



# Development of novel aluminum-based stabilizer solutions for superconducting cables Applicable to future detector magnets

#### S.A.E. Langeslag

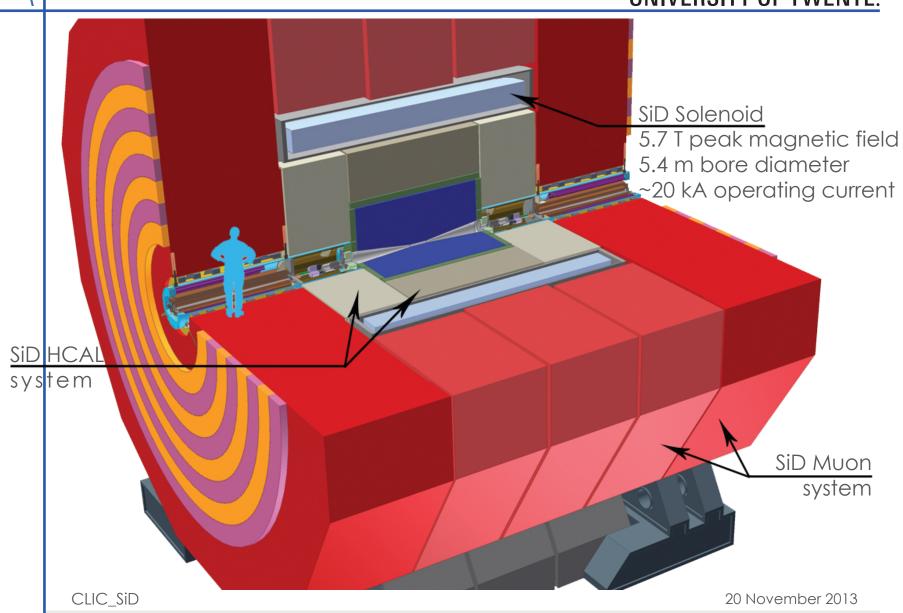
B. Curé, S. Sgobba, A. Dudarev and H.H.J. ten Kate

20 November 2013

WAMAS Workshop on Advanced Materials & Surfaces; Wednesday, 20<sup>th</sup> of November 2013, 11h00

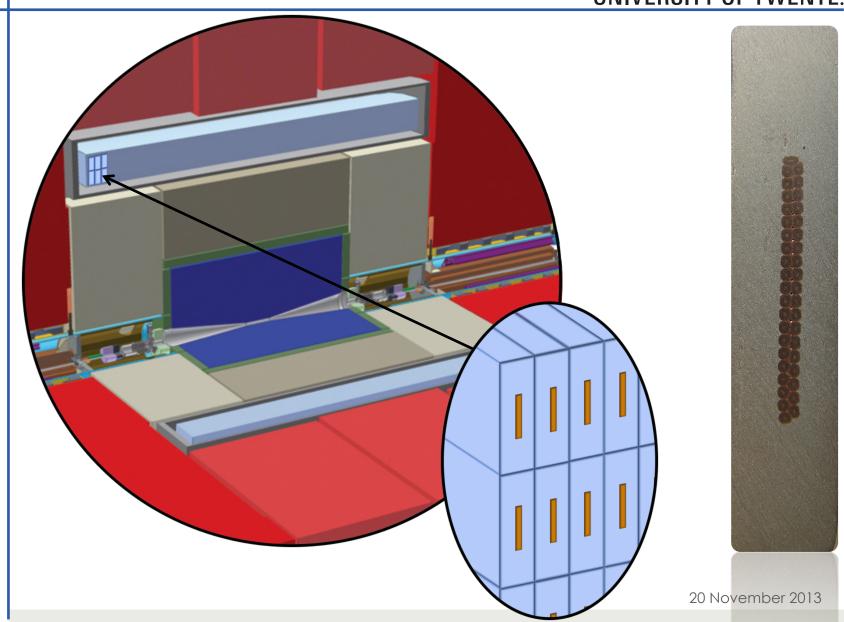


## Large bore, High-field Magnets





## Stabilized Superconducting cable





## Stabilized Superconducting cable

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The self-supporting magnet structure needs to sustain a large hoop force as a result of the high peak magnetic field.

This requires for the conductor to exhibit challenging mechanical properties.

Goal is to develop a prototype for a 60 kA critical current, at 5 T class stabilized superconductor, operating at 4.2 K.

→ Leading us to the development of a conductor with a ~2000 mm<sup>2</sup> cross-sectional area.

The stabilizer should feature a yield strength of >120 MPa at 4.2 K and an RRR of >500.



