

# **FRESCA2 TEST PLANS @ CERN**

**by Marta Bajko**

**on behalf of**

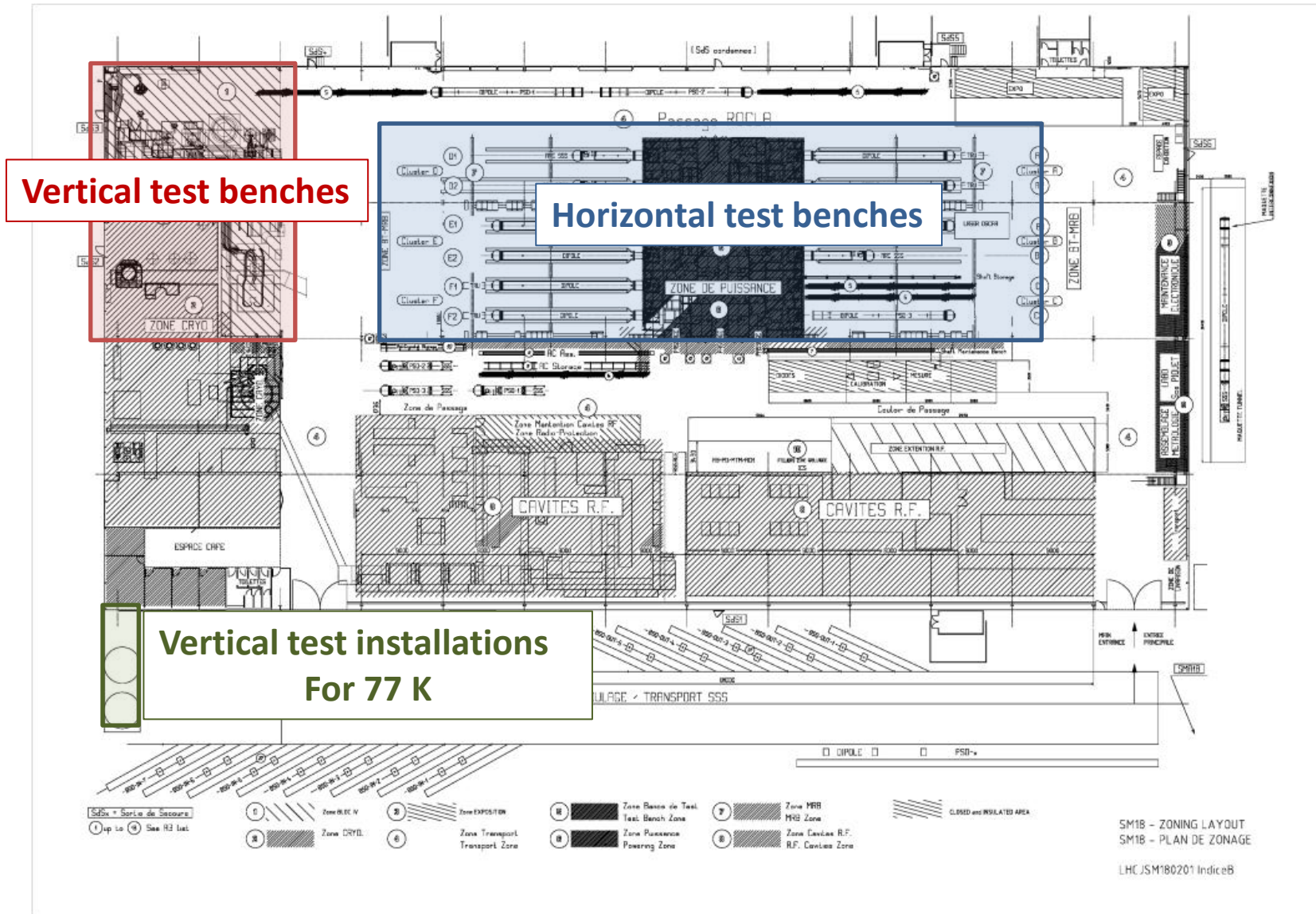
H. Bajas , Vladislav Benda, Juan Carlos Perez  
CERN TE department

**For ESAC Review @ CEA- February 2013**

# Summary

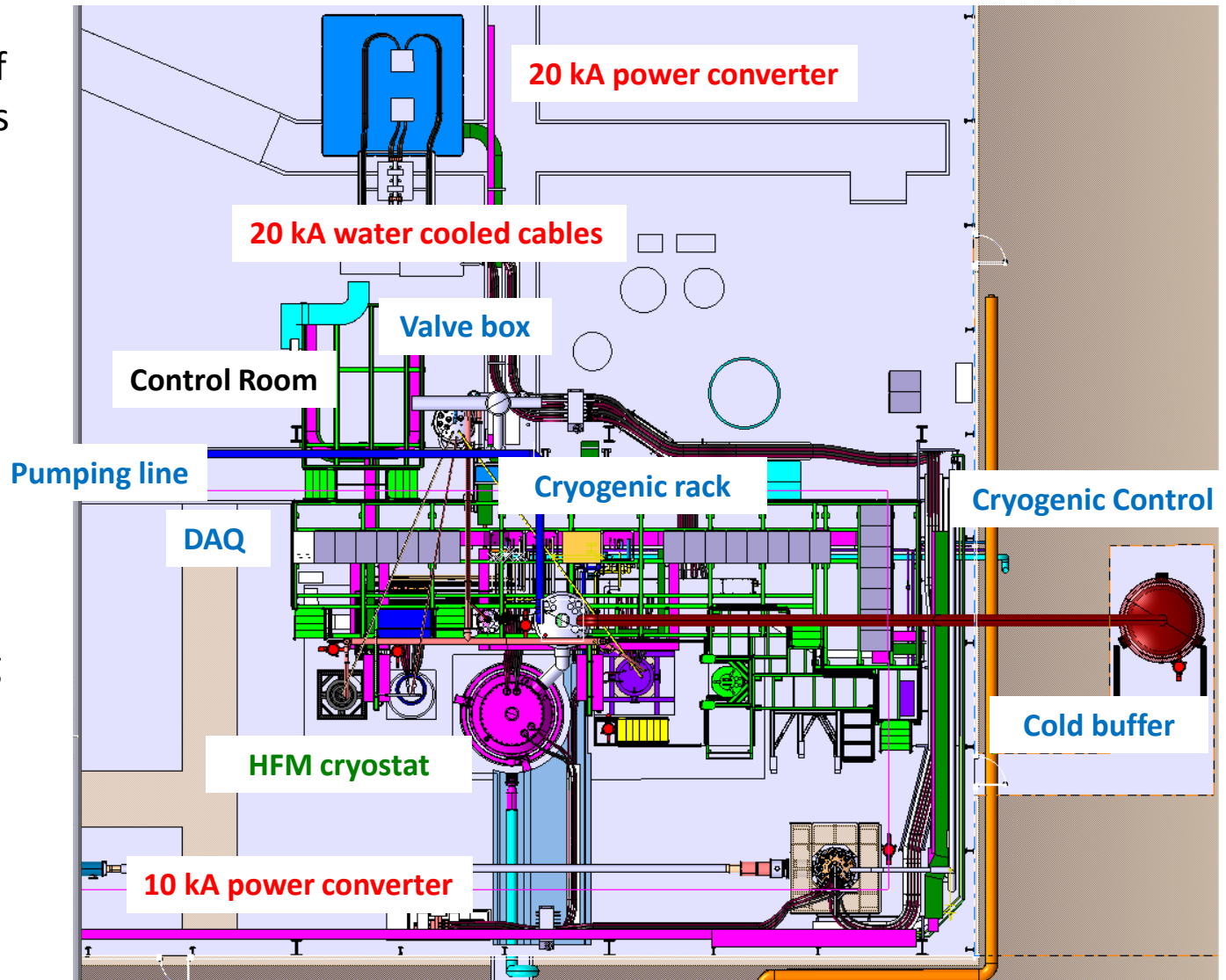
- Cryogenic test station layout
  - 1.9 K test station
  - 77 K test station
- Inputs and constraints for the test station design
- Main ingredients of the HFM test station
- Status of the main ingredients
- Update of the planning

# Cryogenic test station SM18 layout



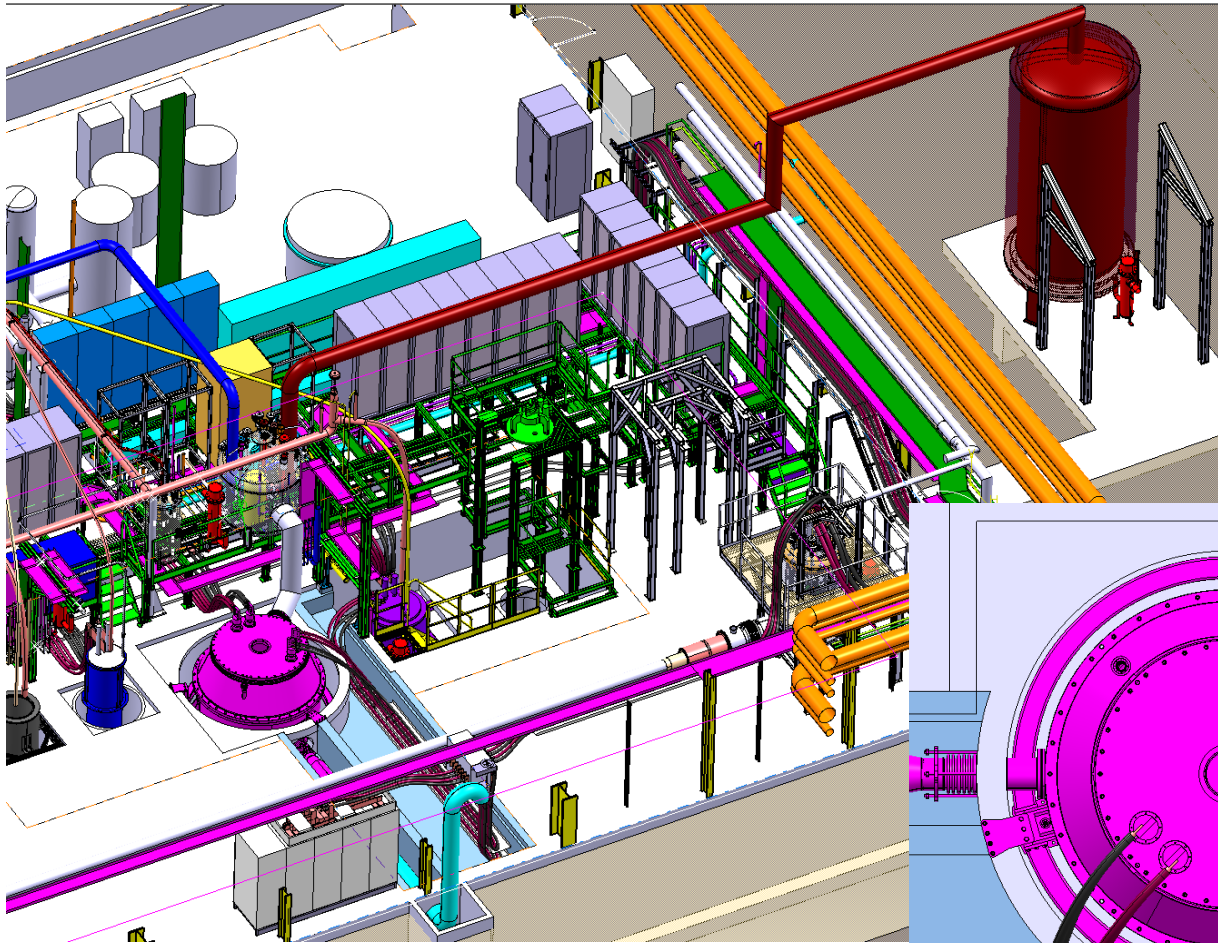
# The Vertical Test station in SM18.

