

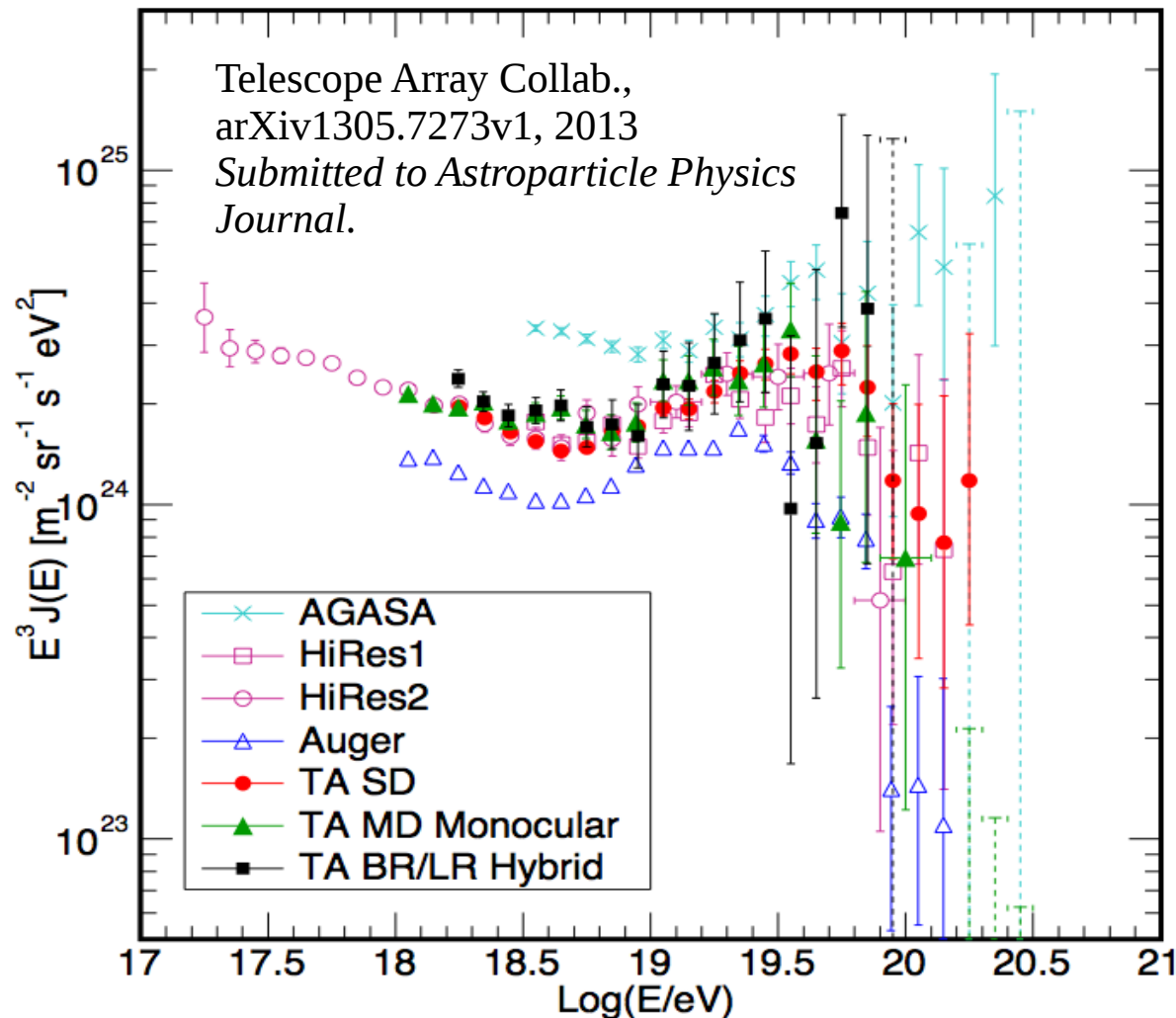
Time-Domain Waveform Studies for ARIANNA

Dr. Jordan Hanson
Ultra-High Energy Neutrino
Parallel Session, TeVPA (2013)
August 26th, 2013

Outline

- How we plan to detect *high-energy neutrinos* via the Askaryan effect
- Conversion of analytical electric fields to voltage waveforms in ARIANNA DAQ (LTI systems)
- Anechoic Chamber measurements performed at the University of Kansas
 - *Experimental Setups (4)*
 - *Types of data taken (scalar versus frequency, time-domain waveforms)*
- Calculation of *effective height* operator of the signal antenna
 - *The best-fit effective height operator*
 - *Including the AC-coupled low-noise amplifier (LNA)*
 - *Checking off-axis*
- Deriving *template waveform induced by neutrino interaction* in ice
- Future work

High Energy Cosmic Ray Spectral Cutoff (GZK effect)

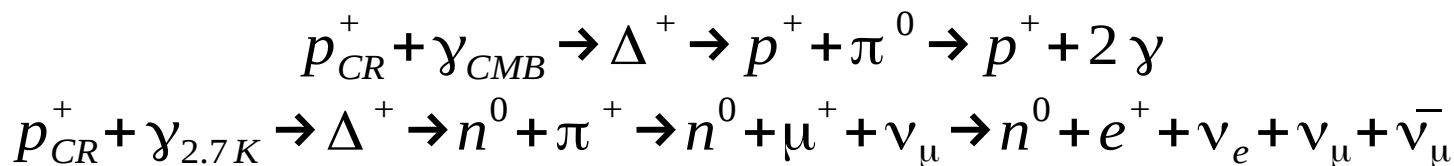


Nucleon-photon threshold effect which produces secondary particles, including *neutrinos*

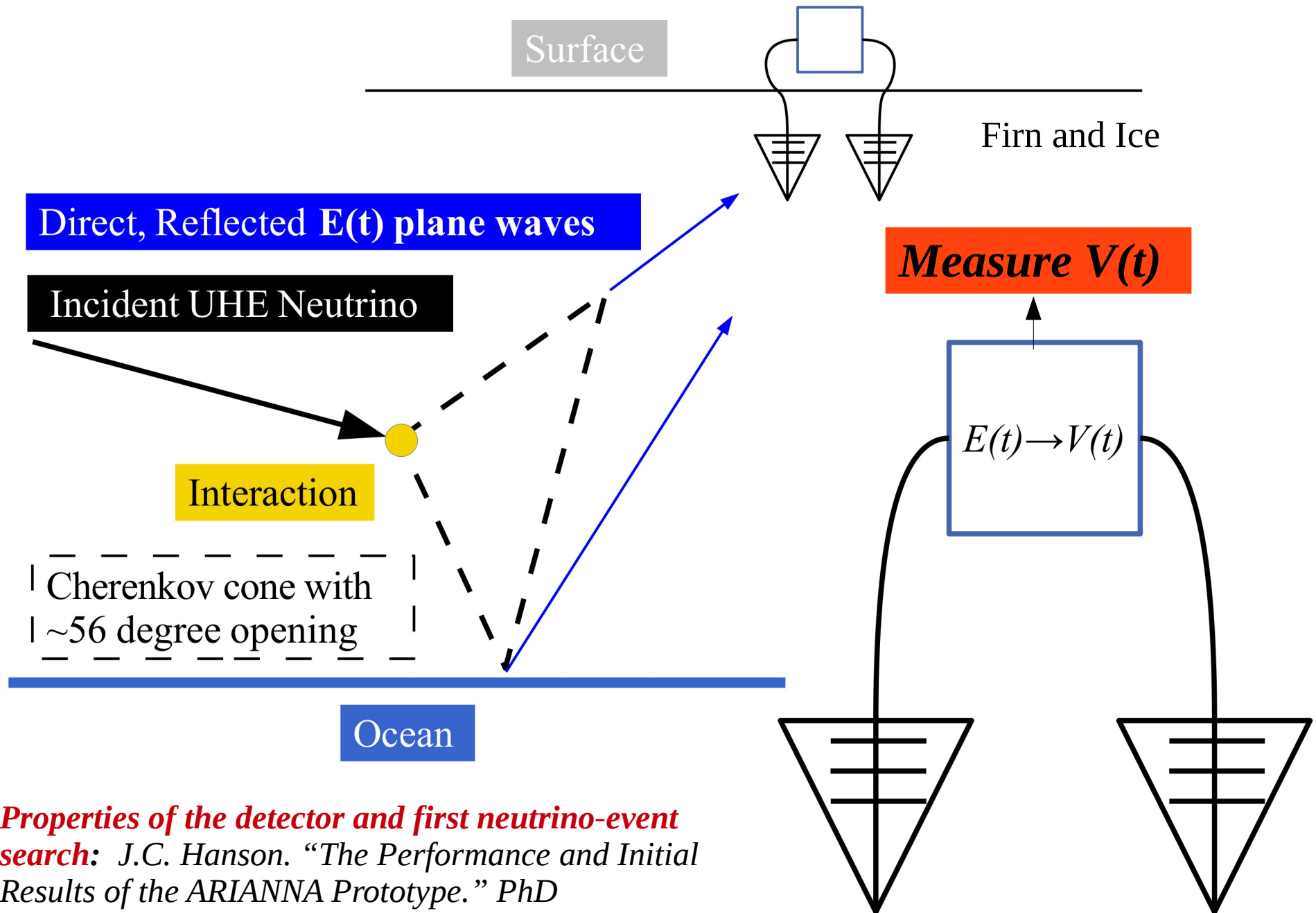
What is the precise origin of these particles?

How *heavy* are they (are they mostly protons, or heavier)?

How does a *neutrino interact* with matter at COM energy of 100 TeV?