#### Reinforced Stabilizer

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- Hybrid solution
  - preservation of conductivity properties
  - mechanical reinforcement
  - homogeneous deformation
  - conductor manufacturing

**\** 







- Microalloying
  - preservation of conductivity properties
  - mechanical reinforcement
  - homogeneous deformation
  - conductor manufacturing



CMS (left) & ATLAS central solenoid (right) conductor

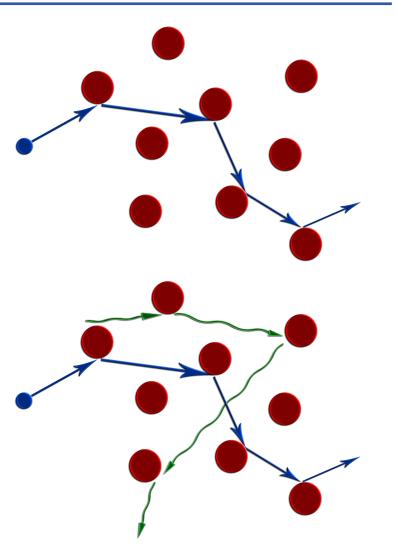


## Preservation of Conductivity

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- Doped Aluminum
  - low solid solubility

- Mechanical Alloying
  - particle or whisker reinforced



Mean free path – Electrical and Thermal resistivity
20 November 2013



## Co-extrusion of Al-Ni stabilized conductor

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#### Scale-up towards a prototype for a 60 kA at 5 T, 4.2 K class conductor

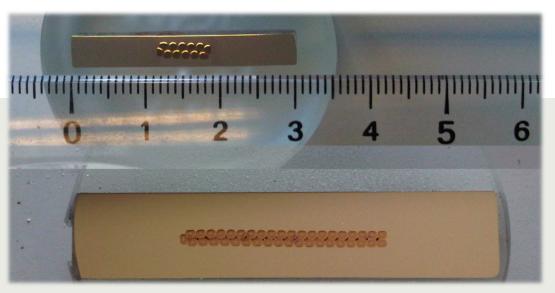
Co-extrusion of a large 40-strand Nb-Ti/Cu superconducting cable with a precipitation type Al-0.1 wt%Ni stabilizer.

Microalloying with Ni contributes to the strength of the stabilizer while avoiding significant degradation in RRR due to its low solid solubility in Al.

The Al-0.1wt%Ni material was made available by KEK, Tsukuba, Ibaraki (J).

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Al-0.1wt.%Ni stabilized ATLAS central solenoid conductor (top) & scaled-up Al-0.1wt.%Ni stabilized prototype conductor (bottom).



## Co-extrusion of Al-Ni stabilized conductor

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Nexans Cortalliod (CH); Extrusion press

Continuous co-extrusion on a 3800 ton press at Nexans, Cortaillod (CH).

Using punch and die of the ATLAS BT conductor (57 x 12 mm<sup>2</sup>).

Cable preheated and brushed to ensure good bonding.

Temperature remained at a constant 400°C, while the pressure was increased with 20-25% with the introduction of Al-0.1wt%Ni, leading to a 1.5 m/min extrusion speed.



## Co-extrusion of Al-Ni stabilized conductor

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Leading to 200 m of 5N-Al coextruded conductor and 100 m of Al-0.1wt%Ni co-extruded conductor.

Multi-pass uni-directional work hardening has been applied to increase the mechanical properties of the as-extruded temper.





Spool (3 m diameter) with co-extruded conductor



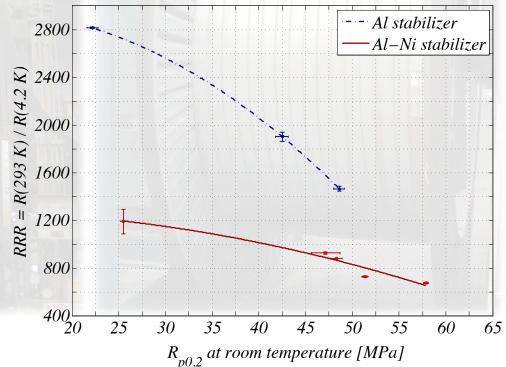
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**TABLE 1.** Properties of co-extruded 5N-Al and Al-0.1wt%Ni as a result of various cross-section reductions due to multi-pass rolling

	Mat.	RRR	$egin{aligned} \mathbf{R}_{p0.2} \ [\mathbf{MPa}] \end{aligned}$	$\mathbf{R}_m$ [MPa]
As-extruded	5N-Al	2814	22	40
	Al-0.1wt%Ni	1191	26	53
20% single pass cold-rolled	5N-Al	1901	42	47
	Al-0.1wt%Ni	879	48	56
30% single pass cold-rolled	5N-Al	1464	49	53
	Al-0.1wt%Ni	673	58	63

RRR in relation to 0.2% yield strength for the two extruded stabilizer materials at the various cold-worked states:

Roughly linear interaction between RRR and  $R_{\rm p0.2}$ 



 $R_{p0.2}$  and  $R_m$  are 0.2% yield strength and ultimate tensile strength respectively.



