

15 – 18 April 2013

CERN

9th DITANET Topical Workshop on
Non-Invasive Beam Size
Measurement for High Brightness
Proton and Heavy Ion Accelerators

Theory of optical Reconstruction for Synchrotron Light Sources

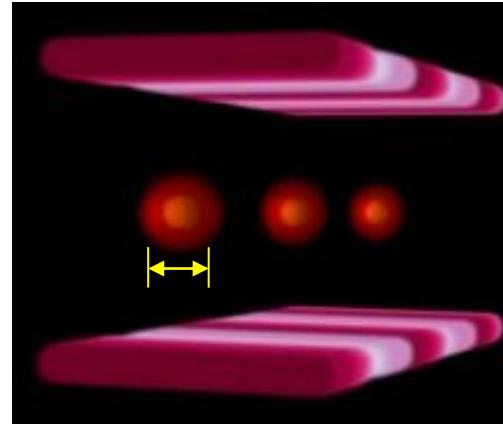
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- Introduction
- Resolution in Frame of Geometrical Optics
- Analytical Approach
- Numerical Near Field Calculations

Size Measurements

task

- › determination of beam profile
 - measurement of characteristical size (rms, ...)



courtesy:
J. Amundson (FNAL)

conventional size measurement

- › take object and measure



difficulties

- › object extremely small
- › object not directly accessible
 - inside vacuum beam pipe, accelerator environment, ...



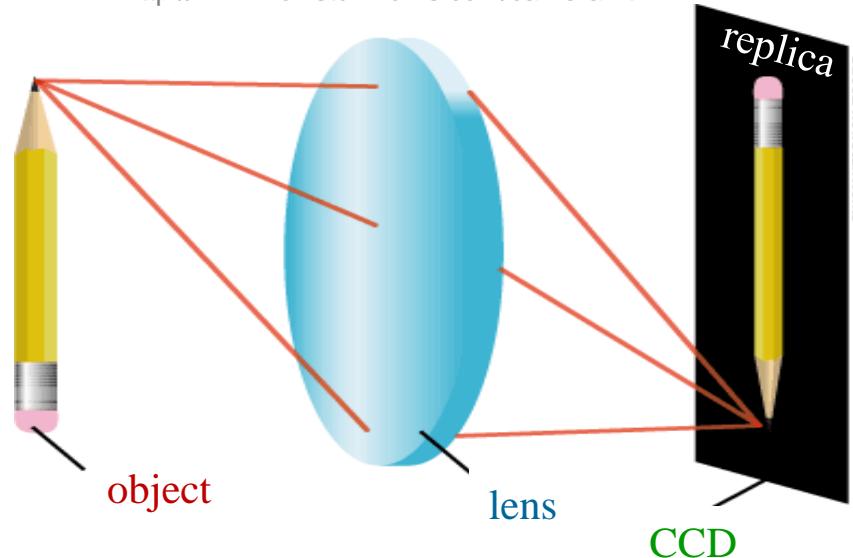
optical imaging

- › generate replica in comfortable environment
- › adjust replica size (image) to size of measuring device (CCD)

Optical Imaging

principle

<http://www.howstuffworks.com/camera.htm>



resolution

extended object (depth of field)
moving object

$$\rightarrow \sigma_{dof}$$

fundamental resolution limit (diffraction)
aberrations, ...

$$\rightarrow \sigma_{dfr}$$

finite sampling width (pixel size)
cross talk, ...

$$\rightarrow \sigma_{ccd}$$

spatial resolution:

$$\sigma = \sqrt{\sigma_{dof}^2 + \sigma_{dfr}^2 + \cancel{\sigma_{ccd}^2}}$$

outline

this talk: image formation (generate replica onto CCD)

talk E. Bravin: image registration

Resolution Consideration (1)

geometrical imaging

- first order image is a „perfect“ (but scaled) replica → no blurring

real image blurred

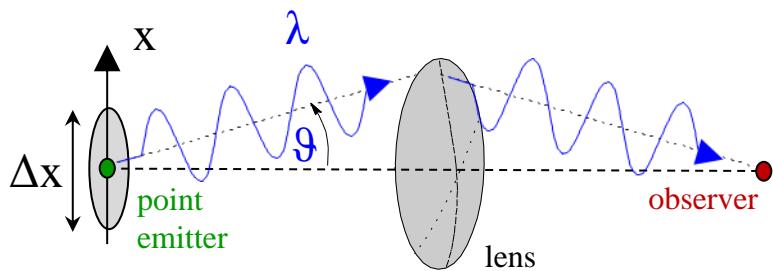
- by aberrations → e.g. spherical aberrations, astigmatism, coma, ... **lens imperfections**
- by diffraction → wave nature of light **fundamental**

neglect aberrations

- diffraction limited** systems → high quality, aberration-free systems

fundamental resolution limit

- point observer detecting photons from point emitter → location of emission point ?



Δx

$$\Delta p_x = 2\hbar k \cdot \sin \theta \approx 2 \cdot \frac{h}{2\pi} \cdot \frac{2\pi}{\lambda} \cdot \sin \theta$$

NA = $\sin \theta$:
numerical aperture

uncertainty principle: $\Delta x \cdot \Delta p_x \approx h$ ⇒

$$\Delta x \approx \frac{\lambda}{2 \sin \theta}$$



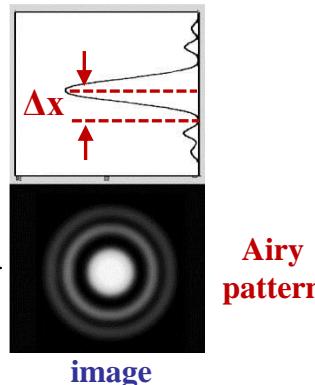
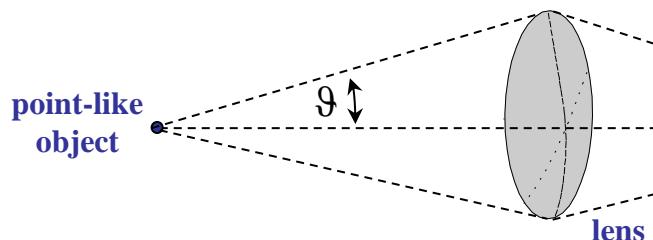
high resolution:

(i) **small λ**

(ii) **high NA**

Resolution Consideration (2)

- image of point source



<http://www.astro.ljmu.ac.uk>

$$\Delta x = 0.61 \frac{M\lambda}{\sin \vartheta}$$

magnification M

- synchrotron radiation (long bending magnet)

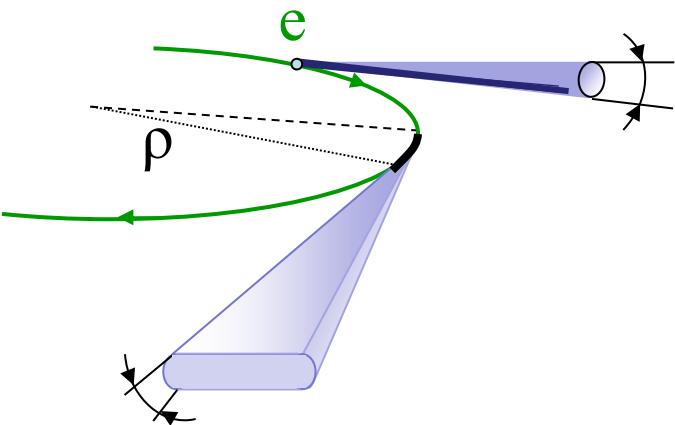
- ▶ strongly collimated emission

→ typical emission angle (out of orbit plane):

$$\Psi_{SR} \approx 1/\gamma$$

- ▶ emission angle \ll acceptance of optical system

→ resolution fully dominated by SR emission characteristics



$$\Psi_{SR} \propto 1/\gamma \text{ rad}$$

- trends in modern light sources

- ▶ X-ray imaging

→ PETRA3 @ DESY with $E = 6 \text{ GeV}$, $\sigma_v \approx 10 \mu\text{m}$:

