



LHC CRAB Cavity Measurements Meeting

Integration of the 4-Rod LHC CRAB cavity
for RF measurements at 4.5K in SM18

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▶ Until now, two test environments are foreseen:

- ▶ SM18 - test cryostat;
- ▶ SPS;

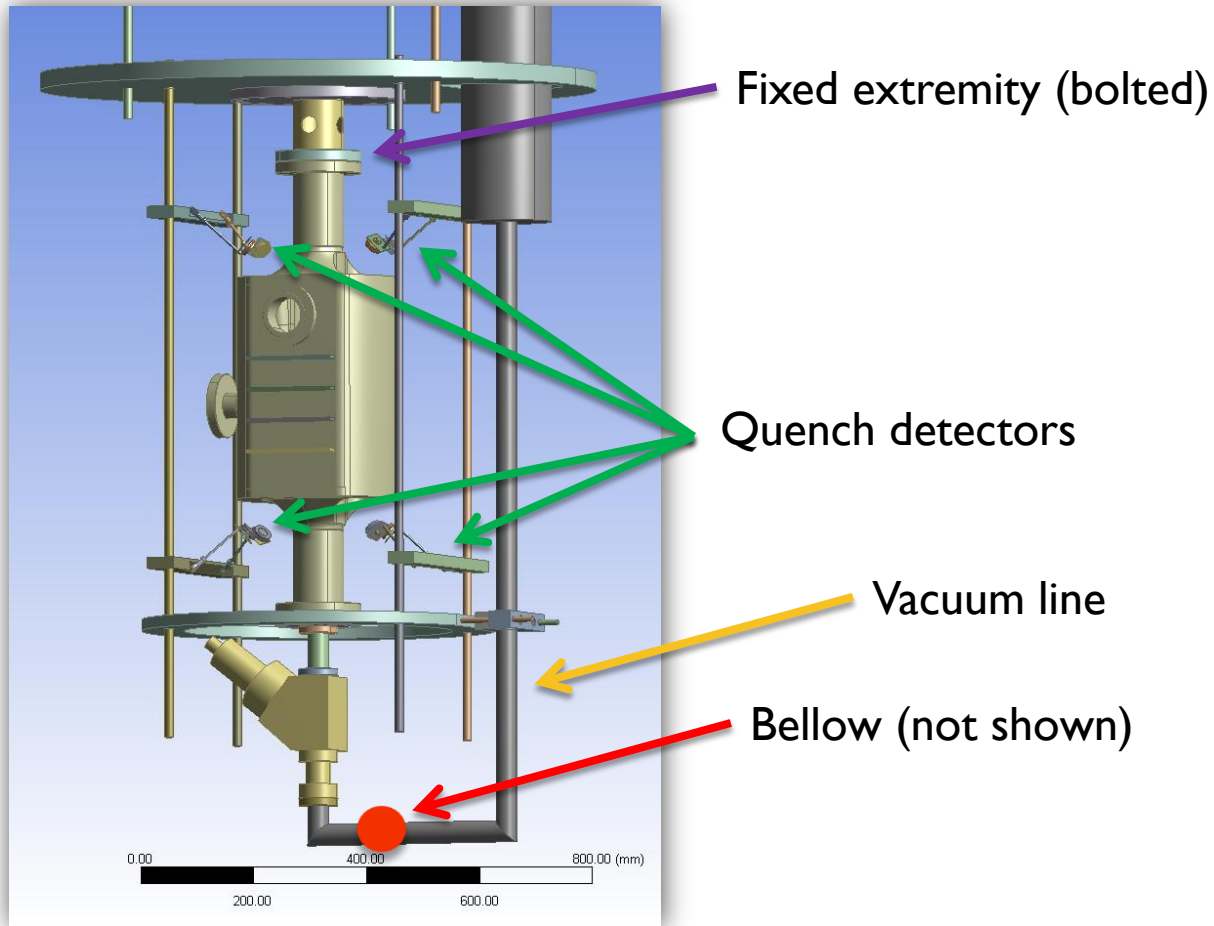
All mechanical calculations done until now assess only this test environment

