

Superconductivity for accelerators

- why bother?

Abolish Ohm's Law

- no power consumption
(although do need refrigeration power)
- high current density \Rightarrow compact windings, high gradients
- ampere turns are cheap, so don't need iron
(although often use it for shielding)

Consequences

- lower power bills
- higher magnetic fields mean reduced bend radius
 - \Rightarrow smaller rings
 - \Rightarrow reduced capital cost
 - \Rightarrow new technical possibilities
(eg muon collider)
- higher quadrupole gradients
 - \Rightarrow higher luminosity



Plan of the Lectures

1 Introduction to Superconductors

- critical field, temperature & current
- superconductors for magnets
- manufacture of superconducting wires
- high temperature superconductors HTS

2 Magnets, 'Training' & Fine Filaments

- coil shapes for solenoids, dipoles & quadrupoles
- engineering current density & load lines
- degradation & training minimum quench energy
- critical state model & fine filaments

3 Magnetization, Cables & AC losses

- filamentary superconductors and magnetization
- coupling between filaments \Rightarrow magnetization
- why cables, coupling in cables
- AC losses in changing fields

4 Quenching and Cryogenics

- the quench process
- resistance growth, current decay, temperature rise
- quench protection schemes
- cryogenic fluids, refrigeration, cryostat design

5 Practical Matters

- LHC quench protection
- current leads
- accelerator magnet manufacture
- some superconducting accelerators

Tutorial 1: Fine Filaments

- how filament size affects magnetization

Tutorial 2: Quenching

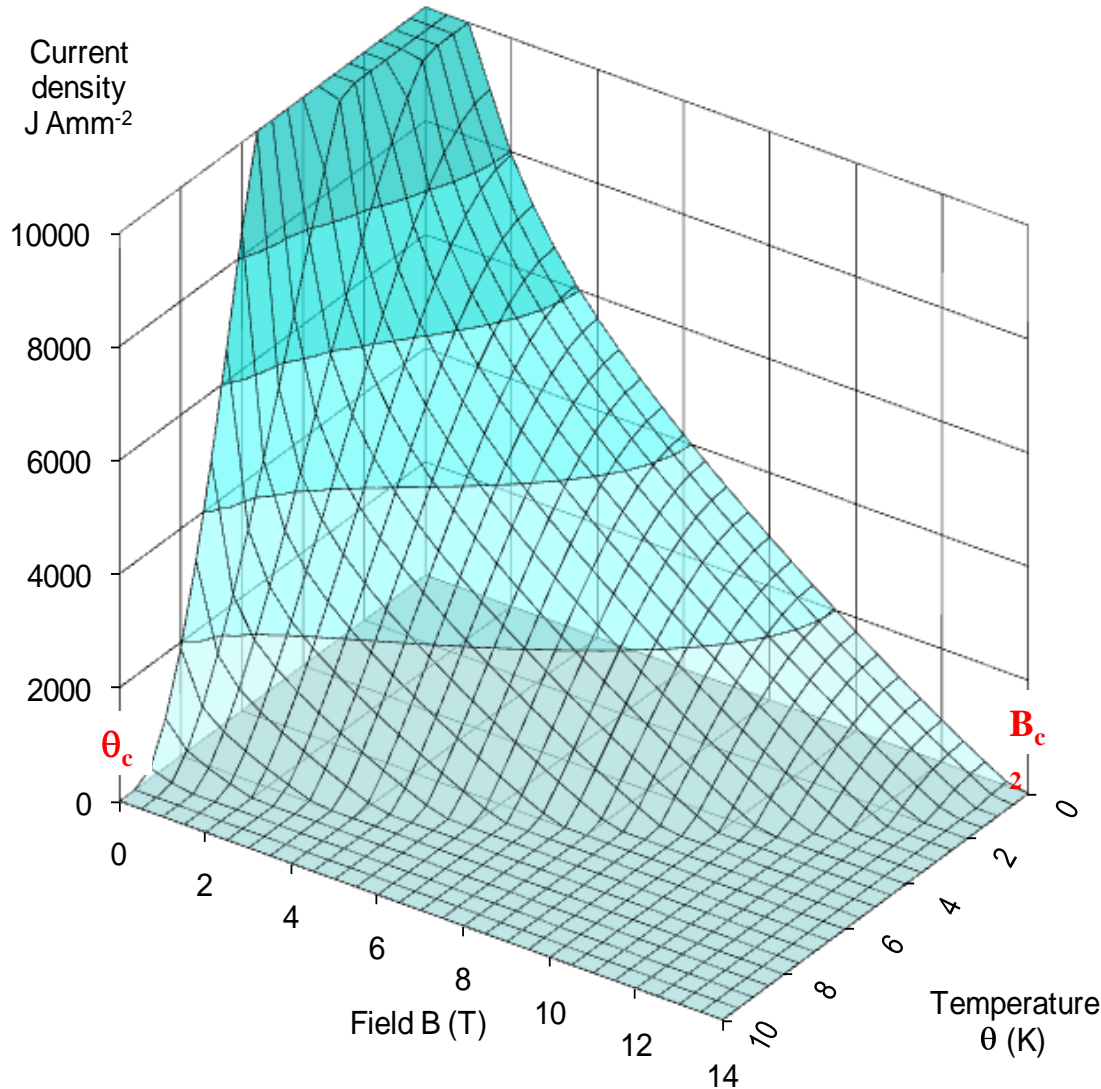
- current decay and temperature rise



*get a feel for the numbers,
bring a calculator*

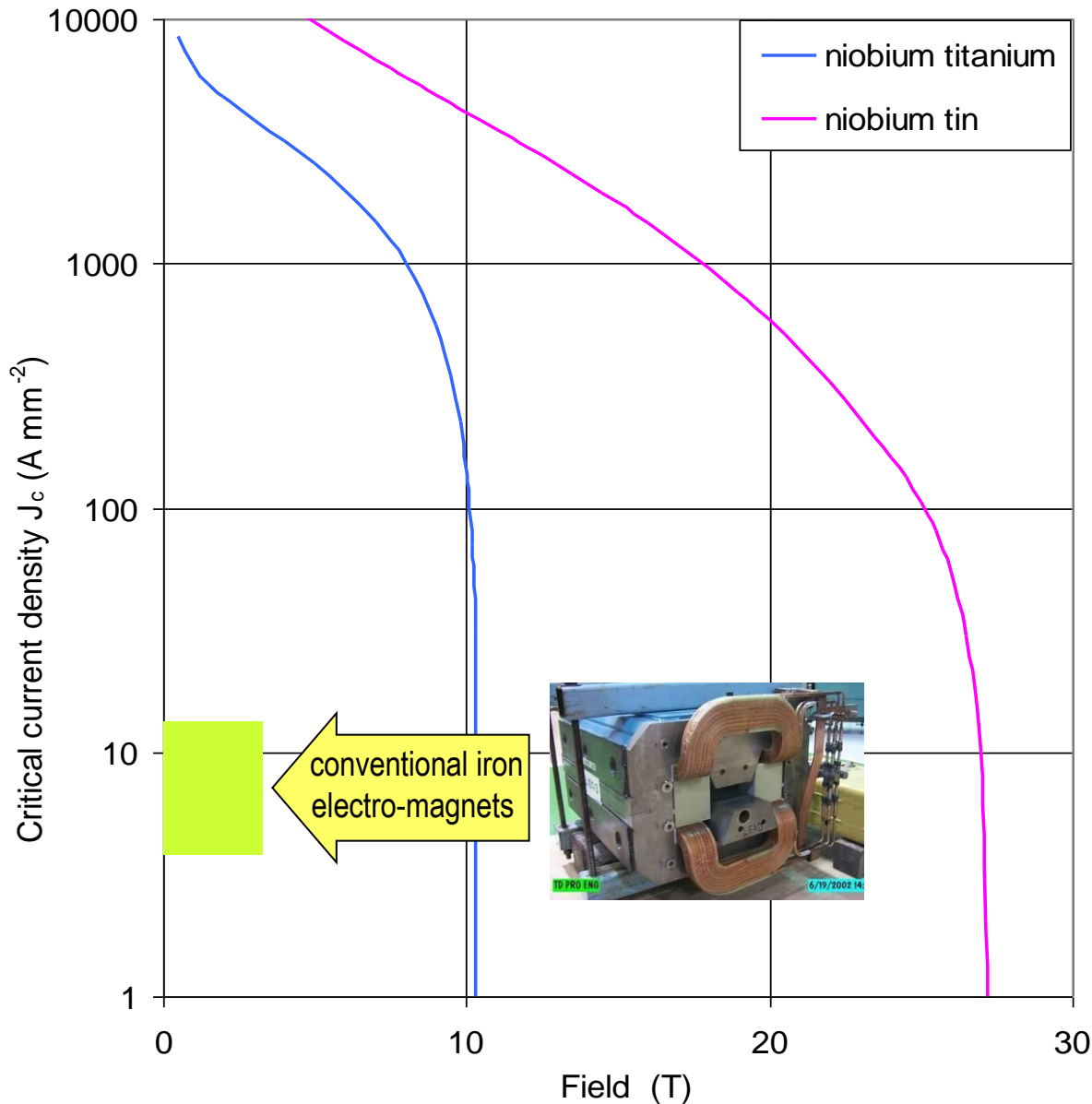
The critical surface of niobium titanium

- **NbTi** is the standard commercial ‘work horse’ of the superconducting magnet business



- **critical surface** is the boundary between superconductivity and normal resistivity in J, B, θ space
- superconductivity prevails everywhere below the surface, resistance everywhere above it
- upper critical field B_{c2} (at zero temperature and current)
- critical temperature θ_c (at zero field and current)
- B_{c2} and θ_c are characteristic of the alloy composition
- critical current density J_c depends on processing

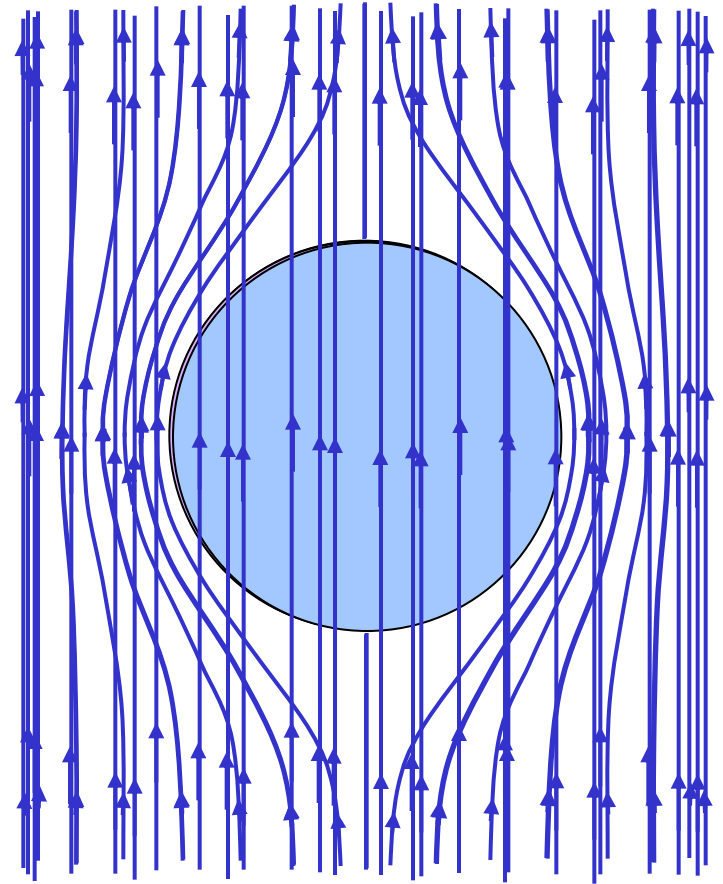
The critical line at 4.2K



- magnets usually work in boiling liquid helium, so the critical surface is often represented by a curve of current versus field at 4.2K
- niobium tin Nb₃Sn has a much higher performance than NbTi
- **but** Nb₃Sn is a brittle intermetallic compound with poor mechanical properties
- both the field and current density of both superconductors are way above the capability of conventional electromagnets

Two kinds of superconductor: type 1

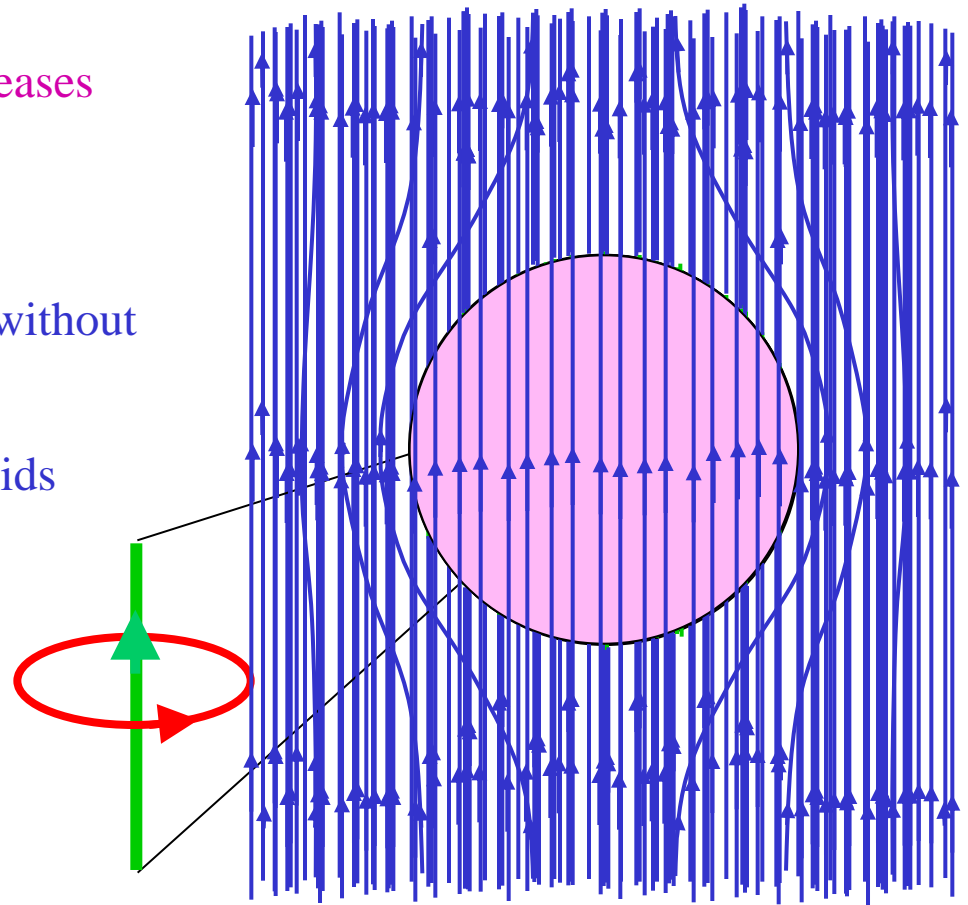
- the materials first discovered by Kammerlingh Onnes in 1911 - soft metals like lead, tin mercury
- sphere of metal at room temperature
- **apply magnetic field**
- **reduce the temperature - resistance decreases**
- **reduce the temperature some more - resistance decreases some more**
- at the critical temperature θ_c the field is pushed out - the **Meissner effect** - superconductivity!
- increase the field - field is kept out
- increase the field some more - superconductivity is extinguished and the field jumps in
- thermodynamic critical field B_c is trade off between **reducing** energy via condensation to superconductivity and **increasing** energy by pushing out field $\sim 0.1T$



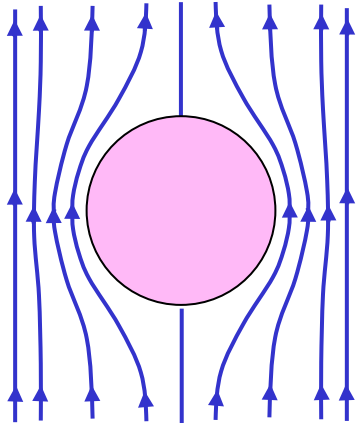
useless for magnets!