The integration of the HFM station is completed.



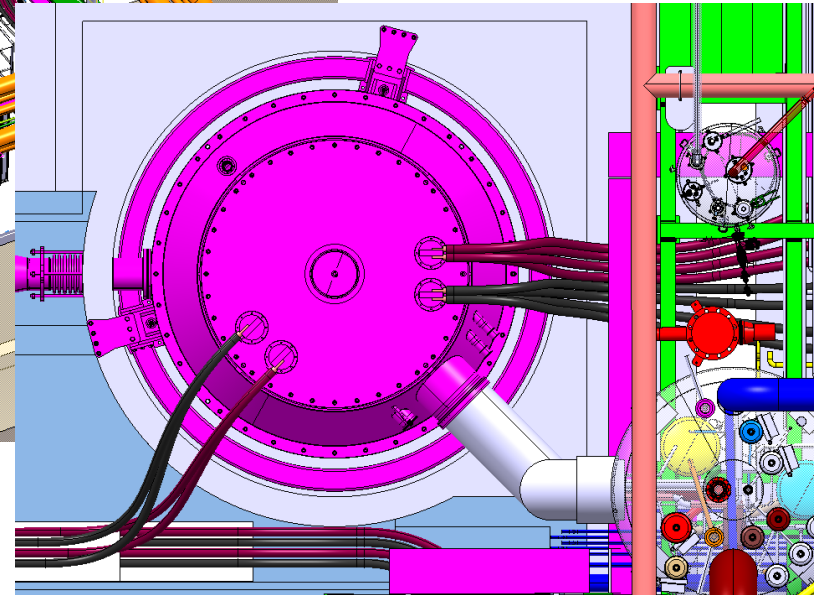
Civil engineering work inside the hall is finished

# Water cooled cables, switches and current leads



HTs current leads will be design on purpose for the test station. The current leads fabrication time: 1 year from  $t_0$ . ( will be in the shadow of the cryogenics)

In the 20 kA circuit current distribution switch is integrated, tested up to 17 kA. A second, smaller one, is needed for the 10 kA circuit.

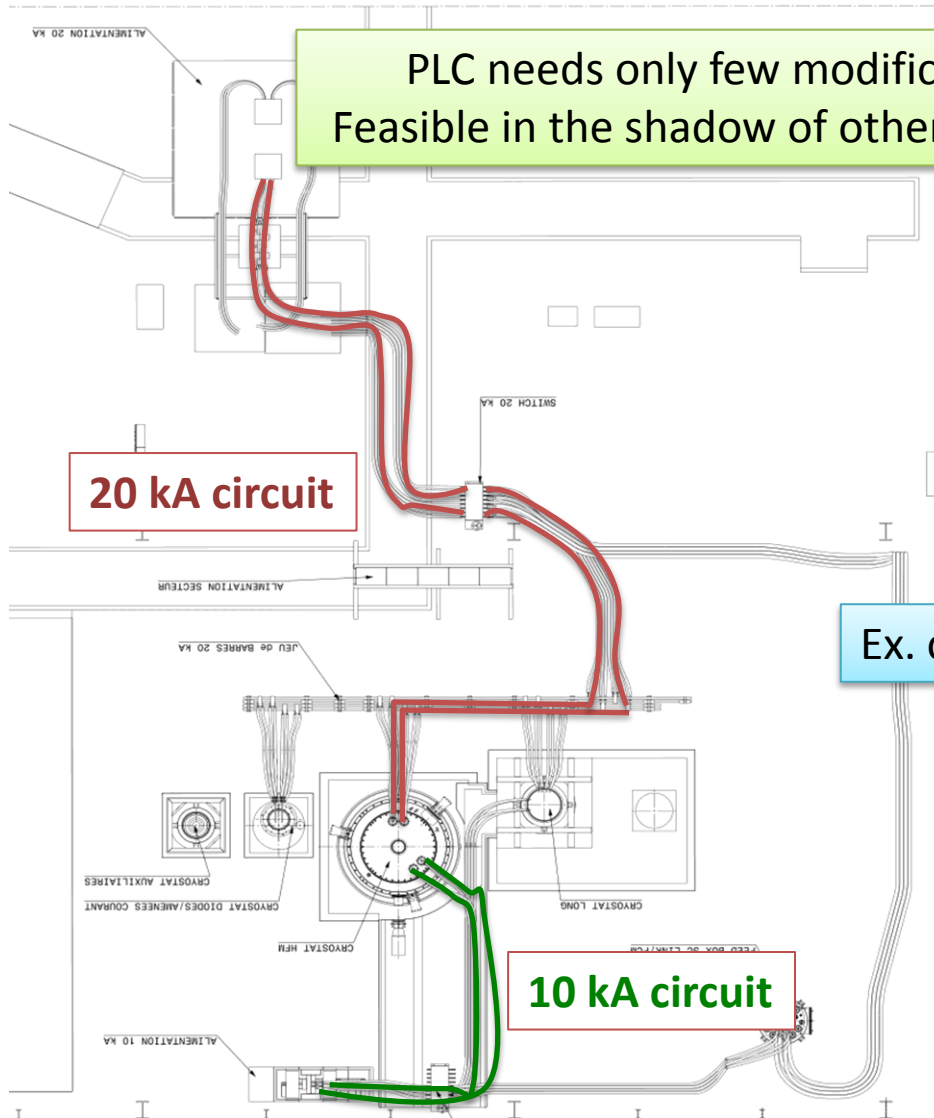


We are in the phase of defining the interface between current leads and water cooled cables. Fabrication time: 9 mounts from  $t_0$

8 x 500 mm copper water cooled cables between bus bars and current leads for the 20 kA circuit

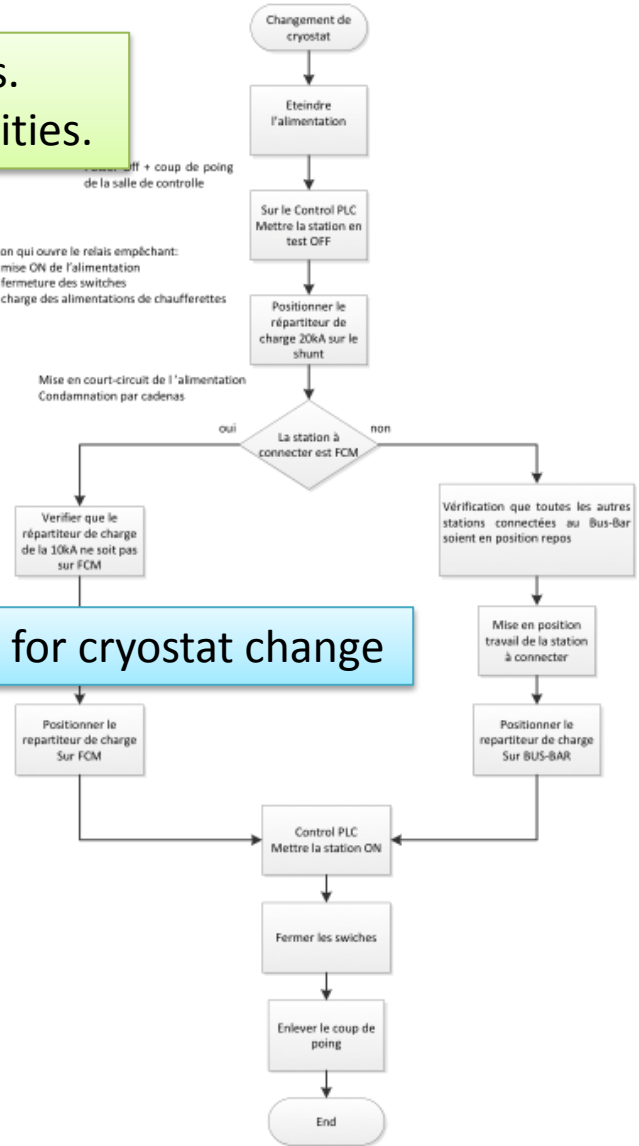
4 x 500 mm Cu water cooled cables between 10 kA power converter and inserts trough a dedicated switch ( < than the existing 16 kA)

