

Optimization of timing performance of large-area FBK SiPMs in the scintillation light readout.

A. Gola, A. Ferri, C. Piemonte, A. Picciotto,
T. Pro, N. Serra, A. Tarolli, N. Zorzi

<http://srs.fbk.eu>

Overview of the SiPM technology at FBK

Original technology

2006

2010-11

RGB-SiPM

(Red-Green-Blue SiPM)

- excellent breakdown voltage uniformity
- low breakdown voltage temperature dependence (gain variation < 1%/C)
- higher efficiency
- lower noise

2012

NUV-SiPM

(Near-UV SiPM)

- excellent breakdown voltage uniformity
- low breakdown voltage temperature dependence (gain variation < 1%/C)
- high efficiency in the near-ultraviolet
- very low dark noise

2012

RGB-SiPM_HD

(Red-Green-Blue SiPM – high density)

- small cell size with high fill factor:
 - high dynamic range
 - low excess noise factor

Redesigned cell border, for obtaining **small cells with high Fill Factor (FF)**.

The 15 um cell RGB-HD has the same FF of the 50 um cell RGB technology.

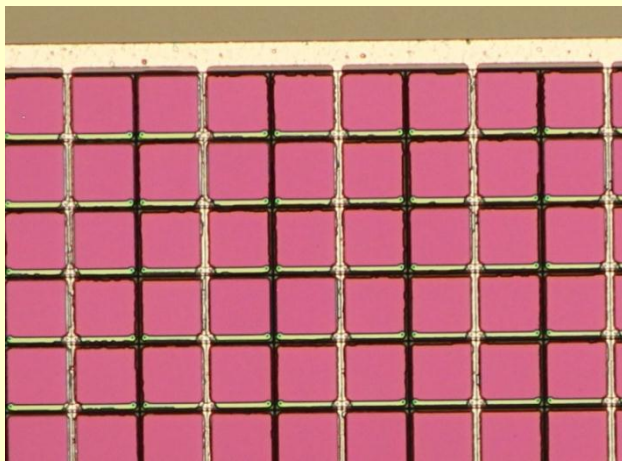
SiPM:

size: **4x4mm²**

cell size: **30x30um²**

cells: ~17000

Fill factor = 74%



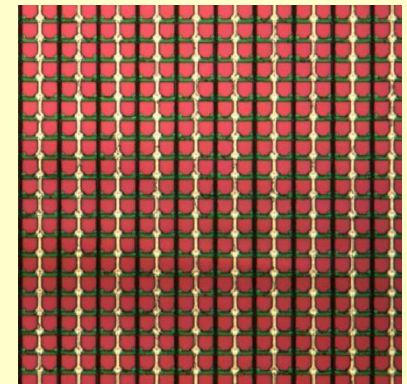
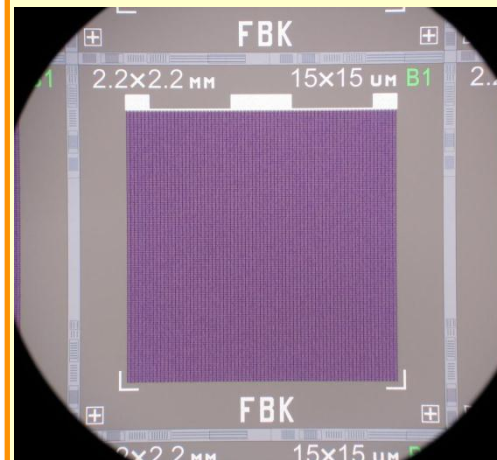
SiPM:

size: **2.2x2.2mm²**

cell size: **15x15um²**

cells: 21316

Fill factor = 48%



2.2x2.2mm² 15um

Response to fast light pulse from LED

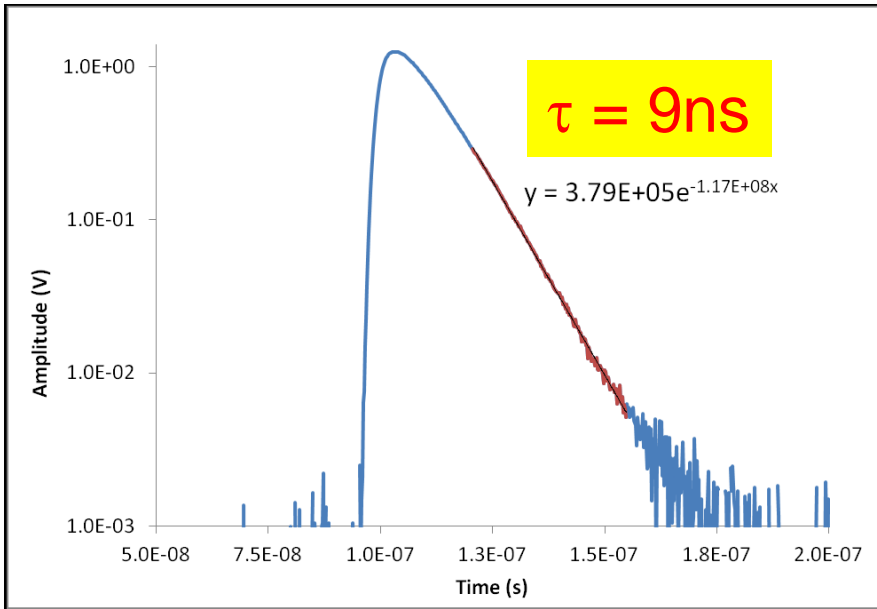
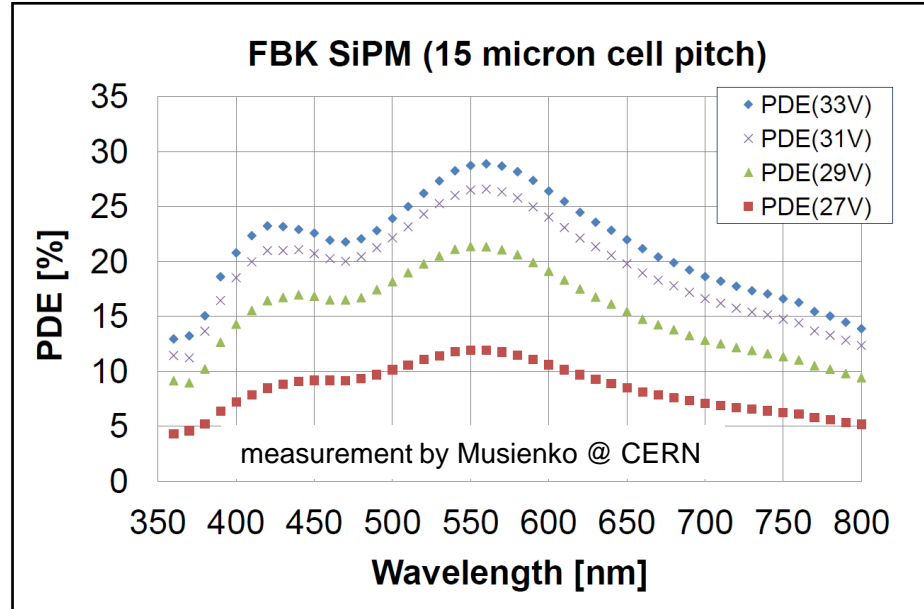


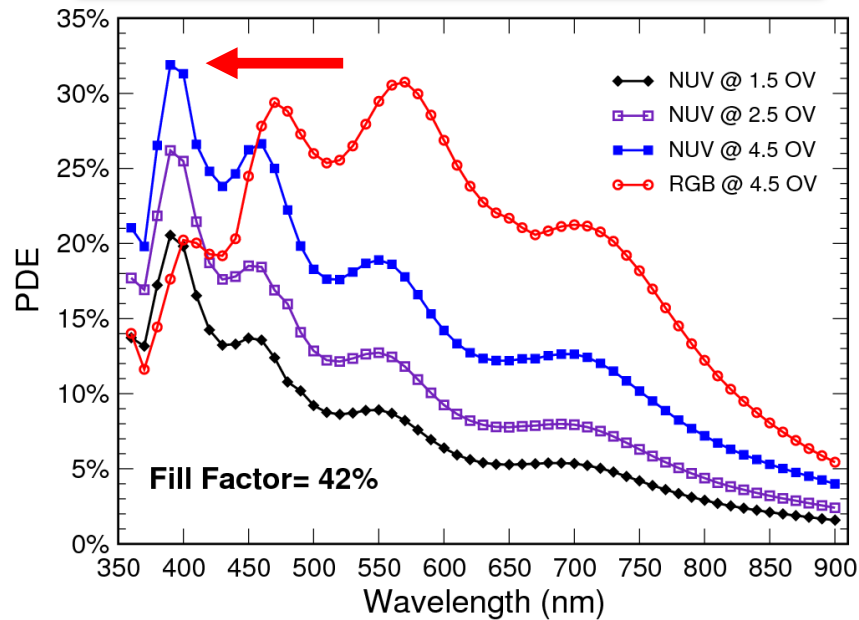
Photo-detection efficiency



very short decay!!

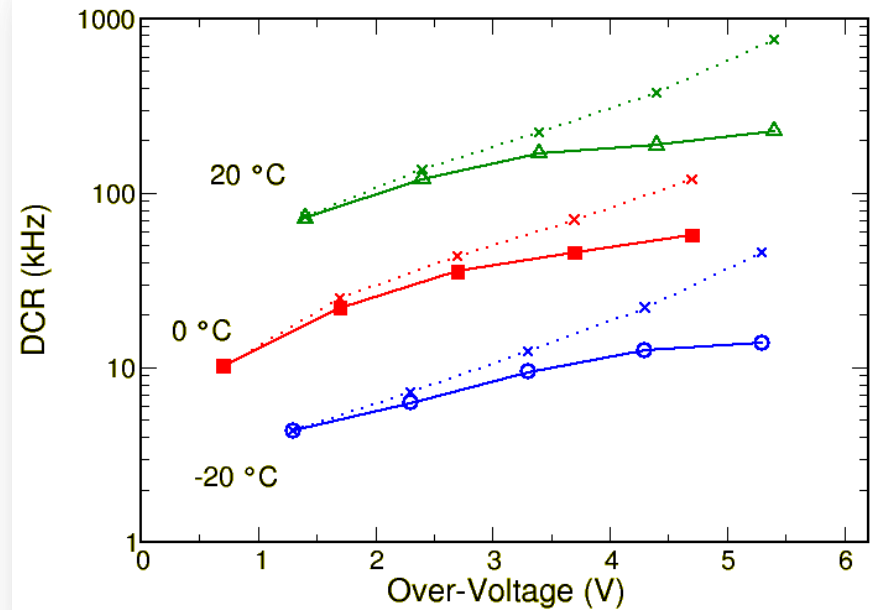
The NUV SiPM is based on a **p-on-n junction**, for **increased PDE at short wavelengths**.

