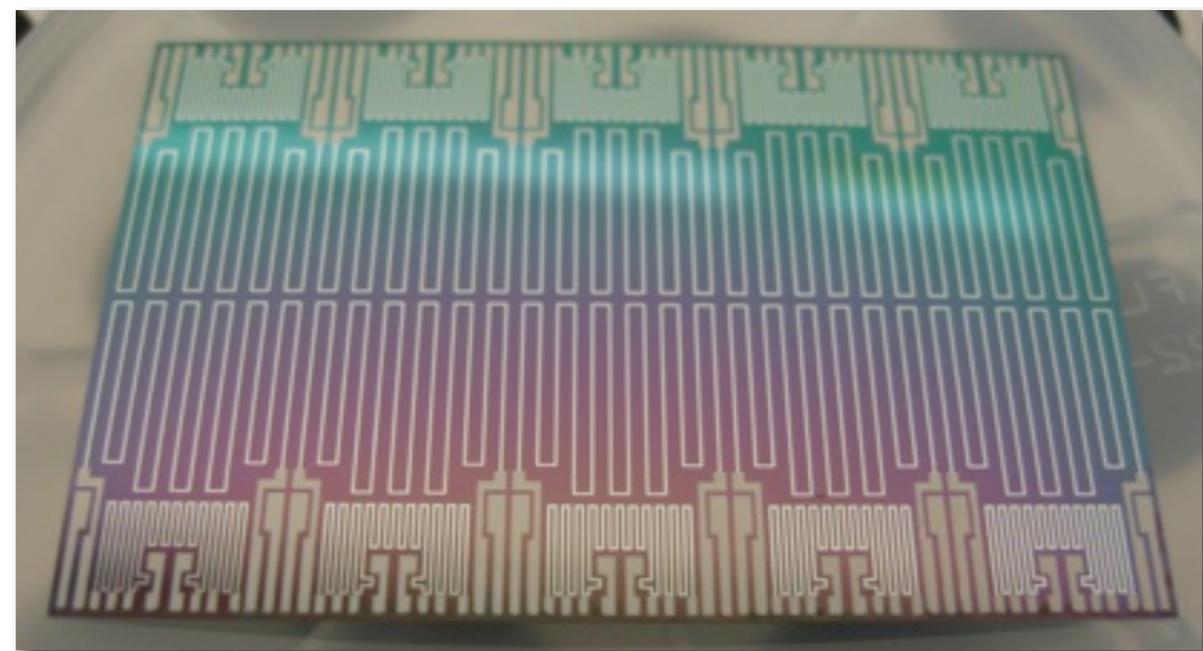
locally thinned to 130 μm in detector acceptance



NA62 silicon prototypes



Silicon microchannel cooling plate



100 μm thick mock-up fabricated with CSEM

Silicon thermo-mechanical mock-ups

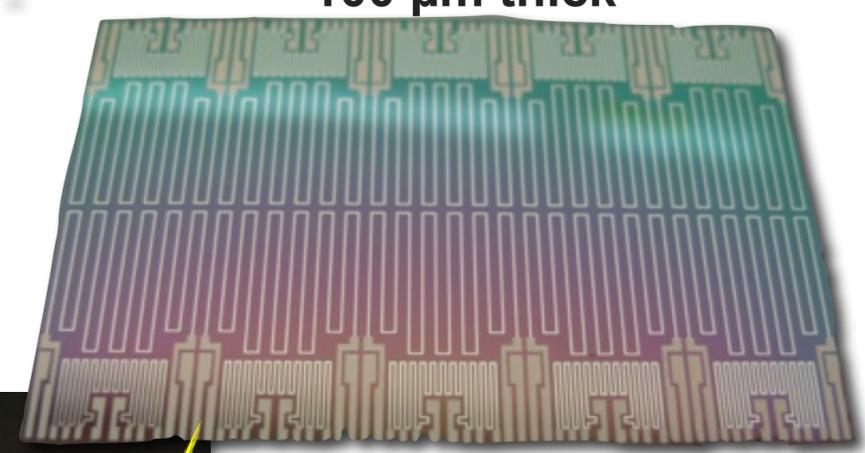
CERN PH-DT is working with major european actors for the fabrication of silicon cooling plates (CEA-LETI, IceMOS...) and is actively collaborating with CSEM on the development of a 6" platform integrating cooling, thermo-mechanical simulations of detector and read-out with Through-Silicon Vias (TSV).

silicon thermo-mechanical mock-ups

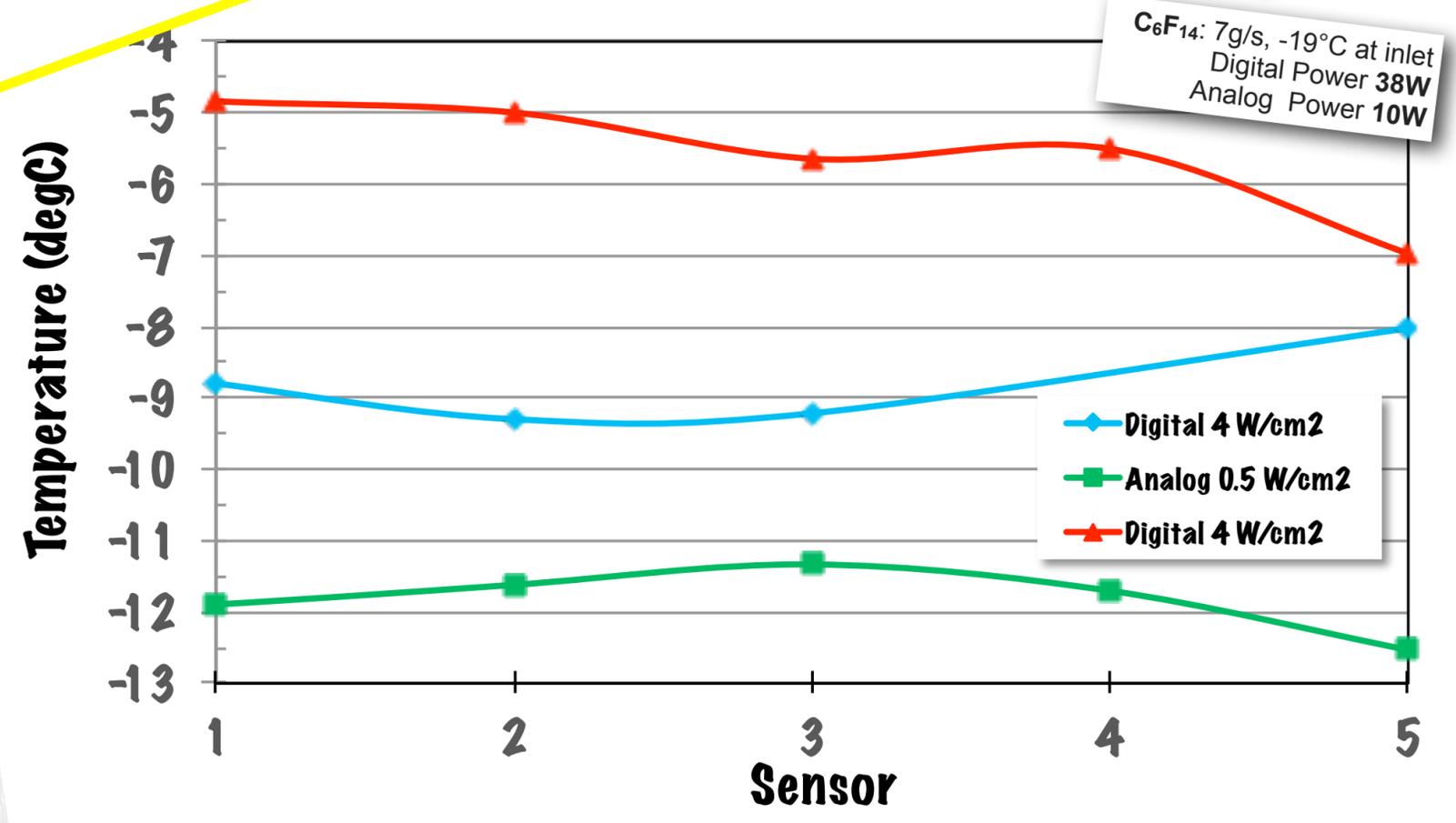
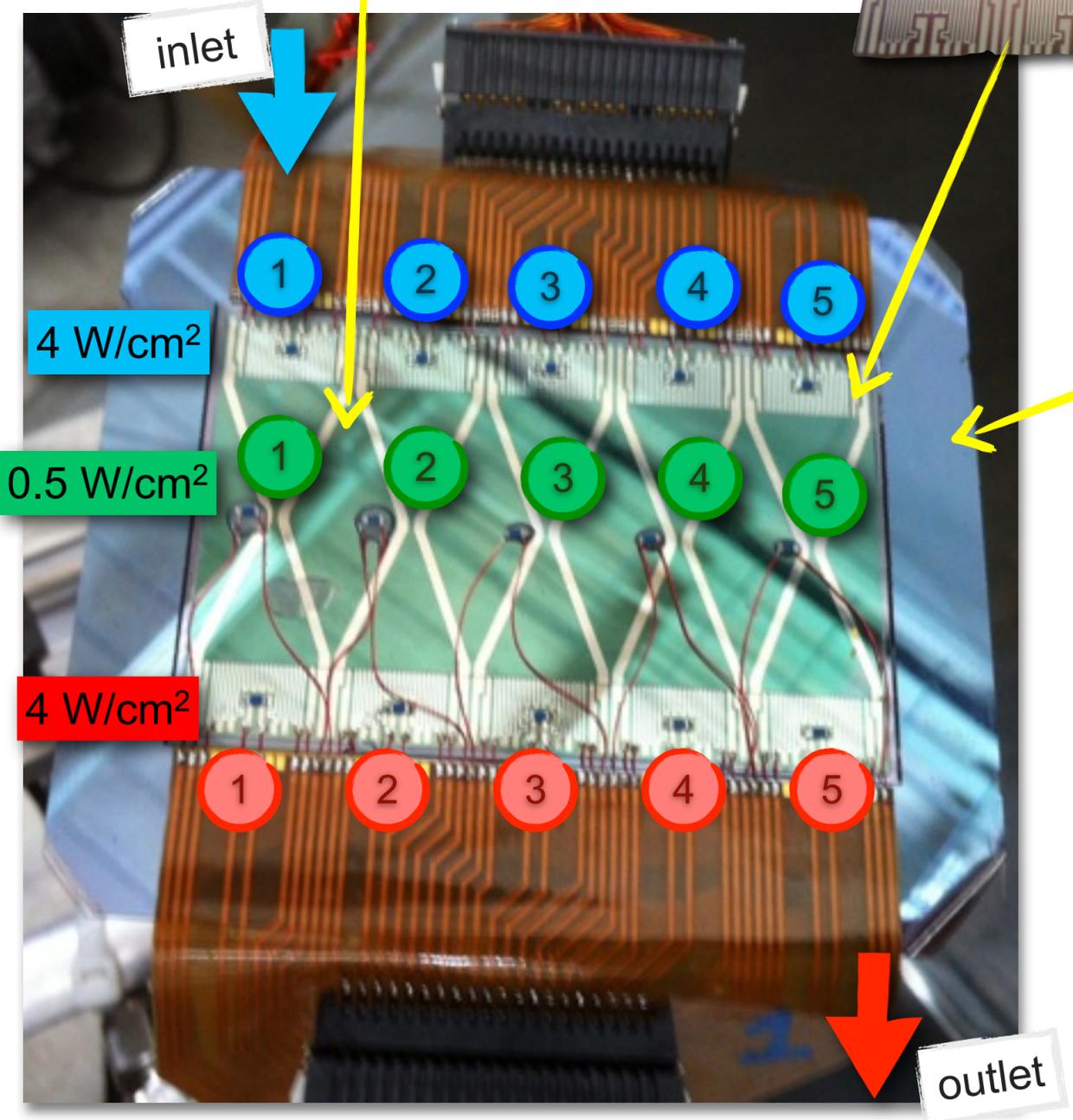
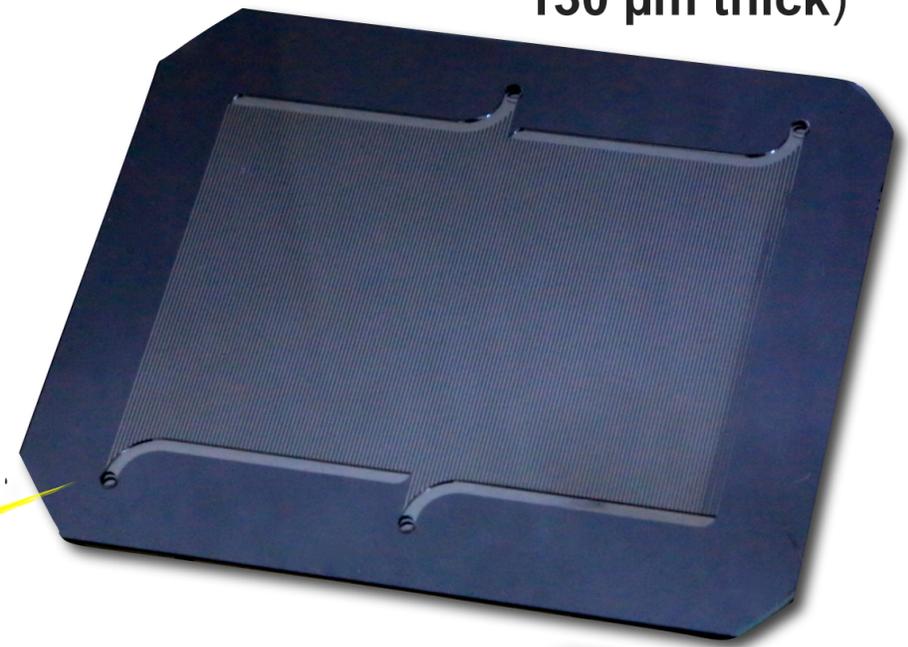
tracker mechanical mock-up
(silicon + metal)
200 μm thick



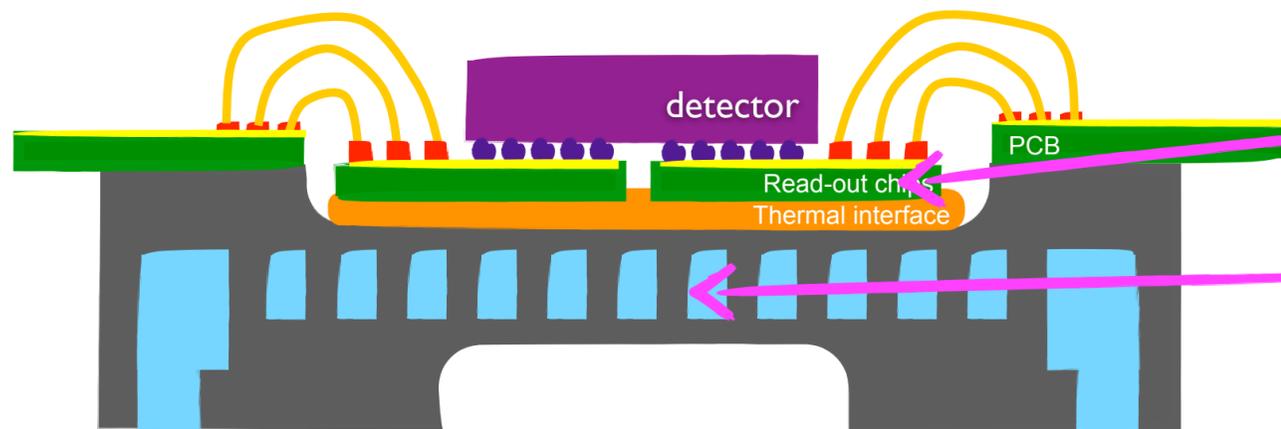
r/o electronics thermo-mechanical mock-up
(silicon + metal)
100 μm thick



cooling plate
(silicon)
130 μm thick

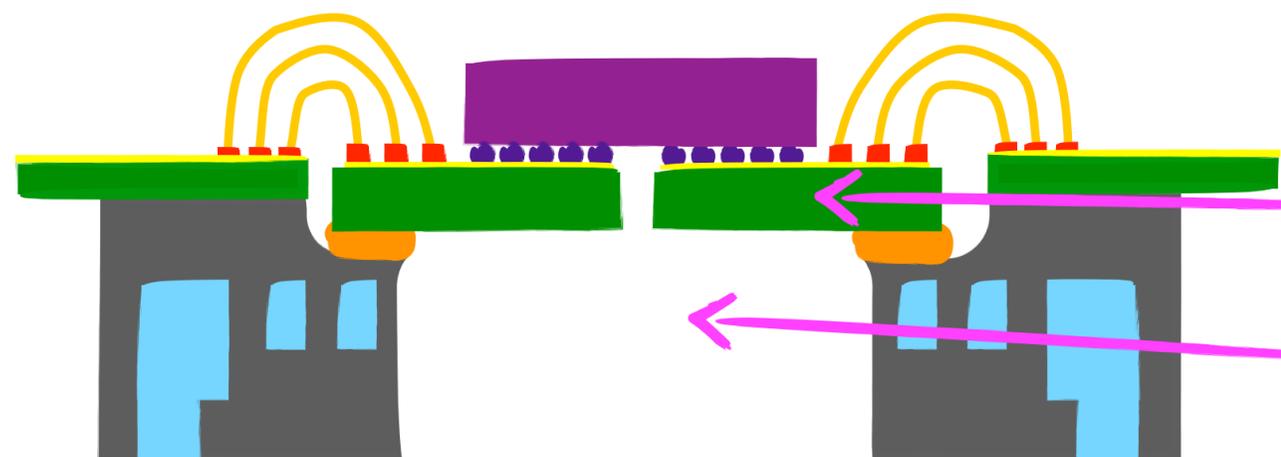


NA62-GTK alternative cooling proposal



■ baseline (**thin plate**)

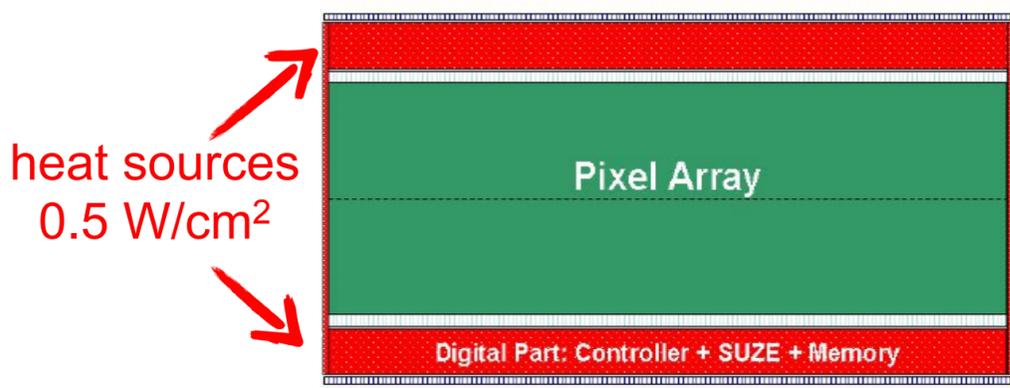
- thin electronics (100 μm)
- thin cooling (130 μm)