# Electrical distribution of vertical test facility



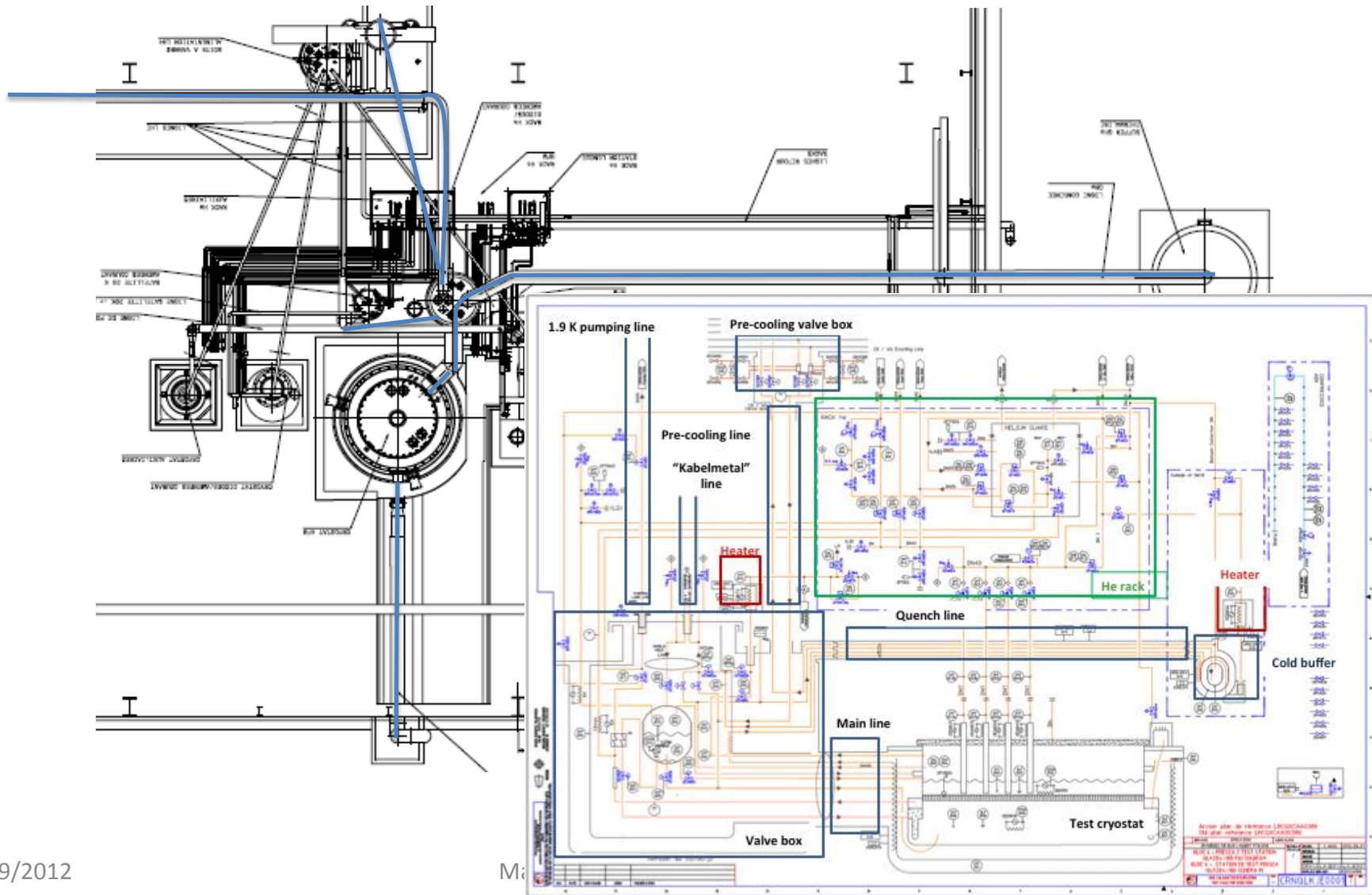
- Action qui ouvre le relais empêchant:
- La mise ON de l'alimentation
  - La fermeture des switches
  - La charge des alimentations de chaufferettes

## Ex. of PLC for cryostat change

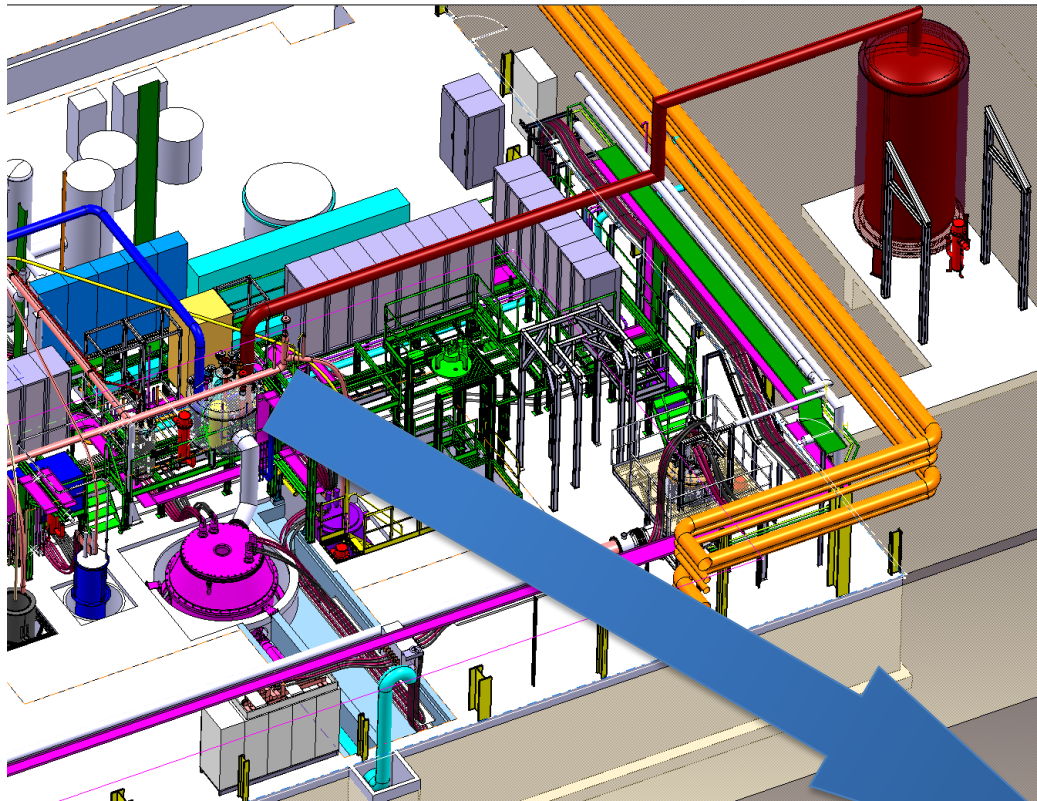


# Cryogenic distribution of the vertical test facility

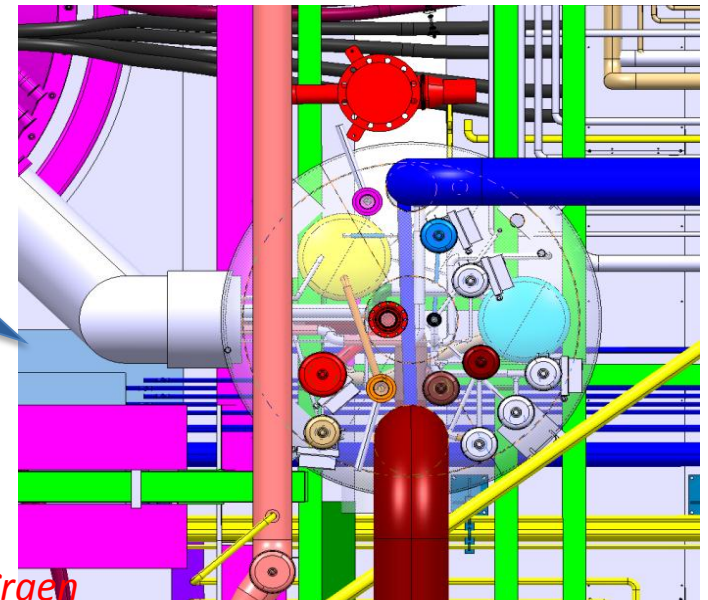
## The HFM lines and the P&I diagram



# Cryogenic items of the HFM



Item	Group	Contracts
Cryostat	TE-MSC	-
Valve Box	TE-CRG	Contract 1
Main Line		
Pre-cooling Line		
Quench Line		
Cold Buffer	TE-CRG	Contract 2
Pre-cooling Valve Box		
He Rack		
1.9K Pumping Line		Contract 3
Kabelmetal Line		Contract 4
15kW Heater		TE-CRG
General Assembly		



End of the installation of cryogenic items: Jun 2014

*For cryostat design and manufacturing see slides of A. Vande Craen*

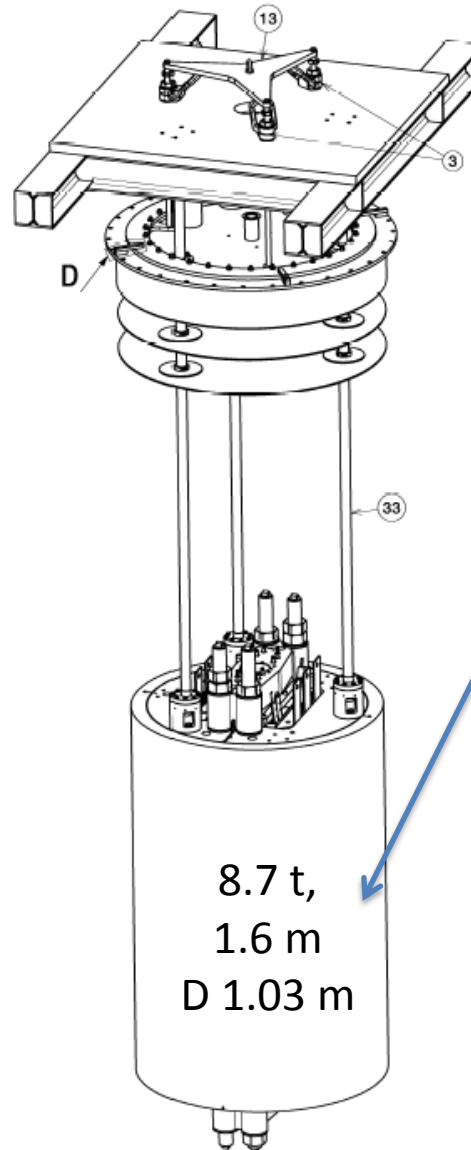


# LN<sub>2</sub> test station : goals and constrains

## GOAL

Before summer 2013 the **study, of the thermo mechanical behaviour** of the structure at different pre-stress is, required.