$$\Delta x (500\text{nm}) = 145\mu\text{m}$$

$$\Delta x (20\text{keV}) = 0.4\mu\text{m}$$

Resolution: 1st Level

diffraction error

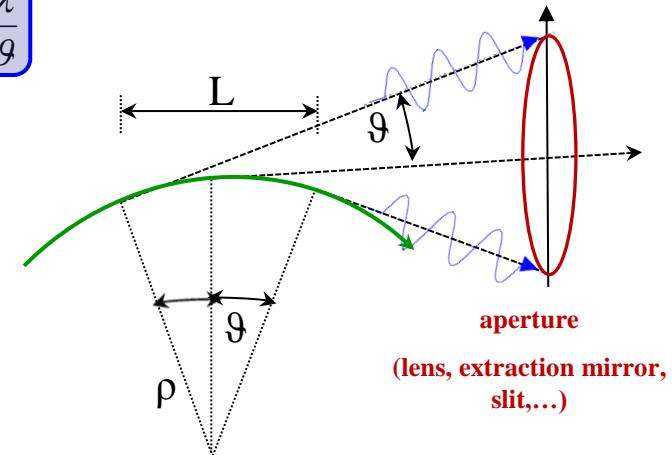
- assumption: plane wave diffraction broadening

$$\Delta x_{\text{dfr}} \approx 0.61 \frac{\lambda}{\vartheta}$$

different acceptance angles ϑ for horizontal/vertical plane:

- horizontal plane: ϑ defined by acceptance of aperture
- vertical plane: ϑ defined by SR natural opening angle Ψ_{SR}

$$\Psi_{\text{SR}} \approx \left(\frac{3\lambda}{4\pi\rho} \right)^{1/3} \quad \text{for } \lambda > \lambda_c \quad (\text{optical SR})$$



depth of field

- radiation from finite part of trajectory: L

- imaging with misalignment Δa :

$$a = a_0 + \Delta a \quad \text{and} \quad 1/f = 1/a_0 + 1/b_0$$

- calculation in frame of paraxial optics:

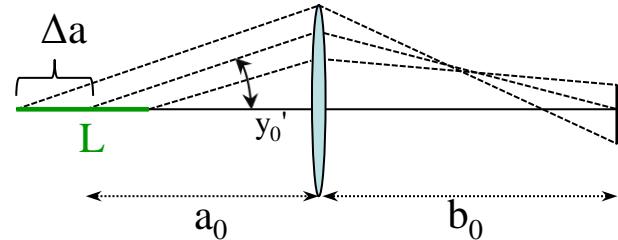
$$\begin{pmatrix} y_1 \\ y'_1 \end{pmatrix} = \begin{pmatrix} 1 & b_0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 1 & 0 \\ -1/f & 1 \end{pmatrix} \cdot \begin{pmatrix} 1 & a \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} y_0 \\ y'_0 \end{pmatrix}$$



$$y_1 = - \left(\frac{b_0}{a_0} \right) \cdot (y_0 + y'_0 \cdot \Delta a)$$

magnification &
inversion original
size size depth of
field

- misalignment is length of trajectory: $\Delta a = L/2 = \rho\vartheta$



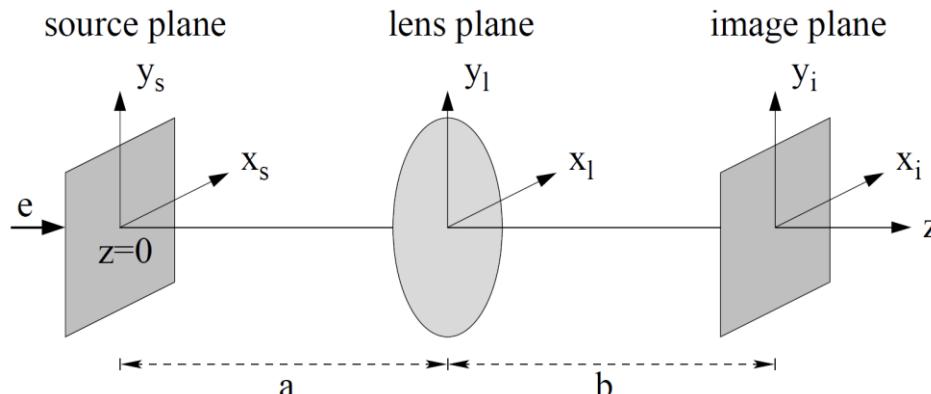
$$\Delta x_{\text{dof}} = y'_0 \cdot \rho\vartheta$$

horizontal plane: $y'_0 = \vartheta$

vertical plane: $y'_0 = \Psi_{\text{SR}}$

Fundamentals of Image Formation

- detailed resolution information
 - requires basic knowledge of image formation
- simple imaging setup



- procedure
 - calculate image of point source (single particle radiation) → **Point Spread Function (PSF)**
 - image of extended object → 2-dim. convolution of **source distribution** and PSF
 - resolution → difference between source distribution and image (resp. PSF)
- PSF calculation
 - el. field in source plane (radiation field) → discussed at a later stage
 - field propagation from element to element → in frame of scalar diffraction theory
 - (i) source plane – lens input
 - (ii) lens input – lens output
 - (iii) lens output – image plane
 - intensity distribution in the image plane

Fundamentals of Image Formation

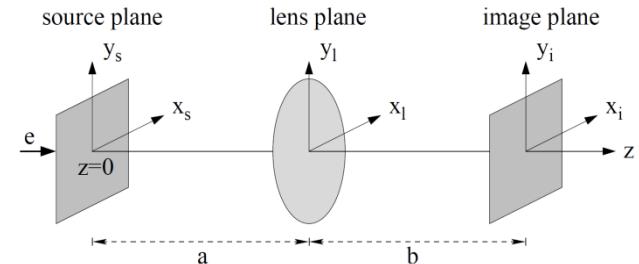
source field

- synchrotron radiation field: **two** different representations
 → form basis of **two different resolution treatments**

(discussed later)

propagation

- scalar diffraction theory
 (here: from source to lens plane)



$$E_{x_l, y_l}^l(\vec{r}_l, \omega) = -i \frac{e^{ika}}{\lambda a} \cdot e^{i \frac{k}{2a} (x_l^2 + y_l^2)} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} dx_s dy_s E_{x_s, y_s}^s(\vec{r}_s, \omega) \cdot e^{i \frac{k}{2a} (x_s^2 + y_s^2)} \cdot e^{-ik \frac{x_s x_l + y_s y_l}{a}}$$

aperture boundaries

- far field (Fraunhofer) approximation: $\frac{k}{2} (x_s^2 + y_s^2)_{\max} \ll a$

$$\rightarrow E_{x_l, y_l}^m(\vec{r}_l, \omega) = -i \frac{e^{ika}}{\lambda a} \cdot e^{i \frac{k}{2a} (x_l^2 + y_l^2)} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} dx_s dy_s E_{x_s, y_s}^s(\vec{r}_s, \omega) \cdot e^{-i(k_x x_s + k_y y_s)} \propto \mathcal{F}(E_{x_s, y_s}^s) \left(k_{x,y} = k \frac{x_s, y_s}{a} \right)$$

→ basis of **Fourier Optics**

thin lens approximation

- quadratic phase shift: $E_{x_l, y_l}^{l_{out}}(\vec{r}_l, \omega) = E_{x_l, y_l}^{l_{in}}(\vec{r}_l, \omega) \cdot e^{-i \frac{k}{2f} (x_l^2 + y_l^2)}$ with $\frac{1}{f} = \frac{1}{a} + \frac{1}{b}$

intensity

$$\frac{d^2 W}{d\omega d\Omega} = \frac{c}{4\pi^2} \left(|\vec{E}_{x_i}^i(\vec{r}_i, \omega)|^2 + |\vec{E}_{y_i}^i(\vec{r}_i, \omega)|^2 \right)$$