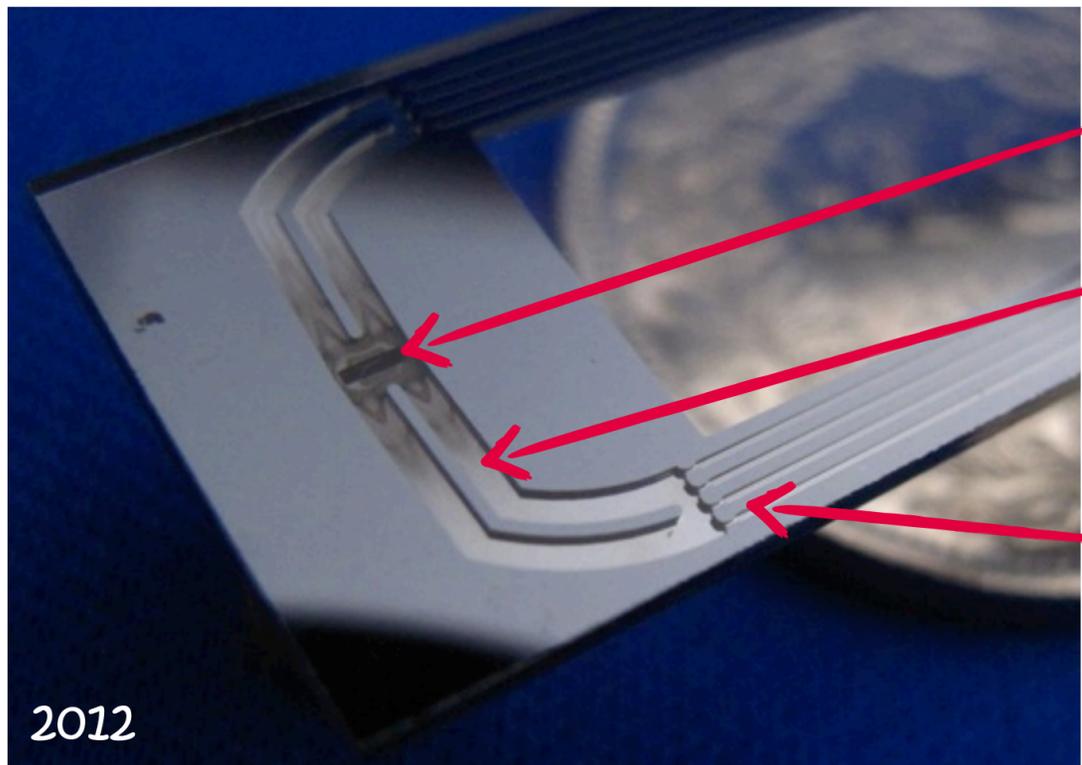
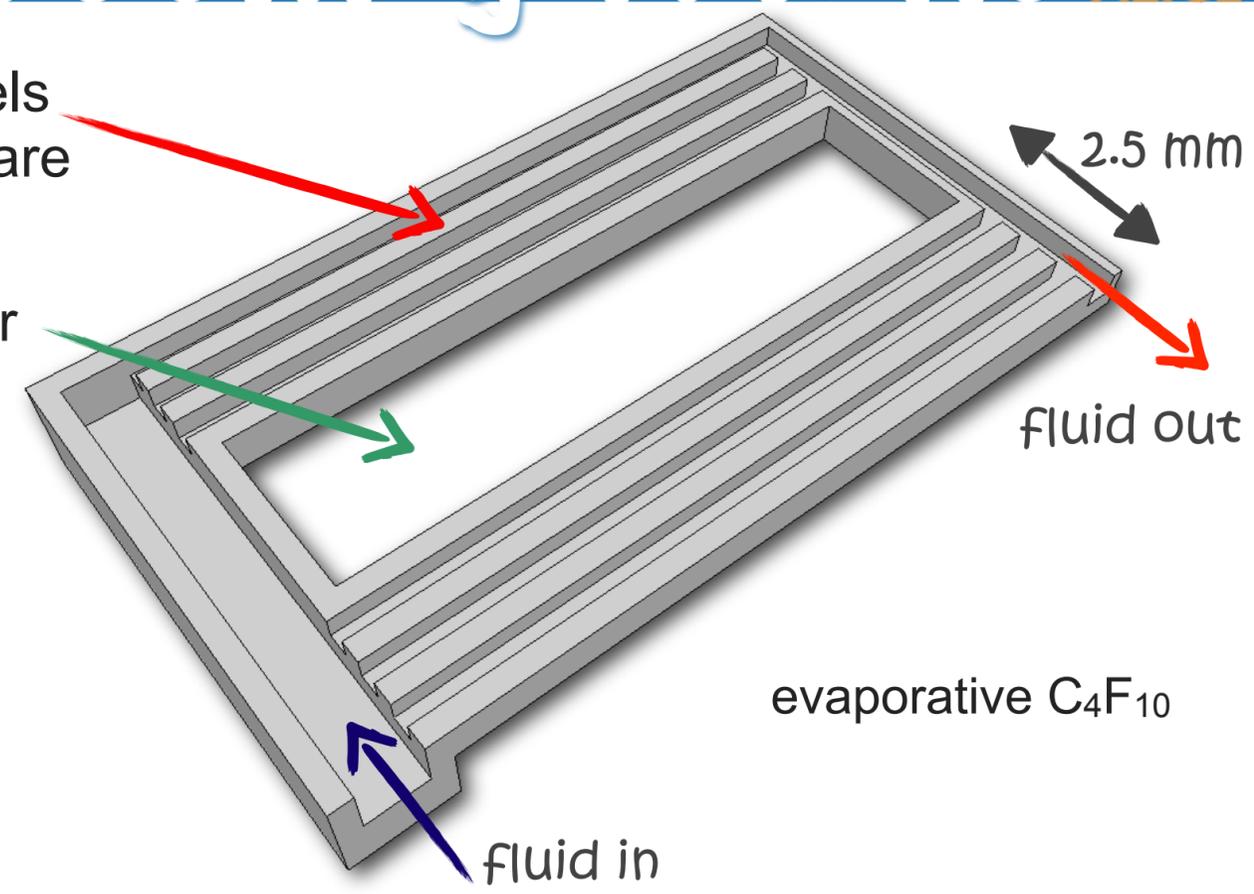
■ alternative (**frame**)

- thicker electronics (200 μm)
- no silicon in acceptance (0 μm)

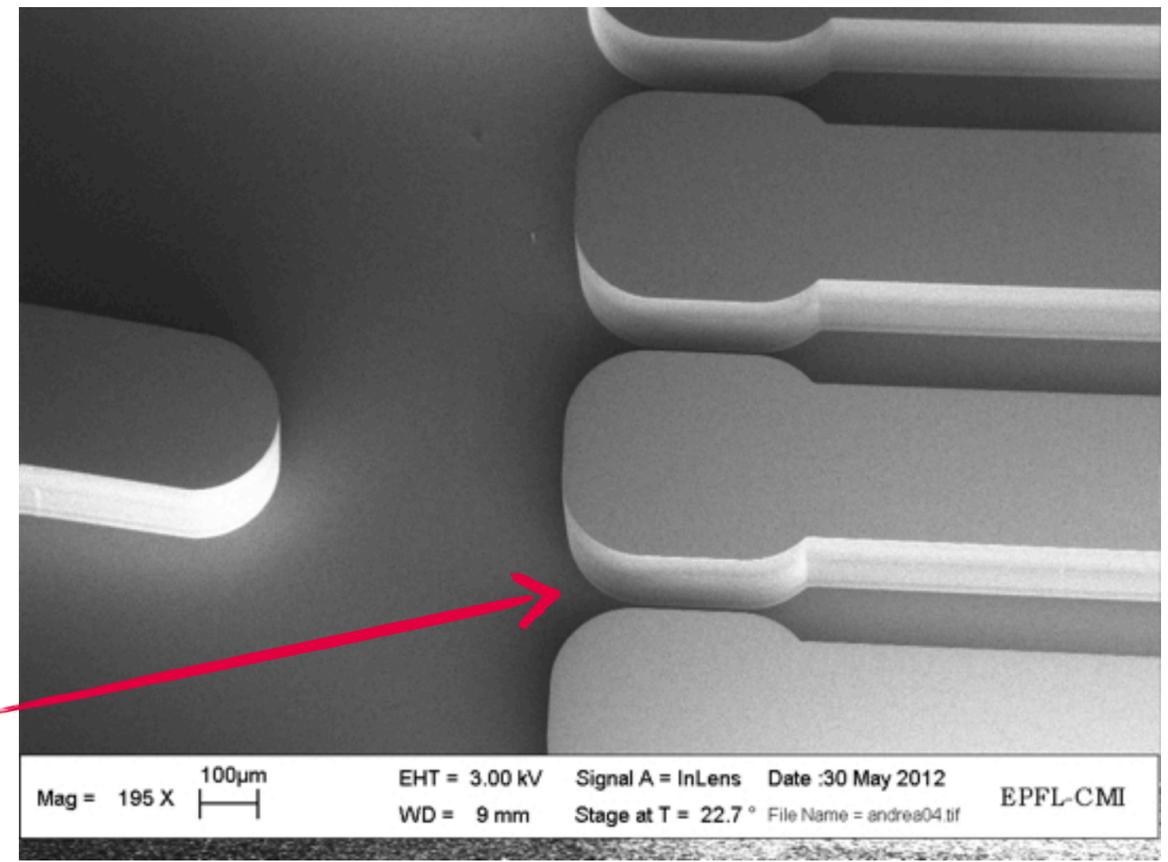
ALICE silicon cooling frame



- cooling μ -channels only where they are needed
- no material under detector



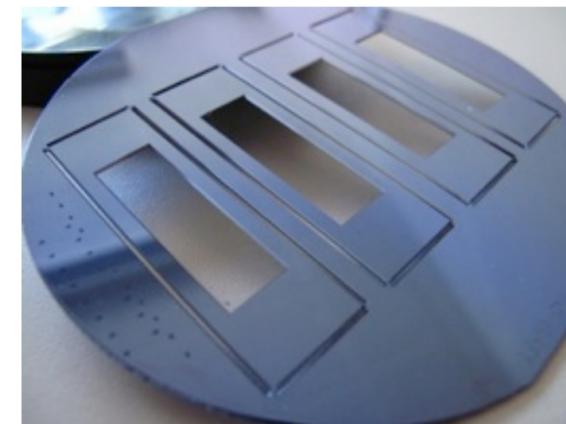
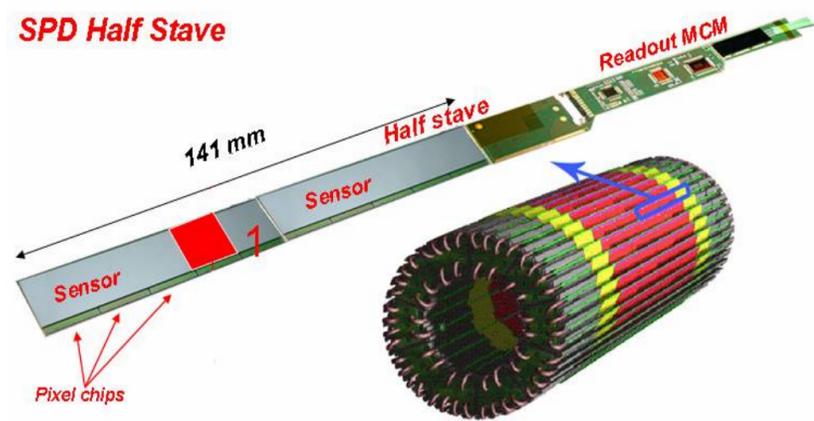
- Inlet
- distribution manifold
- μ -channels restrictions



2012

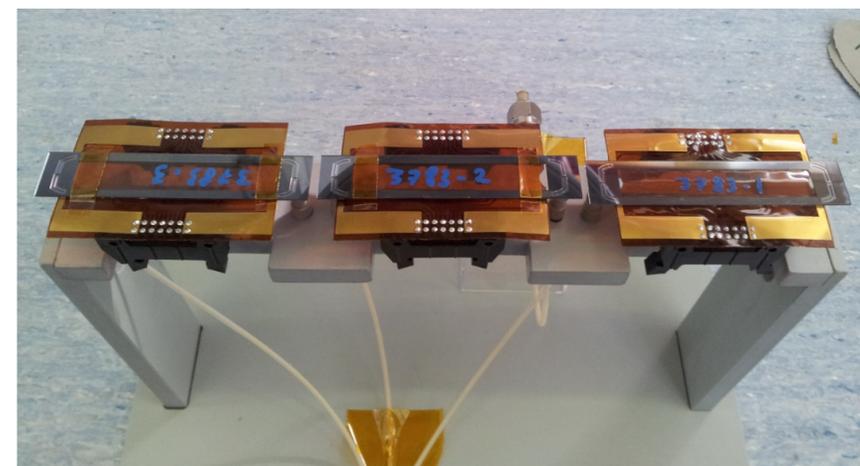
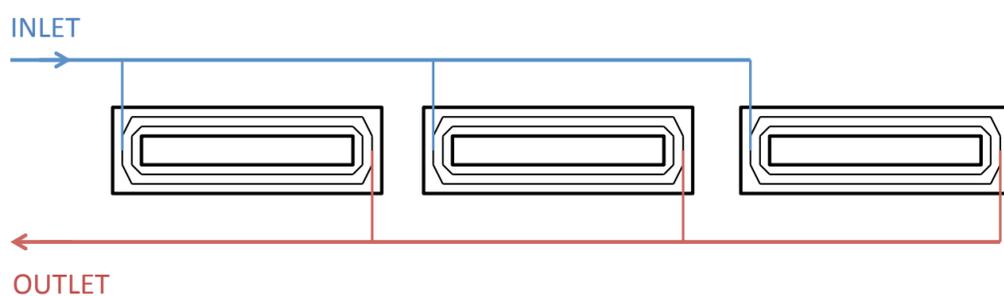
ALICE.. towards a stave

The cooling has to be performed on about 300 mm but the length of the cooling frames is limited by the diameter of the Si wafers.

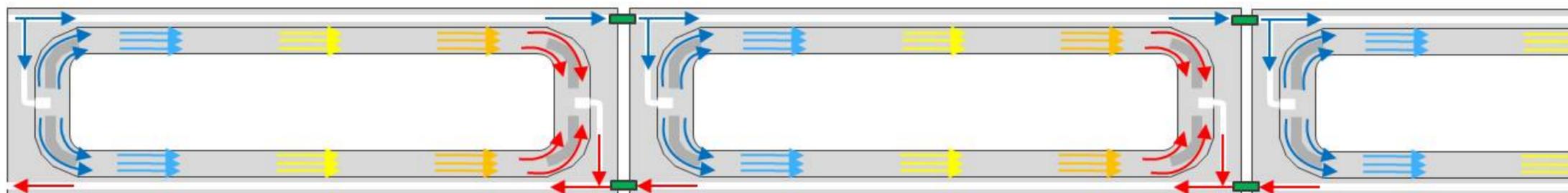


Si wafers, 100 mm diameter.

The proof of principle is performed by daisy-chaining several frames.



A new fabrication process is being developed to connect the frames in-plane with needles.



TOPICAL WORKSHOP ON ELECTRONICS FOR PARTICLE PHYSICS 2011,
26–30 SEPTEMBER 2011,
VIENNA, AUSTRIA

Microfluidic cooling for detectors and electronics

A. Mapelli,^{a,b,1} P. Petagna,^a K. Howell,^c G. Nuessle^d and P. Renaud^b

^aCERN Physics Department,
Geneva, Switzerland

^bEPFL Microsystems Laboratory,
Lausanne, Switzerland

^cGeorge Mason University,
Virginia, United States of America

^dUniversité Catholiques de Louvain
Louvain-la-Neuve, Belgique

E-mail: Alessandro.Mapelli@cern.ch

ABSTRACT: Micro-channel cooling is gaining considerable attention as an alternative technique for cooling of high energy physics detectors and front-end electronics. This technology is being evaluated for future tracking devices, where material budget limitations are a major concern. It is currently under investigation as an option for the cooling of the NA62 Gigatracker silicon pixel detector, where a micro-fabricated silicon cooling plate would stand directly in the beam. Other possible applications are also being studied in the context of LHC detectors upgrades. In this paper, the current status of this R&D at CERN is presented.

KEYWORDS: Detector cooling and thermo-stabilization; Particle tracking detectors (Solid-state detectors)

to appear in *Microelectronics Journal*

Application of Micro-channel Cooling to the Local Thermal Management of Detectors Electronics for Particle Physics

A. Mapelli^{* ****}, G. Nuessle^{**}, P. Petagna^{*}, A. Pezous^{***}, P. Renaud^{****}

^{*}CERN Physics Department, Geneva, Switzerland

^{**}Université Catholique de Louvain, Belgium

^{***}CSEM, Neuchâtel, Switzerland

^{****}EPFL Microsystems Laboratory, Lausanne, Switzerland

ABSTRACT:

Micro-channel cooling is gaining considerable attention as an alternative technique for cooling of high energy physics detectors. This is of particular interest for future trackers, where large surfaces are involved and the amount of material must be drastically reduced. Combining the flexibility of standard micro-fabrication processes with the high thermal efficiency typical of micro-fluidics, it is possible to produce effective thermal management devices well adapted to different specific applications. The first case presented is the NA62 GTK silicon pixel detector, where low temperature liquid fluid will be circulated in a micro-fabricated silicon plate locally thinned to 130 μm in the detector sensitive area. Other applications are presently being developed for evaporative cooling in the context of the ALICE and LHCb detector upgrades at LHC. In the former case the devices are being optimized for low pressure/room temperature evaporation; in the latter for high pressure and temperature below 0°C.

KEYWORDS: electronic cooling, micro-channels, thermal management.

1 MICRO-CHANNEL COOLING IN HEP

Local thermal management through micro-fluidic devices is already under study for possible implementation in future 3D architectures for high power computing. In this context, highly effective micro-fabricated cooling devices, capable of dealing with power densities up to 700 W/cm^2 have been recently proposed. Examples span from 2 mm thick silicon assemblies designed for single phase water cooling [1] to few-mm thick copper plates optimized for two-phase refrigerants [2].

When designing the on-board cooling for High Energy Physics (HEP) tracking detectors, the power densities involved are two order of magnitude lower than in high power computing (typically in the range 0.5–4 W/cm^2). However, large surfaces of silicon detectors are used and, depending on the detector size, a total heating power up to few tens of few kW must be removed. For this kind of application several important issues must be addressed, including the minimization of:

- The amount of material crossed by particles;

- The temperature difference between heat source and heat sink for a given quantity of heat to be removed;
- The temperature gradients on the surface of the sensor.

Furthermore, the detector layout is often very packed and geometrically complex, thus only limited space is available for piping and connections. In many cases, in order to preserve the silicon sensor from severe degradation caused by the high level of radiation, it is also necessary to operate and maintain the detectors at negatives temperatures (typically in the range -10–-20°C) [3]: this increases the impact of CTE mismatch problems between the silicon heat source and a metal heat sink. The thermal management of today's trackers is based on complex networks of mm-size metallic pipes (Fig. 1). The pipes are locally brought in connection with the region where the highest concentrated heat sources are located through heat spreaders, specifically designed to be compliant with mutual displacements due to CTE mismatch. Due to the small contact surfaces and the long chains of thermal resistances typical of these configurations, the temperature difference between the module surface and the coolant ranges typically between 15 and 20°C (see e.g. [4]).