Increased PDE at low λ



PDE vs. wavelength for a NUV-SiPM and RGB-SiPM with $50 \times 50 \mu\text{m}^2$ cell, 42% fill factor.

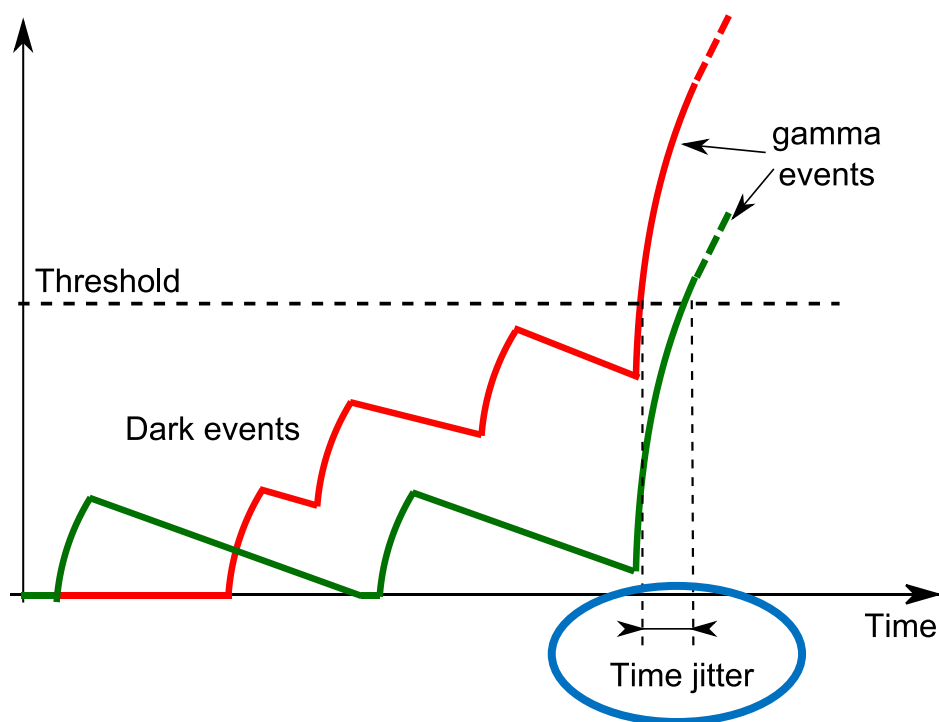
Very low primary DCR



NUV-SiPM: $1 \times 1 \text{mm}^2$ $50 \times 50 \mu\text{m}^2$. *Total and primary dark count rate at 0.5 phe.*

Effects of the SiPM noise: Dark Count Rate

Leading Edge Discriminator (LED) is commonly used for time pick-off with PMTs.



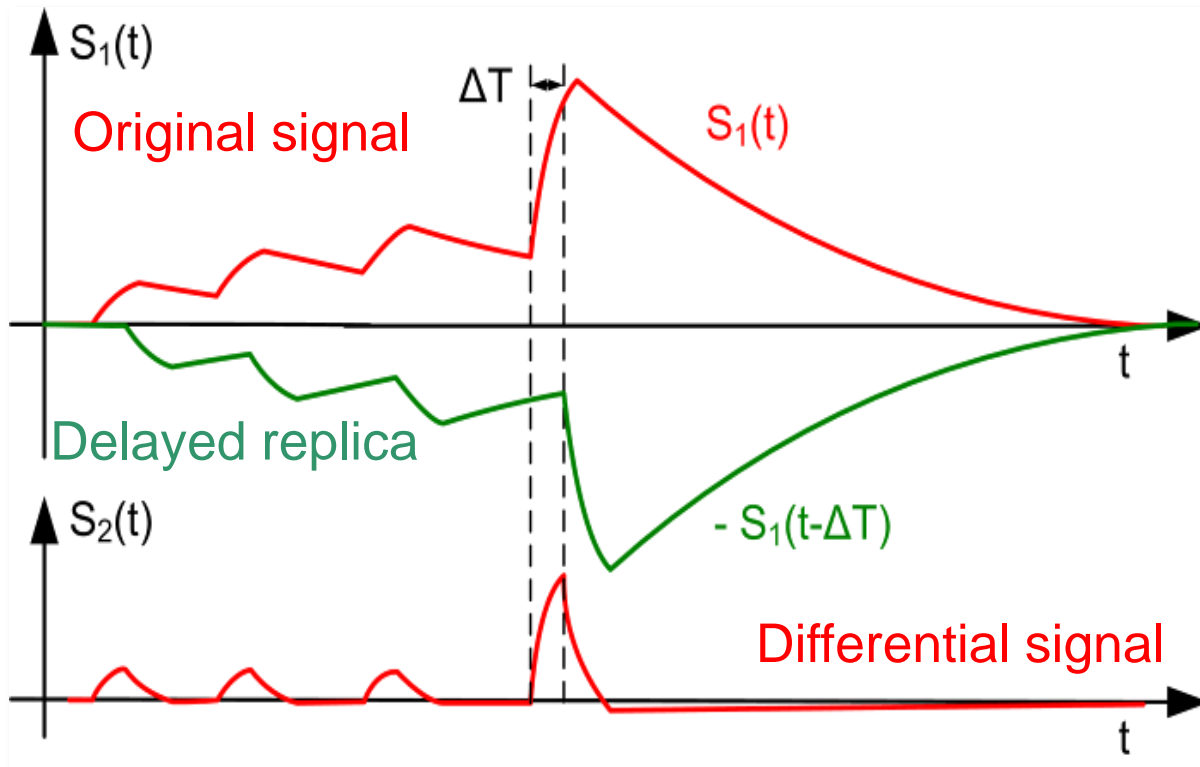
long tail of the
dark events

high dark rate

baseline fluctuation
→ **time jitter**

high LED threshold
→ **worse photon stat.**

In **large area SiPMs** the dark rate can be quite high and consequently also the effect described above.



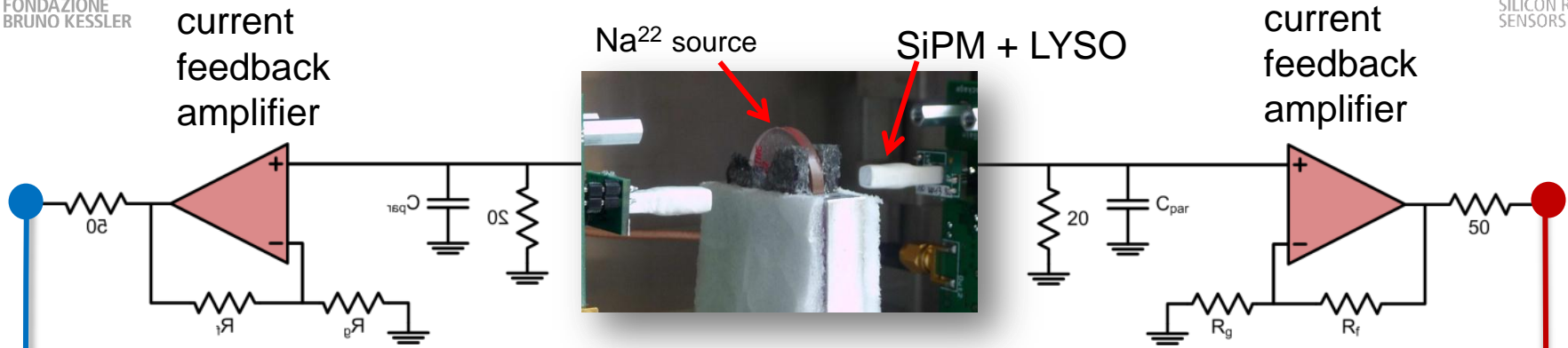
We exploit the difference between rise time and decay time to obtain a signal:

- “free” from baseline fluctuations
- identical initial part of the gamma signal

Then, we use the LED on the differential signal $s_2(t)$.

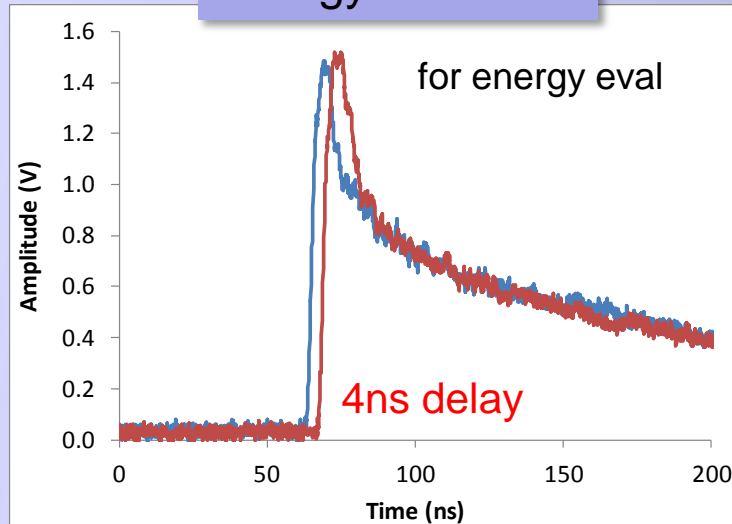
Important: electronic noise is $\sim \sqrt{2}$ higher in differential signal so its effect must be negligible for DLED to be effective