Table 1 – Pressure conditions for each test environment

<i>Test environment</i>	<i>Safety valve set-point</i>	<i>Maximum allowable pressure (PS)</i>	<i>Test pressure (1.43xPS)</i>
SM18 Test cryostat	1.5bar±0.15 *(abs)	1.5bar (abs)	2.1 bar (abs)
SPS	1.8bar±0.15* (abs)	1.8bar (abs)	2.6 bar (abs)

*This tolerance for the set pressure of safety valves is defined by EN ISO 4126-1

Cryostat for 4.5K RF Measurements in SMI8 -Design & Materials-



Integration of prototype
cavity for test in SM18

▶ **Materials:**

- ▶ Cavity body: unalloyed Niobium
- ▶ Connections: AISI 300-Series Stainless Steel (flanges in AISI 316LN)

Typical physical and mechanical properties:

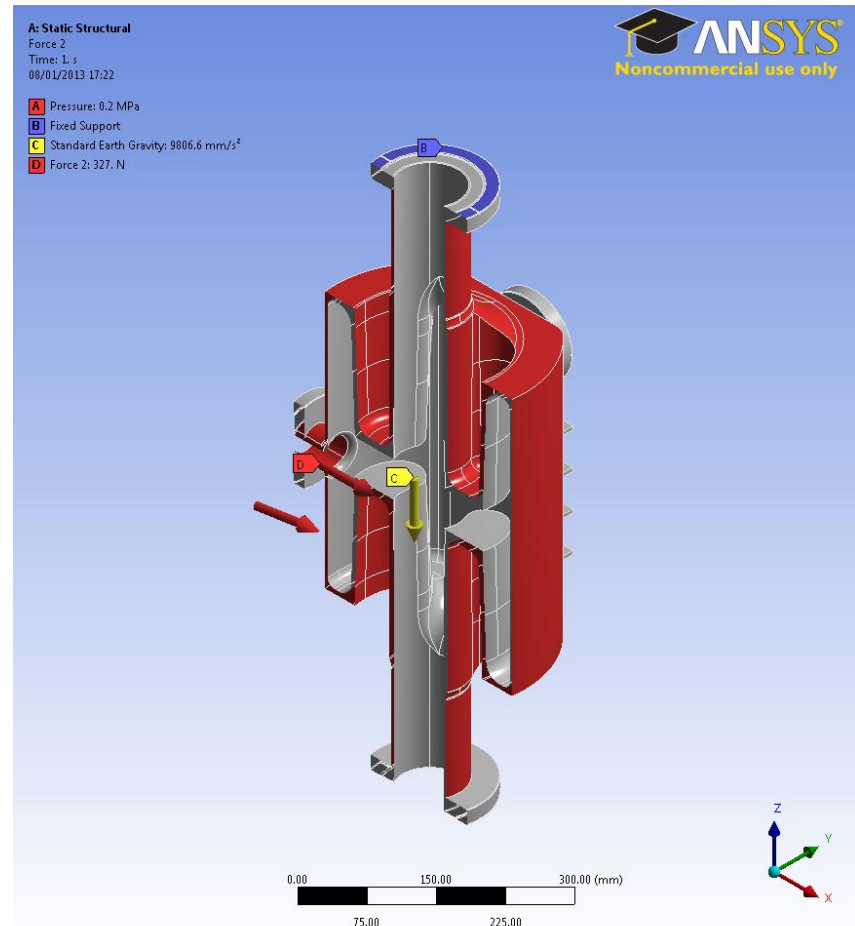
<i>Physical and mechanical properties of unalloyed Niobium at room temperature*</i> <i>-Reactor grade Type 1, UNS R04200-</i>				
Density (kg/m ³)	Young's modulus (GPa)	Poisson's ratio	Yield strength RP _{0.2} (MPa)	Max allowable stress RP _{0.2} /SF (MPa)
8600	100	0.4	75	70
<i>Stainless steel AISI 316LN (1.4429 – round bar)**</i>				
8000	200	0.3	RP _{1.0} =315MPa	RP _{1.0} /SF=300MPa