Two kinds of superconductor: type 2

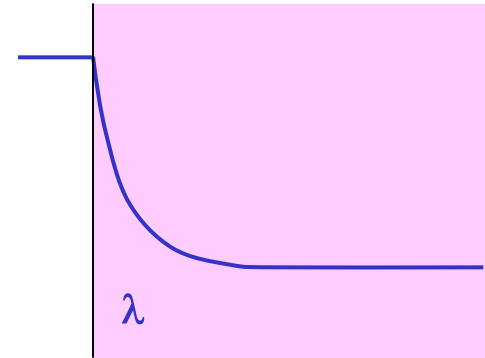
- apply magnetic field
- reduce the temperature - resistance decreases
- at the critical temperature θ_c the field is pushed out
- increase the field - field jumps back in without quenching superconductivity
- it does so in the form of quantized fluxoids
- lower critical field B_{c1}
- supercurrents encircle the resistive core of the fluxoid thereby screening field from the bulk material
- higher field \Rightarrow closer vortex spacing
- superconductivity is extinguished at the (much higher) upper critical field B_{c2}



Type 1 and type 2 superconductors

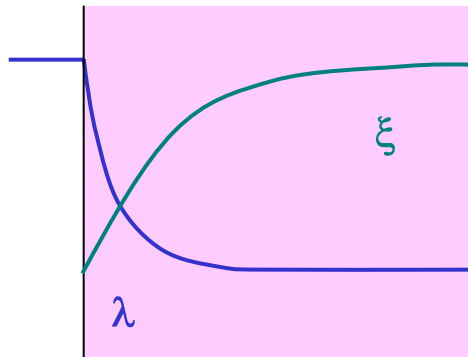


- Meissner effect is not total
- magnetic field penetrates a small distance λ
- the **London Penetration Depth**.

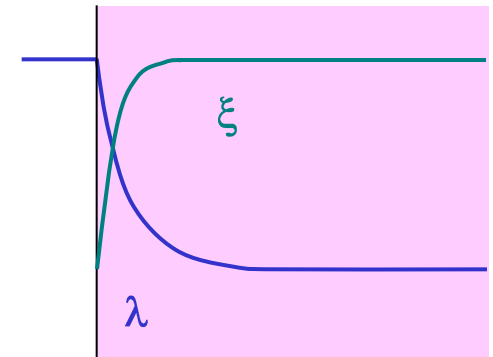


- another characteristic distance is the **coherence length** ξ - the minimum distance over which the electronic state can change from superconducting to normal
- theory of Ginsburg, Landau, Abrikosov and Gorkov **GLAG** defines the ratio $\kappa = \lambda / \xi$

if $\kappa < 1/\sqrt{2}$
material is
Type 1



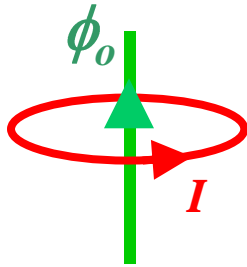
if $k > 1/\sqrt{2}$
material is
Type 2



Critical fields of type 2 superconductors

- recap thermodynamic critical field B_c
- lower critical field $B_{c1} = B_c / \kappa$
- above B_{c1} magnetic field penetrates as discrete quantized **fluxoids**

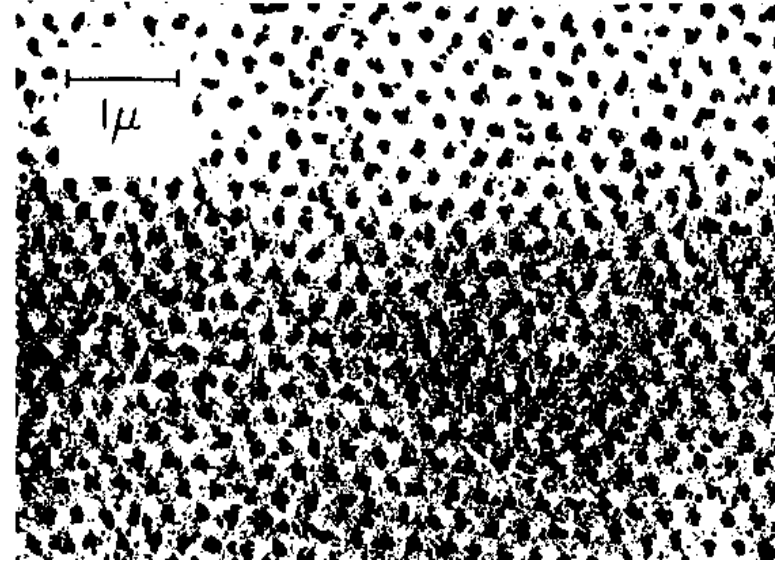
human hair
in earth's
magnetic
field $\sim 50\phi_0$



a fluxoid encloses flux

$$\phi_0 = \frac{h}{2e} = 2 \times 10^{-15} \text{ Wb}$$

h = Planck's constant
 e = electronic charge



**upper
critical field**

$$B_{c2} = \sqrt{2}\kappa B_c$$

in the
'dirty limit' $\kappa \approx 2.4 \times 10^6 \gamma^{\frac{1}{2}} \rho_n$

where ρ_n is the
normal state resistivity
**- best superconductors
are best resistors!**

thus the upper critical field

$$B_{c2} = 3.1 \times 10^3 \gamma \rho_n \theta_c$$

for NbTi: $\gamma \sim 900 \text{ J m}^{-3} \text{ K}^{-2}$ $\rho_n \sim 65 \times 10^{-8} \text{ W m}$ $\theta_c = 9.3 \text{ K}$ hence **$B_{c2} \sim 18.5 \text{ T}$**

Sommerfeld coefficient of electronic specific heat $C_e = \gamma\theta$

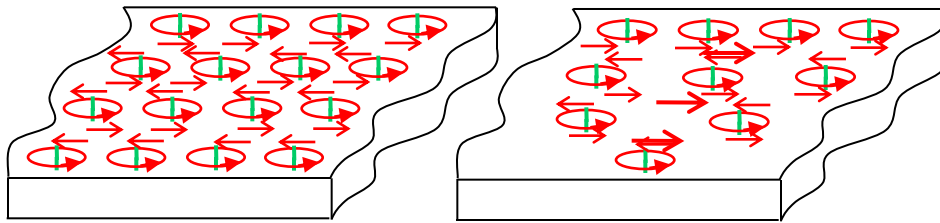
Critical current density: type 2 superconductors

- fluxoids consist of resistive cores with supercurrents circulating round them.

spacing between the fluxoids is:-

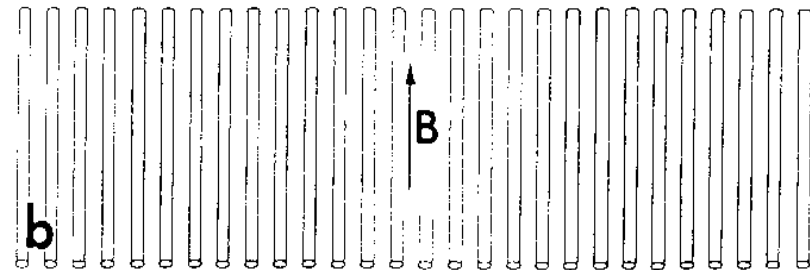
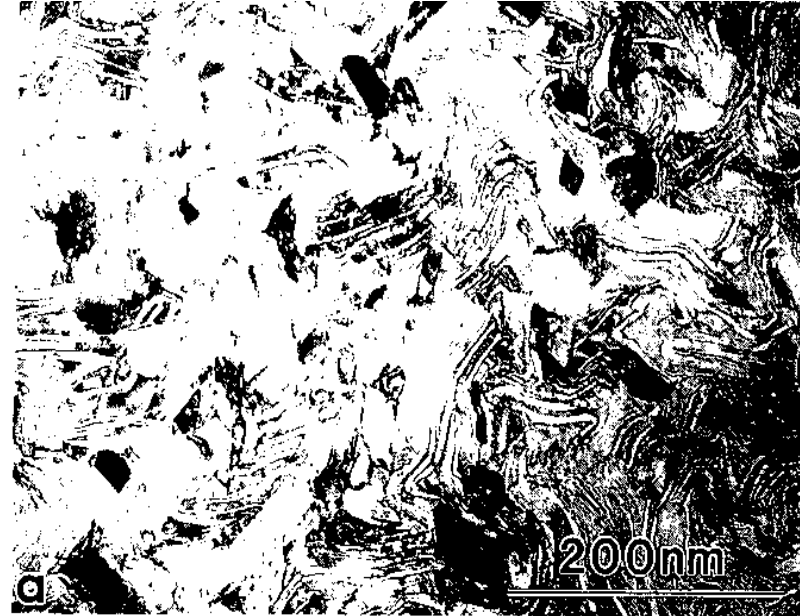
$$d = \left\{ \frac{2 \phi_0}{\sqrt{3} B} \right\}^{\frac{1}{2}} = 22nm \quad \text{at } 5T$$

- each fluxoid carries one unit of flux, so density of fluxoids = average field
uniform density \Rightarrow uniform field
 \Rightarrow zero J (because $\text{Curl } B = \mu_0 J$)
- to get a current density we must produce a **gradient** in the density of fluxoids



- fluxoids like to distribute uniformly
- so we must impose a gradient by inhomogeneities in the material, eg dislocations or precipitates

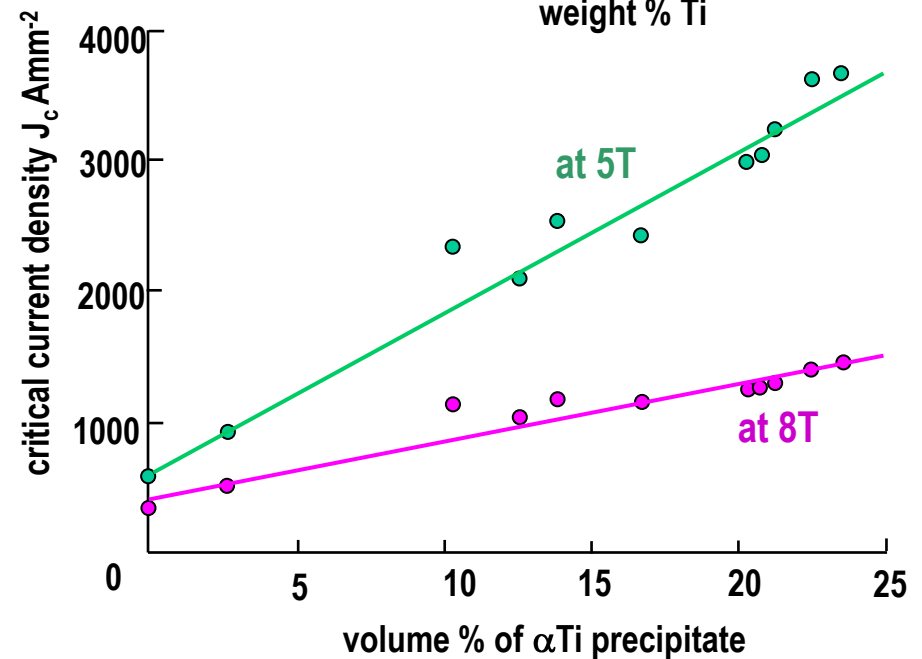
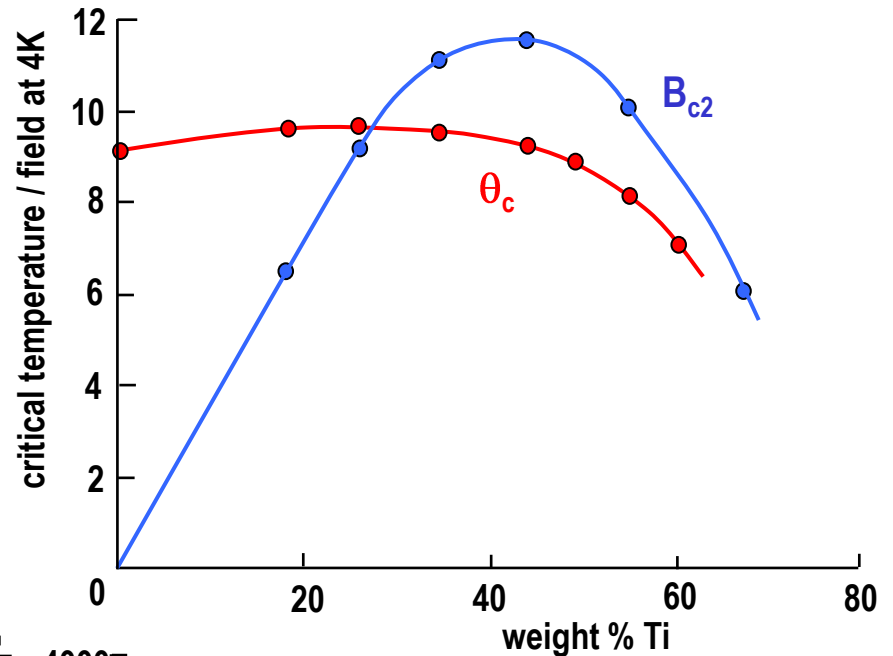
precipitates of α Ti in Nb Ti