Experimental set-up

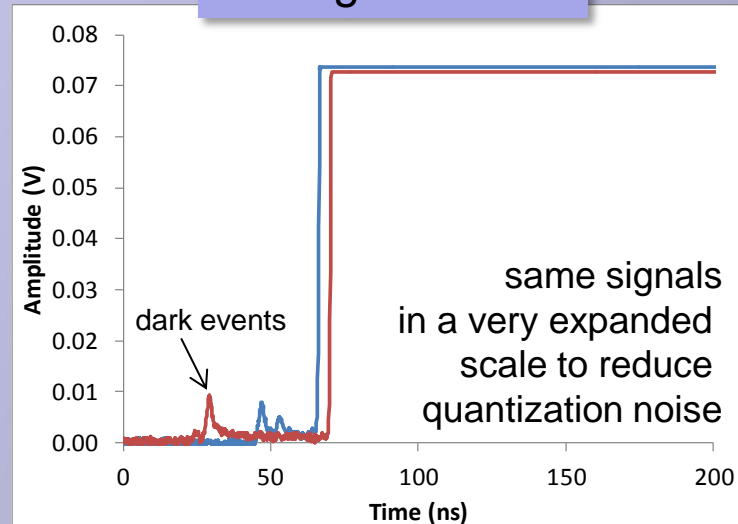


Digital scope (1GHz, 10GSa/s, 8 bit ADC)

Energy channels



Timing channels



Ch1

1MΩ

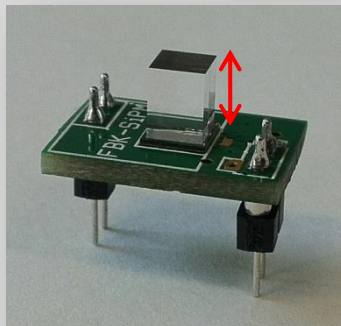
Ch2

Ch3

50Ω

Ch4

Detector “cube”

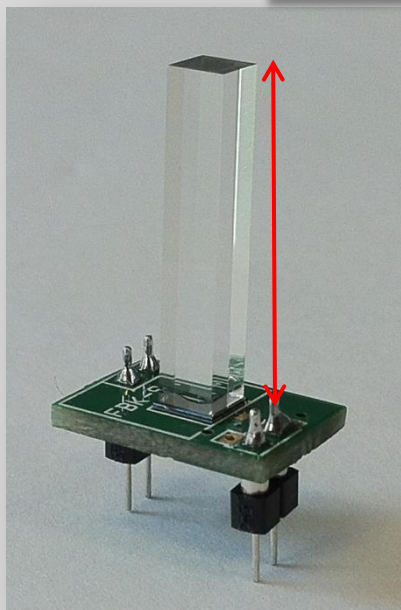


LYSO crystal $3 \times 3 \times 5 \text{mm}^3$

height \sim side

to test ultimate SiPM performance

Detector “PET”



LYSO crystal $3 \times 3 \times 15 \text{mm}^3$

height \sim 5 x side

real PET configuration
(timing affected by light propagation in crystal)

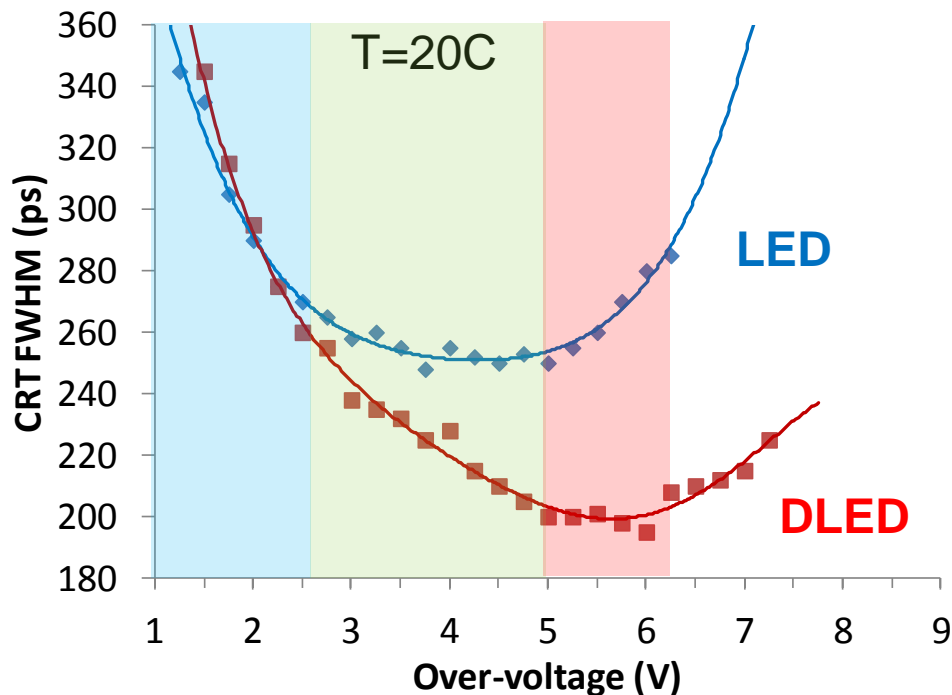
SiPMs used

- $3 \times 3 \text{mm}^2$
- $4 \times 4 \text{mm}^2$

67um cell-size

produced by FBK, Trento

**Detector cube,
3x3mm² SiPM**



**DLED $\Delta T=500$ ps
good up to 1ns**

Low over-voltage:

low gain, low dark rate

- ➔ electronic noise dominates
- ➔ DLED slightly worse than LED

Medium over-voltage:

gain increases

dark noise ampl. > elect. noise

- ➔ LED is flat (increase of PDE is compensated by increase of noise)
- ➔ DLED improves following PDE

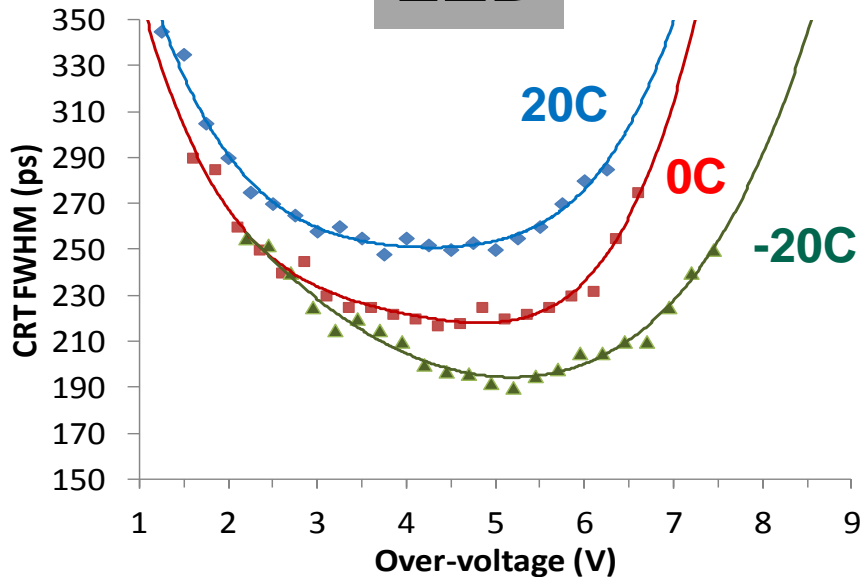
High over-voltage:

high dark noise/rate

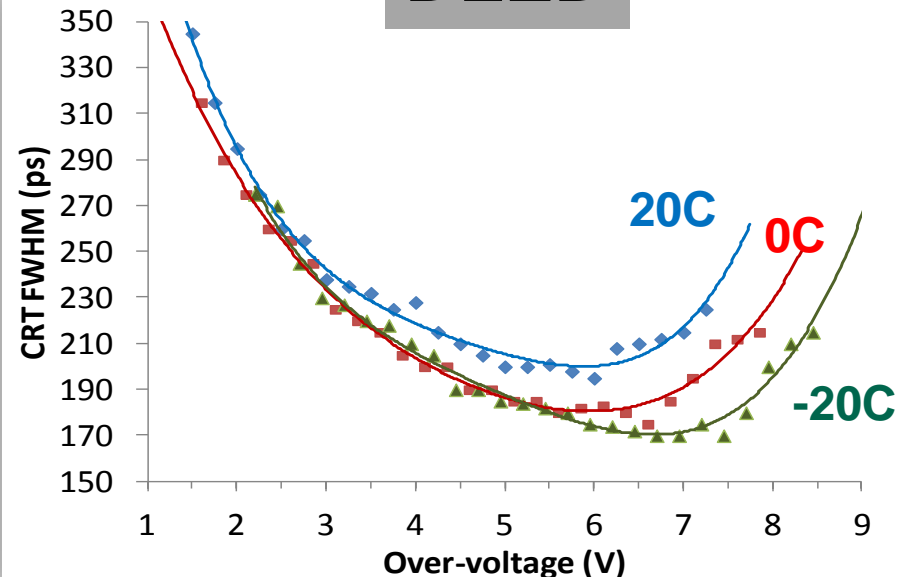
- ➔ LED starts deteriorating
- ➔ DLED still improves for high PDE and good noise compensation

**Detector cube
3x3mm² SiPM**

LED



DLED



LED strongly improves with temperature because of noise (DCR) reduction.

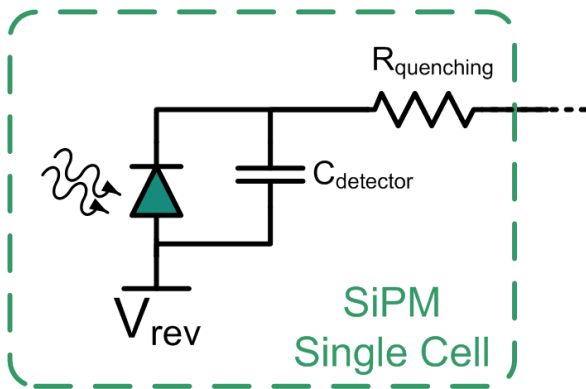
DLED improves less with temperature and only at high over-voltages.

