Exercises for RF Tutorial — Solutions

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1 Cavities

Question 1

1. $c = \lambda \cdot f \to \lambda = \frac{c}{f} = \frac{3 \cdot 10^8 \text{ ms}^{-1}}{150 \cdot 10^6 \text{ s}^{-1}} = 2 \text{ m}$

2. $a = 0.383 \cdot \lambda = 0.383 \cdot 2 \text{ m} = 0.766 \text{ m} \approx 77 \text{ cm} \rightarrow d = 2 \cdot a = 1.54 \text{ m}$

3.
$$\frac{R}{Q} = 185\frac{h}{a} \rightarrow h = \frac{R}{Q} \cdot \frac{a}{185} = 300\Omega \cdot \frac{0.77 \,\text{m}}{185\Omega} = 1.25 \,\text{m}$$

4. $Q = \frac{a}{\delta} \left[1 + \frac{a}{h} \right]^{-1}$ with $\delta = \sqrt{\frac{2}{\omega \sigma \mu}} = \sqrt{\frac{1}{\pi \, f \, \sigma \mu}}$
Copper: $\mu = \mu_0 \cdot \mu_r$; $\mu_0 = 4\pi \cdot 10^{-7} \frac{\text{mkg}}{\text{s}^2 \text{A}^2}$, $\mu_r = 1$; $\rightarrow \delta = \sqrt{\frac{1}{\pi 150 \cdot 10^6 58 \cdot 10^6 4\pi \cdot 10^{-7}}} = 5.4 \cdot 10^{-6} \,\text{m}$
 $\rightarrow Q = \frac{0.77}{5.4 \cdot 10^{-6}} \cdot \left[1 + \frac{0.77}{1.25} \right]^{-1} = 88238$
StSt: $\mu = \mu_0 \cdot \mu_r$; $\mu_0 = 4\pi \cdot 10^{-7} \frac{\text{mkg}}{\text{s}^2 \text{A}^2}$, $\mu_r = 1$; $\rightarrow \delta = \sqrt{\frac{1}{\pi 150 \cdot 10^6 1.4 \cdot 10^6 4\pi \cdot 10^{-7}}} = 3.5 \cdot 10^{-5} \,\text{m}$
 $\rightarrow Q = \frac{0.77}{3.5 \cdot 10^{-5}} \cdot \left[1 + \frac{0.77}{1.25} \right]^{-1} = 13614$
5. $R = \frac{R}{Q} \cdot Q = 300 \cdot 88238 = 26.47 \cdot 10^6 \,\Omega \approx 26 \,\text{M}\Omega$

$$\frac{R}{Q} = \omega L \to L = \frac{R}{Q} \frac{1}{\omega} = \frac{R}{Q} \frac{1}{2\pi f_{\text{res}}} = 300 \frac{1}{2\pi 150 \cdot 10^6} = 318.3 \text{ nH}$$
$$\frac{R}{Q} = \frac{1}{\omega C} \to C = \left[\frac{R}{Q}\omega\right]^{-1} = \left[\frac{R}{Q}2\pi f_{\text{res}}\right]^{-1} = [300 \cdot 2\pi \cdot 150 \cdot 10^6]^{-1} = 3.5 \text{ pF}$$