*Data from GRANTA'S CES Selector 2012 Database

**Data from EN 10088-1 Annex A, EN 13155-3 Annex O, EN 10021:2006, EN 10088-3:2005

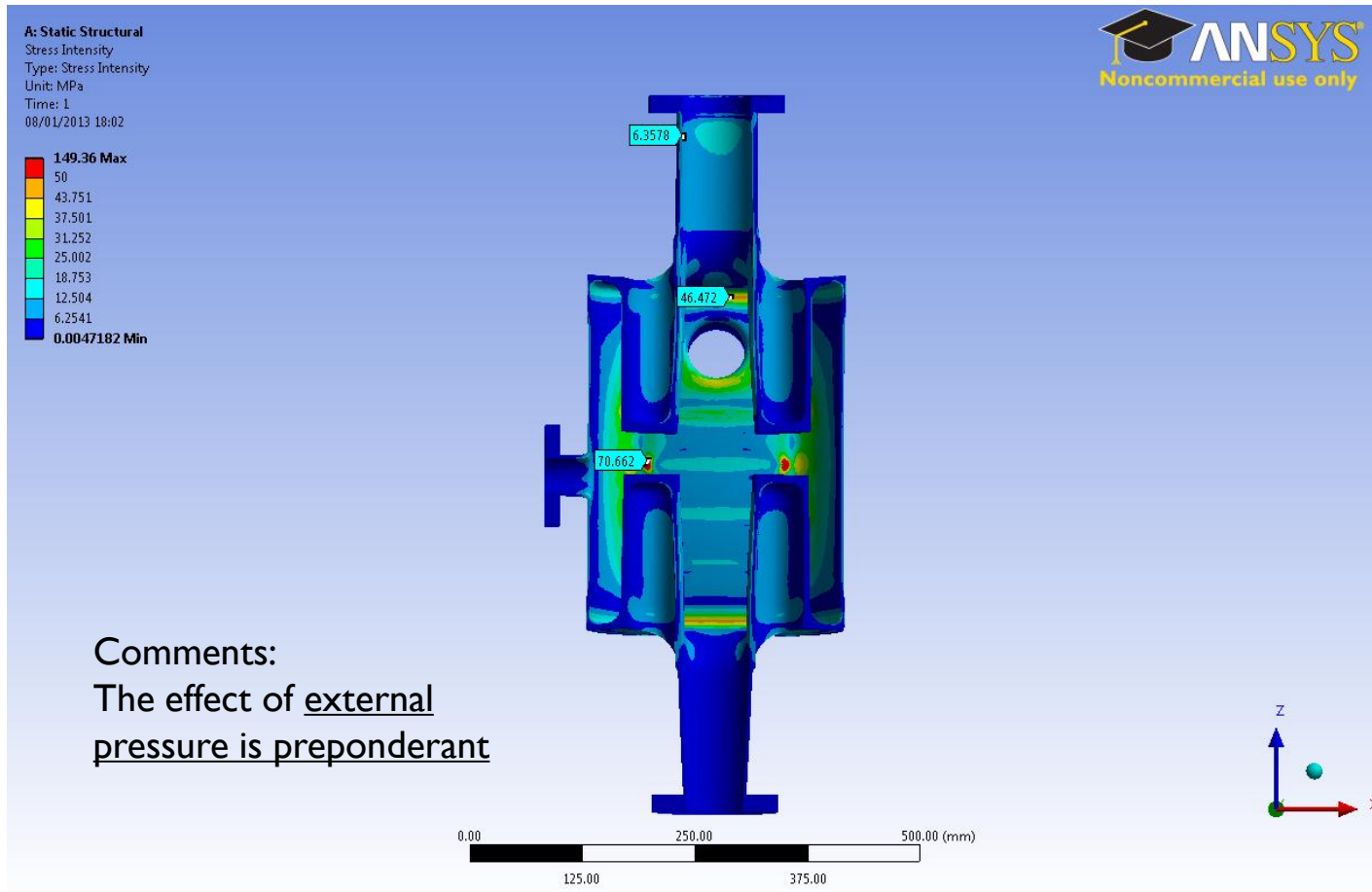
Cryostat for 4.5K RF Measurements in SMI8 -Calculations-