LED@-20C is almost equivalent to DLED@20C

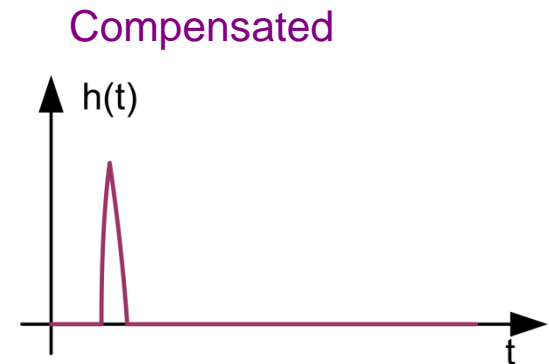
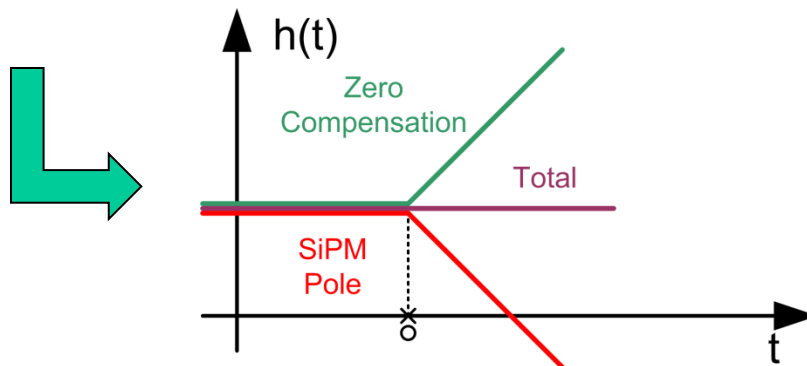
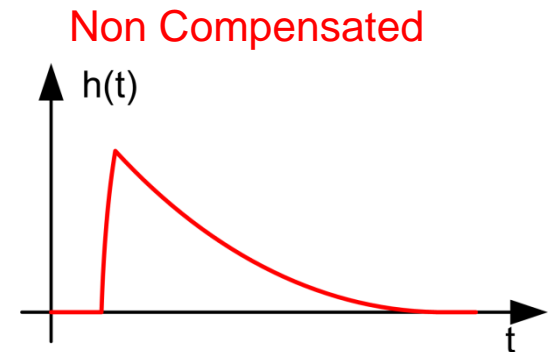
The DLED is **difficult to integrate** in an ASIC → **Pole-Zero Compensation**.

The passive recharge of the cells of the SiPM corresponds to **a single real pole in the pulse response** of the detector in the frequency domain.

→ **Pole cancellation** through a zero at the same frequency in the front end.

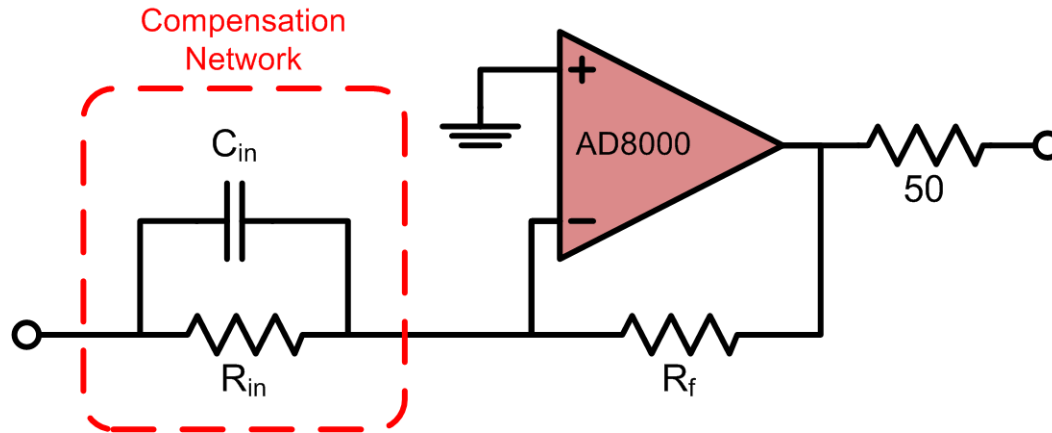


$$\tau = R_q C_d \Rightarrow$$



The PZ in the Time Domain

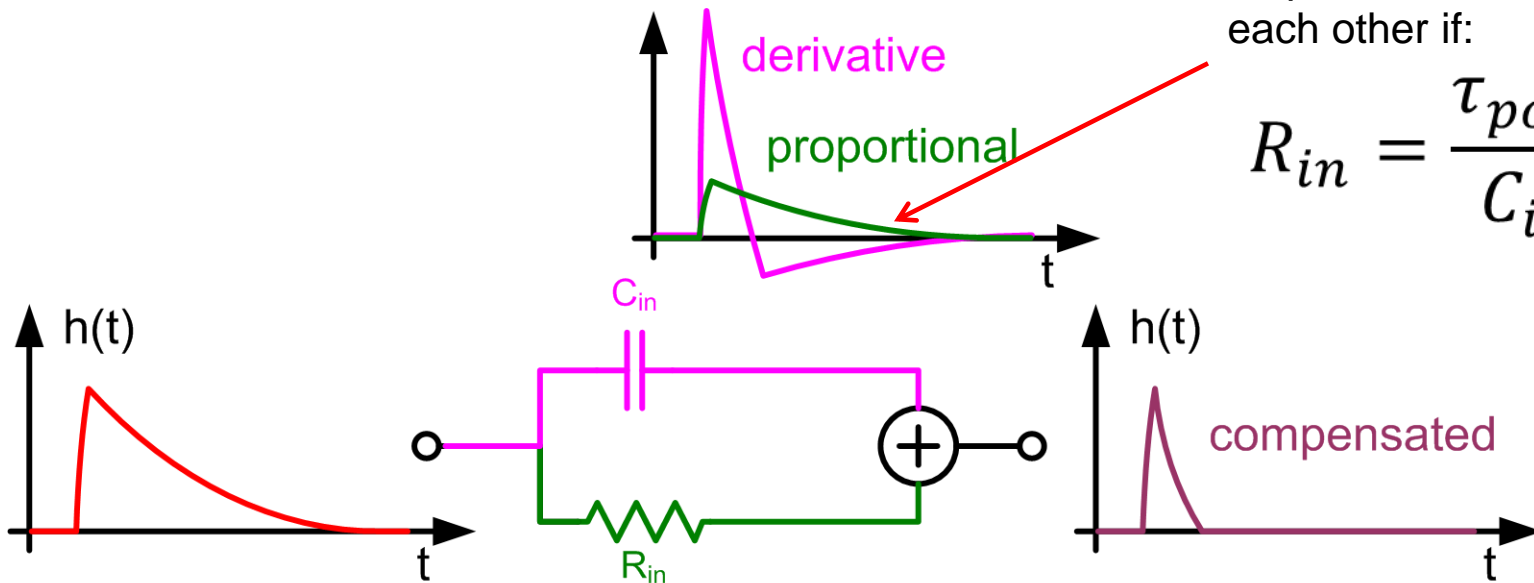
$$\tau_{in} = R_{in} C_{in}$$



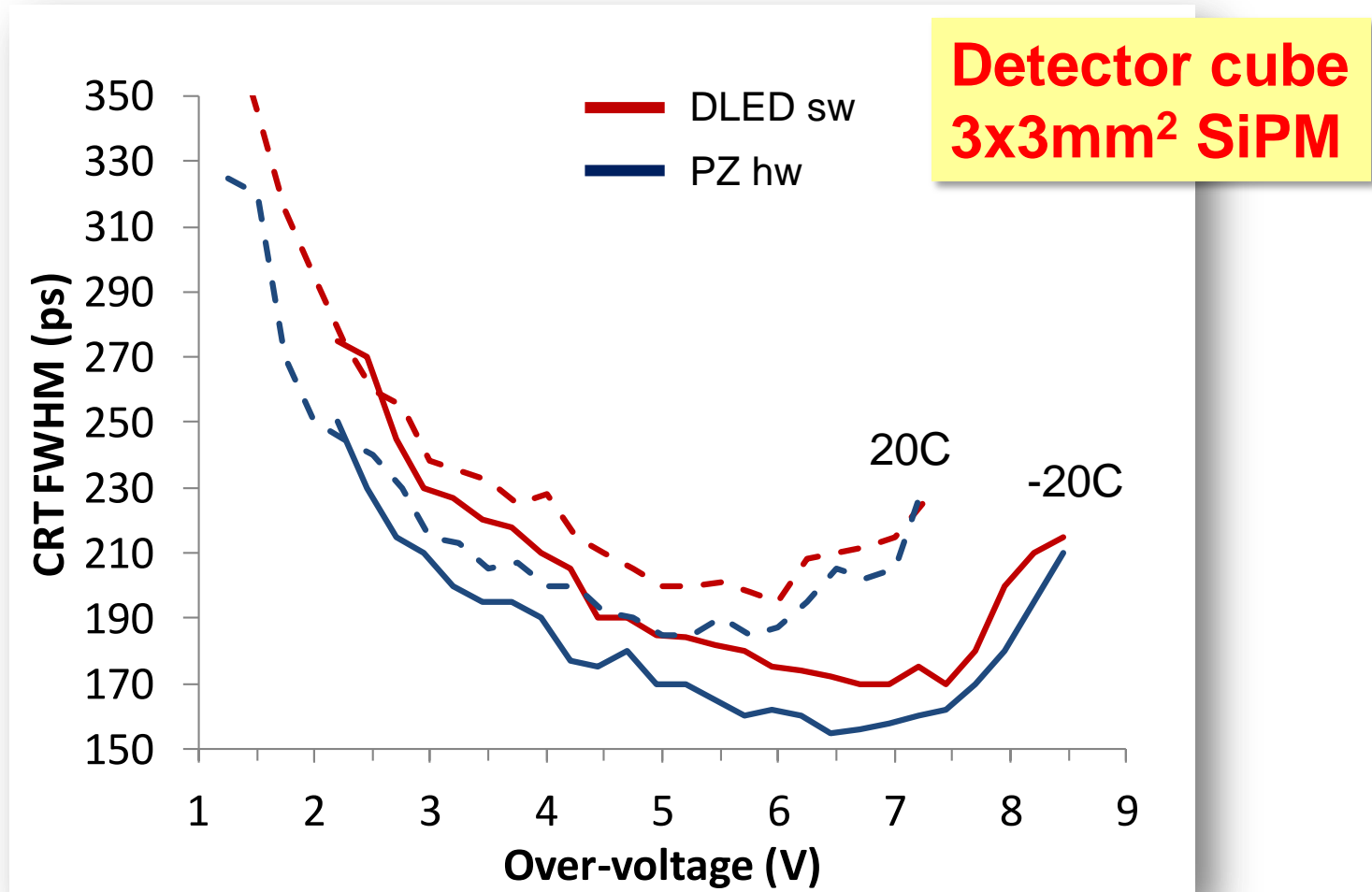
Simple circuit implementation of the PZ method.