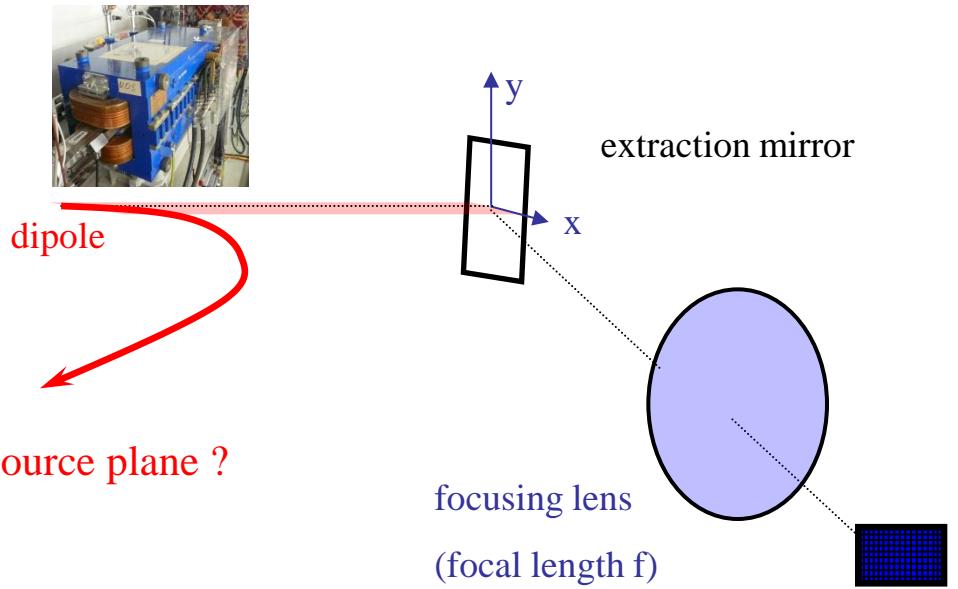
Profile Monitor Considerations

point of interest: monitor resolution

- › consider single particle
- › calculate „point spread function“ (PSF) in image plane
- › convolute beam profile with PSF

tasks

- › radiation source
 - ⇒ SR dipole radiation field
 - ⇒ source plane ?
- › extraction out of vacuum system
 - ⇒ horizontal aperture limitation
- › focusing optics (lens)
 - ⇒ thin lens approximation
- › measurement of spatial intensity distribution
 - ⇒ PSF on CCD detector



Radiation Propagation

- ...in frame of scalar diffraction theory

- source plane to extraction mirror

$$E_{x_m, y_m}^m(\vec{r}_m, \omega) = -i \frac{e^{ika_1}}{\lambda a_1} \cdot e^{i \frac{k}{2a_1} (x_m^2 + y_m^2)} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} dx_s dy_s E_{x_s, y_s}^s(\vec{r}_s, \omega) \cdot e^{i \frac{k}{2a_1} (x_s^2 + y_s^2)} \cdot e^{-ik \frac{x_s x_m + y_s y_m}{a_1}}$$

- extraction mirror to lens input

$$E_{x_l, y_l}^{l_{in}}(\vec{r}_l, \omega) = -i \frac{e^{ika_2}}{\lambda a_2} \cdot e^{i \frac{k}{2a_2} (x_l^2 + y_l^2)} \int_{-x_m/2}^{x_m/2} dx_m \int_{-\infty}^{+\infty} dy_m E_{x_m, y_m}^m(\vec{r}_m, \omega) \cdot e^{i \frac{k}{2a_2} (x_m^2 + y_m^2)} \cdot e^{-ik \frac{x_m x_l + y_m y_l}{a_2}}$$

- lens input to lens output (thin lens approximation)

$$E_{x_l, y_l}^{l_{out}}(\vec{r}_l, \omega) = E_{x_l, y_l}^{l_{in}}(\vec{r}_l, \omega) \cdot e^{-i \frac{k}{2f} (x_l^2 + y_l^2)}$$

with $\frac{1}{f} = \frac{1}{a} + \frac{1}{b}$, $a = a_1 + a_2$

- lens output to image plane (CCD detector)

$$E_{x_i, y_i}^i(\vec{r}_i, \omega) = -i \frac{e^{ikb}}{\lambda b} \cdot e^{i \frac{k}{2b} (x_i^2 + y_i^2)} \int_{-x_l/2}^{x_l/2} dx_l \int_{-y_l/2}^{y_l/2} dy_l E_{x_l, y_l}^{l_{out}}(\vec{r}_l, \omega) \cdot e^{i \frac{k}{2b} (x_l^2 + y_l^2)} \cdot e^{-ik \frac{x_l x_i + y_l y_i}{b}}$$

- measured quantity

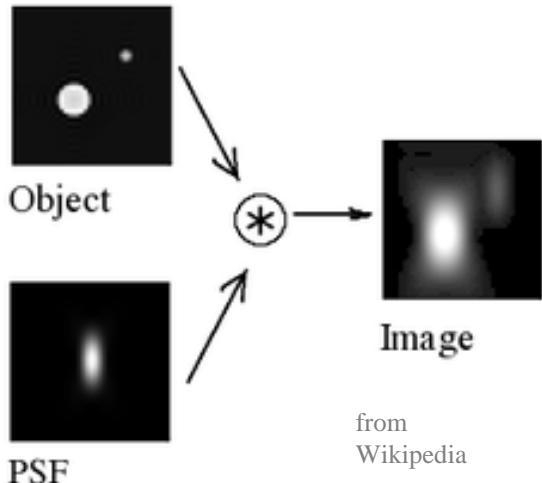
- spatial intensity distribution

$$\frac{d^2W}{d\omega d\Omega} = \frac{c}{4\pi^2} \left(|\vec{E}_{x_i}^i(\vec{r}_i, \omega)|^2 + |\vec{E}_{y_i}^i(\vec{r}_i, \omega)|^2 \right)$$

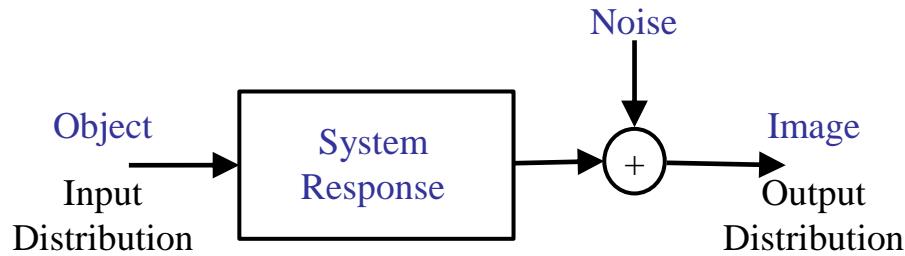
Image Formation: Systems Approach

• image formation

$$\text{Image} = \text{PSF} \otimes \text{Object} + \text{Noise}$$



• systems approach to imaging (Fourier Optics)



‣ Point Spread Function (PSF)

- image of a point source (single particle)
- characteristic of the imaging instrument
- deterministic function

‣ noise

- nondeterministic function
- described in terms of statistical distributions

‣ „standard“ signal theory

- 1-dim. signals (in time domain)
- system analysis with **delta pulse**

‣ imaging

- 2-dim. signals (in spatial domain)
- system analysis with **point source** response: **PSF**

Classical Synchrotron Radiation Field

- source field: particle field described by **Liénard-Wiechert potentials**:

$$\varphi(t) = \left(\frac{-e}{R(1 - \hat{n} \cdot \vec{\beta})} \right)_\tau, \quad \vec{A}(t) = \left(\frac{-e \vec{\beta}}{R(1 - \hat{n} \cdot \vec{\beta})} \right)_\tau$$

field derivation: $E(t) = -\vec{\nabla} \varphi(t) - \frac{1}{c} \dot{\vec{A}}(t), \quad \vec{H}(t) = \vec{\nabla} \times \vec{A}(t)$

$$\rightarrow \vec{E}(t) = -e \left(\frac{(1 - \beta^2)(\hat{n} - \vec{\beta})}{R^2(1 - \hat{n} \cdot \vec{\beta})^3} + \frac{\hat{n} \times [(\hat{n} - \vec{\beta}) \times \dot{\vec{\beta}}]}{cR(1 - \hat{n} \cdot \vec{\beta})^3} \right)_\tau, \quad \vec{H}(t) = \hat{n} \times \vec{E}(t)$$

neglect velocity term (far field approximation)