The LHe test station IS **NOT AVAILABLE** yet, therefore it was decided to set up a dedicated test station at LN<sub>2</sub>.



## CONSTRAINS

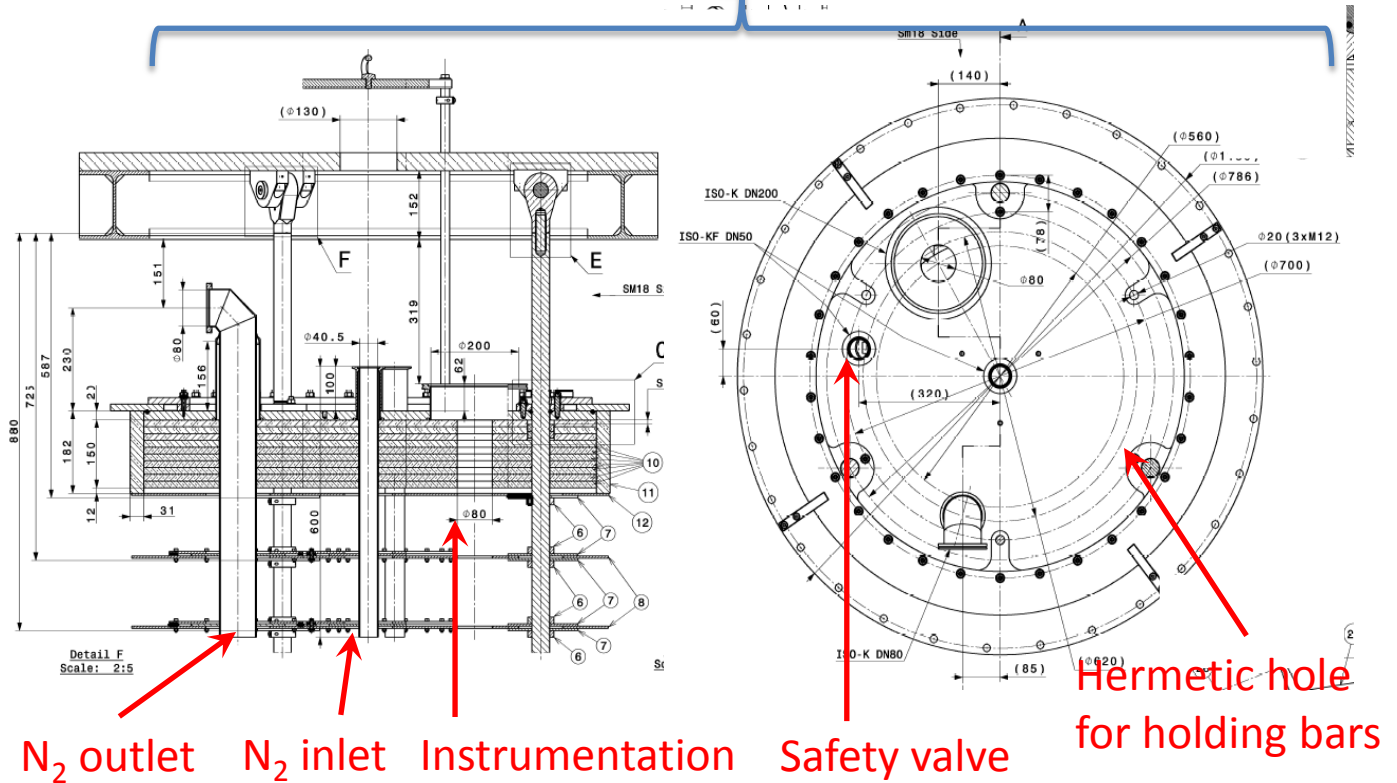
**Huge mass** and **large dimension** of the magnet requires optimized cooling scenario.

Due to differential thermal shrinkage of Al and steel, the maximum temperature difference between two points of the structure was limited to max. **100 K**.

*See presentation of Paolo, Jorge and Juan Carlos*

# LN<sub>2</sub> test station issues: cryostat and top plate

Need of an **insulated cryostat** with a **top-plate** to limit nitrogen consumption, to improve cooling time and prevent ice formation.



# LN<sub>2</sub> test station issues: nitrogen gas or liquid nitrogen?

$\Delta T = 100 \text{ K}$



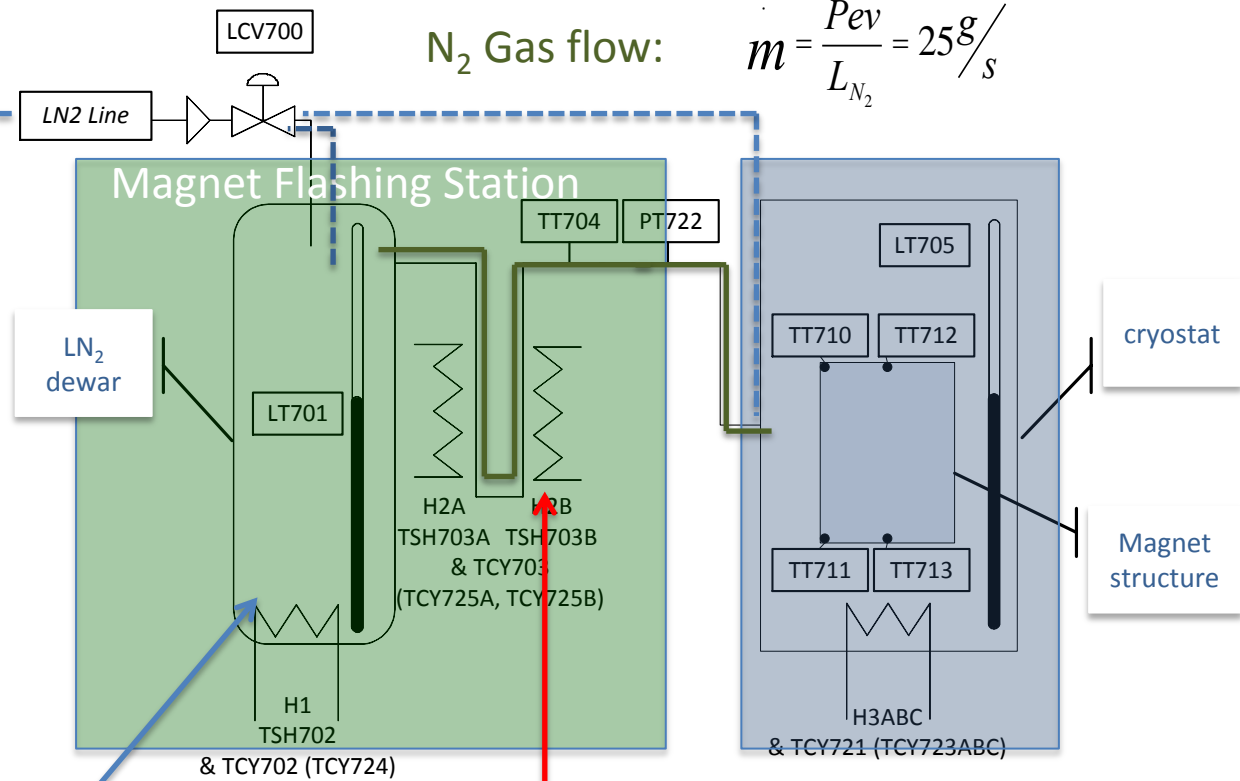
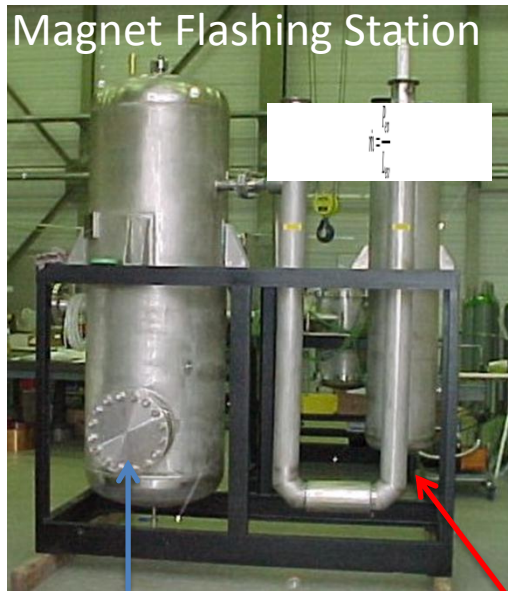
Liquid nitrogen can not directly be used for cooling.

Nitrogen gas should be used with descent flow (high power evaporator) and at controlled temperature (gas heater).