The tails have equal amplitudes and cancel each other if:

$$R_{in} = \frac{\tau_{pole}}{C_{in}}$$

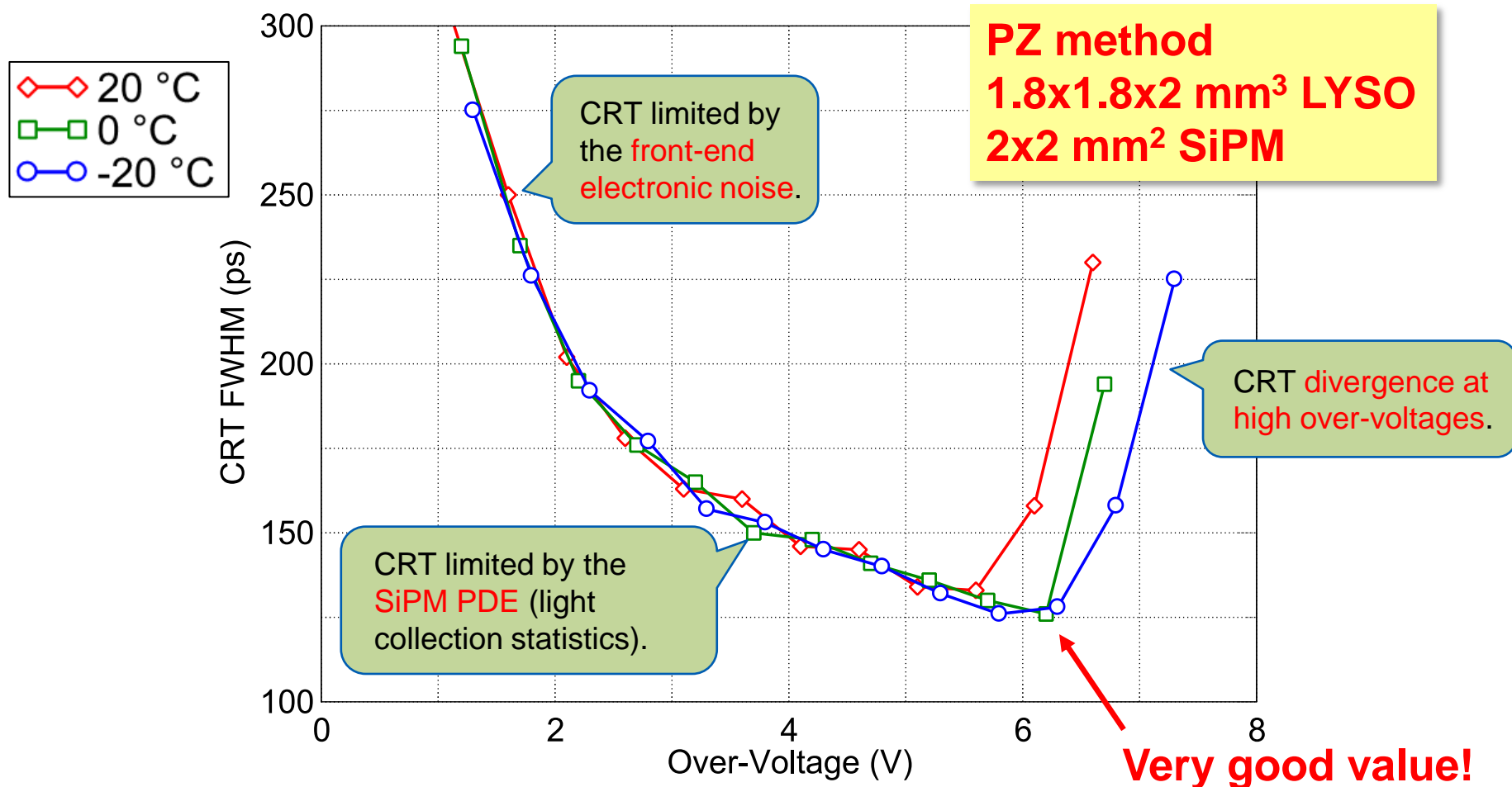


The results are comparable or slightly better with the PZ method than with DLED → less noise without numerical differentiation.

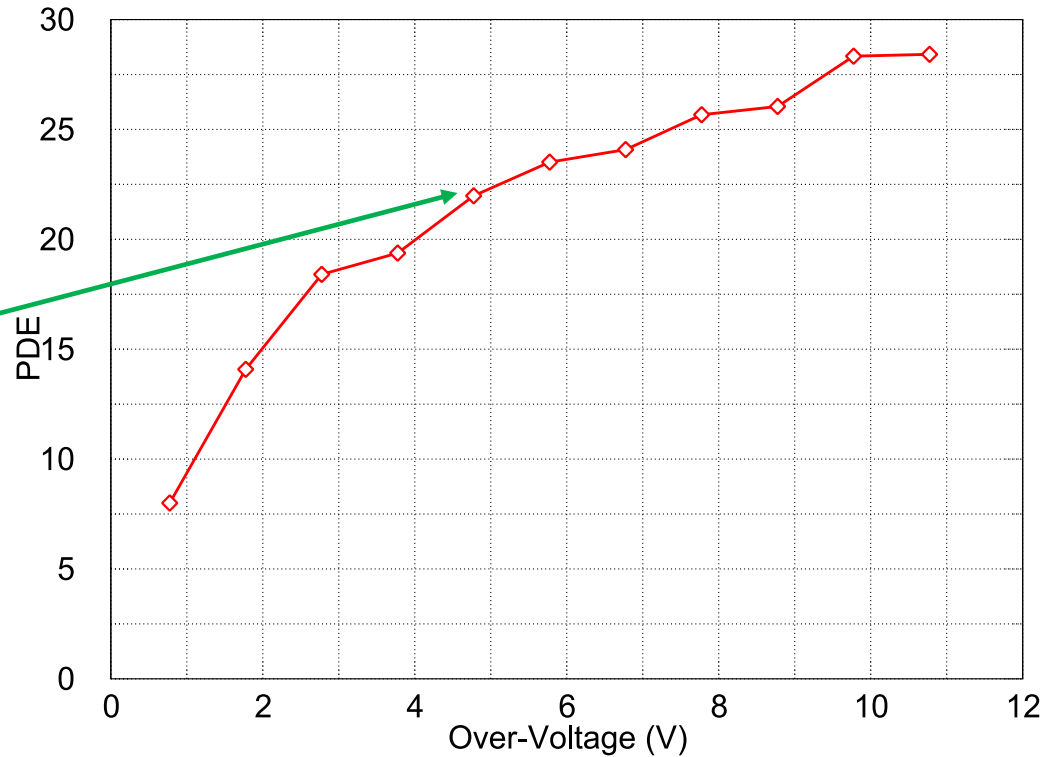
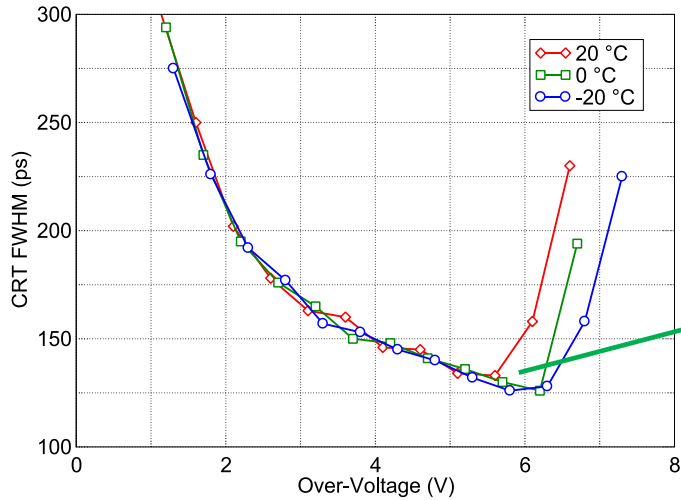


Effects of the SiPM noise: Optical Cross-talk Amplification

With Pole-Zero noise compensation and smaller detectors we observe almost **no dependence of the measured CRT on the DCR of the detector** → **timing resolution should be limited by PDE of the device only.**

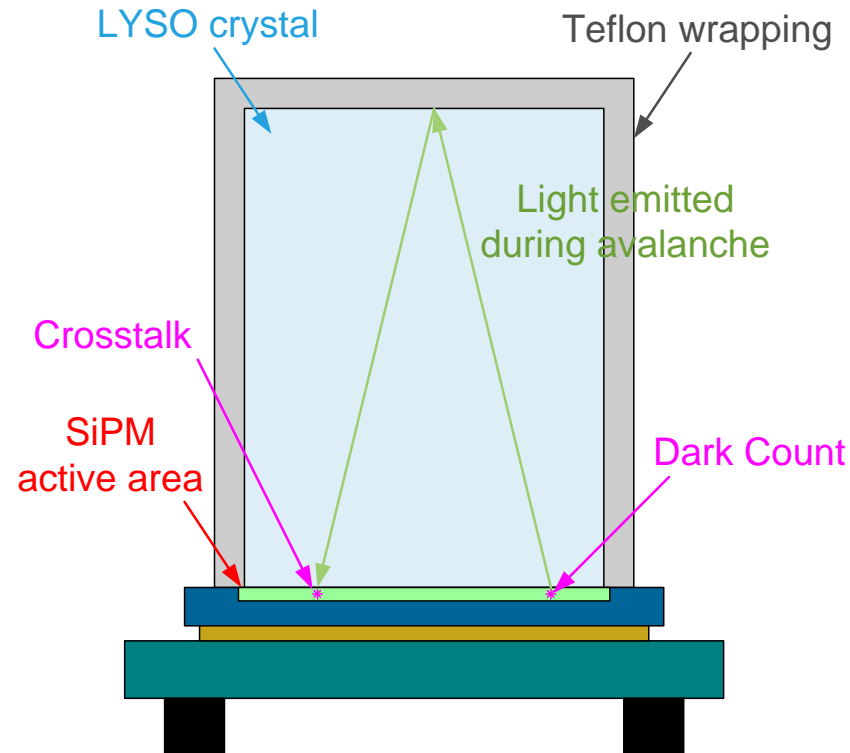


The optimum CRT value is not obtained at maximum PDE.