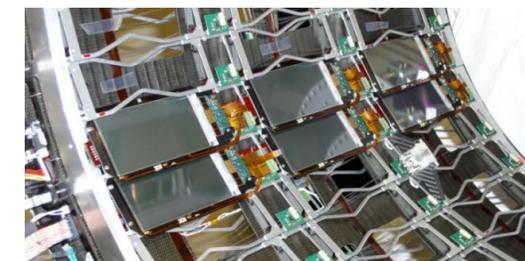


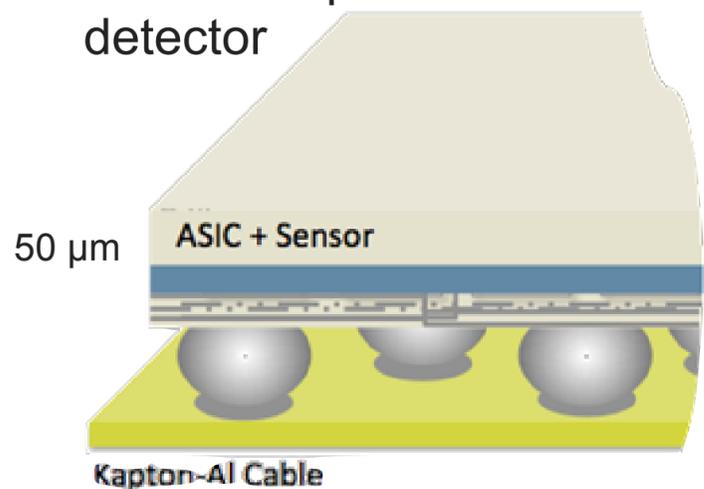
Figure 1: Typical cooling pipe network in today's trackers

Local thermal management through silicon micro-fluidic devices, in connection with either single-phase or two-phase flow, is a good candidate for solving all the above mentioned issues [5], [6]. The concept, schematically depicted in Fig. 2 for the case of a Pixel tracking detector, is extremely simple: a thin micro-structured silicon plate with the same shape and size of the detector module to be cooled is placed in contact with the heat source by an adhesive layer. As the contact surface between the heat source and the heat sink is maximized and the power density is not

2012 JINST 7 C01111

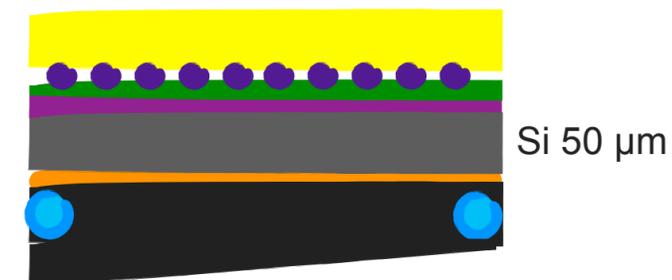
towards integrated cooling

monolithic pixel detector

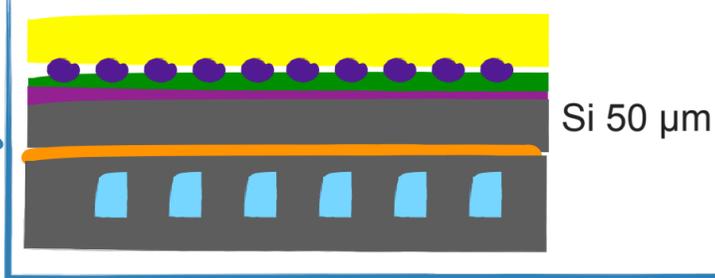


Microchannels integration in silicon detectors (option 3) has to be investigated together with the design and development of the detectors.

Option 1
cooling pipes



Option 2
Si cooling plate



glueing



Si wafers

epi + CMOS

thinning back

bump bonding

oxidation

direct bonding

thinning top

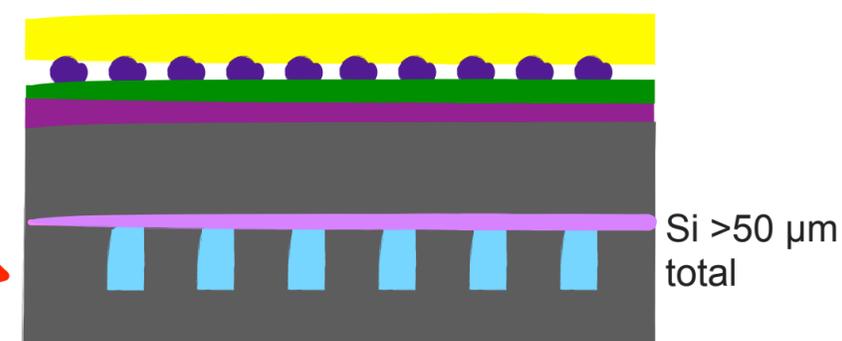
epi + CMOS

etching

SOI with embedded channel

thinning

Option 3
embedded cooling channels



A. Mapelli, L. Musa, P. Petagna, P. Rjedler

SOI: Silicon-On-Insulator

How SOI wafers are made

[From P. N. Dunn, *Solid State Technol.*, October, 32-35 (1993). Copyright 1993 PennWell Publishing Company, with permission.]

Many different silicon-on-insulator materials have been developed over the years, but two are currently being used for IC production: SIMOX (Separated by Implanted OXygen) and bonded wafers.

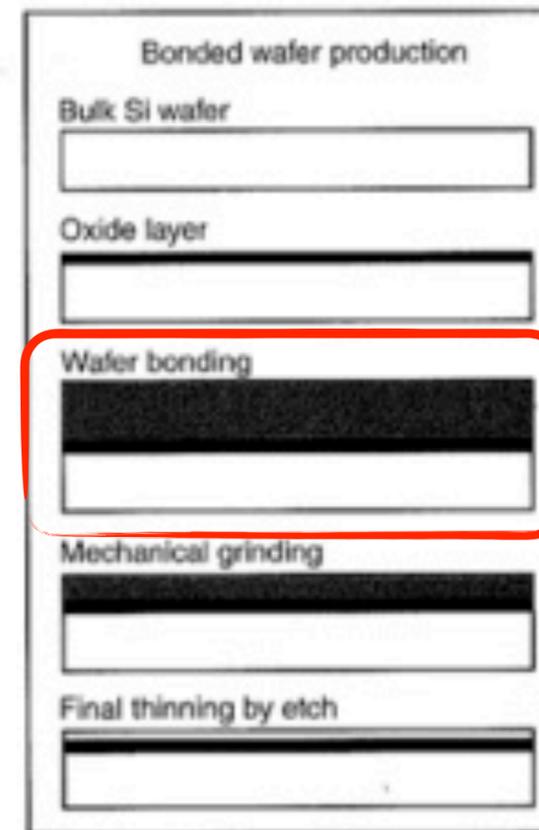
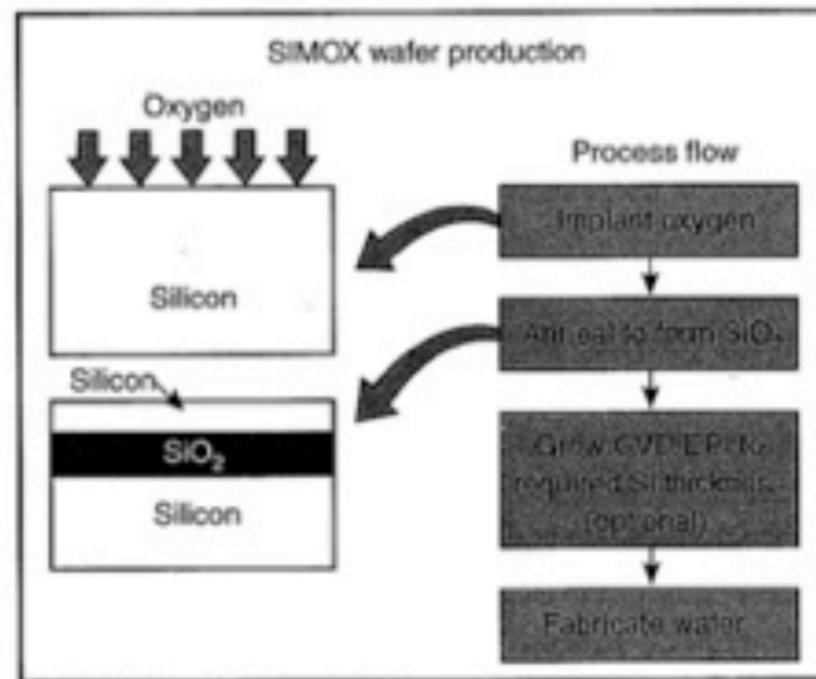
In the SIMOX process, a standard silicon wafer is implanted with oxygen ions, and then annealed at high temperatures; the oxygen and silicon combine to form a silicon oxide layer beneath the wafer surface. To minimize wafer damage, the oxygen is sometimes implanted in two or more passes, each followed by an anneal. The oxide layer's thickness and depth are controlled by varying the energy and dose of the implant and the anneal temperature. In some cases, a CVD process is used to deposit additional silicon on the top layer.

The bonded wafer process starts with an oxide layer of the desired thickness (typically 0.25 to 2 microns) being grown on a standard silicon wafer. That wafer is then bonded at high temperatures to another wafer, with the oxide sand-

wiches between. One of the wafers is then ground to a thickness of a few microns using a mechanical tool.

Because advanced devices require an even thinner layer, more silicon must be removed. The wafer may be etched with a confined plasma, between 3 and 30 mm wide, which is stepped across the wafer surface. A film thickness map is made for each wafer and used to compute the dwell time for the plasma etcher at each

stop. The process can be repeated for additional precision. Silicon thicknesses of a little as 1000 to 3000 Å, with total thickness variation of 200 Å have been achieved. IBM has also developed an etch-back process for bonded wafers.



bonding of a wafer with microchannels instead of bulk silicon

micro-cooling studies for future inner layers of ATLAS Pixels

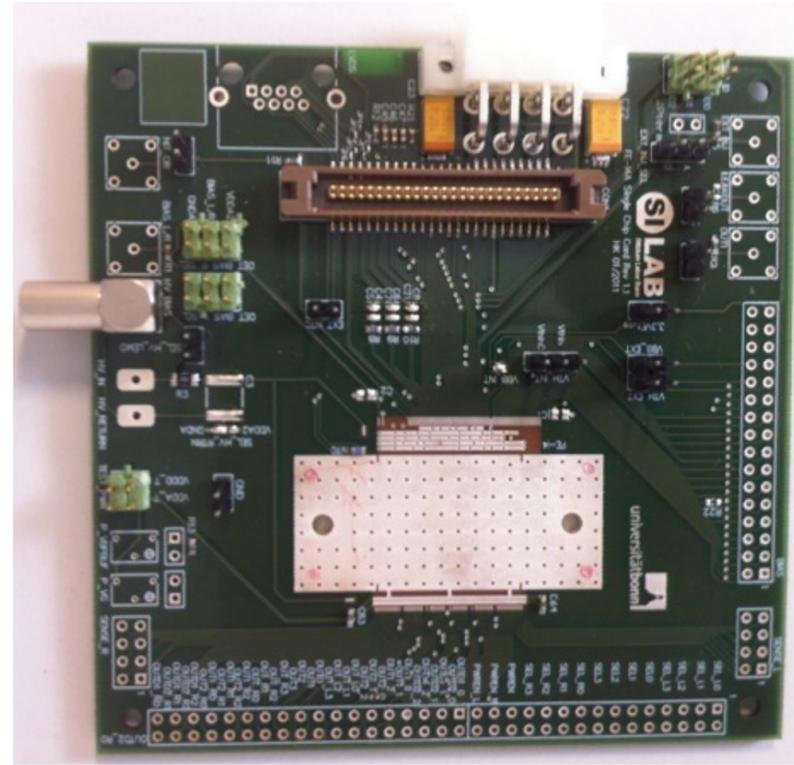
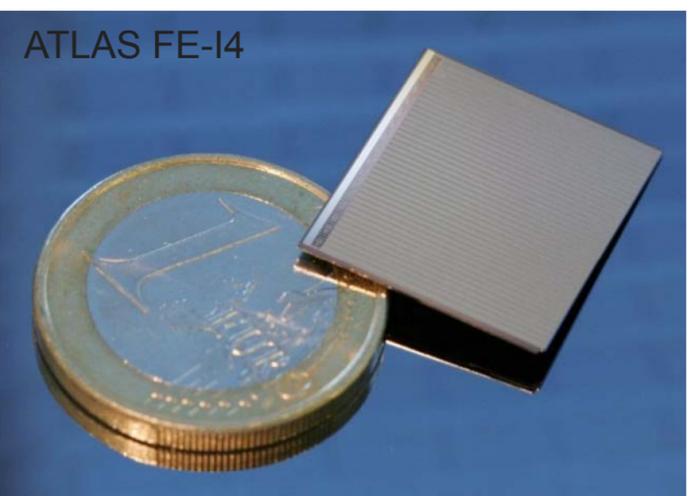


Conclusions

We are exploring ways to build a low mass 3D system for the HL-LHC by looking at:

- Thin modules with reduced IES+embedded cooling and through chip bias supply
- Preliminary simulations on charge multiplication by design (before irradiation) show that gain goes from 2 to 8 depending on configuration at ~120V with good signal response uniformity. Slight decrease of pulse height after irradiation because of trapping but not too disturbing in terms of homogeneity
- Industrial developments and work of other groups with similar needs are very promising
- Still a lot of R&D to understand the feasibility of some of the steps

the heat dissipated by the electronics chip is 1.1W/chip and 0.24W/3D sensor, i.e., overall heat dissipation would be ~1.35W/hybrid. These values are valid for IBL. ATLAS upgrade will result in much higher fluences and, hence, in higher sensor current consumption and, consequently, much higher heat dissipation. Thus, we will also try to make tests with heat dissipation higher than 1.35W/hybrid.



Micro-cooling at FBK

Current development in FBK in collaboration With PISA colleagues for SUPERB detectors, also ALICE is considering for its pixel upgrade

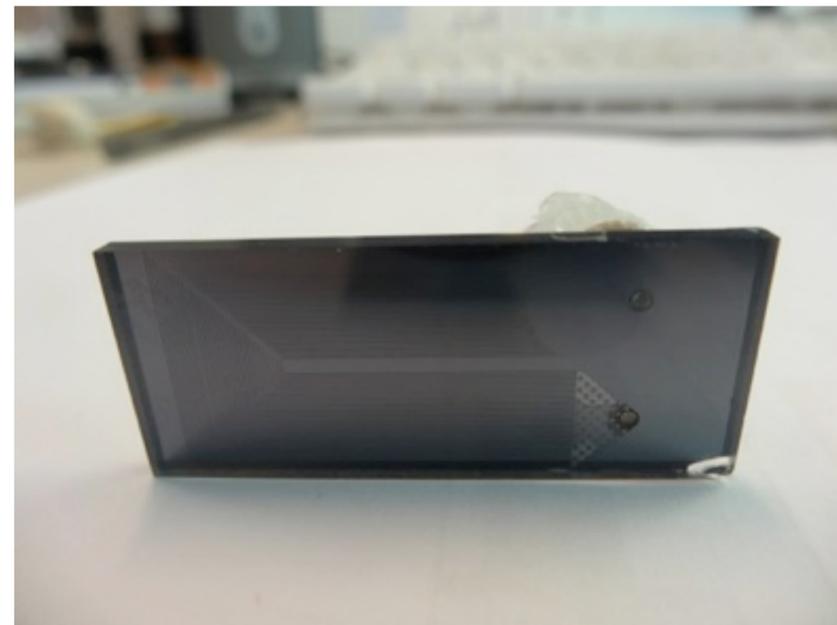
Collaboration has been proposed

Development of light prototypes support for silicon pixel detectors cooling based on microchannel technology

F. Bosi - M. Massa

INFN-Pisa
on behalf of the Super-B SVT Group

F.Bosi, M.Massa, PIXEL 2010, September 6 – 10, 2010 Grindelwald, Switzerland

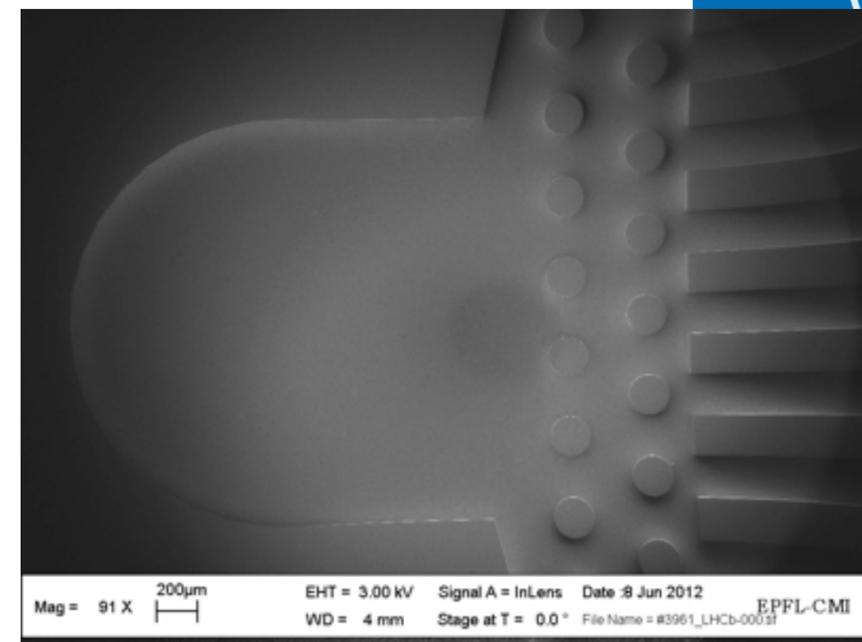
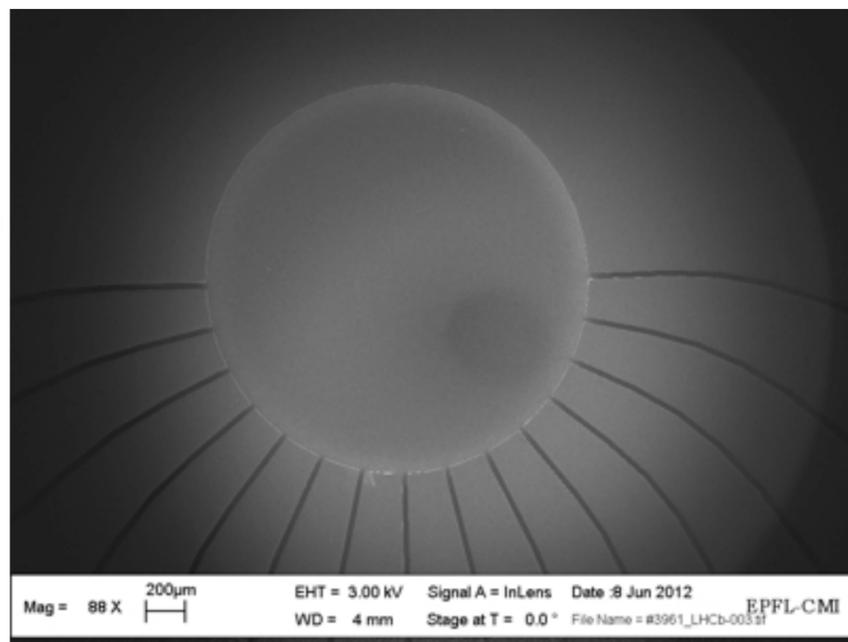
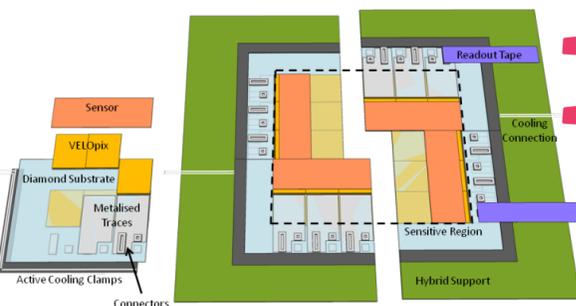


First batch of silicon microcoolers finished. To be tested in the coming days.