LN<sub>2</sub> line from LN<sub>2</sub> dewar

N<sub>2</sub> Gas flow:

$$\dot{m} = \frac{P_{ev}}{L_{N_2}} = 25 \text{ g/s}$$



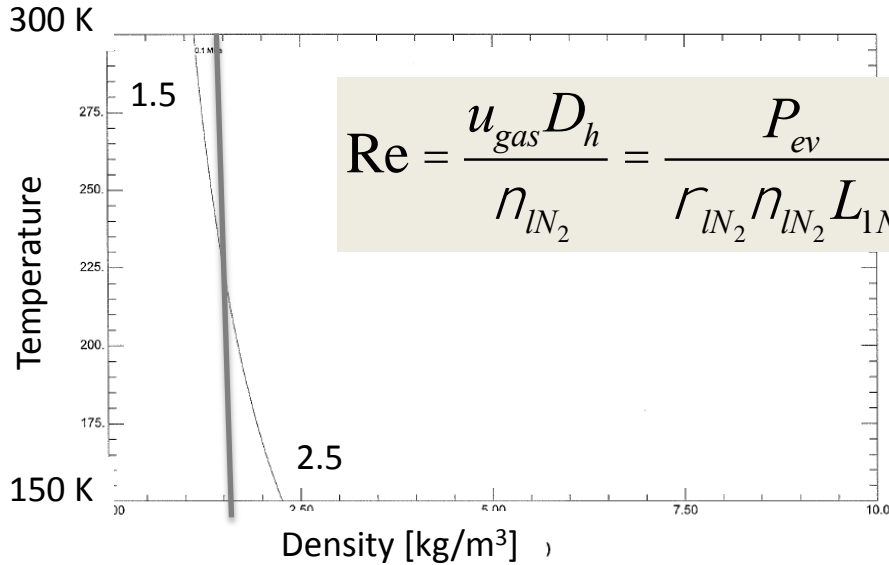
LN<sub>2</sub> evaporator 5 kW

GN<sub>2</sub> heater 2 x 2.5 kW

# LN<sub>2</sub> test station issues: cooling

Analytical transient thermal model shows:

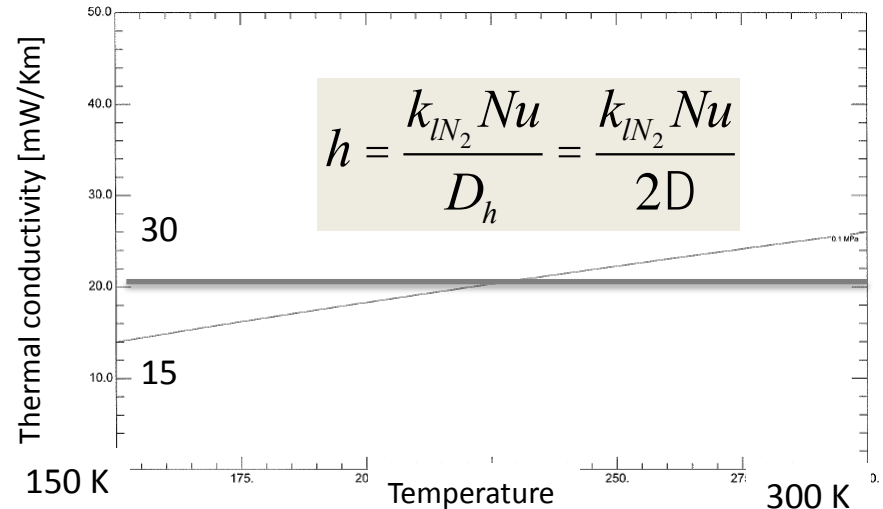
1. Nitrogen gas flow *cannot be turbulent* with the given mass flow rate and geometry.



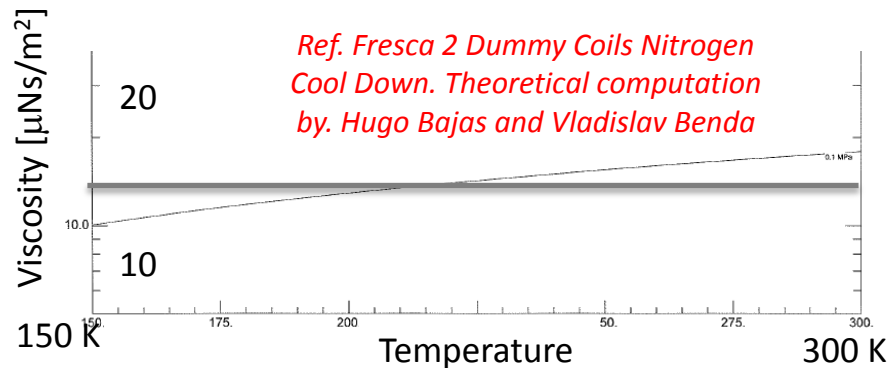
$$Re = \frac{u_{gas} D_h}{\nu_{N_2}} = \frac{P_{ev}}{r_{N_2} n_{N_2} L_{N_2}} \frac{2D}{A_c(D_m, D)}$$

2. The heat convection coefficient is quite low as compared to boiling nitrogen.

*Nu @ const*



$$h = \frac{k_{N_2} Nu}{D_h} = \frac{k_{N_2} Nu}{2D}$$



*Ref. Fresca 2 Dummy Coils Nitrogen Cool Down. Theoretical computation by. Hugo Bajas and Vladislav Benda*

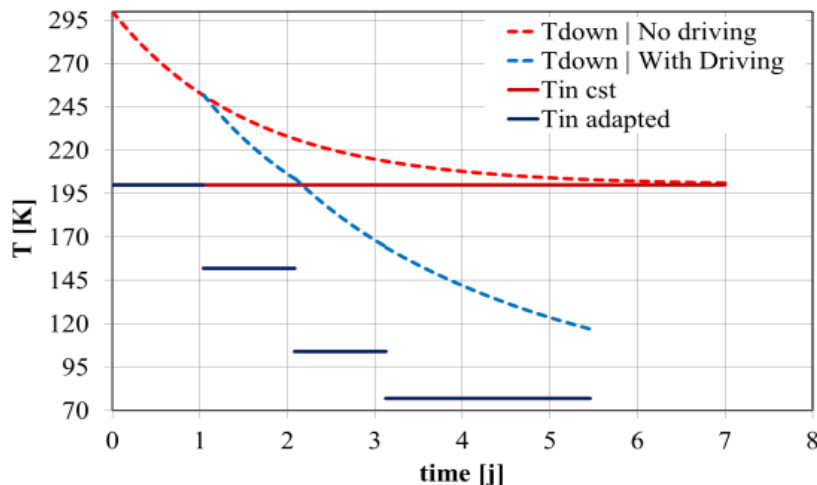
# LN<sub>2</sub> test station issues: cooling time

According to the value of the Biot number ( $< 0.1$ ), the *Lumped Capacitance Method* can be used. Then the temperature can be assumed uniformly distributed within the structure at any time of the transient process.

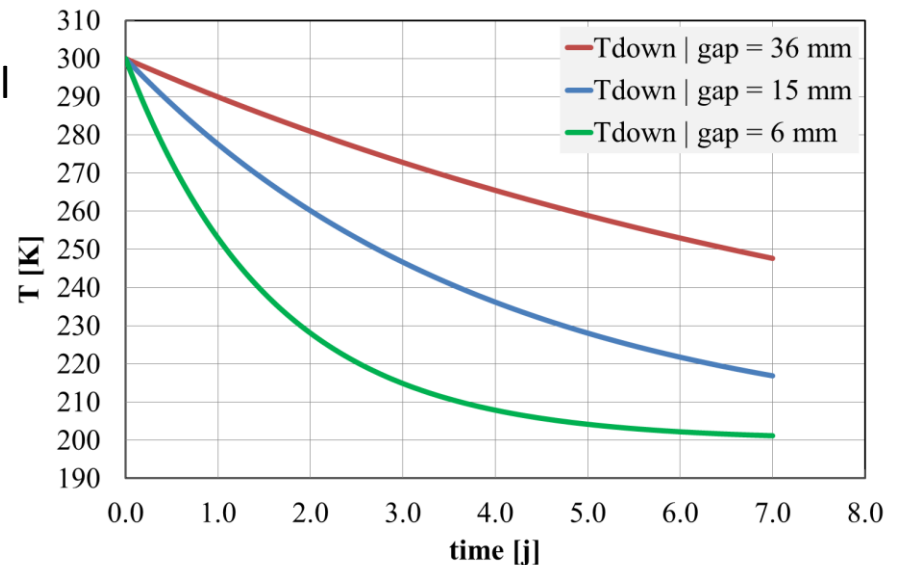
$$r_M V_M C_{pM} \frac{dT}{dt} = h A_s (T_{\infty} - T_M)$$

the temperature evolution is an exponential decay with the time constant  $\tau$  [s]

$$t = \frac{r_M V_M c_{pM}}{\rho D_M L_M h} \quad h = \frac{k_{LN_2} Nu}{D_h} = \frac{k_{LN_2} Nu}{2D}$$



The temperature at the bottom of the magnet



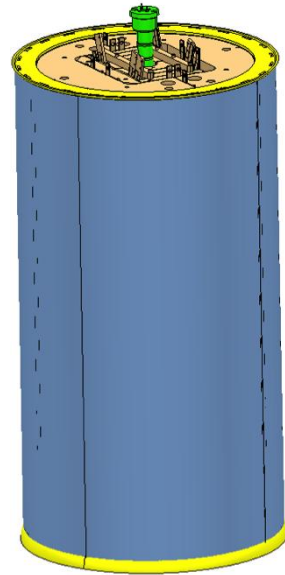
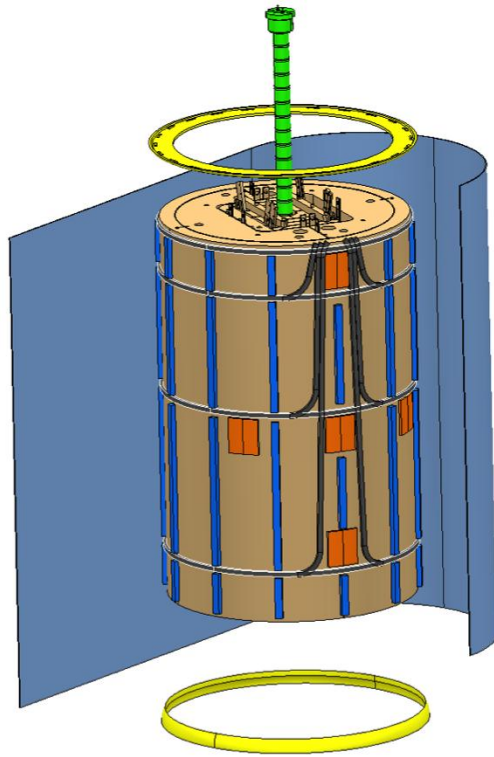
With 36 mm gap the cooling to 180 K would take about 20 days while with 6 mm, 5 days. From this moment LN<sub>2</sub> can be used and in less than 1 day, everywhere in the structure, the 77 K will be achieved.