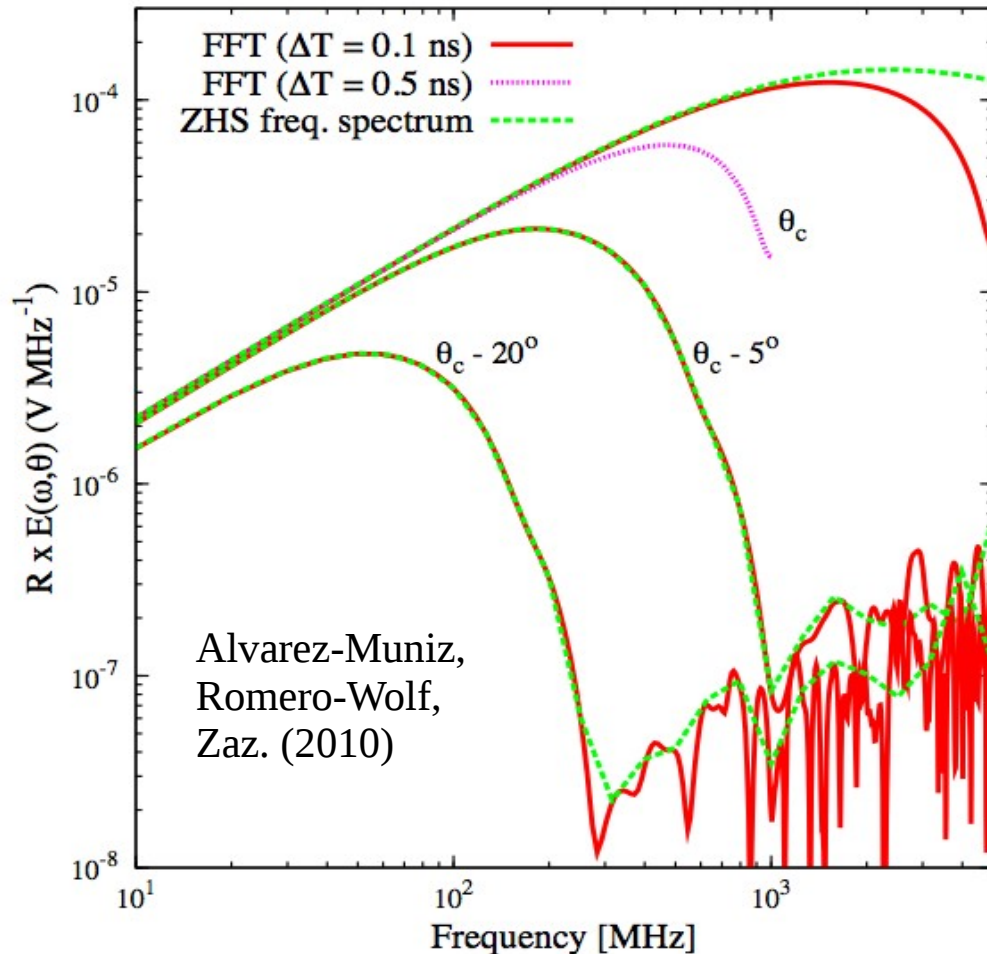
Statement of the Problem



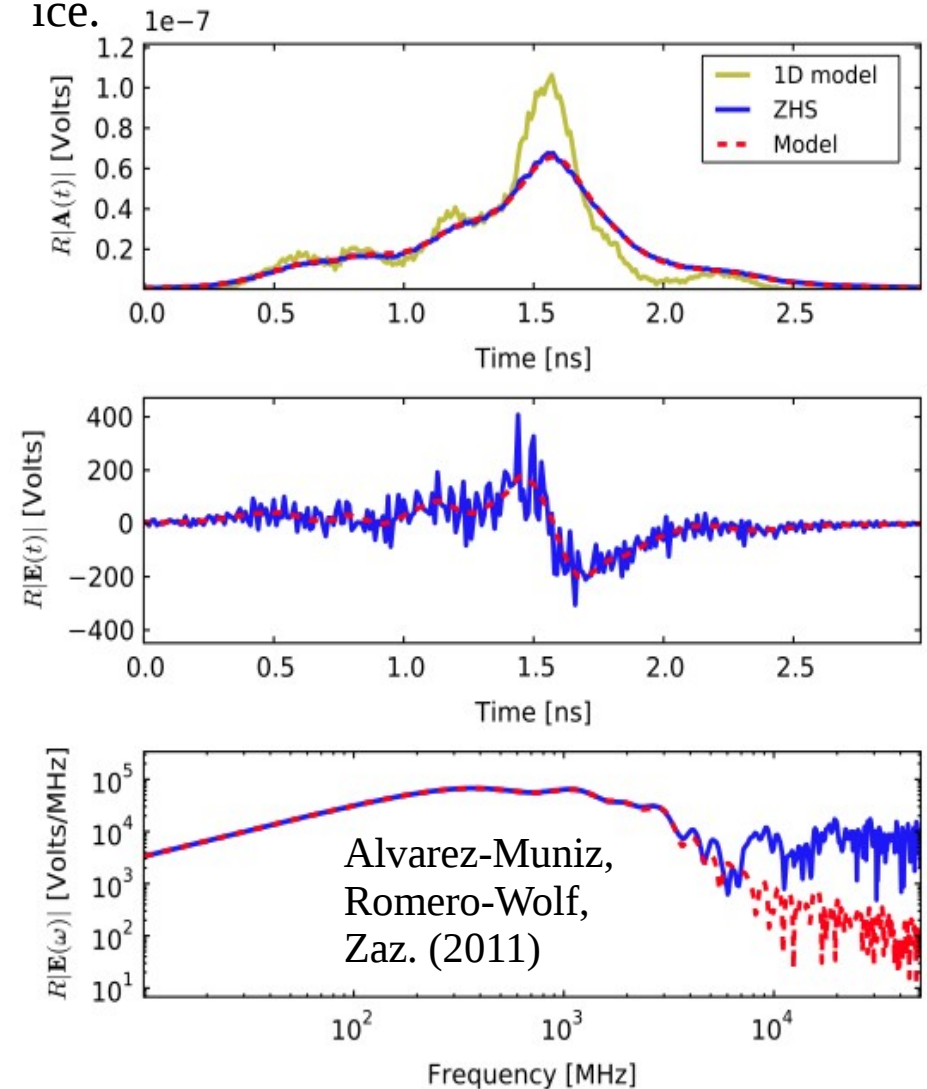
Properties of the detector and first neutrino-event search: J.C. Hanson. "The Performance and Initial Results of the ARIANNA Prototype." PhD Dissertation. (2013)

Statement of the Problem, II: the signal to detect

Spectrum of electric field from 1 PeV shower in ice

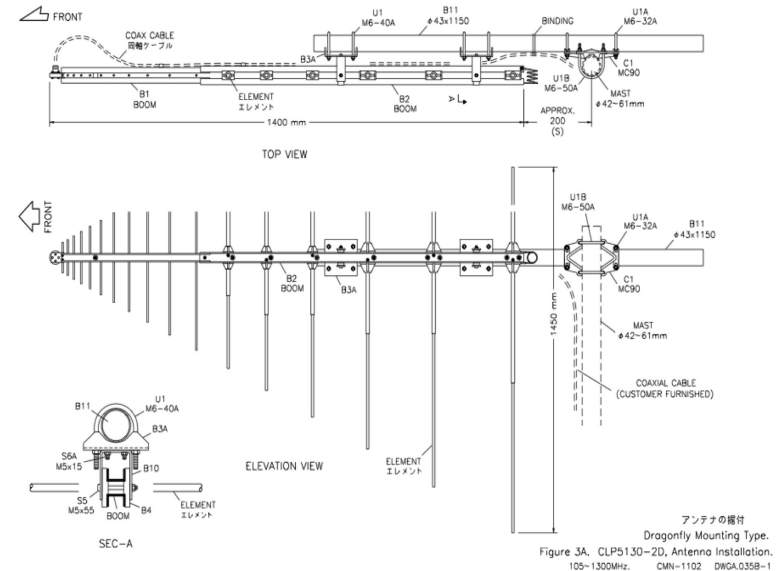
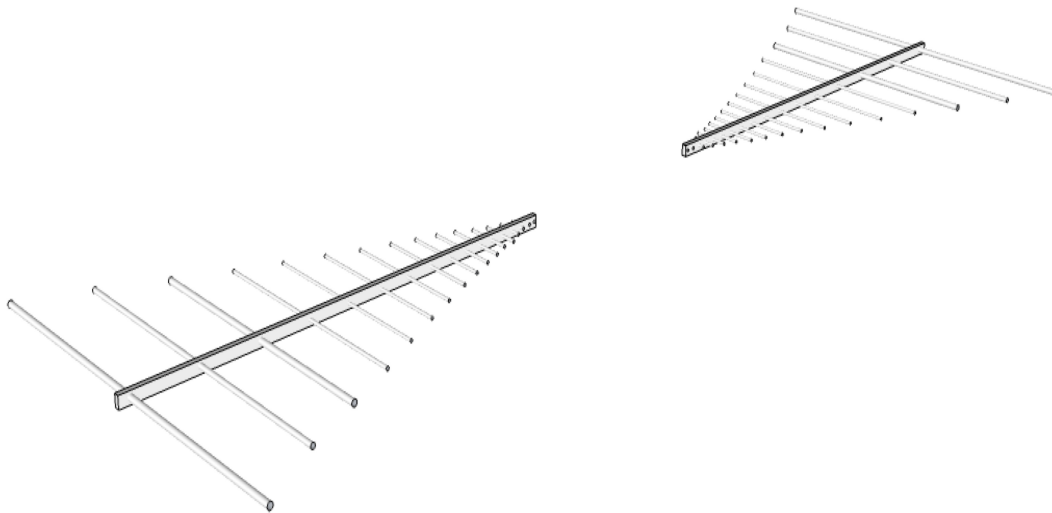


Spectrum+time-domain of 3 EeV shower in ice.



Search: 1 GHz bandwidth, several hundred V/m electric field pulse traveling ~ 1 km through ice

The signal antenna: Log-Periodic Dipole Array



Example of a **frequency-independent** antenna (bandwidth of 100-1300 MHz)

Radiation pattern is maximal in direction of **bore-sight**. The **bore-sight** configuration (shown above) optimizes reception.

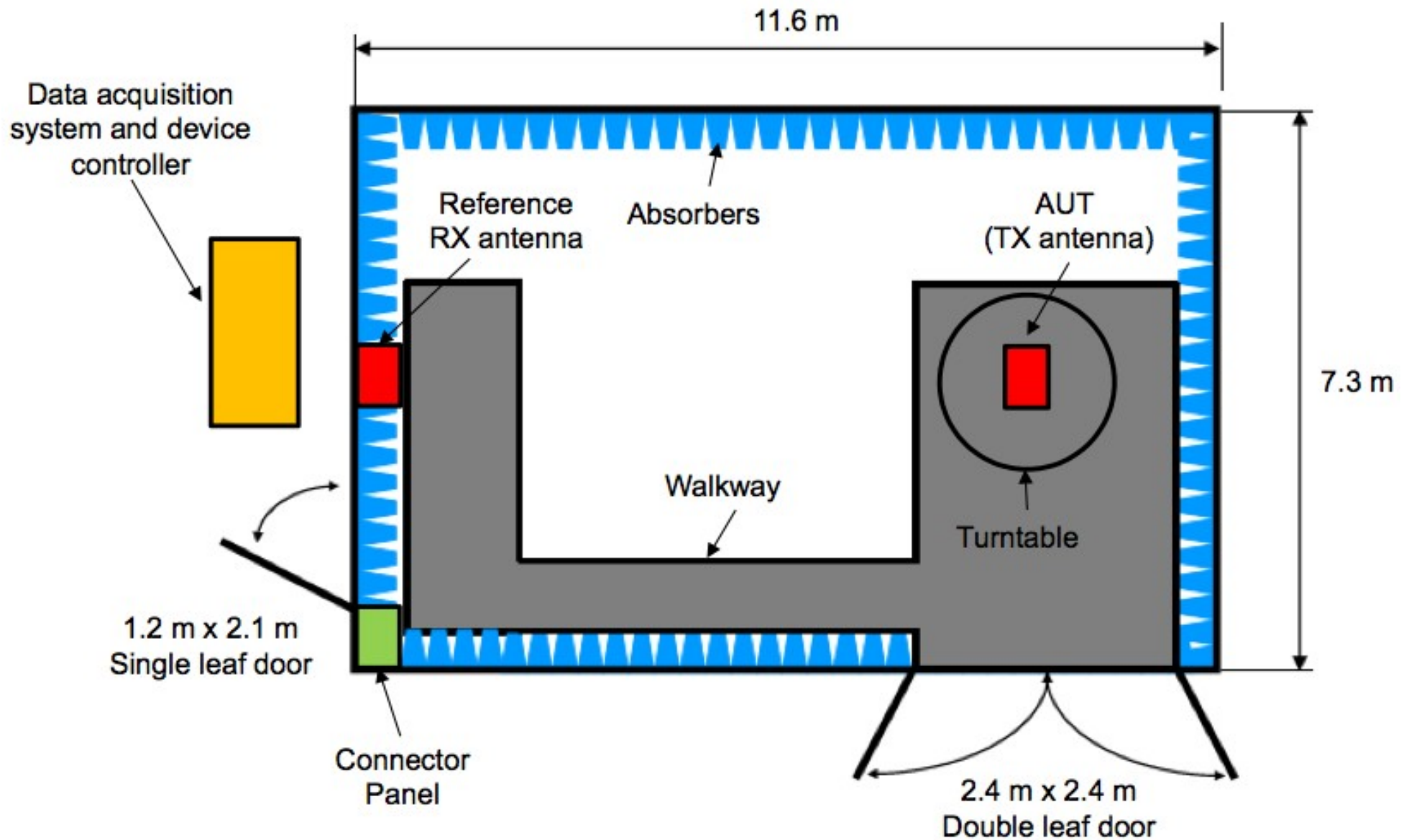
Linearly polarized. The E-plane is the plane containing the dipole elements, the H-plane is perpendicular to E-plane, containing only the **spine** of the antenna