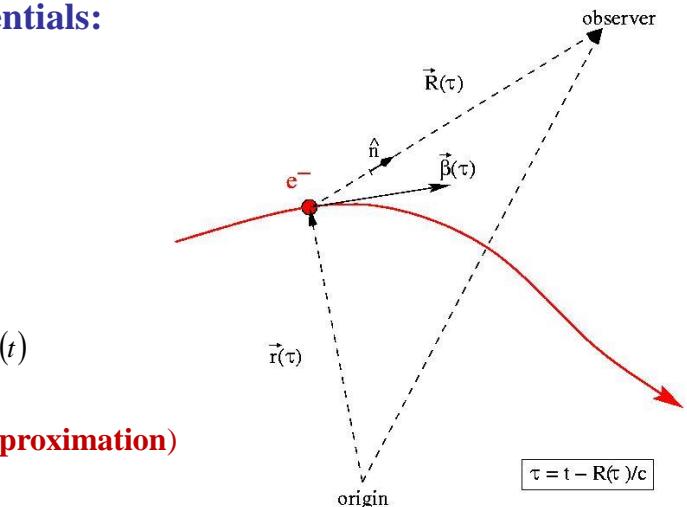
- Fourier transform:

$$\vec{E}(\omega) \approx -\frac{i\omega e}{cR} \int_{-\infty}^{+\infty} d\tau [\hat{n} \times [\hat{n} \times \vec{\beta}]] e^{i\omega(\tau+R(\tau)/c)}$$

- special case: charged particle moving on circular orbit

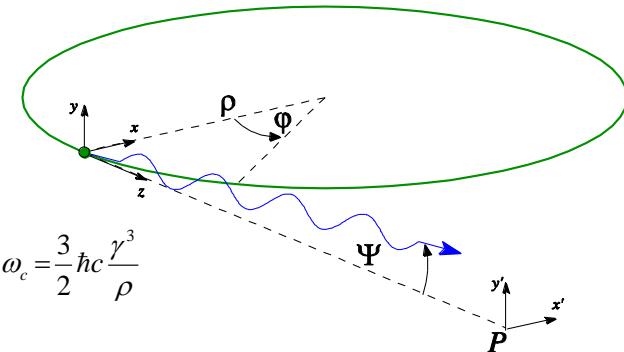
$$E_x(\omega) = E_\sigma = A_\sigma \frac{\hbar\omega}{2\hbar\omega_c} (1 + \gamma^2\Psi^2) \cdot K_{2/3} \left[\frac{\hbar\omega}{2\hbar\omega_c} (1 + \gamma^2\Psi^2)^{3/2} \right]$$

$$E_y(\omega) = E_\pi = A_\pi \frac{\hbar\omega}{2\hbar\omega_c} \gamma \Psi \sqrt{1 + \gamma^2\Psi^2} \cdot K_{1/3} \left[\frac{\hbar\omega}{2\hbar\omega_c} (1 + \gamma^2\Psi^2)^{3/2} \right]$$



→ analytical field description

- comments:
 - approximative field description → far field approximation
 - emission from single point on orbit → additional contributions: depth of field, orbit curvature



Resolution: 2nd Level

• imaging based on analytical field description

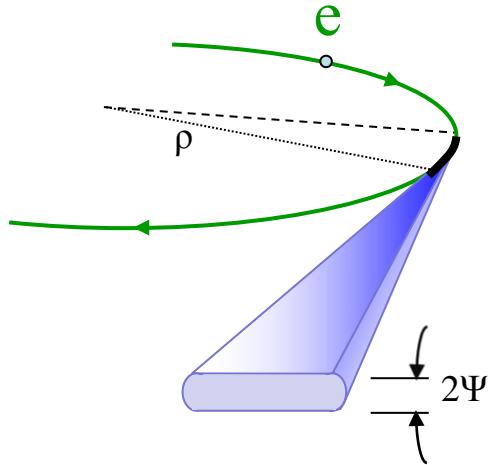
A. Hofmann and F. Méot, Nucl. Instr. Meth. 203 (1982) 483

› horizontal direction

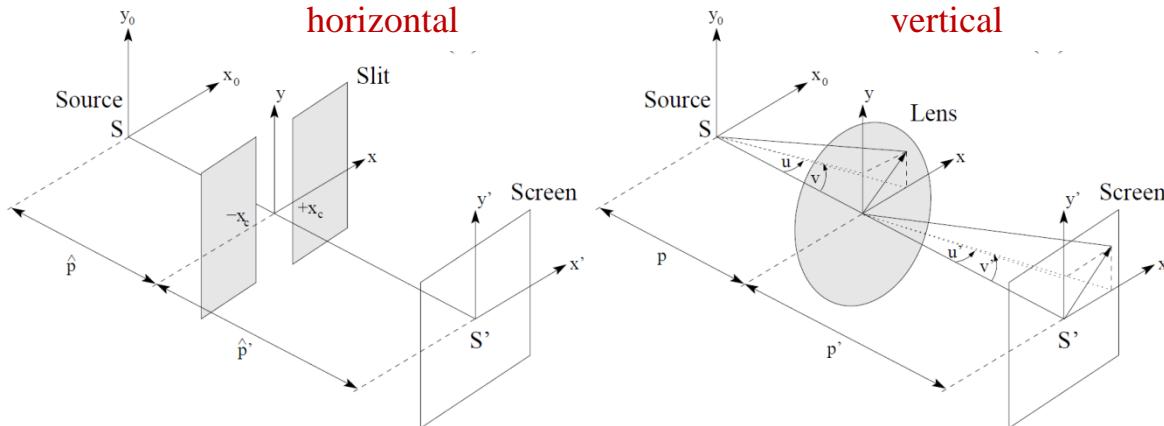
- radiation fan: constant intensity distribution
- aperture limitation: extraction mirror
- ⇒ Fraunhofer diffraction pattern: plane wave diffraction at slit

› vertical direction

- radiation field: analytical expressions for E_σ , E_π
- action of lens: produces magnified image of source distribution
- ⇒ Fraunhofer diffraction pattern: Fourier transform of SR source field