Question 2

- 1. TM_{mnp}: $\lambda = \frac{2}{\sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2 + \left(\frac{p}{c}\right)^2}} \to TM_{101}, a = c$: $\lambda = \frac{2}{\sqrt{\left(\frac{1}{a}\right)^2 + \left(\frac{1}{a}\right)^2}} = \frac{2a}{\sqrt{2}} = \sqrt{2}a = \sqrt{2} \cdot 100 = 141.4 \text{ mm}}$ $c = \lambda \cdot f \to f_{res} = \frac{c}{\lambda} = \frac{3 \cdot 10^8}{141.4 \cdot 10^{-3}} = 2.12 \text{ GHz}$ 2. $\delta = \sqrt{\frac{2}{\omega \sigma \mu}} = \sqrt{\frac{2}{2\pi f_{res} \sigma \mu}} = \sqrt{\frac{2}{2\pi 2 \cdot 12 \cdot 10^9 58 \cdot 10^6 4\pi \cdot 10^{-7}}} = 1.43 \,\mu\text{m}$ $Q = \frac{\lambda}{\delta} \frac{b}{2} \frac{(a^s + c^2)^{\frac{3}{2}}}{c^3(a + 2b) + a^3(c + 2b)} \to a = c, \lambda = \sqrt{2}a$: $Q = \frac{1}{\delta} \frac{ab}{a + 2b} = \frac{1}{1.43 \cdot 10^{-2}} \frac{100 \cdot 50}{100 + 2 \cdot 50} = 17422$ 3. $\frac{1}{Q_L} = \frac{1}{Q_0} + \frac{1}{Q_{ext}} \to Q_L = Q_{ext}$: $\frac{1}{Q_L} = \frac{2}{Q_0} \to Q_L = \frac{Q_0}{2} = \frac{17422}{2} = 8711$ 4. $Q = \frac{f_{res}}{\Delta f} \to \Delta f = \frac{f_{res}}{Q} \to \text{ loaded cavity bandwidth: } \Delta f = \frac{f_{res}}{Q_L} = \frac{2.12 \cdot 10^9}{8711} = 243.6 \text{ kHz}$
 - 5. At critical coupling all power is going into the cavity and no power is reflected. Hence, all power is thermally dissipated: $P_{in} = P_{TH} = 50 \text{ W}$

6.
$$Q = \frac{\omega W}{P} \rightarrow W = \frac{QP}{\omega} = \frac{QP}{2\pi f_{\text{res}}} \rightarrow \text{loaded cavity: } W = \frac{Q_L P_{\text{in}}}{2\pi f_{\text{res}}} = \frac{8711 \cdot 50}{2\pi 2 \cdot 10^9} = 32.7 \,\mu\text{J}$$

1. $\lambda = 2.61a = 417.6 \text{ mm}$

$$c = \lambda \cdot f \to f_{res} = \frac{c}{\lambda} = \frac{3 \cdot 10^8}{417.6 \cdot 10^{-3}} = 718 \text{ MHz}$$
2. $\delta = \sqrt{\frac{2}{\omega \sigma \mu}} = \sqrt{\frac{2}{2\pi f_{res} \sigma \mu}} = \frac{2}{2\pi 718 \cdot 10^6 1.4 \cdot 10^6 4\pi \cdot 10^{-7}} = 15.9 \ \mu \text{m}$

$$Q = \frac{a}{\delta} \left[1 + \frac{a}{h} \right]^{-1} \to h = \frac{aQ\delta}{a - Q\delta} = \frac{160 \cdot 10^{-3} 400015.9 \cdot 10^{-6}}{160 \cdot 10^{-3} - 400015.9 \cdot 10^{-6}} = 105.2 \ \text{mm}$$

3.

4.
$$Q = \frac{f_{\text{res}}}{\Delta f} \to \Delta f = \frac{f_{\text{res}}}{Q} = \frac{718 \cdot 10^6}{4000} = 179.6 \text{ kHz}$$

5.
$$\frac{R}{Q} = 185 \frac{h}{a} = 185 \frac{105.2}{160} = 122 \,\Omega$$

Since the $\frac{R}{Q}$ value is a geometrical factor only, it is independent of the material of the cavity. 6. $R = \frac{R}{Q}Q = 122 \cdot 4000 = 488 \text{ k}\Omega$