Linear Time-Invariant System

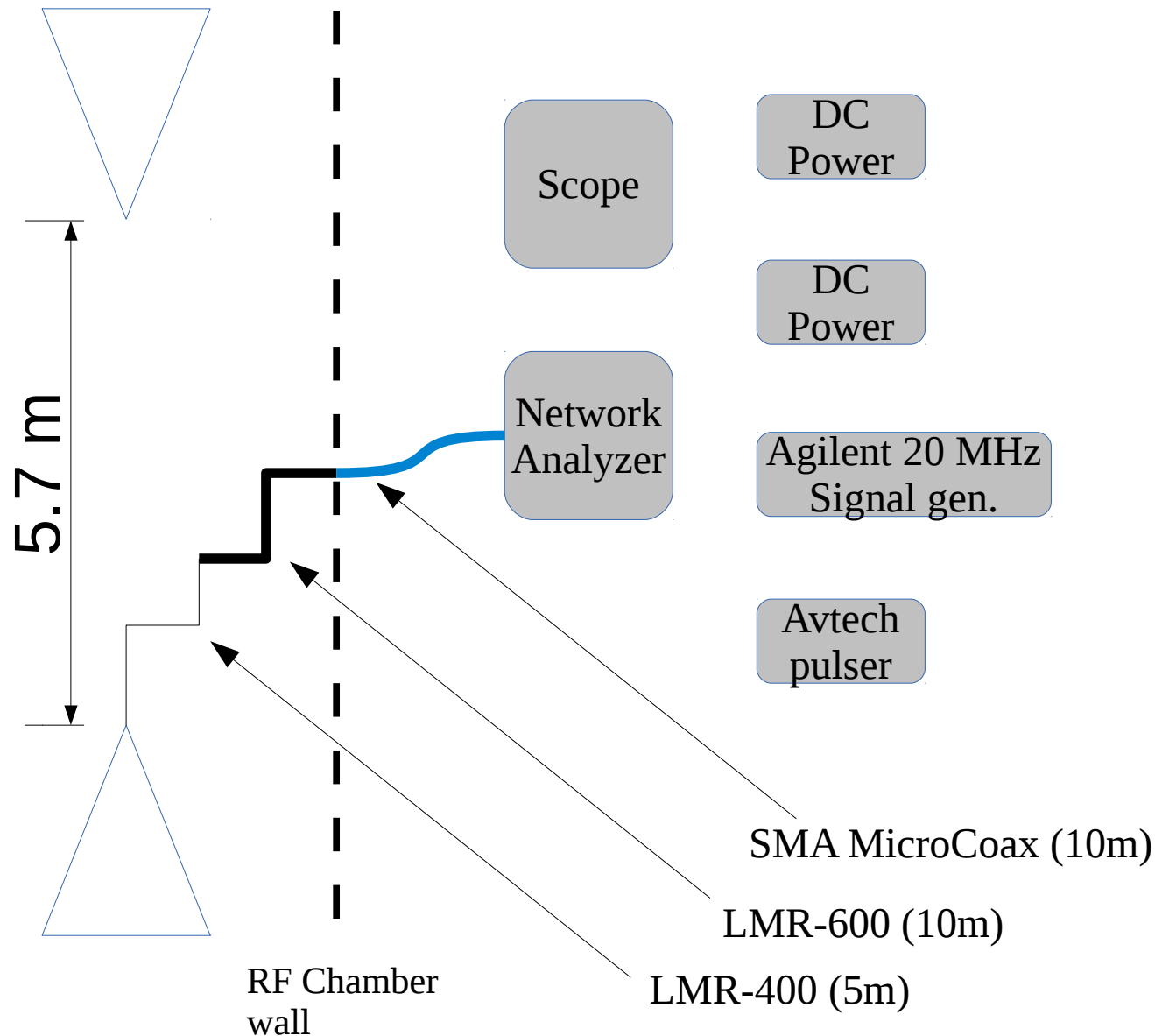
- **Two property** system with single input $x(t)$, single output $y(t)$
 - **Linearity:** $ax_1(t)+bx_2(t) = ay(t)+by(t)$
 - **Time-invariance:** $ax(t-T) = ay(t-T)$
 - The **convolution integral** with kernel r satisfies these two criteria
- **Convolution:** $y(t) = \int_{-\infty}^{\infty} r(\tau) x(t-\tau) d\tau$
- Specifically, for antennas, let $y(t) = V(t)$, the time-dependent voltage. **Taking $r = h(t)$, the effective height**, we have:

$$V(t) = \int_{-\infty}^{\infty} \vec{h}(\tau) \cdot \vec{E}(t-\tau) d\tau$$

Experimental Setup: The Anechoic Chamber



Experimental Setup: scalar LPDA properties (e.g. bandwidth)



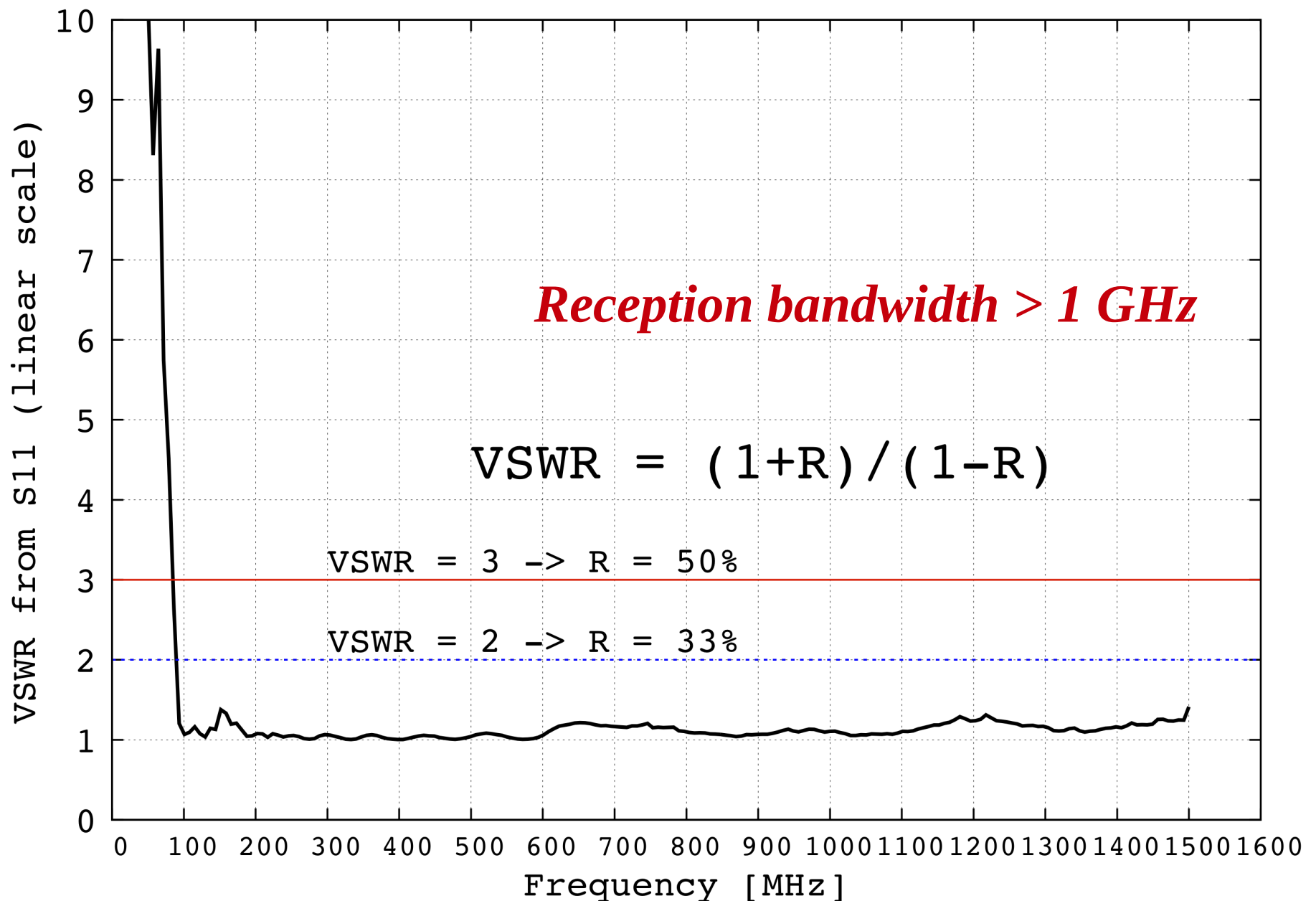
*Attempting to be
in the LPDA
far-field*

***Network analyzer**
measures
reflection and
scattering
parameters vs.
frequency*

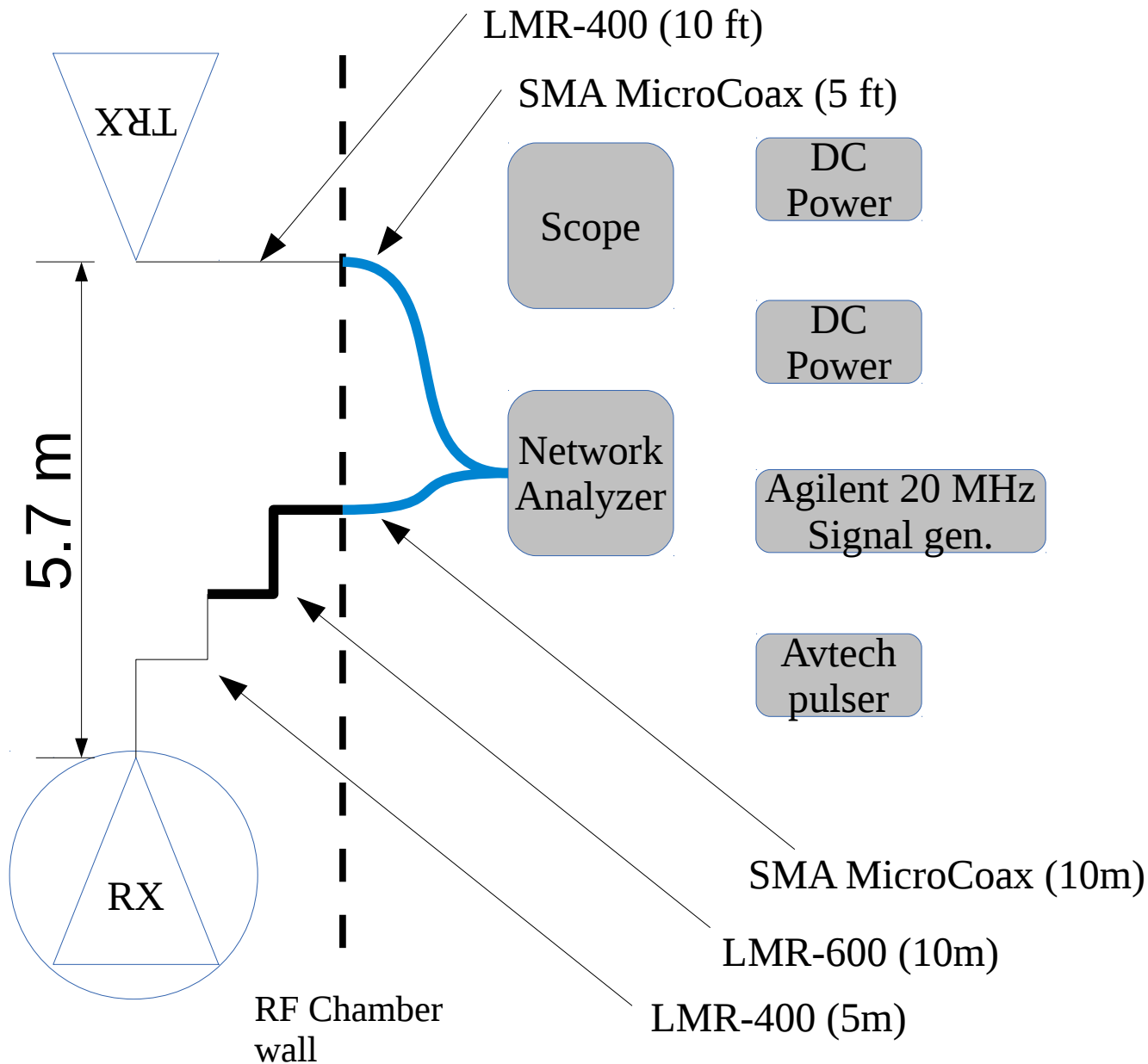
*Cable attenuation
is **minimized**
(subsequent slides)*