- ▶ **Assumptions:**
 - ▶ Stainless Steel (SS) flanges perfectly bonded to cavity body
- ▶ **Boundary conditions:**
 - ▶ External pressure: 0.2MPa
 - ▶ Self-weight
 - ▶ Hold by top flange
 - ▶ Compensation of non-symmetry with external force of 327N (D)
- ▶ **Material model:**
 - ▶ Elastic, Isotropic (see slide 6)



► Results:

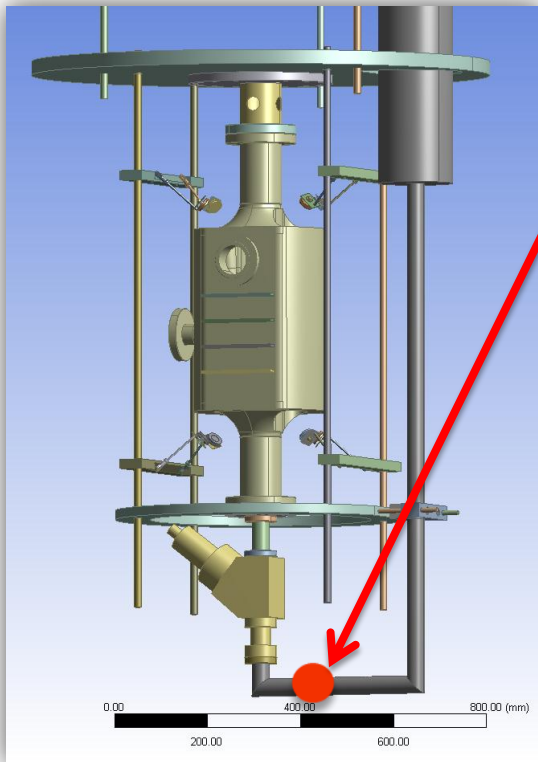
► Stress intensity plot



Cryostat for 4.5K RF Measurements in SMI8 -Calculations-

Additional effort: bellow on vacuum line

- ▶ Additional effort: bellow on vacuum line



Bellow (not shown)

Integration of prototype cavity for test in SM18

Analytical calculations:

CRYOSTAT P1 TESTER CAVITE CRAB/LHC

3/10/2012

$$\Delta P = 2 \text{ bar} \quad \text{Soufflet: 2N40} \quad F = \frac{\pi \times 40^2}{4} \times 0,2 = \underline{250N}$$

$$\text{Distance entre brides} \approx 800 \text{ mm} \rightarrow M = \underline{200 N.m}$$

$$\text{Section tube: } \left\{ \begin{array}{l} \phi_{\text{ext}} = 90 \text{ mm} \\ \phi_{\text{int}} = 84 \text{ mm} \end{array} \right. \rightarrow c = \phi_{\text{ext}}/2 = 45 \text{ mm}$$

$$I = \frac{1}{4} \pi (a_{\text{ext}}^4 - a_{\text{int}}^4) = 776,7 \times 10^3 \text{ mm}^4$$