$$\begin{split} \frac{R}{Q} &= \omega L \to L = \frac{R}{Q} \frac{1}{\omega} = \frac{R}{Q} \frac{1}{2\pi f_{\text{res}}} = 122 \frac{1}{2\pi 718 \cdot 10^6} = 27 \,\text{nH} \\ \frac{R}{Q} &= \frac{1}{\omega C} \to C = \left[\frac{R}{Q}\omega\right]^{-1} = \left[\frac{R}{Q}2\pi f_{\text{res}}\right]^{-1} = [122 \cdot 2\pi \cdot 718 \cdot 10^6]^{-1} = 1.8 \,\text{pF} \\ 7. \ R &= \frac{V^2}{2P} \to V = \sqrt{2PR} = \sqrt{2 \cdot 10 \cdot 488 \cdot 10^3} = 3.1 \,\text{kV} \\ k^2 &= \frac{R}{R_{\text{in}}} \to k = \sqrt{\frac{R}{R_{\text{in}}}} = \sqrt{\frac{488 \cdot 10^3}{50}} = 98.8 \\ 8. \ \delta &= \sqrt{\frac{2}{\omega \sigma \mu}} = \sqrt{\frac{2}{2\pi f_{\text{res}} \sigma \mu}} = \frac{2}{2\pi 718 \cdot 10^6 58 \cdot 10^6 4\pi \cdot 10^{-7}} = 2.5 \,\mu\text{m} \\ Q &= \frac{a}{\delta} \left[1 + \frac{a}{h}\right]^{-1} = \frac{160 \cdot 10^{-3}}{2.5 \cdot 10^{-6}} \left[1 + \frac{160}{105.2}\right]^{-1} = 25746 \\ R &= \frac{R}{Q}Q = 122 \cdot 25746 = 3.1 \,\text{M}\Omega \\ R &= \frac{V^2}{2P} \to V = \sqrt{2PR} = \sqrt{2 \cdot 10 \cdot 3.1 \cdot 10^6} = 7.9 \,\text{kV} \end{split}$$

2 Decibel

Question 4

The solutions are printed in bold font:

Voltage ratio	Power ratio	dB
3.1623	10	10
10	100	20
100	10000	40

The solutions are printed in bold font:

dBm (50 Ω)	RMS Voltage (50 Ω)	milli Watt
0	0.224 V	1
+ 30	7.1 V	1000
- 60	0.224 mV	10 ⁻⁶
+ 20	2.23 V	100

To determine the RMS Voltage, the following relations can be used: $P = U \cdot I$, $I = U/R \rightarrow P = U^2/R \rightarrow U = \sqrt{P \cdot R}$

3 Multiple choice

Question 6

- 1. How will the resonant frequency f_{res} of the E_{010} (TM₀₁₀) mode of a pill box cavity change if height of the cavity is doubled? (check 1)
 - \circ The f_{res} decreases by a factor 2
 - \circ The f_{res} decreases by a factor $\sqrt{2}$
 - \circ The f_{res} increases by a factor 2
 - \circ The f_{res} increases by a factor $\sqrt{2}$
 - \circ The f_{res} will not change The resonance frequency is only dependent on the radius for this mode.
- 2. A critically coupled aluminum pill-box cavity is driven by an RF generator with an output power of 100 kW. How much power would be dissipated by the cavity if it were made of silver? $\sigma_{\text{Aluminium}} = 38 \cdot 10^6 \text{ S/m}$, $\sigma_{\text{Silver}} = 63 \cdot 10^6 \text{ S/m}$. Note: the silver cavity would also be critically coupled (check 1)

 \circ The power dissipation decreases by a factor $\sqrt{\frac{\sigma_{\text{Aluminium}}}{\sigma_{\text{Silver}}}}$

• The power dissipation increases by a factor $\sqrt{\frac{\sigma_{\text{Aluminium}}}{\sigma_{\text{Silver}}}}$