***Other equipment
used in
subsequent
measurements***

Main Result #1: Checking the SWR



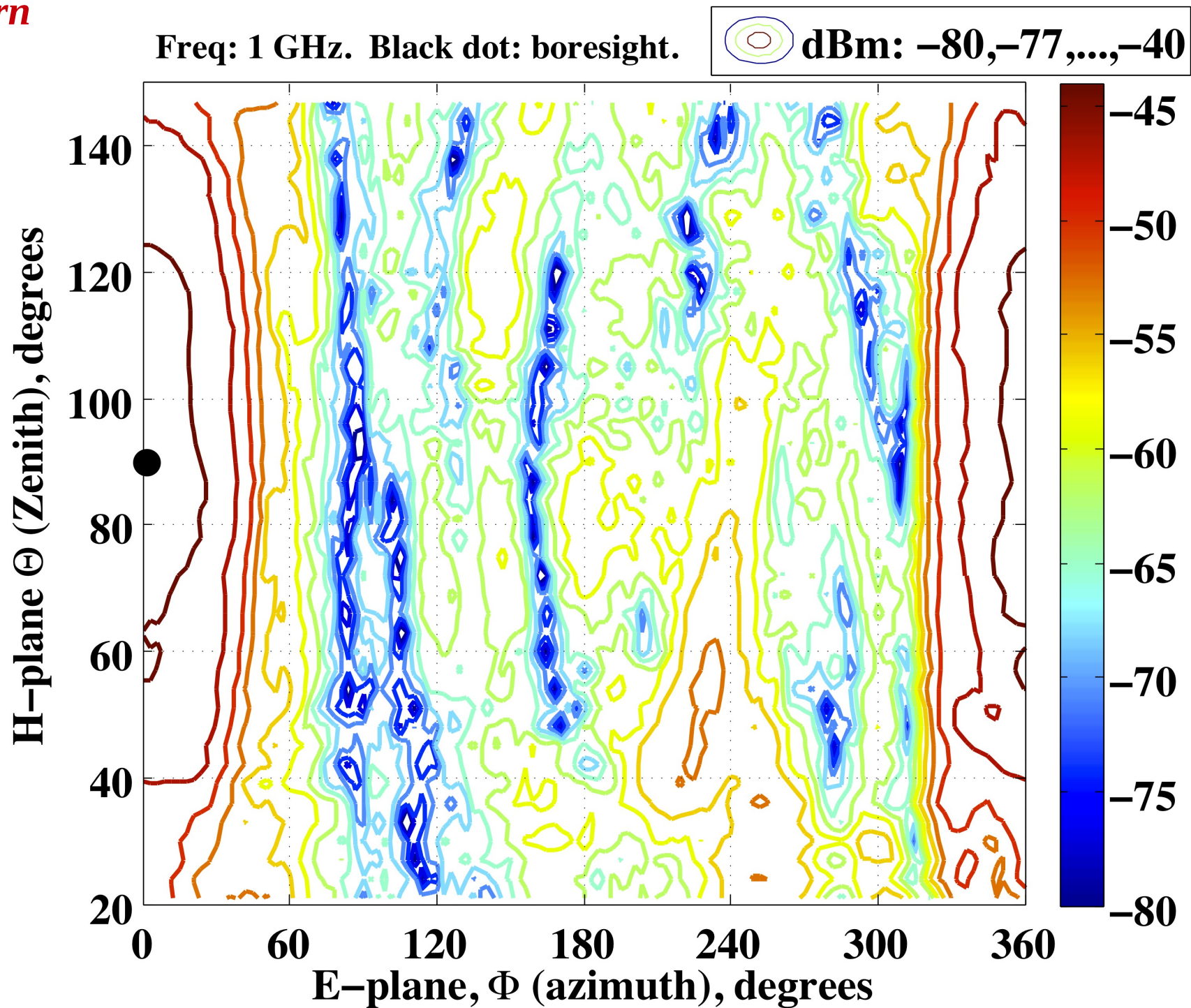
Experimental Setup: 3D radiation pattern, gain



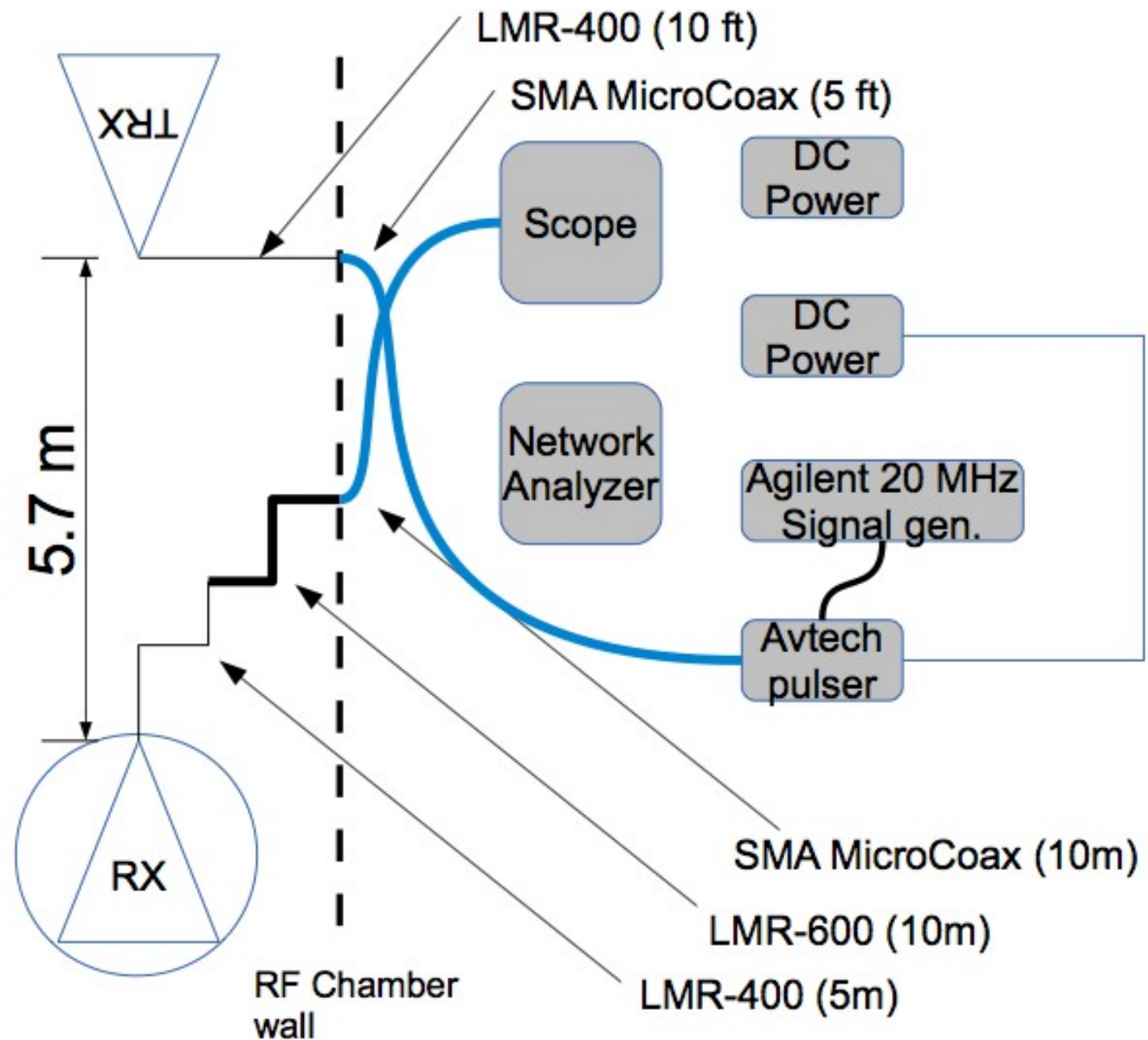
*Measured the full
radiation pattern
vs. frequency,
azimuth, and
zenith angles.*

Achieved 73% coverage of the unit sphere (limited in zenith angle by the mounting stock in the chamber)

Main Result #2: Radiation Pattern



Experimental Setup: impulse response



Derivation of effective height *using this experimental setup*:

r = antenna separation,

c = light speed,

V_L = antenna voltage delivered to load,

Z_L = load resistance (and coaxial line resistance, 50 Ohms),

Z_{in} = antenna input resistance (~50 Ohms),

Z_0 = impedance of free space (120π Ohms) (c.f. P. Miocinonic, 2006)

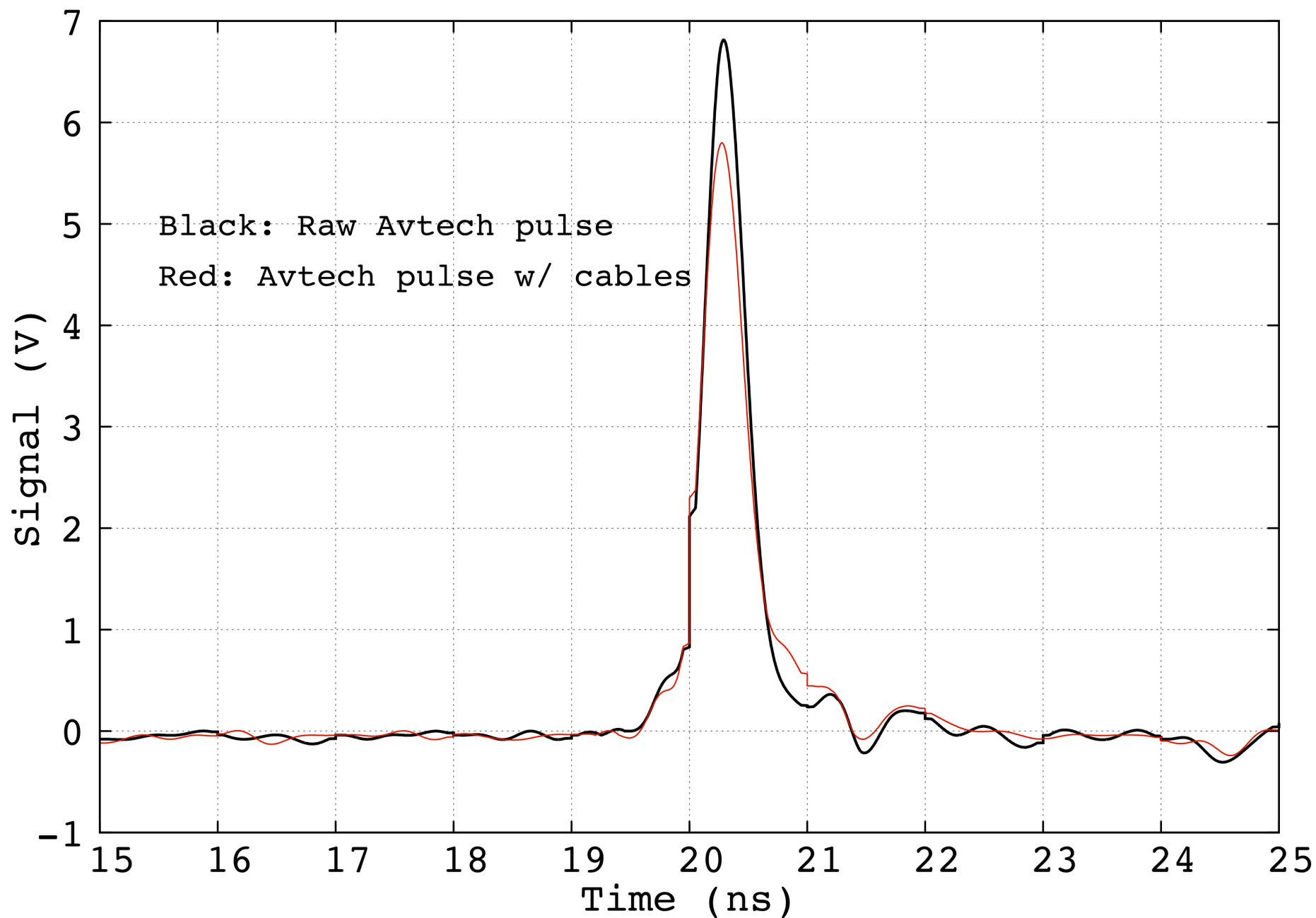
$$V_L(t) = 2 \left(\frac{Z_L}{Z_L + Z_{in}} \right) \vec{h}_{rx}(t) \circ \vec{E}(t)$$

$$\vec{E}(t) = \frac{2}{4\pi r c} \left(\frac{Z_{in}}{Z_{in} + Z_L} \right) \frac{Z_0}{Z_{in}} \vec{h}_{tx} \circ V_{src}(t)$$