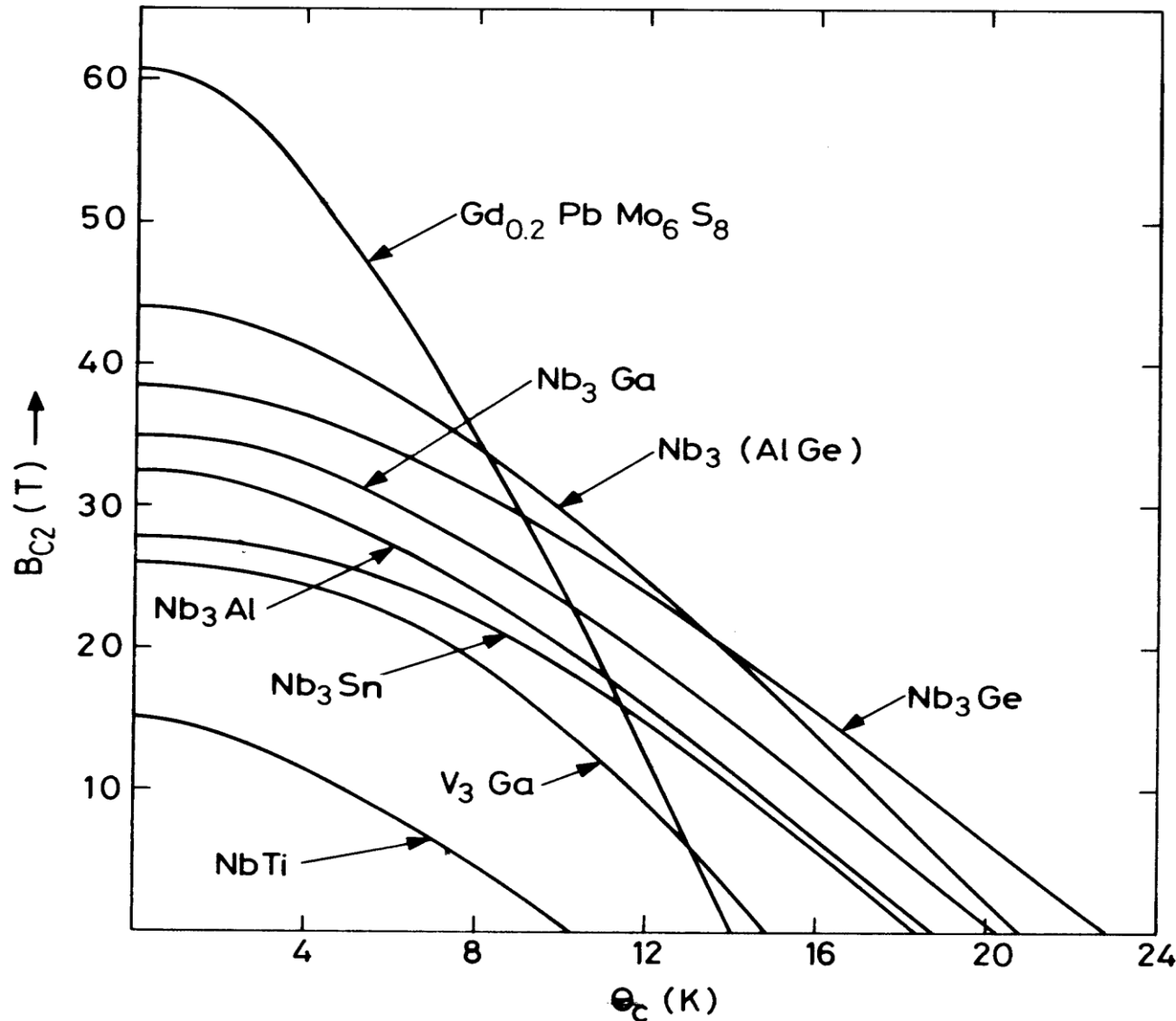
fluxoid lattice at 5T on the same scale

Critical properties

- **Critical temperature θ_c** : choose the right material to have a large energy gap or 'depairing energy'
property of the material
- **Upper Critical field B_{c2}** : choose a Type 2 superconductor with a high critical temperature and a high normal state resistivity
property of the material
- **Critical current density J_c** : mess up the microstructure by cold working and precipitation heat treatments
hard work by the producer



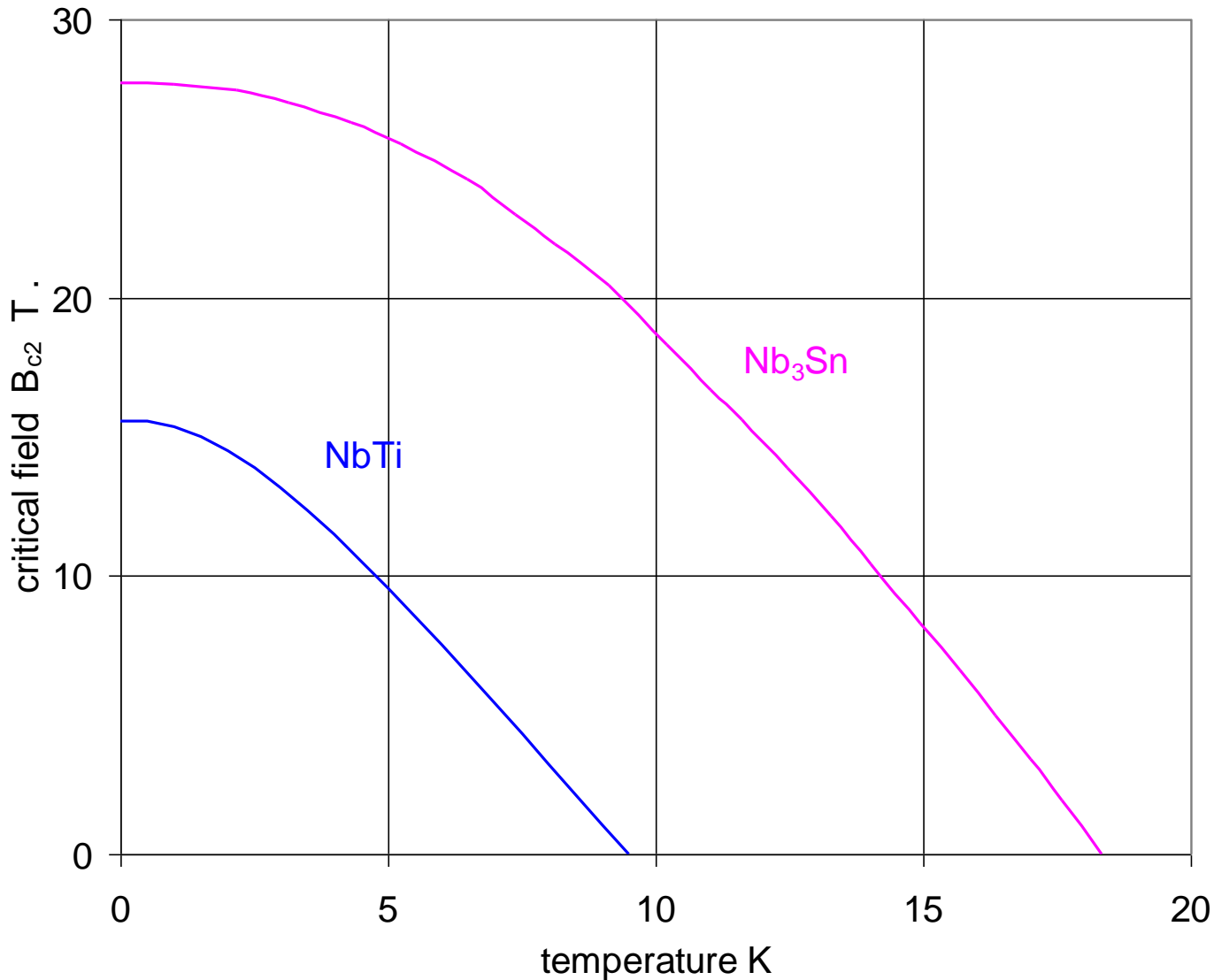
Critical field & temperature of metallic superconductors



Note: of all the metallic superconductors, only NbTi is ductile.

All the rest are brittle intermetallic compounds

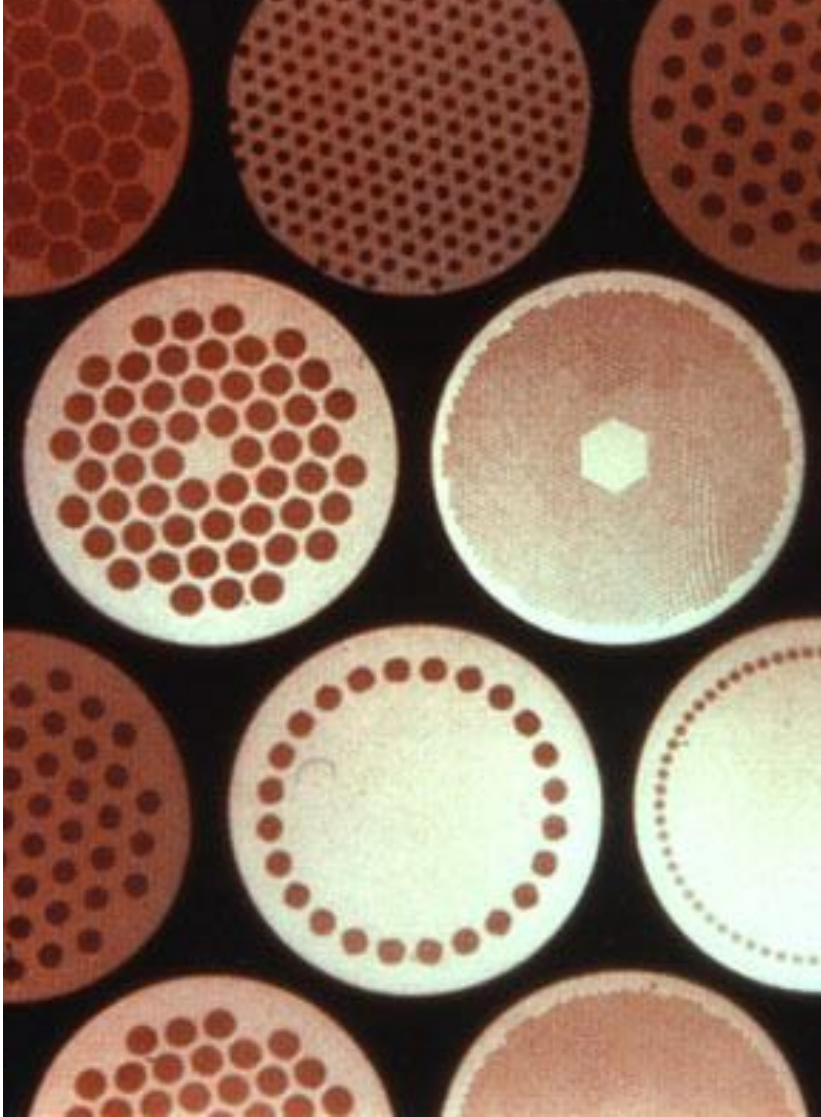
Critical field & temperature of metallic superconductors



To date, all superconducting accelerators have used NbTi.

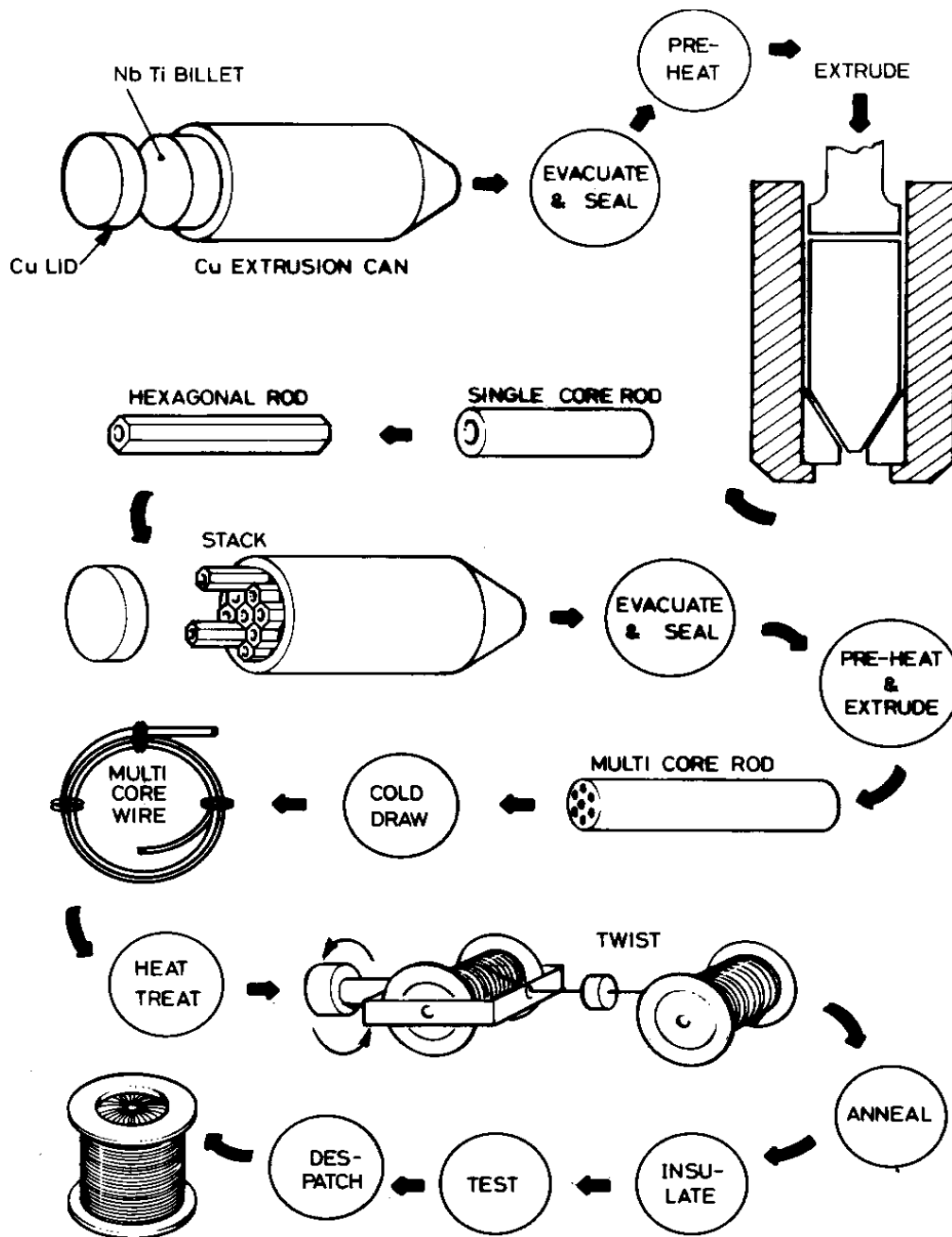
Of the intermetallics, only Nb₃Sn has found significant use in magnets