- The power dissipation will not change Critical coupling is independent of the material.
- 3. Calculate the minimal thickness of a copper shielding box if we want to allow less than 1% of 50 Hz currents flowing in the internal side of the box walls. $\sigma_{\text{Copper}} = 58 * 106 \text{ S/m}, \mu = \mu_0 \mu_r$,
 - $=4\pi\cdot 10^{-7}\,\text{Vs/Am},<1\%\approx 5$ sigma (check 1)
 - \circ 46.7 mm δ = 9.3 mm at 50 Hz which corresponds to $1\sigma \rightarrow 5\sigma = 5 \cdot 9.3 \cdot 10^{-6} = 46.7$ mm
 - $\circ 4.67\,\mathrm{mm}$
 - $\circ~0.46\,\mathrm{mm}$
 - $\circ~0.046~\rm{mm}$
- 4. A rectangular waveguide has a width of a = 10 cm. (check 2)
 - \circ The mode TE₁₀ or H₁₀ has a cutoff frequency of 3 GHz
 - \circ The mode TE₁₀ or H₁₀ has a cutoff frequency of 1.5 GHz $10 \text{ cm} = \frac{\lambda}{2} \rightarrow f_{\text{res}} = \frac{c}{\lambda} = \frac{3 \cdot 10^8}{20 \cdot 10^{-2}} = 1.5 \text{ GHz}$
 - The electric field is parallel to the side with the larger dimensions
 - The electric field is orthogonal to the side with the larger dimensions see cross section pictures
- 5. Which mode is the fundamental mode (lowest cut-off frequency) in a cylindrical waveguide of circular cross-section without inner conductor? (check 1)
 - **TE** separation condition/mode chart
 - ∘ TEM
 - $\circ TM$

6. Which mode is the fundamental mode in a cylindrical waveguide with inner conductor (coaxial line)? (check 1)

 $\circ \, TE$

 \circ **TEM** not simply connected cross section, thus electrostatic potential between inner and outer conductor possible

 \circ TM

7. Adding capacitive loading to a cavity (check 1)

 \circ lowers the resonance frequency $~~f_{res}\propto \frac{1}{\sqrt{C}}\rightarrow C\uparrow\Leftrightarrow f_{res}\downarrow$

- \circ does not affect the resonance frequency
- \circ increases the resonance frequency
- 8. Advantages of a nose cone cavity compared to an ordinary pill box cavity of same dimension (check 1)
 - o Smaller skin depth
 - Higher R/Q field concentration near nose cone increases R/Q

o Higher Q

9. Superconducting cavities usually do not have nose cones because (check 2)

o Superconductors are expensive, so don't waste them for nose cones

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\circ Nose cones are sensitive to multipactoring, which causes excessive heating and must therefore be avoided
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• The shunt impedance is so high that it can't be increased any more by changing the geometry

- Superconductors are sensitive to high electric field around the nose cones
- 10. When doing numerical simulations, geometrical symmetries are exploited in order to (check 2)

 \circ ensure convergence of the simulation algorithms for resonant structures

- reduce calculation time
- account for the transit time factor
- rule out certain higher order modes
- 11. The GSM standard specifies a minimum sensitivity requirement of about $-100 \,\text{dBm}$, while the maximum output power is in the order of 1 W. This corresponds to how many orders of magnitude in power? (Exact values: $-102 \,\text{dBm}$ minimum sensitivity, 1 to 5 W maximum output power) (check 1)

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o 5
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 $\circ 8$

 \circ 13 $-100 \text{ dBm} = 10^{-10} \text{ for mW}, 1 \text{ mW} = 10^{-3} \text{ W} \rightarrow 13 \text{ orders of magnitude}$

12. When you cover then antenna of your mobile with your hand while using it, the attenuation caused is in the order of 20 dB. Human tissue is a rather good absorber, so you can neglect reflections for this calculation. How many percent of the mobile's output power stay in the head and hand? (check 1)

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\circ 9

\circ 99 −20 dB = 10<sup>-2</sup> = 0.01 = 1% goes through → 99% are absorbed

\circ 99.99
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4 Resonant circuits and impedance plane