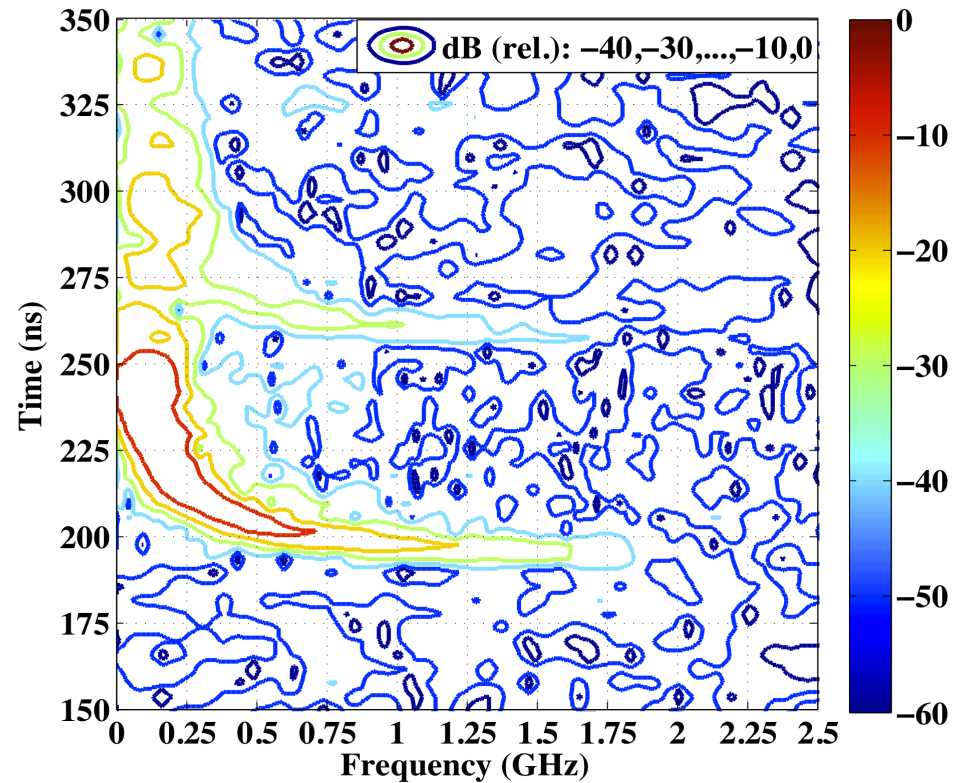
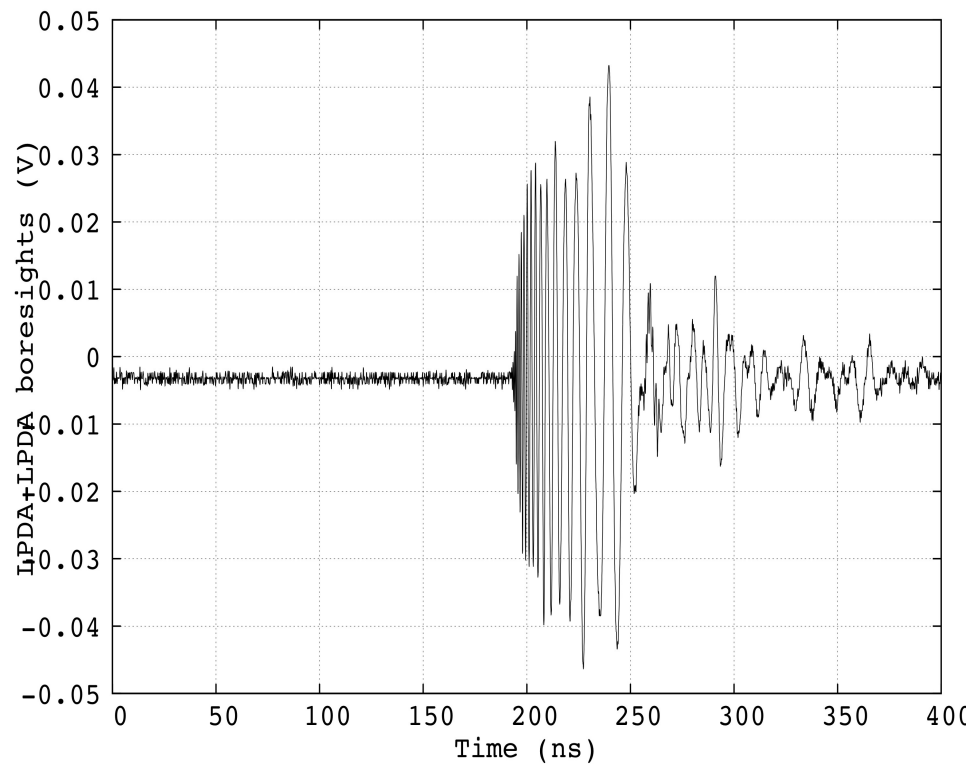
$$V_L(t) = \frac{1}{(2\pi r c)} \frac{Z_0}{Z_L} \vec{h}_{rx}(t) \circ \vec{h}_{rx}(t) \circ \partial_t V_{src}(t) \quad (\vec{h}_{tx} = -2 \partial_t \vec{h}_{rx}(t))$$

Avtech (pulser) signal

Reception bandwidth > 1 GHz



Time-domain Results: raw, bore-sight case



Left: Bore-sight signal data.

Right: Spectrogram of the data on the left; magnitude of the short-time Fourier transform in dB (color scale).

Method for Obtaining $h_{rx}(t)$

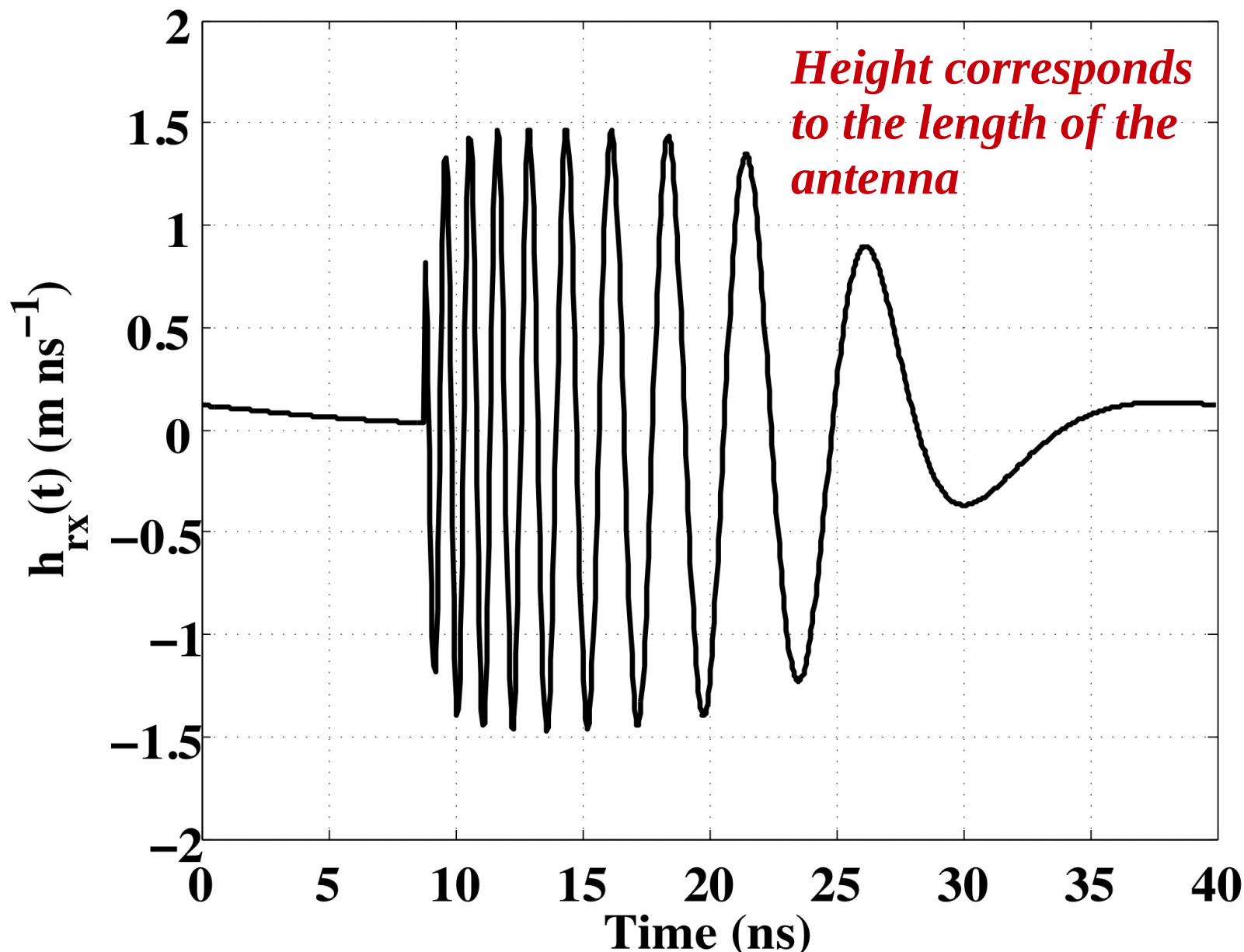
- ***Rotating to Fourier domain and back amplifies noise***
- ***Assume a trial function with parameters, $a(t)$ chosen to turn on/off the function***
- ***Perform a fit that minimizes R after scanning the full parameter space***

$$h_{rx}(t) = A a(t) \cos(2\pi k \ln(t/t_{\text{end}}))$$

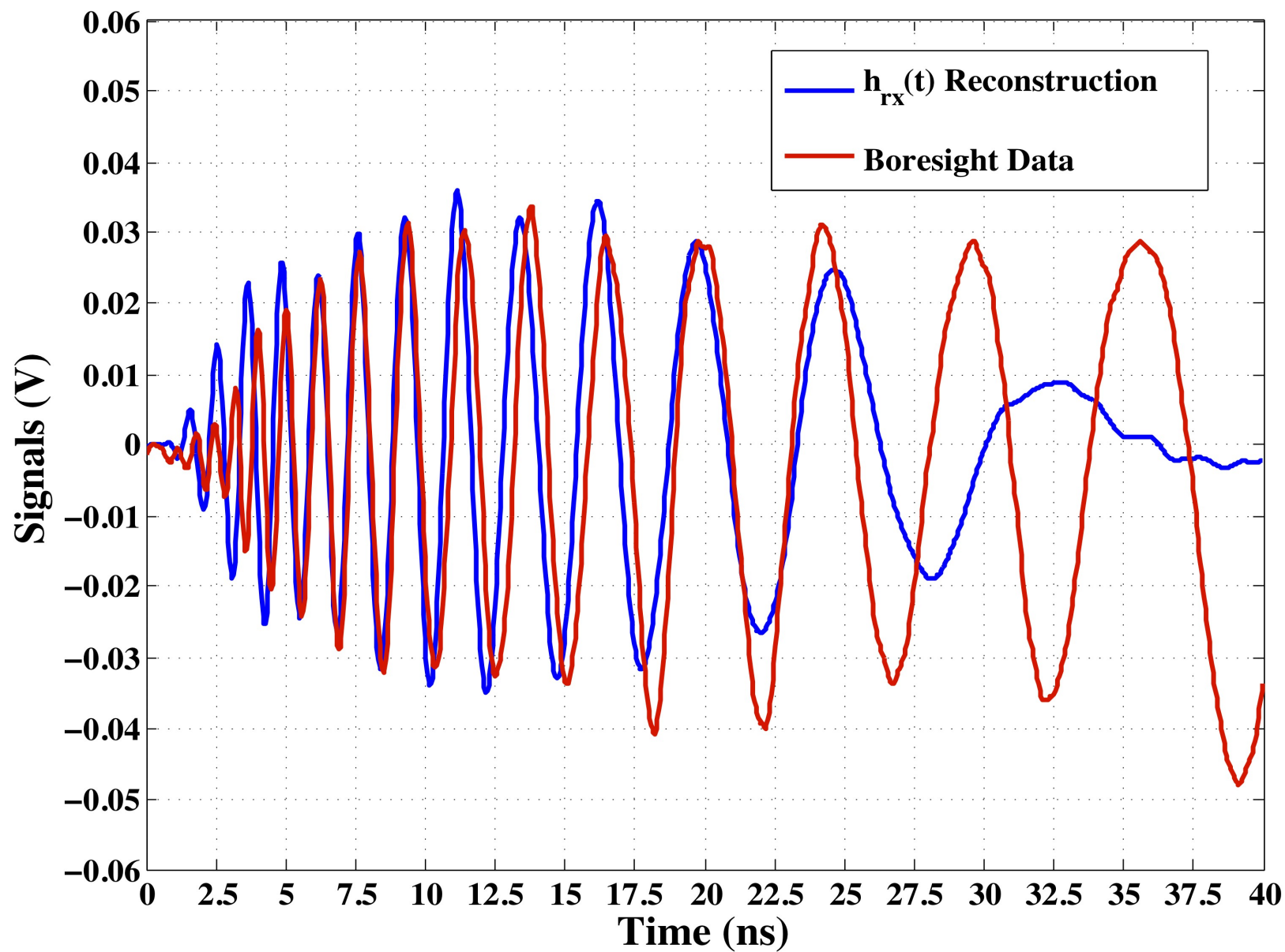
$$a(t) = (2/\pi)^2 \tan^{-1}(t/t_0) \tan^{-1}(-(t-t_{\text{end}})/t_1)$$