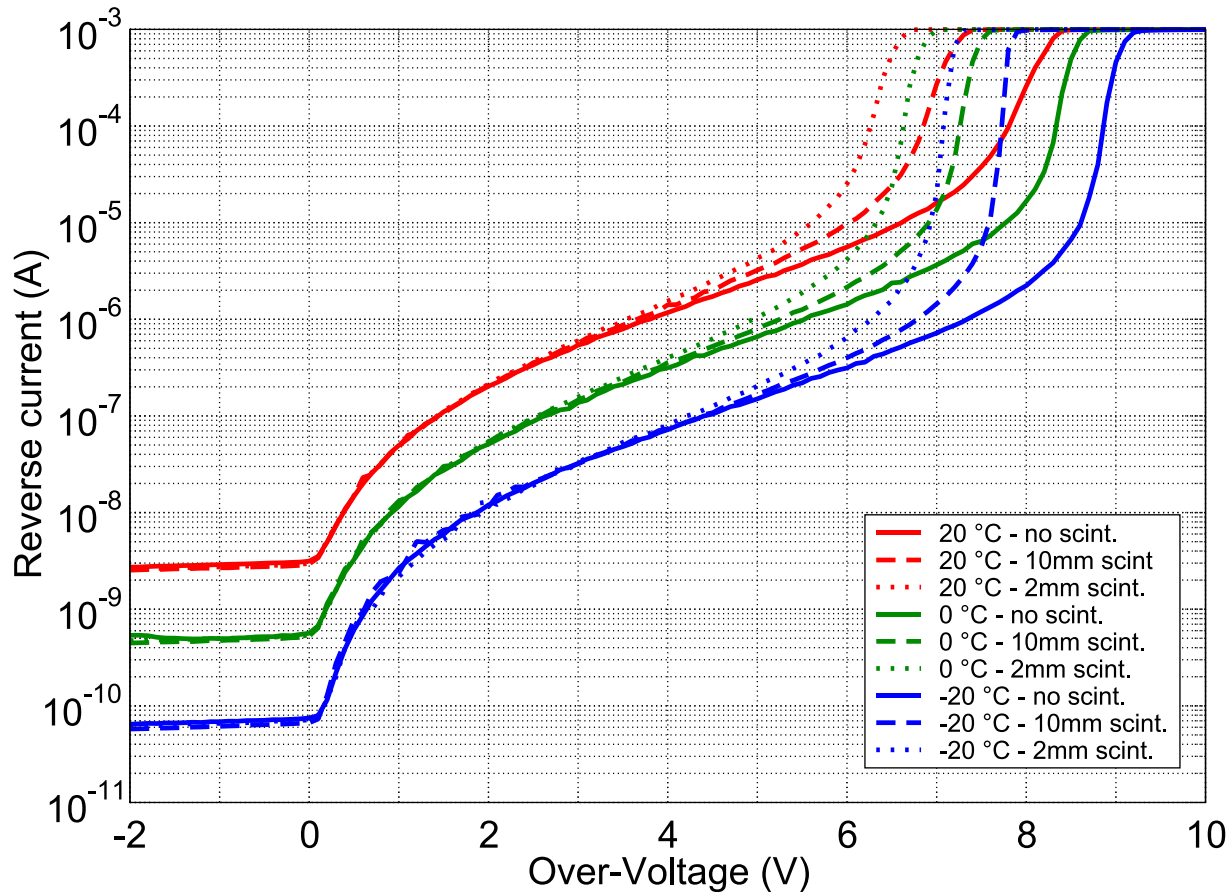
There is some other effect that prevents to operate the device at higher over-voltage and PDE.

The scintillator **reflects the photons emitted by the hot carriers** during the avalanche.



Increase in the collection efficiency of the optical cross-talk photons.

The phenomenon can be easily observed from the reverse current of the device, measured with and without the scintillator.



3 cases:

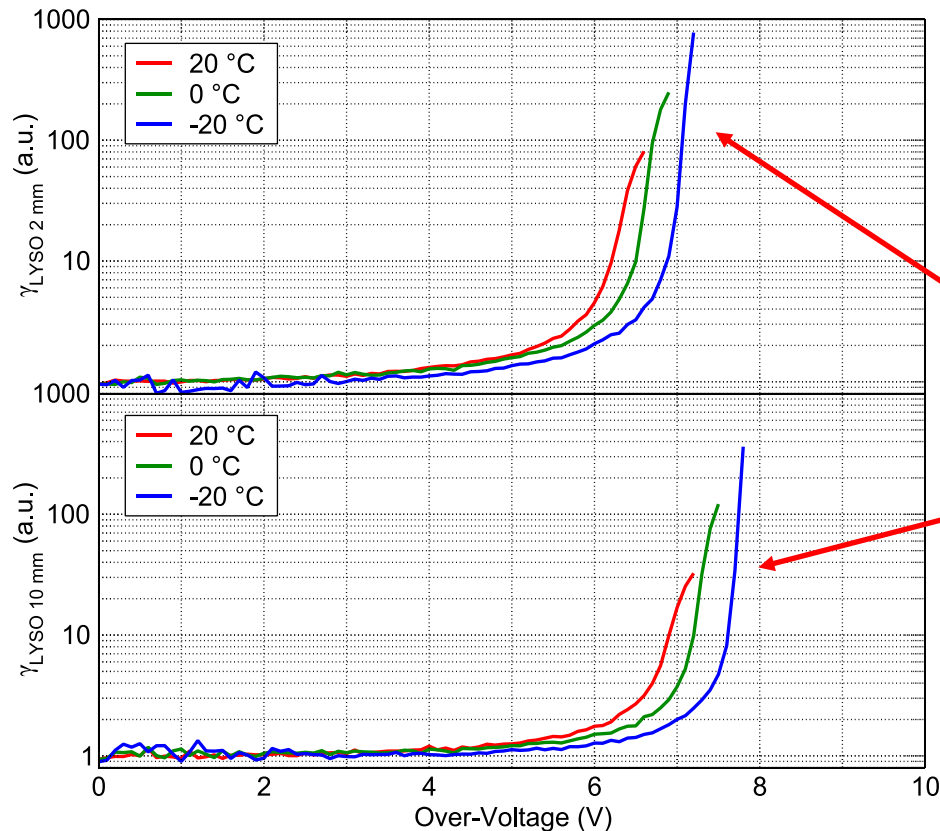
- No scintillator
- 2x2x2 mm³ LYSO
- 2x2x10 mm³ LYSO

3 temperatures:
20°C, 0°C, -20°C

The current increase is larger for the shorter scintillator.

It is possible to define a **DCR amplification coefficient** due to the **scintillator enhanced cross-talk**.

$$\gamma(V_{OV}) = \frac{I_{scint}(V_{OV})}{I_0(V_{OV})} = \frac{DCR_{scint}(V_{OV})}{DCR_0(V_{OV})}$$

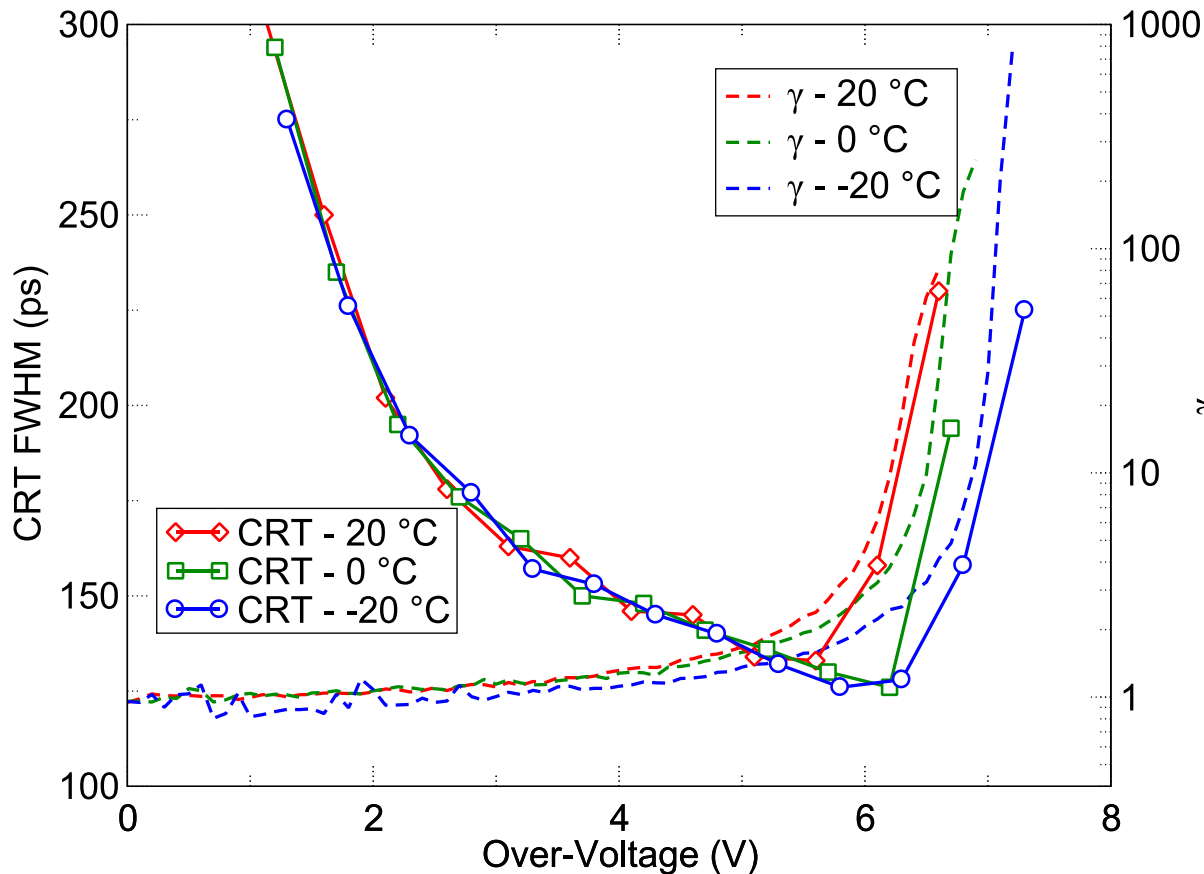


There is no amplification if the LYSO top face is covered with black paint.

Extremely high values!

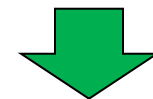
The process rapidly **diverges**.

The γ coefficient shows an **almost perfect correlation with the CRT**.



The PZ filter can **no longer compensate** for the detector noise.