Then the filling of about 1000 l of LN<sub>2</sub> will take an additional day .

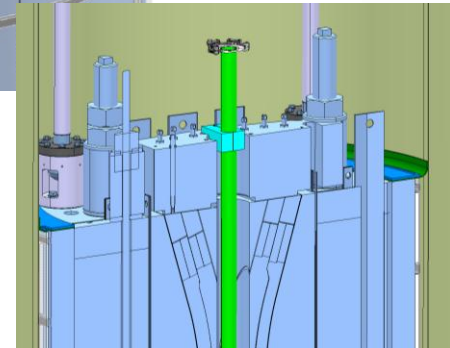
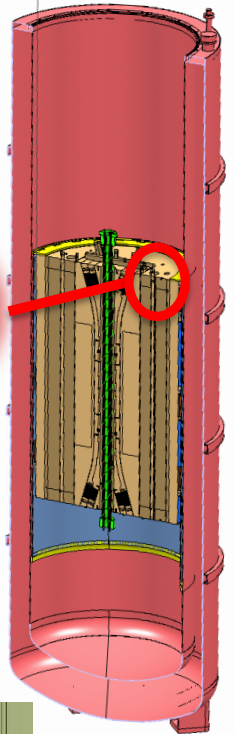
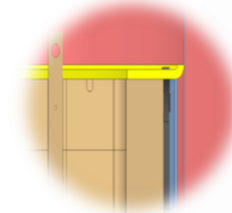
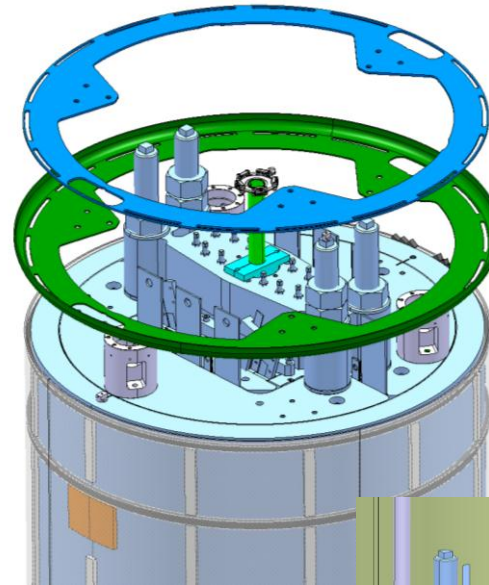
# LN<sub>2</sub> test station issues: reducing the cooling time

Special preparation of the magnet is needed to create cooling channels. The **gap** is reduced to **10 mm** and the gas flow is forced towards the magnet outer shell

The dressed magnet with 3 mm thick “Teflon skirt”



Leak tightness to force the LN<sub>2</sub> flow in between the magnet and the skirt



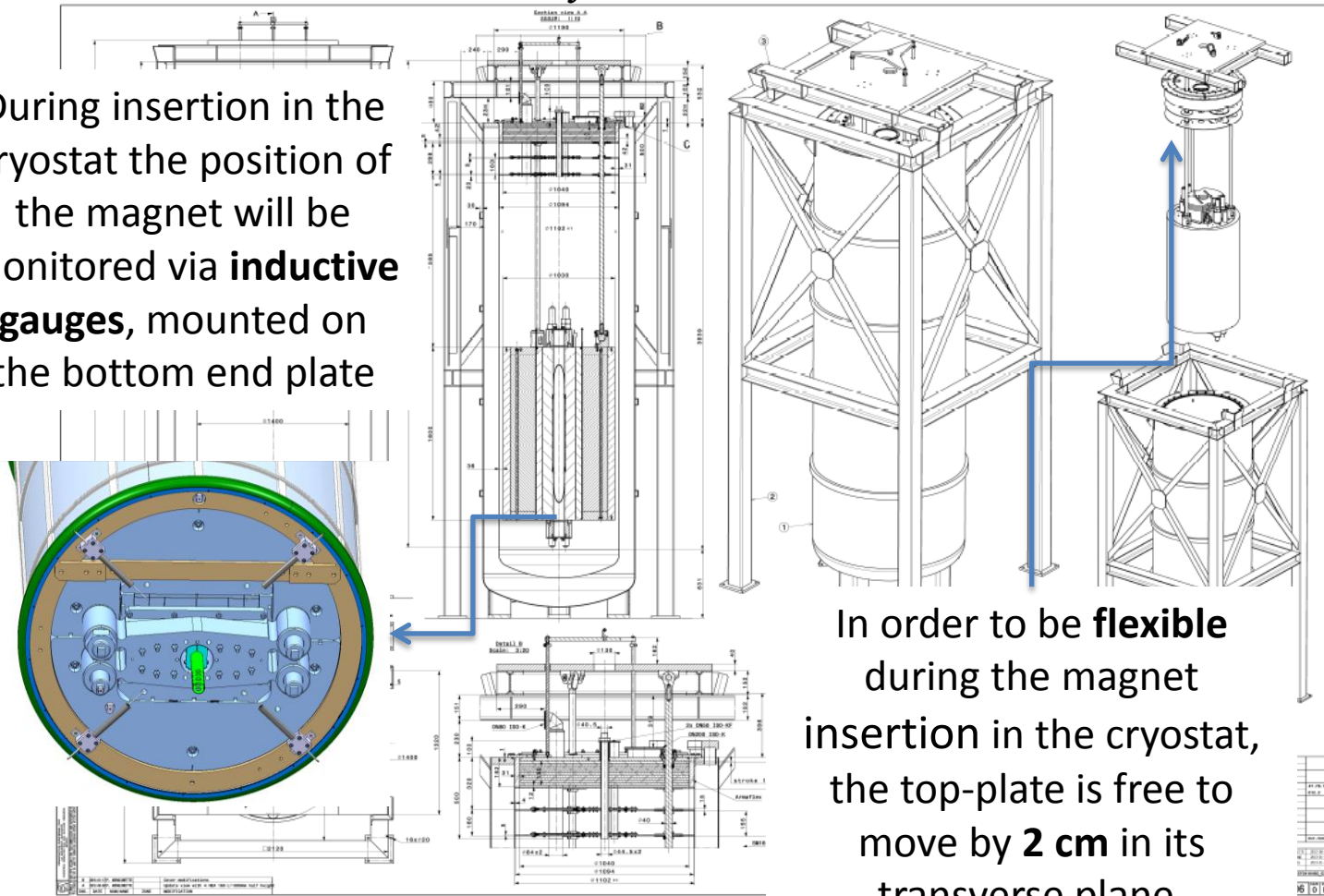
This is a good solution to solve the thermal problem!

# LN<sub>2</sub> test station issues: reducing the cooling time

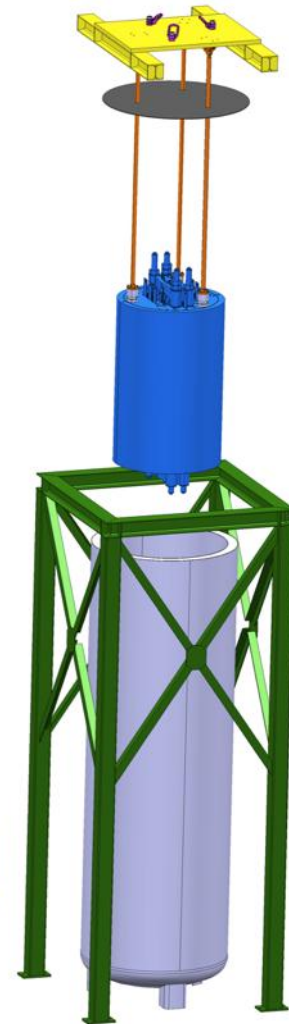
But is a problem for the installation!

As a consequence of the dressing, the distance between the magnet outer diameter and the cryostat inner diameter will be reduced !

During insertion in the cryostat the position of the magnet will be monitored via **inductive gauges**, mounted on the bottom end plate