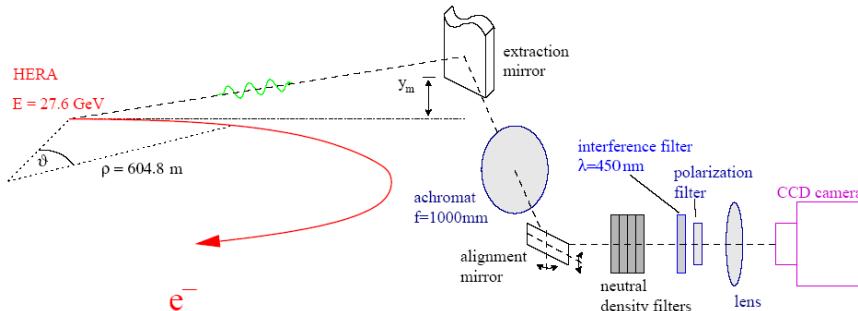
• simplified geometries



Diffraction Broadening

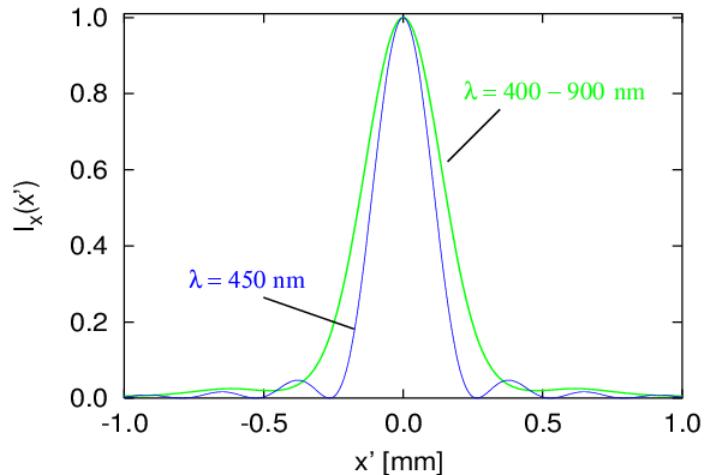
- example: HERAe @ DESY

G. Kube et al., Proc. BIW2004, AIP Conf. Proc. **732** (2004) 350

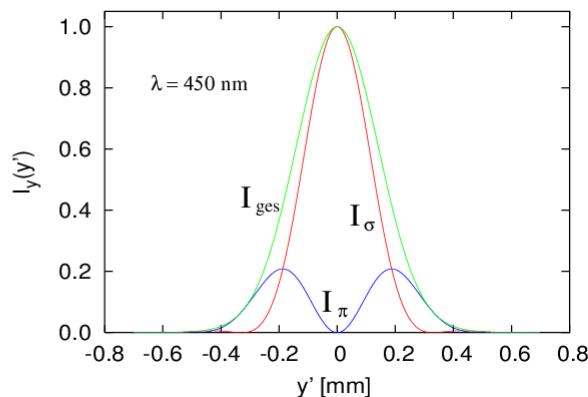
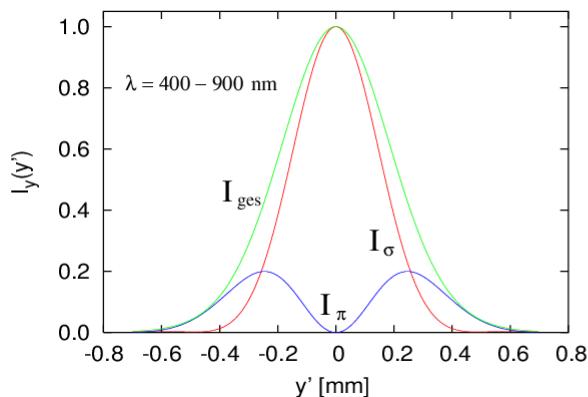


- » E = 27.6 GeV
- » $I_{\max} = 50 \text{ mA}$
- » $p = 604.8 \text{ m}$
- » $a = 6485.5 \text{ mm}$
- » $b = 1182.3 \text{ mm}$
- » $f = 1000 \text{ mm} / 25 \text{ mm}$

- » horizontal PSF



- » vertical PSF

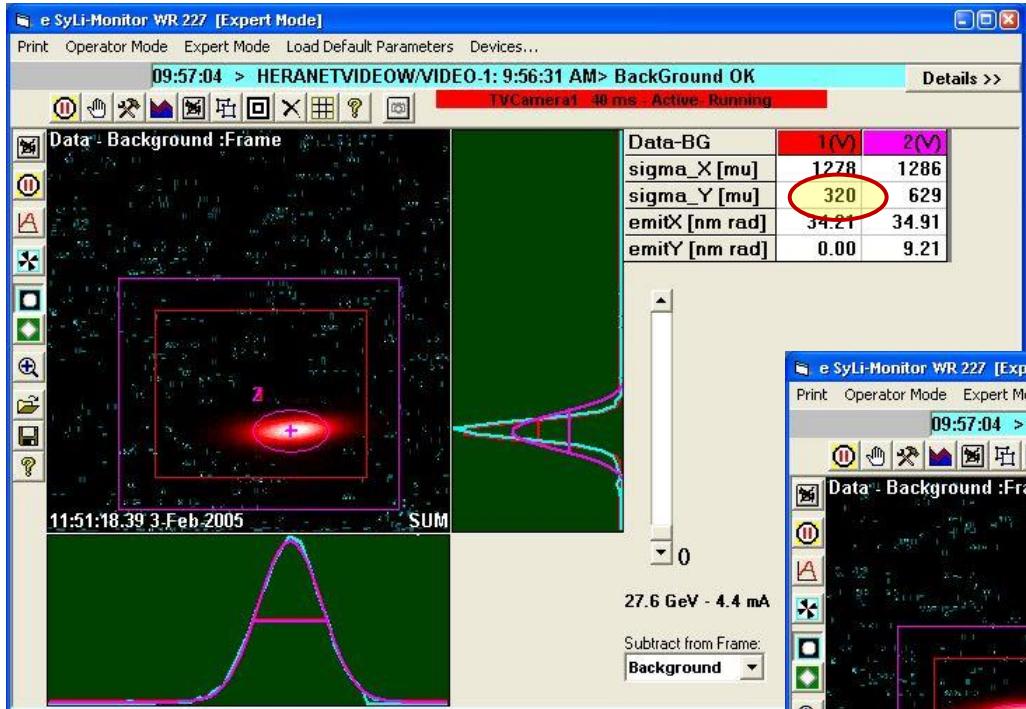


→ good resolution:

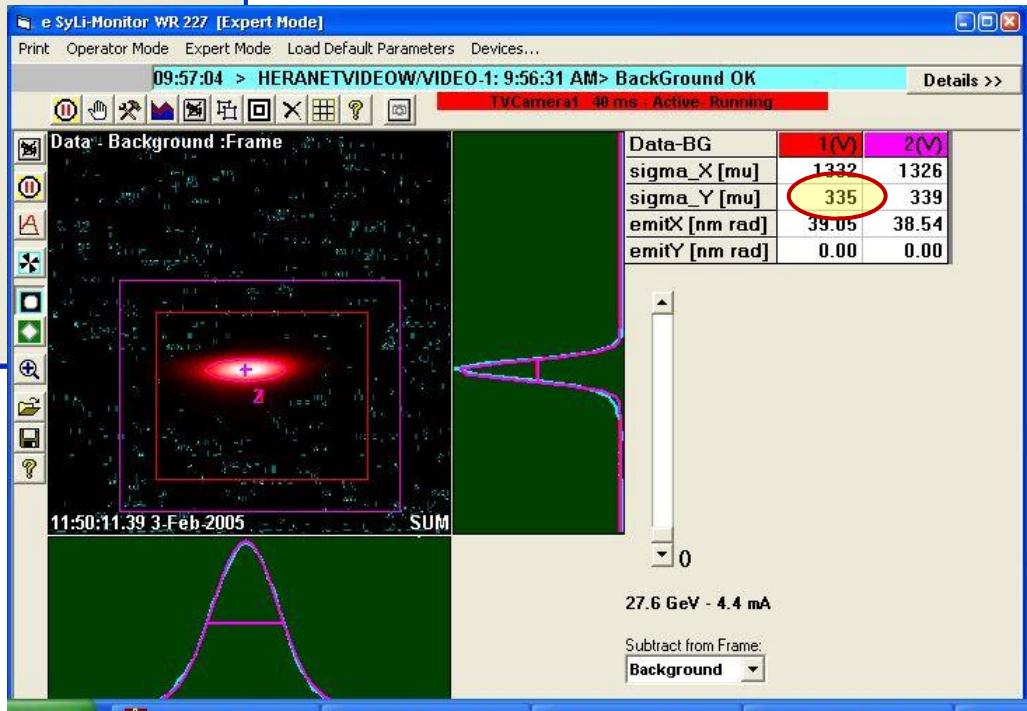
- » monochromatic measurement
→ λ small
- » polarization selection
→ σ -polarization

Polarization Dependency

- screen shot: HERAe @ DESY



➤ σ polarization



➤ π polarization

Depth of Field and Curvature

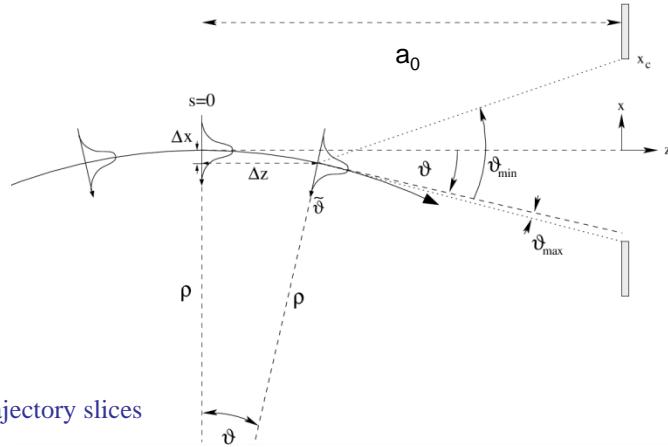
- intensity summation along particle trajectory