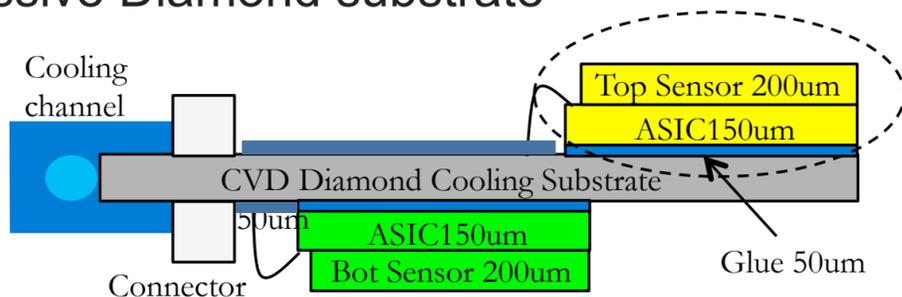
LHCb VeLo upgrade...CO₂ in microchannels

Cooling requirements

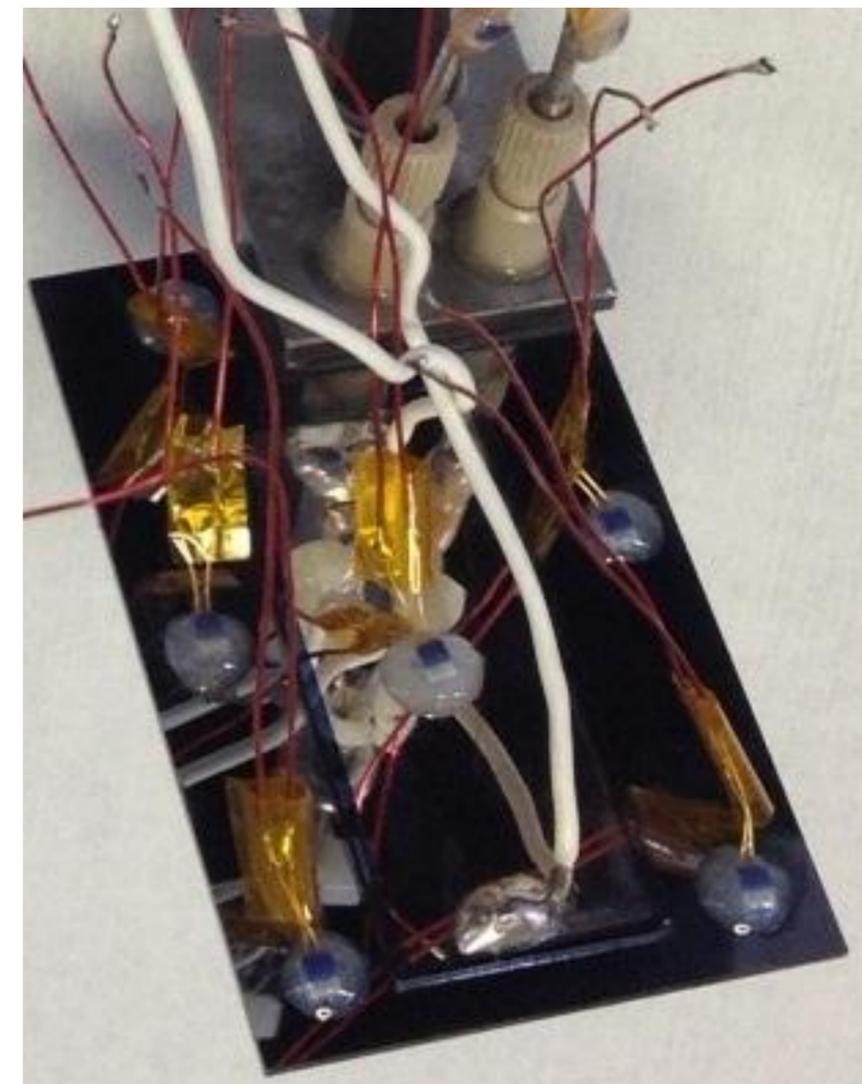
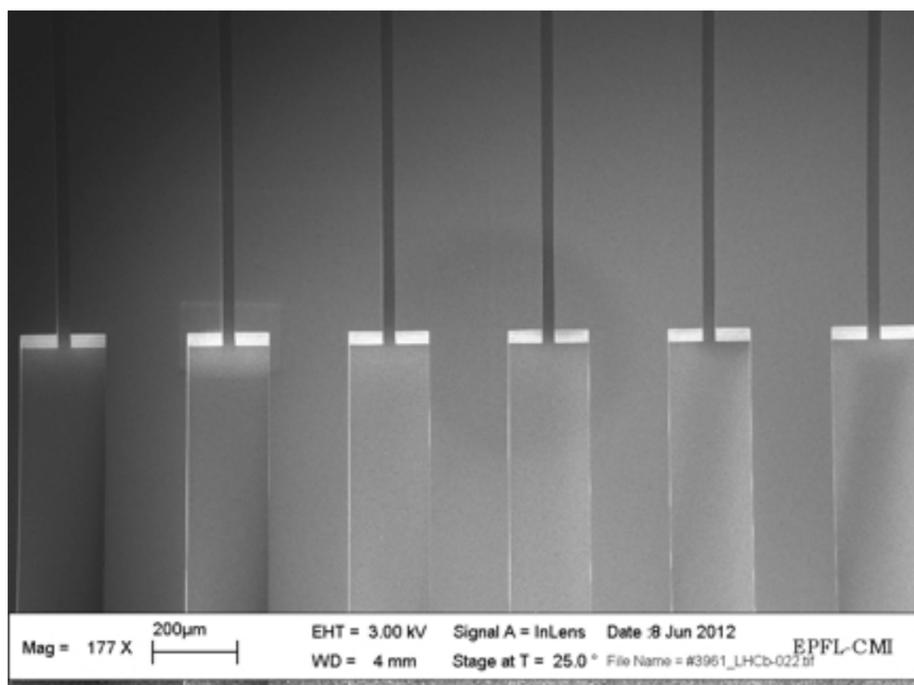
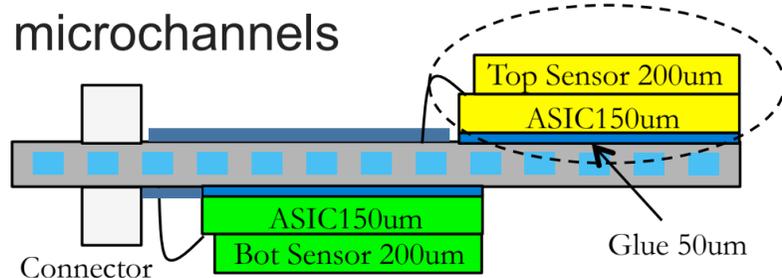
- Diss. power: ~2 W/cm²
- Cooling substrate
- in acceptance: <500 μm
- out of acceptance: 1mm



passive Diamond substrate



Silicon microchannels



First experimental results submitted to NIM

Evaporative CO₂ cooling using microchannels etched in silicon for the future LHCb vertex detector

A. Nomerotski^{a,b}, J. Buytart^a, P. Collins^a, R. Dumps^a, E. Greening^b, M. John^b, A. Mapelli^a,
A. Leflat^c, Y. Li^d, G. Romagnoli^e, B. Verlaat^a.

^a CERN, CH-1211 Genève 23, Switzerland

^b University of Oxford, Particle Physics, Denys Wilkinson Building, Keble Road, Oxford OX1 3RH, UK

^c Skobelitsyn Institute of Nuclear Physics, Moscow State University, Moscow 119991, Russian Federation

^d Department of Engineering Physics, Tsinghua University, Beijing 100084, China

^e Department of Mechanical Engineering, University of Genoa, Via all'Opera Pia 15, Genoa 16145, Italy

Abstract

The extreme radiation dose received by vertex detectors at the Large Hadron Collider dictates stringent requirements on their cooling systems. To be robust against radiation damage, sensors should be maintained below -20°C and at the same time, the considerable heat load generated in the readout chips and the sensors must be removed. Evaporative CO₂ cooling using microchannels etched in a silicon plane in thermal contact with the readout chips is an attractive option. In this paper, we present the first results of microchannel prototypes with circulating, two-phase CO₂ and compare them to simulations. We also discuss a practical design of upgraded VELO detector for the LHCb experiment employing this approach.

Keywords: Silicon sensor; vertex detector; CO₂ cooling; microchannel

NUCLEAR ELECTRONICS & COMPUTING

XXIII International Symposium
 Varna, Bulgaria, September 12-19, 2011

Proceedings of the Symposium

NEC'2011

ЯДЕРНАЯ ЭЛЕКТРОНИКА И КОМПЬЮТИНГ

XXIII Международный симпозиум
 Варна, Болгария, 12-19 сентября 2011 г.

Труды симпозиума

Дубна 2011

Detector challenges at the CLIC multi-TeV e^+e^- collider

D. Dannheim¹

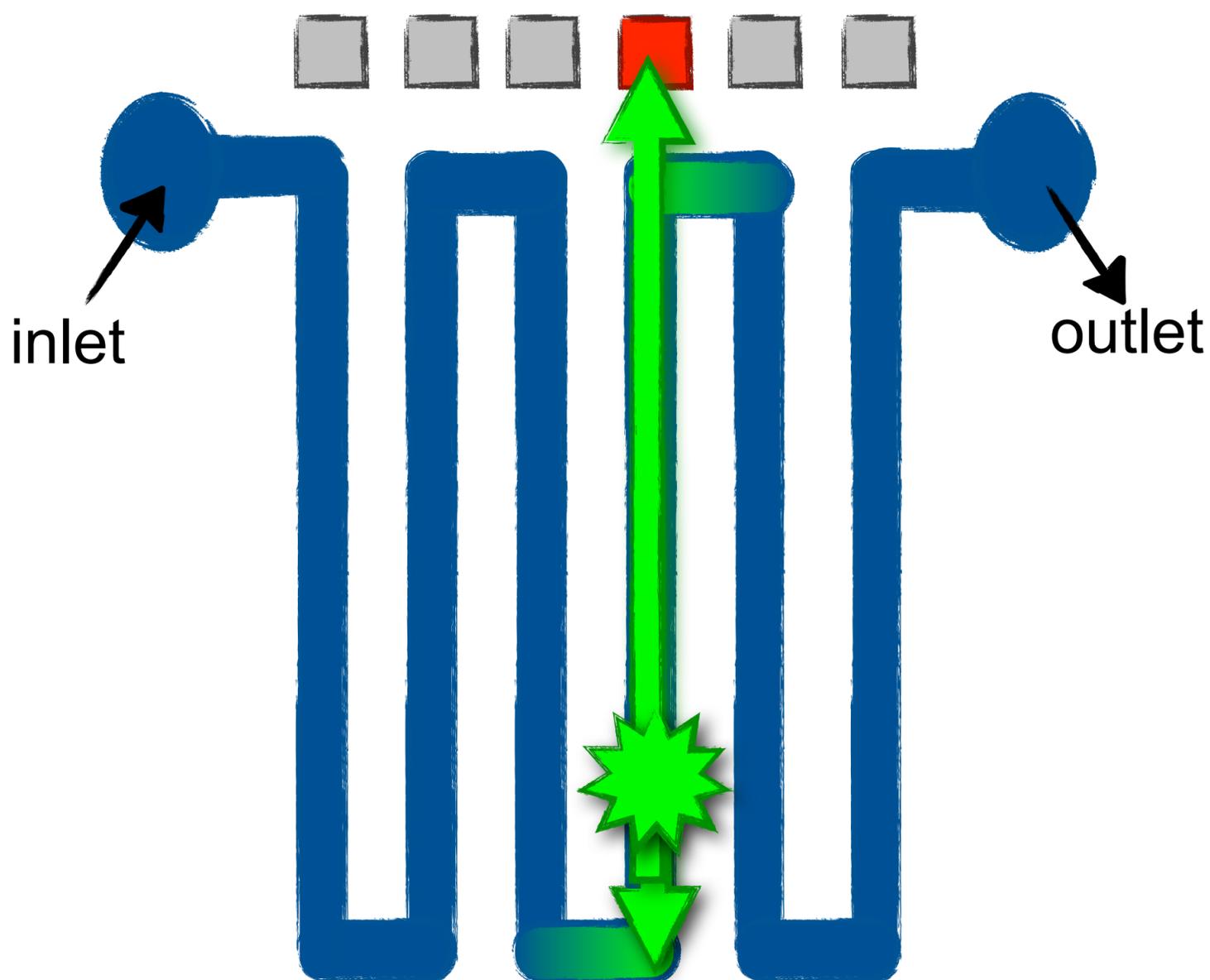
CERN, European Organisation for Nuclear Research, Geneva, Switzerland

- Low-mass cooling solutions. A total power of approximately 500 W will be dissipated in the vertex detectors alone. The small material budget for the inner tracking detectors constrains severely the permitted amount of cooling infrastructure. For the vertex barrel layers, forced air-flow cooling is therefore foreseen. Fig. 6 shows a calculation of the temperature distribution inside the barrel layers of the CLIC_SiD vertex detector in dependence of the air-flow rate. A flow rate of up to 240 liter / s, corresponding to a flow-velocity of 40 km/h, is required to keep the temperatures at an acceptable level. Further R&D is required to demonstrate the feasibility of this air-flow cooling scheme. Possible vibrations arising from the high flow velocities are of particular concern. Supplementary micro-channel cooling [6] or water-based under-pressure cooling may be required in the forward vertex regions;

[6] A. Mapelli et al. Low material budget microfabricated cooling devices for particle detectors and front-end electronics. Nucl. Phys. Proc. Suppl., 215, 2011, pp. 349–352.

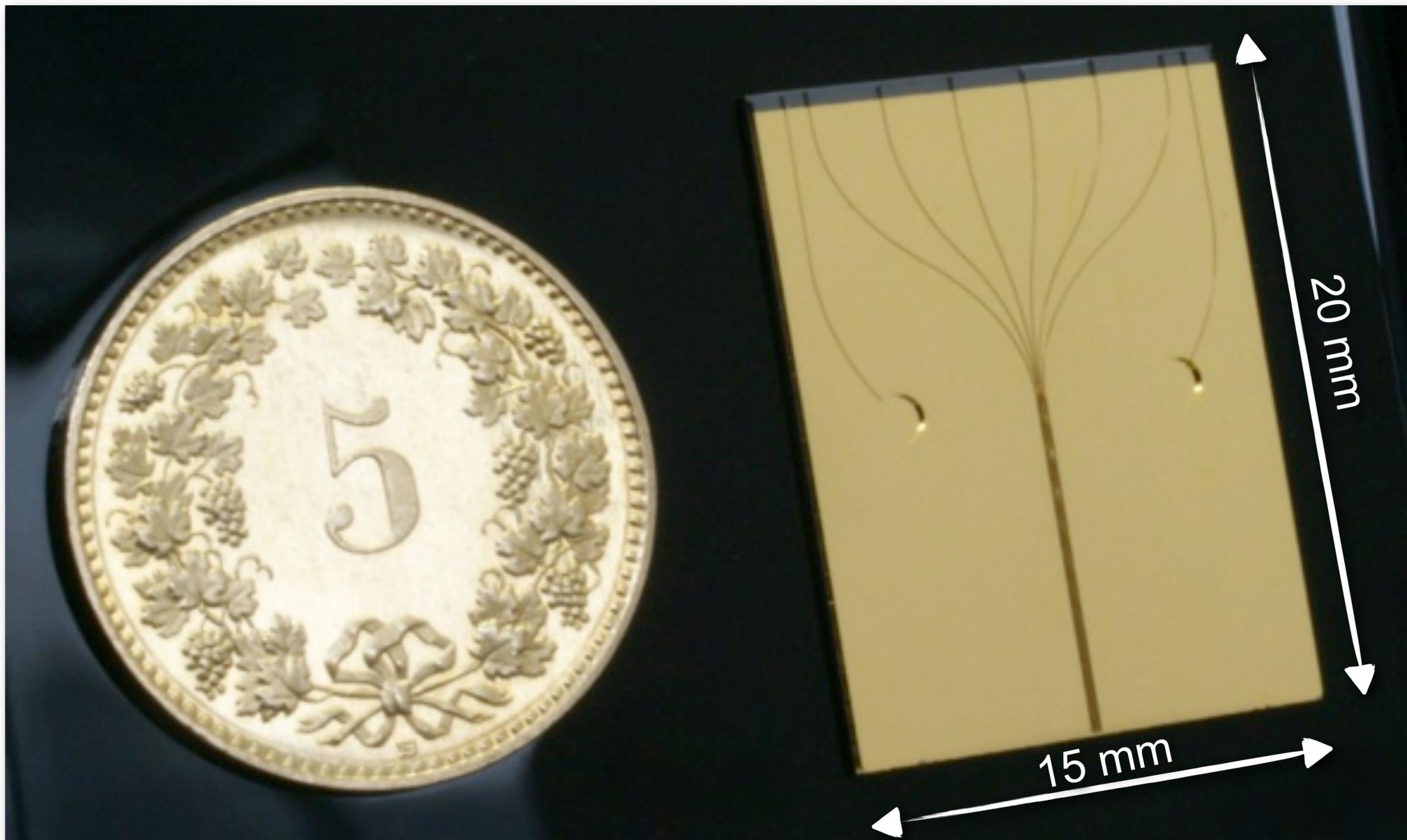
microfluidic scintillation detectors

a single μ -fluidic channel
 defines an array of scintillating
 waveguides



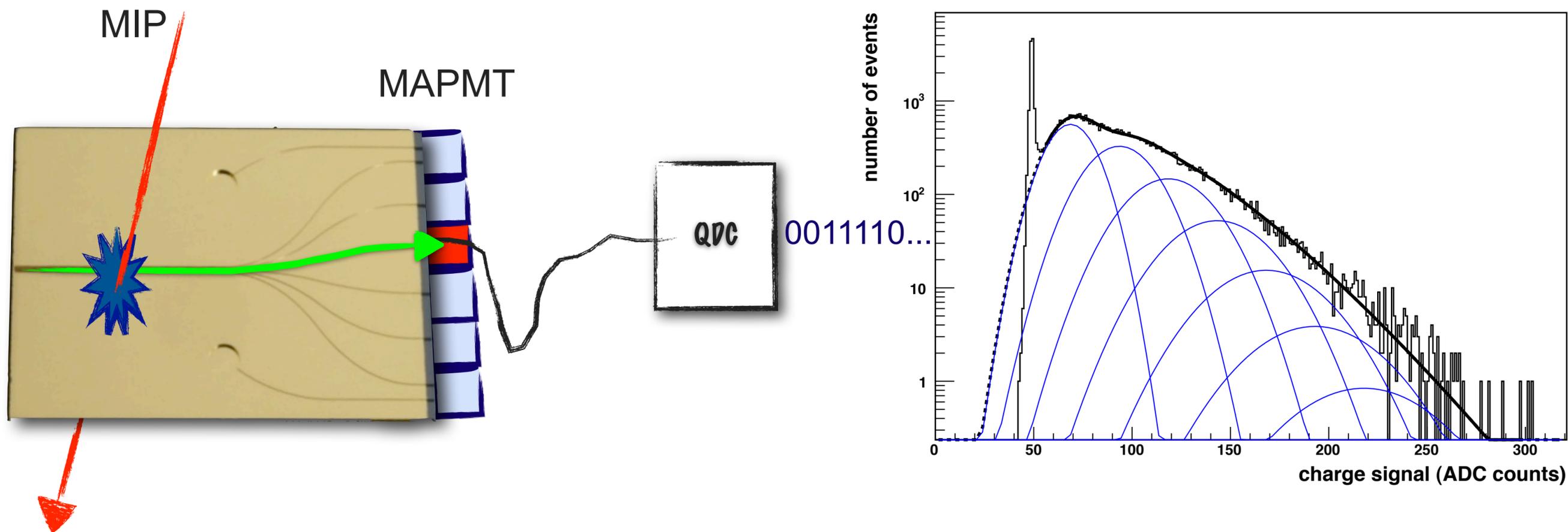
- simple construction
 - standard μ -fabrication processes
- low material budget
 - thin μ -fluidic devices
- high spatial resolution
 - dense arrays of μ -channels
- high radiation resistance
 - liquid scintillator can be circulated and renewed

microfluidic scintillation detector



single photolithography step
200 μm thick micro-channels
50 μm wide channels separated by 10 μm walls