Question 7

1.
$$\omega_{\text{res}} = \frac{1}{\sqrt{\text{LC}}} = \frac{1}{\sqrt{10^{-7} \text{ m}^2 \text{ kg s}^{-2} \text{ A}^{-2} \cdot 10^{-11} \text{ s}^4 \text{ A}^2 \text{ m}^2 \text{ kg}^{-1}}} = \frac{1}{\sqrt{10^{-18}}} \text{ s}^{-1} = 1 \text{ GHz} \rightarrow \text{f} = \frac{1}{2\pi} \cdot \omega$$

 $\frac{\text{R}}{\text{Q}} = \omega \cdot \text{L} \rightarrow \text{Q} = \frac{\text{R}}{\omega \text{L}} = \frac{10^3 \text{ kg m}^2 \text{ s}^{-3} \text{ A}^{-2}}{10^9 \text{ s}^{-1} \cdot 10^{-7} \text{ m}^2 \text{ kg s}^{-2} \text{ A}^{-2}} = 10$
 $\text{Q} = \frac{f_{\text{res}}}{\Delta \text{f}} \rightarrow \Delta \text{f} = \frac{f_{\text{res}}}{\text{Q}} = \frac{159 \cdot 10^6}{10} = 15.9 \text{ MHz}$
 $\text{Q} = \frac{\omega_{\text{res}}}{\Delta \omega} \rightarrow \Delta \omega = \frac{\omega_{\text{res}}}{\text{Q}} = 100 \text{ MHz}$

2. To sketch the circuits in either plane, we calculate the **admittances** for certain 'strategic' frequencies:

$$\omega = 0$$
:

$$\begin{array}{ll} Z_C=-j\,\frac{1}{\omega\,C}=-j\,\infty & Y_C=j\,\frac{1}{\infty}=j\,0\\ Z_L=j\,\omega\,L=j\,0 & Y_L=-j\,\frac{1}{0}=-j\,\infty\\ Z_R=10^3 & Y_R=10^{-3}\\ \text{this leads to:} \end{array}$$

$$\begin{split} \mathbf{Y}_{tot} &= \mathbf{Y}_{C} + \mathbf{Y}_{L} + \mathbf{Y}_{R} = \mathbf{j} \, 0 - \mathbf{j} \, infty + 10^{-3} = 10^{-3} - \mathbf{j} \, infty \\ \mathbf{Z}_{tot} &= \frac{1}{\mathbf{Y}_{tot}} = \frac{1}{10^{-3} - \mathbf{j} \, \infty} = \frac{10^{-3} + \mathbf{j} \, \infty}{10^{-6} + \infty^{2}} = \frac{10^{3}}{\infty^{s}} + \mathbf{j} \, \frac{\infty}{\infty^{2}} = 0 \end{split}$$

 $\omega = \infty$:

after applying the same principle as above, we get:

$$\mathbf{Y}_{tot} = 10^{-3} + \mathbf{j} \,\infty$$

 $Z_{tot} = 0$

 $\omega = \omega_{\text{res}}$:

$$\begin{array}{ll} Z_C = -j \, \frac{1}{\omega C} = - \, j \, \frac{1}{10^9 \cdot 10^{-11}} = - \, j \, 100 & Y_C = j \, \frac{1}{100} = j \, 0.01 \\ Z_L = j \, \omega \, L = j \, 10^9 \cdot 10^{-7} = j \, 100 & Y_L = - \, j \, 0.01 \\ Z_R = 10^3 & Y_R = 10^{-3} \end{array}$$

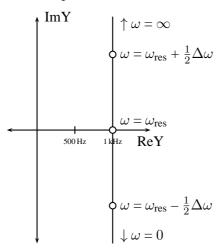
this leads to:

$$\begin{split} \mathbf{Y}_{\text{tot}} &= \mathbf{Y}_{\text{C}} + \mathbf{Y}_{\text{L}} + \mathbf{Y}_{\text{R}} = \mathbf{j} \, 100 - \mathbf{j} \, 100 + 10^{-3} = 10^{-3} \\ \mathbf{Z}_{\text{tot}} &= \frac{1}{\mathbf{Y}_{\text{tot}}} = 10^{3} \\ \omega &= \omega_{\text{res}} \pm \frac{\Delta \mathbf{f}}{2} : \end{split}$$