- emission angles (ϑ, Ψ) normal distributed in source plane
- beam sizes (σ_x, σ_y) normal distributed in source plane
- trajectory element: $ds = \rho d\vartheta$

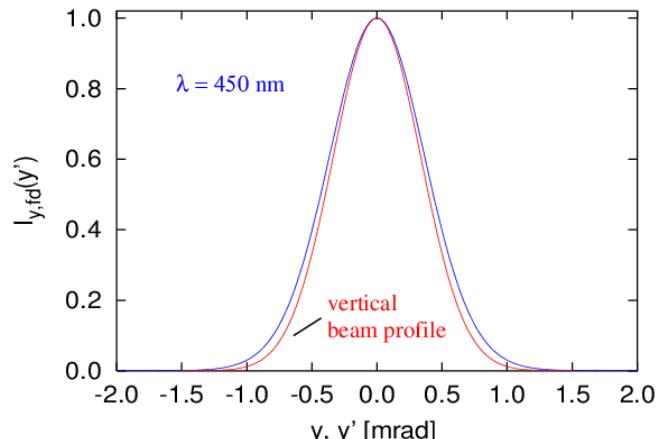
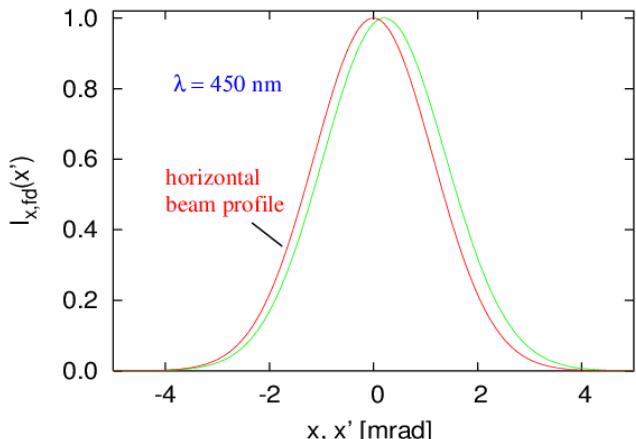
$$I_{y,dof}(y') = I_0 \int_{-\vartheta_{lim}}^{+\vartheta_{lim}} d\vartheta \frac{a_0 \rho h(\vartheta)}{b_0 \sqrt{2\pi} \sqrt{\sigma_y^2 + (\rho \vartheta \sigma_\Psi)^2}} \cdot \exp\left(-\frac{(a_0 y')^2}{2b_0^2 \{\sigma_y^2 + (\rho \vartheta \sigma_\Psi)^2\}}\right)$$

$$I_{x,dof}(x') = I_0 \int_{-\vartheta_{lim}}^{+\vartheta_{lim}} d\vartheta \frac{a_0 \rho h(\vartheta)}{b_0 \sqrt{2\pi} \sqrt{\sigma_x^2 + (\rho \vartheta \sigma_g)^2}} \cdot \exp\left(-\frac{a_0^2 (x' - \rho \vartheta^2)^2}{2b_0^2 \{\sigma_x^2 + (\rho \vartheta \sigma_g)^2\}}\right)$$

- each slice shifted by $\Delta x = \rho \vartheta^2$ against position at $s=0$ (curvature of trajectory)
- weight function $h(\vartheta)$: accounts for amount of light extracted by mirror from different trajectory slices



- example: HERAe @ DESY



Synchrotron Radiation Field

- second representation: starting point again **Liénard-Wiechert potentials**

$$\varphi(t) = \left(\frac{-e}{R(1 - \hat{n} \cdot \vec{\beta})} \right)_\tau, \quad \vec{A}(t) = \left(\frac{-e \vec{\beta}}{R(1 - \hat{n} \cdot \vec{\beta})} \right)_\tau$$

- Fourier transform of potentials:

$$\varphi(\omega) = -e \int_{-\infty}^{+\infty} d\tau \frac{1}{R(\tau)} e^{i\omega(\tau+R(\tau)/c)}, \quad \vec{A}(\omega) = -e \int_{-\infty}^{+\infty} d\tau \frac{\vec{\beta}(\tau)}{R(\tau)} e^{i\omega(\tau+R(\tau)/c)}$$

- field derivation:

$$\vec{E}(\omega) = -\frac{i\omega e}{c} \int_{-\infty}^{+\infty} d\tau \left[\frac{(\vec{\beta} - \hat{n})}{R(\tau)} - \frac{ic}{\omega} \frac{\hat{n}}{R^2(\tau)} \right] e^{i\omega(\tau+R(\tau)/c)}$$

with $\tau = \int_0^z \frac{dz}{c\beta_z(z)} = \frac{1}{c} \int_0^z dz \left[1 + \frac{1 + (\gamma\beta_x)^2 + (\gamma\beta_y)^2}{2\gamma^2} \right]$

- knowledge of arbitrary particle orbit: $\vec{E}(\omega)$ determined
- arbitrary magnetic field configuration: determines orbit and $\vec{E}(\omega)$

- comments:
 - (i) exact field description → numerical near field calculation
 - (ii) includes depth of field & curvature → no additional contributions, only field propagation
 - (iii) free codes available → easy field calculation, even field propagation!

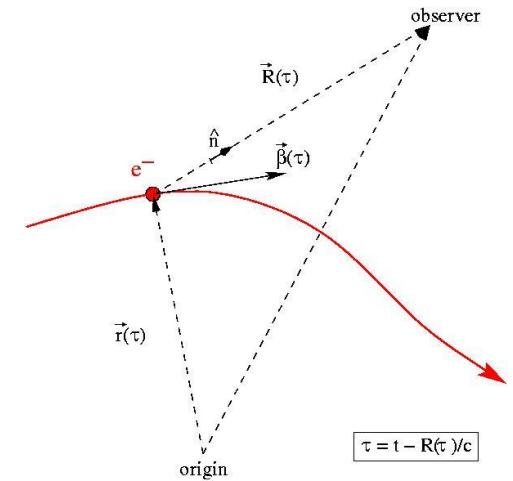
SRW: <http://www.esrf.eu/Accelerators/Groups/InsertionDevices/Software/SRW>

(Chubar & Elleaume, ESRF)

Spectra: <http://radian.rimma.riken.go.jp//spectra/index.html>

(Tanaka & Kitamura, SPring8)

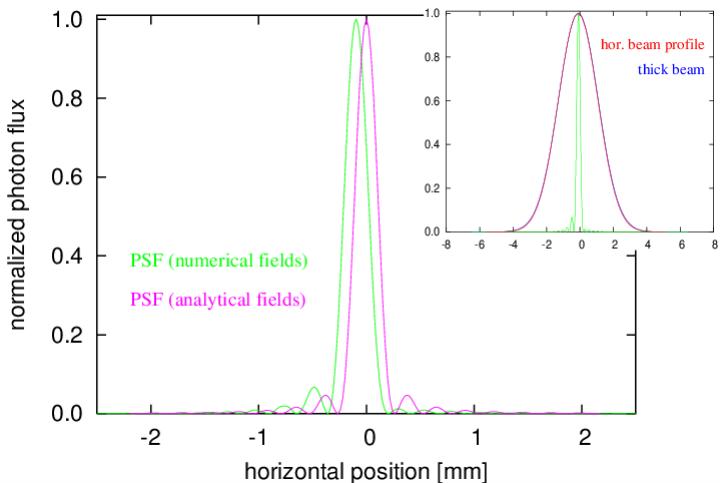
O.Chubar and P.Elleaume,
Proc. EPAC96, Stockholm (1996) 1177



Comparison

- resolution broadening effects for the HERAe emittance monitor

- calculation of spatial SR intensity distribution including beam emittance
- quadratical subtraction of beam size ($\sigma_x = 1175 \mu\text{m}$, $\sigma_y = 260 \mu\text{m}$)