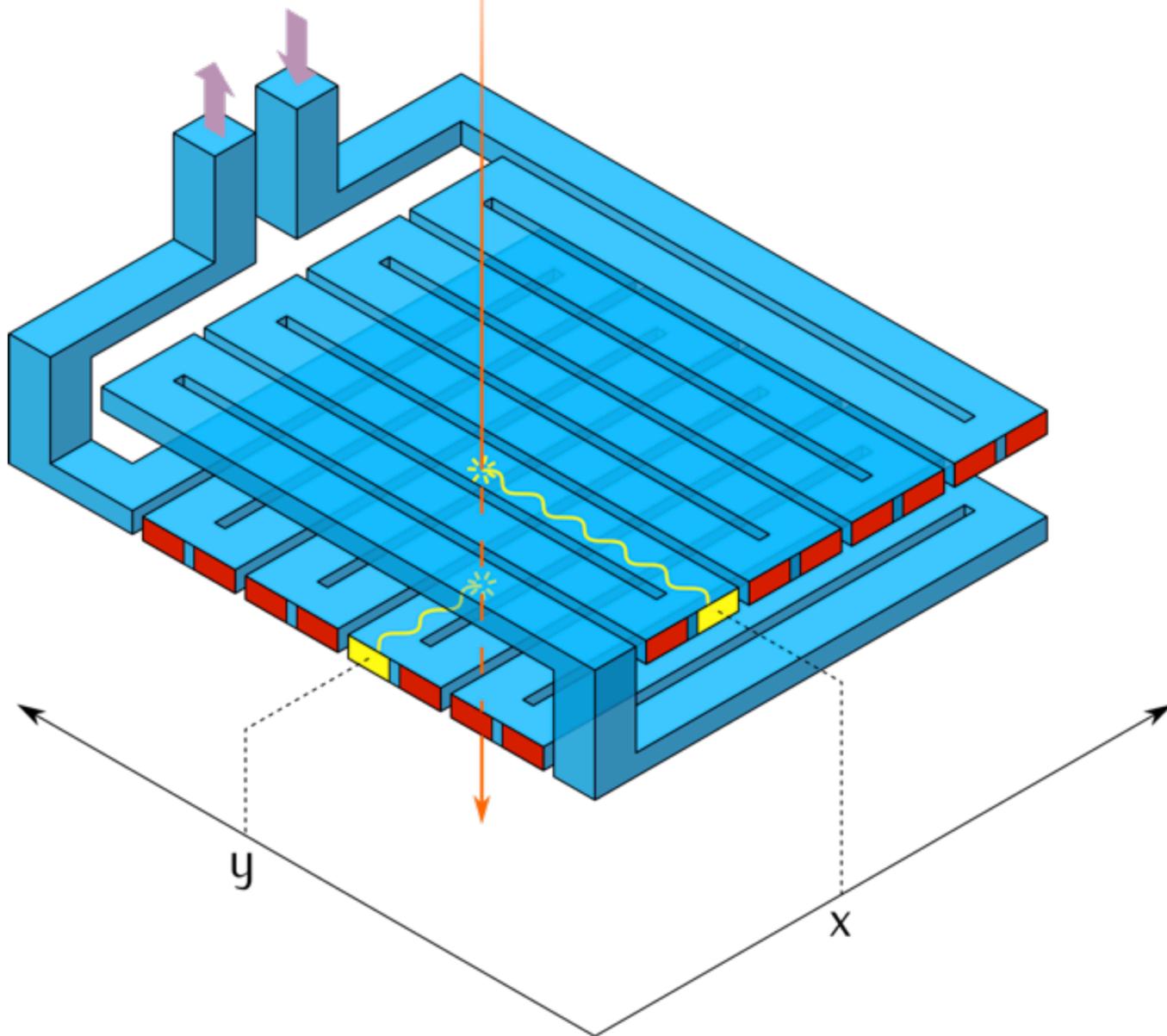
experimental results



light yield = 1.6 pe
 detection efficiency 80%

A. Mapelli *et al.*, *Sens. Act. A* 162 (2010) 272-275

XY.. bi-layer microfluidic device



CERN group

Andrea Catinaccio, Benedetto Gorini, Maurice Haguenaer, Zoe Lawson, Giovanna Lehmann Miotto, Pietro Maoddi, Alessandro Mapelli, Raul Murillo Garcia, Paolo Petagna, Wainer Vandelli

EPFL group

Sébastien Jiguet, Philippe Renaud, Noelia Vico Trivino

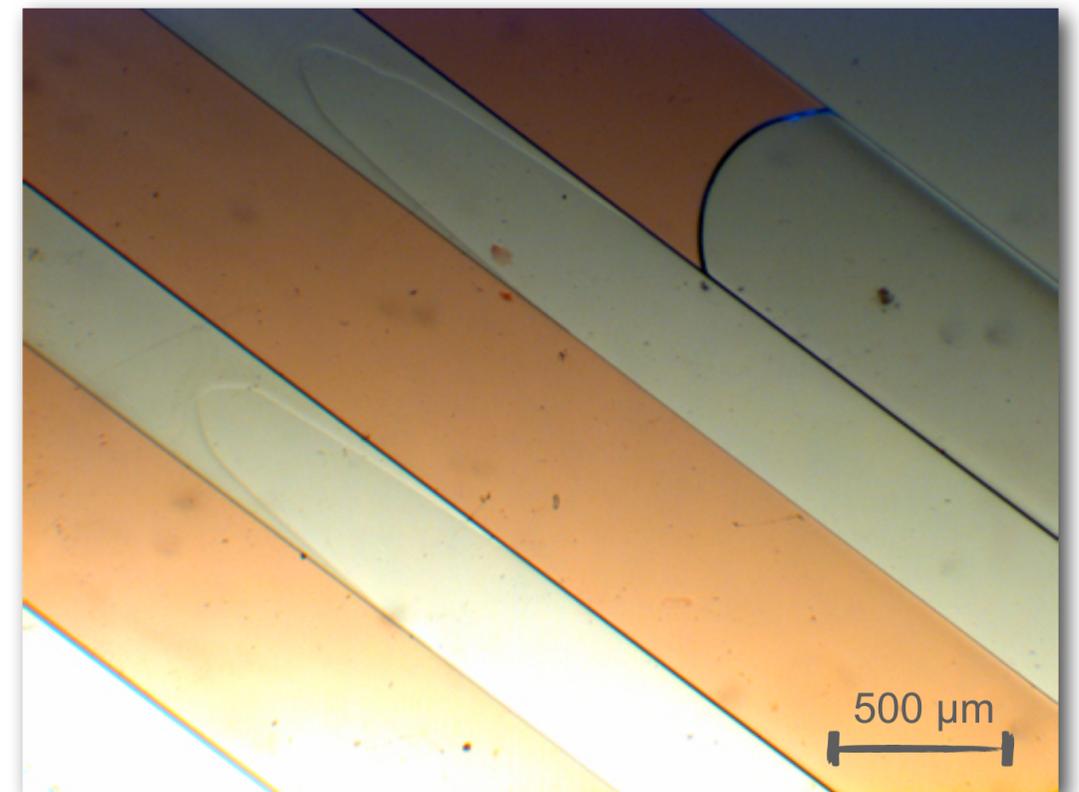
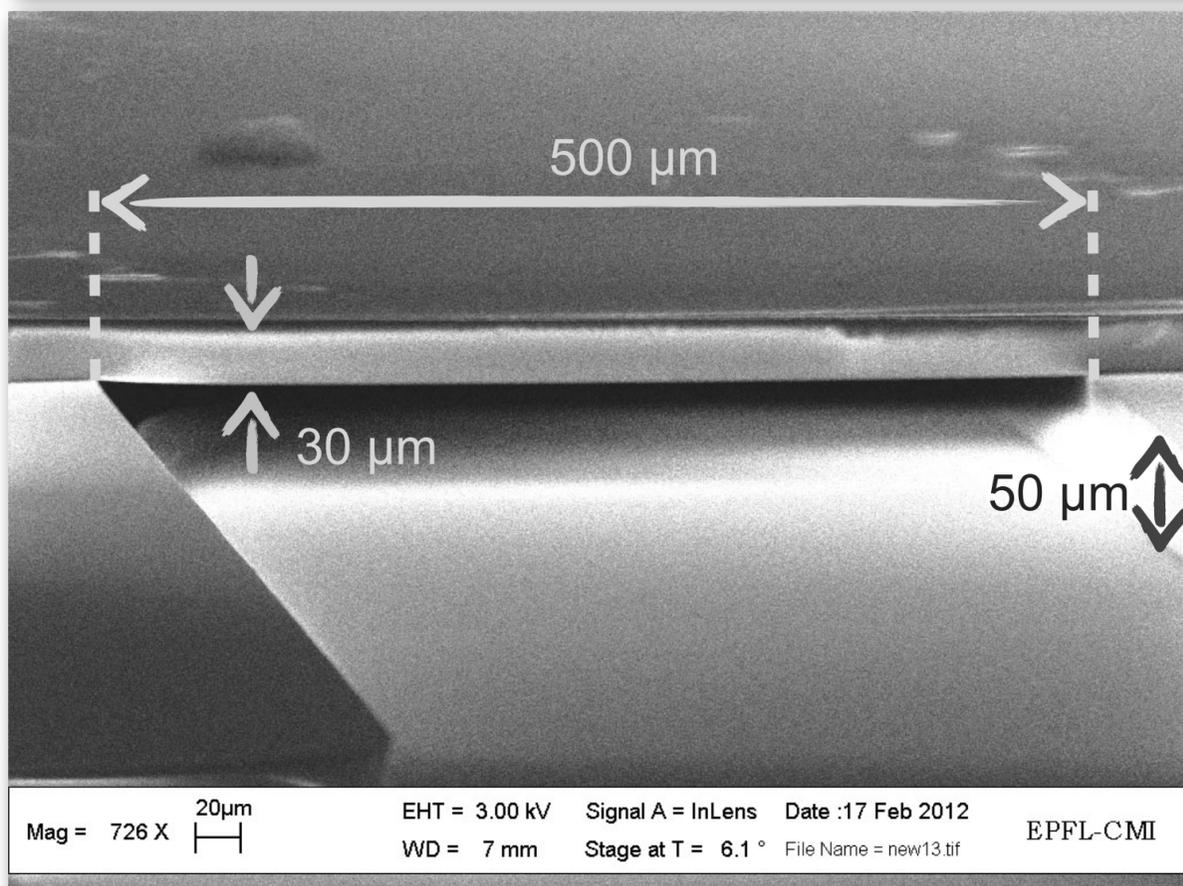
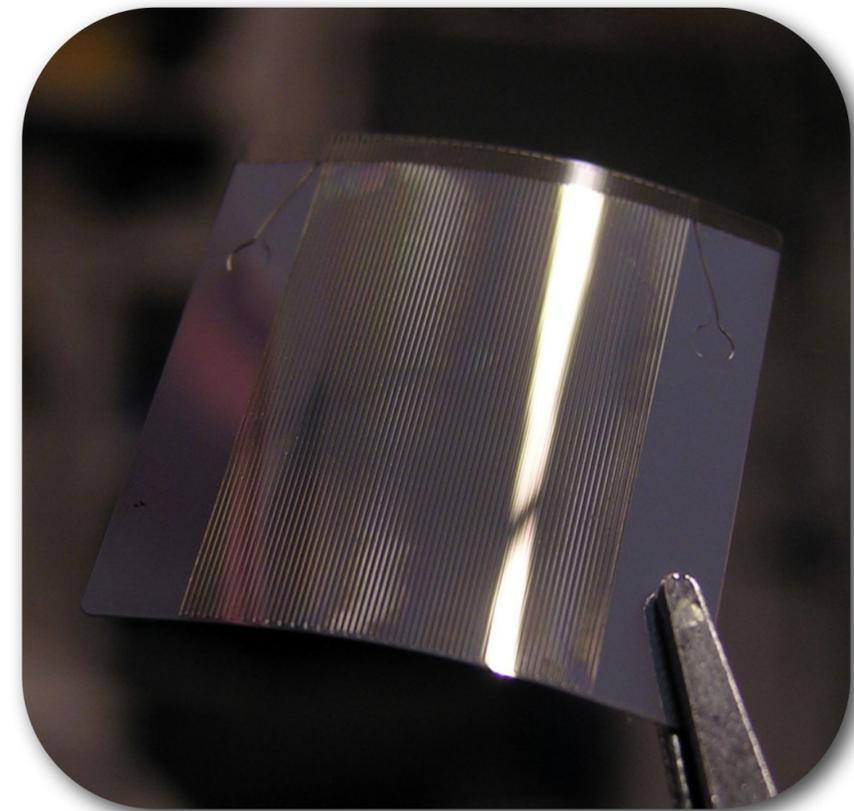
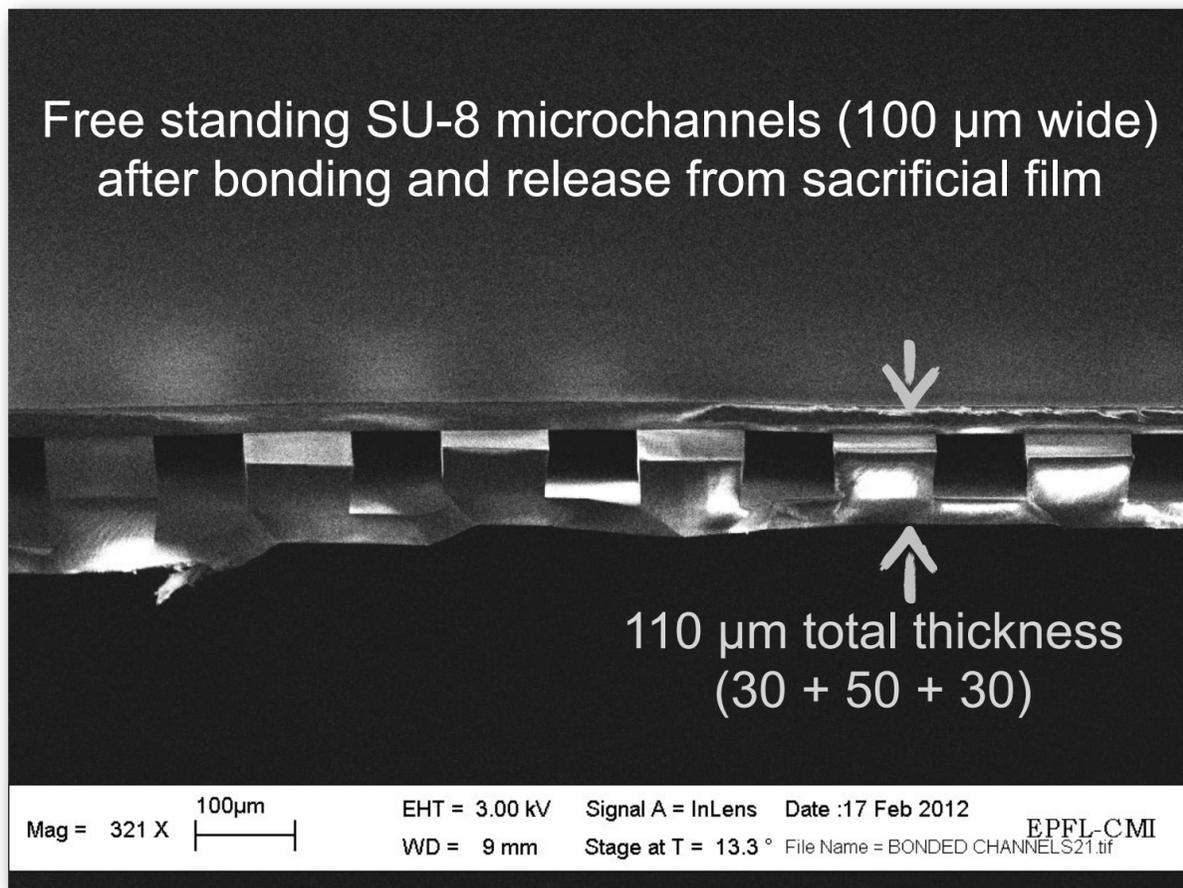
INFN group

Guglielmo Gemignani, Daniele Ruggieri, Francesco Safai-Tehrani, Riccardo Vari, Stefano Veneziano

Under investigation for tracking, calorimetry for **HEP** and online beam monitoring for **hadrontherapy with KT funds**.

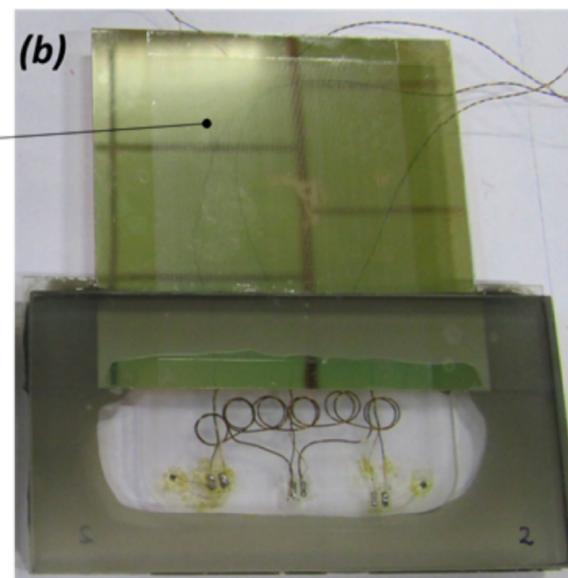
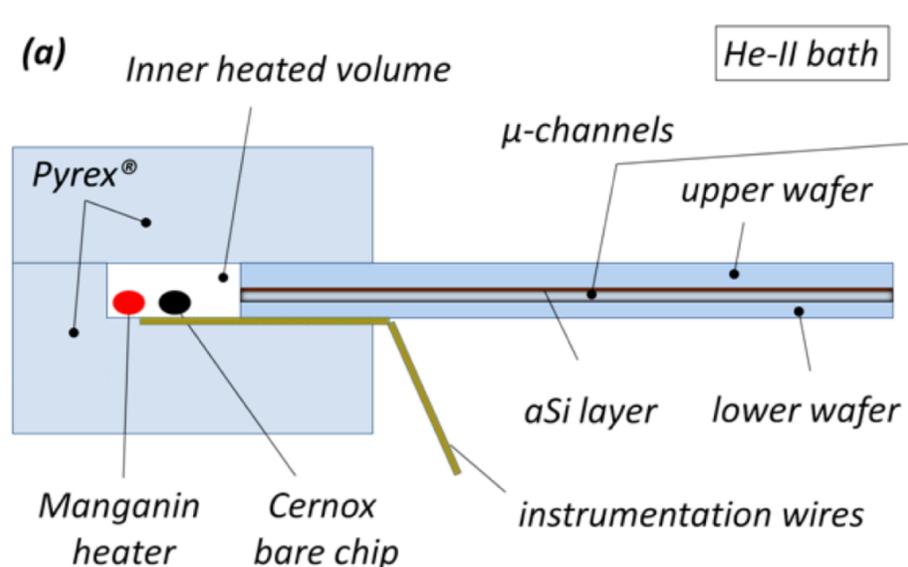
Patent filed May, 8th 2012
PCT/EP2012001980

embedded microchannels

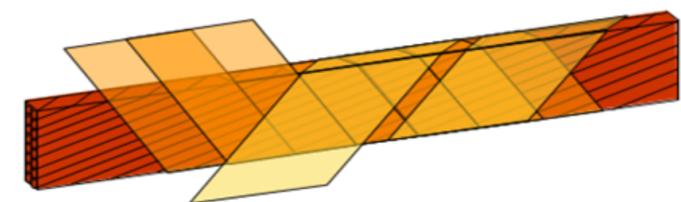


μ HeII, superfluid He in glass microchannels

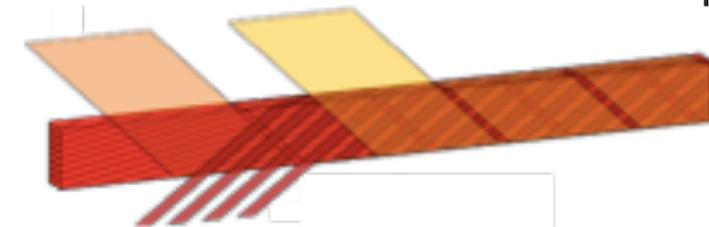
- study the heat transfer of superfluid He in microchannels
- improve the insulation of LHC magnets for upgrade plans.