Practical wires for magnets



- some 40 years after its development, NbTi is still the most popular magnet conductor, with Nb₃Sn being used for special high field magnets and HTS for some developmental prototypes.
- for reasons that will be described later, superconducting materials are always used in combination with a good normal conductor such as copper
- to ensure intimate mixing between the two, the superconductor is made in the form of fine filaments embedded in a matrix of copper
- typical dimensions are:
 - wire diameter = 0.3 - 1.0mm
 - filament diameter = 10 - 60μm
- for electromagnetic reasons, the composite wires are twisted so that the filaments look like a rope (see Lecture 3)

NbTi manufacture



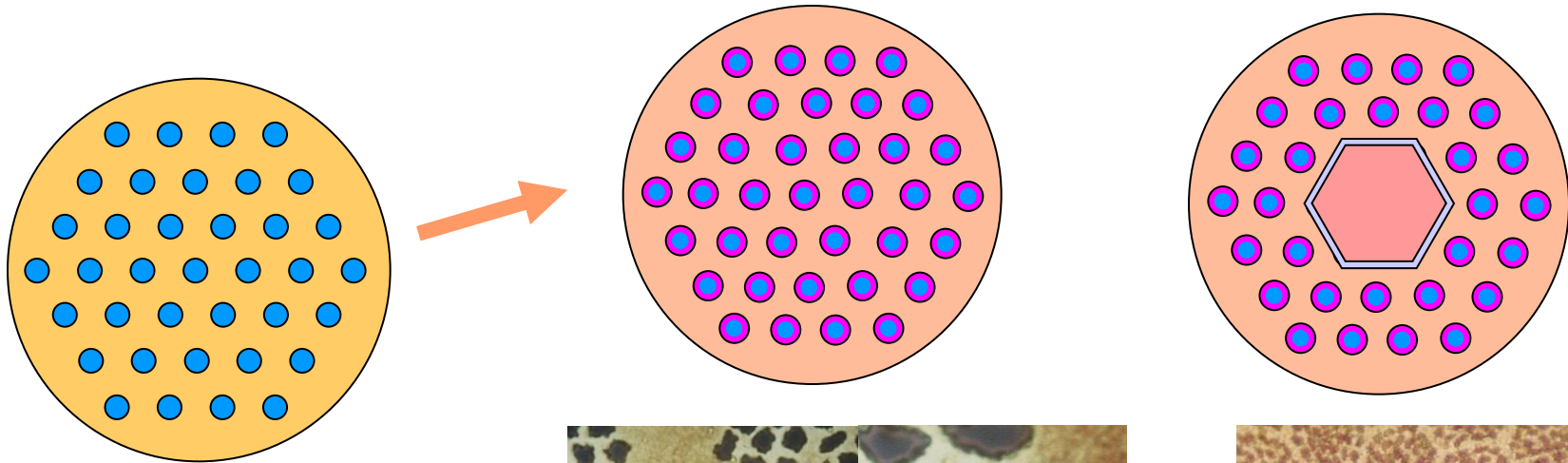
- vacuum melting of NbTi billets
- hot extrusion of the copper NbTi composite
- sequence of cold drawing and intermediate heat treatments to precipitate α Ti phases as flux pinning centres
- for very fine filaments, must avoid the formation of brittle CuTi intermetallic compounds during heat treatment
 - usually done by enclosing the NbTi in a thin Nb shell
- twisting to avoid coupling - see lecture 2

Filamentary Nb_3Sn wire via the bronze route

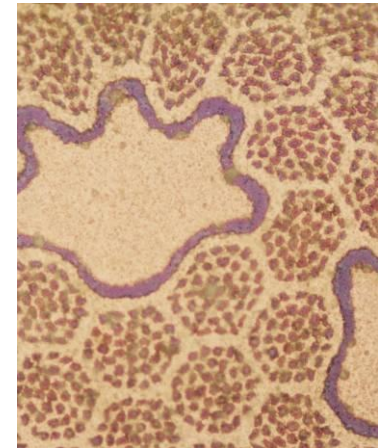
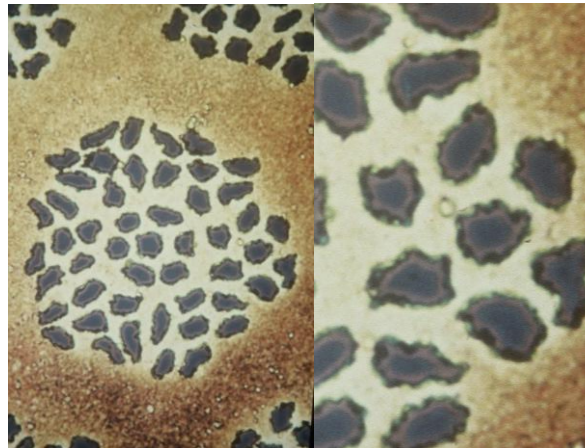
Nb_3Sn is a brittle material and cannot be drawn down. Instead must draw down pure niobium in a matrix of bronze (copper tin)

At final size the wire is heated ($\sim 700^\circ C$ for some days) tin diffuses through the Cu and reacts with the Nb to form Nb_3Sn

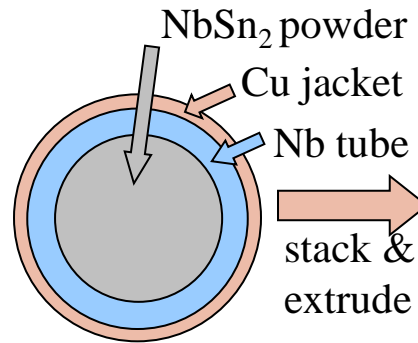
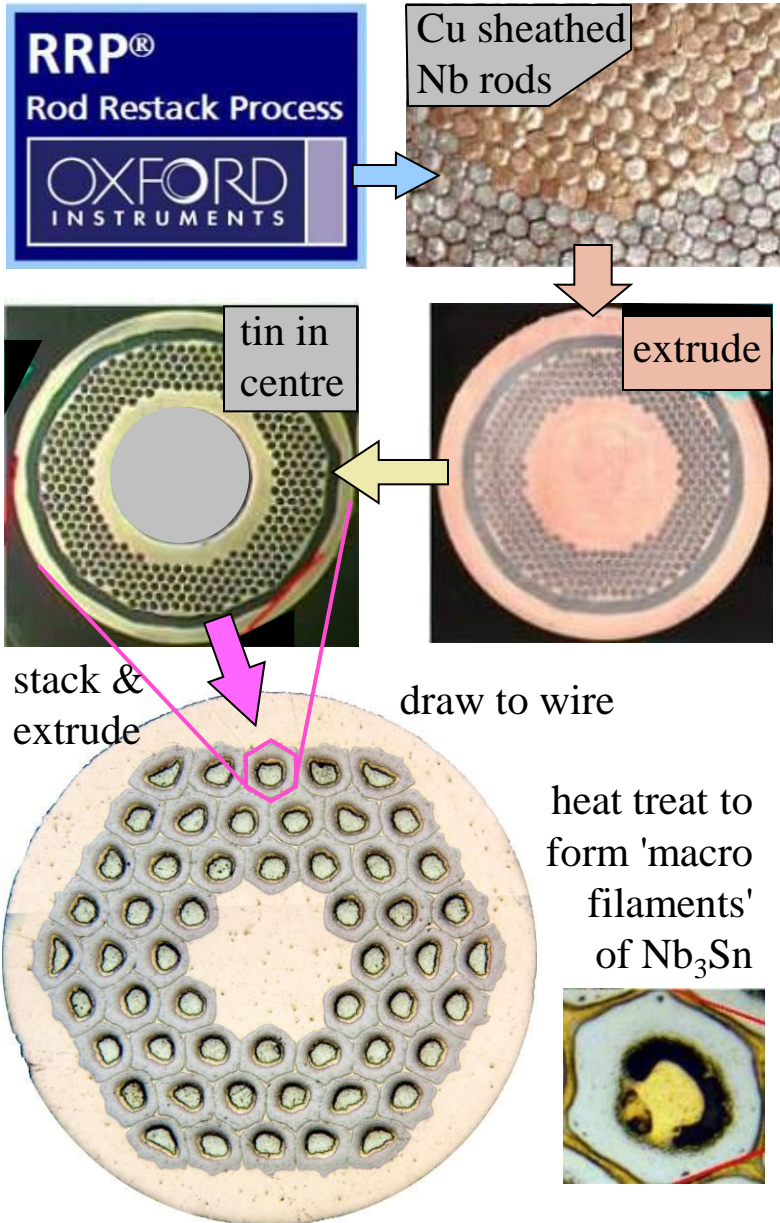
The remaining copper still contains $\sim 3wt\%$ tin and has a high resistivity $\sim 6 \times 10^{-8} \Omega m$. So include 'islands' of pure copper surrounded by a diffusion barrier



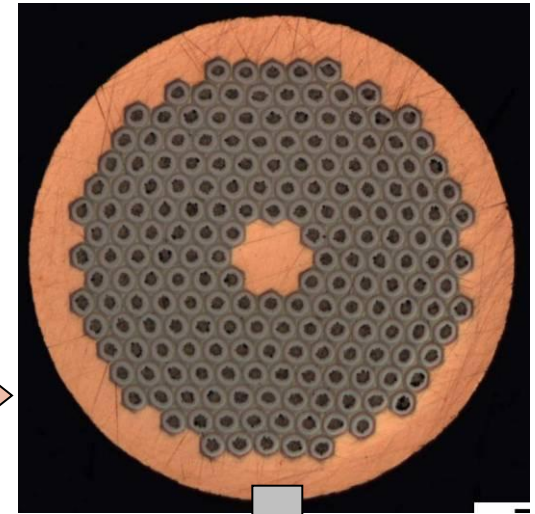
- *BUT maximum ductile bronze is $\sim 13wt\%$ tin,*
- *reaction slows at $\sim 3wt\%$*
- *so low engineering J_c*



Nb_3Sn with higher engineering J_c



Powder in tube PIT

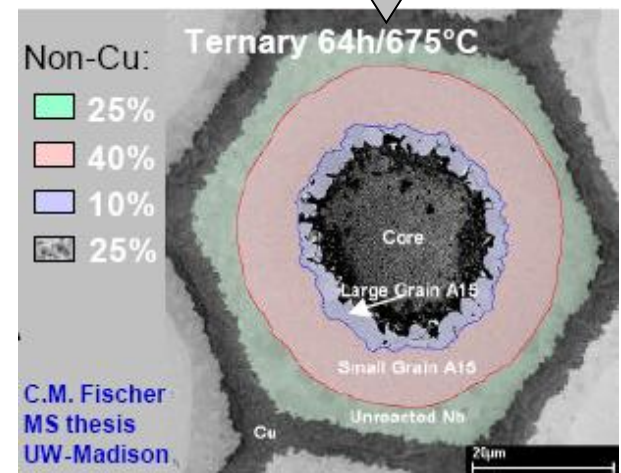


draw to wire

heat treat

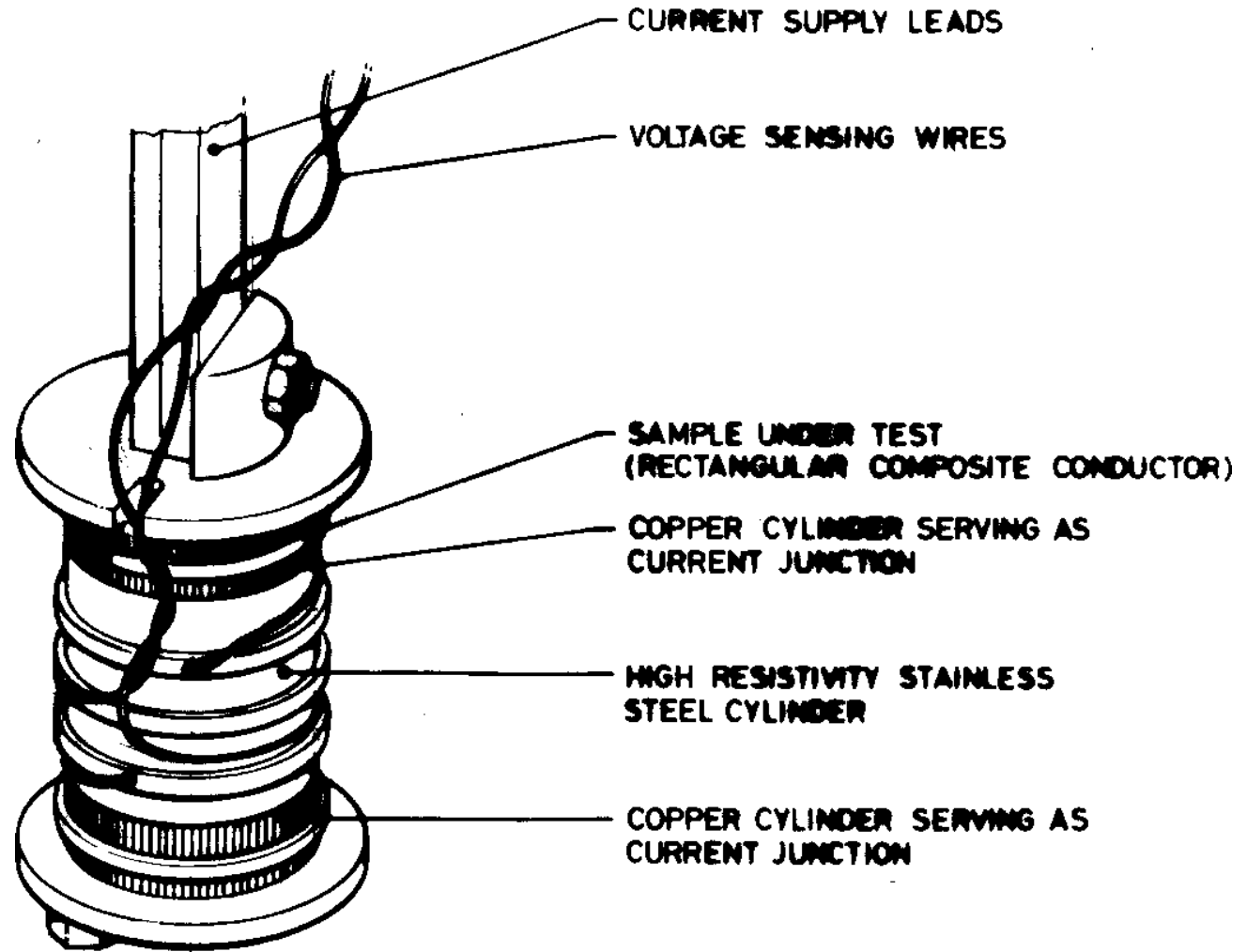
both make high J_{eng} (RRP is the highest)