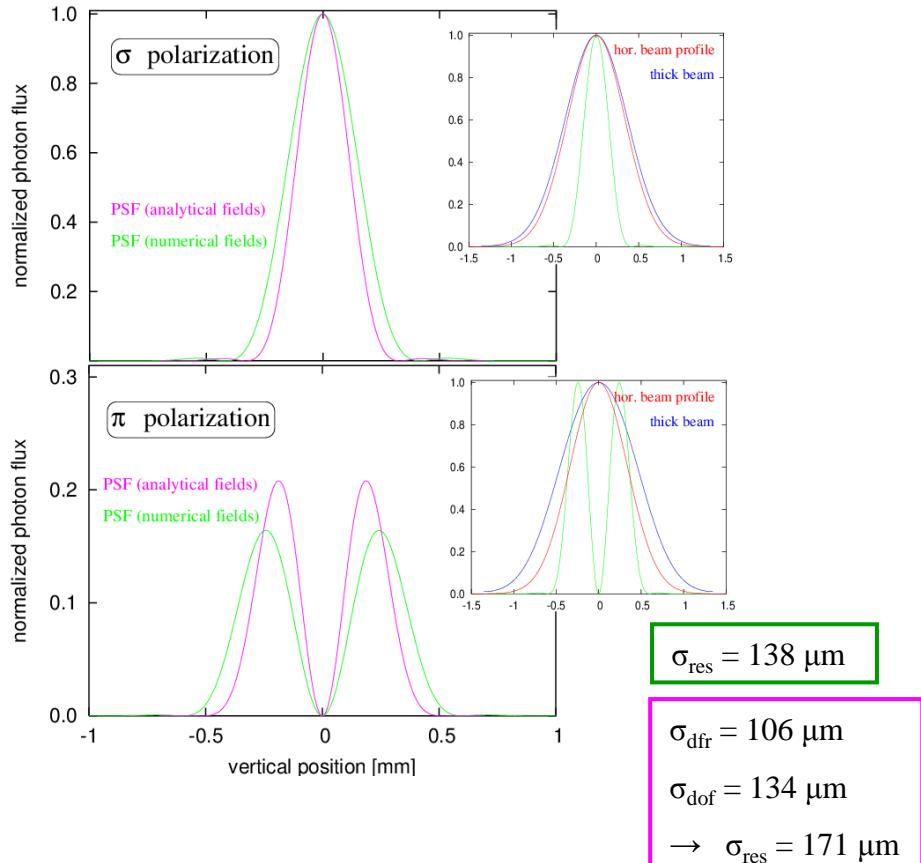
- near field description:
- analytical description:

$$\sigma_{\text{res}} = 203 \mu\text{m}$$

$$\sigma_{\text{dfr}} = 188 \mu\text{m}$$

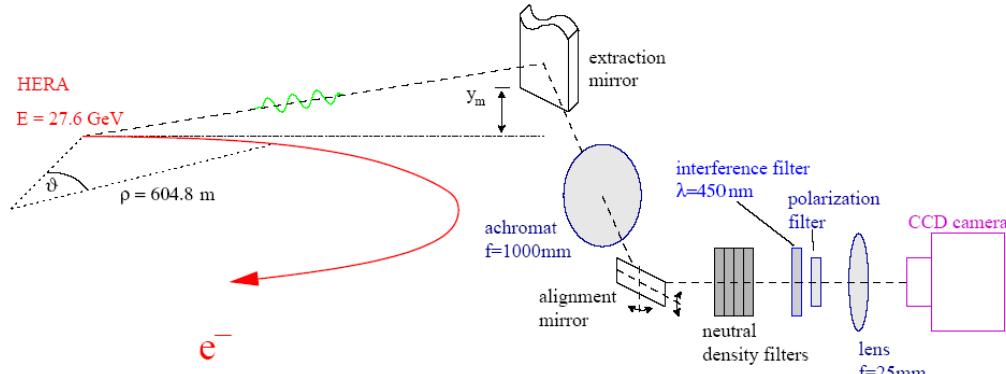
$$\sigma_{\text{dof}} = 275 \mu\text{m}$$

$$\rightarrow \sigma_{\text{res}} = 333 \mu\text{m}$$



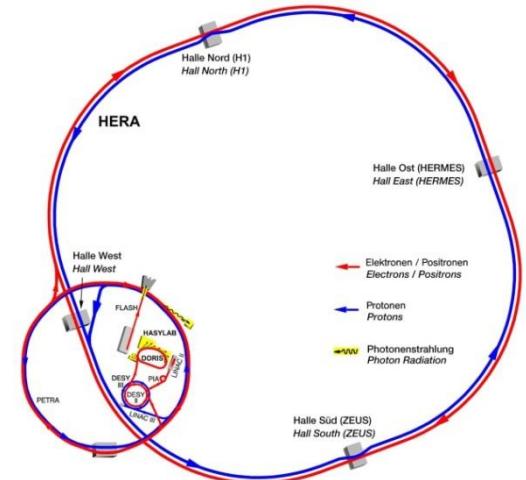
SyLi Monitor for HERAe @ DESY

- monitor setup



- HERA @ DESY

27.6 GeV $e^+(e^-)$ / 920 GeV p

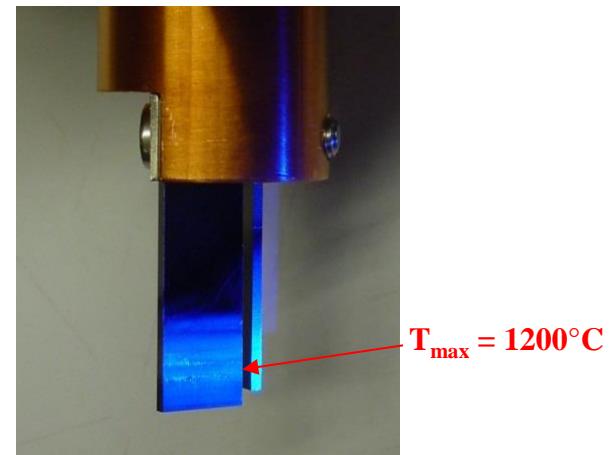


- HERA e beam size: $\sigma_{\text{hor}} = 1175 \mu\text{m}$, $\sigma_{\text{vert}} = 260 \mu\text{m}$

→ resolution with **optical SR** sufficient

- problem:** **heat load on extraction mirror** (X-ray part of SR)

- material with low absorption coefficient (Be)
- cooling of extraction mirror
- **not sufficient to prevent image distortion...**