LHC standard insulation



Enhanced insulation for LHC upgrade



P.P. Granieri, A. Mapelli et al., "Steady-state transfer through micro-channels in pressurized HeII"

Presented at CEC/ICMC 2011

(<http://cdsweb.cern.ch/record/1416393/>)

new field of application

Electrons in semiconductors

+

⇒ Microelectronics

Photons in semiconductors

+

⇒ Optoelectronics

Instrumentation

+

⇒ Micromechanics

Chemistry & biotechnology

+

⇒ Microfluidics

Optics

+

⇒ Micro-optics

Quantum mechanics

+

⇒ Nanotechnology

Robotics/mechatronics

+

⇒ Micromachines

M
I
C
R
O
F
A
B
R
I
C
A
T
I
O
N

HEP

+

⇒ to be defined...

Introduction to microfabrication, S. Franssila, 2004

- Looking closer into microfabrication techniques could lead to
 - integration of services (e.g. cooling in silicon,..)
 - novel particle detectors
 - anticipation of problems and issues in the development phase
 - at the moment, silicon thermo-mechanical mock-ups allow to gain expertise in manipulating and operating thin silicon devices waiting for the real objects to be fabricated by external partners
- At CERN, several projects have been launched in PH-DT in collaboration with various experimental groups
 - micro-channel cooling
 - adopted by NA62 for the GigaTracker
 - experimental results published by LHCb for the VeLo upgrade
 - under consideration by ATLAS, ALICE... and CLIC collider
 - micro-fluidic scintillating detection
 - single particle trackers and calorimeters for HEP
 - beam monitors for hadrontherapy
- At long term, the formation of a centre of competence in microfabrication within the PH Department, with synergies with the existing excellence in microelectronics design and wire-bonding module integration, would crucially advance the development of novel detectors for LHC and future projects.

The Micromegas technology research and development

- Since 1992, at the CEA Saclay and at CERN, the Micromegas technology has been developed in order to obtain more stable, reliable, precise and faster detectors. In 2001, twelve large Micromegas detectors plane of) were used for the first time in a large scale experiment at COMPASS situated on the Super Proton Synchrotron accelerator at CERN. Since 2002 they have been detecting millions of different particles per seconds and still continue today.
- Another example of the development of the Micromegas detectors is the invention of the “bulk” technology. The “**bulk**” technology consists of the integration of the micro-mesh with the printed circuit board (that carries the readout electrodes) in order to build a monolithic detector. Such a detector is very robust and can be produce within an industrial process (a successful try has been conducted with the 3M firm in 2006[5]) allowing public applications. For instance, by modifying the micro-mesh in order to make it photo-sensitive to UV light, the Micromegas can be used to prevent forest fires[6].

http://en.wikipedia.org/wiki/Micromegas_detector



examples of micro-fabricated stuff

Miniature 8" Wafer Disposable Insulin Pump

Small

- Size: 6 mm x 10 mm
- Flow range: up to 5 ml/h
- Stroke Volume: 200 nl, 0.02 U

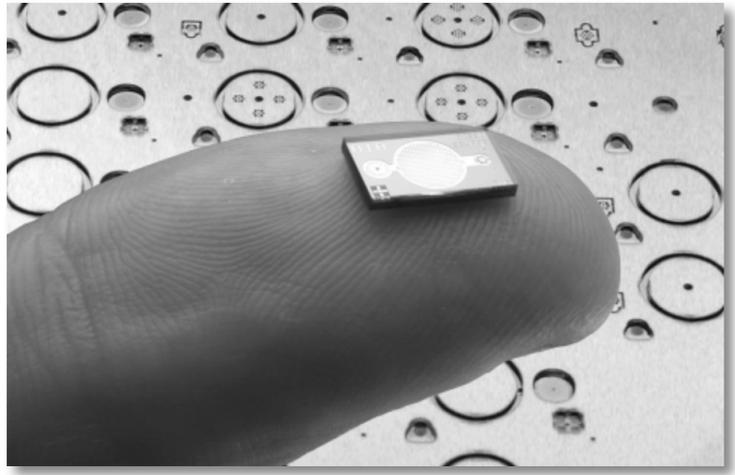
Precise

- Nominal Accuracy $\pm 5\%$
- Reproducibility $\pm 2\%$

Safe

- Built-In failure detection
- Anti Free-flow features

Source: Debiotech



μ -chip pump (6 x 10 mm)

Contact Lens Sensor

Continuous Intraocular Pressure (IOP) Monitoring to aid the diagnosis and treatment of Glaucoma

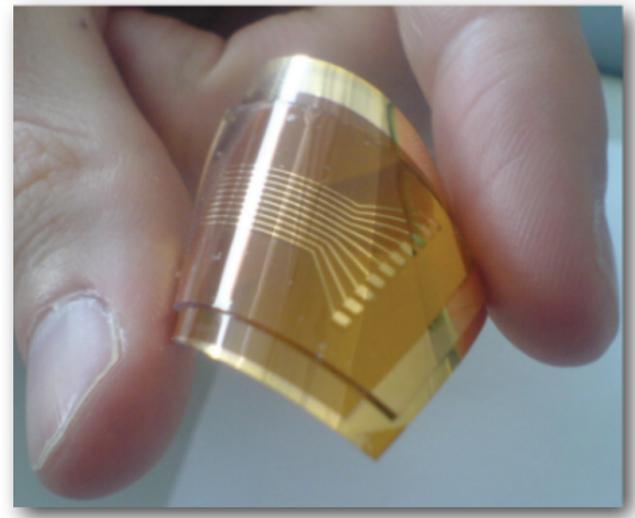
Unmet medical need
Continuous monitoring of IOP

Technology approach
Design and develop a micro system comprising a strain gage and a telemetric microprocessor to be embedded in a soft silicone contact lens of less than 600 μ m thickness

Results
Product patented and CE marked
Extensive clinicals ongoing
Publications in IOVS and Acta Ophthalmologica

Partners
Project initiated at EPFL in the laboratory of Prof. Ph Renaud (LMIS4)

MEMS strain gage MEMS antenna ASIC



Coil-on-a-Chip™ Technology for Magnetic Resonance (MR) Micro-imaging

Technology commercially available

MR-imaging microchip, integrating planar RF microcoils with diameters down to 20 μ m

Very high isotropic resolution, down to 3 x 3 x 3 μ m³

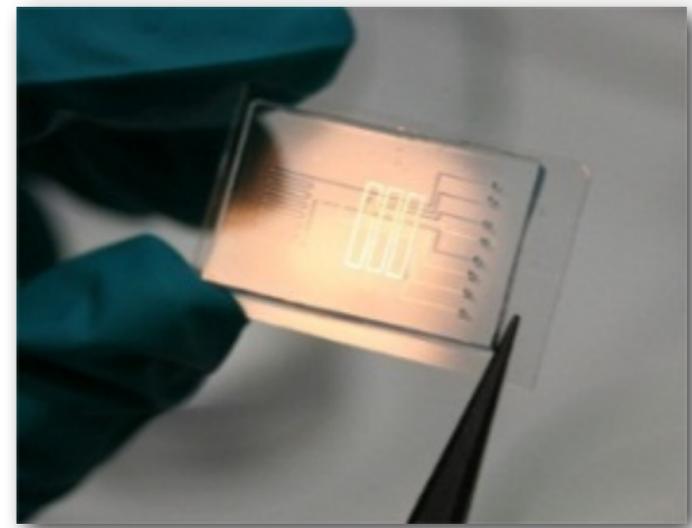
The technology allows MR investigations of submillimeter samples:

**Tissue slices
Animal cells
Mineral samples,
Microstructures, etc.**

3D Model of the microchip (left) and photograph of a 50 μ m (ID) planar micromachined coil (right)

(A) Histology of a rat spinal cord tissue slice. Alpha motor neurons (dark red, ~50 μ m Diameter) and their nuclei (yellow)

(B) State of the art MR-Image of the same tissue slice. Resolution: 7.8 μ m in-plane. Flint, J.J., et al., Magnetic resonance microscopy of mammalian neurons, NeuroImage, 46 (4), 1037-1040 (2009).



Micromirrors & Microprojectors

lemoptix

Characteristics:

- High Brightness
- Ultra-Miniature
- Always in Focus
- Energy Efficient
- Low Cost
- High Resolution
- Vibrant Colors

Wafer

Micro Projector

MEMS Scanning Mirror

Plug-and-play microprojector module From Q1 2011

On the market since 2009

Mimotec SA: Micropièces pour grandes idées

Technologie UV-LIGA (Lithographie, Galvanisation und Abformung)

- Grande liberté de design
- Etat de surface polie
- Idéal du prototype à la série
- Précision élevée (+/- 2 μ m)
- Microstructure $\geq 5\mu$ m
- Coûts concurrentiels

Domaines d'applications

- Micromoule
- Micropièce

Mimotec
Micropièces pour grandes idées

News MEMS Around the Body

Disposable Insulin Pump

MEMS Pressure Sensors on Flexible Plastic Substrate close to Eyes for Glaucoma Detection

24-hour disposable contact lens with pressure sensor – ST and Sensimed

Insulin pump system

Intraocular pressure

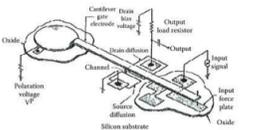
MEMS node

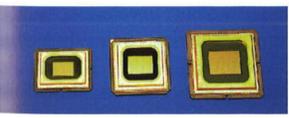
Movement recognition

Body Gateway

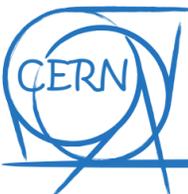
Source: Debiotech, www.jewelump.com

microfabrication milestones

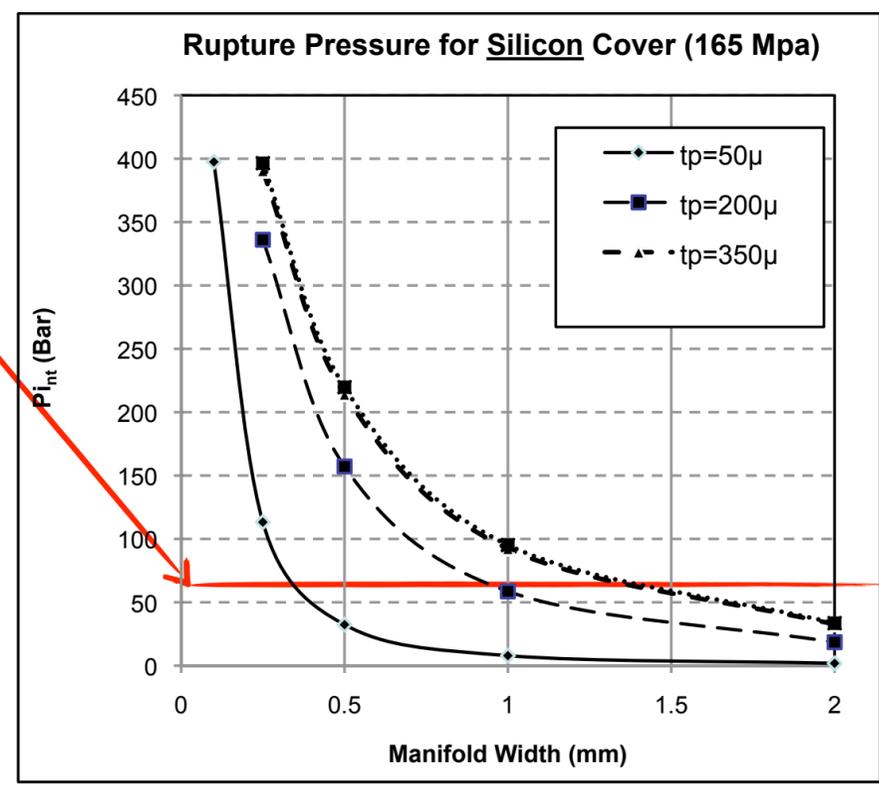
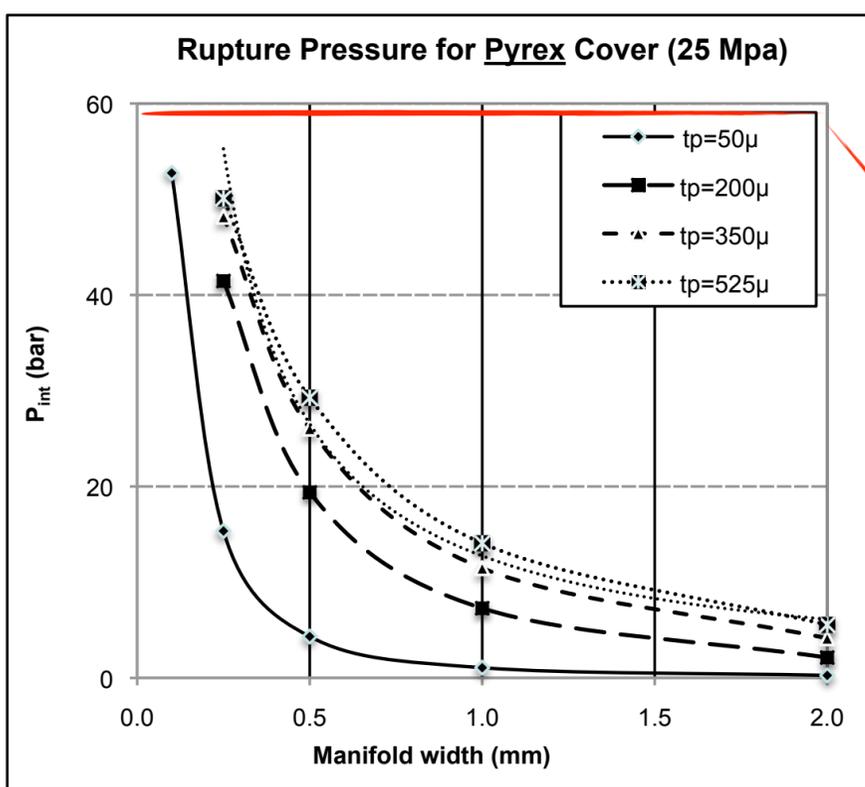
Year	Fact
1824	Berzelius discovers Si
1910	First patent on the MOS transistor concept
1927	Field effect transistor patented (Lilienfeld)
1939	First pn junction transistor (J. Bardeen, W.H. Brattain, W. Shockley)
1947 (23 December)	Invention of the transistor made from germanium at Bell Telephone Laboratories
	
1954	Evidence of piezoresistive effect in Si and Ge by Smith ⁹
1956	An early milestone for the use of single-crystal silicon in MEMS was the discovery of porous Si by Uhlir ⁸
1958	Jack Kilby of Texas Instruments invents the IC, using GE devices. A patent was issued to Kilby in 1959. A few months later, Robert Noyce of Fairchild Semiconductor announced the development of a planar Si IC
	
1960s IC (1st Monolithic BJT IC, 4BJT)	
1958	Silicon strain gauges commercially available
1958	First IC (oscillator)
1959	R. Feynman famous talk: "There's Plenty of Room at the Bottom" ⁷
1961	Fabrication of the first piezoresistive sensor, pressure (Kulite)
1967	Anisotropic deep silicon etching (H.A. Waggener ¹²)
1967	First surface micromachining process (H. Nathanson ²⁸): resonant gate before it was called MEMS
	
1969-1970	Anodic bonding of glass to Si ¹³
1972	National Semiconductor: commercialize a Si MEMS pressure sensor
1975	Gas chromatograph on a Si wafer by S.C. Terry, J.H. Jerman, and J.B. Angell at Stanford University ²³
1977	First capacitive pressure sensor (Stanford) ¹⁶
1977	IBM-HP: micromachined ink-jet nozzle ²⁴
	
1980	K.E. Petersen, silicon torsional scanning mirror ²⁴

Year	Fact
1982	Review paper "Silicon as a mechanical material" published by K.E. Petersen ²⁵
1982	Disposable blood pressure transducer (Foxboro/ICT, Honeywell, \$40)
1982	The use of x-ray lithography in combination with electroplating and molding (or LIGA), introduced by Ehrfeld and his colleagues ²⁹
1983	Integrated pressure sensor (Honeywell)
1983	"First" polysilicon MEMS device (Howe, Muller UCB ²⁶); see also Nathanson in 1967 ²⁸
1986	Silicon to silicon wafer bonding (M. Shimbo ¹⁴)
1987	Texas Instrument's Larry Hornbeck invents the digital micromirror devices (DMDs)
1988	Rotary electrostatic side drive motors (Fan, Tai, Muller ³⁰) Electrostatic micromotor (UC-Berkeley BSAC)
1988	First MEMS conference (first transducers conference held in 1987)
1989	Lateral comb drive (Tang, Nguyen, Howe ³¹)
	
1990	The concept of miniaturized total chemical analysis system or μ -TAS is introduced by Manz et al. ³² This may be seen as the beginning of BIOMEMS
1992	Grating light modulator (Solgaard, Sandejas, Bloom)
1992	First MUMPS process (MCNC) (with support of DARPA). Now owned by MEMSCAP
1992	First MEMS CAD tools: MIT, S.D. Senturia, MEMCAD 1.0 Michigan, Selden Crary, CAEMEMS 1.0
1992	Single-crystal reactive etching and metallization (SCREAM) developed at Process (Cornell)
1993	Analog devices: commercialize multi-axis accelerometer integrating electronics (ADXL50)
1995	Intellisense Inc. introduces MEMS CAD IntelliSuite. MEMCAD 2.0 is launched, and ISE introduces SOLIDIS and ICMAT
1996	The first digital mirror device (DMD)-based products (Texas Instruments) appear on the market
	
TI's VGA (640 x 480), the SVGA (800 x 600), and the XGA (1024 x 768)	
1996	DRIE (Bosch Process)
1997	Printing meets lithography when George M. Whitesides et al. at Harvard discover soft lithography ²⁷
1998	First PCR-microchips
1998	Sandia's ultraplanar multilevel technology SUMMIT-IV and -V technologies. Four- and five-level poly-Si processes