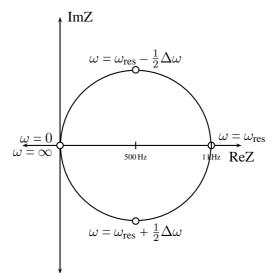
 $Y_{tot} = 10^{-3} \pm j \, 0.01$

 $Z_{tot} = 0.5 \cdot 10^3 \mp \ j \, 0.5 \cdot 10^3$

plotting the circuit in the admittance plane looks like:



3. in the impedance plane:



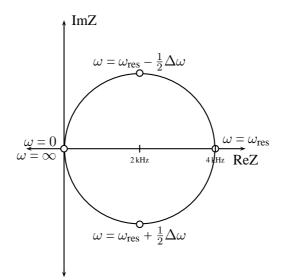
1. $\omega_{\text{res}} = 2\pi \, \text{f}_{\text{res}} = 100 \, \text{MHz}$

$$\frac{R}{Q} = \omega_{\text{res}} L \to L = \frac{R}{Q} \cdot \frac{1}{\omega_{\text{res}}} = 2 \,\mu\text{H}$$
$$\omega_{\text{res}} = \frac{1}{\sqrt{LC}} \to C = \frac{1}{\omega^2 L} = 50 \,\text{pF}$$

2. $\mathbf{Q} = \frac{\omega_{\text{res}}}{\Delta \omega} \rightarrow \Delta \omega = \frac{\omega_{\text{res}}}{\mathbf{Q}} = 5 \text{ MHz}$

Frequency	Admittance	Impedance
0	$-j\infty$	0
$\omega_{ m res} - rac{\Delta \omega}{2} \ \omega_{ m res}$	$\begin{array}{c} 0.25 \cdot 10^{-3} - \mathrm{j} 0.25 \cdot 10^{-3} \\ 0.25 \cdot 10^{3-} \end{array}$	$2 \cdot 10^3 + j 2 \cdot 10^3$
$\omega_{\rm res}$	$0.25 \cdot 10^{3-}$	$4 \cdot 10^3$
$\omega_{\rm res} + \frac{\Delta \omega}{2}$	$0.25 \cdot 10^{-3} + j 0.25 \cdot 10^{-3}$	$2 \cdot 10^3 - j 2 \cdot 10^3$
∞ –	j∞	0

Sketching this in the impedance plane, we get:



5 Transmission lines and striplines

Question 9

1.
$$Z = \sqrt{\frac{L'}{C'}} \rightarrow L' = Z^2 C'$$

 $v = \frac{1}{\sqrt{L'C'}} \rightarrow L' = \frac{1}{v^2 C'}$
 $\rightarrow \frac{1}{v^2 C'} = Z^2 C' \rightarrow C' = \frac{1}{vZ} = \frac{1}{0.5 \cdot 3 \cdot 10^8 \cdot 75} = 88.9 \text{ pF}$
 $\rightarrow L' = Z^2 C' = 75^2 \cdot 88.9 \cdot 10^{-12} = 500 \text{ nH}$
2. $v = \frac{c}{\mu_r \epsilon_r} \rightarrow \epsilon_r = \left[\frac{v^2}{c^2}\mu_r\right]^{-1} = \frac{0.5 \cdot c^s}{c^2} = 4$
3. $Z = \sqrt{\frac{\mu_r}{\epsilon_r}} 60 \ln\left(\frac{R}{r}\right) \rightarrow r = R \cdot e^{-\frac{Z}{60}\sqrt{\frac{\epsilon_r}{\mu_r}}} = 10 \cdot e^{\frac{75}{60}\frac{1}{\sqrt{4}}} = 0.82 \text{ mm}$