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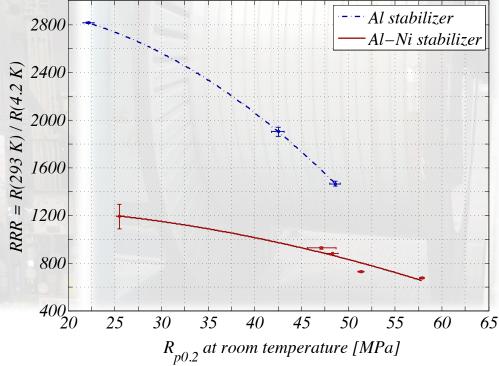
RRR in relation to 0.2% yield strength for the two extruded stabilizer materials at the various cold-worked states:

Roughly linear interaction between RRR and  $R_{\rm p0.2}$ 

Higher workability of the Al-0.1wt%Ni alloy

Increase in  $R_{p0.2}$  with use of work hardening has a less detrimental effect on the RRR of the Al-Ni alloy.







## Work hardening; Bi-directional rolling

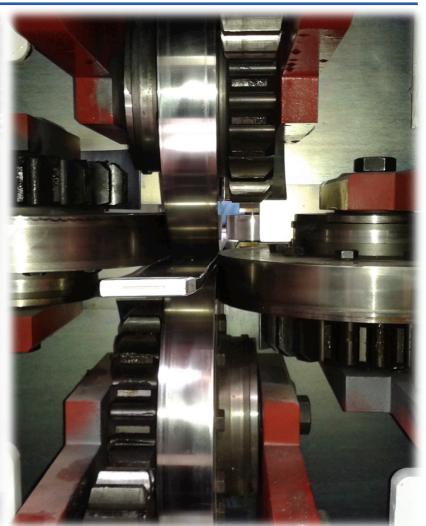
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Bi-directional (Turks head) rolling was preformed on a 50 ton DEM rolling mill at Criotec, Chivasso (I).

A set-up used for ITER cable-inconduit production.

Rolling was conducted on 1.5 m samples, width constrained to preserve cable integrity and a realistic aspect ratio.

The rolling process was made possible by ENEA, Rome (I).



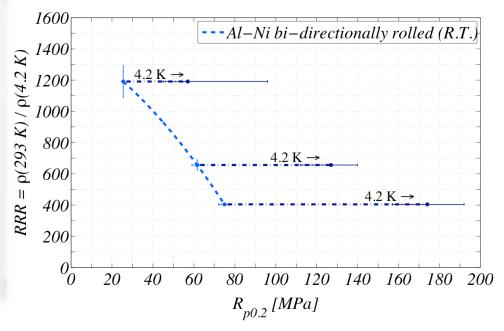


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**TABLE 2.** Properties of co-extruded Al-0.1wt%Ni as a result of various cross-section reductions due to bi-directional rolling

Illia.	Temp. [K]	RRR	$egin{aligned} \mathbf{R}_{p0.2} \ [\mathbf{MPa}] \end{aligned}$	$\mathbf{R}_m$ [MPa]
As-extruded	293	1191	26	53
	4.2	- 0	57	303
20% single pass cold-rolled	293	656	62	67
1 1	4.2	-	127	376
30% single pass cold-rolled	293	404	75	81
	4.2	-	157*	496

High workability of Al-0.1wt%Ni alloy in a production-scale work-hardening sequence.



Results for the co-extruded Al-0.1wt.%Ni conductor subjected to various work-hardening processes.