Year	Fact
1999	DNA microarray techniques
	
Affymetrix genechip	
1999	Electrokinetic platforms (Caliper, Aclara, and Agilent)
2000	Nortel buys Xros for \$3.25 billion
2002	The telecom recession puts many things on standby
	
Lucent 3D optical switch	
2004	MEMS rebuilds. First application of accelerometer in consumer electronics (CE) to hard drive protection in notebooks. IBM puts dual-axis accelerometer in the notebook (now Lenovo)
2006	Sony (PS3) and Nintendo (Wii) introduce motion-based game controllers
2007	Apple announces the iPhone with motion-based features



structural resistance Pyrex and Si



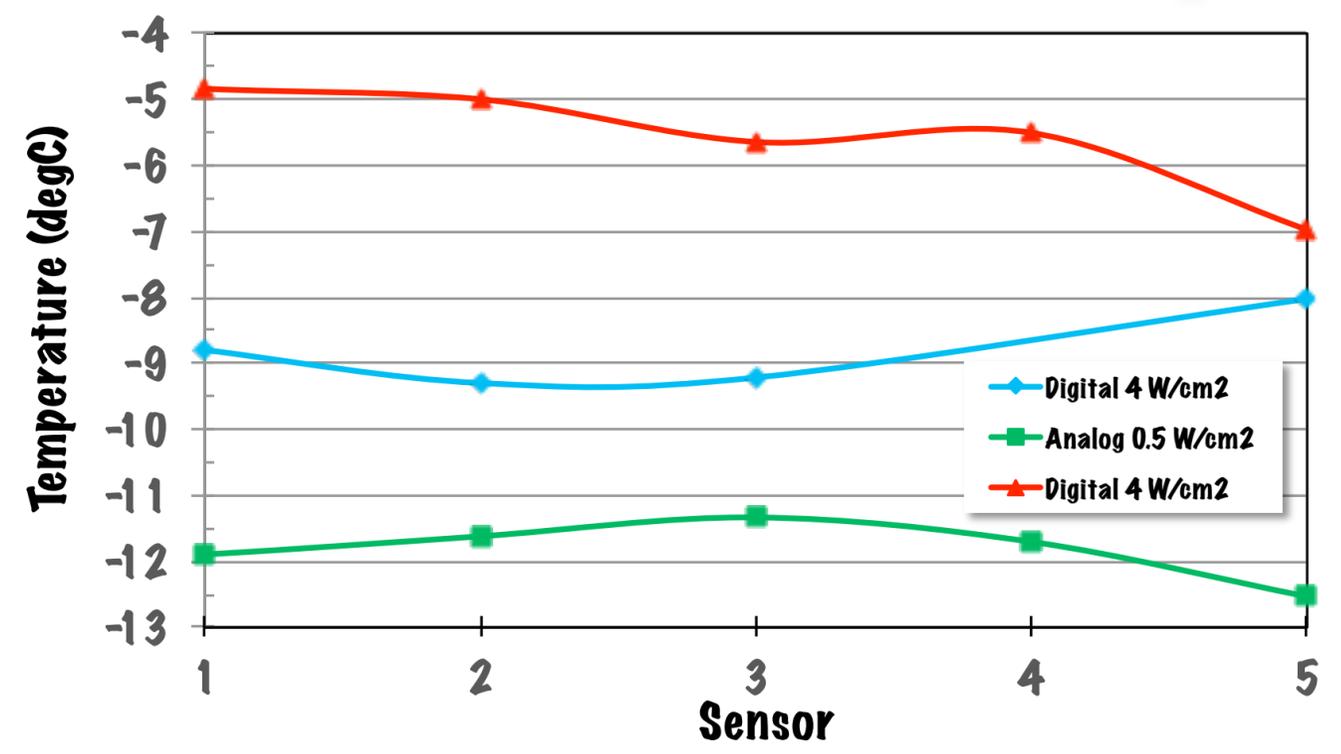
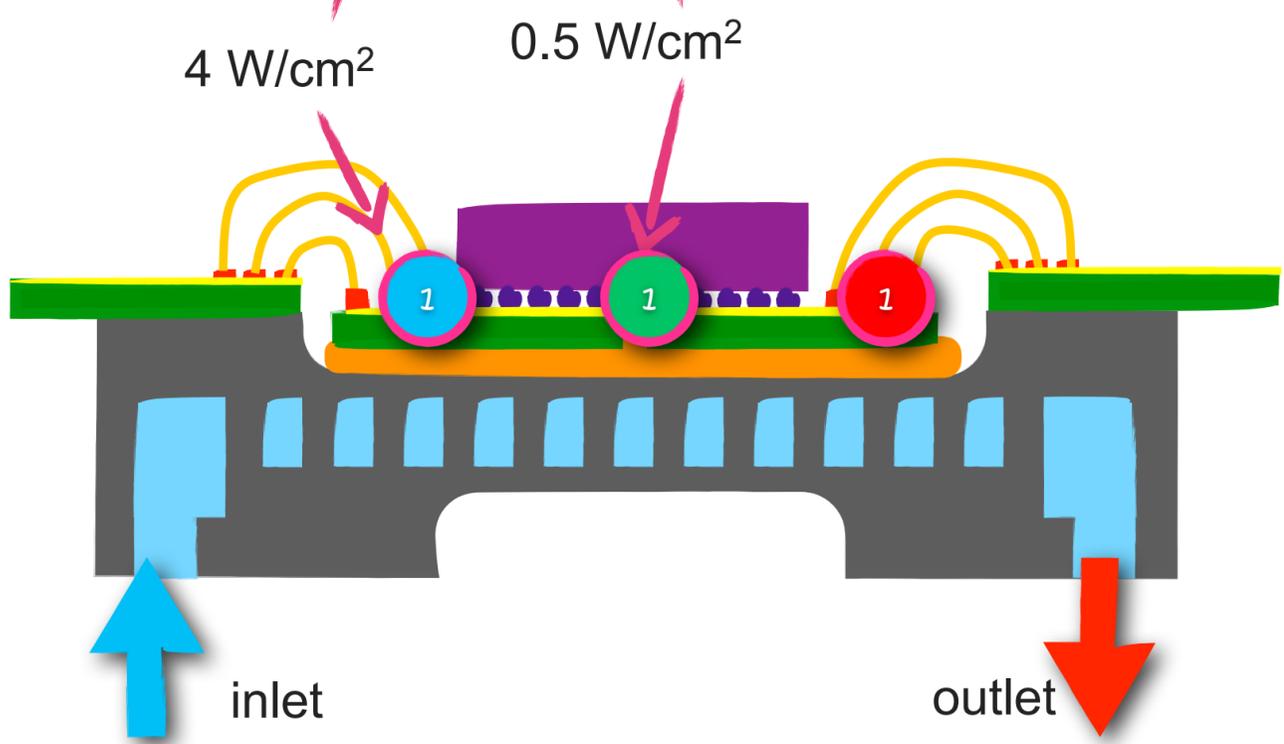
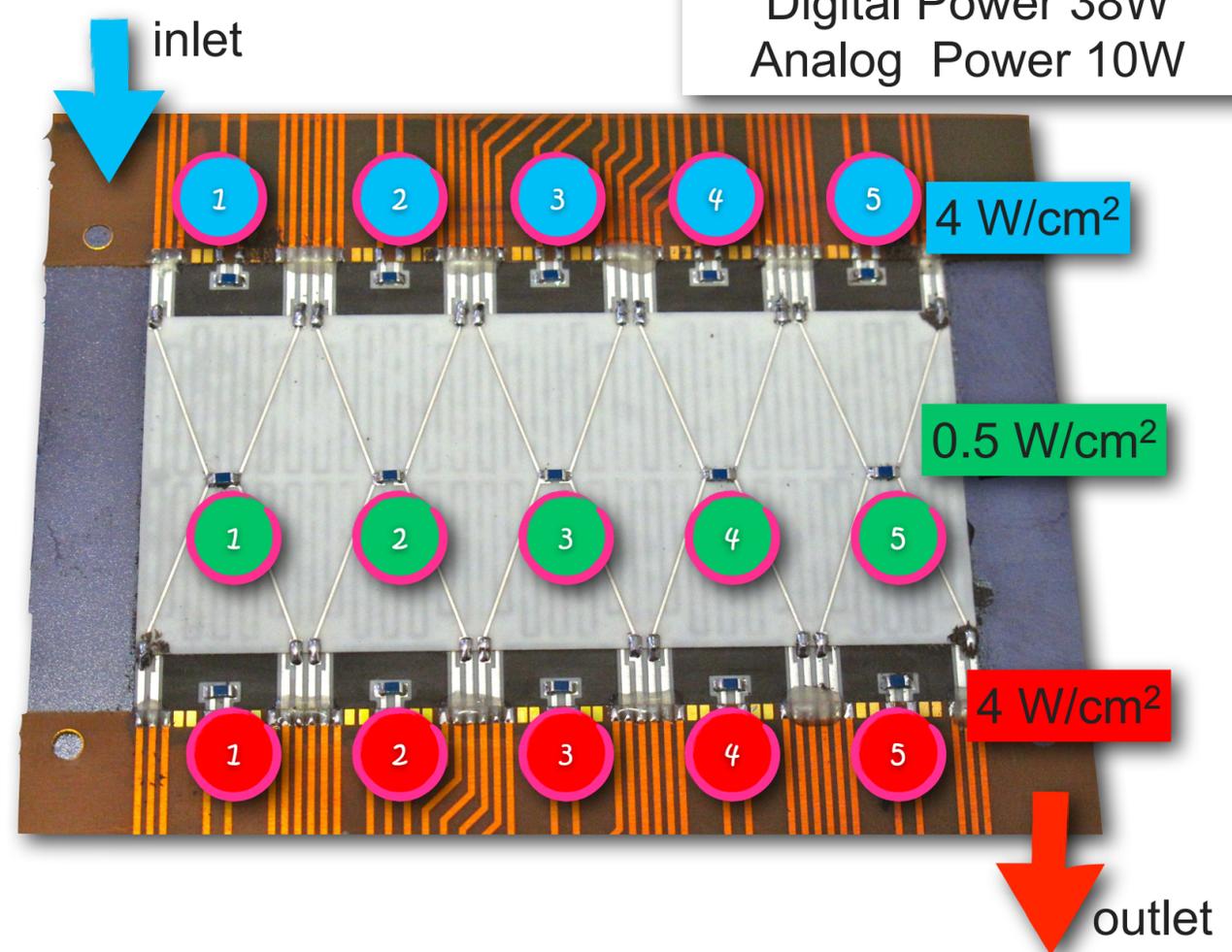
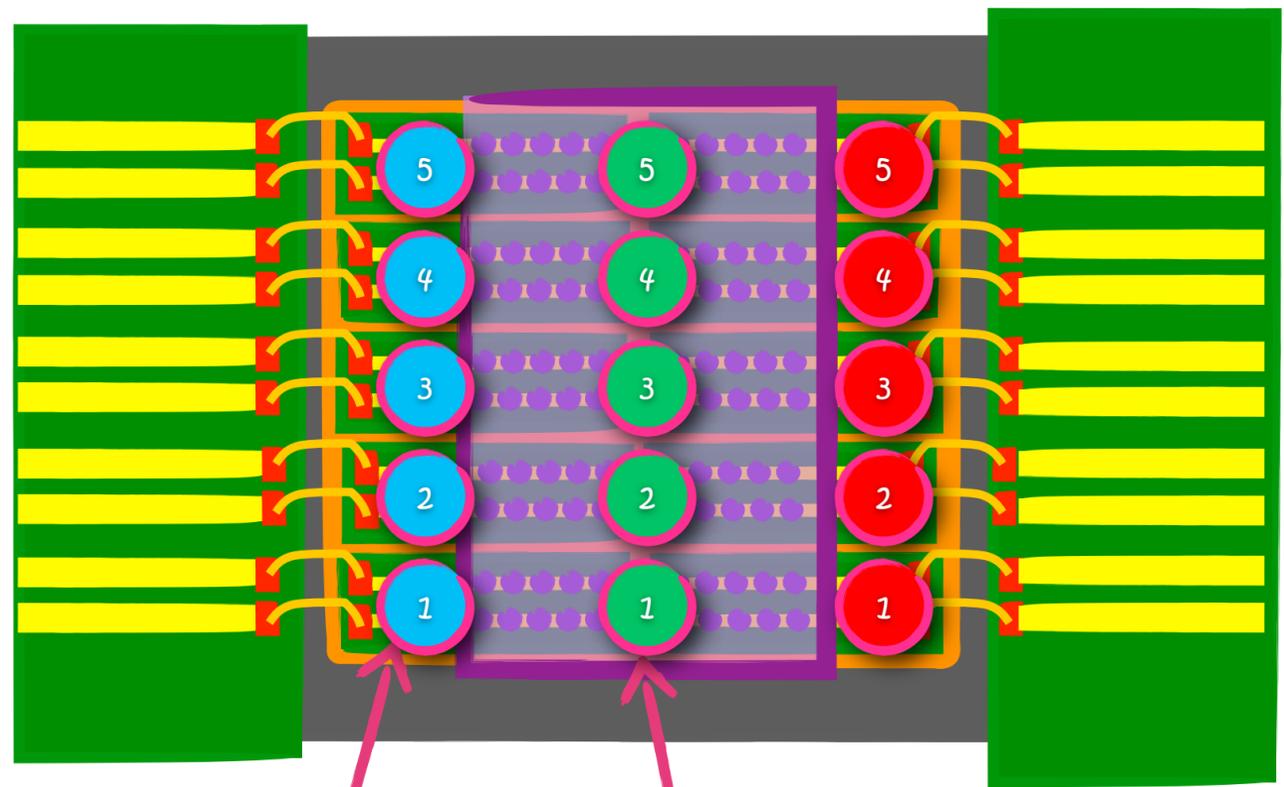
what is micro-fabrication?

- same technologies used in micro-electronics but for new applications
 - micro-electronics
 - opto-electronics
 - light emission devices, light detectors, light transmission
 - Micro-optics
 - movable mirrors (e.g. TEXAS INSTRUMENTS PROJECTORS)
 - integrated waveguides
 - Micro-fluidics
 - micro-channels (e.g. LAB-ON-CHIP)
 - micro-pumps (e.g. DRUG DELIVERY, INKJET PRINTER NOZZLES)
 - MEMS: Micro-Electro-Mechanical Systems
 - micro-mechanics (Pressure sensors, resonators, gyroscopes, switches,...), micro-machines, micro-sensors, actuators
 - micro-accelerators (e.g. CAR AIR-BAGS)
 - Nanotechnology
 - AFM tips, nano-electronics, bottom-up approach
 - ...
- Typical dimensions
 - around $1\ \mu\text{m}$ in the plane of the wafer (from $0.1\ \mu\text{m}$ to $100\ \mu\text{m}$)
 - vertical dimensions from atomic-layers (0.1nm) to hundreds of micrometres
- processes can be transferred out of cleanroom environment

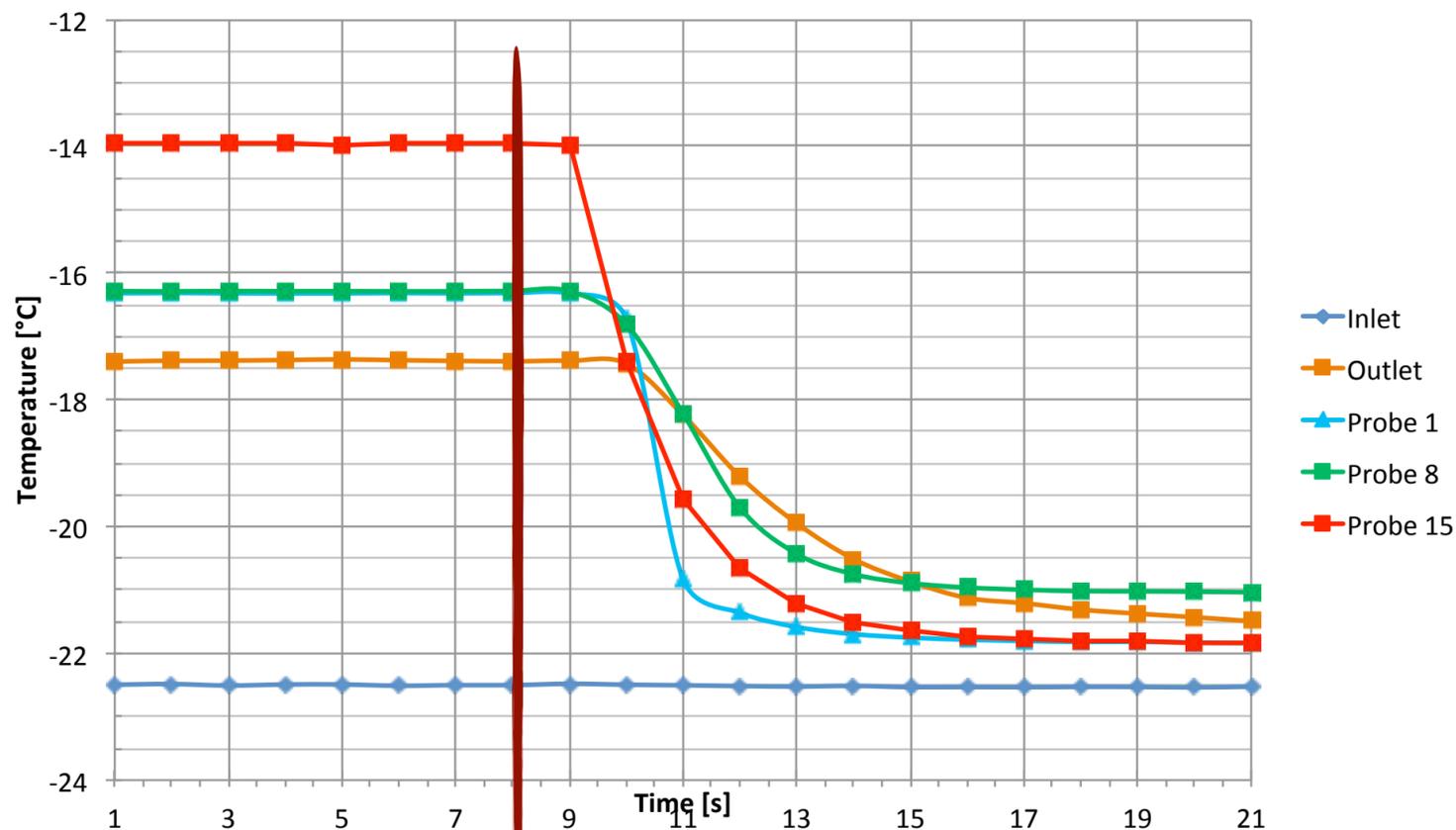
- **Miniaturization techniques are**
 - top-down methods, in which one builds down from the large to the small, and
 - bottom-up methods, in which one builds up from the small to the large.
- **Micromachining, also microfabrication, micromanufacturing, or micro electromechanical systems (MEMS) refers to the fabrication of devices with at least some of their dimensions in the micrometer range.**
- **In the early years, this discipline was almost exclusively based on thin and thick film processes and materials borrowed from IC fabrication labs.**
- **Although the term MEMS is still very popular, a much more apt description today for microfabrication and the other techniques described below is miniaturization engineering, a discipline based on a thorough knowledge and understanding of intended applications, different micromanufacturing options, the behavior of materials, and scaling laws. The latter describes the laws that express how structures scale when all their dimensions are isomorphically reduced.**
- **MEMS: MicroElectroMechanical Systems (US)**
- **MST: MicroSystems Technology (Europe)**
- **Micromachining (Japan)**
- **Microengineering (UK)**