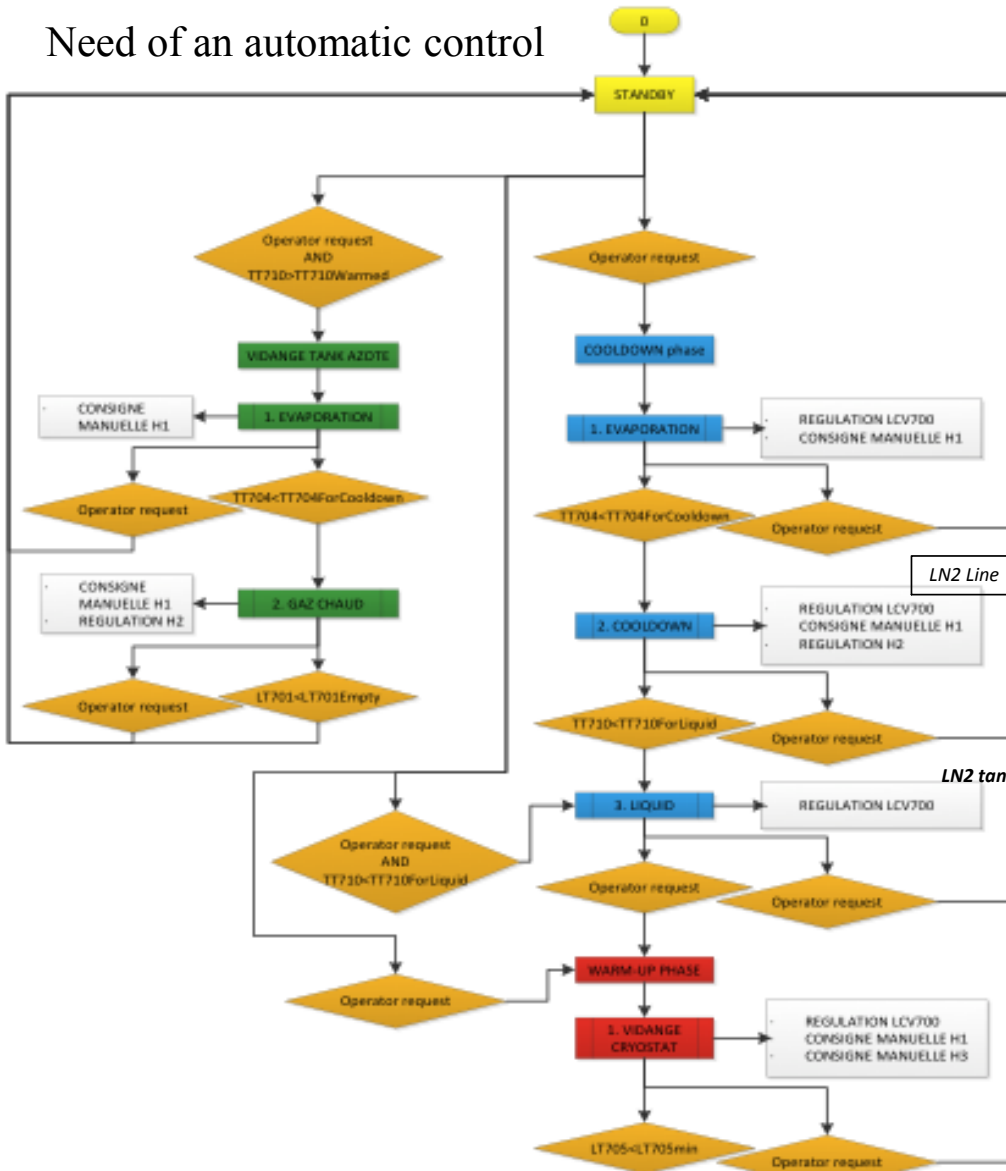


In order to be **flexible** during the magnet insertion in the cryostat, the top-plate is free to move by **2 cm** in its transverse plane.



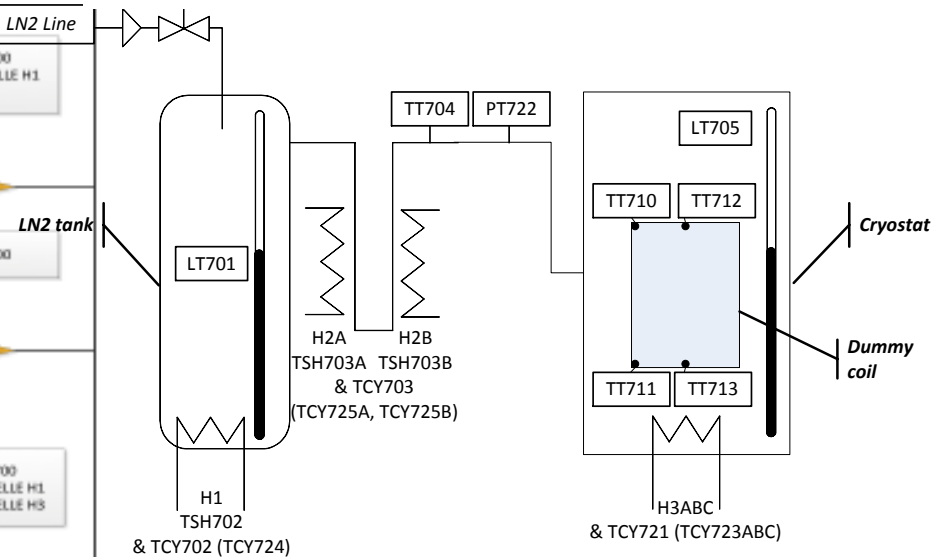
# LN<sub>2</sub> test station issues: PLC during cooling time

Need of an automatic control



- Regulation made with UNICOS standard
- User interface in control room via TechNet
- Management of interlocks & alarms
- Default limit parameters can be configured
- Operator **can exit manually** every (sub-)phase in case of need
- Operator **can start manually** cool-down, liquid (under conditions), warm-up, and emptying phase (under conditions)

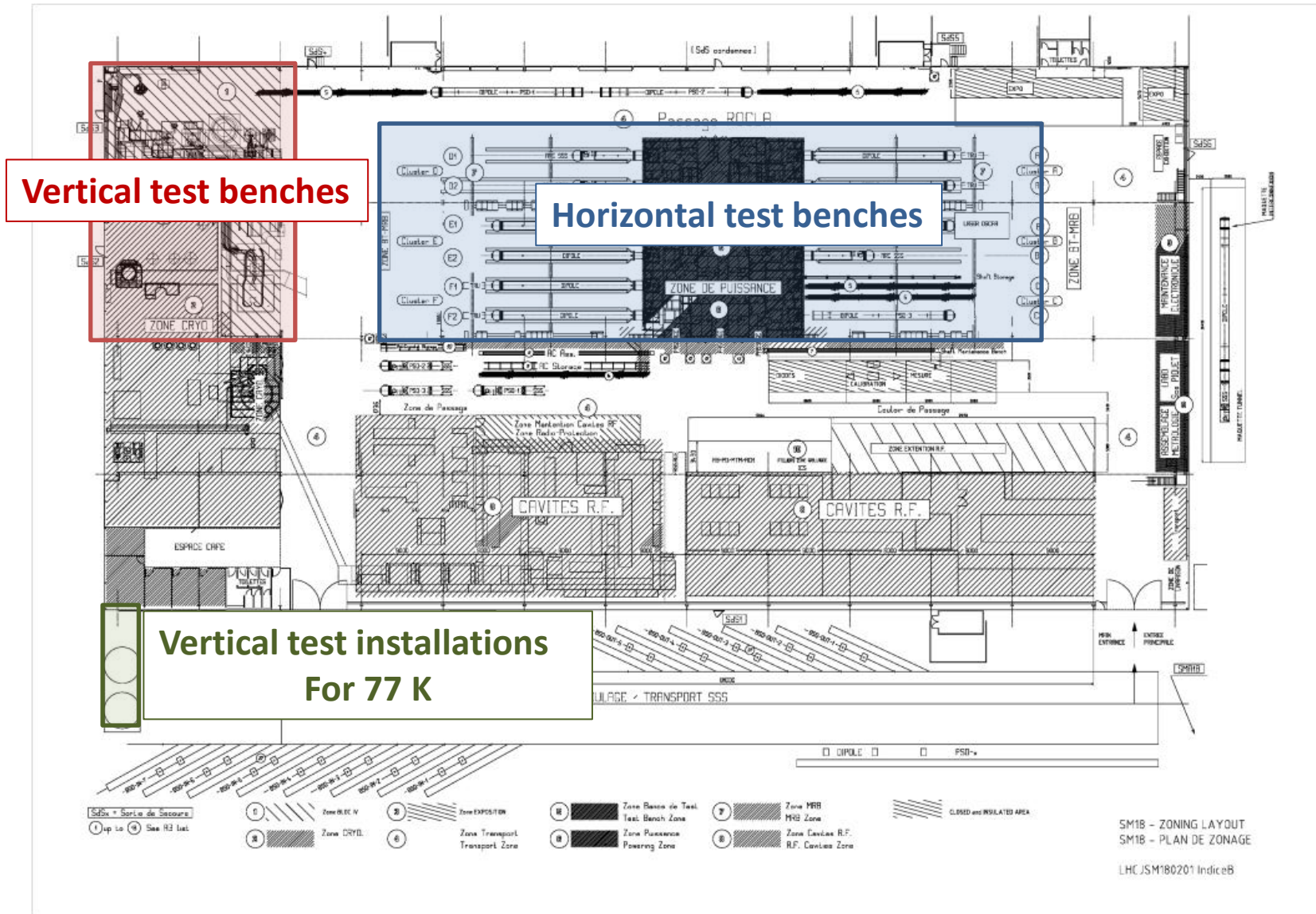
*Ref. Plc for LN2 test station by M. Charrondiere*



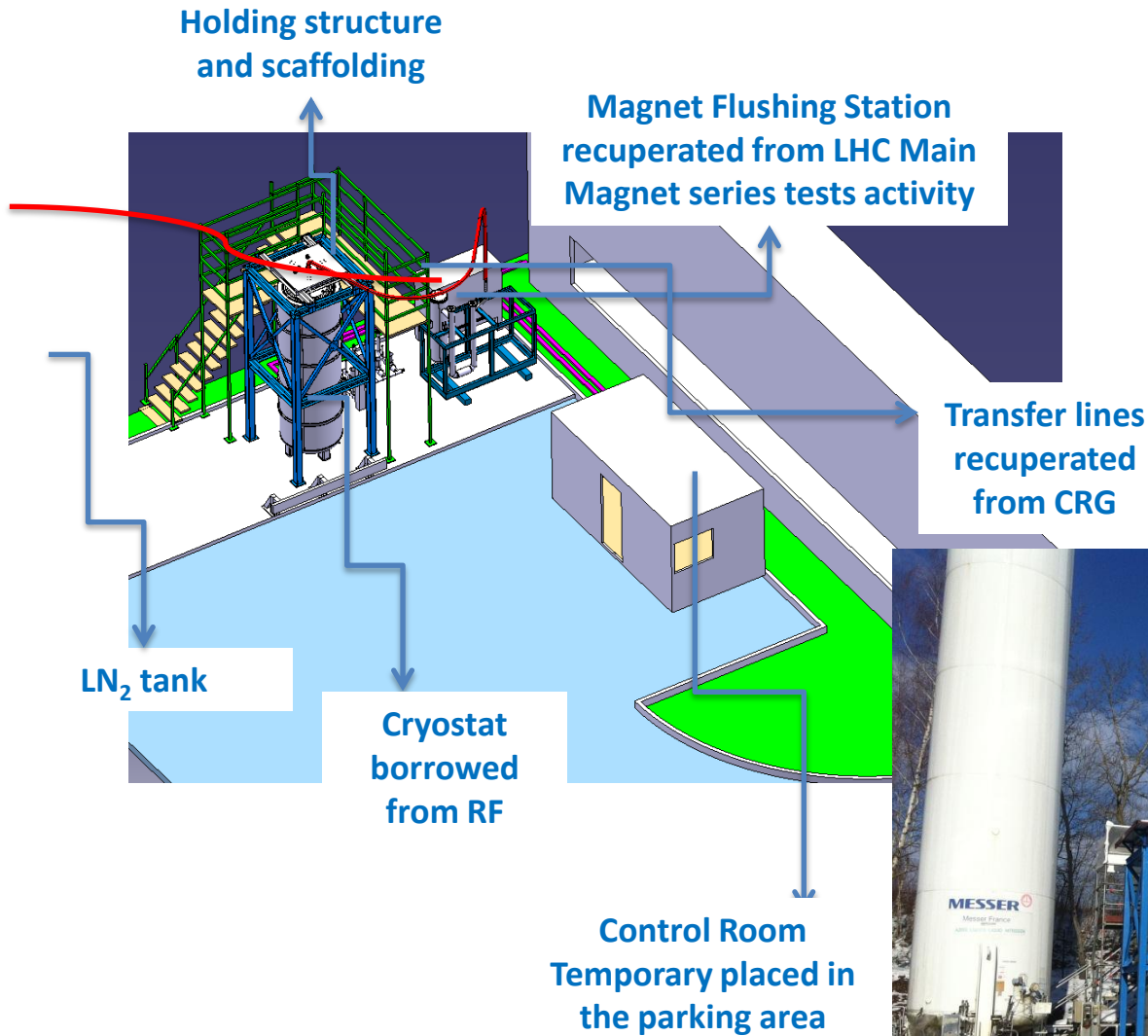
H3 is a heater for warm up or for direct cooling with LN<sub>2</sub>