<sup>\*</sup> deduced from two measurements



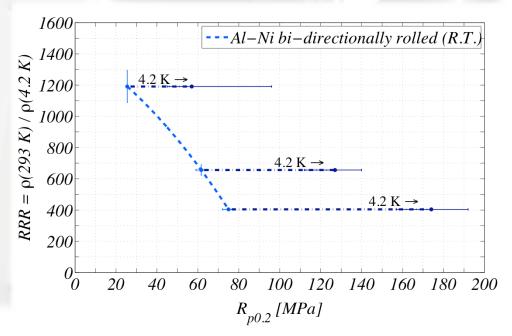
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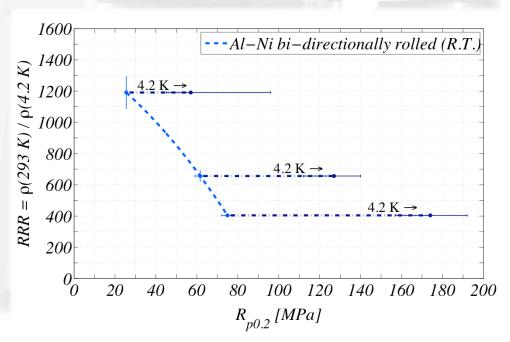
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High workability of Al-0.1wt%Ni alloy in a production-scale work-hardening sequence.

Significant increase in R<sub>p0.2</sub> at 4.2 K

Roughly linear interaction between RRR and  $R_{\text{p0.2}}$ 

~120 MPa at 4.2 K when ~19% cold-reduced, maintaining an RRR of ~700.



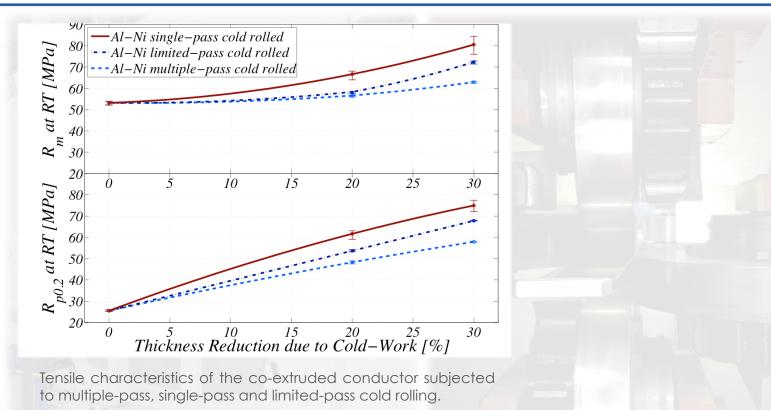
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## Single-pass vs. Multi-pass rolling

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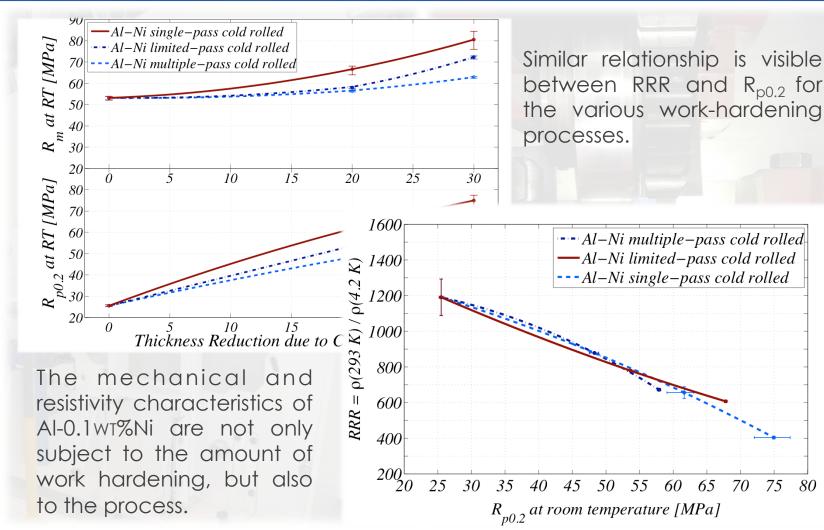
Distinct decrease in mechanical properties with number of cold-roll passes.

Process of recovery of dislocation pinning points in between passes in this dilute Al-Ni alloy.



## Single-pass vs. Multi-pass rolling

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RRR plotted as function of Rp0.2 for the various cold-worked states, for the different work-hardening processes.



In collaboration with the industry a successful co-extrusion of a record-size, ~700 mm<sup>2</sup>, Al-0.1wt%Ni stabilized superconductor has been achieved.

The expected increase in  $R_{p0,2}$  with dilute Ni alloying is confirmed.

The Al-0.1wt%Ni material exhibits a higher workability, and shows a less detrimental effect of the work hardening on the conductivity characteristics with respect to 5N-Al.