Question 10 1. $\mathbf{Z} = \frac{60\Omega}{\sqrt{\epsilon_r}} \cdot \ln\left[\frac{1.9b}{0.8w+t}\right] = \frac{60\Omega}{\sqrt{4}} \cdot \ln\left[\frac{1.9\cdot15}{0.8\cdot3.1+0.02}\right] = 73 \,\Omega$

2.
$$Z = \sqrt{\epsilon_r} \frac{1}{C'c} \rightarrow C' = \sqrt{\epsilon_r} \frac{1}{Zc} = \sqrt{4} \frac{1}{73 \cdot 3 \cdot 10^8} = 91.3 \text{ pF/ul}$$

 $Z = \sqrt{\frac{L'}{C'}} \rightarrow L' = Z^2 C' = 73^2 \cdot 91.3 \cdot 10^{-12} = 486.7 \text{ nH/ul}$
3. $v = \frac{c}{\sqrt{\epsilon_r}} = \frac{c}{\sqrt{4}} = 0.5 \text{ c}$

Question 11
1.
$$Z = \sqrt{\epsilon_r} \frac{1}{C'c} \rightarrow C' = \sqrt{\epsilon_r} \frac{1}{Zc} = \sqrt{2.1} \frac{1}{50 \cdot 3 \cdot 10^8} = 96.6 \text{ pF/ul}$$

 $Z = \sqrt{\frac{L'}{C'}} \rightarrow L' = Z^2 C' = 50^2 \cdot 96.6 \cdot 10^{-12} = 241.5 \text{ nH/ul}$
2. $v = \frac{c}{\sqrt{\epsilon_r}} = \frac{c}{\sqrt{2.1}} = 0.69 \text{ c}$

6 S-parameters

Question 12

Component	Isolator	Circulator	Transmission line, length $\lambda/2$	3 dB attenuator
S-matrix	S_2	S_4	S_3	S_1

Question 13

Transmission line:

$$S_1 = \frac{1}{\sqrt{2}} \begin{bmatrix} 0 & \mathrm{e}^{-\mathrm{j}\beta l} \\ \mathrm{e}^{-\mathrm{j}\beta l} & 0 \end{bmatrix} = \begin{bmatrix} 0 & \mathrm{e}^{-\mathrm{j}\frac{2\pi}{\lambda}l} \\ \mathrm{e}^{-\mathrm{j}\frac{2\pi}{\lambda}l} & 0 \end{bmatrix} = \begin{bmatrix} 0 & \mathrm{e}^{-\mathrm{j}\frac{2\pi}{\lambda}\frac{\lambda}{4}} \\ \mathrm{e}^{-\mathrm{j}\frac{2\pi}{\lambda}\frac{\lambda}{4}} & 0 \end{bmatrix} = \begin{bmatrix} 0 & \mathrm{e}^{-\mathrm{j}\frac{\pi}{2}} \\ \mathrm{e}^{-\mathrm{j}\frac{\pi}{2}} & 0 \end{bmatrix} = \begin{bmatrix} 0 & -\mathrm{j} \\ -\mathrm{j} & 0 \end{bmatrix}$$

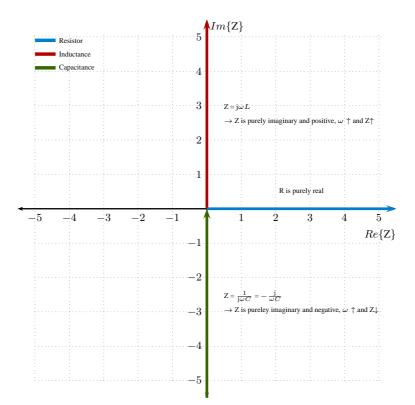
Amplifier:

$$S_2 = \begin{bmatrix} 0 & 0\\ \sqrt{10} & 0 \end{bmatrix} = \begin{bmatrix} 0 & 0\\ 3.16 & 0 \end{bmatrix}$$
(1)