but large filaments



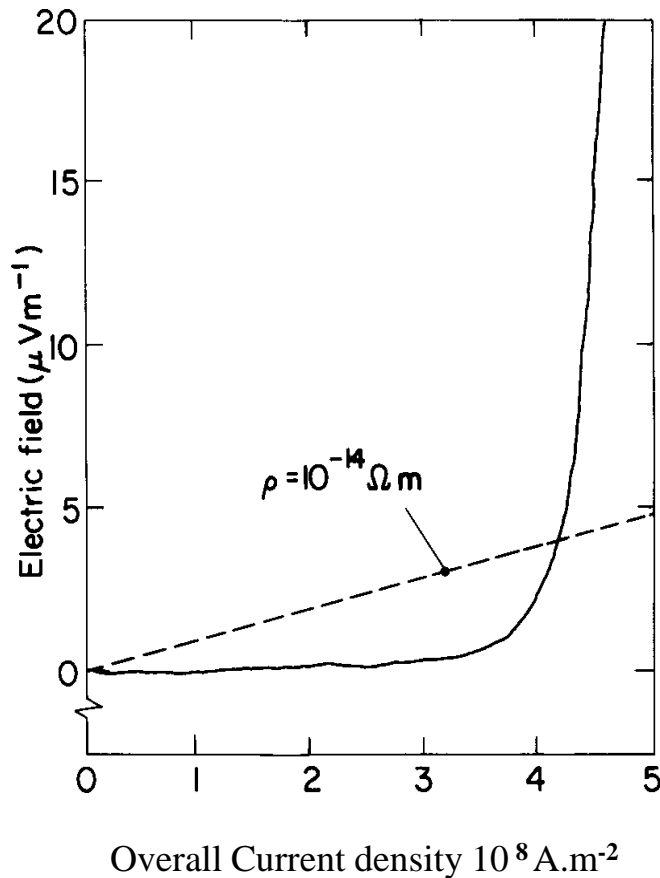
Measurement of critical current

- this sample holder is placed in the bore of a superconducting solenoid, usually in liquid helium boiling at 4.2K
- at each field level the current is slowly increased and voltage across the test section is measured



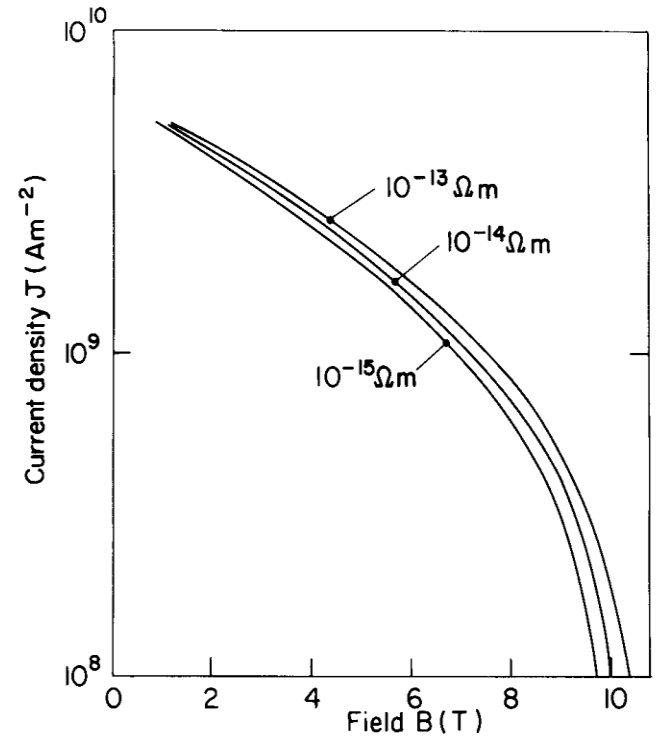
Resistive transition 1

When measured sensitively, the boundary between superconducting and resistive states is not sharp, but slightly blurred.



If we measure J_c with voltage taps across the sample, we see that the voltage rises gradually.

To define J_c , we must therefore define a measurement sensitivity in terms of electric field or effective resistivity.



Commonly used definitions are $\rho = 10^{-14} \Omega\cdot\text{m}$ or $E = 1 \mu\text{V}\cdot\text{m}^{-1}$

Critical current defined at this level is about what you would expect the conductor in a resin impregnated solenoid to achieve. At higher resistivity, self heating starts to raise the internal temperature and reduce the critical current

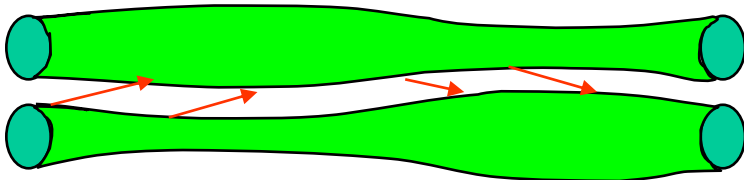
Resistive transition 2

It has been found empirically that the resistive transition may be represented by a power law

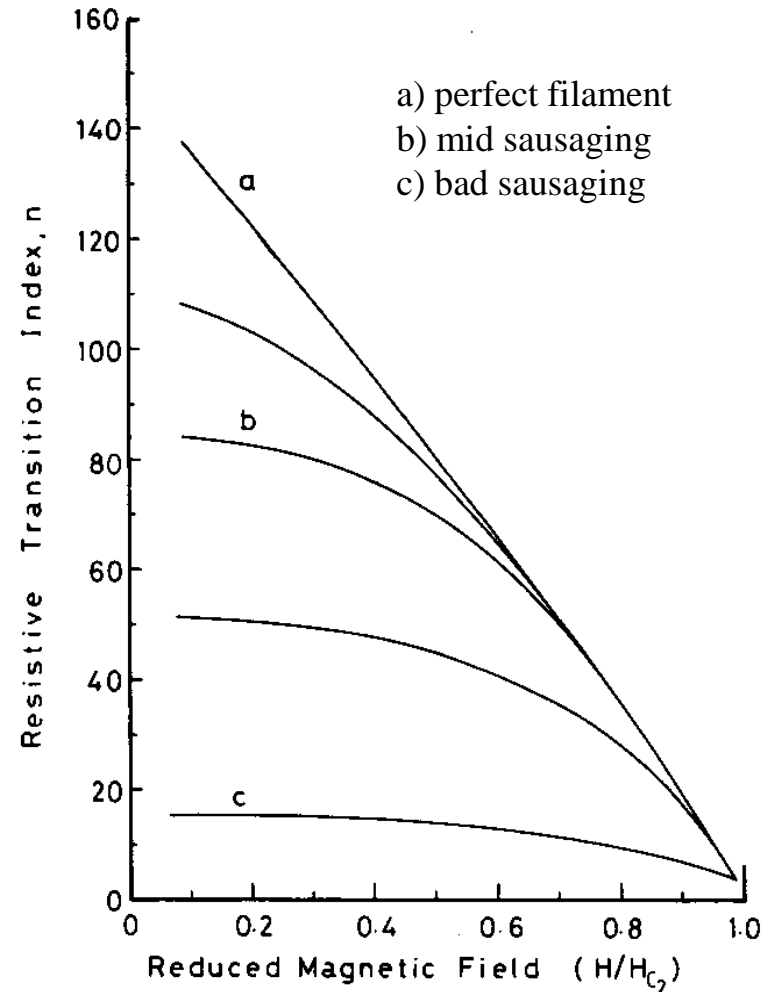
$$\rho(J) = \rho_o \left\{ \frac{J}{J_o} \right\}^n$$

where n is called the resistive transition index.

- the effect is partly within the filaments (flux flow) and partly between the filaments
- 'sausaging of the filaments, forces current to cross the copper matrix as critical current is approached.



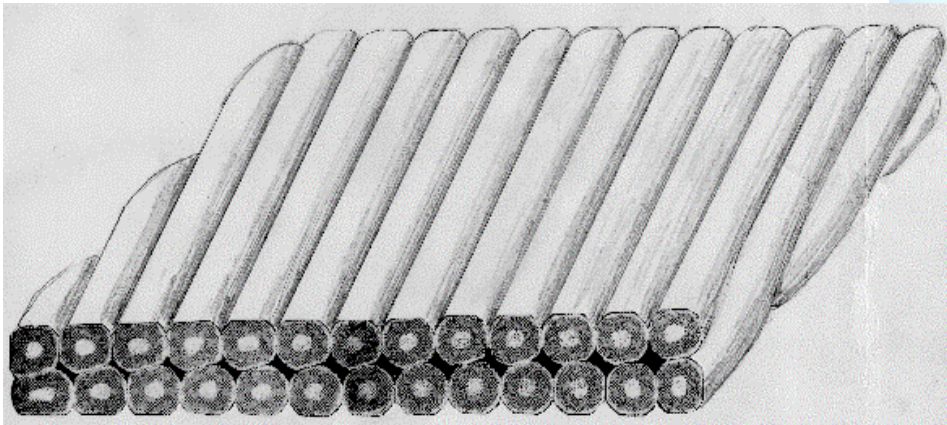
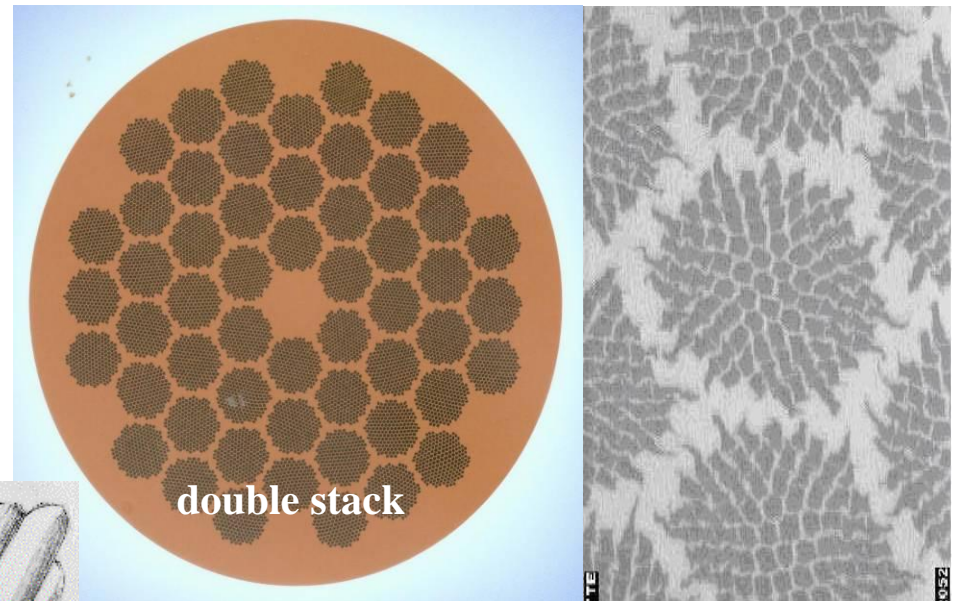
- resistive transition can be the main source of decay in persistent magnets
- 'n' is often taken as a measure of quality - look for $n > 50$
- HTS conductors so far have low $n \sim 5 - 10$



Conductors for accelerator magnets



- to date, all superconducting accelerators have used NbTi superconductor.
- to control field errors and ac losses, the filaments must be $< 10\mu\text{m}$ diameter (lectures 2 & 3)



- to get the necessary high operating currents, many wires must be cabled together (lecture 3)

Engineering current density

In designing a magnet, what really matters is the overall 'engineering' current density J_{eng}

$$J_{eng} = \frac{\text{current}}{\text{unit cell area}} = J_{sup} \times \lambda_{sup}$$

fill factor within the wire $\lambda_{wire} = \frac{1}{(+ mat)}$

where mat = matrix : superconductor ratio

typically:

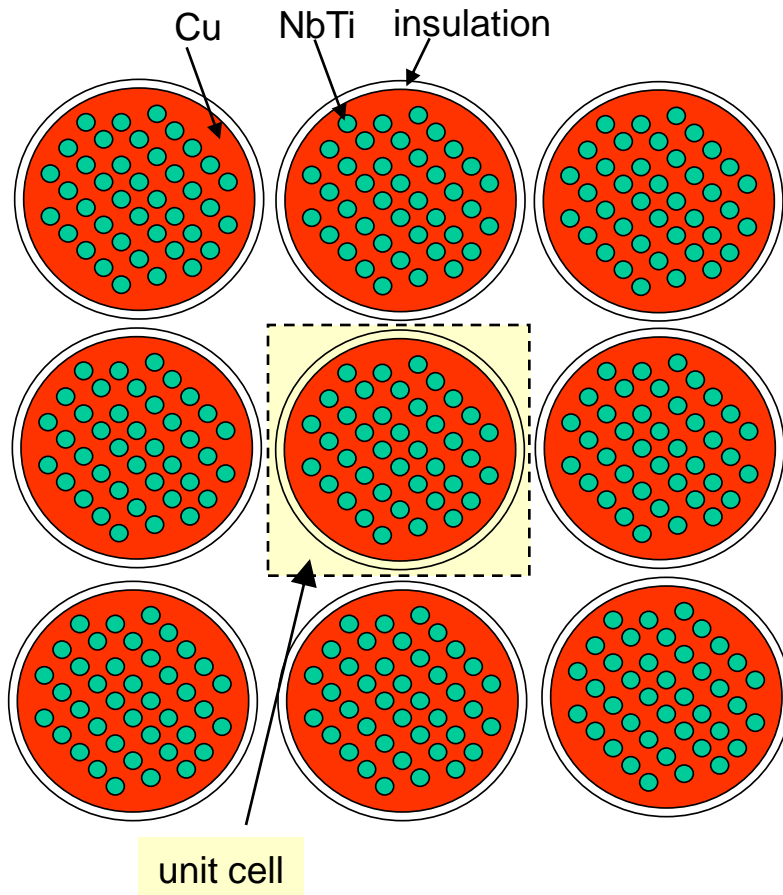
for NbTi $mat = 1.5$ to 3.0 ie $\lambda_{sup} = 0.4$ to 0.25