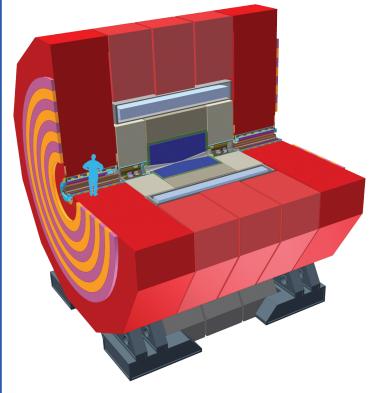
the enhancement of the **mechanical properties at 4.2 K is promising** for future detector application.

The material characteristics of Al-0.1wt%Ni are subject to both work-hardening amount as well as certain parameters of the work-hardening process.

→ An **optimal work-hardening sequence** needs to be developed.

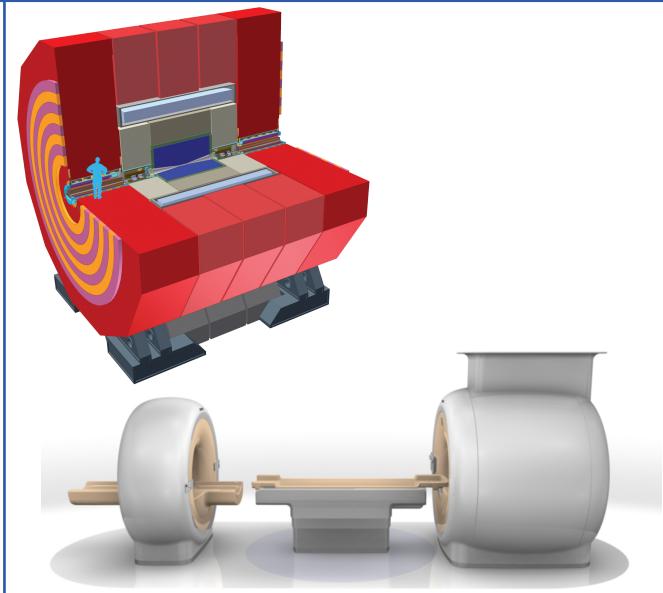


## **Applications**



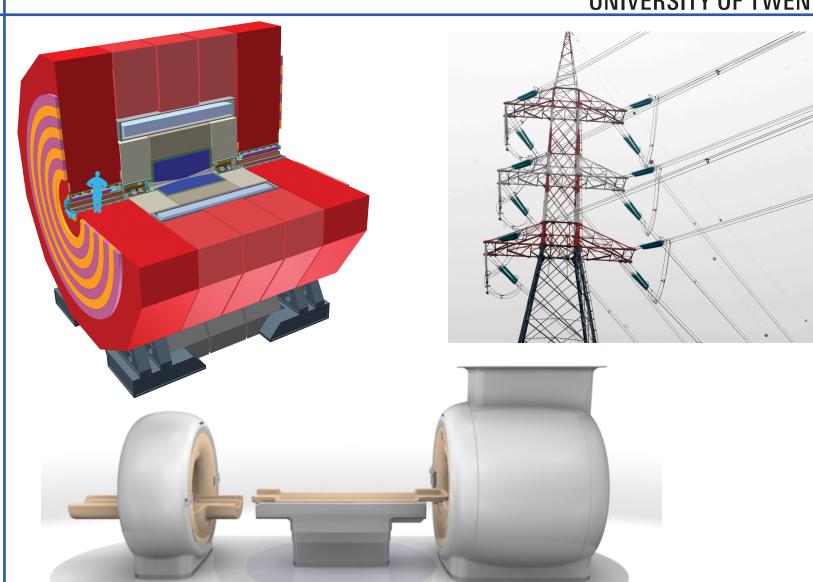


## **Applications**





## Applications







Thank you for your kind attention



## Response to Partial Annealing

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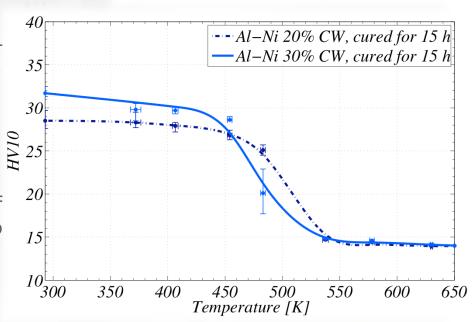
Clear temperature range where recovery of lattice defects takes place; reversing work-hardening.

- → 470 K 530 K for 20% reduced
- → 450 K 510 K for 30% reduced

Coil resin curing should not exceed temperatures (for 15 h) of:

- → 470 K for 20% reduced
- → 450 K for 30% reduced

No indication was found of precipitation hardening due to artificial aging.



Hardness, HV10, of 20% and 30% single pass cold-rolled short samples subjected to various thermal treatments with a duration of 15 h.