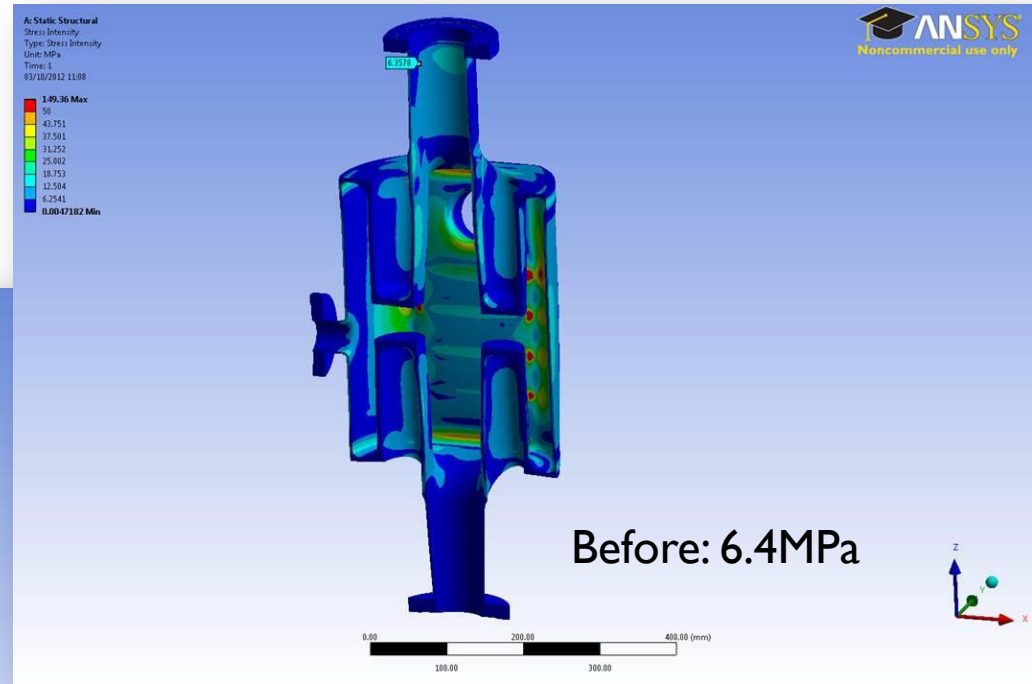
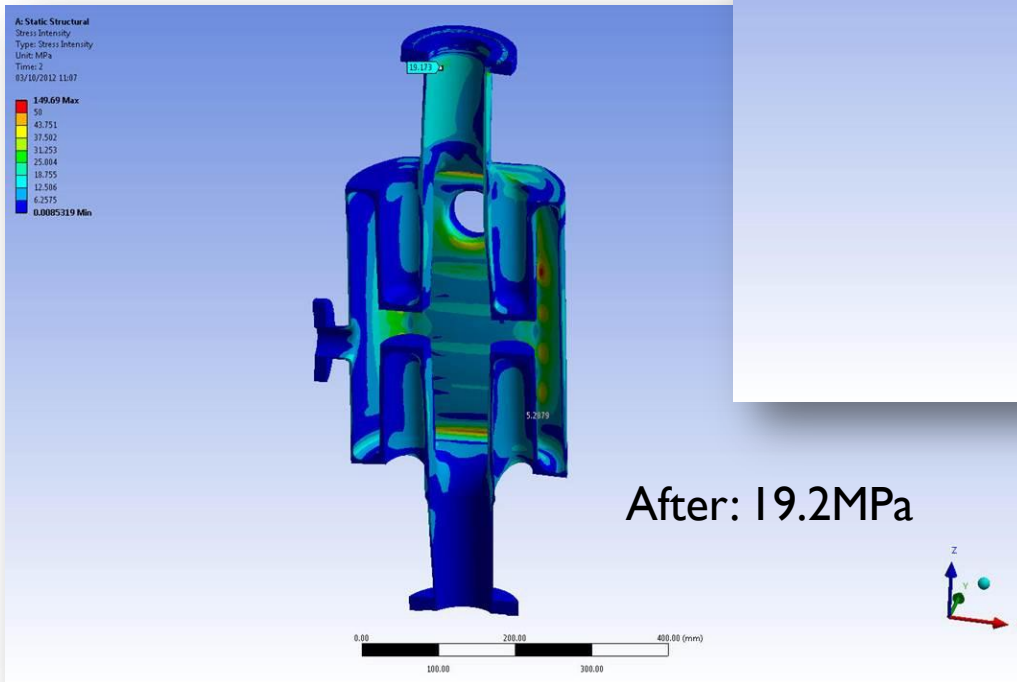
$$\sigma_{\text{sur}} = \frac{M \times c}{I} \rightarrow \sigma_{\text{sur}} = \frac{200 \times 10^3 \text{ N.m} \times 45 \text{ mm}}{776,7 \times 10^3 \text{ mm}^4} = \underline{12 \text{ MPa}}$$