for Nb₃Sn $mat \sim 3.0$ ie $\lambda_{sup} \sim 0.25$

for B2212 $mat = 3.0$ to 4.0 ie $\lambda_{sup} = 0.25$ to 0.2

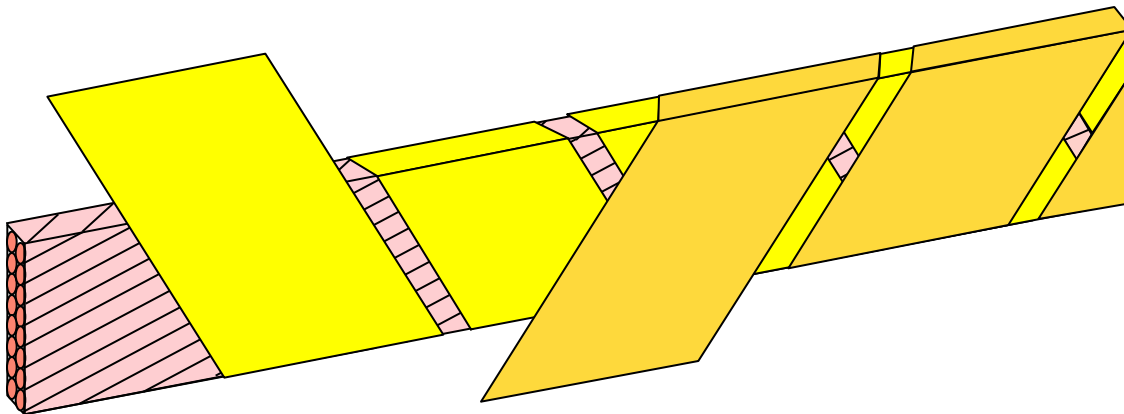
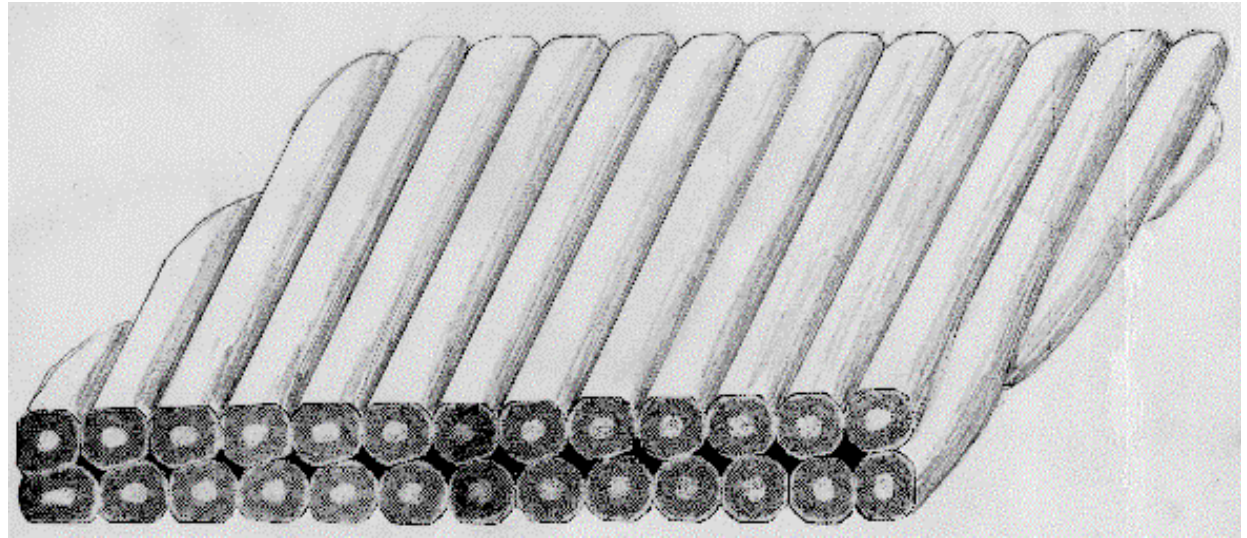
$\lambda_{winding}$ takes account of space occupied by insulation, cooling channels, mechanical reinforcement etc and is typically 0.7 to 0.8

So typically J_{eng} is only 15% to 30% of $J_{supercon}$



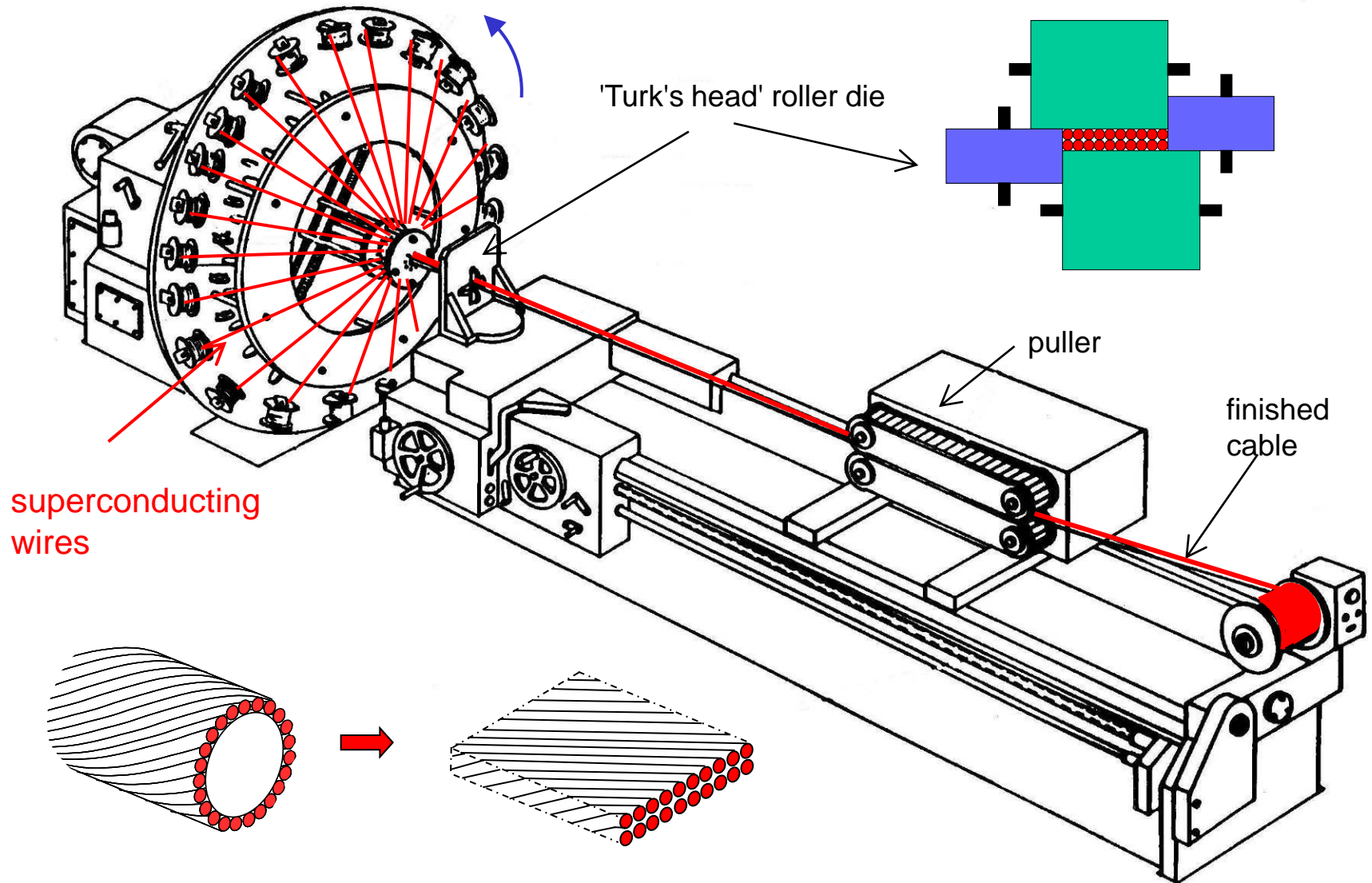
Rutherford cable

- for high current applications, such as accelerators, we need many wires in parallel
- the most popular way of doing this is the Rutherford cable (see lecture 3)