# Cryogenic test station SM18 layout

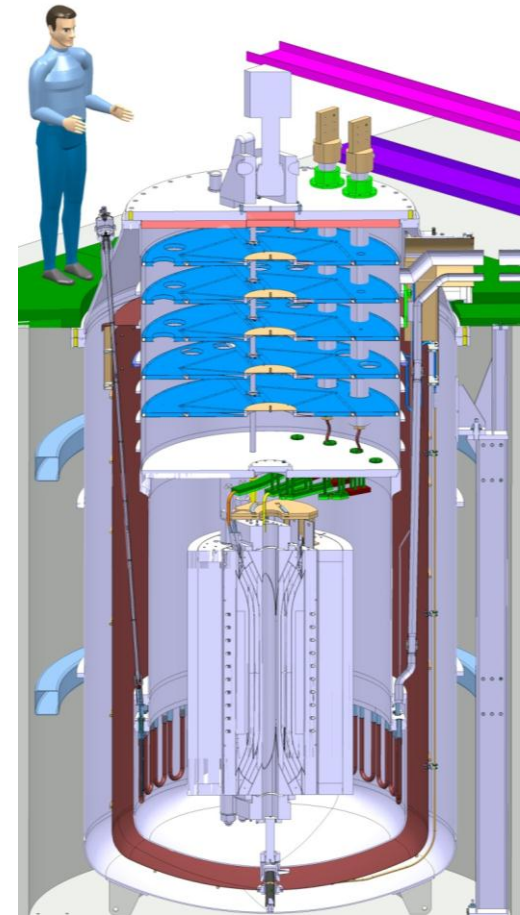
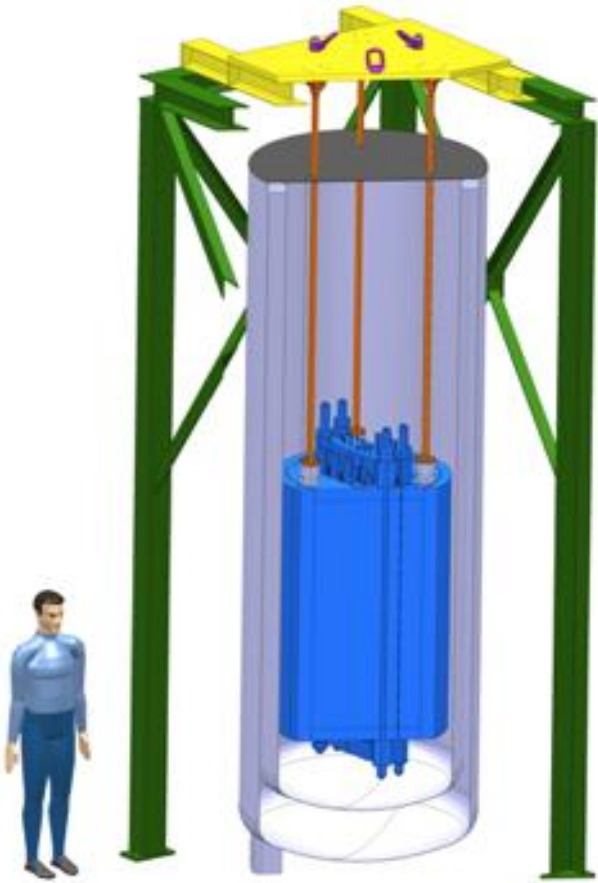


# LN<sub>2</sub> Test station layout in Sm18



# When can we test?

@ 77 K: end of April 2013



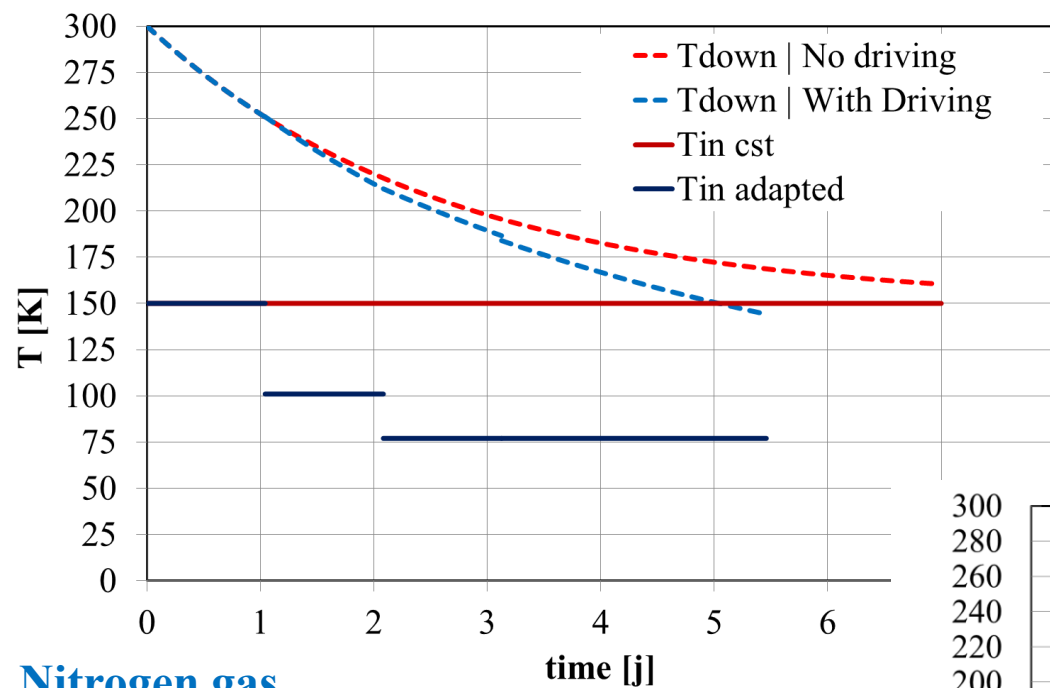
@ 1.9 K: end of September 2014

# Acknowledgement

Christian Giloux, Patrick Viret, Maryline Charrondiere  
Pierre Minginette, Philippe Perret,  
Gijs De Rijk, Nicolas Peray,  
Olivier Pirotte

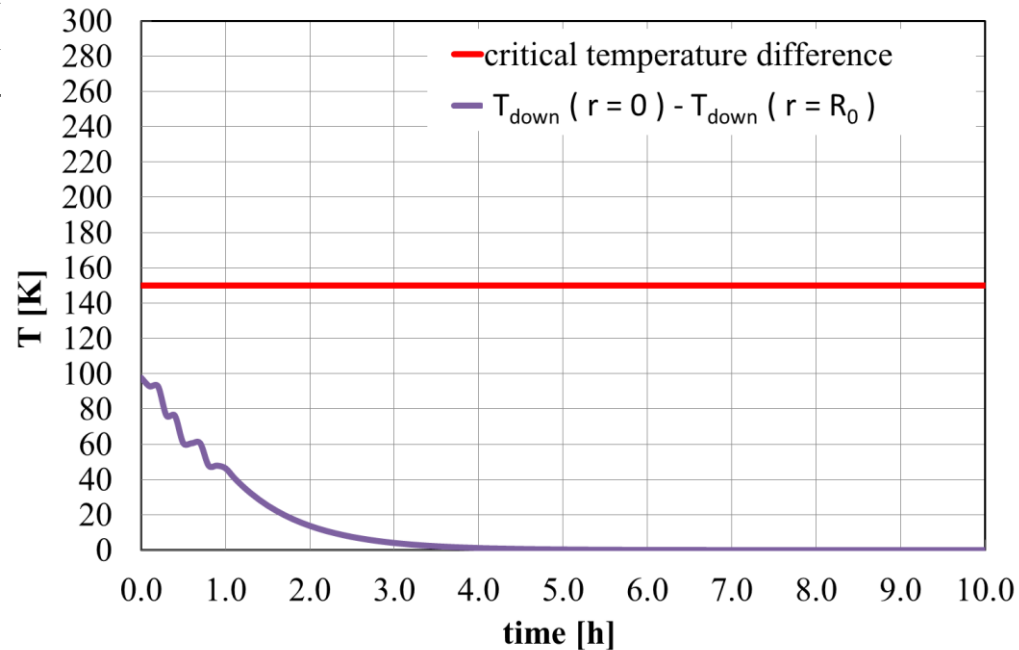
And many other for the construction of the test station  
(up to 20 sections across CERN)





**Nitrogen gas injection**

**Nitrogen liquid injection**



In case 150 K difference is allowed with a 10mm gap, we inject the 1<sup>st</sup> day gas at  $T_{\text{in}} = 150$  K then the 2<sup>nd</sup> day at  $T_{\text{in}} = 100$  K, the 3<sup>rd</sup> day liquid can be injected safely.  
*In 4 days, the magnet is cold.*