$$\sigma_{\text{max}} = \frac{250}{\frac{\pi}{4} (90^2 - 84^2)} = \underline{92 \text{ MPa}}$$

Normal stress increase due to isolated effort: 12MPa

- ▶ Additional effort: bellow on vacuum line

Validation with a FE model:



Effect due to isolated effort:
12.8MPa (validates analytical result)

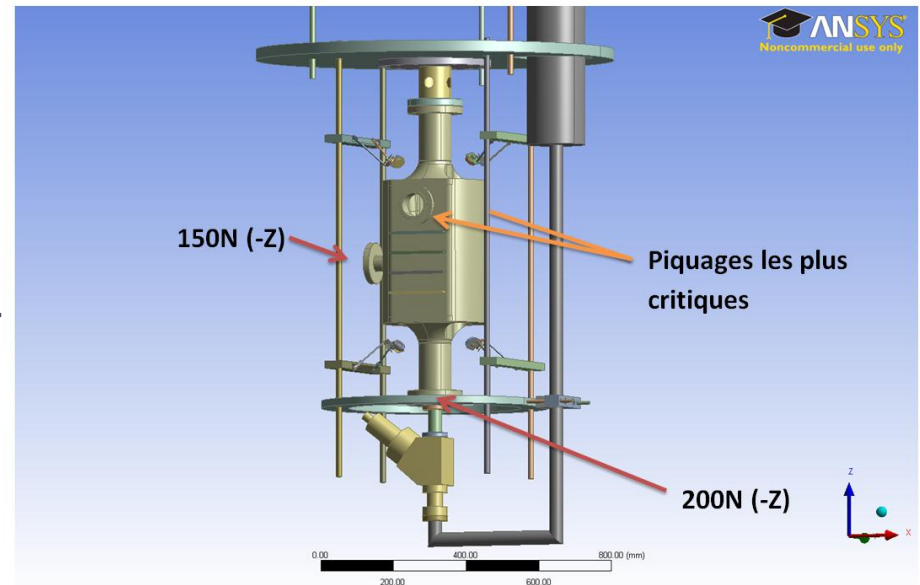
Comments

▶ Comments

- ▶ The effect of the external pressure of 0.2MPa is preponderant for the structural strength;
- ▶ The cavity is expected to withstand the foreseen integration design;
- ▶ Additionally, it is also expected to withstand the additional force coming from the bellow in series with the vacuum line;

- ▶ Moreover, this design was found out to have enough strength to tolerate the following additional loads->

Final note: natural vibration modes can be triggered at low frequency...