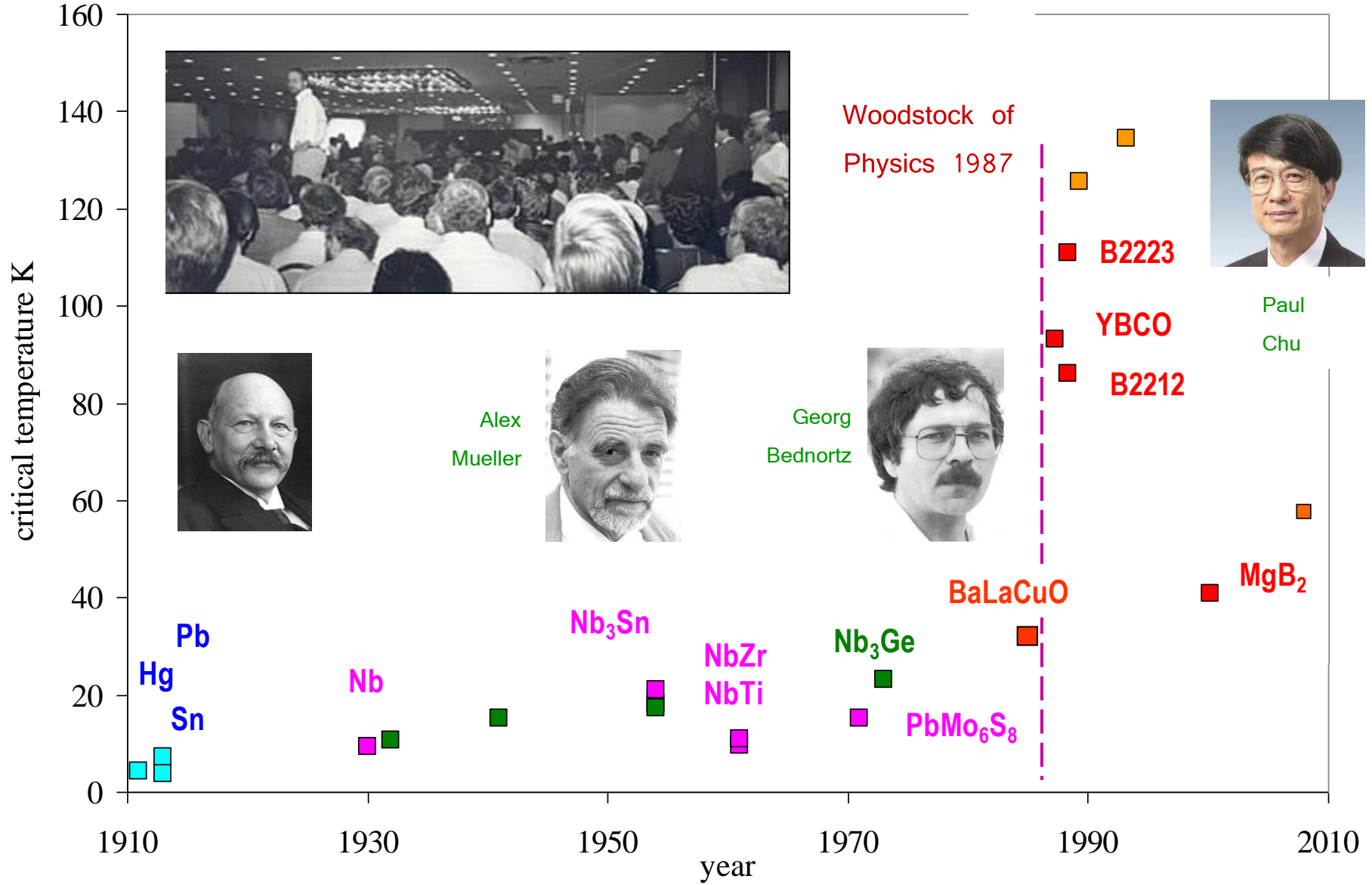


- Rutherford cable is usually insulated by wrapping it with Kapton tape

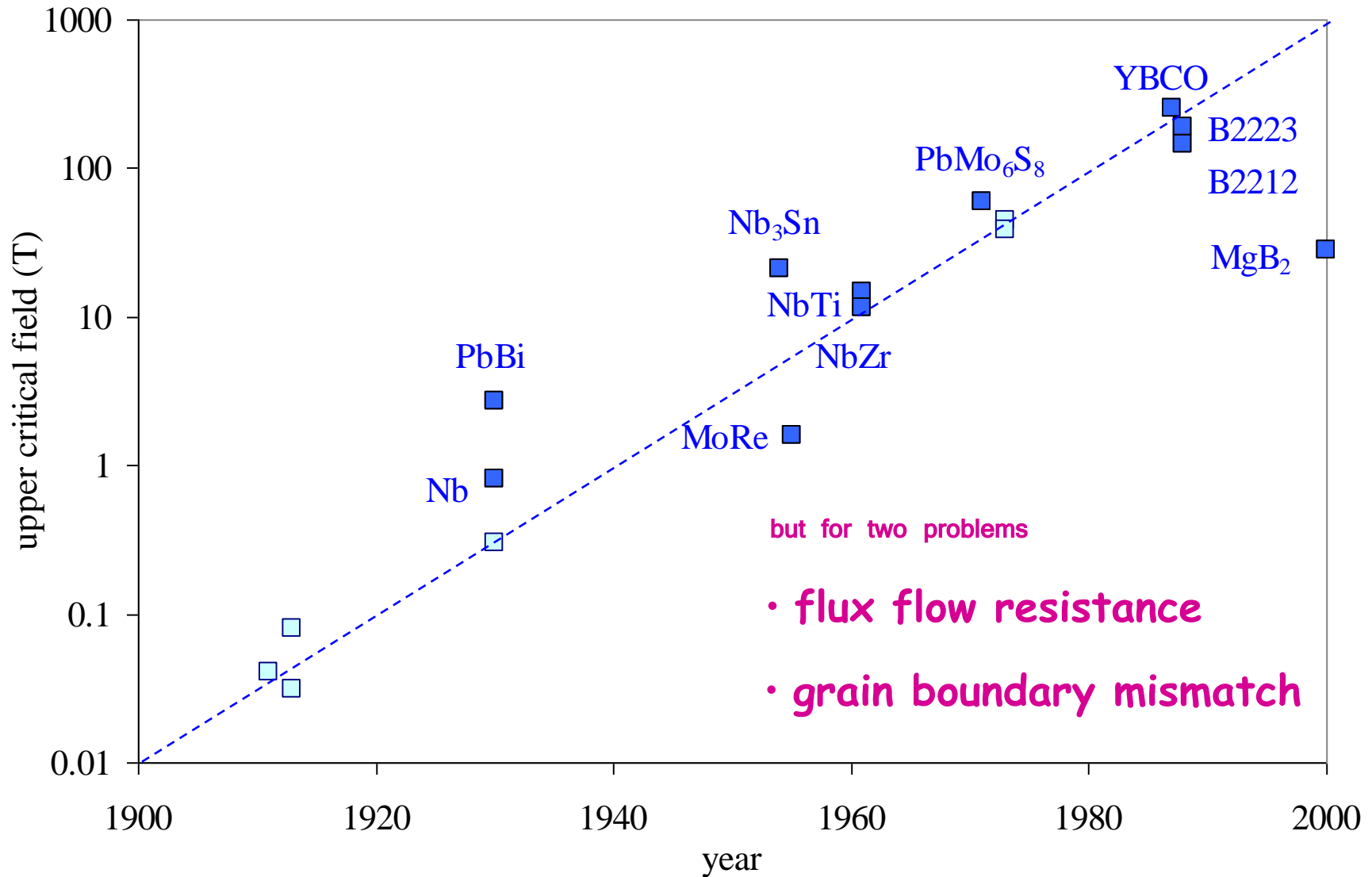
Manufacture of Rutherford cable



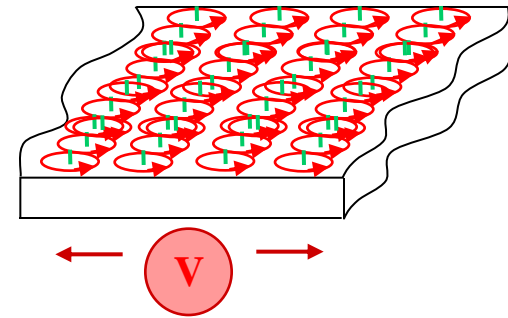
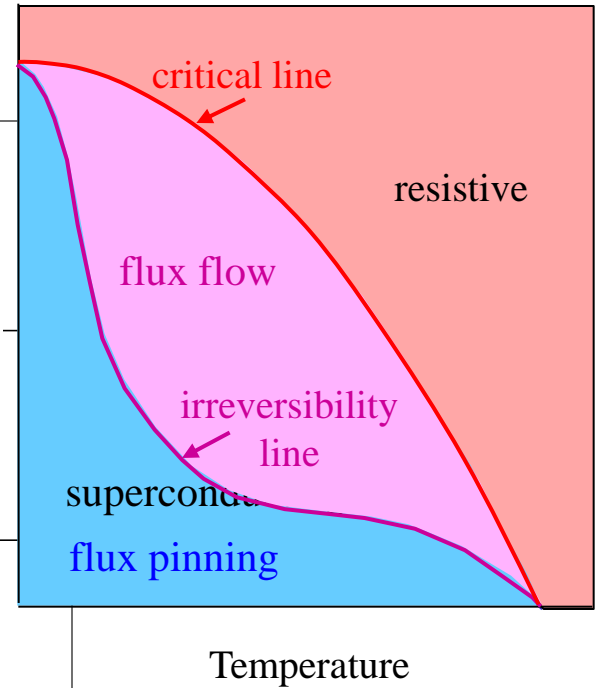
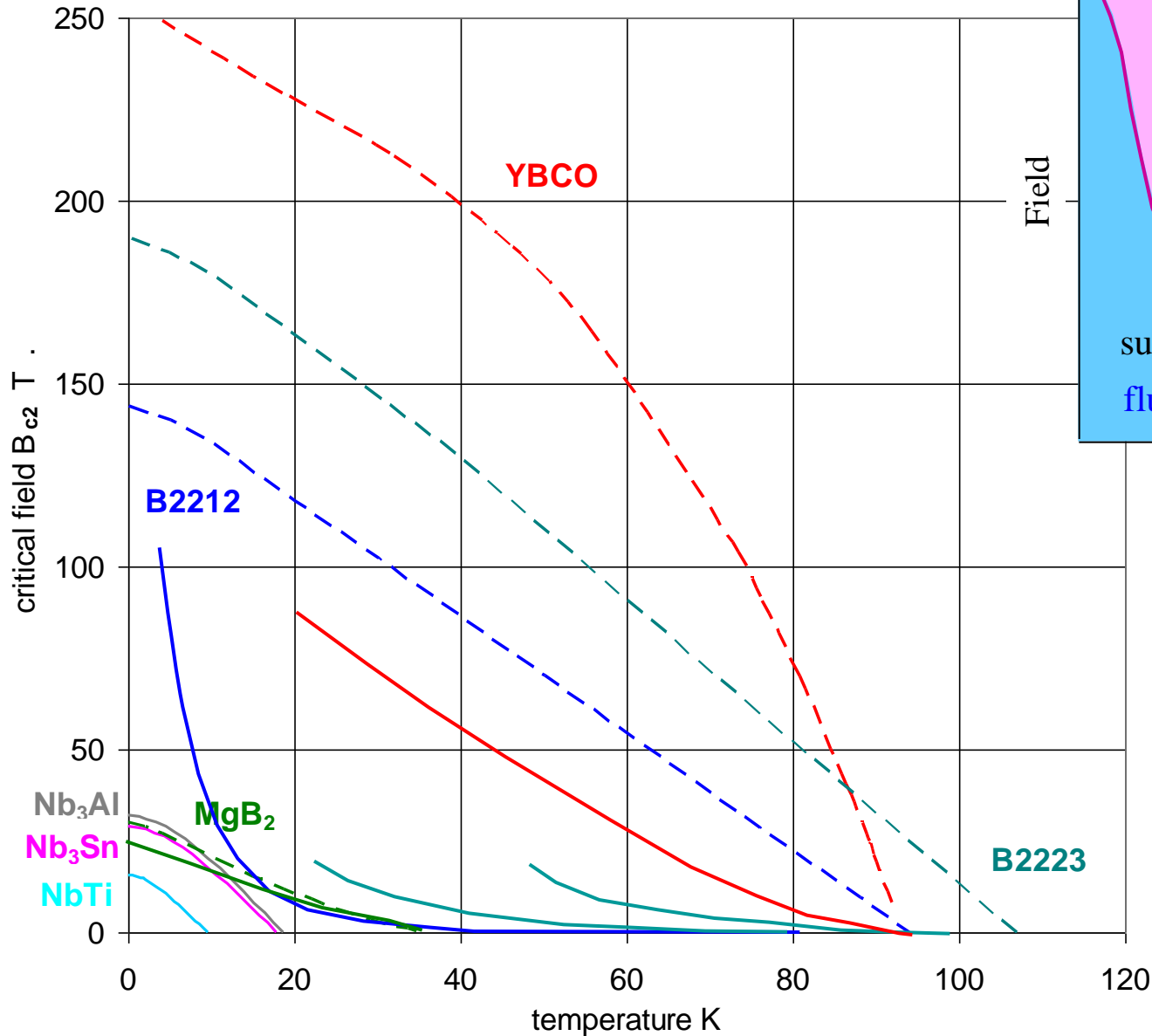
A century of critical temperatures



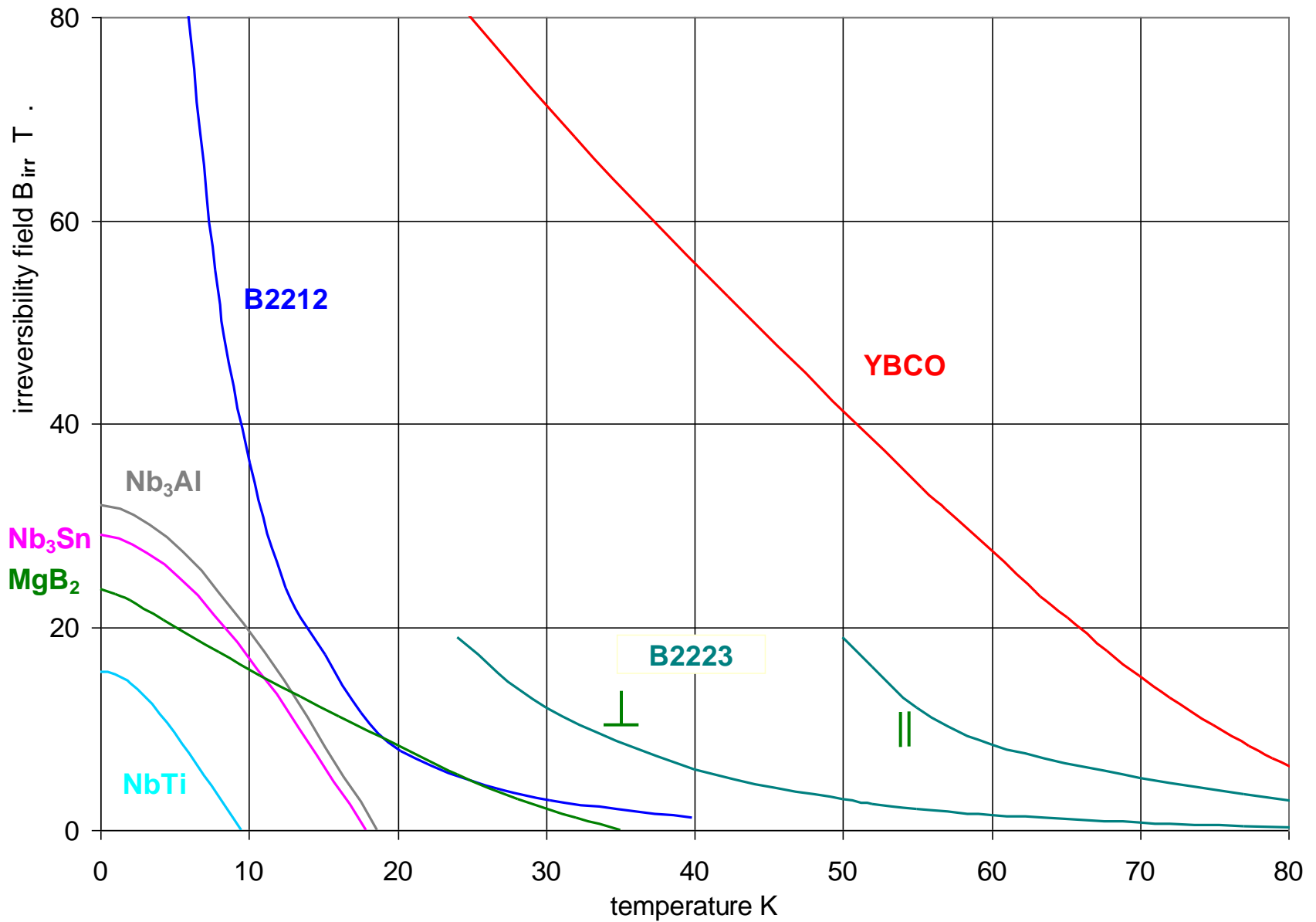
Wonderful materials for magnets



1) Flux flow resistance

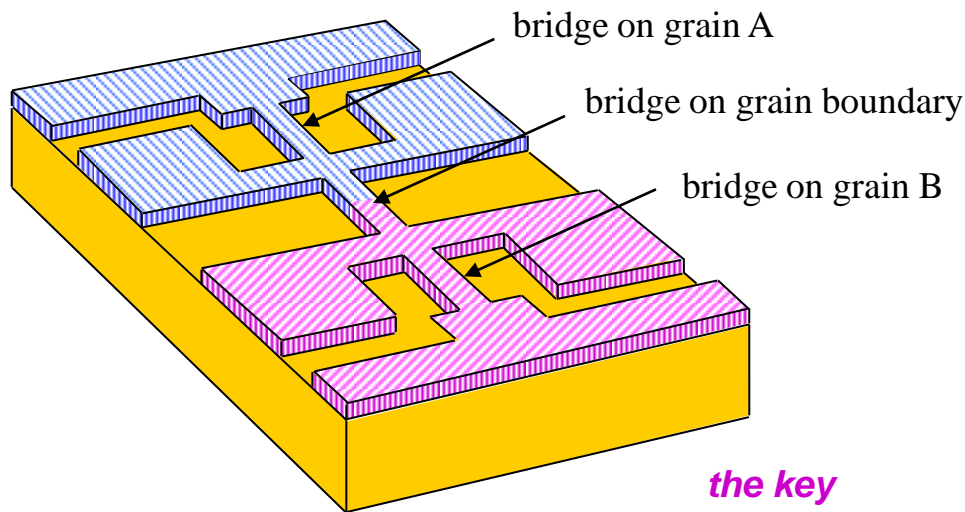
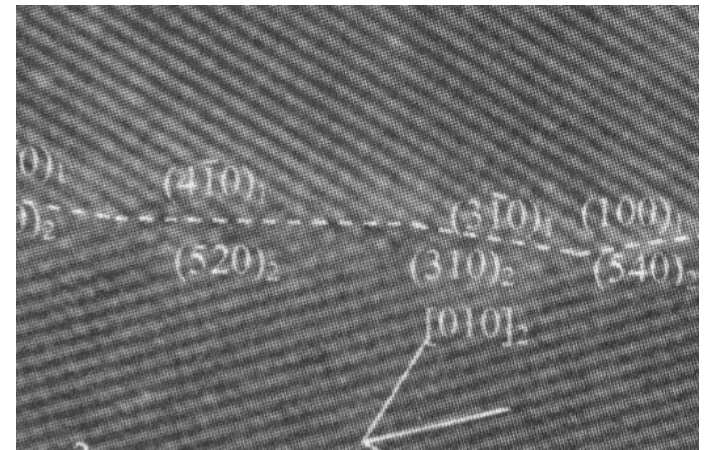