$$R = \frac{1}{N} \sum_i^N (f_{\text{data}}(t_i) - f_{\text{model}}(t_i))^2$$

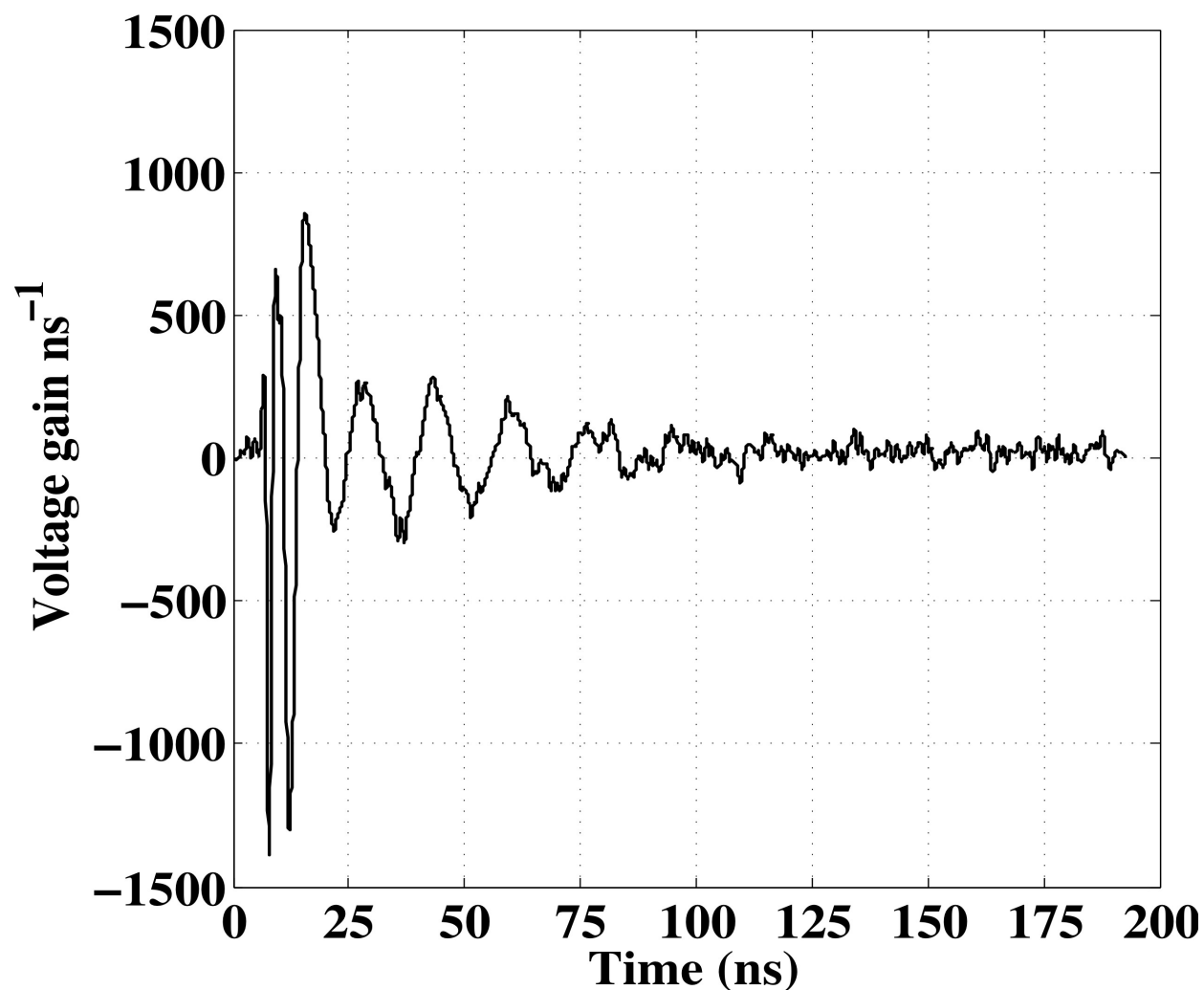
Main Result #3: Bore-sight $h_{rx}(t)$



Main Result #3: Bore-sight $h_{rx}(t)$



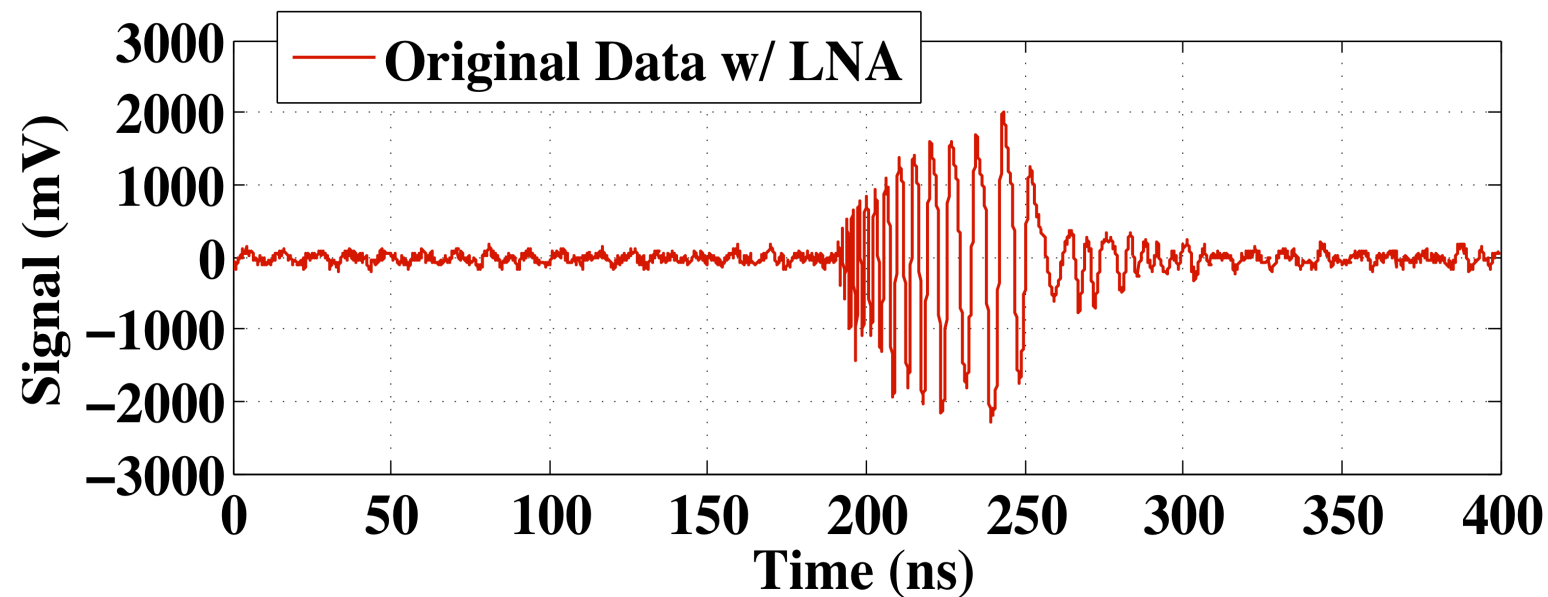
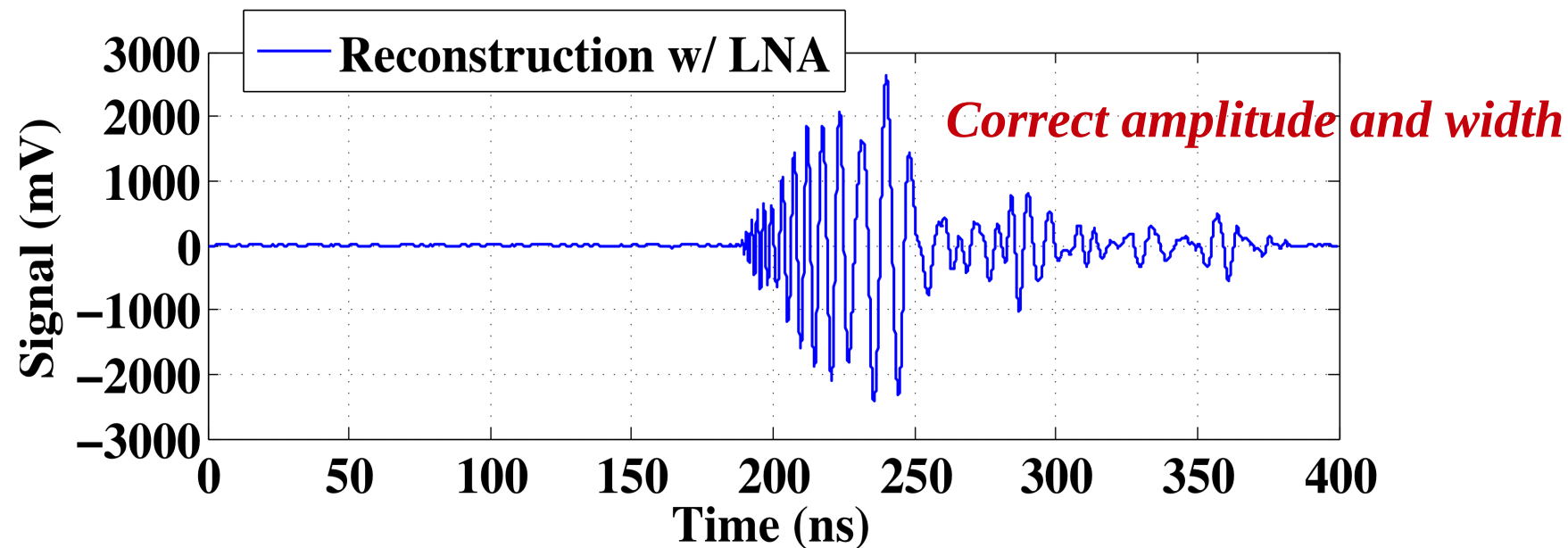
Main Result #4: Bore-sight $h_{rx}(t)$ w/ Amplifier