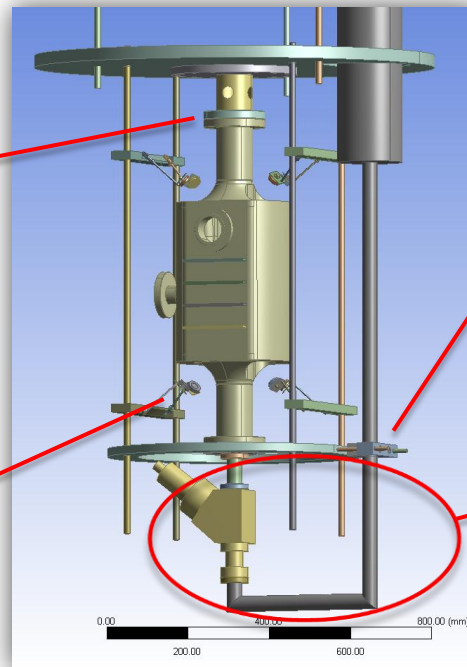


Limitations and modifications being studied

- ▶ The following limitations were pointed out by the first tests:

Coupled load bearing / leak tightness interface:
Bending efforts not compensated by the copper joint may have been in the origin of the observed leak...

Insufficient support for acoustic detectors?



Over-constrained system not allowing significant adjustment

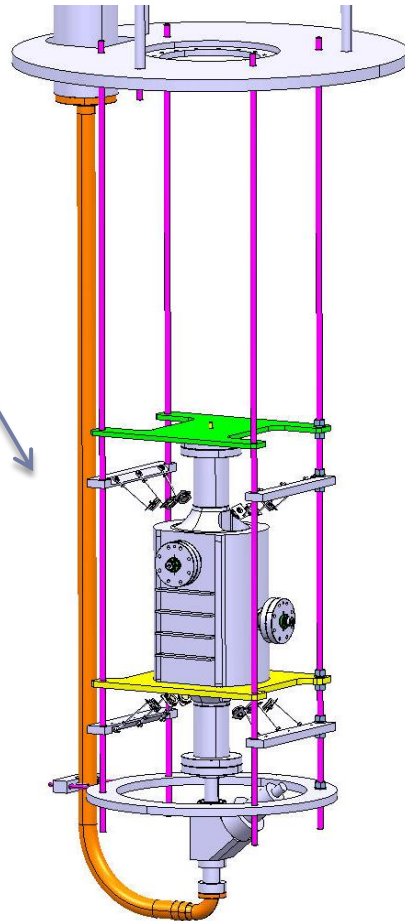
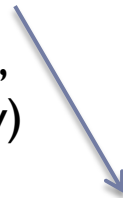
The position of the vacuum line coming from the top didn't allow to position correctly the vacuum valve: the in-line bellow was installed with significant deformation in order to compensate this positioning defect

Integration of prototype cavity for test in SM18

Modifications being studied

- ▶ The following upgrades are being studied:

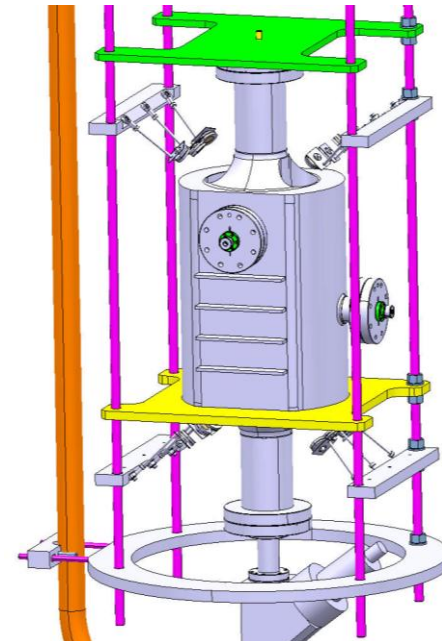
Vacuum supplied through long metallic flexible (minimizes efforts, increases versatility)



Next:
Do acoustic detectors holding system need improvements?

Support system:

- Decoupling of structural/leak tightness boundaries;
- Fixed-sliding extremities allowing free expansion/contraction





Thank you for your attention