Accessible fields for magnets

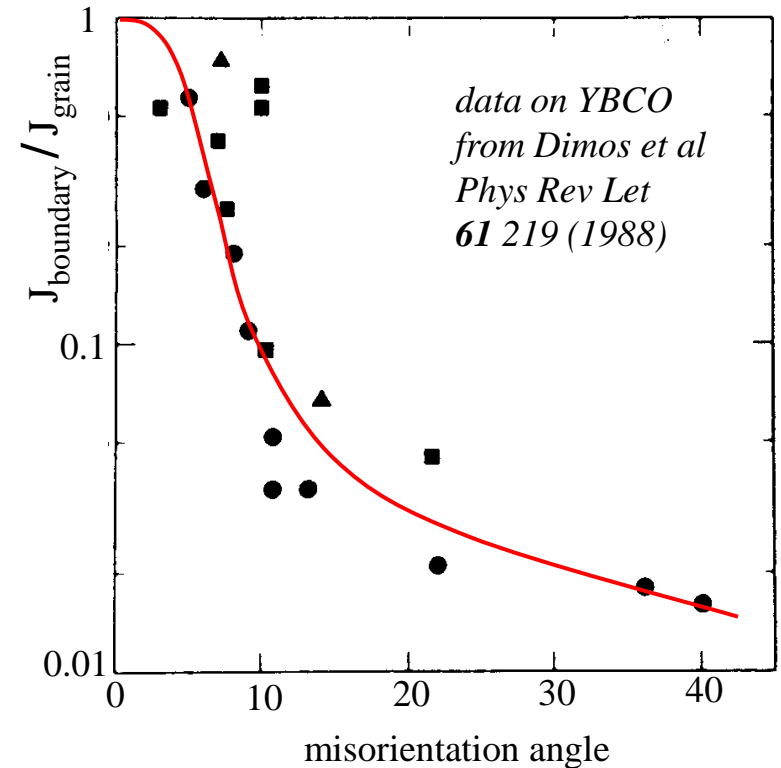


2) Grain boundary mismatch

- crystal planes in grains point in different directions
- critical currents are high within the grains
- J_c across the grain boundary depends on the misorientation angle
- For good J_c must align the grains to within a few degrees



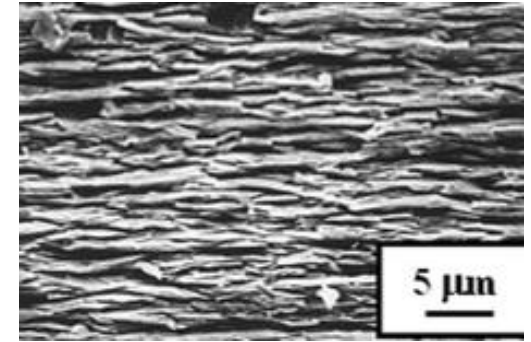
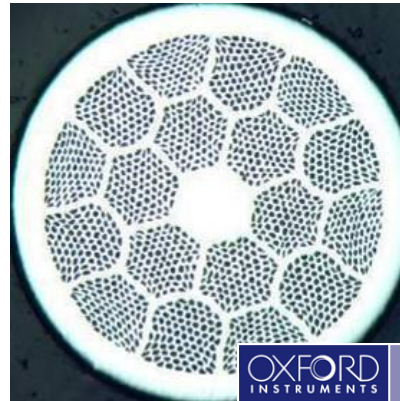
the key measurement of Dimos et al



Production of BSCCo wires & tapes

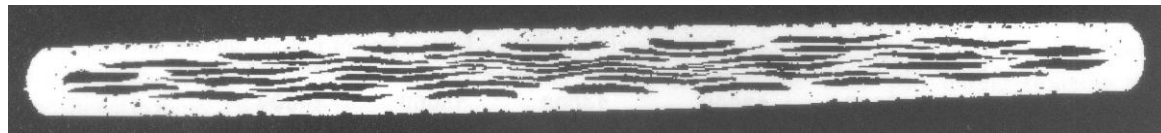
B2212 wire

- draw down B2212 powder in silver tube
- restack, draw down round and heat treat
- grains align when processed with silver



B2223 tape

- roll flat \Rightarrow heat treat.....produces B2223 \Rightarrow press flat \Rightarrow heat treat ..., fills voids, heals cracks, helps alignment



NST

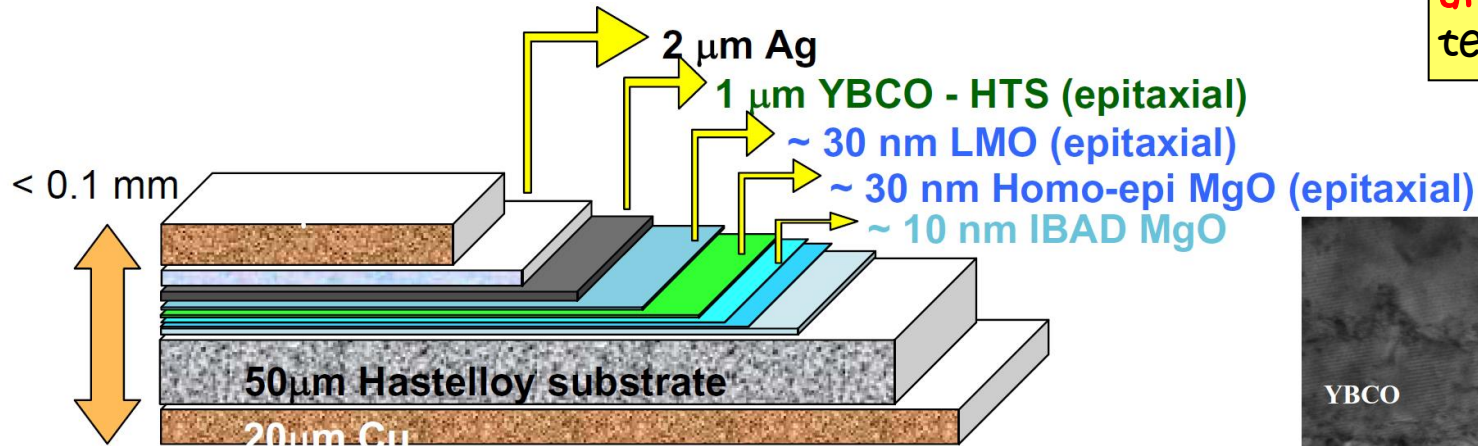
- size \sim 4mm \times 0.2mm, piece length \sim 1 - 2km, filling factor 25% - 40%
- can be made with gold alloy (low conductivity) matrix for current leads
- can be laminated with stainless steel foil to improve mechanical properties

but low
irreversibility
field/temperature

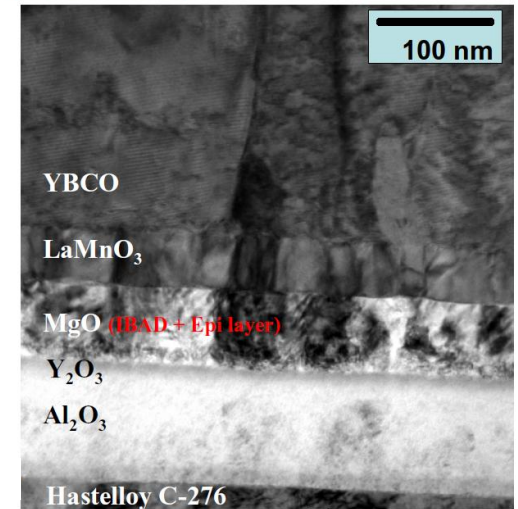
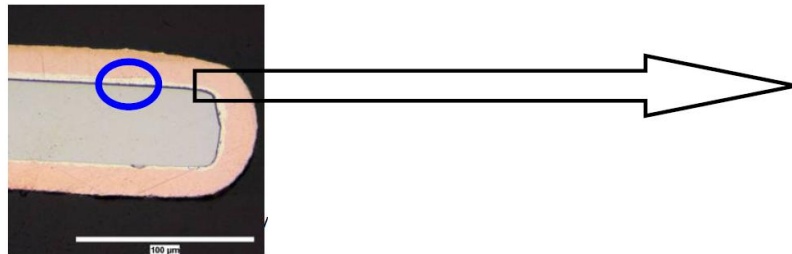


Coated YBCO tape

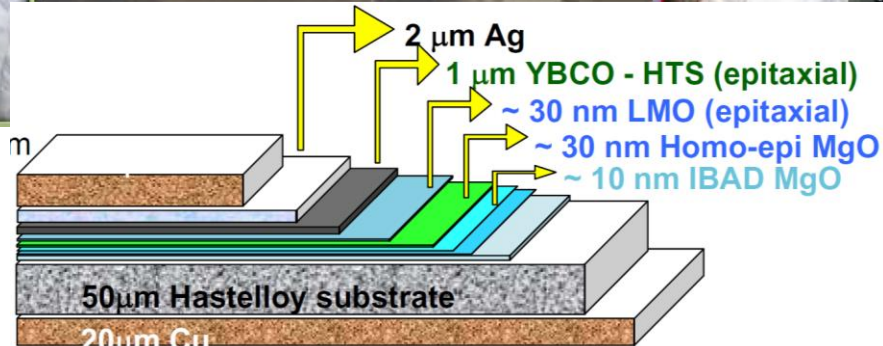
- YBCO has the best irreversibility field, but it is very sensitive to grain boundary misalignment
- the grains do not line up naturally - they must be persuaded
- deposit YBCO on a substrate where the grains are aligned and the lattice roughly matches YBCO



OK high field
and high
temperature



YBCO coated tape at



Lecture 1: concluding remarks

- superconductors allow us to build magnets which burn no power (except refrigeration)
- ampere turns are cheap, so don't need iron
 - ⇒ fields higher than iron saturation (but still use iron for shielding)
- performance of all superconductors described by the critical surface in $B J \theta$ space,
- three kinds of superconductor
 - **type 1**: low temperature, unsuitable for high field
 - **type 2**: low temperature, good for high field - but must create flux pinning to get current density
 - **HTS**: high temperature, high field - but current density is still a problem
- NbTi is the most common commercial superconductor - standard production process
- Nb₃Sn has higher critical field & temperature - specialized commercial production
- BSCO high temperature **or** high field, but not both - prototype commercial production
- YBCO high temperature **and** high field, but must align the grains - prototype commercial production
- measure I_c to check specification, the index n indicates quality
- for accelerators, so far it's only been NbTi, usually in Rutherford cables

Some useful references

Superconducting Magnets

- Superconducting Accelerator Magnets: KH Mess, P Schmuser, S Wolf., pub World Scientific, (1996) ISBN 981-02-2790-6
- Case Studies in Superconducting Magnets, Second edition: Y Iwasa, pub Springer (2009), ISBN 978-0-387-09799-2.
- High Field Superconducting Magnets: FM Asner, pub Oxford University Press (1999) ISBN 0 19 851764 5
- Superconducting Magnets: MN Wilson, pub Oxford University Press (1983) ISBN 0-019-854805-2
- Proc Applied Superconductivity Conference: pub as IEEE Trans Applied Superconductivity, Mar 93 to 99, and as IEEE Trans Magnetics Mar 75 to 91
- Handbook of Applied Superconductivity ed B Seeber, pub UK Institute Physics 1998

Cryogenics

- Experimental Techniques for Low-temperature Measurements: J. W. Ekin Pub. Oxford University Press, ISBN 978-0-19-857054-7
- Helium Cryogenics Van Sciver SW, pub Plenum 86 ISBN 0-0306-42335-9
- Cryogenic Engineering, Hands BA, pub Academic Press 86 ISBN 0-012-322991-X
- Cryogenics: published monthly by Butterworths
- Cryogenie: Ses Applications en Supraconductivite, pub IIR 177 Boulevard Maiesherbes F5017 Paris France

Materials Mechanical

- Materials at Low Temperature: Ed RP Reed & AF Clark, pub Am. Soc. Metals 1983. ISBN 0-87170-146-4
- Handbook on Materials for Superconducting Machinery pub Batelle Columbus Laboratories 1977.
- Nonmetallic materials and composites at low temperatures: Ed AF Clark, RP Reed, G Hartwig pub Plenum
- Nonmetallic materials and composites at low temperatures 2, Ed G Hartwig, D Evans, pub Plenum 1982
- Austenitic Steels at low temperatures Editors R.P.Reed and T.Horiuchi, pub Plenum 1983

Superconducting Materials

- Superconductor Science and Technology, published monthly by Institute of Physics (UK).
- Superconductivity of metals and Cuprates, JR Waldram, Institute of Physics Publishing (1996) ISBN 0 85274 337 8
- High Temperature Superconductors: Processing and Science, A Bourdillon and NX Tan Bourdillon, Academic Press, ISBN 0 12 117680 0
- Superconductivity: A Very Short Introduction by Stephen J. Blundell: Oxford University Press (2009) ISBN 978-0-19-954090-7

on the Web

- **Lectures on Superconductivity** <http://www.msm.cam.ac.uk/ascg/lectures>.
A series of lectures produced for SCENET by Cambridge University: fundamentals, materials, electronics, applications. Also available as a DVD
- **Superconducting Accelerator Magnets** <http://www.mjb-plus.com>.
A course developed from SSC experience, available from website for \$20
- www.superconductors.org website run by an enthusiast; gives some basic info and links
- **Superconductivity Course** at the (UK) Open University.
<http://openlearn.open.ac.uk/course/view.php?id=2397> Good coverage of basics.
- **Wikipedia** on Superconductivity <http://en.wikipedia.org/wiki/Superconductivity>
Good on basics with lots of references and links.
- **European Society for Applied Superconductivity** <http://www.esas.org/>
News, events and people in the area of applied superconductivity
- **CONNECTUS** Consortium of European Companies determined to use Superconductivity
<http://www.conectus.org/>
- **IEEE Council on Superconductivity** <http://www.ewh.ieee.org/tc/csc/>
News, events and people in the area of applied superconductivity (US based)

Materials data on the Web

- Cryogenic properties (1-300 K) of many solids, including thermal conductivity, specific heat, and thermal expansion, have been empirically fitted and the equation parameters are available free on the web at www.cryogenics.nist.gov
- Thermodynamic properties of gases (and liquids) available free as a programme which you can interrogate for your own temperature interval etc.
<http://webbook.nist.gov/chemistry/fluid/>
- Plots and automated data-look-up using the NIST equations are available on the web for a fee from www.cpia.jhu.edu
- Other fee web sites that use their own fitting equations for a number of cryogenic material properties include: www.cryodata.com (cryogenic properties of about 100 materials), and www.jahm.com (temperature dependent properties of about 1000 materials, many at cryogenic temperatures).
- Commercially supplied room-temperature data are available free online for about 10 to 20 properties of about 24,000 materials at www.matweb.com

Cryodata Software Products

GASPAK

properties of pure fluids from the triple point to high temperatures.

HEPAK

properties of helium including superfluid above 0.8 K, up to 1500 K.

STEAMPAK

properties of water from the triple point to 2000 K and 200 MPa.

METALPAK, CPPACK, EXPAK

reference properties of metals and other solids, 1 - 300 K.

CRYOCOMP

properties and thermal design calculations for solid materials, 1 - 300 K.

SUPERMAGNET

four unique engineering design codes for superconducting magnet systems.

KRYOM

numerical modelling calculations on radiation-shielded cryogenic enclosures.

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