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CLIC Main Beam quadrupole active pre-alignment based on cam movers

# Main Beam Quadrupole (MB <br> Quad) pre-alignment requirements 

Pre-alignment within $17 \mu \mathrm{~m}$ in sliding windows of 200 m
$\rightarrow$ active pre-alignment on single MB Quads
within $1 \mu \mathrm{~m} / 100 \mu \mathrm{rad}$ in 5 d.o.f.
(stroke +/- 3 mm )
Provide rigid support for the nanostabilization system

High first eigenfrequency (preferably above 100 Hz )

## Approach: cam movers

Originally developed at SLAC and since then successfully deployed in several synchrotrons and light sources
Transforms camshaft rotation to translation Very high movement resolution can be achieved


## Cam mover prototype

Based on PSI design
1 d.o.f. tests verified submicron movement resolution and repeatability
Stroke +/- 5 mm


## Cam mover prototype



SKF 22209 E
(a)


IKO NAST 45 ZZUU
(b)

(c)

| Configuration No. | Bearing type | Bearing reference | Housing <br> type |
| :--- | :--- | :--- | :--- |
| 1 | Spherical roller bearing | SKF 22209 E | Cylindrical |
| 2 | Roller follower | IKO NAST 45 ZZUU | Cylindrical |
| 3 | Roller follower | IKO NAST 45 ZZUUR | Spherical |



## Cam mover prototype - precision

|  | $0-9$ Msteps | $1-8$ Msteps |
| :--- | :--- | :--- |
| Configuration 1 | $1.0 \mu \mathrm{~m}$ | $0.33 \mu \mathrm{~m}$ |
| Configuration 2 | $0.38 \mu \mathrm{~m}$ | $0.18 \mu \mathrm{~m}$ |
| Configuration 3 | $0.23 \mu \mathrm{~m}$ | $0.31 \mu \mathrm{~m}$ |



## MB Quad types

CLIC will have 4 types of MB Quads
At least two different cam mover types will be needed


Estimated masses (quadrupole + stabilization system)

Type 1: 300 kg
Type 4: 800 kg

## Type 4 cam mover

Manufacturer: ZTS VVU Kosice from Slovakia
Design was optimized in an iterative process R. Leuxe, F. Lackner, ZTS VVU Kosice

6 cams were manufactured, then tested and calibrated in the 1 d.o.f. mock-up


## Type 4 cam mover

Combination of a worm drive ( $\mathrm{i}=60$ ) and a Spinea reduction gear ( $\mathrm{i}=85$ )

High movement resolution ( $<0.031 \mu \mathrm{~m}$ )
Self-locking (worm drive)
Negligible backlash (Spinea)
High precision rotary absolute encoder
Keeps track of orientation in case of power cut Eliminates the powertrain's backlash and hysteresis

## Type 4 cam mover

ZTS VVU Kosice
Two bearing types were chosen for further testing So far only the roller follower with spherical housing (point contact) has been thoroughly tested


## 5 d.o.f. mock-up for type 4

5 d.o.f. mock-up was built in the old ISR tunnel at CERN
5 cam movers with appropriate interfaces can handle the 5 d.o.f. movements

All except longitudinal movement (blocked)


## 5 d.o.f. mock-up for type 4



## 5 d.o.f. mock-up for type 4



## 5 d.o.f. mock-up for type 4

Chassis orientation is measured using a stretched wire, 2 WPS (W1, W4) and an inclinometer (M-T)
Cam reference angles are calculated based on Dr. Andreas Streun's (PSI) formulas


## 5 d.o.f. mock-up for type 4

## User inputs

 dx and dy in points AXE-1 and AXE-2 as well as roll Transformed to point M offsets (input to Streun's algorithms) Measured orientationInclinometer gives roll directly
AXE-1 and AXE-2 offsets calculated based on W1 and W4 offsets roll
Re-adjustment error (movement accuracy) is the difference between user inputs and measured orientation


## 5 d.o.f. results for type 4

Positioning repeatability below $5 \mu \mathrm{~m}$ (AXE-1 and AXE-2 offsets) and below 5 rad (roll) Movement accuracy (with respect to a reference position)
$10-20 \mu \mathrm{~m} / \mu \mathrm{rad}$ for simple movements Up to $100 \mu \mathrm{~m} / \mu \mathrm{rad}$ for complex movements