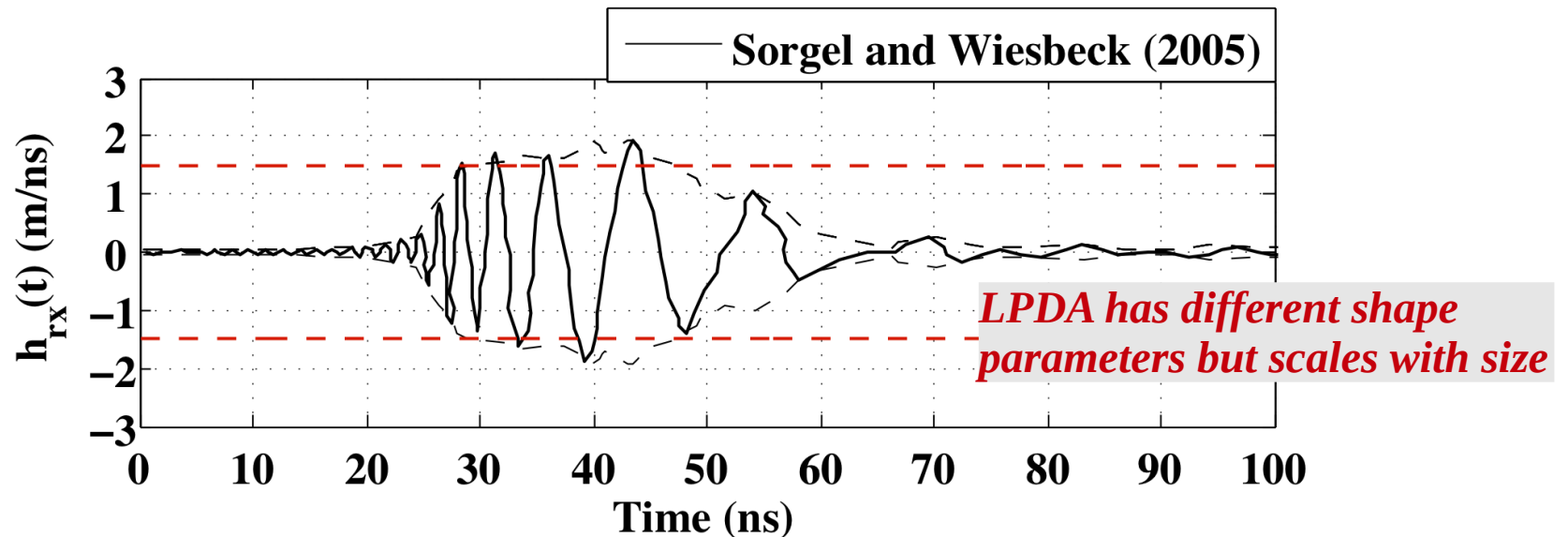
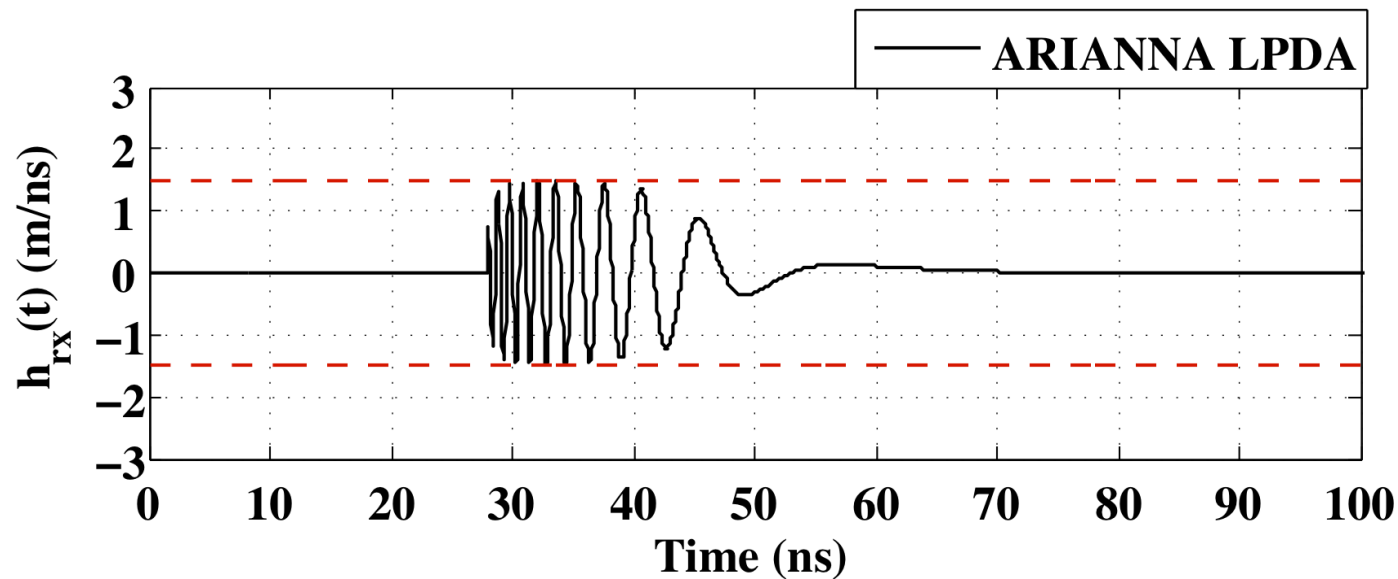
Credit: James Walker and Steve Barwick, UCI

$$V_L(t) = \frac{1}{(2\pi r c)} \frac{Z_0}{Z_L} H_{\text{amp}}(t) \circ \vec{h}_{rx}(t) \circ \vec{h}_{rx}(t) \circ \partial_t V_{src}(t)$$

Main Result #4: Bore-sight $h_{rx}(t)$ w/ Amplifier

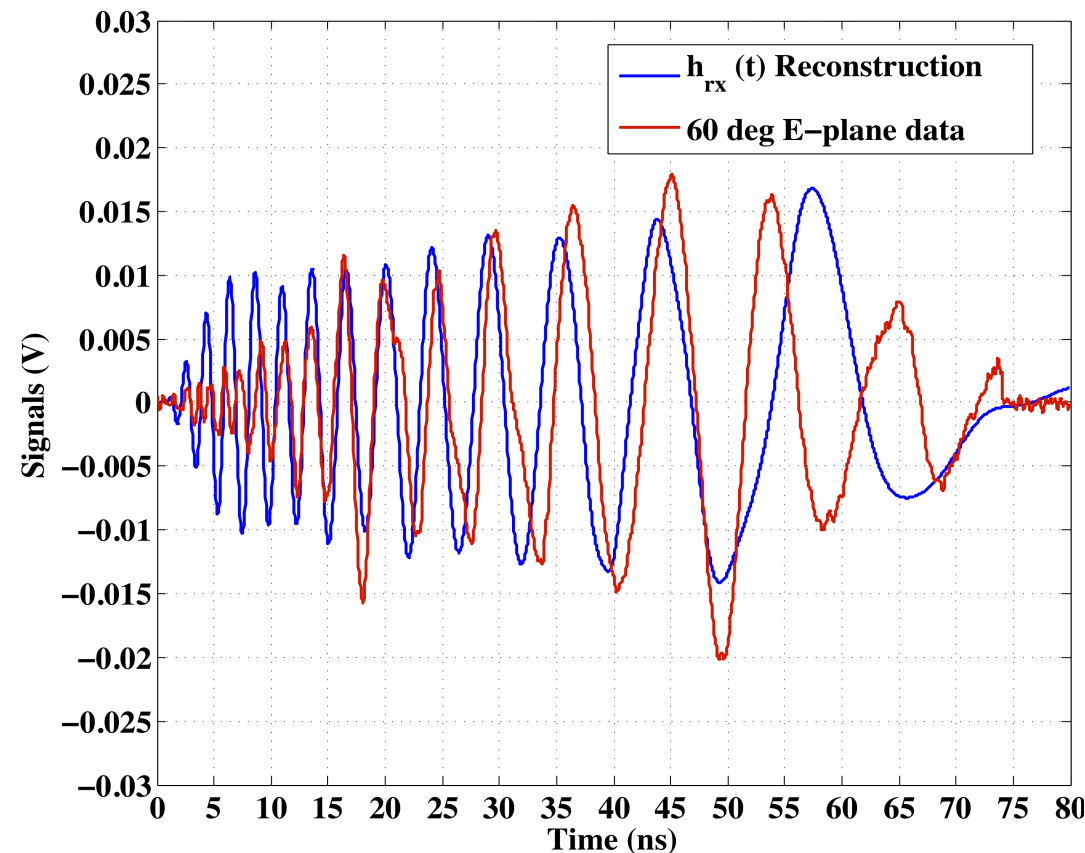
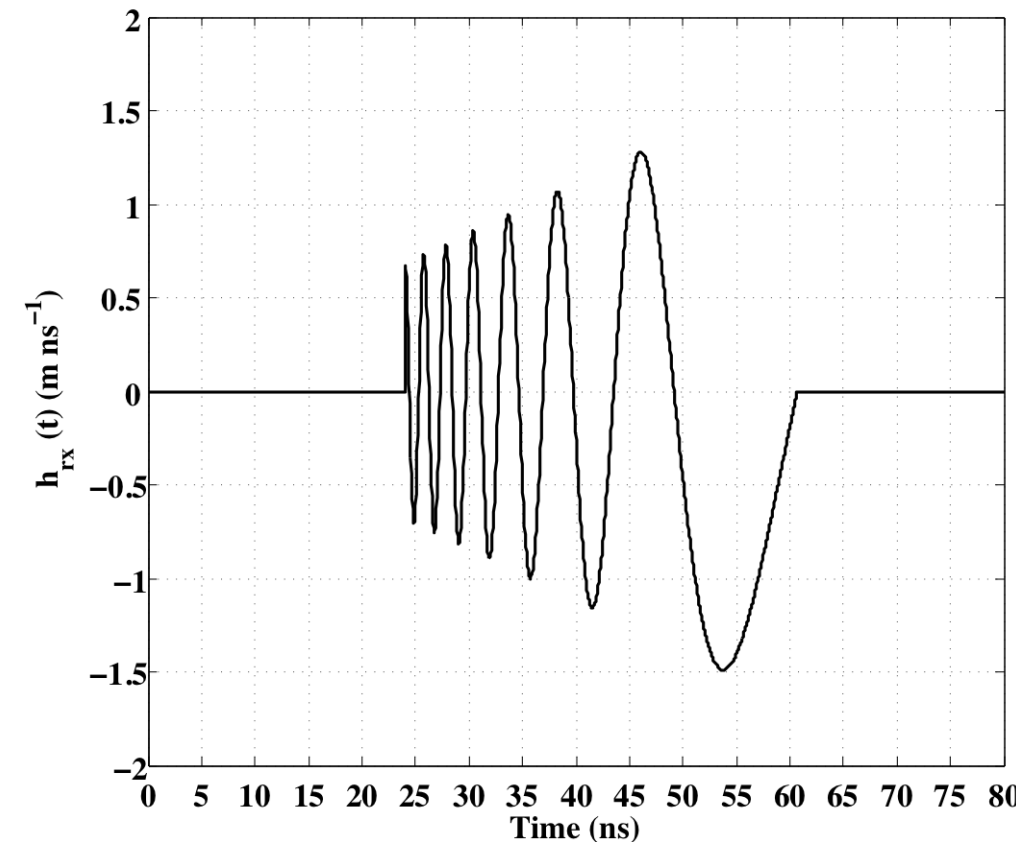


Comparing Effective Height to Others' Results



Note: data from this reference has been scaled to match LPDA sizes.

Checking off-axis: 60 degrees in E-plane



Effective height: Similar height at late times and lower frequencies, but frequency modes above 600 MHz are missing (early times).

Reconstruction: Early times (500-600 MHz) are large, but excellent match after 15 ns. The overall signal is much longer.

Interactions with Askaryan Electric Fields, Comparisons with Monte Carlo simulation