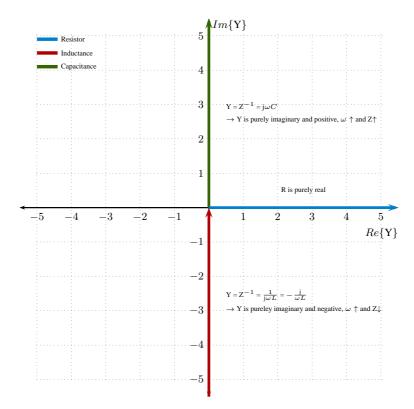
7 Impedances and Smith chart

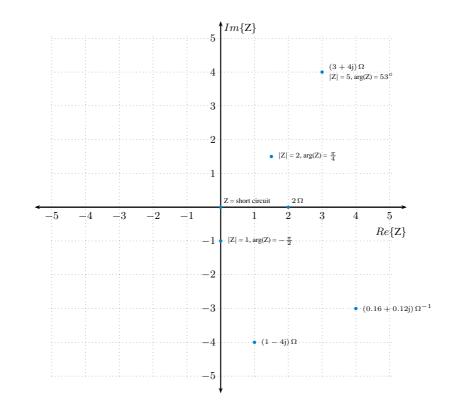
Question 14

1. Impedance plane

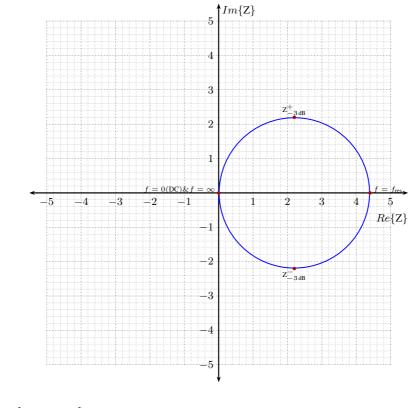


2. Admittance plane





Question 16



 $f_{\rm res} = \frac{1}{2\pi} \frac{1}{\sqrt{LC}} = \frac{1}{2\pi} \frac{1}{\sqrt{150 \cdot 10^{-9} \cdot 80 \cdot 10^{-12}}} = 45.9 \, \rm MHz$

- 1. At resonance $Im\{\mathbf{Z}\} = 0 \rightarrow f_{\text{res}} = f_7 = 105.2 \text{ MHz}$
- 2. Lower 3 dB point: $\arg\{Z\} = 45^{\circ} \rightarrow f^{-}_{-3dB} = f_2$

Upper 3 dB point: $\arg\{Z\} = -45^{\circ} \rightarrow f^+_{-3dB} = f_5$

 $\mathrm{BW} = f_5 - f_2 = 300\,\mathrm{kHz}$

- 3. The resonant circuit is a parallel resonator with RLC
- 4. $R = Z(f_7) = 230 \,\mathrm{k}\Omega$
- 5. The locus of impedance is a vertical line in the Y-plane with $\text{Re}\{Y\} = 4.35 \,\mu\text{S}$ and $|Y_{-3dB}| = 6.15 \,\mu\text{S}$

6.
$$Q = \frac{f_{\text{res}}}{\Delta f_{\text{res}}} = \frac{105.2 \cdot 10^6}{300 \cdot 10^3} = 350$$

 $\frac{R}{Q} = \omega L \rightarrow L = \frac{R}{Q} \frac{1}{\omega} = \frac{230 \cdot 10^3}{350} \frac{1}{2\pi 105.2 \cdot 10^6} = 994 \text{ nH}$
 $\frac{R}{Q} = \frac{1}{\omega C} \rightarrow C = \left[\frac{R}{Q}\omega\right]^{-1} = 2.3 \text{ pF}$

Question 18 - Question 20

Check your results with the online tool (Dellsperger)!