## 5 d.o.f. results for type 4



## 5 d.o.f. control - iterative method

Clearly the accuracy requirement cannot be met with one movement so an iterative method was applied
Search position until the chassis is within $1 \mu \mathrm{~m} / 5 \mu \mathrm{rad}$ from reference position $3-5$ iterations without load
$5-10$ iterations with load

## 5 d.o.f. results for type 4

CERN Mechanical Measurement Lab (ENMME) performed the experimental modal analysis of the 5 d.o.f. mock-up

The lowest natural frequency was found at 15 Hz which is lower than expected
This might be due to the support under cam movers $\rightarrow$ small test setup to verify this will be built shortly (waiting for delivery of parts)

## Type 1 cam mover

Was developed at CERN
Very challenging to meet all requirements simultaneously

Space restriction (no space for two gearboxes)
Enough torque ( 10 - 20 Nm)
Resolution ( $<0.5 \mu \mathrm{~m}$ )
Self-locking
Negligible backlash

## Type 1 cam mover

A suitable set of components was finally found (resolution $<0.35 \mu \mathrm{~m}$ )
Oriental Motor high resolution stepper motor
0.36\%/step

Davall Gears custom Spiradrive gearbox
i = 90
Self-locking
Negligible backlash

R. Leuxe

## Type 1 cam mover

The first Spiradrive ${ }^{\circledR}$ series is equipped with high tensile brass pinion to have negligible backlash

The pinion broke down while the first cam mover was under 1 d.o.f. tests with 100 kg additional weight
Remaining gearboxes should
be tested with reduced load in
1 d.o.f. and with full load in
5 d.o.f. to finally determine if they can be used

## Type 1 cam mover

A new series of Spiradrive ${ }^{\circledR}$ gearboxes, equipped with steel pinions, was manufactured

Better wear and torque resistance but introduces up to 5 arc minutes of backlash $\rightarrow$ requires more complex positioning algorithms

## Next steps - type 4

5 d.o.f. tests using different bearing type in cam movers

Spherical roller bearing with cylindrical housing instead of a roller follower with spherical housing
$\rightarrow$ Line contact instead of point contact Modifications and calibration on-going

- More work needed than foreseen

5 d.o.f. mock-up can be re-built when the cam movers are ready ( $\sim 2-3$ weeks)
Wearing and temperature tests

## Next steps - type 4

Integration with the nano-stabilization system

Ready once 5 d.o.f. tests have been repeated using spherical roller bearings Improvement of control software and positioning algorithms

Cam mover control software unreliable and inaccessible $\rightarrow$ mock-up software needs lots of error detection and recovery functions

## Next steps - type 1

Assembly of 10 cam movers
5 with steel pinion (priority) and 5 with brass pinion
1 d.o.f. tests and calibration
5 d.o.f. mock-up
Finalize design and build in ISR
Adapt positioning algorithms to new dimensions and backlash
Adapt software to new hardware
Cam mover design optimization (FEA)

## Long term (all types)

Replace expensive absolute encoders with a simpler system to recover position data
E.g. high precision proximity sensors (suggested by ZTS VVU Kosice)

Link MB quad coordinate system to CLIC coordinate system $\rightarrow$ absolute positioning

## Long term (all types)

Study the possibility to get positioning feedback directly from alignment sensors (no need for iterations)

Not possible with type 4 (limited functionality of cam control software)
Fast acquisition racks already exist at the CERN Survey section BUT
WPS reading stabilizes only after ~ 1s after the end of a movement

## Long term (all types)

Development of a generic 5 d.o.f. calibration process which can handle all 4 types of MB quads and their associated alignment sensors and cam movers

Before the calibration process itself can be defined, several studies have to be finished

- Support under cam movers
- Control strategy (mathematical model, feedback, trajectory planning...)
- Alignment strategy


## Long term

Cam mover based alignment in the MDI region

## Questions?

## Credits

Pre-alignment team
Michail Anastasopoulos Mathieu Duquenne
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