SyLi Monitor for HERAe @ DESY

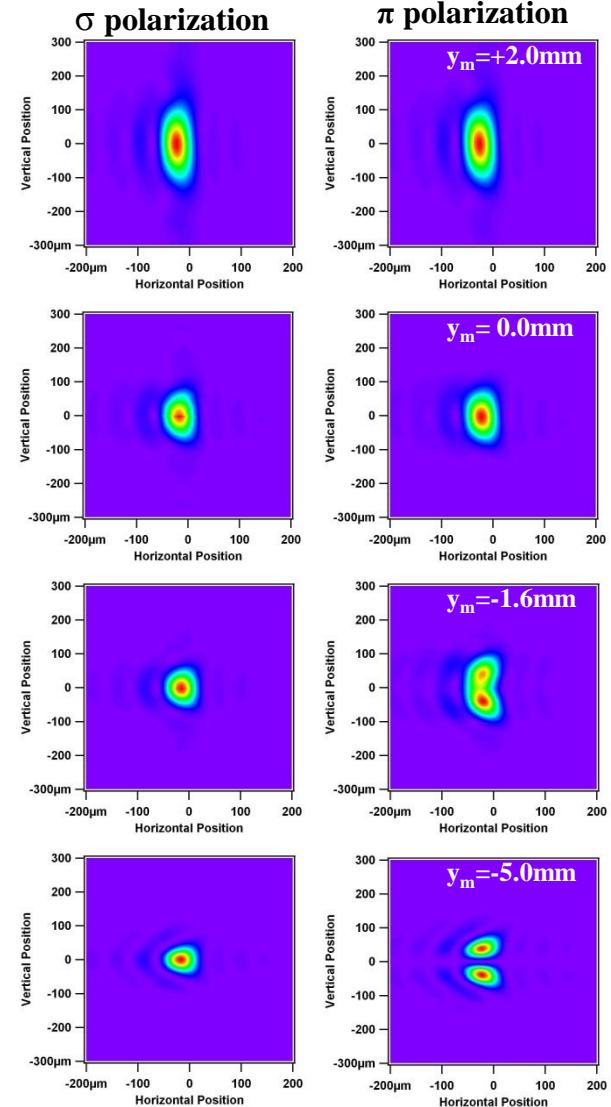
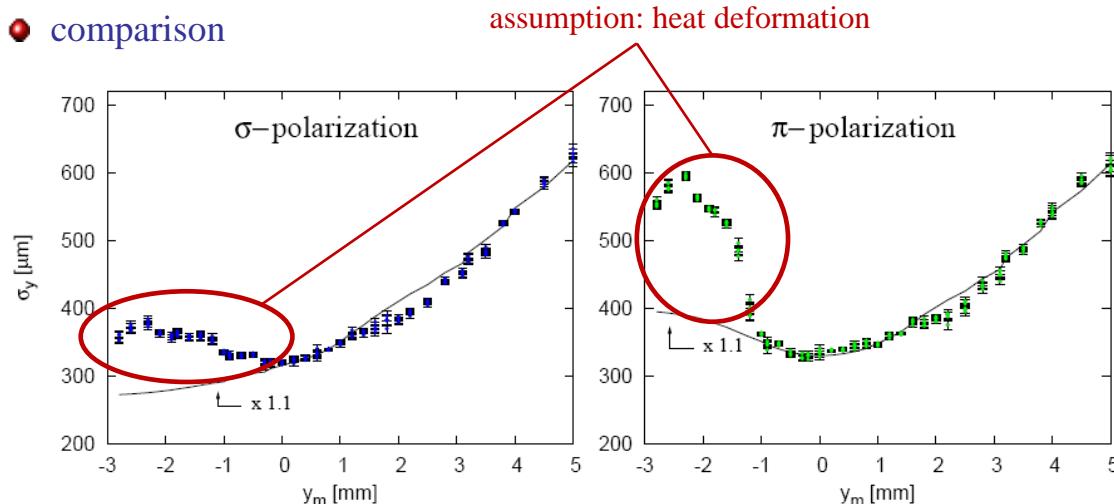
• solution: observation out of orbit plane

- move mirror above orbit plane
 - X-ray part of SR is emitted close to beam axis and will not hit the mirror surface
 - optical SR components have larger angular distribution and are reflected at mirror surface
- ▷ influence on monitor resolution ?

• resolution calculation (for single particle)

- numerical near field calculation with SRW code

• comparison



G. Kube et al., Proc. of DIPAC05, Lyon, France (2005) 202

Proton Synchrotron Radiation

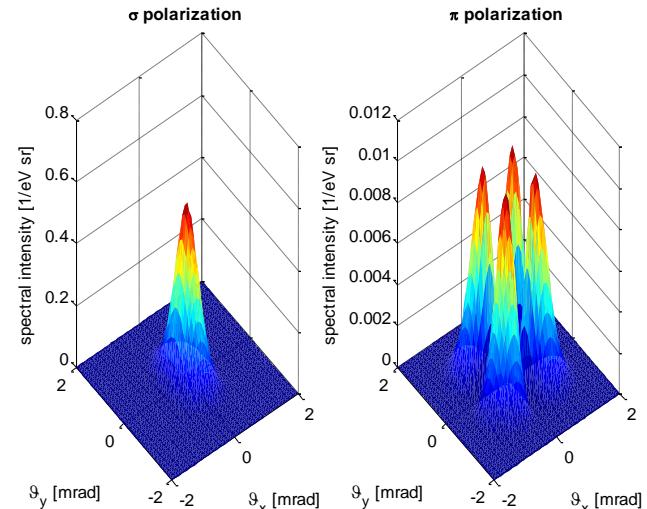
analytical approach

R. Coisson, Phys. Rev. A20 (1979), pp.524-528

► fringe field parametrization: $B(z) = \frac{B_0}{2} (1 + \text{erf}(z/L))$

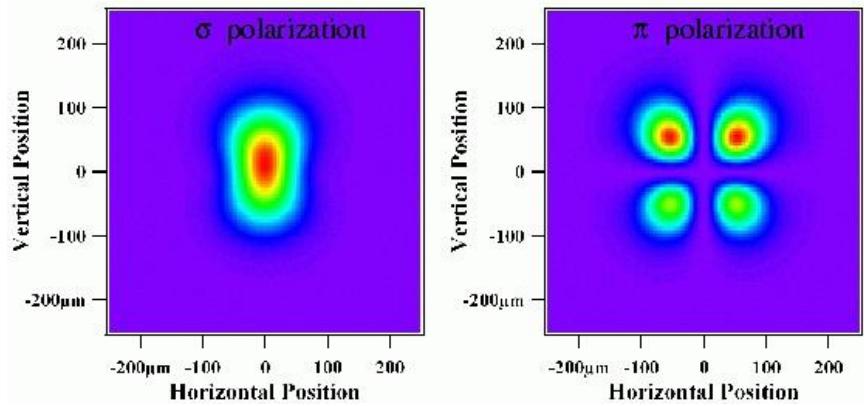
$$\frac{d^2N}{d\Omega d(\hbar\omega)} = \frac{8\alpha}{\pi^2} \mu_N^2 \frac{\gamma^6}{(\hbar\omega)^3} B_0^2 f^2 \exp \left[-2 \left\{ \frac{L(1+\vartheta^2\gamma^2)}{4\gamma^2\hbar c} \hbar\omega \right\}^2 \right]$$

$$f^2 = f_x^2 + f_y^2 \quad \text{with} \quad f_x = \frac{\gamma^2(\vartheta_x^2 + \vartheta_y^2) - 1}{(1 + \vartheta^2\gamma^2)^3}, \quad f_y = \frac{2\gamma^2\vartheta_x\vartheta_y}{(1 + \vartheta^2\gamma^2)^3}.$$



numerical approach

- el.field fully determined via particle orbit
- takes into account exact field distribution
- calculation based on SRW code



Summary and Conclusion

• resolution in terms of geometrical optics

- good resolution: λ small
- balance acceptance angle ϑ : σ_{dfr} vs. σ_{dof}

J.A. Clarke, Proc. EPAC94, London (1994) 1643

R. Littauer, Proc. 2nd SLAC Summer School (1982) 902

A. Hofmann and K.W. Robinson, IEEE Trans.Nucl.Sci.**18** (1971) 937

• resolution based on analytical approach

- good vertical resolution: σ polarization
- calculation of broadened beam profiles in image plane
- optimization of ϑ possible

A. Hofmann and F. Méot, Nucl. Instr. Meth.**203** (1982) 483

A. Andersson and J. Tagger, Nucl. Instr. Meth. **A364** (1995) 4

G. Kube et al., Proc. BIW2004, AIP Conf. Proc. **732** (2004) 350

A. Hofmann, CAS 1996, 2003, ...

• numerical near field calculations

- detailed resolution information
- curvature and depth of field included
 - disturbed wave front (no more spherical)
- possible for arbitrary magnetic configurations

O. Chubar and P. Elleaume, Proc. EPAC96, Stockholm (1996) 1177

T. Tanaka and H. Kitamura, J. Synchrotron Rad. **8** (2001) 1221

G. Kube et al., Proc. of DIPAC05, Lyon, France (2005) 202

• analytical approach including depth of field/curvature

- based on paraxial Green's function
- other
 - disturbed wave front characterized by phase factor

G. Geloni et al., DESY preprint 05-032

O. Chubar et al., Nucl. Instr. Meth. **A435** (1999) 495

R.A. Bosch, Nucl. Instr. Meth. **A431** (1999) 320