Reduction of the effective PDE, due to cells busy with DCR.



Basically, the SiPM stops working.

For reaching higher over-voltage and PDE, it is **necessary to reduce the amount of cross-talk:**

- **Color filters in the scintillator**
 - Suppression of external cross-talk
- **Optical Trenches and Double Junction**
 - Suppression of internal cross-talk (total CT is determined by both internal and external components)
- **Smaller cells with smaller gain but same fill-factor**
 - Updated fabrication technology and cell-edge layout

We have demonstrated that the **effect of dark noise** on timing measurements with SiPM coupled to LYSO crystal **can be largely compensated**.

The baseline compensation can be implemented with a simple, **ASIC compatible, analog circuit**.

Once the effects of the DCR are removed, we can observe a **different phenomenon, limiting the timing resolution of the SiPM**, related to the **optical cross-talk, increased by the scintillator**.

Possible solutions are under investigation, however the **HD technology** seems a **very promising option**.

HyperImage project



SUBLIMA project



FBK-INFN MEMS2 agreement

Back-up slides

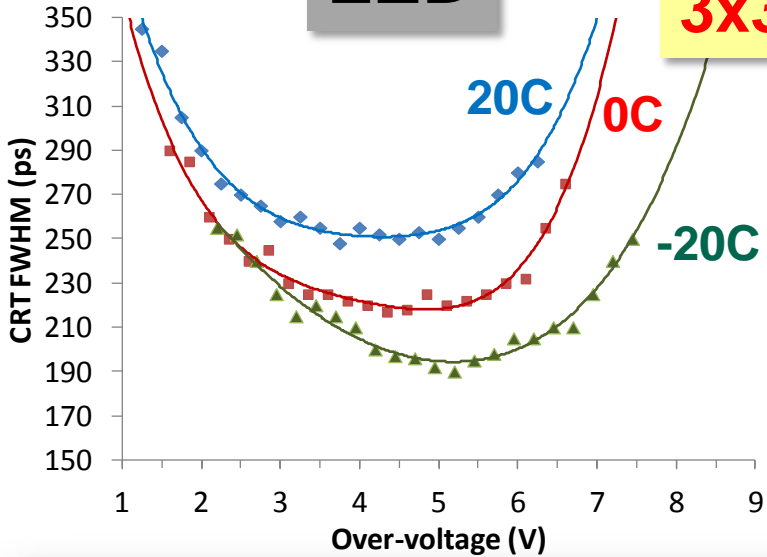
In the next slides:

- **CRT vs Temperature**
- **Threshold level**
- **crystal height**
- **SiPM size**

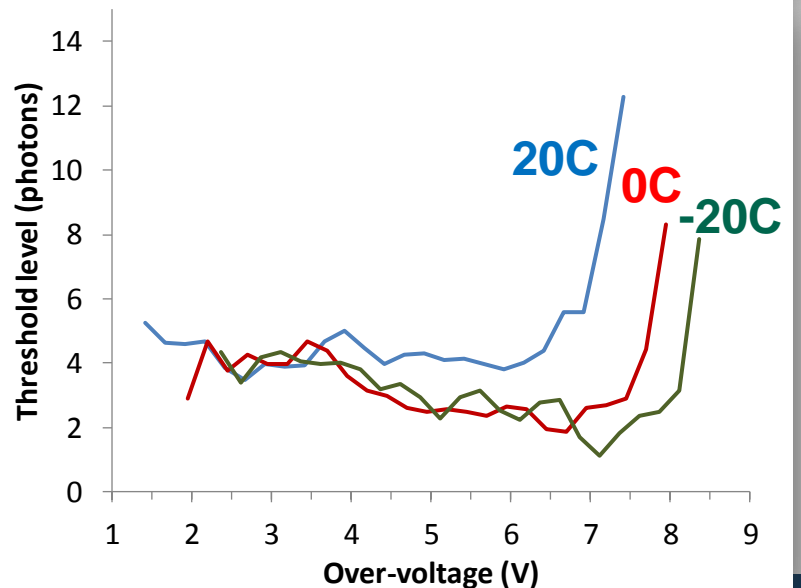
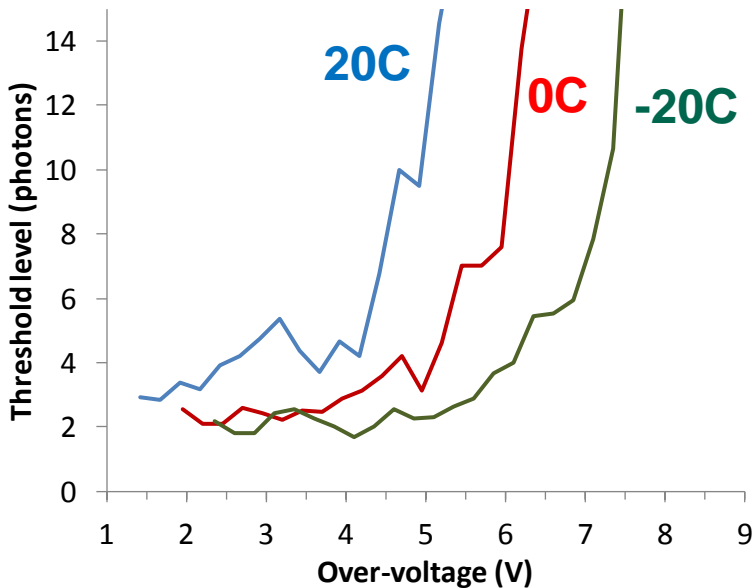
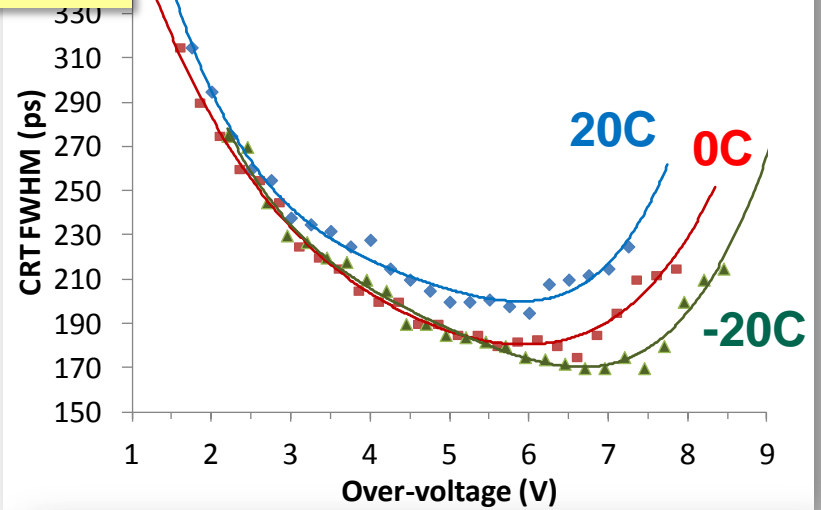
Optimum Threshold level

**Detector cube
3x3mm² SiPM**

LED



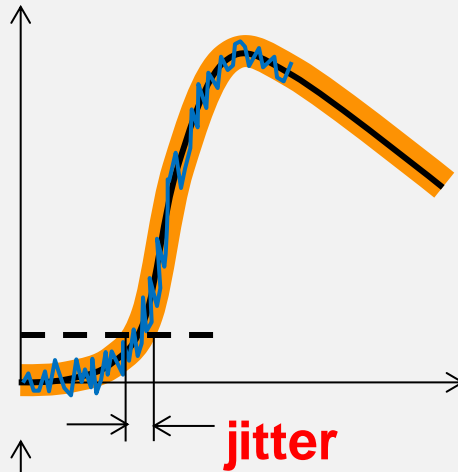
DLED



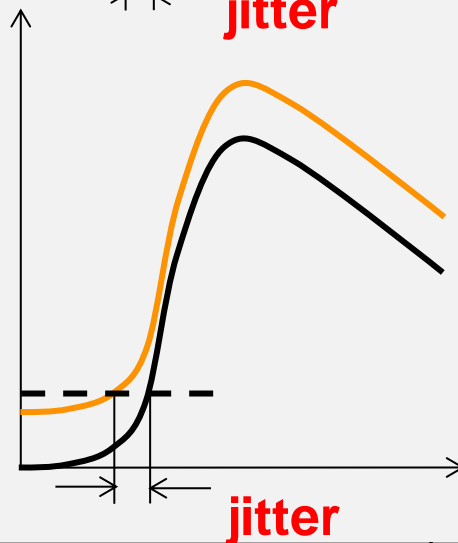
LED is widely used in PMT-based systems

What is the effect of noise on timing?

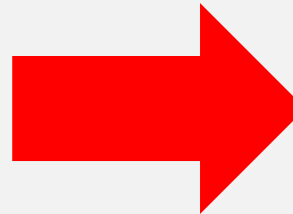
signal
distortion
HF noise



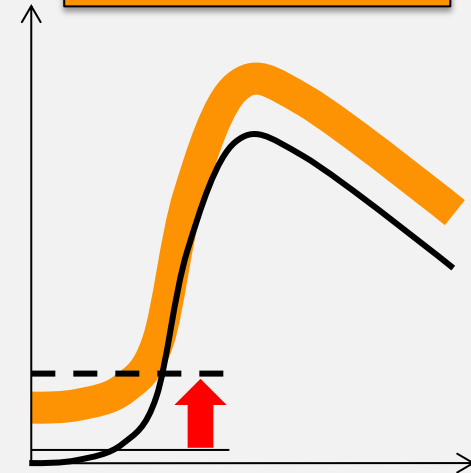
baseline
fluctuation
LF noise



furthermore

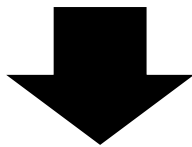
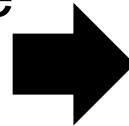