NA62 thin Si cooling plate

C₆F₁₄: 7g/s, -19°C at inlet
 Digital Power 38W
 Analog Power 10W



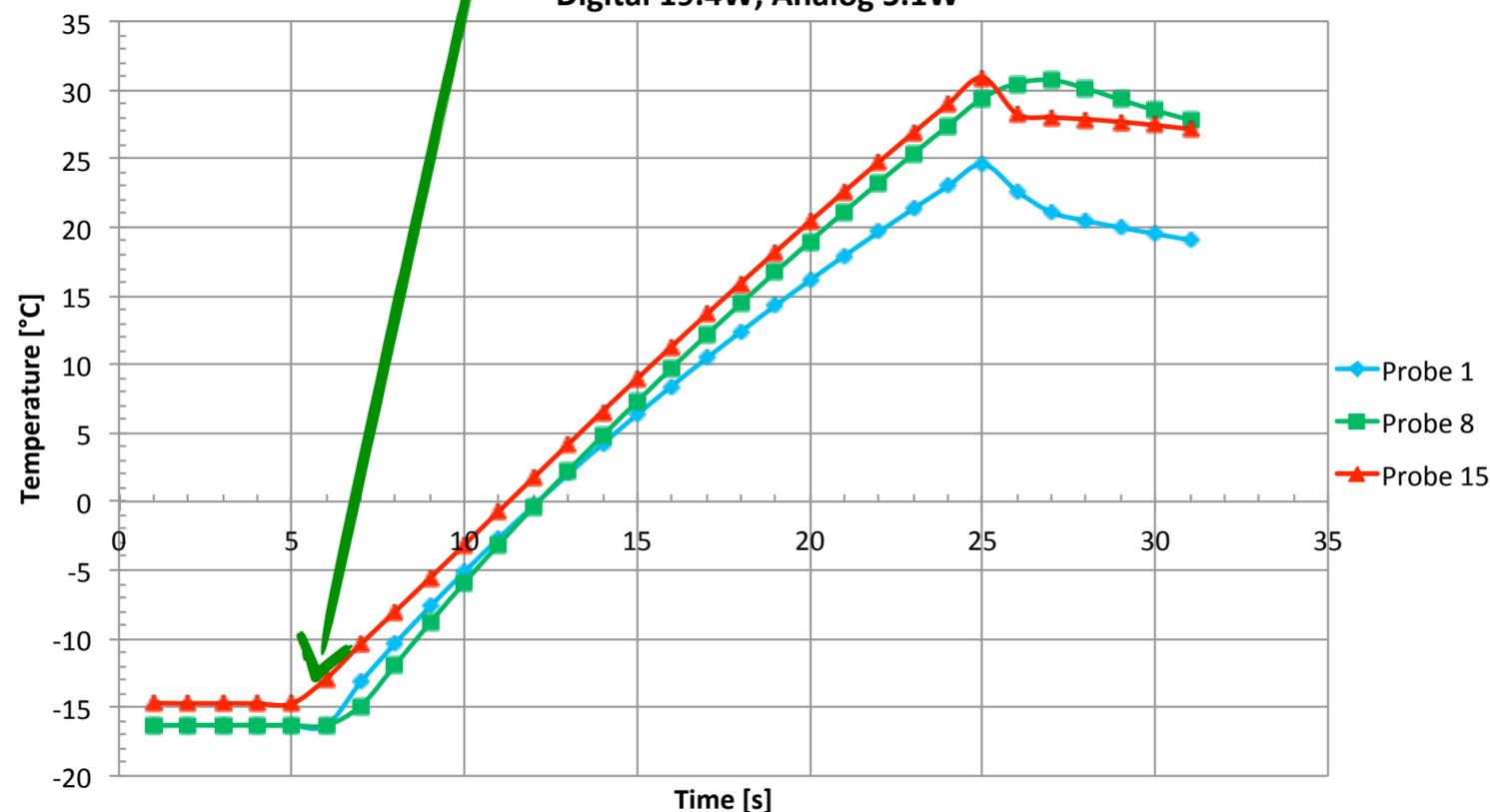
5gm/s, -22°C Inlet, Digital 19.4W, Analog 5.1W



Power Failure
Temperature stabilizes in 8 s

Hydraulic Failure
Temperature rises at 2.3°C/s

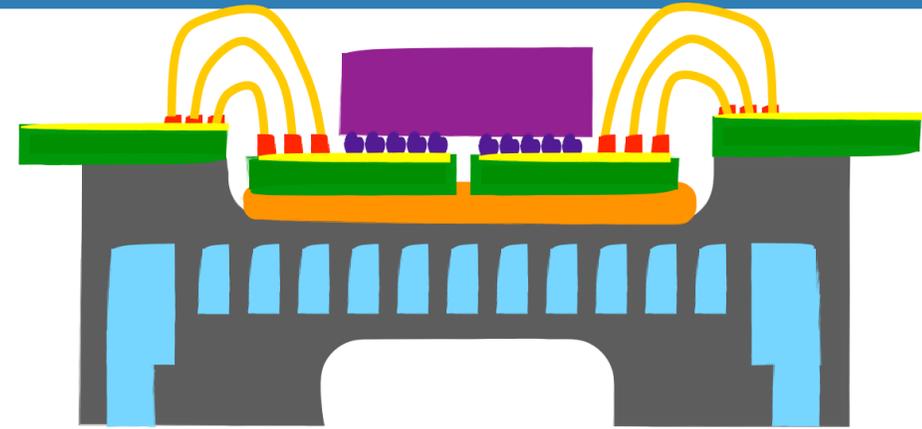
Hydraulic Failure: 5gm/s, -22°C Inlet
Digital 19.4W, Analog 5.1W



towards integrated micro-cooling

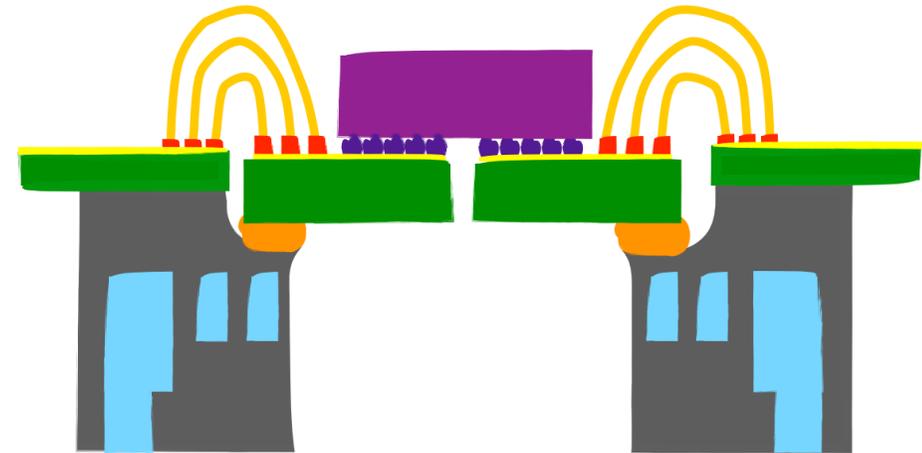
1. thin silicon cooling plate

NA62
LHCb



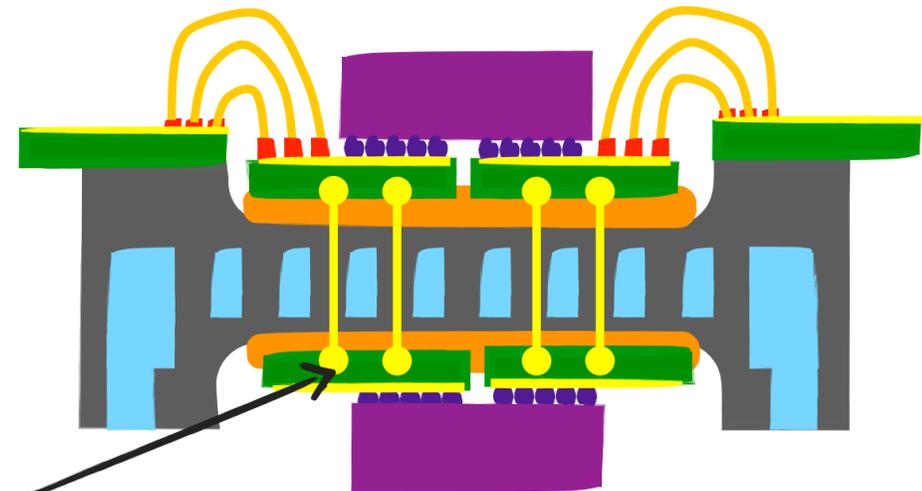
2. silicon cooling frame

NA62
ALICE



3. silicon cooling plate with TSVs

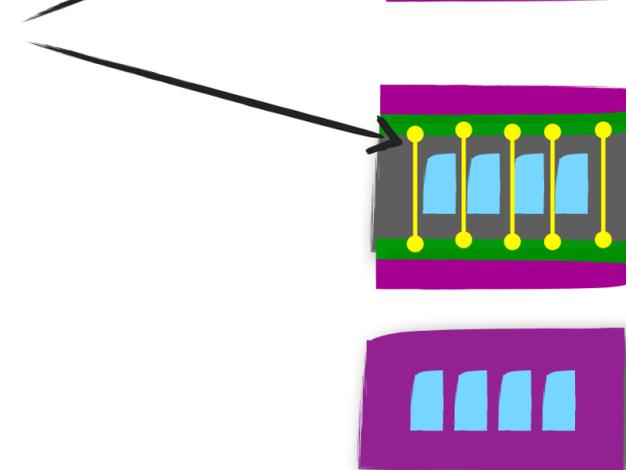
3D architectures
project will start in Sept. 2012

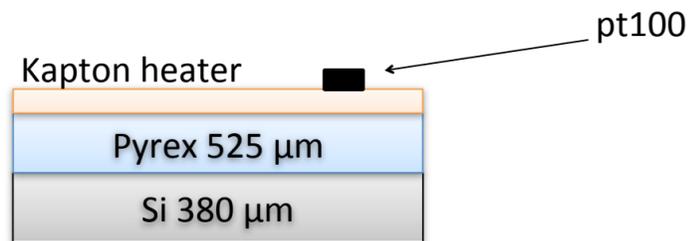


TSV: Through Silicon Via

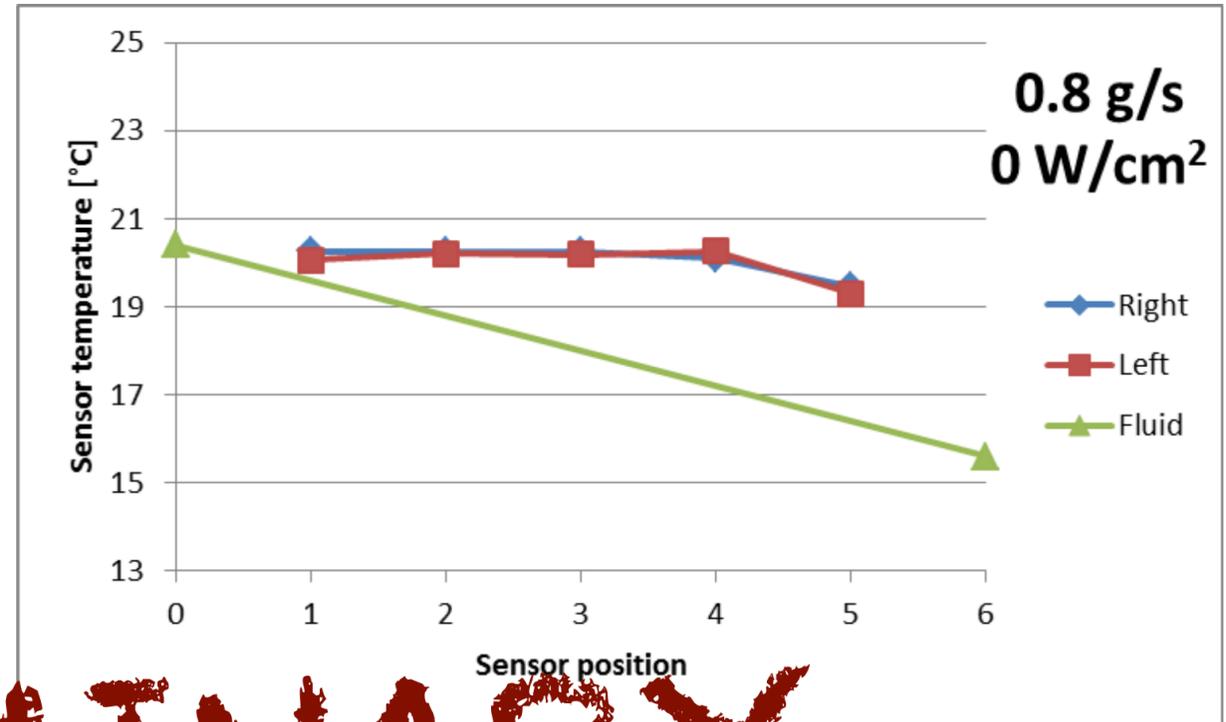
... integration of the μ -channels

in-plane connectivity
in the bulk of the Si detector
in the read-out chips

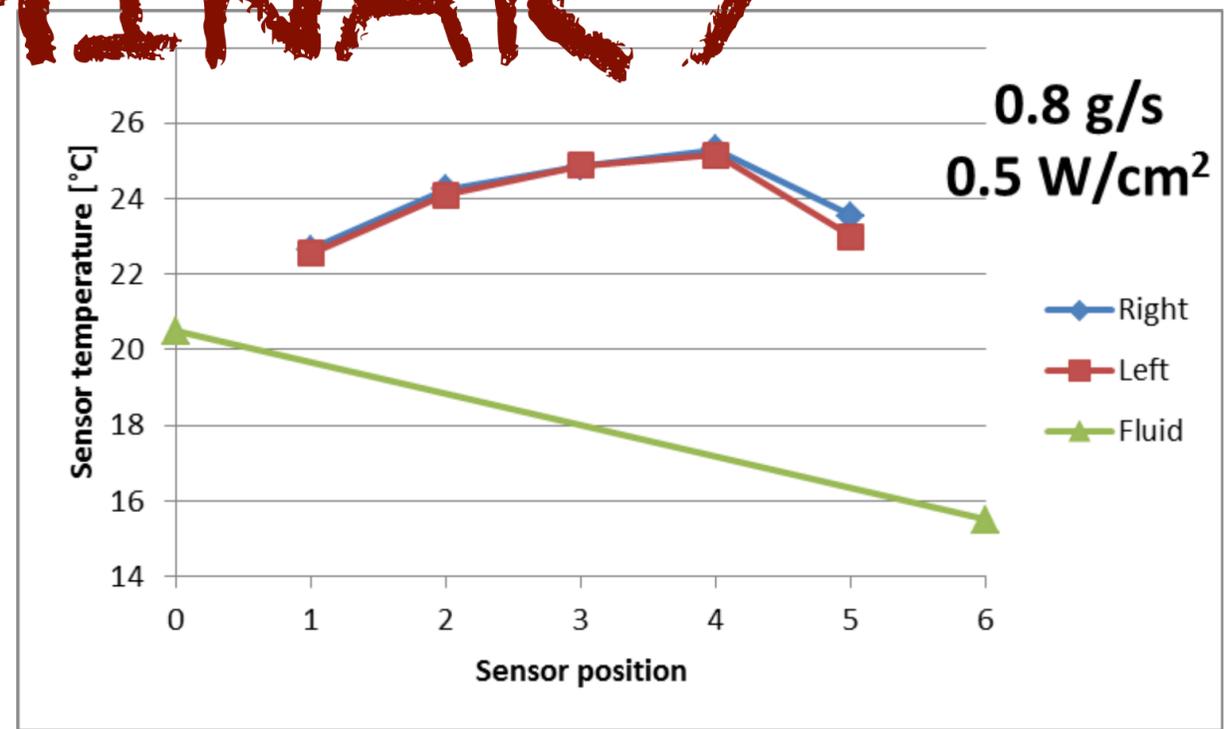
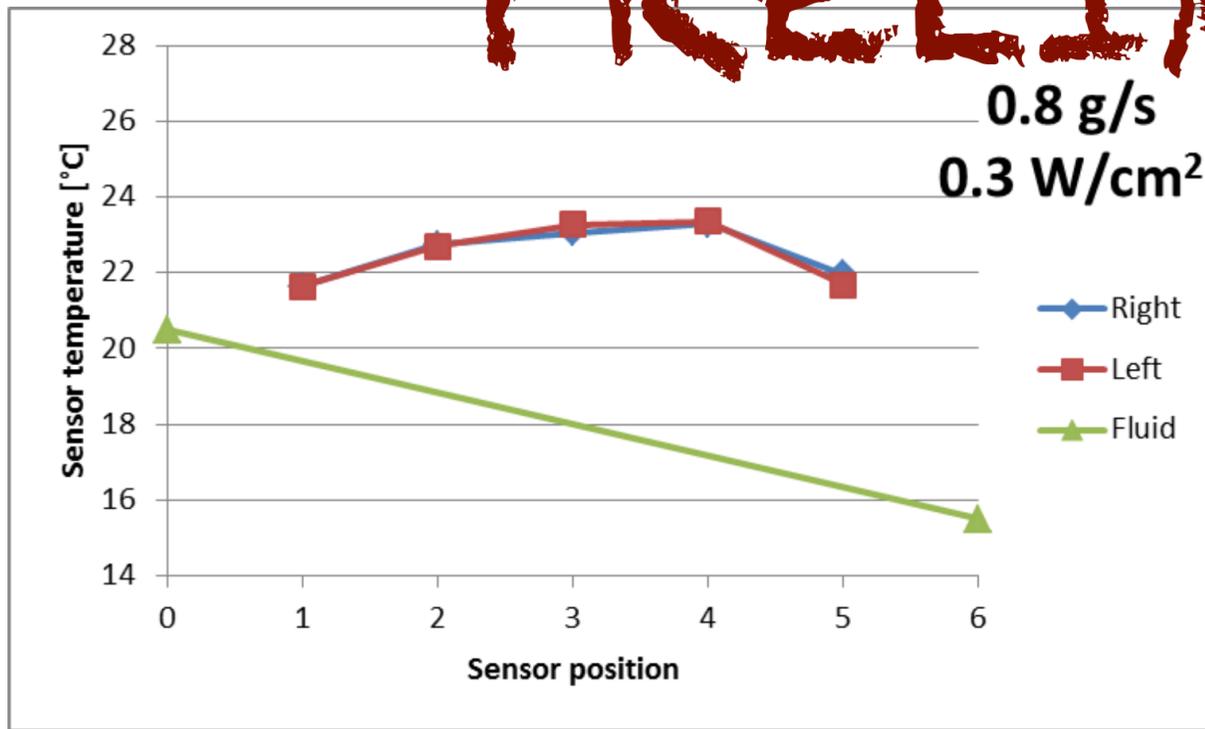




Preliminary tests using the first frame available: due to fabrication problems this frame has the heater glued on the pyrex side (high thermal resistance).
Future tests with the heater on silicon side.



PRELIMINARY





- **CERN group**
 - Andrea Catinaccio
 - Benedetto Gorini
 - Maurice Haguenaue
 - Zoe Lawson
 - Giovanna Lehmann Miotto
 - Pietro Maoddi
 - Alessandro Mapelli
 - Raul Murillo Garcia
 - Paolo Petagna
 - Wainer Vandelli
- **EPFL group**
 - Sébastien Jiguet
 - Philippe Renaud
 - Noelia Vico Triviño
- **INFN group**
 - Guglielmo Gemignani
 - Daniele Ruggieri
 - Francesco Safai-Tehrani
 - Riccardo Vari
 - Stefano Veneziano