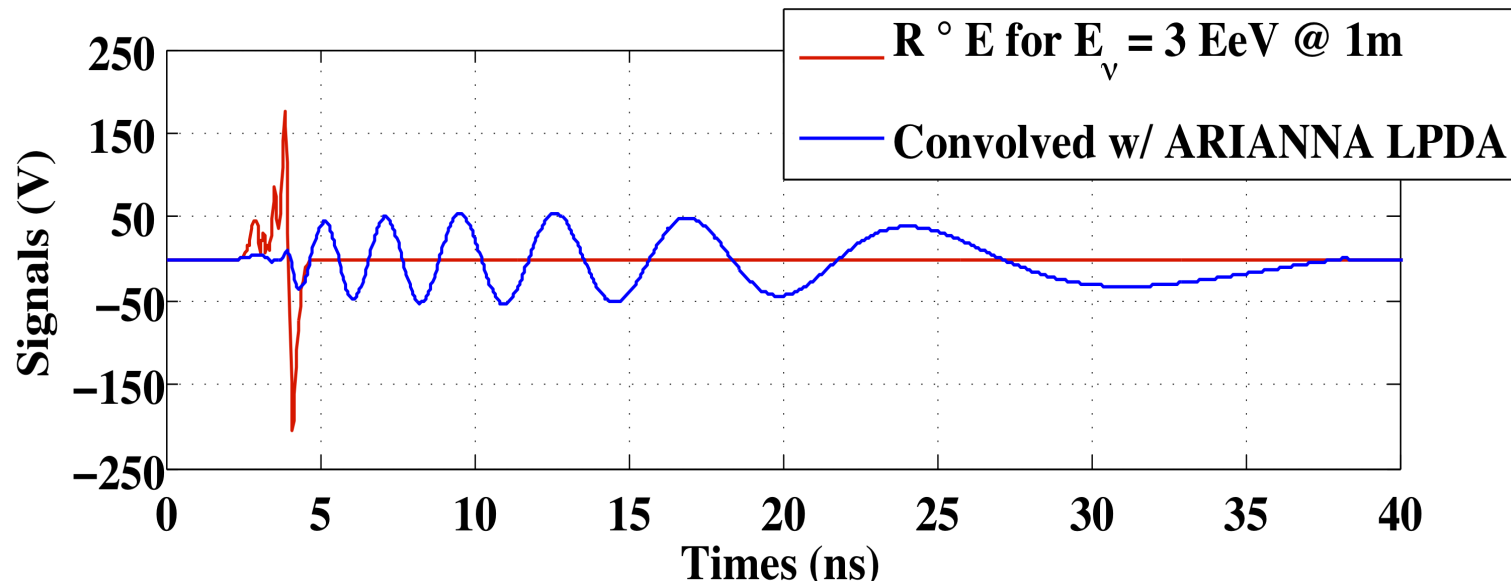
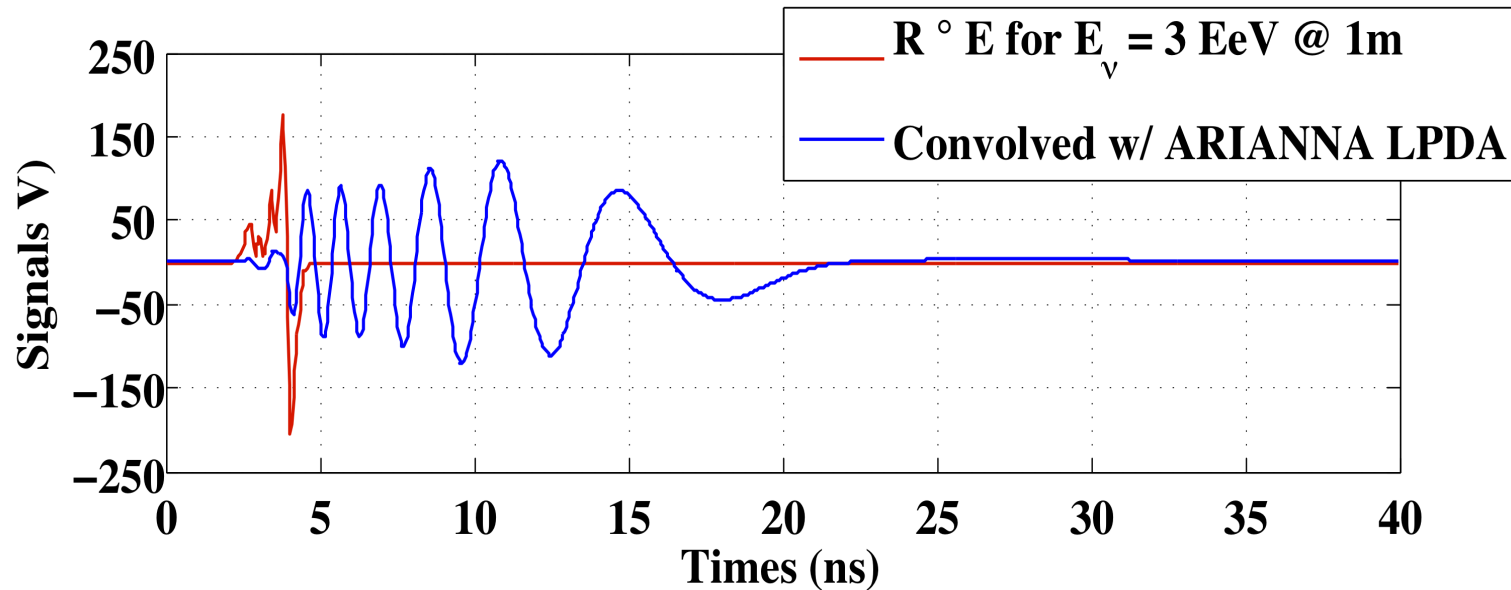
- *Electric field strength typically parameterized from data, with respect to energy and frequency (Saltzberg et al., 2000), (Alvarez-Munis et al., 2010)*
- *Observed strength depends on viewing-angle with respect to Cherenkov angle*
- *Propagation and attenuation (λ = attenuation length)*
- *Signal voltage depends on viewing angle of the antenna*

$$E_{1m} = \frac{2.53 \times 10^{-7} E_v [TeV] (v/v_0)}{1 + (v/v_0)^{1.44}} \quad (V m^{-1} MHz^{-1})$$

$$E_{1m}(\theta_v) = E_{1m} \frac{\sin(\theta_v)}{\sin(\theta_c)} \exp\left(-\ln 2 \left((\theta_v - \theta_c)/\Delta \theta\right)^2\right) \quad (V m^{-1} MHz^{-1})$$

$$V_{LPDA} = P(\theta_v) \frac{\Delta v}{\sqrt{2}} \frac{\sin \theta_v}{\sin \theta_c} \exp \frac{-r/\lambda}{r} \sum_i E_{1m}(\theta_v) h_{eff}(v_i)$$

Main Result #5: Comparing Monte Carlo with Time-Domain Calculation



Conclusion

- **Discussed UHE neutrinos, the Askaryan Effect**
- **Mathematics of converting electric field waveform to voltage waveform**
- **Measured antenna properties, including conversion from E-field to voltage waveform**
- **Demonstrated angular monte carlo agreement, and computed neutrino waveforms entering ARIANNA DAQ.**
- **Future work: must span the angular space to generalize the fits, improve high-frequency agreement**

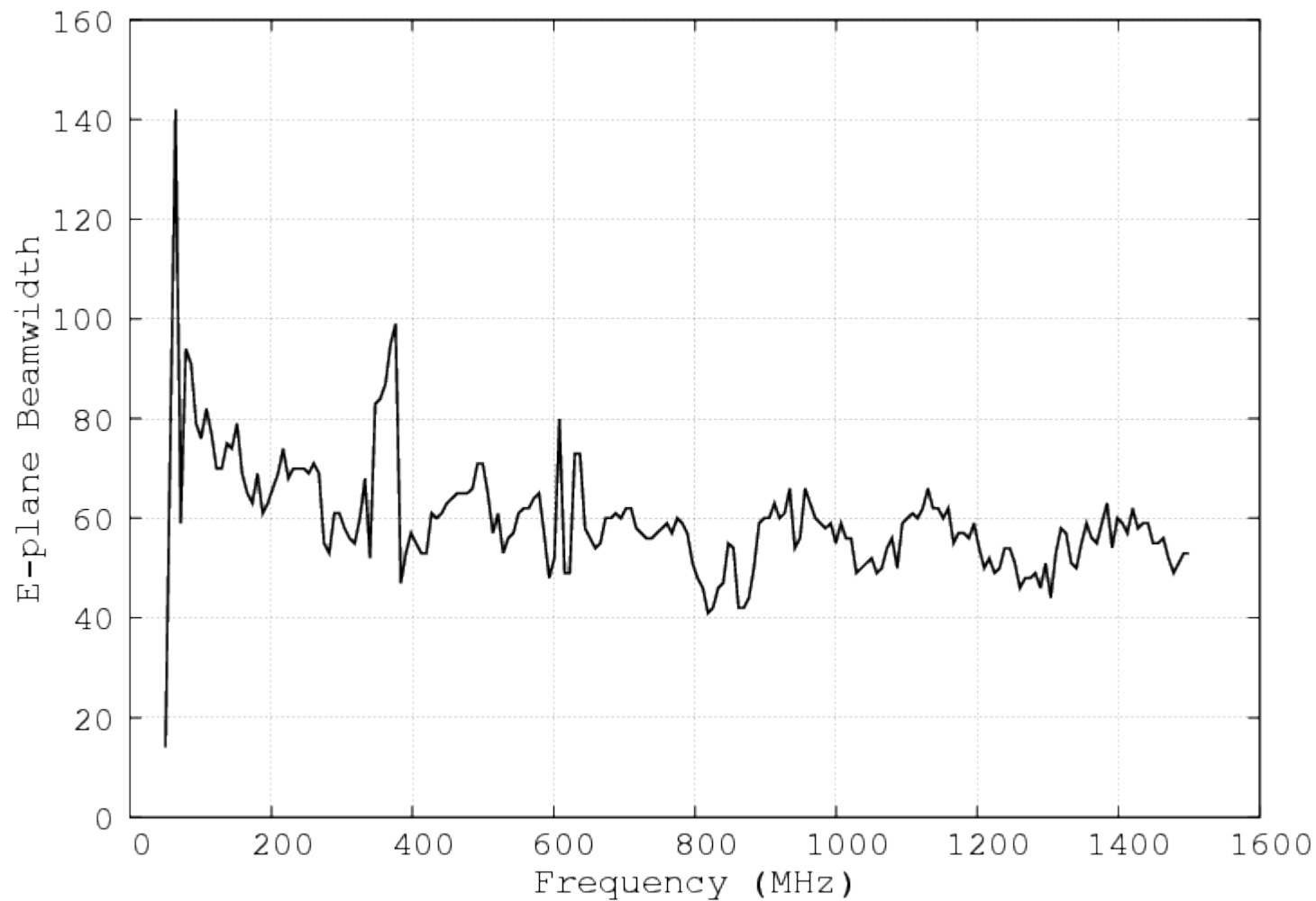
References

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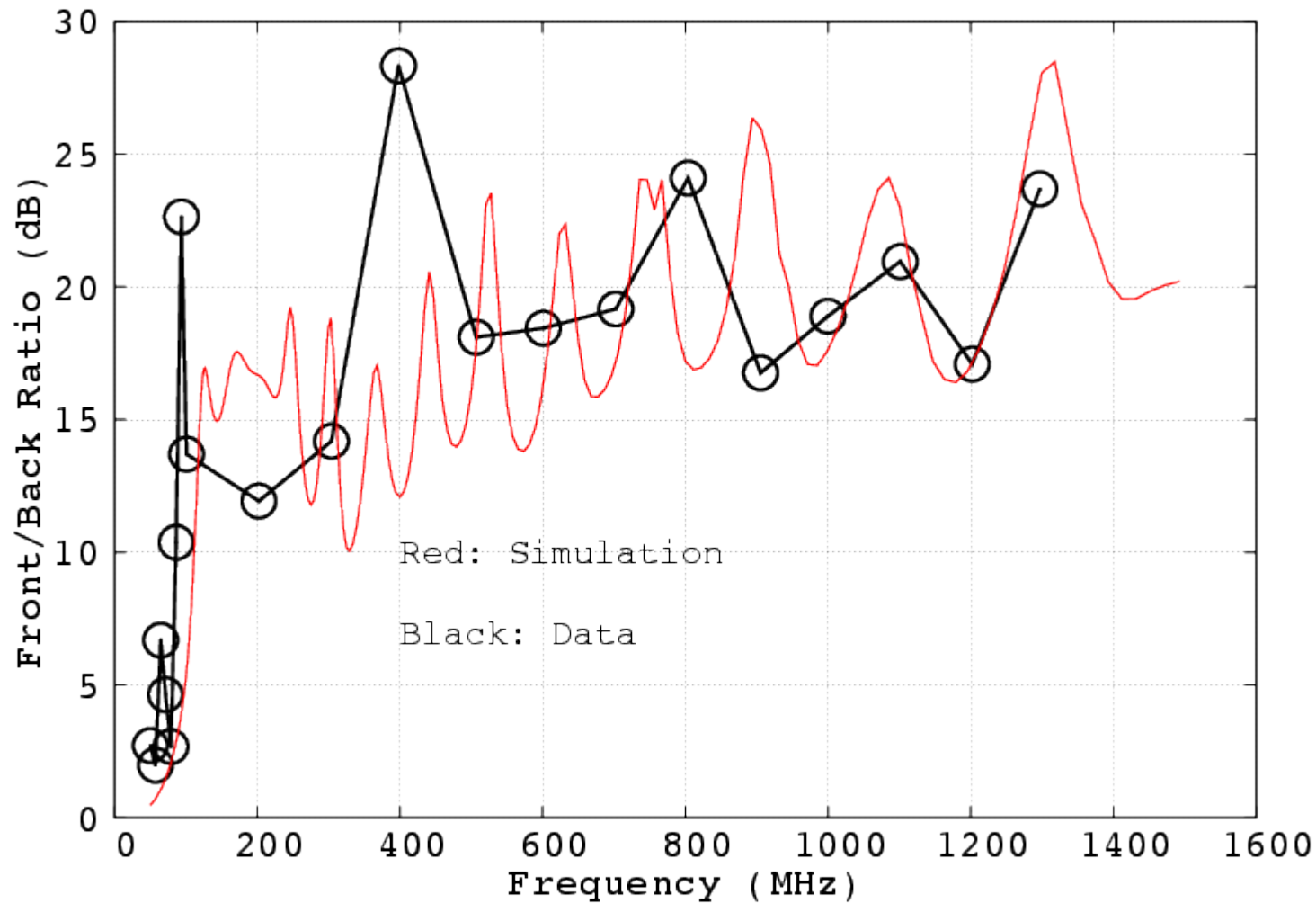
Backup slides



E-Plane beam-width ~ 60 degrees



Front-Back Ratio ~ -15 dB



Gain vs. Frequency