forced to use a
higher threshold



jitter for worse
photon statistics

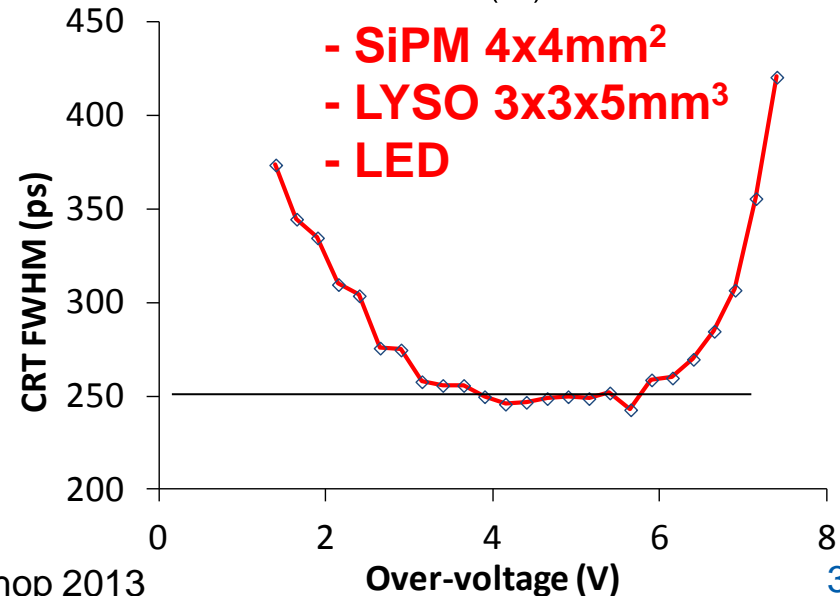
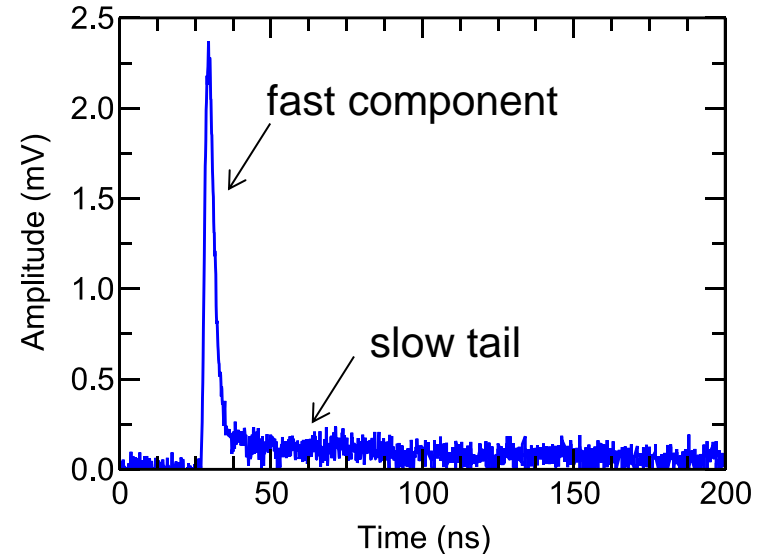
In this case we increase both the quenching resistor and the quenching capacitor in order to enhance the fast component and decrease the slow one.

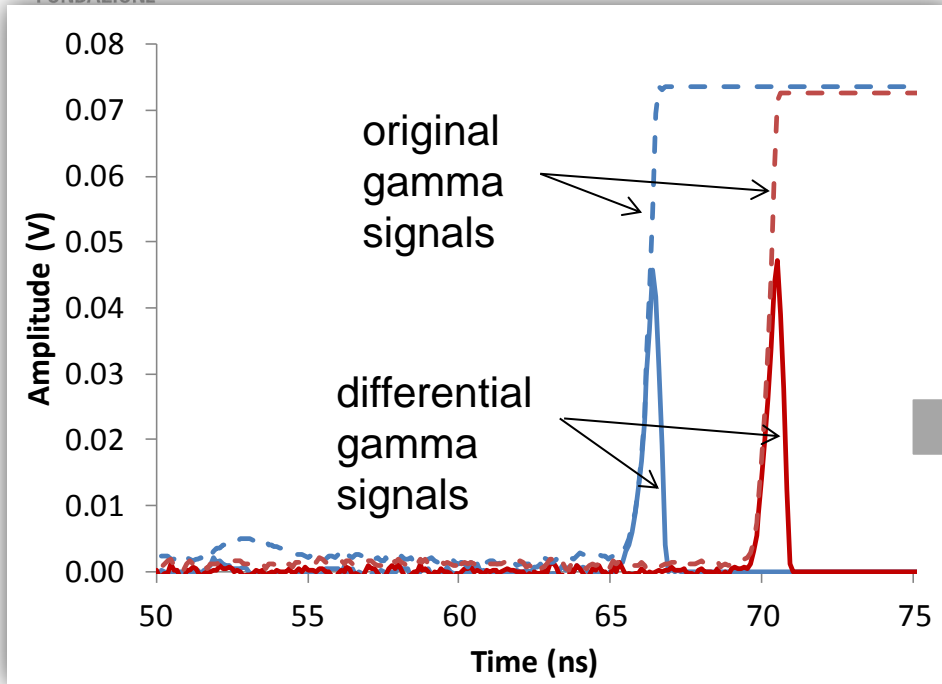


Steeper rising edge of the gamma pulse and lower baseline fluctuation



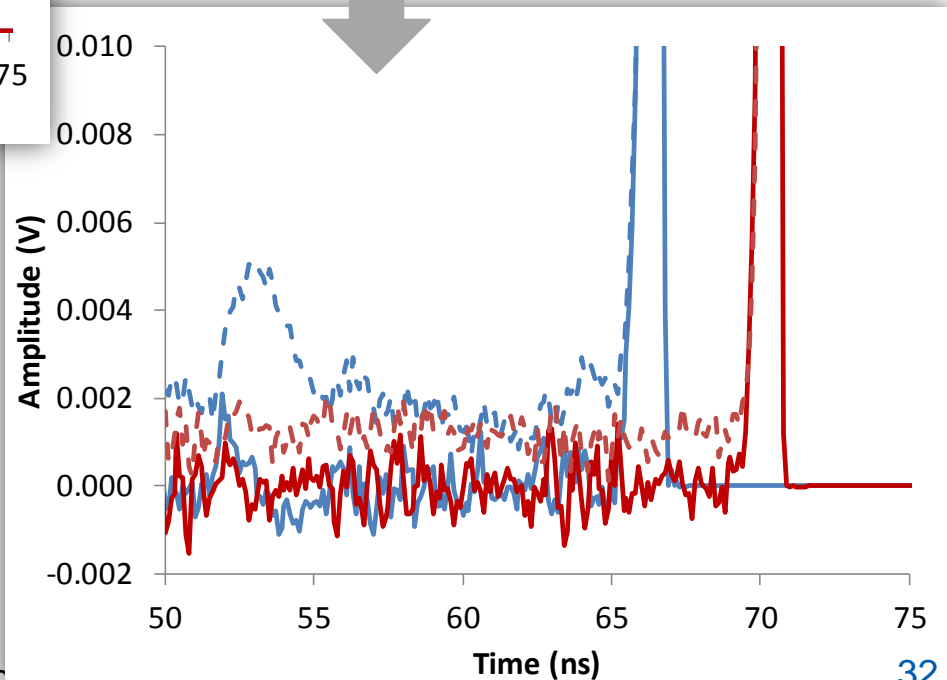
SCR of a 4x4mm² SiPM





+ initial part of gamma ray signal preserved

expanded y scale

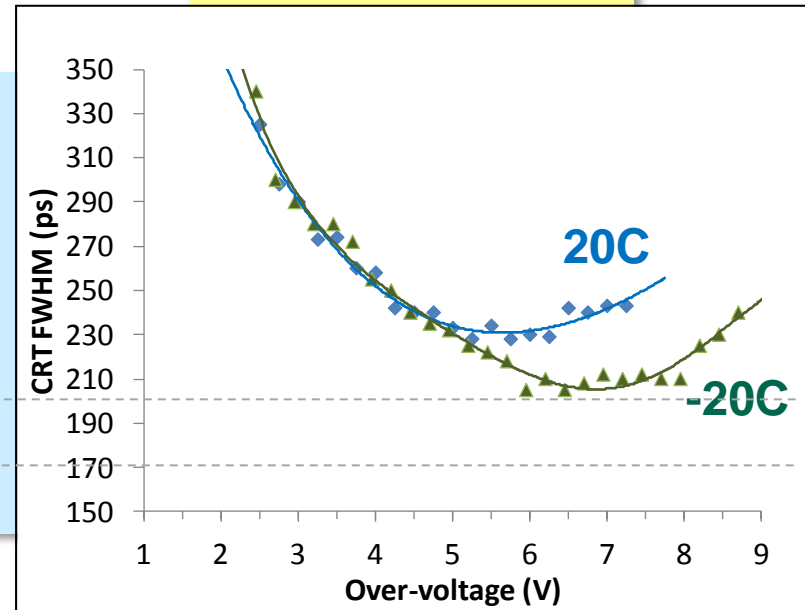
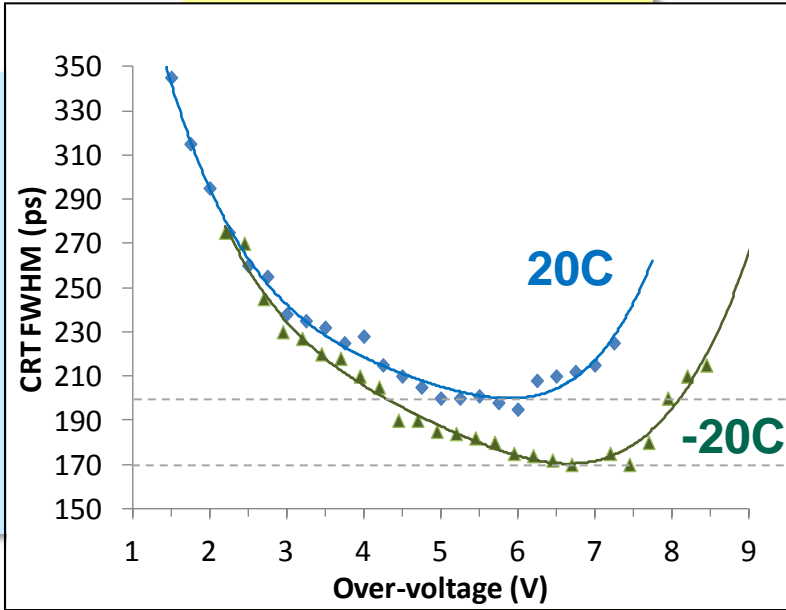


+ baseline compensated;
+ electronic noise increased;

Detector cube

Detector PET

SiPM 3x3mm²



SiPM 4x4mm²

